

SEWER CAPACITY STUDY

FOR

COMPTON COLLEGE

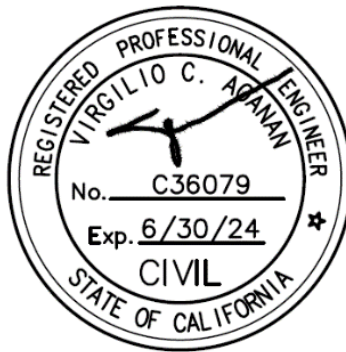
1111 E. ARTESIA BLVD.,
COMPTON, CA 90221

February 13, 2024

PREPARED FOR:

HPI ARCHITECTURE
115 22ND STREET,
NEWPORT BEACH, CA 92663

PREPARED BY:



VIRGIL C. AOANAN, P.E., S.E., QSD

Los Angeles

1041 S. Garfield Ave., Suite 210, Alhambra, CA 91801
Tel: 323-729-6098 ■ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ■ Fax: 949-679-9370
www.vcaeng.com

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1. PROJECT DESCRIPTION AND APPROACH

This sewer capacity study is prepared by VCA Engineers, Inc. to examine the existing sanitary sewer system that will have an impact on the proposed student housing building located within the campus of Compton College. The proposed housing buildings are located at 1111 E. Artesia Boulevard, CA 90221, in the northern part of the campus.

The project involves the Phase 1 construction of two separate three (3) story student housing buildings with sewer demands of 686.5 DFU (345 GPM) for Wing A with four plumbing laterals and 421.5 DFU (211 GPM) for Wing B with one plumbing lateral servicing a total of 250 beds. This study will verify how the proposed development will impact the flow capacity of the existing sewer infrastructure downstream southerly of the project location. There are two municipal downstream connections at the campus: one (1) 8-inch line discharging to a manhole owned by City of Long Beach located on the east side of the campus, and one (1) 12-inch line discharging to a manhole owned by County of Los Angeles located on the south side of the campus. These connections serve separate in-campus main sewer lines that flow from northerly upstream end to the southerly municipal connections.

This study will analyze the effect of additional sewer demands imposed by the new student housing on the 2 existing campus main lines and their discharge to the municipal points of connections. This report will provide three (3) options of routing and connections to service the student housing project:

1. Connect Wing A and B to the Long Beach Sewer System
2. Connect Wing A to the Long Beach Sewer System and Wing B to the LA County Sewer System.
3. Connect Wing A and B to the LA County Sewer System

It should be noted that the 8-inch line that discharges to the City of Long Beach Sewer System was previously servicing existing buildings that were demolished for Wing A and Wing B to be constructed.

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

The procedure used herein to analyze the impact of the new sewer demands to the existing sewer system is as follows:

1. New load demands (Q_N) were calculated per plumbing requirements and converted to flow rates; Fixture Units (FU) to Gallons per Minute (GPM) to Cubic feet per second (cfs).
2. The peak flowrates (Q_P) on the existing sanitary sewer system were determined by performing a sewer flow monitoring of 7 and 14 days.
3. The monitored peak flowrate was increased with a peaking factor of 2.5 per industry generally accepted standards to generate the factored peak flowrate ($Q_P * 2.5 = Q_M$). The factored peak flowrate (Q_M) will become the total existing current demand.
4. The sum of the new load demands plus the total existing current demand will become the new total sewer demand ($Q_T = Q_N + Q_M$).
5. The existing pipe's capacity (Q_C) will be calculated using Manning's Equation flowing at half full ($D/d = 0.5$) and with a roughness coefficient of 0.013 per LA County Department of Public Works standards.
6. If the pipe capacity is greater than the new total demand ($Q_C > Q_T$), then the existing sewer system is adequate to receive the new load demands (Q_N).

2. SITE DESCRIPTION

The proposed project site's assessor's parcel number is 7318-006-900 as per Los Angeles County Assessor Parcel Map. Its approximate coordinates are Longitude: 33° 52' 47.4" N and Latitude: 118° 12' 33.9" W. The project site is bounded around E. Greenleaf Boulevard, Harbor Avenue, Campus Drive, and Artesia Boulevard and is approximately 125,547 SF. The location of the project site is highlighted on the Google map shown in Figure 1.

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com



Figure 1. Project Site Location

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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

3. EXISTING SEWER PIPE SYSTEM ANALYSIS

3.1 SEWER UTILITY DATA

Compton Community College sewer utility data is referenced from the below documents. These are included in the Appendix.

1. Subsurface Utility Survey dated October 28, 2022 prepared for PCM3 by Util Locate (Appendix A).
2. Utility Survey dated March 17, 2023 by VCA Engineers Inc. (Subconsultant: Ultra Engineering Inc.) (Appendix B).
3. Topographical Survey dated March 10, 2023 by VCA Engineers Inc. (Appendix C).
4. Wet Utility and Manhole Dipping, CCTV, and Potholing dated September 22, 2023 by VCA Engineers (Subconsultant: Ultra Engineering Inc.) (Appendix D).
5. Additional Manhole Rim Elevation Surveyed on December 7, 2023 by VCA Engineers Inc. (Appendix E).
6. Utility Infrastructure - Phase 1 Set Drawings dated January 27, 2012 by S&K Engineers (Appendix F).

3.2 EXISTING SEWER PIPE MUNICIPAL CONNECTIONS

Within the vicinity of the project site there are two existing sanitary sewer main lines: **Line A** located to the east which connects to the City of Long Beach sanitary sewer system, and **Line B** located to the west which connects to the County of Los Angeles sanitary sewer system. **Line A** is comprised of a 6-inch VCP sanitary sewer line which is then upsized to an 8-inch VCP sanitary sewer line. **Line B** is comprised of an 8-inch PVC sanitary sewer line which is then upsized to a 10-inch PVC sanitary sewer line and finally upsized to a 12-inch PVC sanitary sewer line. The existing sanitary sewer system and lateral connections are shown on Figure 2.

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

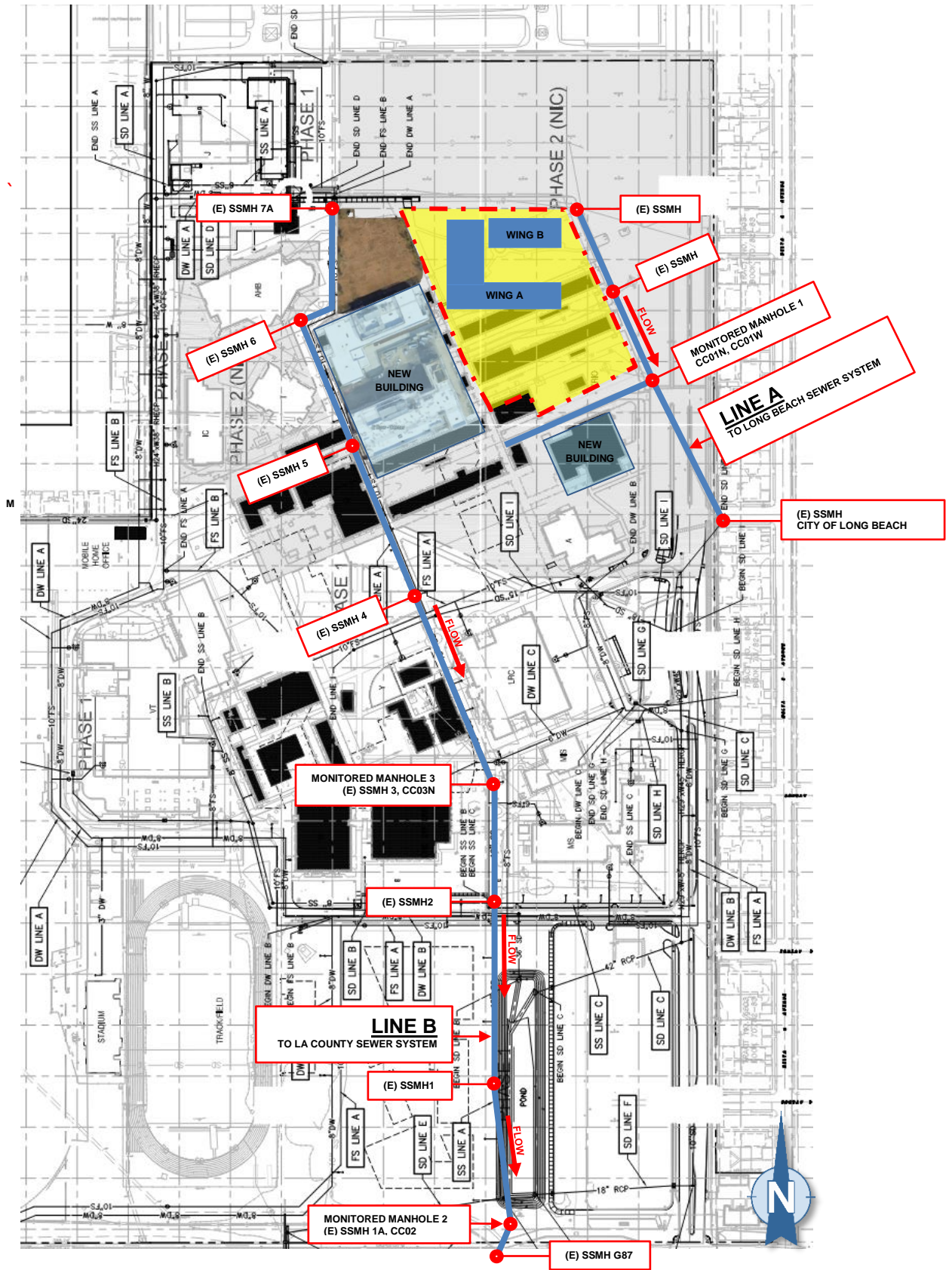


Figure 2: Existing Sanitary System

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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

3.3 FLOW MONITORING

Two flow monitoring studies were conducted by ADS Environmental Services to analyze the existing flows at the downstream manholes before their discharge to the municipal sanitary sewer system.

A flow monitoring is typically performed for collecting data of flow at 5-minute intervals throughout the monitoring period. This approach will quantify wastewater flow monitoring at different locations for a study period. This monitoring data will determine the flow rate per day including the minimum, maximum and the average flow. The analysis of data will be used to accumulate the total flow (Q_P) for the total monitoring period.

A 7-day flow monitoring study was conducted on Line A during Monday, 3rd of April 2023 to Monday, 10th of April 2023 on two distinct manholes. Two observations were conducted at Manhole CC01, the last campus sewer manhole before wastewater is discharged to the manhole owned by City of Long Beach. These observations were named as CC01N (At 8-inch pipe inlet) and CC01W (At 6-inch pipe inlet). One observation was conducted at Manhole CC02, the last campus manhole before wastewater is discharge to the manhole owned by County of Los Angeles. This observation was named CCO2 (At 12-inch pipe inlet). Appendix H shows the results of this study.

A 14-day flow monitoring study was conducted on Line B during Thursday, 19th of October 2023 to Wednesday, 1st November 2023 on two distinct manholes. The monitoring date was intended to ensure school had started and student activities were engaged. Two observations were conducted at this discharge location. One observations was conducted at Manhole CC02 (At 12-inch pipe inlet), the last campus manhole before wastewater is discharged to the manhole owned by County of Los Angeles. Another observation was conducted at Manhole CC03, sewer manhole located in the middle of campus which ultimately discharges into CC02. This observations was named CC03N (At 10-inch pipe inlet). Appendix I shows the results of this study.

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

3.4 MONITORED FLOW RATE (Q_M) – EXISTING DEMAND

Table 1 below provides a summary of the sewer flow monitoring and observed flow conditions. To provide a more conservative value, the monitored peak flowrate of the sewer line (Q_P) in question is increased with a peaking factor of 2.5. This factored peak flowrate (Q_M = 2.5 x Q_P) will become the total existing current demand.

Table 1. Observed Flow Conditions Summary

OBSERVED FLOW CONDITIONS							
Determination of Flow Peak Flow	Factors	Units	7 days			14 days	
			LINE A		LINE B	LINE B	
			CC01N	CC01W	CC02	CC02	CC03N
Monitored Peak Flow	Q _P	MGD	0	0.011	0.023	0.105	0.057
		cfs	0	0.017	0.036	0.162	0.088
Factored Peak Flow (Monitored Peak Flow*2.5)	Q _M	MGD	0	0.028	0.058	0.263	0.143
		cfs	0	0.043	0.089	0.406	0.220

See Figure 2 for locations of Line A, Line B and the Monitored Manholes.

3.5 EXISTING PIPE CAPACITY (Q_C)

Presently, there are two (2) existing sanitary on-site sewer main lines in placed within the vicinity of the project site. The proposed sanitary sewer lines will be connecting into these existing sanitary on-site sewer main lines located on the east and west side of the project site.

An existing 6-inch sanitary sewer line begins at the manhole north of the project site and runs 180' to the southeast before connecting to an existing manhole, immediately east of Wing A. From there, the sewer line converts into an 8-inch and continues to run southeast for approximately 480' at existing manhole CC01 before finally connecting to the manhole owned by City of Long Beach. This existing main line is being identified as Line A.

The calculated pipe capacity (Q_C) of the existing 6-inch pipe is 0.22 cfs, using a roughness coefficient of 0.013 and a slope of 0.64% at half full depth. The calculated pipe capacity (Q_C) of the existing 8-inch pipe is 0.44 cfs, using a roughness coefficient of 0.013 and a slope of 0.54% at half full depth.

The existing manhole SSMH 7A is the start of Line B. Upstream of SSMH 7A, there is a sewer ejector. The existing sanitary sewer line connecting the sewer ejector to SSMH 7A is a 4-inch PVC pipe. The inlet pipe of the sewer ejector is a gravity 6-inch PVC pipe. Downstream of SSMH 7A is an 8-inch line which runs south then turns to be discharged to SSMH 6. South of SSMH 6 is a 10-inch that runs 180' to the southeast and connects to

an existing sewer manhole SSMH 3 (CC03N). South of SSMH 3 is a 10-inch pipe that runs 234' south and connects to an existing sewer manhole SSMH 2. South of SSMH 2 is a 12-inch pipe that runs 628' into SSMH 1A (CC02). Downstream of SSMH 1A is a 12-inch line which runs southwest and discharges to LA County owned SSMH G87. See Appendix G for Line B As-built Profile.

The existing pipe capacity (Q_C) at the 6-inch line upstream from sewer ejector is calculated as 0.21 cfs with a roughness coefficient of 0.013 and slope of 0.58% at half full depth. The capacity of the 6-inch line will also be used as the demand since data on the actual demand is unknown at this time. The 8-inch pipe, connected from SSMH 7A to SSMH 6, is calculated to a pipe capacity (Q_C) of 0.46 cfs with a roughness coefficient of 0.013 and a slope of 0.58% at half full depth. The 10-inch line, connected from SSMH 6 to SSMH 2, is calculated to a pipe capacity (Q_C) of 0.69 cfs with a roughness coefficient of 0.013 and a slope of 0.40% at half full depth. Lastly, the 12-inch pipe line, connected from SSMH 2 to the County connection, is calculated to a pipe capacity (Q_C) of 1.13 cfs with a roughness coefficient of 0.013 and a slope of 0.40% at half full depth.

The existing pipe capacity should be determined to know if it is adequate to support the new total demand flow (Q_N). Existing parameters should be given in order to determine the flow rate of the existing pipe (Q_C). Existing parameters to consider are the following:

- Monitored Peak Flowrate (Q_P)
- Factored Peak Flowrate (Q_M)
- Diameter of existing pipe (D)
- Manning's Roughness Coefficient (n) = 0.013
- Slope of the Existing Pipe (S)
- Depth of Flow (d)
- Proportional Depth of Flow (d/D)
- Velocity of flow (v)

Calculations of the existing pipe capacity will determine if the existing pipe can support the new total demand of the proposed structures and if the waste flow can discharge at a proportional depth of flow of ($d/D = 50\%$ to 75%) per LA County Standard S-C4 as shown in Appendix M.

Refer to Appendix J for the calculations of the existing pipe capacity (Q_C) and *Figure 2* for the location of the existing sewer main lines and manholes.

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

4. NEW SANITARY SEWER SYSTEM ANALYSIS

4.1 NEW SEWER CONNECTIONS

The project site will consist of two (2) proposed buildings, Wing A and Wing B. Wing A is an L-Shaped, long leg horizontal structure situated at the Northwest and South portion of the project site. Wing B is a rectangular shaped structure located at the Northeast side of the project site, just north of Wing A.

Wing A will have four proposed point of connections being on the north side of the long leg side of the L-shaped building. The point of connection POC A will pick up 219.5 domestic fixture units, which will generate 69 GPM or 0.154 cfs while POC B will pick up 225 domestic fixture units, which will generate 70 GPM or 0.156 cfs. Furthermore, the point of connection POC C will pick up 2 domestic fixture units, which will generate 1 GPM or 0.002 cfs and the point of connection POC D will pick up 242 domestic fixture units, which will generate 74 GPM or 0.165 cfs.

Wing B will have one proposed point of connection POC E on the north side of the building. This POC will pick up 421.5 domestic fixture units, which will generate 108 GPM or 0.241 cfs. See Figure 3 for the points of connection.

4.2 LATERAL PIPE SIZES

Proposed sanitary sewer lines were sized to handle the new demand flow. All four proposed sanitary sewer laterals connecting POC A, B, C, D, and E to the trunk lines will be sized to a minimum 6-inch pipe. (See Appendix K for Proposed Sewer Pipe Capacity Calculations).

Wing A is composed of four lateral connections, the POC A, B, C, and D. The total flow from Wing A will be equal to 688.5 domestic fixture units and will generate 214 GPM which is equal to 0.477 cfs.

Wing B is composed of one lateral connection POC E. The POC E consists of 421.5 domestic fixture units and will generate 108 GPM which is equal to 0.241 cfs.

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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

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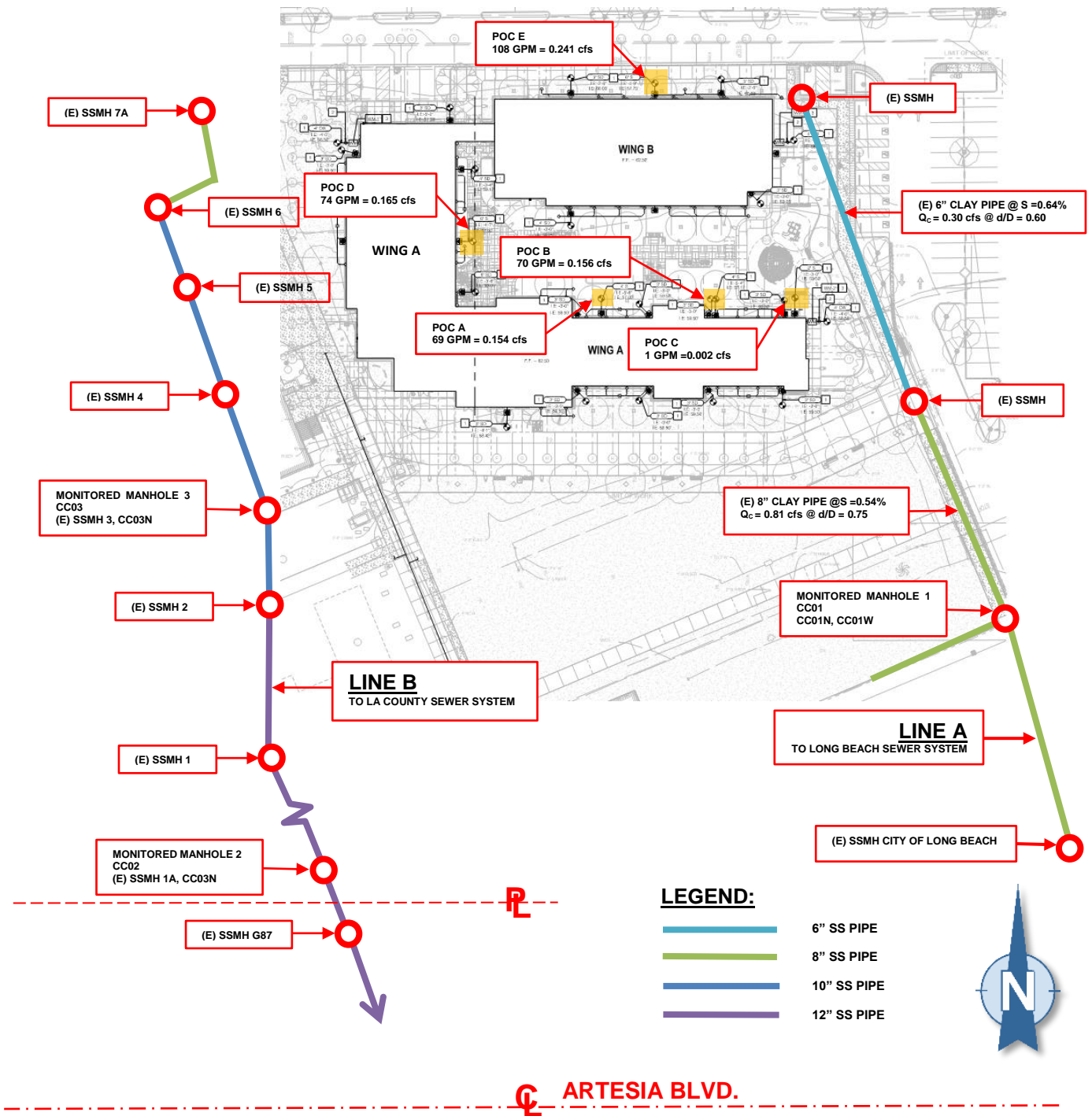


Figure 3: Point of Connections

5. SCENARIO ANALYSIS FOR TOTAL DEMAND FLOW (Q_T)

The Post Development Flow downstream of the project site was determined by adding the monitored existing maximum flow (with the peaking factor applied, Q_M) and the peak flow generated by the proposed development (Q_N). Three connection analyses were identified:

ANALYSIS 1: BOTH WING A AND WING B TO CONNECT LINE A

SEWER DEMAND

EXISTING DEMAND

Factored Peak Flowrate (Q_M) @ CC01N = 0.00 cfs

Factored Peak Flowrate (Q_M) @ CC01W = 0.043 cfs

FUTURE DEMAND

WING A = 0.154 cfs + 0.156 cfs + 0.002 cfs + 0.165 cfs
= 0.477 cfs

WING B = 0.241 cfs

Total Project Demand (Q_T) = 0.477 cfs + 0.241 cfs = 0.718 cfs

TOTAL SEWER DEMAND (Q_T) = 0.00 cfs + 0.043 cfs + 0.718 cfs = 0.761 cfs

LINE A – EXISTING SEWER CAPACITY

6-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.64\%$ = 0.22 cfs

6-inch Pipe Capacity @ $d/D = 0.60$ and $S = 0.64\%$ = 0.30 cfs

8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.54\%$ = 0.44 cfs

8-inch Pipe Capacity @ $d/D = 0.75$ and $S = 0.54\%$ = 0.81 cfs

COMPARISONS

Wing B Future Demand = 0.241 cfs < 6-inch pipe capacity = 0.30 cfs @ $d/D = 0.60$

Wing A Future Demand = 0.477 cfs < 8-inch pipe capacity = 0.60 cfs @ $d/D = 0.60$

$Q_T = 0.761$ cfs < 8-inch pipe capacity = 0.81 cfs @ $d/D = 0.75$

OBSERVATIONS

1. Wing B future demand is less than the existing 6-inch pipe capacity at $d/D = 0.60$; (0.241 cfs < 0.30 cfs).
2. Total project demand Q_T (0.761 cfs) is less than the capacity of the existing 8-inch pipe at $d/D = 0.75$ (0.81 cfs).
3. Capacity of the City of Long Beach Sewer line was not calculated as existing elevations, pipe length, slope and sizes are required to confirm capacity.

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

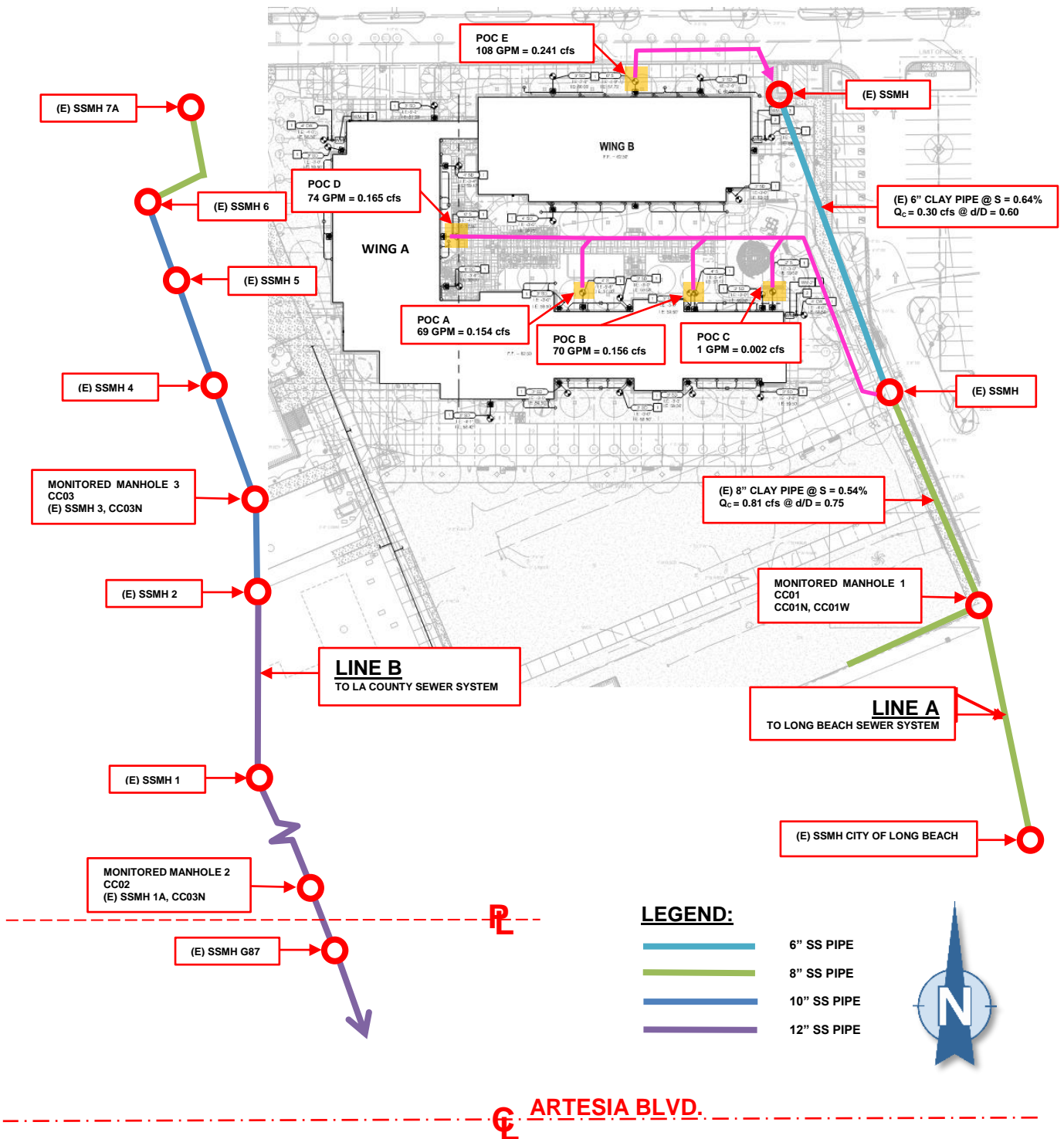


Figure 4: Scenario Analysis I Sewer System

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

ANALYSIS 2: WING B CONNECT TO LINE B AND WING A CONNECT TO LINE A

SEWER DEMAND

A. WING A TO LINE A

EXISTING DEMAND

Factored Peak Flowrate (Q_M) @ CCO1N = 0.00 cfs

Factored Peak Flowrate (Q_M) @ CCO1W = 0.043 cfs

FUTURE DEMAND (Q_N)

WING A = 0.154 cfs + 0.156 cfs + 0.002 + 0.165 cfs = 0.477 cfs

TOTAL SEWER DEMAND (Q_T) = 0.00 cfs + 0.043 cfs + 0.477 cfs = 0.52 cfs

LINE A – EXISTING SEWER CAPACITY

8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.54\%$ = 0.44 cfs

8-inch Pipe Capacity @ $d/D = 0.60$ and $S = 0.54\%$ = 0.60 cfs

COMPARISONS

Wing A Future Demand = 0.477 cfs < 8-inch pipe capacity @ $d/D = 0.60$ = 0.60 cfs

$Q_T = 0.52$ cfs < 8-inch pipe capacity @ $d/D = 0.60$ = 0.60 cfs

B. WING B TO LINE B

EXISTING DEMAND

6-inch Pipe Upstream Sewer Ejector = 0.21 cfs (Based on 6-inch pipe capacity)

Factored Peak Flowrate (Q_M) @ CCO2 = 0.41 cfs

FUTURE DEMAND

WING B = 0.241 cfs

TOTAL SEWER DEMAND (Q_T)

At SSMH 7A = 0.21 cfs + 0.241 cfs = 0.451 cfs

Downstream to LA County Sewer System = 0.41 cfs + 0.451 cfs = 0.861 cfs

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Irvine

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Tel: 949-679-0870 ▪ Fax: 949-679-9370

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LINE B – EXISTING SEWER CAPACITY

6-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.21 cfs

8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.46 cfs

12-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.40\%$ = 1.13 cfs

LINE B – NEW SEWER CAPACITY

8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.50\%$ = 0.51 cfs

COMPARISONS

Wing B future demand = 0.241 cfs < New 8-inch pipe capacity = 0.51 cfs @ $d/D = 0.50$

Q_T at SSMH 7A = 0.451 cfs < 8-inch pipe capacity = 0.46 cfs @ $d/D = 0.50$

Q_T at LA County Sewer System = 0.861 cfs < 12-inch pipe capacity = 1.13 cfs @ $d/D = 0.50$

OBSERVATIONS

WING A TO LINE A

1. Wing A future demand is less than the existing 8-inch pipe capacity at $d/D = 0.60$; (0.477 cfs < 0.60 cfs).
2. Total project demand Q_T (0.52 cfs) is less than the capacity of the existing 8-inch pipe capacity at $d/D = 0.60$ (0.60 cfs).

WING B TO LINE B

1. Wing B future demand is less than the new 8-inch pipe capacity at $d/D = 0.50$; (0.241 cfs < 0.51 cfs).
2. Total demand Q_T to SSMH 7A (0.451 cfs) is less than the existing 8-inch pipe capacity at $d/D = 0.50$ (0.46 cfs).
3. Total demand Q_T to LA County Sewer System (0.861 cfs) is less than the existing 12-inch pipe capacity at $d/D = 0.50$ (1.13 cfs).
4. If Line B will serve Wing B only, then Line B is adequate to support the total sewer demand and still have a net future available capacity of 0.269 cfs (1.13 cfs – 0.861 cfs or 121 GPM) for any future connections through 12-inch line.

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

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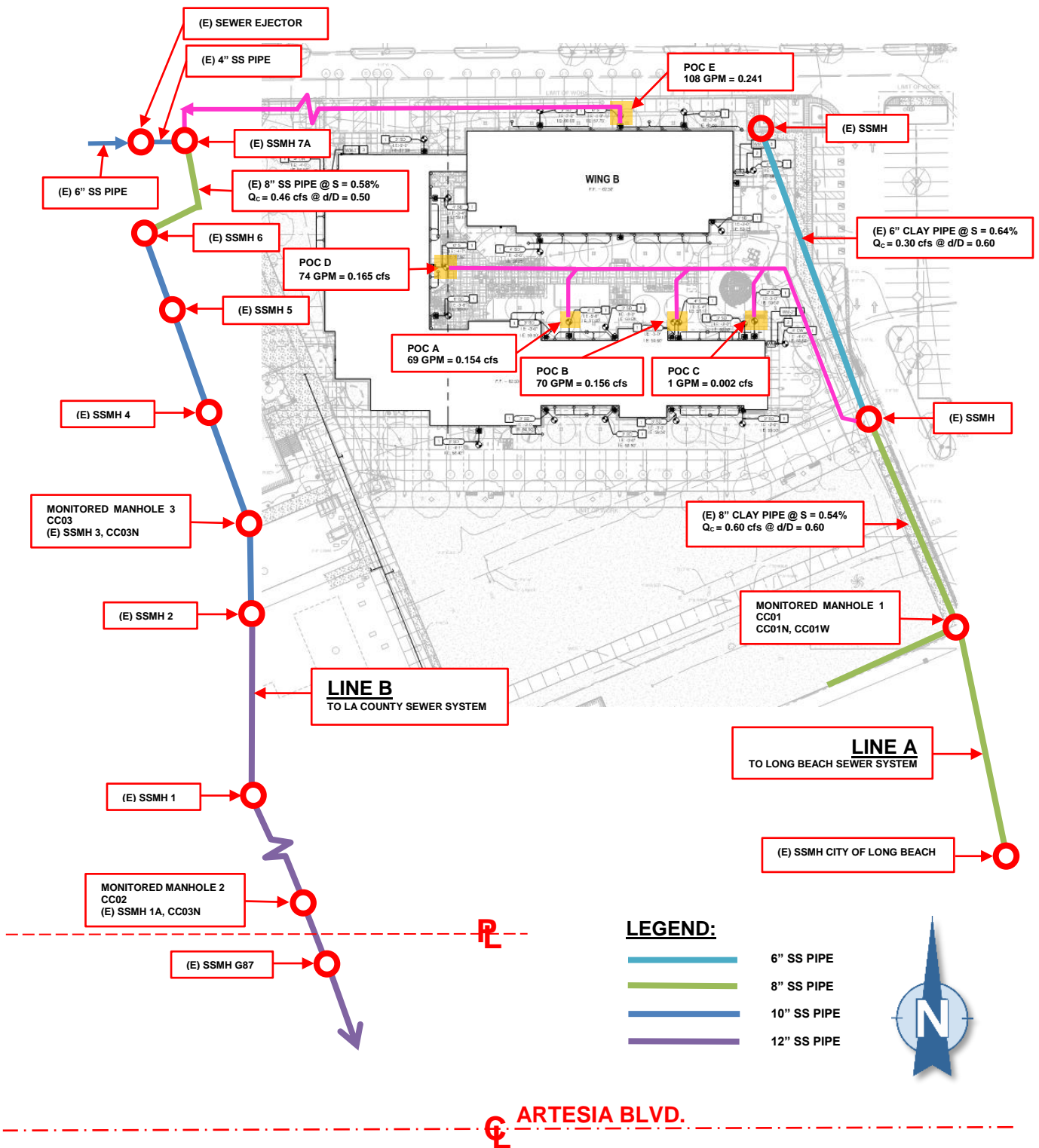


Figure 5: Scenario Analysis 2 Sewer System

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
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 www.vcaeng.com

ANALYSIS 3: WING A AND WING B TO CONNECT TO SSMH 7A

SEWER DEMAND

WING A AND B TO LINE B

EXISTING DEMAND

6-inch Pipe Upstream Sewer Ejector = 0.21 cfs (based on 6-inch pipe capacity)
Factored Peak Flowrate (Q_M) @ CCO2 = 0.41 cfs

FUTURE DEMAND

WING A = 0.477 cfs
WING B = 0.241 cfs

Total Future Demand = 0.477 cfs + 0.241 cfs = 0.718 cfs

TOTAL SEWER DEMAND (Q_T)

At SSMH 7A = 0.21 cfs + 0.718 cfs = 0.928 cfs
Downstream to LA County Sewer System = 0.41 cfs + 0.928 cfs = 1.338 cfs

0.92

LINE B – EXISTING SEWER CAPACITY

6-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.21 cfs
8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.46 cfs
12-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.40\%$ = 1.13 cfs
12-inch Pipe Capacity @ $d/D = 0.60$ and $S = 0.40\%$ = 1.52 cfs

LINE B – NEW SEWER CAPACITY

8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.50\%$ = 0.51 cfs
10-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.50\%$ = 0.92 cfs
10-inch Replacement Pipe Sewer Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.99 cfs

COMPARISONS

Total Future Demand = 0.718 cfs < New 10-inch pipe capacity = 0.92 cfs @ $d/D = 0.50$

Q_T at SSMH 7A = 0.928 cfs < 10-inch Replacement Pipe = 0.99 cfs @ $d/D = 0.50$

Q_T at LA County Sewer System = 1.338 cfs < 12-inch pipe capacity = 1.52 cfs @ $d/D = 0.60$

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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
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OBSERVATIONS

1. Wing A can be conveyed directly to SSMH7A.
2. Since there is a new building near the SSMH 6, connection directly to SSMH 6 from Wing A is not possible.
3. Since the demand in Wing A and Wing B will be conveyed as one all towards SSMH7A, a new 10-inch pipe will be required for the conveyance of the total demand of both buildings. The total demand of Wings A and B is 0.718 cfs is less than new 10-inch line capacity of 0.92 cfs.
4. Thus the existing 8-inch line will have to be replaced by a new 10-inch line between SSMH7A and SSMH6.
5. The total demand at SSMH 7A including from the ejector pump equaling 0.928 cfs is less than the capacity of 0.99 cfs of the new replacement 10-inch line.
6. Installation of the replacement 10-inch line is in the same location as the existing 8-inch line. Thus trenching will not occur thru unverified subsurface areas but through where the existing line minimizing unforeseen conditions and obstructions.
7. The total demand at LA County Sewer System including from the ejector pump equaling 1.338 cfs is less than the capacity of 1.52 cfs of the existing 12-inch line.

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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
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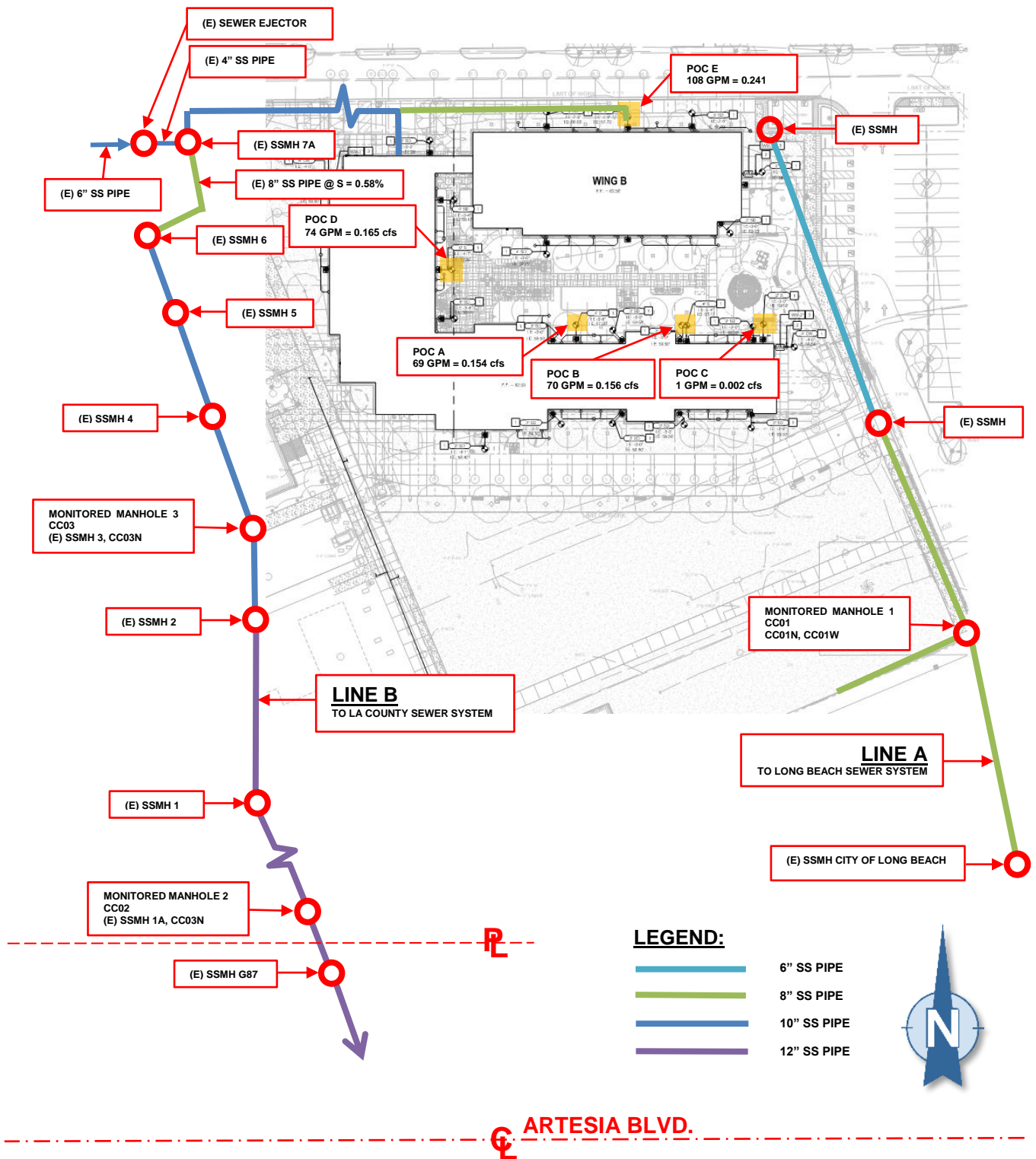


Figure 6: Scenario Analysis 3 Sewer System

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 e-mail: vca@vcaeng.com

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2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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ANALYSIS 4: WING A AND WING B TO CONNECT TO SEWER EJECTOR

SEWER DEMAND

WING A AND B TO LINE B

EXISTING DEMAND

6-inch Pipe Upstream Sewer Ejector = 0.21 cfs (based on 6-inch pipe capacity)
Factored Peak Flowrate (Q_M) @ CCO2 = 0.41 cfs

FUTURE DEMAND

WING A = 0.477 cfs
WING B = 0.241 cfs

Total Future Demand = 0.477 cfs + 0.241 cfs = 0.718 cfs

TOTAL SEWER DEMAND (Q_T)

At Sewer Ejector = 0.21 cfs + 0.718 cfs = 0.928 cfs
At SSMH 7A = 0.21 cfs + 0.718 cfs = 0.928 cfs
Downstream to LA County Sewer System = 0.41 cfs + 0.928 cfs = 1.338 cfs

LINE B – EXISTING SEWER CAPACITY

6-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.21 cfs
8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.46 cfs
12-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.40\%$ = 1.13 cfs
12-inch Pipe Capacity @ $d/D = 0.60$ and $S = 0.40\%$ = 1.52 cfs

LINE B – NEW SEWER CAPACITY

8-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.50\%$ = 0.51 cfs
10-inch Pipe Capacity @ $d/D = 0.50$ and $S = 0.50\%$ = 0.92 cfs
10-inch Pipe Capacity @ $d/D = 0.60$ and $S = 0.50\%$ = 1.23 cfs
6-inch Pipe Capacity @ $d/D = 0.50$ and $S = 5.23\%$ = 0.76 cfs
6-inch Pipe Capacity @ $d/D = 0.60$ and $S = 5.23\%$ = 1.02 cfs
10-inch Replacement Pipe Sewer Capacity @ $d/D = 0.50$ and $S = 0.58\%$ = 0.99 cfs

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COMPARISONS

Total Future Demand = 0.718 cfs < New 10-inch pipe capacity = 0.92 cfs @ d/D = 0.50

Q_T at Sewer Ejector = 0.928 cfs < New 10-inch pipe capacity = 1.23 cfs @ d/D = 0.60

Q_T at Sewer Ejector = 0.928 cfs < New 6-inch pipe capacity = 1.02 cfs @ d/D = 0.60

Q_T at SSMH 7A = 0.928 cfs < 10-inch Replacement Pipe = 0.99 cfs @ d/D = 0.50

Q_T at LA County Sewer System = 1.338 cfs < 12-inch pipe capacity = 1.52 cfs @ d/D = 0.60

OBSERVATIONS

1. Since the demand in Wing A and Wing B will be conveyed as one all towards Sewer Ejector, a new 10-inch pipe will be required for the conveyance of the total demand of both buildings. The total demand of Wings A and B is 0.718 cfs is less than new 10-inch line capacity of 0.92 cfs.
2. A portion of 6-inch existing line between SSMH 7 and Sewer Ejector will be removed and replaced to meet new invert elevation, a new 10-inch line will be required to convey the total demand of both buildings and including from the 6-inch line. The total demand is 0.928 cfs is less than new 10-inch line capacity of 1.23 cfs.
3. The existing sewer pipe line after Sewer ejector pump of 4-inch pipe will be removed and replaced to 6-inch pipe to support the total demand. The total demand at demand at existing 6-inch pipe is 0.928 cfs is less than 6-inch pipe capacity of 1.02 cfs.
4. Thus the existing 8-inch line will have to be replaced by a new 10-inch line between SSMH7A and SSMH6.
5. The total demand at SSMH 7A including from the ejector pump equaling 0.928 cfs is less than the capacity of 0.99 cfs of the new replacement 10-inch line.
6. Installation of the replacement 10-inch line is in the same location as the existing 8-inch line. Thus trenching will not occur thru unverified subsurface areas but through where the existing line minimizing unforeseen conditions and obstructions.
7. The total demand at LA County Sewer System including from the ejector pump equaling 1.338 cfs is less than the capacity of 1.52 cfs of the existing 12-inch line.

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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

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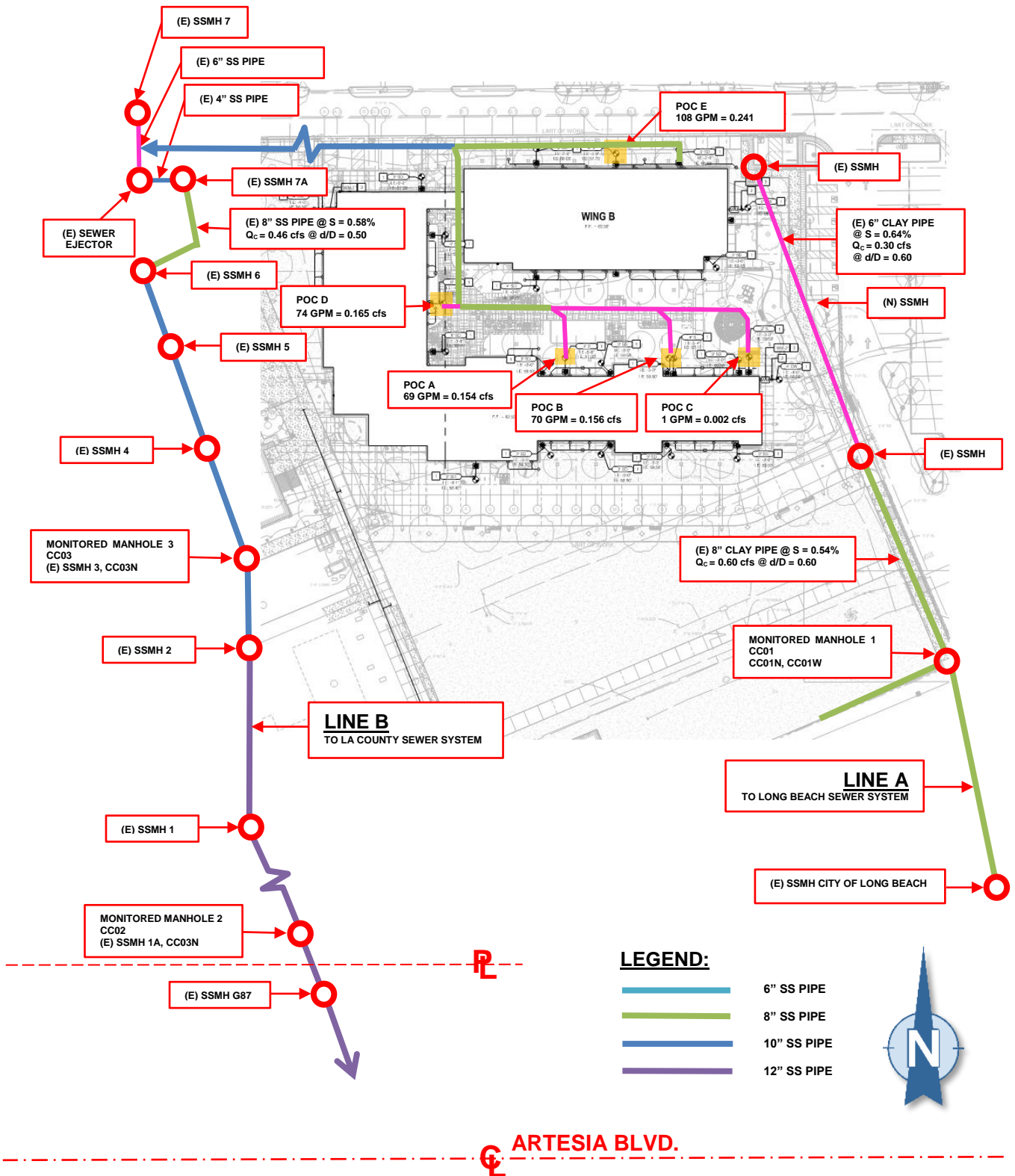


Figure 7: Scenario Analysis 4 Sewer System

6. CONCLUSION

The below conclusion is solely based on the impact of the proposed student housing building will have on the existing sanitary system. Accordingly, each scenario will be looked into and evaluated for its merits and flaws.

SCENARIO ANALYSIS 1

Merits:

- This scenario is feasible.
- Although the risk of clogging exists, it is acceptable.

Flaws:

- Demands for new, under construction and future buildings were not detected in the flow monitoring investigation and not taken into account.
- No new demand can be imposed on the existing line.

SCENARIO ANALYSIS 2

Merits:

- This is feasible.
- Existing lines will be available for new demands.
- Impact to the City and County line is the minimal.

Flaws:

- Demand for the newly constructed and under construction buildings were not included in the flow monitoring investigation. This demand was not taken into account and if added, will lessen the capacity of Line B.

SCENARIO ANALYSIS 3

Merits:

- This is feasible.

Flaws:

- Existing 8” pipe from SSMH 7A to SSMH 6 will need to be upsized to a 10-inch pipe.
- Existing 8-inch line is at capacity. No new demands can be introduced into the line.
- Demand for the newly constructed and under construction buildings were not included in the flow monitoring investigation. This demand was not taken into account and if added, will lessen the capacity of Line B.

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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
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SCENARIO ANALYSIS 4

Merits:

- This is feasible.

Flaws:

- Portion of an existing 6” pipe from SSMH 7 to Sewer ejector pump will need to be removed and upsized to a 10-inch pipe.
- Existing 8” pipe from SSMH 7A to SSMH 6 will need to be upsized to a 10-inch pipe.
- Existing 8-inch line is at capacity. No new demands can be introduced into the line.
- Demand for the newly constructed and under construction buildings were not included in the flow monitoring investigation. This demand was not taken into account and if added, will lessen the capacity of Line B.

7. RECOMMENDATION

The most viable option to be recommended is Scenario Analysis 4, which will convey the discharge of Line A and Line B as one. This approach will avoid overburdening each of the existing lines with additional sewer demands.

There are other demands that were not considered in this study. Buildings that are in construction and not yet occupied new buildings are inactive and their wastes were not detected by the flow monitoring investigation. Thus, their demands are not included and not part of the study. Demand on future buildings was also not included in the study as their demands are unknown at this time. Additional study may be required to ensure the existing lines are not overburdened because of these potential new or additional connections.

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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

APPENDIX

The appendices attached here are the materials that was used as reference and a guide for this study.

- Appendix A: Subsurface Utility (October 28, 2022), VCA Engineers Inc. (Subconsultant: Ultra Engineering Inc.)
- Appendix B: Utility Survey (March 17, 2023), VCA Engineers Inc.
- Appendix C: Topographical Survey (March 10, 2023), VCA Engineers Inc.
- Appendix D: Wet Utility and Manhole Dipping, CCTV, and Potholing (September 22, 2023), VCA Engineers Inc. (Subconsultant: Ultra Engineering Inc.)
- Appendix E: Additional Manhole Rim Elevation Survey (December 7, 2023), VCA Engineers Inc.
- Appendix F: Utility Infrastructure-Phase 1 Set Drawings (January 27, 2012), S&K Engineers
- Appendix G: Profile of Line B
- Appendix H: 7 days Monitoring Flow Study, ADS Environmental Services
- Appendix I: 14 days Monitoring Flow Study, ADS Environmental Services
- Appendix J: Existing Sewer Pipe Capacity Calculations
- Appendix K: Total Sewer Demand
- Appendix L: New Total Demand Calculations
- Appendix M: Excerpts from LA County DPW Sanitary Sewer Procedural Manual

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Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

APPENDIX A

SUBSURFACE UTILITY

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
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SUBSURFACE UTILITY MAP
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 Email: info@util-locate.com Web: www.util-locate.com

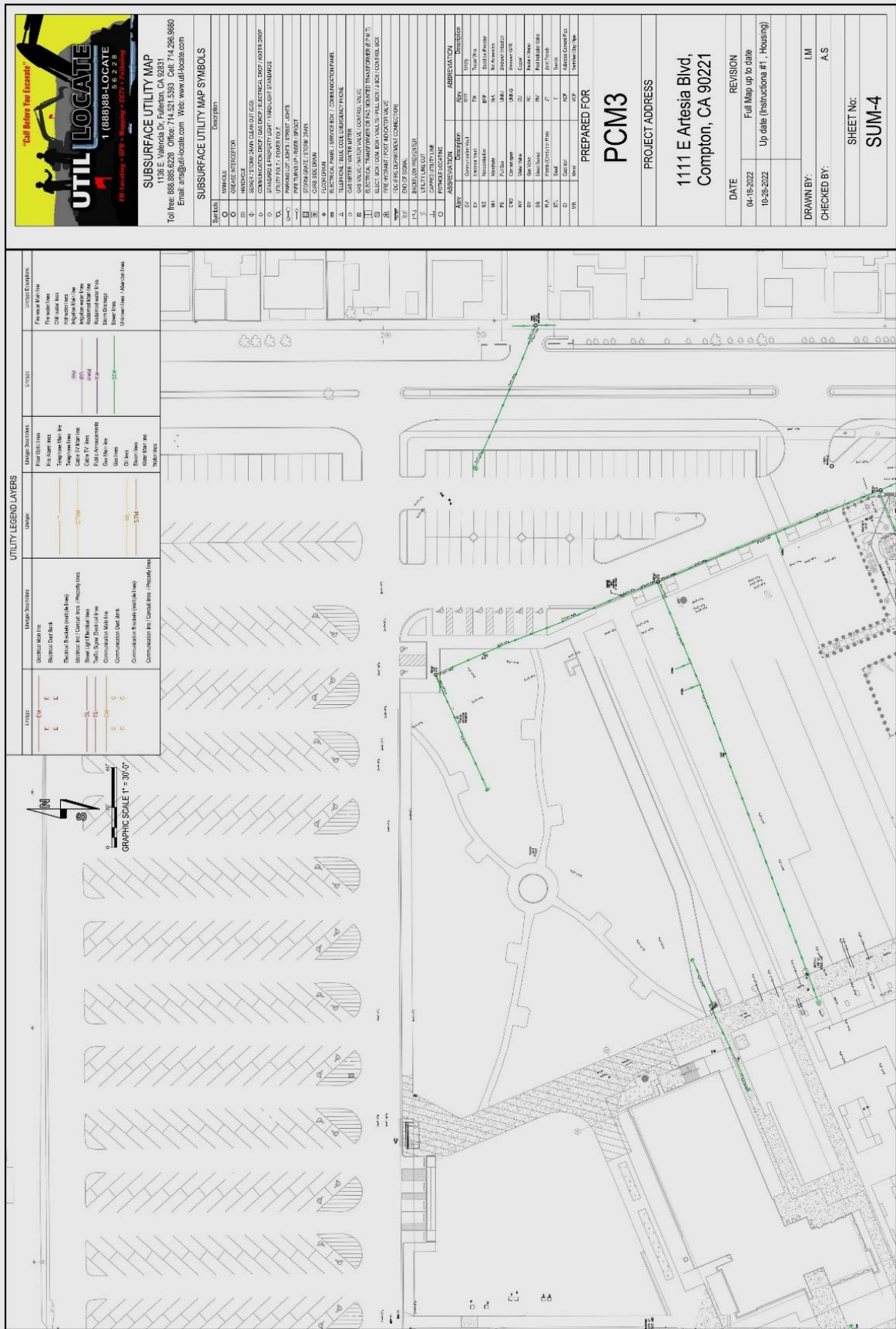
SUBSURFACE UTILITY MAP SYMBOLS

SYMBOL	DESCRIPTION
(Symbol)	Water Main
(Symbol)	Sanitary Sewer
(Symbol)	Storm Sewer
(Symbol)	Electric Power
(Symbol)	Gas
(Symbol)	Communication
(Symbol)	Fire Alarm
(Symbol)	TV
(Symbol)	Other

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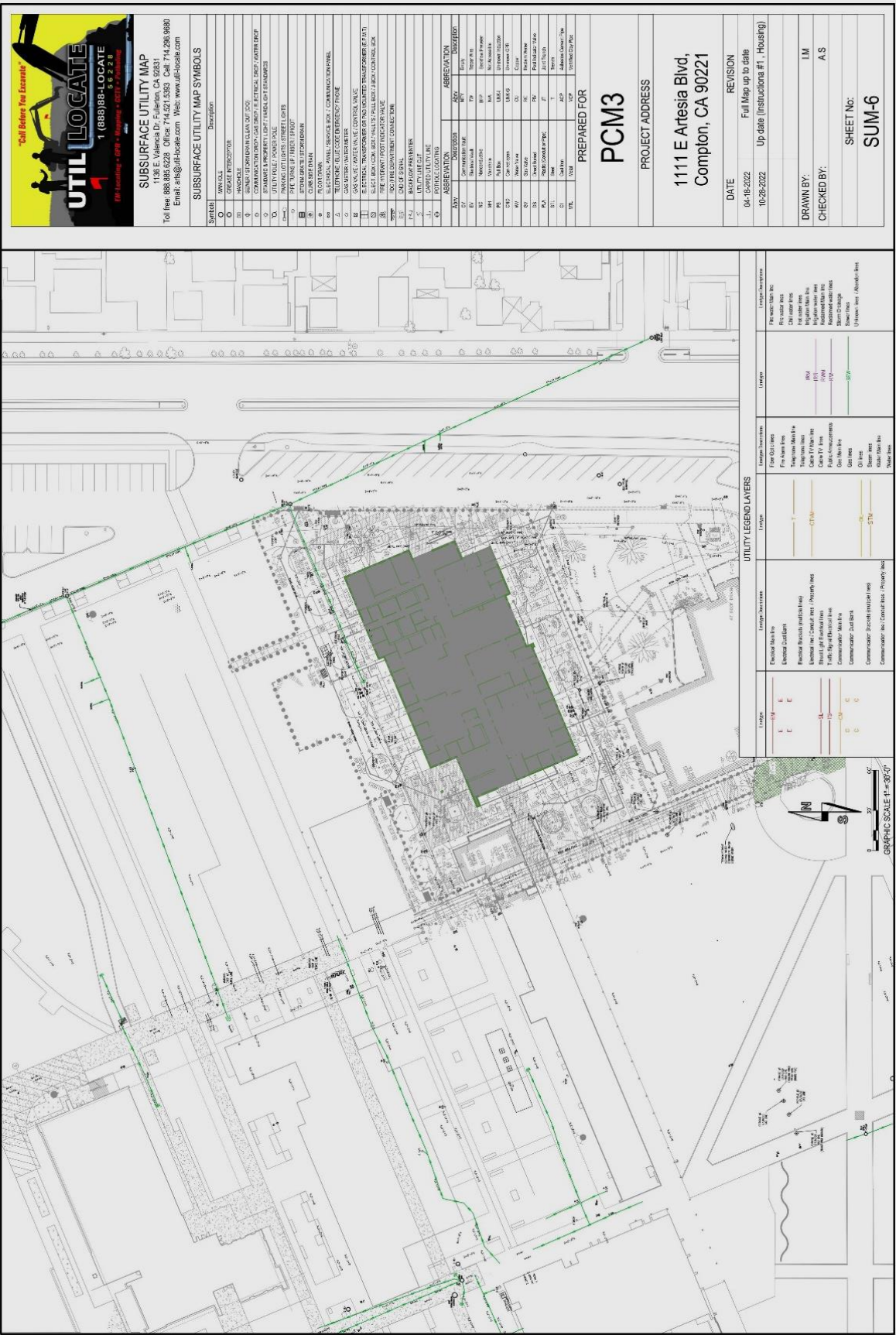
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 Tel: 949-679-0870 • Fax: 949-679-9370
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Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

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Tel: 949-679-0870 ▪ Fax: 949-679-9370
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Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

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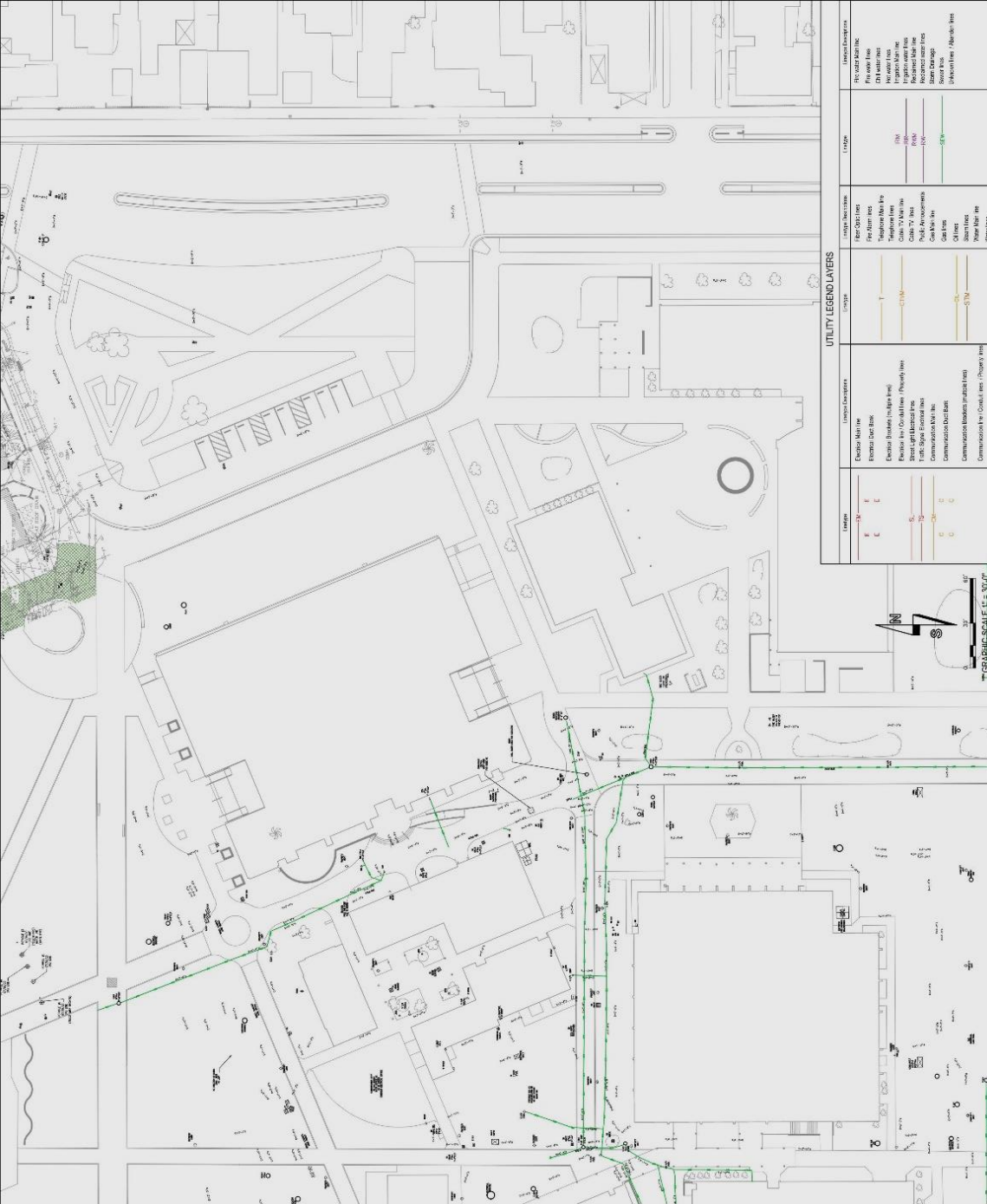
SUBSURFACE UTILITY MAP SYMBOLS

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 Compton, CA 90221**

DATE	REVISION
04-19-2022	Full Map up to date
10-25-2022	Up date (Instruccions #1, Housing)
DRAWN BY:	LM
CHECKED BY:	AS
SHEET NO.: SUM-8	



UTILITY LEGEND LAYERS

Layer	Symbol	Color	Line Style	Description
Electric (High Voltage)	Line with triangles	Red	Solid	Electric (High Voltage)
Electric (Low Voltage)	Line with circles	Yellow	Solid	Electric (Low Voltage)
Gas	Line with crosses	Blue	Solid	Gas
Water	Line with dots	Green	Solid	Water
Sewer	Line with dashes	Purple	Solid	Sewer
Storm Drain	Line with vertical bars	Light Blue	Solid	Storm Drain
Telephone	Line with horizontal bars	Orange	Solid	Telephone
Cable TV	Line with diagonal bars	Pink	Solid	Cable TV
Other Utilities	Line with various symbols	Various	Solid	Other Utilities



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 Tel: 323-729-6098 ▪ Fax: 323-729-6043
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 2151 Michelson Dr. # 242, Irvine, CA 92612
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APPENDIX B

UTILITY SURVEY

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
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 626-444-4444
 www.vcaeng.com

NOTES:

The survey was conducted by the VCA Engineering staff on 08/11/2011. The survey was conducted in accordance with the California State Board of Geomata Engineering, California State Board of Professional Engineers, and California State Board of Professional Land Surveyors.

Contractor shall verify the location of all existing utilities before excavation. Call 811 for a utility map.

Contractor shall hand-check to a point of no conflict 24" on either side of the estimated depth.

Depths shown are approximate. Estimated depths are based on the location of the utility lines to the facility. The location of the utility lines may vary along the length of the facility.

The scope of this survey does not include the location of any other utilities not shown on the map.

The map was prepared by the VCA Engineering staff on 08/11/2011. The map was prepared in accordance with the California State Board of Geomata Engineering, California State Board of Professional Engineers, and California State Board of Professional Land Surveyors.

In the event the information shown in this map is not accurate, the user shall be responsible for the accuracy of the plan.

Contractor shall verify the location of all existing utilities before excavation.

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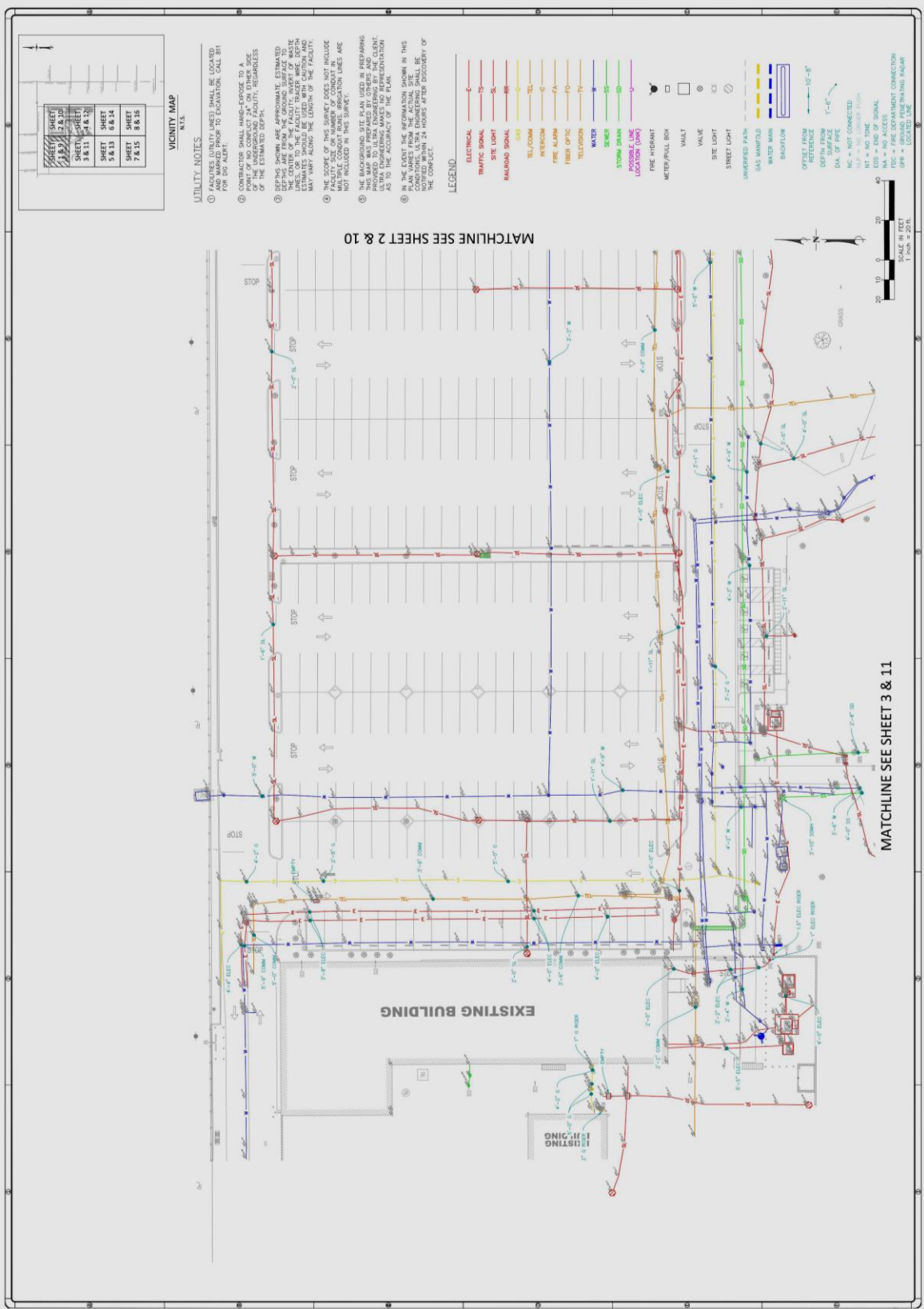
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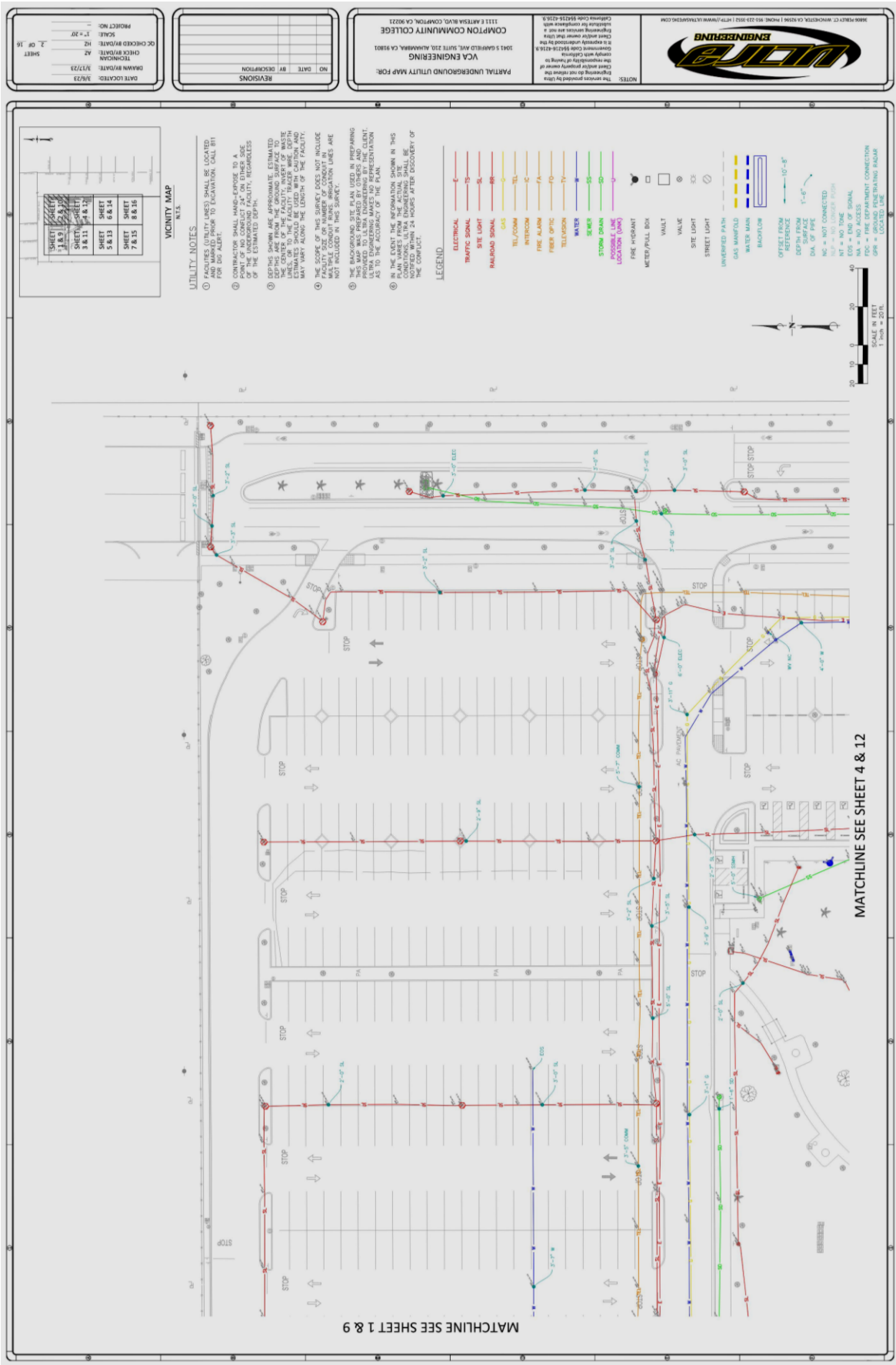
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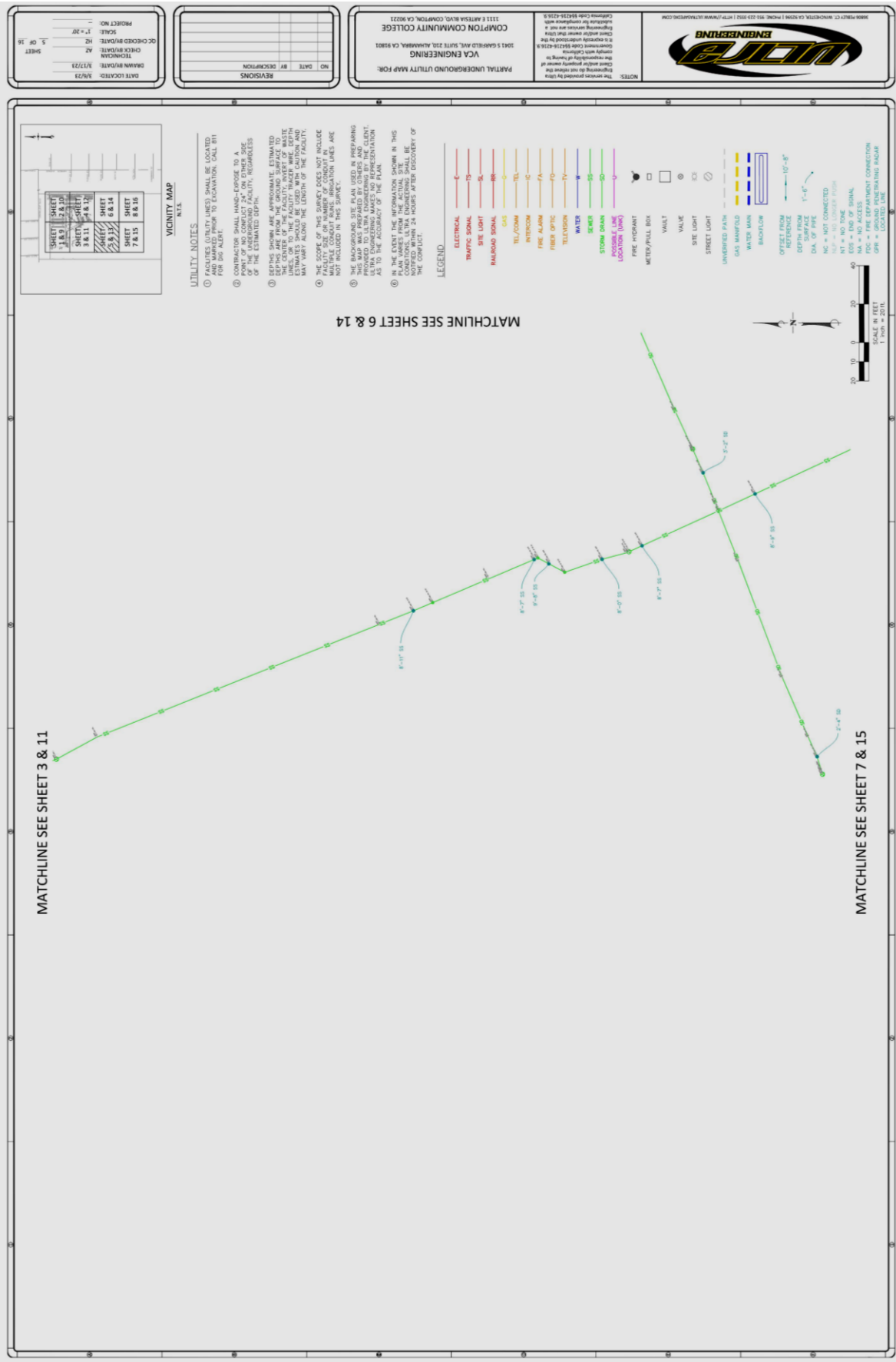
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PROJECT NO. -

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SHEET 5 OF 16

DATE LOCATED 3/17/23

DRAWN BY/DATE M/2/23

TECHNICAL AZ

NO. **DATE** **BY** **DESCRIPTION**

PARTIAL UNDERGROUND UTILITY MAP FOR:

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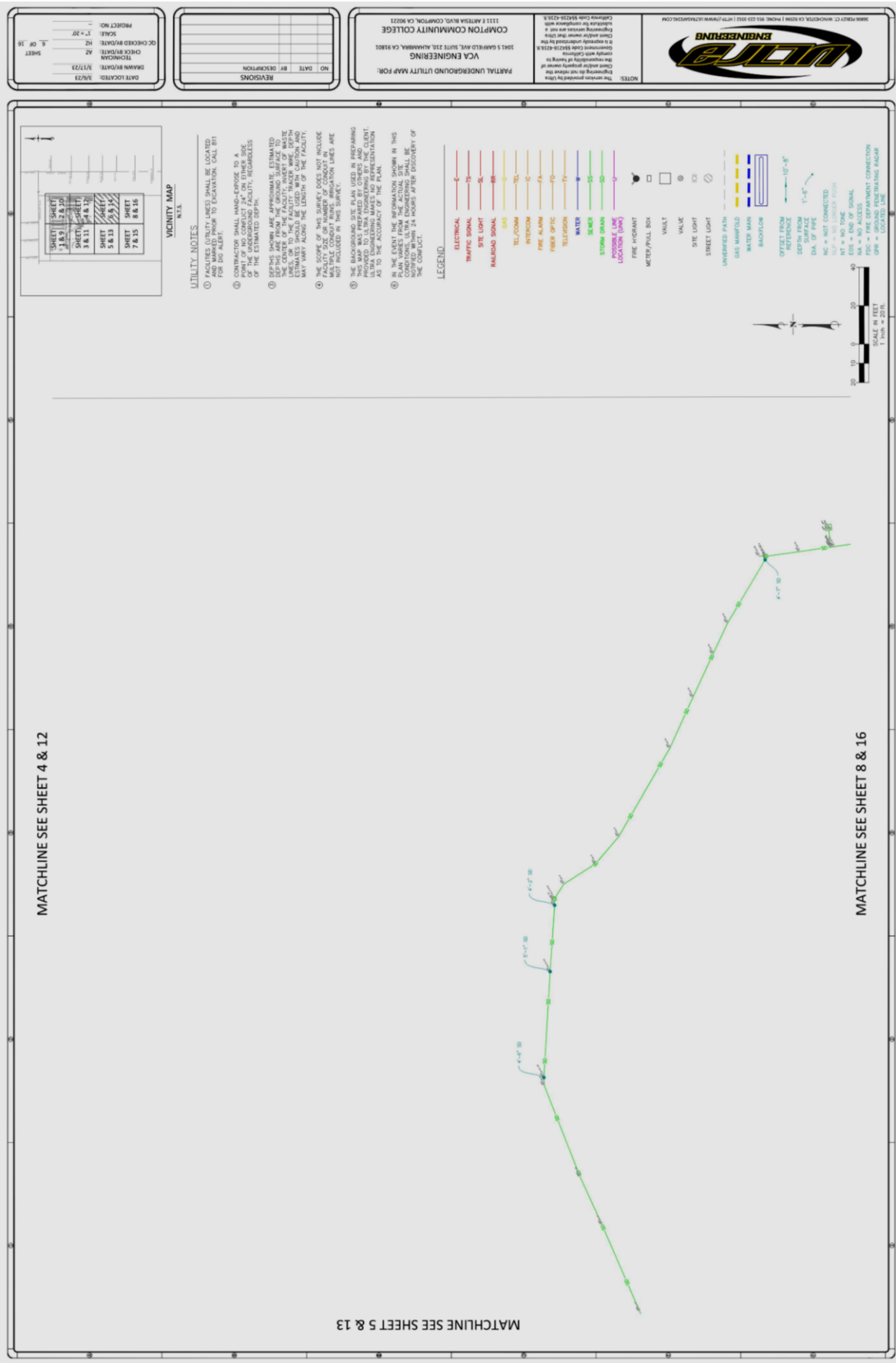
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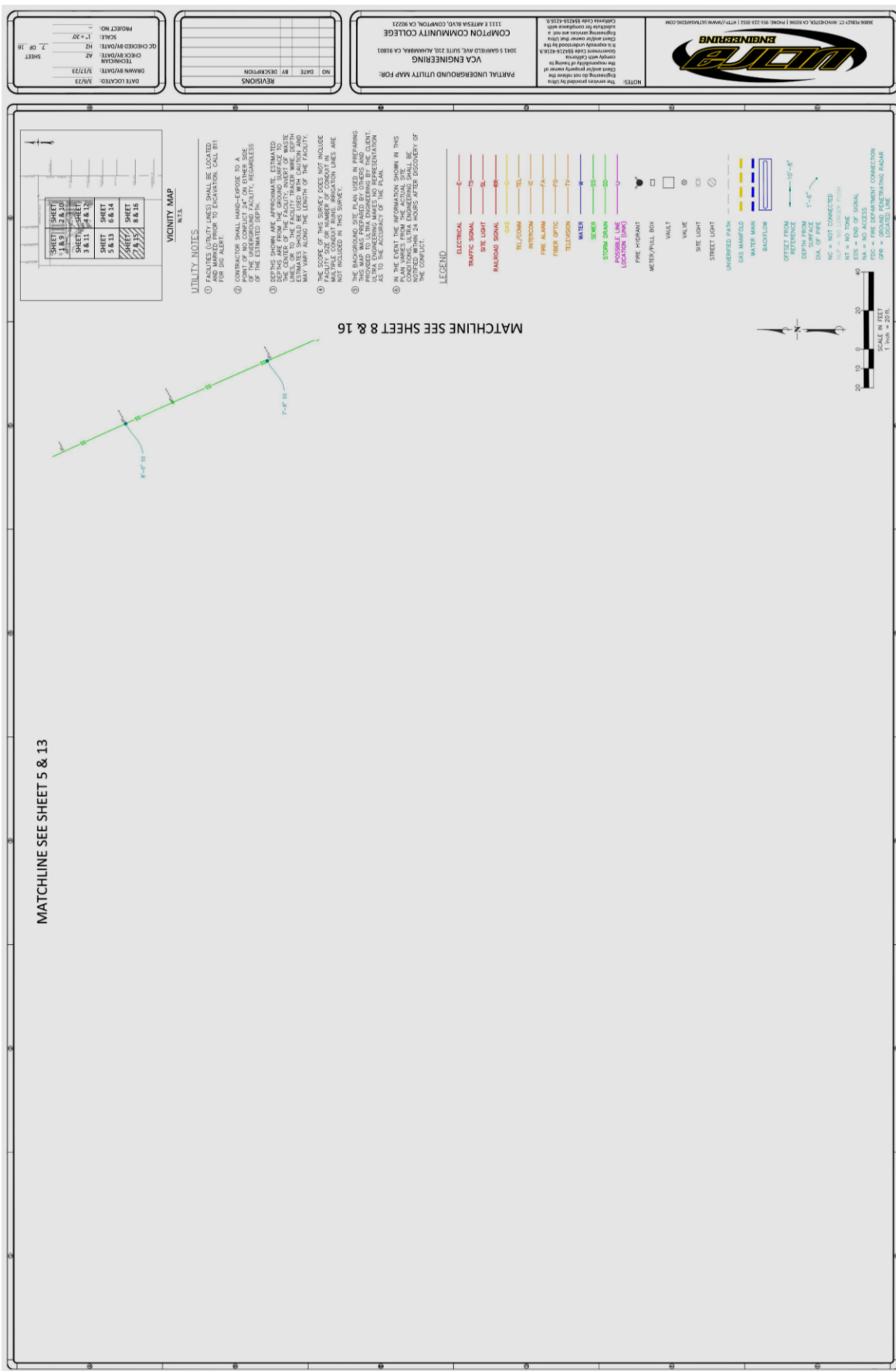
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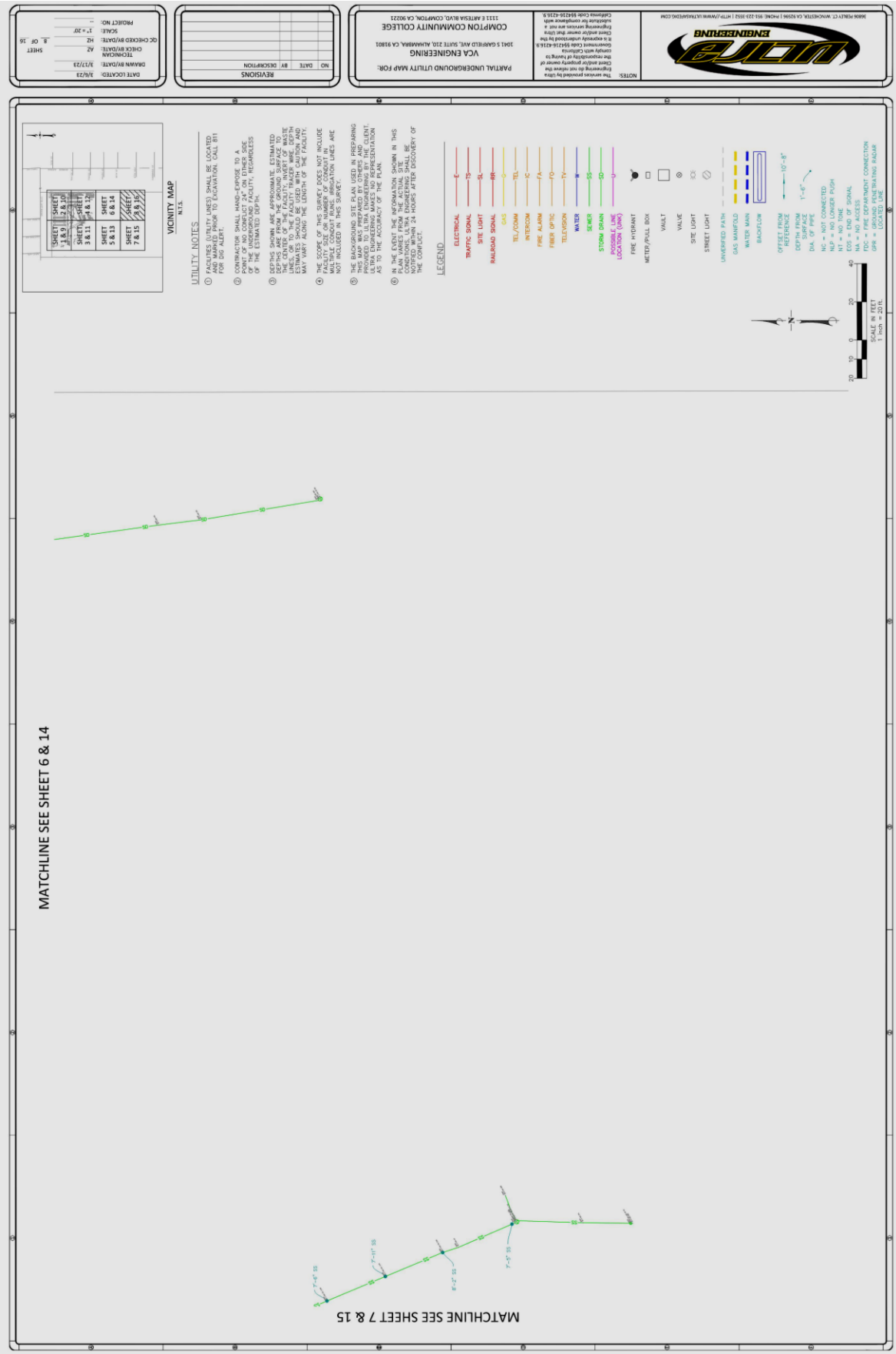
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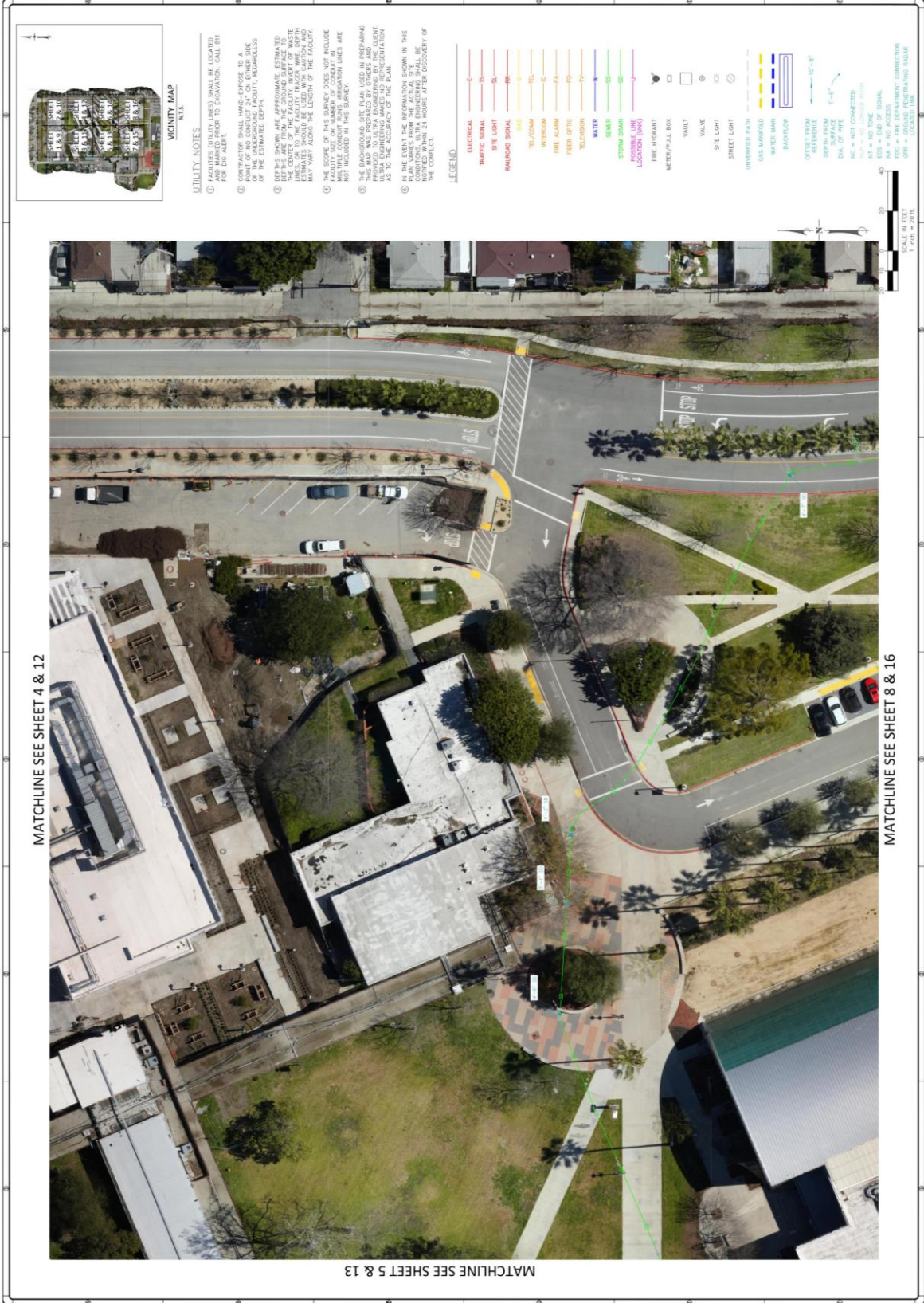
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APPENDIX C

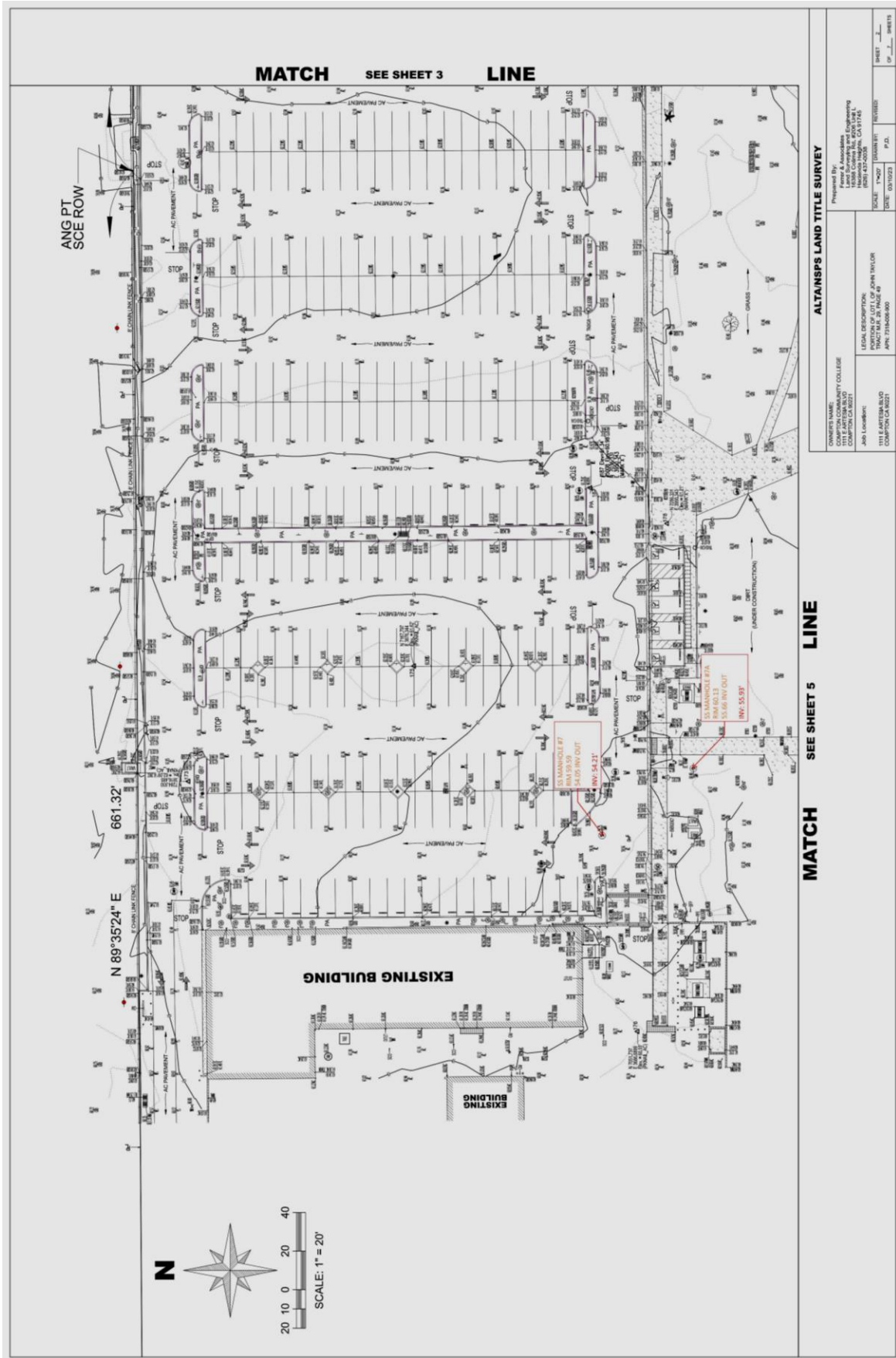
TOPOGRAPHICAL SURVEY

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

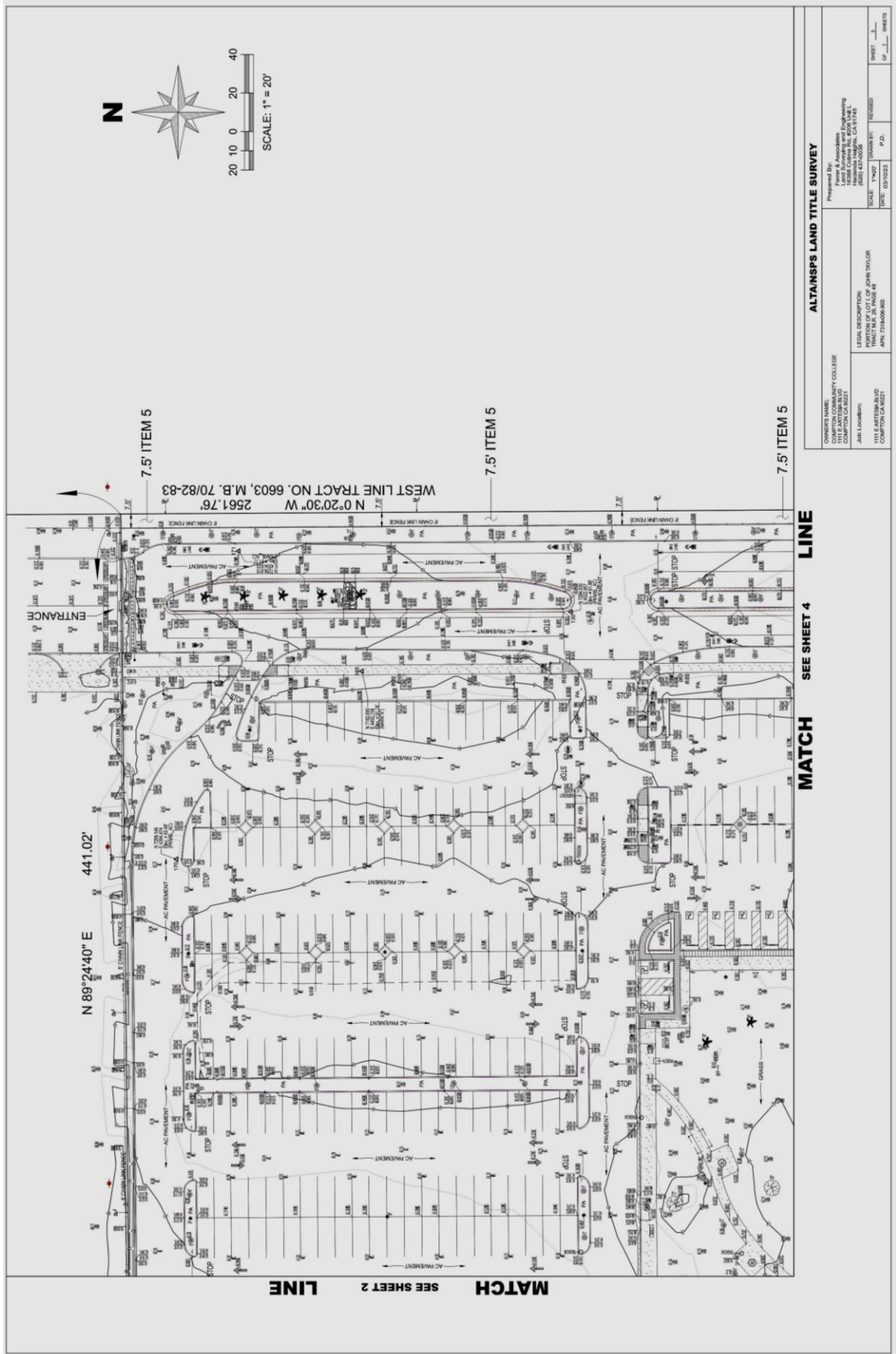
2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com



OWNERS NAME: STATE UNIVERSITY COLLEGE 1111 EASTERN BLVD COMPTON CA 90271		Prepared BY: Ferrer & Associates Engineering 15384 Central Exp. CV# 118 L 15384 Central Exp. CV# 118 L (951) 437-0208	
JOB LOCATION: 1111 EASTERN BLVD COMPTON CA 90271		DATE: 04/10/23	
LEGAL DESCRIPTION: TRACT # 28, PAGE # 47 APN: 775006900		REVISION: P.D.	
		SHEET 1 OF 1 SHEETS	

Los Angeles
 1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

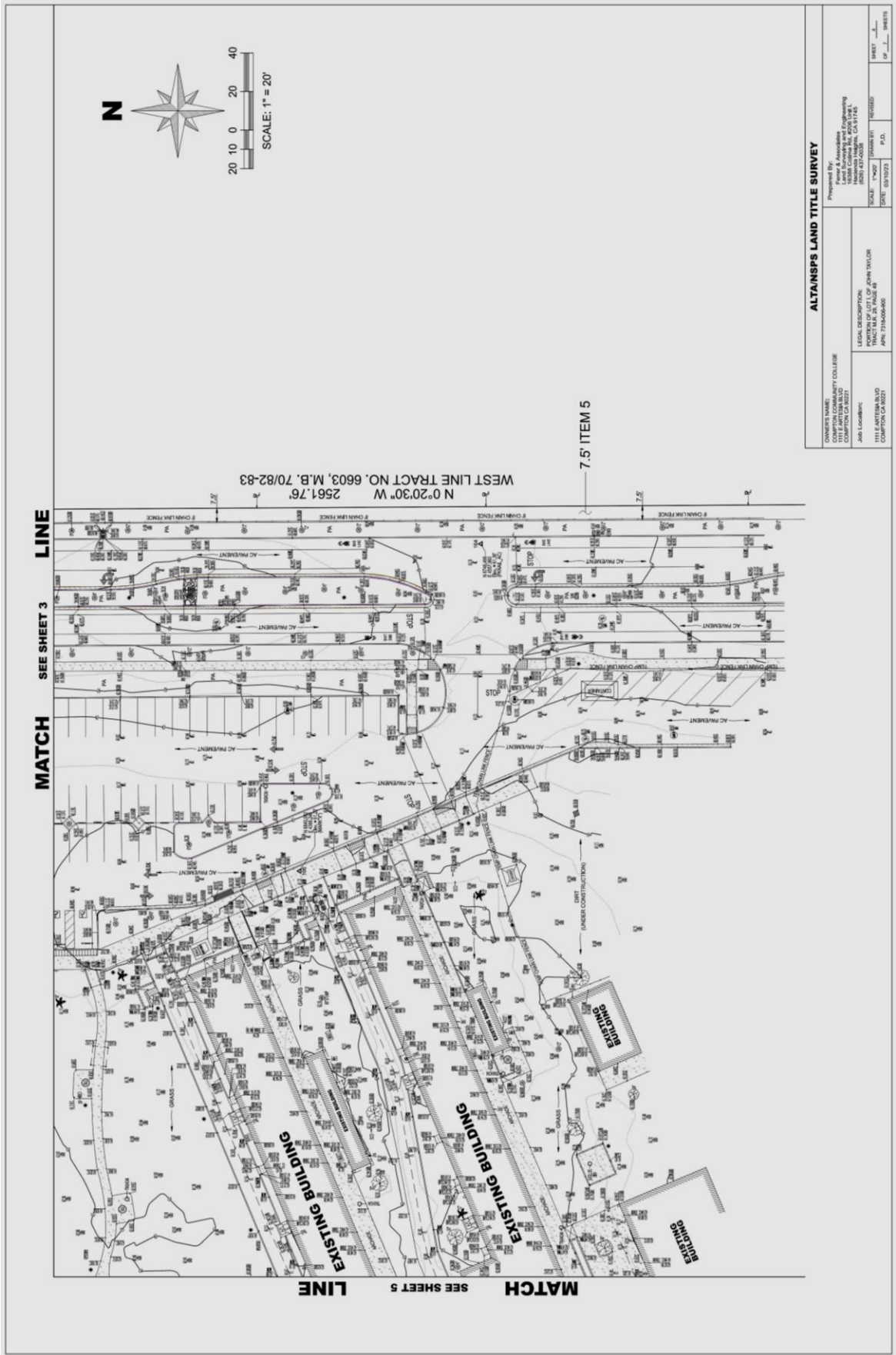
Irvine
 2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com



ALTANSPS LAND TITLE SURVEY	
OWNER'S NAME: SANTA ANITA COMMUNITY COLLEGE 1111 E ARTEMIS BLVD COMPTON CA 90221	Prepared By: Ferre & Associates 16333 Cimarron Rd #208 Los Angeles CA 90048 (818) 421-0208
JOB LOCATION: 1111 E ARTEMIS BLVD COMPTON CA 90221	DATE: 03/19/22 P.D.
LEGAL DESCRIPTION: TRACT NO. 6603, M.B. 70/82-83	SCALE: 1"=20' DRAWN BY: REVISED:
APR: 734008-000	SHEET 4 OF 4 SHEETS

Los Angeles
 1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine
 2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com



ALTA/NSPS LAND TITLE SURVEY			
OWNER'S NAME: SANTA ANITA UNIVERSITY COLLEGE 1111 E ARTISAN BLVD COMPTON CA 90221	Prepared By: VCA & Associates Engineering 16300 Cimarron Rd, Suite 100 Irvine, CA 92614 (949) 457-6028	DATE: 03/15/23	SHEET 1 OF 1 SHEETS
JOB LOCATION: 1111 E ARTISAN BLVD COMPTON CA 90221	LEGAL DESCRIPTION: TRACT NO. 26, PAGE 48 APN: 071800600	SCALE: 1"=20'	DATE: 03/15/23

Los Angeles
 1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine
 2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com



ALTANSPS LAND TITLE SURVEY	
OWNER'S NAME: THE ANTON BELLO CORPORATION (C/S 2221)	Prepared By: VCA Engineering 11111 S. TAYLOR IRVINE, CALIFORNIA 92612 (949) 453-0870
JOB NUMBER: THE ANTON BELLO CORPORATION (C/S 2221)	LEGAL DESCRIPTION: PORTION OF LOT 1 OF JOHN TAYLOR TRACT NO. 28, PAGE 49 47N 12E 28R 49S
DATE: 03/05/21 P.L.D.	REVISION: SHEET 1 OF 1 SHEETS

Los Angeles
 1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine
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LEGAL DESCRIPTION PER PRELIMINARY TITLE REPORT: (CONT.)

PARCEL V (CONT.):
SAND LAND IS REGISTERED UNDER THE LAND TITLE LAW, EXCEPT THEREFROM ALL MINERALS, PETROLEUM, OIL, NATURAL GAS, AND PRODUCTS DERIVED THEREFROM, WITHIN OR UNDERLYING SAID LAND OR THAT MAY BE PRODUCED THEREFROM, AND ALL RIGHTS THEREOF PROVIDED, HOWEVER, THAT FIRST PARTY, ITS SUCCESSORS OR ASSIGNS, SHALL HAVE THE RIGHT TO ENTER BENEATH THE SURFACE OF SAID LAND BY LATERAL OR SLANT DRILLING AND BORING FOR SUCH PURPOSES PROVIDED, FURTHER, THAT IN SO DOING FIRST PARTY, ITS SUCCESSORS OR ASSIGNS, SHALL NOT DISTURB THE SURFACE OF SAID LAND, OR ANY IMPROVEMENTS THEREON, AS EXCEPTED AND RESERVED IN THE DEED FROM SOUTHERN PACIFIC COMPANY, A CORPORATION, TO COMPTON JUNIOR COLLEGE DISTRICT OF LOS ANGELES COUNTY, REGISTERED NOVEMBER 5, 1997, IN THE OFFICE OF THE REGISTRAR OF TITLES.

PARCEL VI:
THOSE PORTIONS OF LOTS 2, 4, 5, AND 6 OF THE JOHN TAYLOR TRACT, PARTLY IN THE CITY OF LONG BEACH, AND PARTLY IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 29 PAGE 49 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT THE INTERSECTION OF THE SOUTHERLY LINE OF SAID LOT 2, WITH A LINE PARALLEL WITH AND DISTANT WESTERLY 250 FEET, MEASURED AT RIGHT ANGLES, FROM THE WESTERLY LINE, AND ITS SOUTHERLY PROLONGATION, OF TRACT NO. 6603, AS PER MAP RECORDED IN BOOK 70 PAGES 82 AND 83 OF MAPS, RECORDS OF SAID COUNTY, THENCE ALONG SAID SOUTHERLY LINE, NORTH 89° 54' EAST 250 FEET TO THE SOUTHERLY PROLONGATION OF SAID WESTERLY LINE, THENCE ALONG NORTH 02° 10' EAST 2949.08 FEET TO THE SOUTHERLY LINE OF THE LAND DESCRIBED IN DEED TO SOUTHERN CALIFORNIA EDISON COMPANY, FILED AS DOCUMENT NO. 156994 UNDER CERTIFICATE OF TITLE NO. F435077, IN THE OFFICE OF THE REGISTRAR OF TITLES OF SAID COUNTY; THENCE ALONG SAID LAST MENTIONED SOUTHERLY LINE SOUTH 87° 54' WEST 250 FEET TO A LINE PARALLEL WITH AND DISTANT WESTERLY 250 FEET MEASURED AT RIGHT ANGLES, FROM SAID WESTERLY LINE OF TRACT NO. 6603; THENCE SOUTH 00° 02' 10" WEST 2949.08 FEET TO THE POINT OF BEGINNING.

EXCEPT THEREFROM THE SOUTHERLY 38.5 FEET THEREOF. SAID LAND IS REGISTERED UNDER THE LAND TITLE LAW.

EXCEPTING THEREFROM ALL MINERALS, PETROLEUM, OIL, NATURAL GAS, AND PRODUCTS DERIVED THEREFROM, WITHIN OR UNDERLYING SAID LAND OR THAT MAY BE PRODUCED THEREFROM, AND ALL RIGHTS THEREOF PROVIDED, HOWEVER, THAT FIRST PARTY, ITS SUCCESSORS OR ASSIGNS, SHALL HAVE THE RIGHT TO ENTER BENEATH THE SURFACE OF SAID LAND BY LATERAL OR SLANT DRILLING AND BORING FOR SUCH PURPOSES PROVIDED, FURTHER, THAT IN SO DOING FIRST PARTY, ITS SUCCESSORS OR ASSIGNS, SHALL NOT DISTURB THE SURFACE OF SAID LAND, OR ANY IMPROVEMENTS THEREON, AS EXCEPTED AND RESERVED IN THE DEED FROM SOUTHERN PACIFIC COMPANY, A CORPORATION, TO COMPTON JUNIOR COLLEGE DISTRICT OF LOS ANGELES COUNTY, REGISTERED NOVEMBER 5, 1997, IN THE OFFICE OF THE COUNTY REGISTRAR OF TITLES.

PARCEL VII:
THAT PORTION OF LOT 9 OF THE HELLMAN TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 2 PAGE 924 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT IN THE SOUTHERLY LINE OF SAID LOT, DISTANT NORTH 89° 54' EAST 617.28 FEET FROM THE SOUTHWESTERLY CORNER OF SAID LOT; THENCE NORTH 00° 06' WEST 650.00 FEET TO THE TRUE POINT OF BEGINNING; THENCE NORTH 60° 44' EAST 607.22 FEET TO THE BEGINNING OF A TANGENT CURVE CONCAVE NORTHERLY, HAVING A RADIUS OF 502.68 FEET; THENCE EASTERLY ALONG THE ARC OF SAID CURVE A DISTANCE OF 54.27 FEET TO A POINT IN THE EASTERLY LINE OF SAID LOT 9, SAID EASTERLY LINE BEING ALSO THE WESTERLY LINE OF LOT 1 OF THE JOHN TAYLOR TRACT, AS PER MAP RECORDED IN BOOK 70 PAGES 82 AND 83 OF MAPS, RECORDS OF SAID COUNTY, THENCE SOUTHWESTERLY ALONG THE EASTERLY LINE NORTH 00° 06' WEST 563.32 FEET TO A POINT IN A CURVE CONCAVE NORTHERLY HAVING A RADIUS OF 452.64 FEET, BEING CONCENTRIC WITH AND DISTANT NORTHERLY 50 FEET; MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET, SAID POINT BEING ALSO SOUTHEASTERLY CORNER OF THE LAND DESCRIBED IN PARCEL 3 OF THE DEED TO HARVEY MACHINE CO., INC., RECORDED ON DECEMBER 31, 1946, AS INSTRUMENT NO. 1870, IN BOOK 2596A PAGE 248, OF OFFICIAL RECORDS OF SAID COUNTY; THENCE WESTERLY ALONG THE ARC HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET, MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET, TO THE POINT OF BEGINNING; THENCE SOUTH ALONG SAID PARALLEL LINE 1029.88 FEET TO THE POINT OF BEGINNING.

PARCEL VIII:
THAT PORTION OF LOT 9 OF THE HELLMAN TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 2 PAGE 924 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT IN THE SOUTHERLY LINE OF SAID LOT, DISTANT NORTH 89° 54' EAST 617.28 FEET FROM THE SOUTHWESTERLY CORNER OF SAID LOT; THENCE NORTH 00° 06' WEST 650.00 FEET TO THE TRUE POINT OF BEGINNING; THENCE NORTH 60° 44' EAST 607.22 FEET TO THE BEGINNING OF A TANGENT CURVE CONCAVE NORTHERLY, HAVING A RADIUS OF 502.68 FEET; THENCE EASTERLY ALONG THE ARC OF SAID CURVE A DISTANCE OF 54.27 FEET TO A POINT IN THE EASTERLY LINE OF SAID LOT 9, SAID EASTERLY LINE BEING ALSO THE WESTERLY LINE OF LOT 1 OF THE JOHN TAYLOR TRACT, AS PER MAP RECORDED IN BOOK 70 PAGES 82 AND 83 OF MAPS, RECORDS OF SAID COUNTY, THENCE SOUTHWESTERLY ALONG THE EASTERLY LINE NORTH 00° 06' WEST 563.32 FEET TO A POINT IN A CURVE CONCAVE NORTHERLY HAVING A RADIUS OF 452.64 FEET, BEING CONCENTRIC WITH AND DISTANT NORTHERLY 50 FEET; MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET, SAID POINT BEING ALSO SOUTHEASTERLY CORNER OF THE LAND DESCRIBED IN PARCEL 3 OF THE DEED TO HARVEY MACHINE CO., INC., RECORDED ON DECEMBER 31, 1946, AS INSTRUMENT NO. 1870, IN BOOK 2596A PAGE 248, OF OFFICIAL RECORDS OF SAID COUNTY; THENCE WESTERLY ALONG THE ARC HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET, MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET, TO THE POINT OF BEGINNING; THENCE SOUTH ALONG SAID PARALLEL LINE 1029.88 FEET TO THE POINT OF BEGINNING.

LEGAL DESCRIPTION PER PRELIMINARY TITLE REPORT: (CONT.)

PARCEL II (CONT.):
1029.88 FEET TO THE POINT OF BEGINNING; THENCE SOUTH 1029.88 FEET TO THE POINT OF BEGINNING.

PARCEL III:
THAT PORTION OF LOT 1 OF THE JOHN TAYLOR TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS SHOWN ON THE MAP RECORDED IN BOOK 29 PAGE 49 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT IN THE WESTERLY LINE OF SAID LOT 1, SAID POINT BEING THE NORTHEASTERLY CORNER OF LOT 9 OF THE HELLMAN TRACT AS SHOWN ON MAP RECORDED IN BOOK 2 PAGE 924, ET SEQ., MISCELLANEOUS RECORDS IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, THENCE ALONG THE WESTERLY LINE OF SAID LOT 1, THENCE ALONG SAID WESTERLY LINE NORTH 89° 54' WEST 398.52 FEET TO A LINE PARALLEL WITH AND DISTANT WESTERLY 250 FEET TO THE POINT OF BEGINNING.

PARCEL IV:
THOSE PORTIONS OF LOTS 1, 2 AND 4 OF THE JOHN TAYLOR TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS SHOWN ON MAP RECORDED IN BOOK 29 PAGE 49 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT THE INTERSECTION OF THE EASTERLY PROLONGATION OF THE NORTHERLY LINE OF LOT 1, WITH AND DISTANT 488.52 FEET EASTERLY AT RIGHT ANGLES FROM THE WESTERLY LINE OF SAID LOT 1; THENCE ALONG SAID PARALLEL LINE SOUTH 182.33 FEET TO THE BEGINNING OF A TANGENT CURVE CONCAVE NORTHWESTERLY AND HAVING A RADIUS OF 502.68 FEET; THENCE SOUTHWESTERLY ALONG SAID CURVE THROUGH A CENTRAL ANGLE OF 83° 46' 53" A DISTANCE OF 735.34 FEET TO THE WESTERLY LINE OF SAID LOT 1; THENCE ALONG SAID WESTERLY LINE SOUTH 67.00 FEET TO THE SOUTHERLY CORNER OF SAID LOT 1; THENCE ALONG SAID SOUTHERLY LINE SOUTH 87° 54' WEST 250 FEET TO THE POINT OF BEGINNING.

PARCEL V:
THAT PORTION OF LOT 10 OF THE JOHN TAYLOR TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 29 PAGE 49 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT THE INTERSECTION OF THE EASTERLY PROLONGATION OF THE NORTHERLY LINE OF LOT 9 OF THE HELLMAN TRACT, AS PER MAP RECORDED IN BOOK 2 PAGE 924 ET SEQ., OF MISCELLANEOUS RECORDS OF SAID COUNTY, WITH A LINE THAT IS PARALLEL WITH AND DISTANT EASTERLY 448.52 FEET, MEASURED AT RIGHT ANGLES, FROM THE WESTERLY LINE OF SAID LOT 1; THENCE ALONG SAID PARALLEL LINE NORTH 00° 06' WEST 563.32 FEET TO A POINT IN A CURVE CONCAVE NORTHERLY HAVING A RADIUS OF 502.68 FEET; THENCE SOUTHWESTERLY ALONG SAID CURVE THROUGH A CENTRAL ANGLE OF 83° 46' 53" A DISTANCE OF 735.34 FEET TO THE WESTERLY LINE OF SAID LOT 1; THENCE NORTH ALONG SAID WESTERLY LINE 50.32 FEET TO A POINT IN A CURVE CONCAVE NORTHERLY HAVING A RADIUS OF 452.68 FEET, SAID CURVE BEING CONCENTRIC WITH AND DISTANT NORTHERLY 50 FEET, MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET; THENCE NORTHEASTERLY ALONG THE ARC HEREBEFORE MENTIONED AS HAVING A RADIUS OF 452.68 FEET, MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 452.68 FEET, TO THE POINT OF BEGINNING; THENCE SOUTH ALONG SAID PARALLEL LINE 1029.88 FEET TO THE POINT OF BEGINNING.

PARCEL VI:
THAT PORTION OF LOT 10 OF THE JOHN TAYLOR TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 29 PAGE 49 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT THE INTERSECTION OF THE EASTERLY PROLONGATION OF THE NORTHERLY LINE OF LOT 9 OF THE HELLMAN TRACT, AS PER MAP RECORDED IN BOOK 2 PAGE 924 ET SEQ., OF MISCELLANEOUS RECORDS OF SAID COUNTY, WITH A LINE THAT IS PARALLEL WITH AND DISTANT EASTERLY 448.52 FEET, MEASURED AT RIGHT ANGLES, FROM THE WESTERLY LINE OF SAID LOT 1; THENCE ALONG SAID PARALLEL LINE NORTH 00° 06' WEST 563.32 FEET TO A POINT IN A CURVE CONCAVE NORTHERLY HAVING A RADIUS OF 502.68 FEET; THENCE SOUTHWESTERLY ALONG SAID CURVE THROUGH A CENTRAL ANGLE OF 83° 46' 53" A DISTANCE OF 735.34 FEET TO THE WESTERLY LINE OF SAID LOT 1; THENCE NORTH ALONG SAID WESTERLY LINE 50.32 FEET TO A POINT IN A CURVE CONCAVE NORTHERLY HAVING A RADIUS OF 452.68 FEET, SAID CURVE BEING CONCENTRIC WITH AND DISTANT NORTHERLY 50 FEET, MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 502.68 FEET; THENCE NORTHEASTERLY ALONG THE ARC HEREBEFORE MENTIONED AS HAVING A RADIUS OF 452.68 FEET, MEASURED RADially FROM THE CURVE HEREBEFORE MENTIONED AS HAVING A RADIUS OF 452.68 FEET, TO THE POINT OF BEGINNING; THENCE SOUTH ALONG SAID PARALLEL LINE 1029.88 FEET TO THE POINT OF BEGINNING.

SURVEYOR'S NOTES:

- 1. THE FOLLOWING TITLE REPORT WAS RELIED UPON IN THE PREPARATION OF THIS SURVEY: TITLE REPORT NO. LT-2005-0119296 BY: LANDAMERICA LAWYERS TITLE
2. TITLE REPORT CITED FOR FULL EXCEPTIONS AND EXCLUSIONS DISCLOSED THEREWITH.
3. ZONING DISTRICT: THIS PROPERTY IS LOCATED IN ZONING RM - MEDIUM DENSITY RESIDENTIAL.
4. UTILITY NOTES: THE LOCATION OF UTILITIES SHOWN HEREON ARE FROM OBSERVED EVIDENCE OF ABOVE GROUND APPURTENANCES. THE SURVEYOR MAKES NO GUARANTEE THAT THE UNDERGROUND UTILITIES SHOWN COMPRISE ALL SUCH UTILITIES IN THE AREA, EITHER IN SERVICE OR ABANDONED. THE SURVEYOR FURTHER DOES NOT WARRANT THAT THE UNDERGROUND UTILITIES SHOWN ARE IN THE EXACT LOCATION INDICATED ALTHOUGH HE DOES CERTIFY THAT THEY ARE LOCATED FROM THE INFORMATION PROVIDED. THE SURVEYOR HAS NOT PHYSICALLY LOCATED THE UNDERGROUND UTILITIES.
5. FLOOD ZONE: PROPERTY IS LOCATED WITHIN SHARED ZONE V PER FEMA FLOOD INSURANCE RATE MAP NUMBER 98010118Z, CD, 03 DEPTEMBER, 2006. SHARED ZONE V INDICATES ANS OF 2% ANNUAL CHANCE FLOOD AREAS OF 1% ANNUAL CHANCE FLOOD WITH AVERAGE DEPTHS OF LESS THAN 1 FOOT OR WITH DRAINAGE AREAS LESS THAN 1 SQUARE MILE, AND AREAS PROTECTED BY LEVEES FROM 1% ANNUAL CHANCE FLOOD.
6. THE BASIS OF BEARINGS FOR THIS ALTAIRNSP LAND TITLE SURVEY IS N 07°15'19" W FOR THE CENTER LINE OF SANTA FE AVENUE AS SHOWN ON PAVEMENT MAP No. 16478, M.A. 102, PAGES 16/48, RECORDED IN THE OFFICE OF THE COUNTY RECORDER OF LOS ANGELES COUNTY.
7. THE VERTICAL BENCHMARK FOR THIS ALTAIRNSP LAND TITLE SURVEY IS A LOS ANGELES COUNTY CORNER WORKING BENCHMARK 379529, BEING ALATAG L286411 E CB SUSANA RD 0.5FT S/O BCR @ SE COR ARTESIA BLVD.
8. DATUM: NAD 1983. ELEVATION = 57.108 FEET (2013 ADJUSTMENT)
9. CONTOUR INTERVAL = 0.50'
10. THE PROPERTY ADDRESS IS 1111 E ARTESIA BLVD, COMPTON CA 90221.
11. THE ASSESSOR'S PARCEL NUMBER IS 7318-006-000.

LEGAL DESCRIPTION PER PRELIMINARY TITLE REPORT:

THE FOLLOWING LEGAL DESCRIPTION IS PER TITLE REPORT, ORDER NO. LT-2005-0119296, PREPARED BY LANDAMERICA LAWYERS TITLE. THE LAND REFERRED TO HEREIN BELOW IS SITUATED IN THE COUNTY OF LOS ANGELES, STATE OF CALIFORNIA AND IS DESCRIBED AS FOLLOWS:

PARCEL I:
THAT PORTION OF LOT 10 OF THE JOHN TAYLOR TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 29 PAGE 49 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT IN THE WESTERLY LINE OF SAID LOT 1, SAID POINT BEING THE NORTHEASTERLY CORNER OF LOT 9 OF THE HELLMAN TRACT AS SHOWN ON MAP RECORDED IN BOOK 2 PAGE 924 ET SEQ., OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, THENCE ALONG THE EASTERLY PROLONGATION OF THE NORTHERLY LINE OF SAID LOT 9, NORTH 89° 54' OOK EAST 398.52 FEET TO A LINE THAT IS PARALLEL WITH AND DISTANT 398.52 FEET EASTERLY AT RIGHT ANGLES FROM THE WESTERLY LINE OF SAID LOT 1; THENCE ALONG SAID PARALLEL LINE NORTH 1029.88 FEET TO THE SOUTHERLY LINE OF THE LAND DESCRIBED IN DEED TO SOUTHERN CALIFORNIA EDISON COMPANY, REGISTERED NOVEMBER 5, 1997, IN THE OFFICE OF THE REGISTRAR OF TITLES OF SAID COUNTY; THENCE ALONG SAID SOUTHERLY LINE SOUTH 87° 54' WEST 250 FEET TO THE WESTERLY LINE OF SAID LOT 1; THENCE SOUTH 1029.88 FEET TO THE POINT OF BEGINNING.

PARCEL II:
THOSE PORTIONS OF LOTS 1, 4, 5 AND 6 OF THE JOHN TAYLOR TRACT, IN THE CITY OF COMPTON, COUNTY OF LOS ANGELES, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 29 PAGE 49 OF MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER OF SAID COUNTY, DESCRIBED AS FOLLOWS:

BEGINNING AT THE INTERSECTION OF THE EASTERLY PROLONGATION OF THE NORTHERLY LINE OF LOT 9 OF HELLMAN TRACT AS SHOWN ON MAP RECORDED IN BOOK 2 PAGE 924, ET SEQ., MISCELLANEOUS RECORDS, IN THE OFFICE OF THE COUNTY RECORDER, WITH A LINE THAT IS PARALLEL WITH AND DISTANT WESTERLY 250 FEET TO THE POINT OF BEGINNING; THENCE SOUTH ALONG SAID PARALLEL LINE 1029.88 FEET TO THE POINT OF BEGINNING.

Table with survey details: Owners Name (Altairnsps Land Title Survey), Surveyor Name (VCA Engineering), Date (03/10/2015), and other metadata.

Table with survey details: Owners Name (Altairnsps Land Title Survey), Surveyor Name (VCA Engineering), Date (03/10/2015), and other metadata.

Table with survey details: Owners Name (Altairnsps Land Title Survey), Surveyor Name (VCA Engineering), Date (03/10/2015), and other metadata.

Los Angeles
1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine
2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

APPENDIX D

POTHOLING

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
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e-mail: vca@vcaeng.com

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www.vcaeng.com



**Ultra Engineering Contractors,
Inc.**

31301 Auld Road, Murrieta, CA 92563

1-951-223-3552

Pothole Log Report

for

VCA Engineers, Inc.

Compton

Ultra Engineering Contractors Inc.

License # 971768







Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	005	1111 East Artesia Boulevard, Compton, CA, USA	Other	N/A	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Other	Other	N/A	N/A	N/A	08:05
Utility Comment N/A			Material Comment N/A			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments: No lateral exist jump inside storm drain and confirmed no lateral comes in from that area took pictures						

Ultra Engineering Contractors Inc.

License # 971768



Los Angeles

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	006	1111 East Artesia Boulevard, Compton, CA, USA	Asphalt	4"	Class II	2"
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Storm Drain	RCP	24"	C-1.90	C-3.90	08:23

Utility Comment -

Material Comment -



Pothole:



Measurement:



Utility:



Proximity:

Comments:

Ultra Engineering Contractors Inc.

License # 971768



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 www.vcaeng.com

Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	004	1111 East Artesia Boulevard, Compton, CA, USA	Other	DIP	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Sewage	RCP	24"	C-1.70	C-3.70	10:11
Utility Comment -			Material Comment -			
Pothole:			Measurement:			
Utility:			Proximity:			
Comments:						

Ultra Engineering Contractors Inc.

License # 971768







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 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	003	1111 East Artesia Boulevard, Compton, CA, USA	Other	DIP	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Sewage	PVC	6"	C-3.80	C-4.30	09:07
Utility Comment -			Material Comment -			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Los Angeles

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 Tel: 323-729-6098 ▪ Fax: 323-729-6043
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Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	003 A	1111 East Artesia Boulevard, Compton, CA, USA	Other	DIP	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Sewage	Steel	4"	C-3.20	C-3.53	09:09
Utility Comment -			Material Comment -			
Pothole:			Measurement:			
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	001	1111 East Artesia Boulevard, Compton, CA, USA	Other	DIP	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Sewage	PVC	6"	C-7.10	C-7.60	09:40
Utility Comment -			Material Comment -			
Pothole:			Measurement:			
Utility:			Proximity:			
Comments: Manhole # 3						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	002	1111 East Artesia Boulevard, Compton, CA, USA	Other	DIP	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Sewage	PVC	6"	C-6.75	C-7.25	09:48
Utility Comment -			Material Comment -			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/22/2023	007	1111 East Artesia Boulevard, Compton, CA, USA	Other	DIP	None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
	Sewage	PVC	10"	C-7.55	C-8.40	
Utility Comment -			Material Comment -			
Pothole:			Measurement:			
Utility:			Proximity:			
Comments: ManHole # 3						

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 e-mail: vca@vcaeng.com

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/25/2023	007A	1111 East Artesia Boulevard, Compton, CA, USA	Other	DIP	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Sewage	PVC	6"	C-7.60	C-8.10	
Utility Comment -			Material Comment -			
Pothole:			Measurement:			
Utility:			Proximity:			
Comments:						

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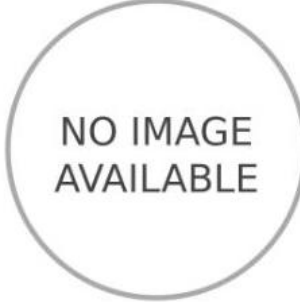


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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
09/25/2023	Manhole 2	1111 East Artesia Boulevard, Compton, CA, USA	Other	-	None	-
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
-	Other	Other	-	-	-	07:54
Utility Comment -			Material Comment -			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			

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Comments: Unable to do Manhole #2 because we were not allowed to be on jobsite without permission from superintendent

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**Ultra Engineering Contractors,
Inc.**

31301 Auld Road, Murrieta, CA 92563

1-951-223-3552

Pothole Log Report

for

VCA Engineers, Inc.

Compton

Ultra Engineering Contractors Inc.

License # 971768







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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	1	In front of Allied health building	Asphalt	6"	Class II	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
0	Water	Steel	13"	-5.25	-6.33	07:01
Utility Comment			Material Comment			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	2	In front of instructional building, number one	Soil		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
0	Water	PVC	7" o.d.	-3.40	-3.98	09:24
Utility Comment			Material Comment			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	2a	In front of instructional building, number one	Soil		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
0	Other	Concrete Case	48"	-4.40	-5.20	
Utility Comment			Material Comment			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	003	Instructional building one	Soil		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
	Comm.	Concrete	60"	-2.20	-9.00	10:21
Utility Comment			Material Comment			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	004	Instructional building one	Soil		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
	Electric	Concrete	60"	-2.40	-9.90	11:09
Utility Comment			Material Comment			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	5	Near Lot F	Other		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
0	Sewage	Steel	6"	-5.00	-5.50	11:44
Utility Comment			Material Comment			
Pothole:			Measurement:			
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	6	In front of F building	Other		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
0	Sewage	PVC	12"	-2.50	-3.50	12:41
Utility Comment			Material Comment			
Pothole:			Measurement:			
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	7	Building F	Other		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
0	Sewage	VCP	6"	-5.10	-5.60	12:15
Utility Comment			Material Comment			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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Date	PH	Location	Surface Material	Surface Depth	Base Material	Base Depth
04/12/2023	8	In front of student services	Other		None	
Offset	Utility Type	Material Type	Size	Depth Top	Depth Bottom	Time
0	Sewage	VCP	6"	-5.60	-6.10	12:26
Utility Comment			Material Comment			
						
Pothole:			Measurement:			
						
Utility:			Proximity:			
Comments:						

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APPENDIX E

ADDITIONAL MANHOLE RIM ELEVATION SURVEY

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

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e-mail: vca@vcaeng.com

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 e-mail: vca@vcaeng.com

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 e-mail: vca@vcaeng.com

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APPENDIX F

UTILITY INFRASTRUCTURE-PHASE 1 SET DRAWINGS

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e-mail: vca@vcaeng.com

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Tel: 949-679-0870 ▪ Fax: 949-679-9370
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S&K
 S&K ENGINEERING, INC.
 10145 GARFIELD AVE. #210
 ALHAMBRA, CALIFORNIA 91801
 TEL: 323-729-6098 FAX: 323-729-6043
 WWW.VCAENG.COM
 Job No: 08872

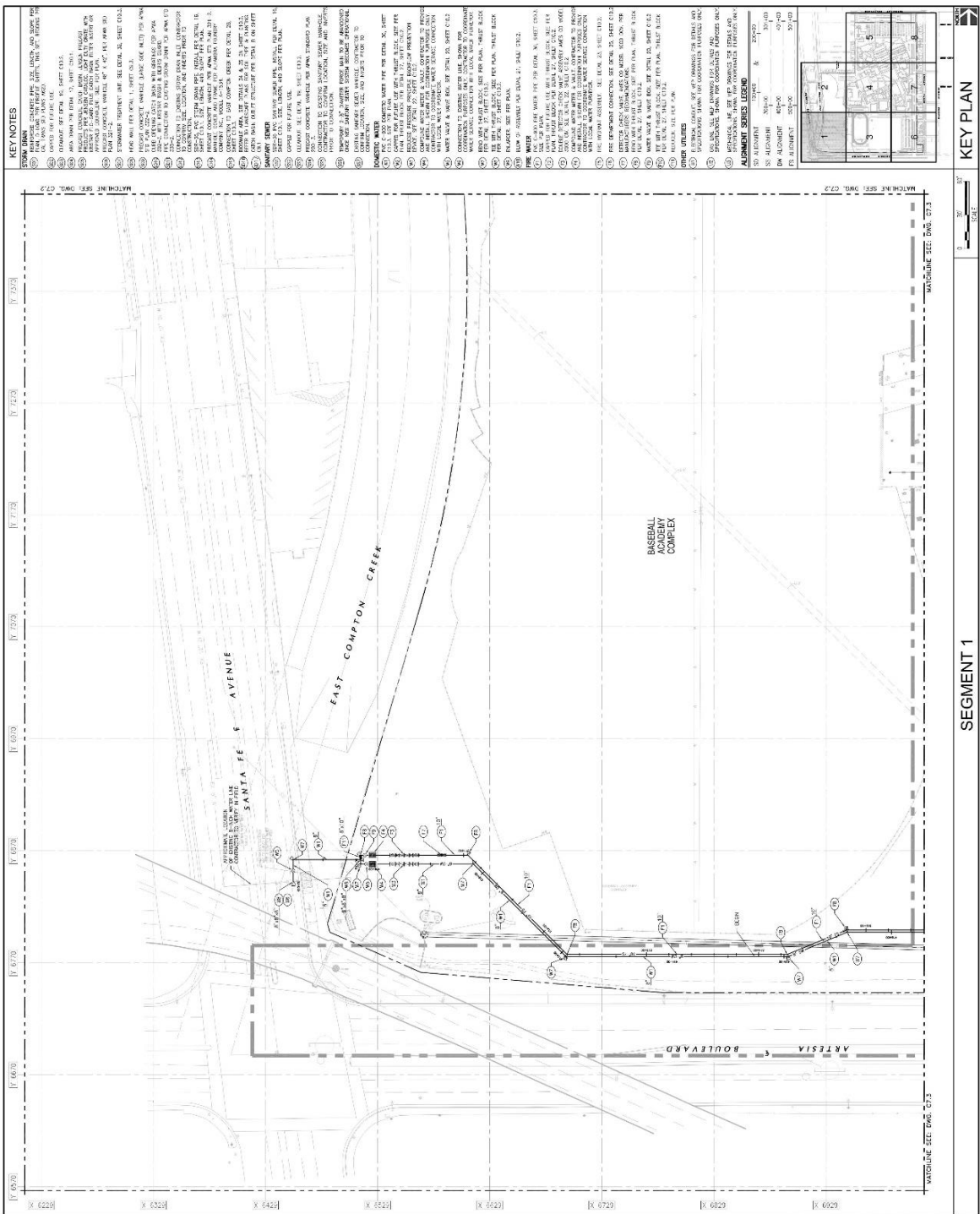
**EL CAMINO COLLEGE
 COMPTON COMMUNITY EDUCATIONAL CENTER
 UTILITY INFRASTRUCTURE - PHASE 1
 CONTRACT DOCUMENTS**

1111 E ARTESIA BLVD. - COMPTON, CA 90721

DATE: 01/17/17
 DRAWN BY: 101222
 CHECKED BY: 101222
 DESIGNED BY: 101222
 PROJECT NO: 17-000000
 SHEET NO: 01-000000


DRAWING TITLE: UTILITY PLAN
 SEGMENT 1

C7.1
 44 OF 65







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 e-mail: vca@vcaeng.com

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 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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S&K
ENGINEERING
1000 WEST 10TH STREET
MORNING HAVEN, CALIFORNIA 91768
TEL: 951-261-7700 FAX: 951-261-7727



COMPTON COMMUNITY COLLEGE DISTRICT
EL CAMINO COLLEGE
COMPTON COMMUNITY EDUCATIONAL CENTER
UTILITY INFRASTRUCTURE - PHASE 1
CONTRACT DOCUMENTS
7311 E. ARTISSA BLVD. - COMPTON, CA 90221

DATE: January 21, 2013

DESIGNED BY: S&K/E

CHECKED BY: S&K/E

PROJECT NO: 13-001

DATE: 01/21/13

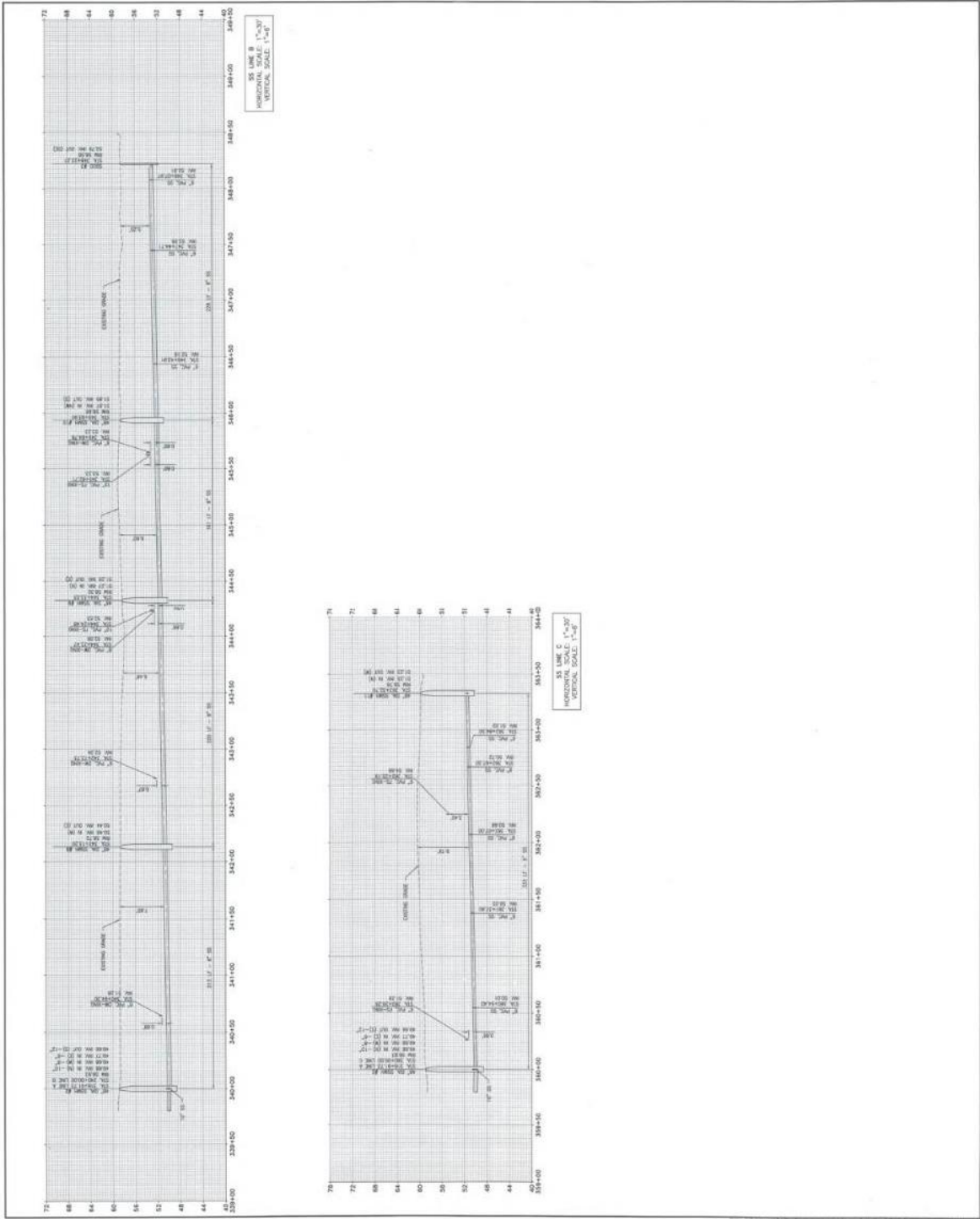
SCALE: 1"=40'

REVISIONS

NO.	DESCRIPTION	DATE


REVISION: 1103
SANITARY SEWER LINE
B AND C PROFILE

DRAWING NO: **C9.5**






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e-mail: vca@vcaeng.com


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SUNSHINE ENGINEERING & ARCHITECTURE
101 EAST HUNTINGTON DRIVE
MONROVIA, CALIFORNIA 91766
TEL: 626-251-1177 FAX: 626-251-1177

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REGISTERED PROFESSIONAL ARCHITECT

COMPTON COMMUNITY COLLEGE DISTRICT
EL CAMINO COLLEGE
COMPTON COMMUNITY EDUCATIONAL CENTER
UTILITY INFRASTRUCTURE - PHASE 1
1111 E. ARTESIA BLVD. - COMPTON, CA 90221

DATE: January 22, 2013

DESIGNED BY: R.L.S.

CHECKED BY: R.L.S.

REVISIONS

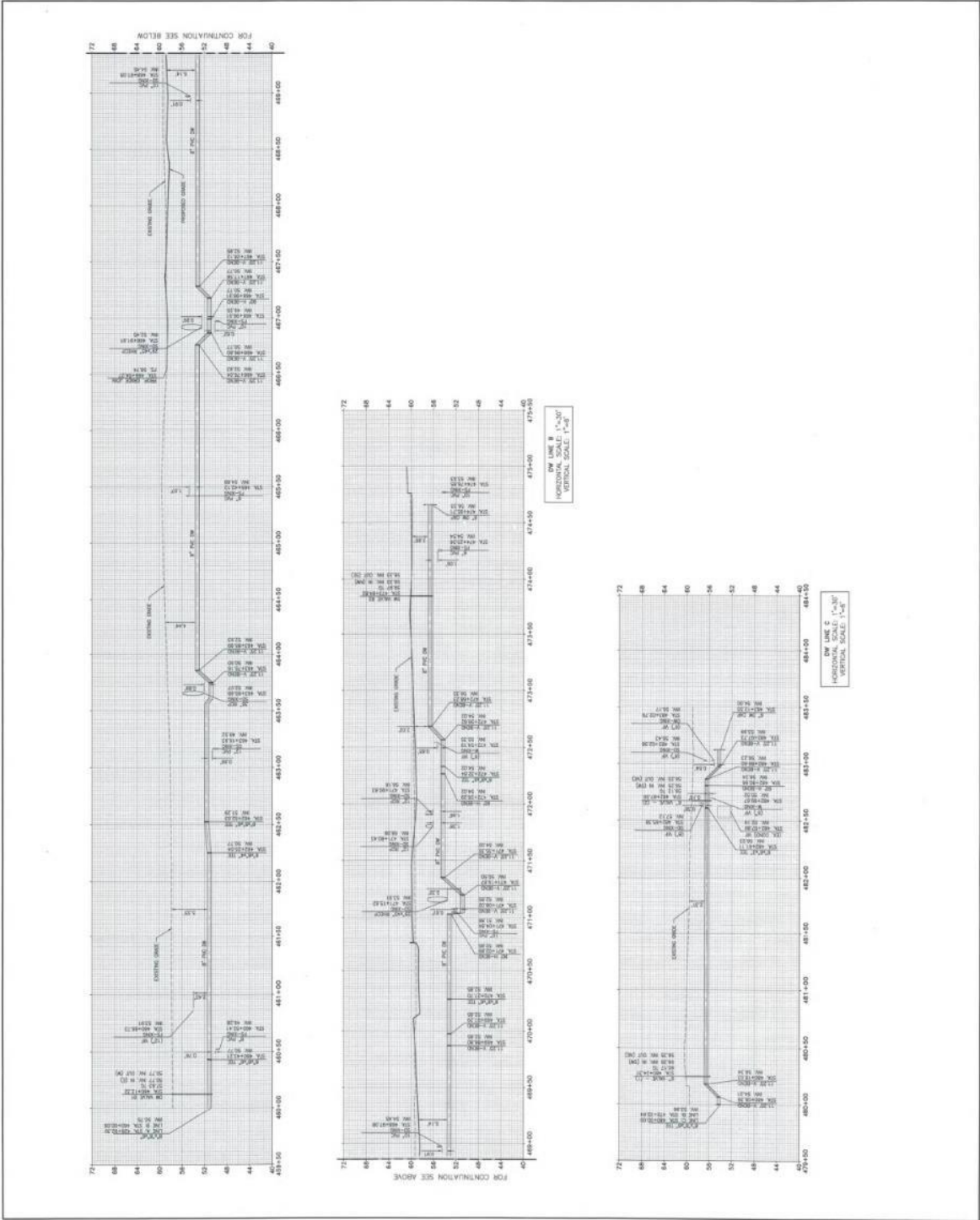
NO.	DESCRIPTION	DATE
1	ISSUE FOR PERMIT	01/22/13

DRAWING TITLE

**DOMESTIC WATER
LINE B PROFILE**

DRAWING NO.

C99



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e-mail: vca@vcaeng.com

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Tel: 949-679-0870 ▪ Fax: 949-679-9370
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SPECIALTY CONTRACTORS
10000 VAN NUYS BLVD., SUITE 100
VAN NUYS, CALIFORNIA 91411
TEL: 818-708-1188 FAX: 818-708-1482

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CIVIL
STATE OF CALIFORNIA
NO. 44521

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CIVIL
STATE OF CALIFORNIA
NO. 44521

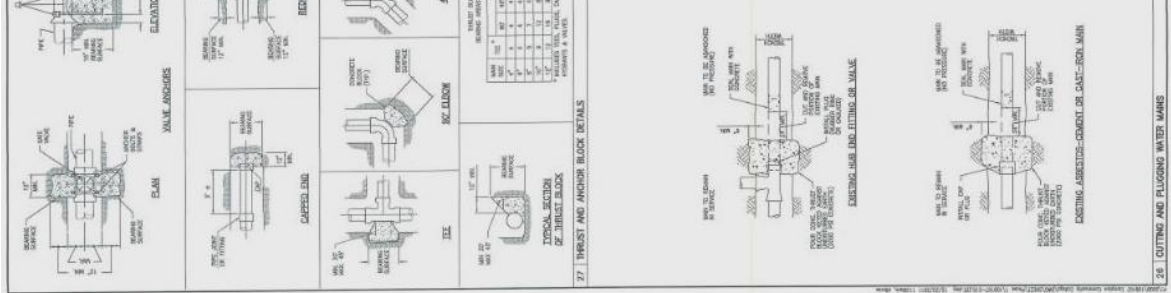
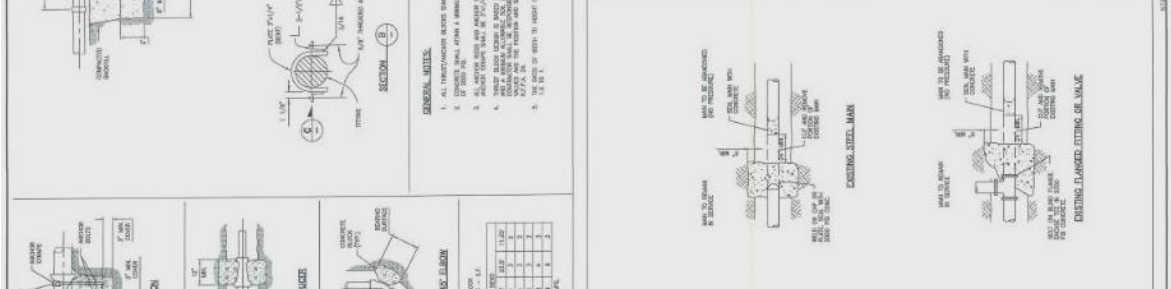
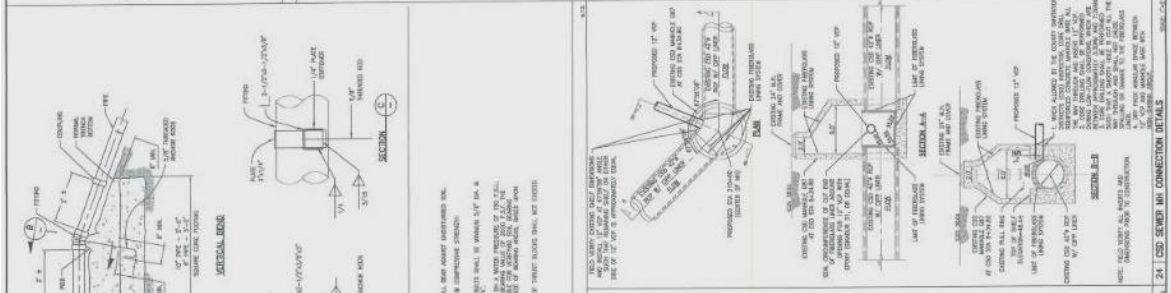
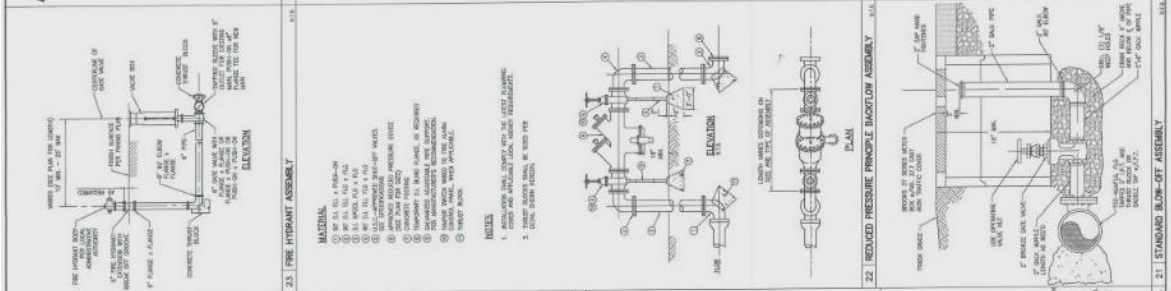
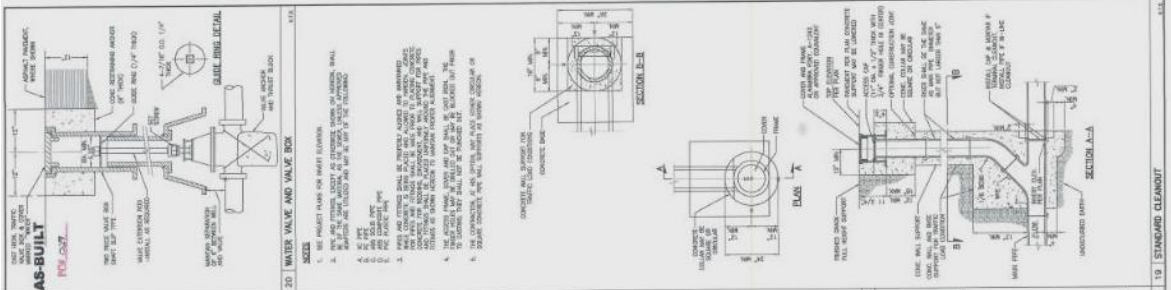
REGISTERED PROFESSIONAL ENGINEER
CIVIL
STATE OF CALIFORNIA
NO. 44521

COMPTON COMMUNITY COLLEGE DISTRICT
EL CAMINO COLLEGE
UTILITY INFRASTRUCTURE - PHASE 1
CONTRACT DOCUMENTS
1111 E. ARTISTA BLVD. - COMPTON, CA 90221

DATE: JANUARY 11, 2011
DRAWN BY: E.L.P.A.L. CHECKED BY: S.A.C.-C.
SCALE: AS SHOWN

REV.	DESCRIPTION	DATE	BY	CHKD.

EXAMINER NO. **C10.2**
SHEET NO. 13 OF 18



APPENDIX G

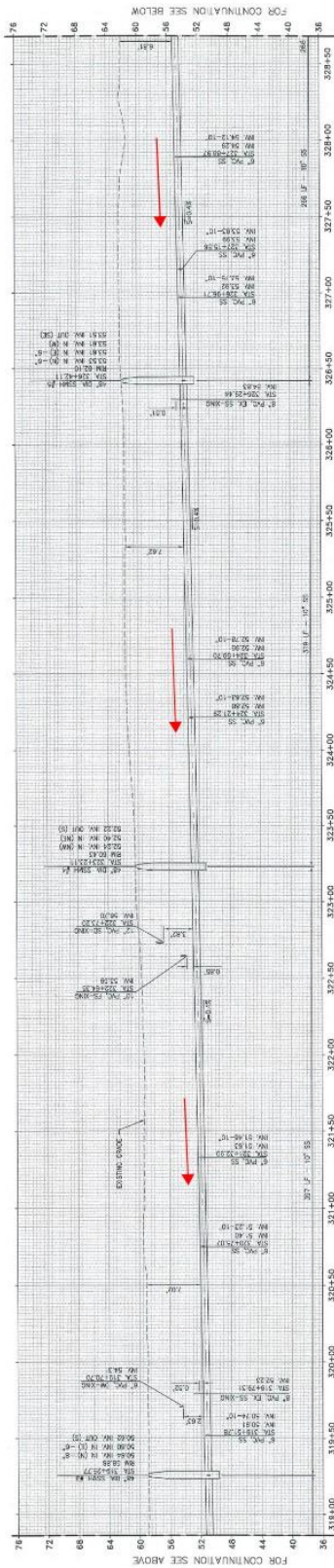
PROFILE OF LINE B

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e-mail: vca@vcaeng.com

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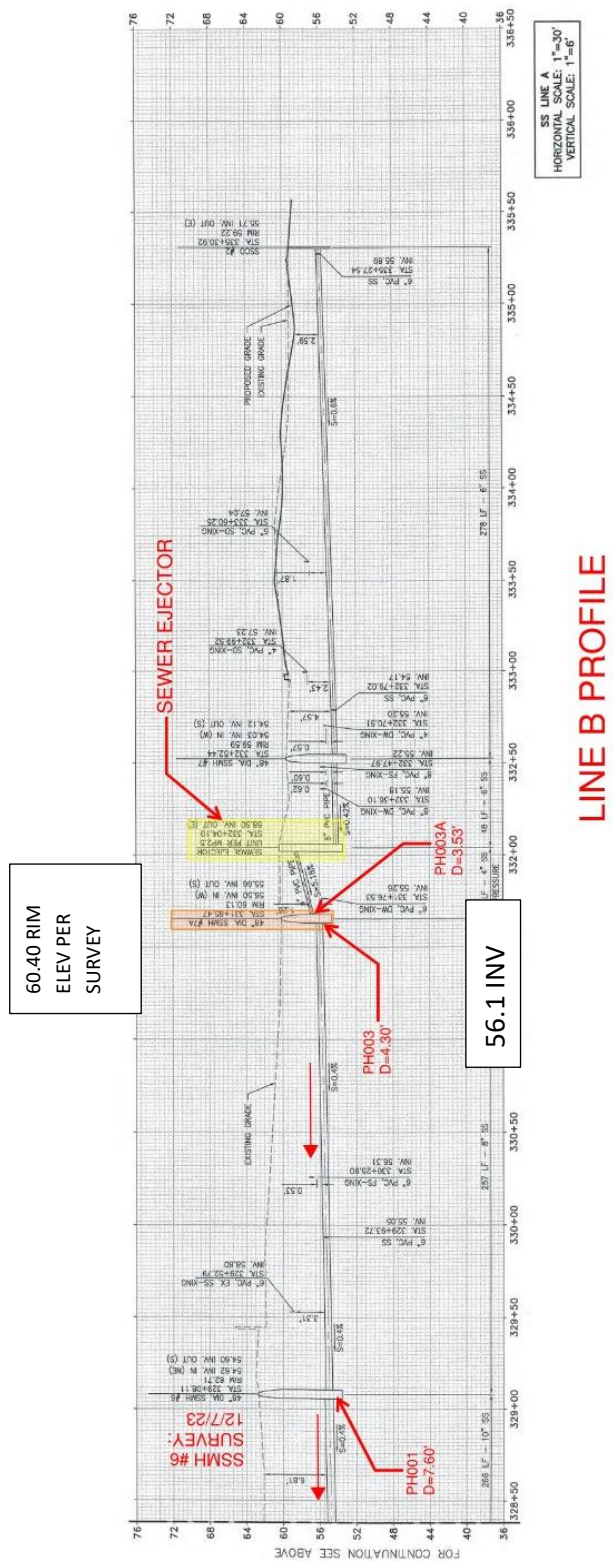
LINE B PROFILE

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APPENDIX H

7 DAYS MONITORING FLOW STUDY

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e-mail: vca@vcaeng.com

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CC01N

Site Commentary

SITE INFORMATION

Pipe	Round (8 in H)
Silt	0.00 (in)

OBSERVATIONS

5-minute flow depth, velocity, and quantity data observed during **Monday, 03 April 2023 to Monday, 10 April 2023**, along with observed minimum and maximum data, are provided in the following table.

The data for this site is of lower than typical accuracy due to the very low flows observed. This site often operated below detection limits for the flow monitor.

Observed Flow Conditions			
Item	DFINAL (in)	VFINAL (ft/s)	QFINAL (MGD - Total MG)
Average	0.12	0.00	0.000
Minimum	0.00	0.00	0.000
Maximum	0.95	0.00	0.000
Min Time	04/10/2023 9:00:00 AM	04/10/2023 11:45:00 PM	04/10/2023 11:45:00 PM
Max Time	04/10/2023 12:30:00 PM	04/03/2023 12:00:00 AM	04/03/2023 12:00:00 AM

Based upon the quality and consistency of the observed flow depth and velocity data, the Continuity equation was used to calculate flow rate and quantities during the monitoring period.

Values in the Observed Flow Conditions table are based on the five minutes average and data on the graphical reports are based on the fifteen minutes average.

DATA UPTIME

Data uptime observed during **Monday, 03 April 2023 to Monday, 10 April 2023** is provided in the following table:

Percent Uptime	
DFINAL (in)	100
VFINAL (ft/s)	100
QFINAL (MGD - Total MG)	100



Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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Project Name: ComptonCol.VCA.TFM.CA22		City: Compton		Agency: Compton		FM Initials: VM	
Site Name: CC01N		Install Date: 3/31/23		Monitor Type		Peak Doppler	
Address/Location: 1111 E Artesia Blvd, Compton, CA 90221				Monitor Model		Triton +	
				Data Acquisition		Manual/Wireless Collect	
				Manhole ID		Unknown	
Access: Drive		Type of System:		Sanitary <input checked="" type="checkbox"/>		Storm <input type="checkbox"/>	
				Combined <input type="checkbox"/>		Pipe Height: 8.00 "	
						Pipe Width: 8.00 "	



Investigation Information:				Manhole Information:			
Date/Time of Investigation:		03/27/23 @ 7:25 AM		Manhole Depth:		6'-2"	
Site Hydraulics:		Low/Dry straight flow		Manhole Material / Condition		Brick/Good	
Upstream Input: (L/S, P/S)		--		Pipe Material / Condition: VCP/Good			
Upstream Manhole:		Not Investigated		Land Use:			
				Residential <input type="checkbox"/>		Commercial <input type="checkbox"/>	
				Industrial <input type="checkbox"/>		Other <input checked="" type="checkbox"/>	
Downstream Manhole:		Not investigated		Oxygen: 20.9		H2S: 0	
				LEL: 0		CO: 0	
Depth of Flow:		0.00 " +/- 0.25"		Safety Notes: 2 man crew required and one blower is to be operated at all times.			
Range (Air DOF):		+/-					
Peak Velocity:		0.00 fps					
Silt:		0 Inches					

Other Information:

Cross Section		Plan	

Installation Information		Backup			Distance
Installation Type:	Standard	Yes	No	?	
Sensors Devices:	Ultrasonic/Velocity/Pressure	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Surcharge Height:	0	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Rain Gauge Zone:		<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	

Additional Site Information / Comments:

Standard Traffic Control with No Safety Concerns

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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

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2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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CC01W

Site Commentary

SITE INFORMATION

Pipe	Elliptical (5.88 in H x 6 in W)
Silt	0.00 (in)

OBSERVATIONS

5-minute flow depth, velocity, and quantity data observed during **Monday, 03 April 2023 to Monday, 10 April 2023**, along with observed minimum and maximum data, are provided in the following table.

The data for this site is of lower than typical accuracy due to the very low flows observed. This site often operated near lower detection limits for the flow monitor.

Observed Flow Conditions			
Item	DFINAL (in)	VFINAL (ft/s)	QFINAL (MGD - Total MG)
Average	0.27	0.23	0.001
Minimum	0.12	0.08	0.000
Maximum	1.00	1.00	0.011
Min Time	04/08/2023 2:00:00 PM	04/08/2023 2:00:00 PM	04/08/2023 2:00:00 PM
Max Time	04/10/2023 12:15:00 PM	04/07/2023 1:00:00 PM	04/10/2023 12:15:00 PM

Based upon the quality and consistency of the observed flow depth and velocity data, the Continuity equation was used to calculate flow rate and quantities during the monitoring period.

Values in the Observed Flow Conditions table are based on the five minutes average and data on the graphical reports are based on the fifteen minutes average.

DATA UPTIME

Data uptime observed during **Monday, 03 April 2023 to Monday, 10 April 2023** is provided in the following table:

Percent Uptime	
DFINAL (in)	100
VFINAL (ft/s)	100
QFINAL (MGD - Total MG)	100



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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

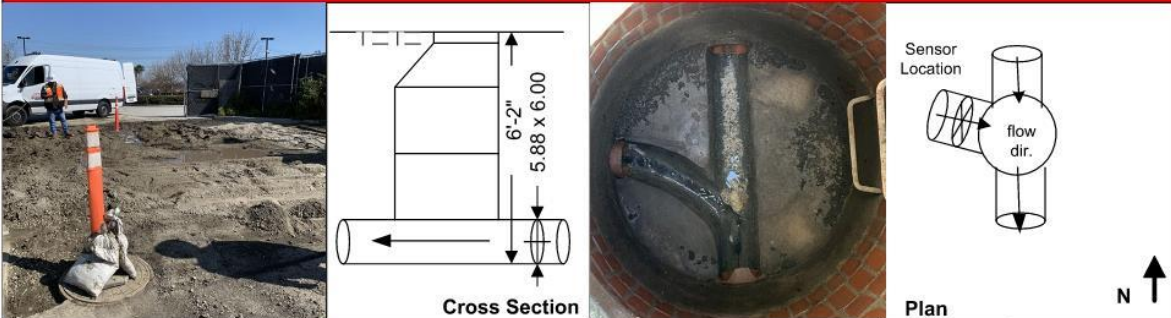
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 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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Project Name: ComptonCol.VCA.TFM.CA22		City: Compton	Agency: Compton	FM Initials: VM
Site Name: CC01W	Install Date: 3/31/23		Monitor Type	Peak Doppler
Address/Location: 1111 E Artesia Blvd, Compton, CA 90221			Monitor Model	Triton +
			Data Acquisition	Manual/Wireless Collect
			Manhole ID	Unknown
Access: Drive	Type of System:	Sanitary <input checked="" type="checkbox"/>	Storm <input type="checkbox"/>	Combined <input type="checkbox"/>
			Pipe Height:	5.88 "
			Pipe Width:	6.00 "



Investigation Information:		Manhole Information:			
Date/Time of Investigation:	03/27/23 @ 7:25 AM	Manhole Depth:	6'-2"		
Site Hydraulics:	Low/Dry curved flow	Manhole Material / Condition	Brick/Good		
Upstream Input: (L/S, P/S)	--	Pipe Material / Condition:	VCP/Good		
Upstream Manhole:	Not Investigated	Land Use:	Residential <input type="checkbox"/>	Commercial <input type="checkbox"/>	Industrial <input type="checkbox"/>
Downstream Manhole:	Not investigated		Other <input checked="" type="checkbox"/>		
Depth of Flow:	0.13 " +/- 0.25"	Oxygen:	20.9	H2S:	0
Range (Air DOF):	+/-	LEL:	0	CO:	0
Peak Velocity:	0.00 fps	Safety Notes:			
Silt:	0 Inches	2 man crew required and one blower is to be operated at all times.			

Other Information:



Installation Information		Backup			Distance
Installation Type:	Sensors Devices:	Yes	No	?	
Standard	Ultrasonic/Velocity/Pressure	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Surcharge Height: 0		<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Rain Gauge Zone:		<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	

Additional Site Information / Comments:

Standard Traffic Control with No Safety Concerns

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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CC02

Site Commentary

SITE INFORMATION

Pipe	Elliptical (11.88 in H x 11.5 in W)
Silt	0.00 (in)

OBSERVATIONS

5-minute flow depth, velocity, and quantity data observed during **Monday, 03 April 2023 to Monday, 10 April 2023**, along with observed minimum and maximum data, are provided in the following table.

The data for this site is of lower than typical accuracy due to the very low flows observed. This site often operated near lower detection limits for the flow monitor.

Observed Flow Conditions			
Item	DFINAL (in)	VFINAL (ft/s)	QFINAL (MGD - Total MG)
Average	0.53	0.43	0.004
Minimum	0.18	0.14	0.000
Maximum	1.36	1.23	0.023
Min Time	04/09/2023 5:30:00 AM	04/03/2023 4:15:00 AM	04/08/2023 2:15:00 AM
Max Time	04/07/2023 11:45:00 AM	04/08/2023 2:45:00 AM	04/08/2023 2:45:00 AM

Based upon the quality and consistency of the observed flow depth and velocity data, the Continuity equation was used to calculate flow rate and quantities during the monitoring period.

Values in the Observed Flow Conditions table are based on the five minutes average and data on the graphical reports are based on the fifteen minutes average.

DATA UPTIME

Data uptime observed during **Monday, 03 April 2023 to Monday, 10 April 2023** is provided in the following table:

Percent Uptime	
DFINAL (in)	100
VFINAL (ft/s)	100
QFINAL (MGD - Total MG)	100



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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

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2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

Project Name: ComptonCol.VCA.TFM.CA22		City: Compton	Agency: Compton	FM Initials: VM
Site Name: CC02	Install Date: 3/31/23		Monitor Type:	Peak Doppler
Address/Location: 1111 E Artesia Blvd, Compton, CA 90221			Monitor Model:	Triton +
			Data Acquisition:	Manual/Wireless Collect
			Manhole ID:	Unknown
Access:	Type of System:	Sanitary <input checked="" type="checkbox"/>	Storm <input type="checkbox"/>	Combined <input type="checkbox"/>
Drive				
			Pipe Height:	11.88 "
			Pipe Width:	11.50 "



Investigation Information:		Manhole Information:			
Date/Time of Investigation:	03/27/23 @ 7:25 AM	Manhole Depth:	11'-3"		
Site Hydraulics:	Low straight flow	Manhole Material / Condition:	Precast/Good		
Upstream Input: (L/S, P/S)	--	Pipe Material / Condition:	VCP/Good		
Upstream Manhole:	Not Investigated	Land Use:	Residential <input type="checkbox"/>	Commercial <input type="checkbox"/>	Industrial <input type="checkbox"/>
Downstream Manhole:	Not investigated		Other <input checked="" type="checkbox"/>		
Depth of Flow:	1.25 " +/- 0.25"	Oxygen:	20.9	H2S:	0
Range (Air DOF):	+/-	LEL:	0	CO:	0
Peak Velocity:	0.00 fps	Safety Notes: 2 man crew required and one blower is to be operated at all times.			
Silt:	0 Inches				

Other Information:

	 Cross Section		 Plan
--	--------------------------	--	-----------------

Installation Information		Backup				Distance
Installation Type:	Standard	Yes	No	?		
Sensors Devices:	Ultrasonic/Velocity/Pressure	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>		
Surcharge Height:	0	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>		
Rain Gauge Zone:		<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>		

Additional Site Information / Comments:

Standard Traffic Control with No Safety Concerns

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

APPENDIX I

14 DAYS MONITORING FLOW STUDY

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
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CC02

Site Commentary

SITE INFORMATION

Pipe	Elliptical (11.88 in H x 11.5 in W)
Silt	0.00 (in)

OBSERVATIONS

Average flow depth, velocity, and quantity data observed during **Thursday, 19 October 2023 to Wednesday, 01 November 2023**, along with observed minimum and maximum data, are provided in the following table.

Site operated at an average depth of 1.2 inches, however on 10/31/23 at 4pm for about an hour depth was within 1.5 inches of full pipe. This was most likely caused by debris settling in the line temporarily causing backwater conditions. Site resumed normal free flow conditions around 4:50pm. Average velocity at this location operates very close to the lower detection limit at 0.25 ft/s. Average flow is around 0.006 MGD and registering 0 or undetectable for much of the period. Data accuracy is lower than typical because of the low flow and slow conditions in these pipes.

Observed Flow Conditions			
Item	DFINAL (in)	VFINAL (ft/s)	QFINAL (MGD - Total MG)
Average	1.18	0.27	0.006
Minimum	0.39	0.00	0.000
Maximum	10.63	1.75	0.105
Min Time	10/21/2023 4:55:00 AM	11/01/2023 10:55:00 PM	11/01/2023 10:55:00 PM
Max Time	10/31/2023 4:50:00 PM	10/26/2023 1:20:00 PM	10/30/2023 9:15:00 PM

Based upon the quality and consistency of the observed flow depth and velocity data, the Continuity equation was used to calculate flow rate and quantities during the monitoring period.

Values in the Observed Flow Conditions table are based on the five minute average and data on the graphical reports are based on the fifteen minute average.

DATA UPTIME

Data uptime observed during **Thursday, 19 October 2023 to Wednesday, 01 November 2023** is provided in the following table:

Percent Uptime	
DFINAL (in)	100
VFINAL (ft/s)	100
QFINAL (MGD - Total MG)	100



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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

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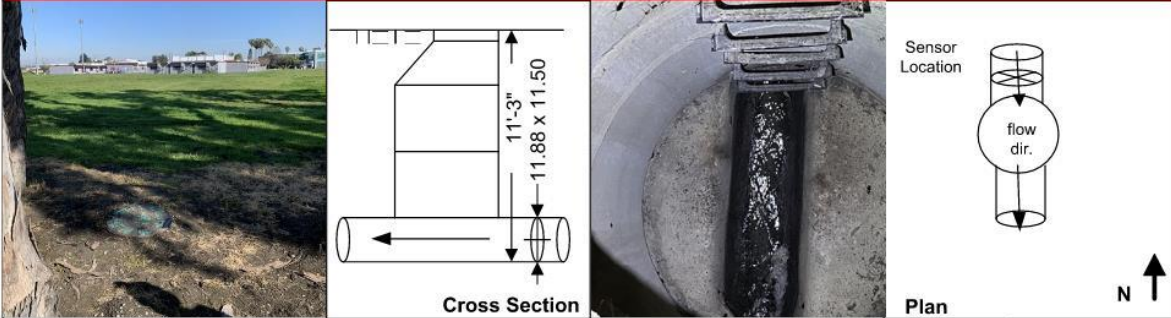
Project Name: ComptonCol.VCA.2TFM.CA22		City: Compton	Agency: Compton	FM Initials: VM
Site Name: CC02	Install Date: 10/18/2023		Monitor Type	Peak Doppler
Address/Location: 1111 E Artesia Blvd, Compton, CA 90221		Monitor Model		Triton +
		Data Acquisition		Manual/Wireless Collect
		Manhole ID		Unknown
Access: Drive	Type of System:	Sanitary <input checked="" type="checkbox"/>	Storm <input type="checkbox"/>	Combined <input type="checkbox"/>
		Pipe Height:		11.88 "
		Pipe Width:		11.50 "



Investigation Information: Manhole Information:

Date/Time of Investigation:	10/11/2023 @ 6:25 AM	Manhole Depth:	11'-3"
Site Hydraulics:	Low straight flow	Manhole Material / Condition:	Precast/Good
Upstream Input: (L/S, P/S)	---	Pipe Material / Condition:	VCP/Good
Upstream Manhole:	Not Investigated	Land Use:	Residential <input type="checkbox"/> Commercial <input type="checkbox"/> Industrial <input type="checkbox"/> Other <input checked="" type="checkbox"/>
Downstream Manhole:	Not investigated	Oxygen: 20.9	H2S: 0 LEL: 0 CO: 0
Depth of Flow:	0.88 " +/- 0.25"	Safety Notes: 2 man crew required and one blower is to be operated at all times.	
Range (Air DOF):	+/-		
Peak Velocity:	0.00 fps		
Silt:	0 Inches		

Other Information:



Installation Information		Backup	Yes	No	?	Distance
Installation Type:	Standard	Trunk	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Sensors Devices:	Ultrasonic/Velocity/Pressure	Lift / Pump Station	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Surcharge Height:	0	WWTP	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Rain Gauge Zone:		Other	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	

Additional Site Information / Comments:

Standard Traffic Control with No Safety Concerns

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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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CC03N

Site Commentary

SITE INFORMATION

Pipe	Round (10 in H)
Silt	0.00 (in)

OBSERVATIONS

Average flow depth, velocity, and quantity data observed during **Thursday, 19 October 2023 to Wednesday, 01 November 2023**, along with observed minimum and maximum data, are provided in the following table.

This site operates at mostly below 0.5 inches of water with a max 5 min. depth of 1.5 inches and a max hourly depth of 0.8 inches. Average velocity at this location is about 0.30 ft/s which is close to detection limits. Average flow is about 0.001 MGD and registering 0 or undetectable for much of the period. Data accuracy is lower than typical because of the low flow and slow conditions in these pipes.

Observed Flow Conditions			
Item	DFINAL (in)	VFINAL (ft/s)	QFINAL (MGD - Total MG)
Average	0.18	0.28	0.001
Minimum	0.00	0.00	0.000
Maximum	1.53	1.68	0.057
Min Time	11/01/2023 8:40:00 PM	11/01/2023 11:55:00 PM	11/01/2023 11:55:00 PM
Max Time	10/24/2023 2:40:00 PM	10/27/2023 8:25:00 AM	10/24/2023 2:40:00 PM

Based upon the quality and consistency of the observed flow depth and velocity data, the Continuity equation was used to calculate flow rate and quantities during the monitoring period.

Values in the Observed Flow Conditions table are based on the five minute average and data on the graphical reports are based on the fifteen minute average.

DATA UPTIME

Data uptime observed during **Thursday, 19 October 2023 to Wednesday, 01 November 2023** is provided in the following table:

Percent Uptime	
DFINAL (in)	100
VFINAL (ft/s)	100
QFINAL (MGD - Total MG)	100



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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
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Project Name: ComptonCol.VCA.2TFM.CA22		City: Compton	Agency: Compton	FM Initials: VM
Site Name: CC03N	Install Date: 10/18/2023		Monitor Type	Peak Doppler
Address/Location: 1111 E Artesia Blvd, Compton, CA 90221		Monitor Model		Triton +
		Data Acquisition		Manual/Wireless Collect
		Manhole ID		Unknown
Access: Drive	Type of System:	Sanitary <input checked="" type="checkbox"/>	Storm <input type="checkbox"/>	Combined <input type="checkbox"/>
		Pipe Height:		10.00 "
		Pipe Width:		10.00 "



Investigation Information:		Manhole Information:			
Date/Time of Investigation:	10/11/2023 @ 6:25 AM	Manhole Depth:	8'-4"		
Site Hydraulics:	Low straight flow	Manhole Material / Condition	Precast/Good		
Upstream Input: (L/S, P/S)	---	Pipe Material / Condition:	VCP/Good		
Upstream Manhole:	Not Investigated	Land Use:	Residential <input type="checkbox"/>	Commercial <input type="checkbox"/>	Industrial <input type="checkbox"/>
Downstream Manhole:	Not investigated		Other <input checked="" type="checkbox"/>		
Depth of Flow:	0.88 " +/- 0.25"	Oxygen: 20.9	H2S: 0	LEL: 0	CO: 0
Range (Air DOF):	+/-	Safety Notes: 2 man crew required and one blower is to be operated at all times.			
Peak Velocity:	1.10 fps				
Silt:	0 Inches				

Other Information:

--	--	--	--

Installation Information		Backup	Yes	No	?	Distance
Installation Type:	Standard	Trunk	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Sensors Devices:	Ultrasonic/Velocity/Pressure	Lift / Pump Station	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Surcharge Height:	0	WWTP	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
Rain Gauge Zone:		Other	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	

Additional Site Information / Comments:

Standard Traffic Control with No Safety Concerns

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1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

APPENDIX J

EXISTING SEWER PIPE CALCULATIONS

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
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Existing Pipe Capacity at Monitored Manhole			LINE A		LINE B		
Existing Sewer Pipe Capacity at d/D=0.50	Factors	Units	Manhole 1		Manhole 2		Manhole 3
			CC01N	CC01W	CC02 OLD	CC02 NEW	CC03N
Monitored Peak Flow	Q _P	cfs	0.00	0.02	0.04	0.16	0.09
Factored Peak Flow (Monitored Peak Flow*2.5)	Q_M	cfs	0.00	0.04	0.09	0.41	0.22
Diameter of existing pipe	D	inch	8.00	6.00	12.00	12.00	10.00
		ft	0.67	0.50	1.00	1.00	0.83
Manning's Roughness Coefficient	n	-	0.013	0.013	0.013	0.013	0.013
Slope of SS Pipe	S	-	0.0054	0.0050	0.0040	0.0040	0.0040
Flow Depth	d	ft	4.00	3.00	6.00	6.00	5.00
Proportional Depth of Flow	d/D	-	0.50	0.50	0.50	0.50	0.50
Angle of flow	Θ	radians	3.14	3.14	3.14	3.14	3.14
Area of flow	A	sq. ft.	0.17	0.10	0.39	0.39	0.27
Wetted Perimeter	W _P	ft	1.05	0.79	1.57	1.57	1.31
Hydraulic radius (A/W _P)	R	ft	0.17	0.13	0.25	0.25	0.21
Flow velocity	v	fps	2.54	2.02	2.87	2.87	2.54
Flow Rate of Existing Pipe at d/D=0.50	Q_C	cfs	0.44	0.20	1.13	1.13	0.69
Q_M < Q_C : OK	-	-	OK	OK	OK	OK	OK

Existing Sewer Pipe Capacity at d/D=0.50	Factors	Units	LINE A	LINE B	
			6" Northerly	6" Upstream Sewer Ejector	8" Downstream SSMH 7A
Diameter of existing pipe	D	inch	6.00	6.00	8.00
		ft	0.50	0.50	0.67
Manning's Roughness Coefficient	n	-	0.013	0.013	0.013
Slope of SS Pipe	S	-	0.0064	0.0058	0.0058
Flow Depth	d	ft	3.00	3.00	4.00
Proportional Depth of Flow	d/D	-	0.50	0.50	0.50
Angle of flow	Θ	radians	3.14	3.14	3.14
Area of flow	A	sq. ft.	0.10	0.10	0.17
Wetted Perimeter	W _P	ft	0.79	0.79	1.05
Hydraulic radius (A/W _P)	R	ft	0.13	0.13	0.17
Flow velocity	v	fps	2.29	2.18	2.64
Flow Rate of Existing Pipe at d/D=0.50	Q_C	cfs	0.22	0.21	0.46

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

APPENDIX K

TOTAL SEWER DEMAND

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
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New Demand Flow Rate		
POC	Q	
	GPM	cfs
A	69	0.154
B	70	0.156
C	1	0.002
D	74	0.165
E	108	0.241

Total Sewer Demand (QT) : SCENARIO ANALYSIS 1	Factors	Units	LINE A
Factored Peak Flow (Monitored Peak Flow*2.5) CC01N	Q_M	cfs	0.00
Factored Peak Flow (Monitored Peak Flow*2.5) CC01W	Q_M	cfs	0.043
Future Demand Wing A	Q_N	cfs	0.477
Future Demand Wing B	Q_N	cfs	0.241
Total Sewer Demand	Q_T	cfs	0.761

Total Sewer Demand (QT) : SCENARIO ANALYSIS 2	Factors	Units	LINE A	LINE B @ (E) SSMH 7A	LINE B @ (E) 12" PIPE
Factored Peak Flow (Monitored Peak Flow*2.5) CC01N	Q_M	cfs	0.00	-	-
Factored Peak Flow (Monitored Peak Flow*2.5) CC01W	Q_M	cfs	0.043	-	-
Factored Peak Flow (Monitored Peak Flow*2.5) CC02					0.41
Existing 6" pipe (Sewer Ejector)	Q	cfs	-	0.210	0.21
Future Demand Wing A	Q_N	cfs	0.477	-	-
Future Demand Wing B	Q_N	cfs	-	0.241	0.241
Total Sewer Demand	Q_T	cfs	0.520	0.451	0.861

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 • Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 • Fax: 949-679-9370
 www.vcaeng.com

Total Sewer Demand (QT) : SCENARIO ANALYSIS 3	Factors	Units	LINE B	LINE B @ (E) 12" PIPE
Factored Peak Flow (Monitored Peak Flow*2.5) CC02			-	0.41
Existing 6" pipe (Sewer Ejector)	Q	cfs	0.210	0.21
Future Demand Wing A	Q _N	cfs	0.477	0.477
Future Demand Wing B	Q _N	cfs	0.241	0.241
Total Sewer Demand	Q _T	cfs	0.928	1.338

Total Sewer Demand (QT) : SCENARIO ANALYSIS 4	Factors	Units	LINE B	LINE B @ (E) 12" PIPE
Factored Peak Flow (Monitored Peak Flow*2.5) CC02			-	0.41
Existing 6" pipe (Sewer Ejector)	Q	cfs	0.210	0.21
Future Demand Wing A	Q _N	cfs	0.477	0.477
Future Demand Wing B	Q _N	cfs	0.241	0.241
Total Sewer Demand	Q _T	cfs	0.928	1.338

Los Angeles

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 e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 ▪ Fax: 949-679-9370
 www.vcaeng.com

APPENDIX L

EXISTING PIPE CAPACITY (Q_C) vs. TOTAL SEWER DEMAND (Q_T)

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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

Irvine

2151 Michelson Dr. # 242, Irvine, CA 92612
Tel: 949-679-0870 ▪ Fax: 949-679-9370
www.vcaeng.com

A. SCENARIO ANALYSIS 1

SCENARIO ANALYSIS 1			WING B		WING A		TOTAL DEMAND	
Total Sewer Demand (Q_T)			0.241	0.241	0.477	0.477	0.718	0.761
Calculations for Velocity and Discharge								
Diameter of Pipe	D	inches	6	6	8	8	8	8
Manning's Roughness Coefficient	n		0.013	0.013	0.013	0.013	0.013	0.013
Slope of SD Pipe	S	ft/ft	0.0064	0.0064	0.0054	0.0054	0.0054	0.0054
Proportional Depth of Flow	d/D		0.5	0.6	0.5	0.6	0.75	0.75
Flow Depth	d	inches	3	3.6	4	4.8	6	6
Angle of Flow	Θ	radians	3.1416	3.5443	3.1416	3.5443	4.1888	4.1888
Area of Flow	a	sq.ft	0.10	0.12	0.17	0.22	0.28	0.28
Wetted Perimeter	p	ft	0.79	0.89	1.05	1.18	1.40	1.40
Hydraulic Radius	r	ft	0.13	0.14	0.17	0.19	0.20	0.20
Using Manning's Equation, for pipe at flow depth 'd'								
Flow Velocity	v	fps	2.29	2.46	2.55	2.73	2.89	2.89
Pipe Capacity Flow Rate	Q_C	cfs	0.22	0.30	0.44	0.60	0.81	0.81
Is calculated Velocity greater than 2 fps?			YES	YES	YES	YES	YES	YES
Is the pipe capacity > hydrology accumulated flow rate?			NO	YES	NO	YES	YES	YES
Try Again			NG	OK	NG	OK	OK	OK

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Irvine

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 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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B. SCENARIO ANALYSIS 2

SCENARIO ANALYSIS 2			WING A TO LINE A		TOTAL DEMAND	WING B	TOTAL DEMAND	
							SSMH 7A	12" PIPE
Total Sewer Demand (Q_T)			0.477	0.477	0.52	0.241	0.451	0.861
Calculations for Velocity and Discharge								
Diameter of Pipe	D	inches	8	8	8	8	8	12
Manning's Roughness Coefficient	n		0.013	0.013	0.013	0.011	0.013	0.013
Slope of SD Pipe	S	ft/ft	0.0054	0.0054	0.0054	0.004	0.0058	0.004
Proportional Depth of Flow	d/D		0.5	0.6	0.6	0.5	0.5	0.5
Flow Depth	d	inches	4	4.8	4.8	4	4	6
Angle of Flow	Θ	radians	3.1416	3.5443	3.5443	3.1416	3.1416	3.1416
Area of Flow	a	sq.ft	0.17	0.22	0.22	0.17	0.17	0.39
Wetted Perimeter	p	ft	1.05	1.18	1.18	1.05	1.05	1.57
Hydraulic Radius	r	ft	0.17	0.19	0.19	0.17	0.17	0.25
Using Manning's Equation, for pipe at flow depth 'd'								
Flow Velocity	v	fps	2.55	2.73	2.73	2.59	2.64	2.87
Pipe Capacity Flow Rate	Q_C	cfs	0.44	0.60	0.60	0.45	0.46	1.13
Is calculated Velocity greater than 2 fps?			YES	YES	YES	YES	YES	YES
Is the pipe capacity > hydrology accumulated flow rate?			NO	YES	YES	YES	YES	YES
Try Again			NG	OK	OK	OK	OK	OK

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C. SCENARIO ANALYSIS 3

SCENARIO ANALYSIS 3			WING A + WING B		TOTAL DEMAND			
					SSMH 7A		12" PIPE	
Total Sewer Demand (Q_T)			0.718	0.718	0.928	0.928	1.338	1.338
Calculations for Velocity and Discharge								
Diameter of Pipe	D	inches	8	10	8	10	12	12
Manning's Roughness Coefficient	n		0.011	0.011	0.013	0.011	0.013	0.013
Slope of SD Pipe	S	ft/ft	0.005	0.005	0.0058	0.0058	0.004	0.004
Proportional Depth of Flow	d/D		0.5	0.5	0.5	0.5	0.5	0.6
Flow Depth	d	inches	4	5	4	5	6	7.2
Angle of Flow	Θ	radians	3.1416	3.1416	3.1416	3.1416	3.1416	3.5443
Area of Flow	a	sq.ft	0.17	0.27	0.17	0.27	0.39	0.49
Wetted Perimeter	p	ft	1.05	1.31	1.05	1.31	1.57	1.77
Hydraulic Radius	r	ft	0.17	0.21	0.17	0.21	0.25	0.28

Using Manning's Equation, for pipe at flow depth 'd'

Flow Velocity	v	fps	2.90	3.36	2.64	3.62	2.87	3.08
Pipe Capacity Flow Rate	Q_C	cfs	0.51	0.92	0.46	0.99	1.13	1.52

Is calculated Velocity greater than 2 fps?	YES	YES	YES	YES	YES	YES	YES
Is the pipe capacity > hydrology accumulated flow rate?	NO	YES	NO	YES	NO	YES	YES
Try Again	NG	OK	NG	OK	NG	OK	OK

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Irvine

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 Tel: 949-679-0870 ▪ Fax: 949-679-9370
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D. SCENARIO ANALYSIS 4

SCENARIO ANALYSIS 4			WING A + WING B				SE OUT		TOTAL DEMAND			
									SSMH 7A		12" PIPE	
Total Sewer Demand (Q _T)			0.718	0.718	0.928	0.928	0.928	0.928	0.928	1.338	1.338	
Calculations for Velocity and Discharge												
Diameter of Pipe	D	inches	8	10	10	10	6	6	8	10	12	12
Manning's Roughness Coefficient	n		0.011	0.011	0.011	0.011	0.011	0.011	0.013	0.011	0.013	0.013
Slope of SD Pipe	S	ft/ft	0.005	0.005	0.005	0.005	0.0523	0.0523	0.0058	0.0058	0.004	0.004
Proportional Depth of Flow	d/D		0.5	0.5	0.5	0.6	0.5	0.6	0.5	0.5	0.5	0.6
Flow Depth	d	inches	4	5	5	6	3	3.6	4	5	6	7.2
Angle of Flow	Θ	radians	3.1416	3.1416	3.1416	3.5443	3.1416	3.5443	3.1416	3.1416	3.1416	3.5443
Area of Flow	a	sq.ft	0.17	0.27	0.27	0.34	0.10	0.12	0.17	0.27	0.39	0.49
Wetted Perimeter	p	ft	1.05	1.31	1.31	1.48	0.79	0.89	1.05	1.31	1.57	1.77
Hydraulic Radius	r	ft	0.17	0.21	0.21	0.23	0.13	0.14	0.17	0.21	0.25	0.28
Using Manning's Equation, for pipe at flow depth 'd'												
Flow Velocity	v	fps	2.90	3.36	3.36	3.61	7.74	8.30	2.64	3.62	2.87	3.08
Pipe Capacity Flow Rate	Q _C	cfs	0.51	0.92	0.92	1.23	0.76	1.02	0.46	0.99	1.13	1.52
Is calculated Velocity greater than 2 fps?			YES	YES	YES	YES	YES	YES	YES	YES	YES	YES
Is the pipe capacity > hydrology accumulated flow rate?			NO	YES	NO	YES	NO	YES	NO	YES	NO	YES
Try Again			NG	OK	NG	OK	NG	OK	NG	OK	NG	OK

Los Angeles

1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 ▪ Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine

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APPENDIX M

Excerpts from LA County DPW Sanitary Sewer Procedural Manual

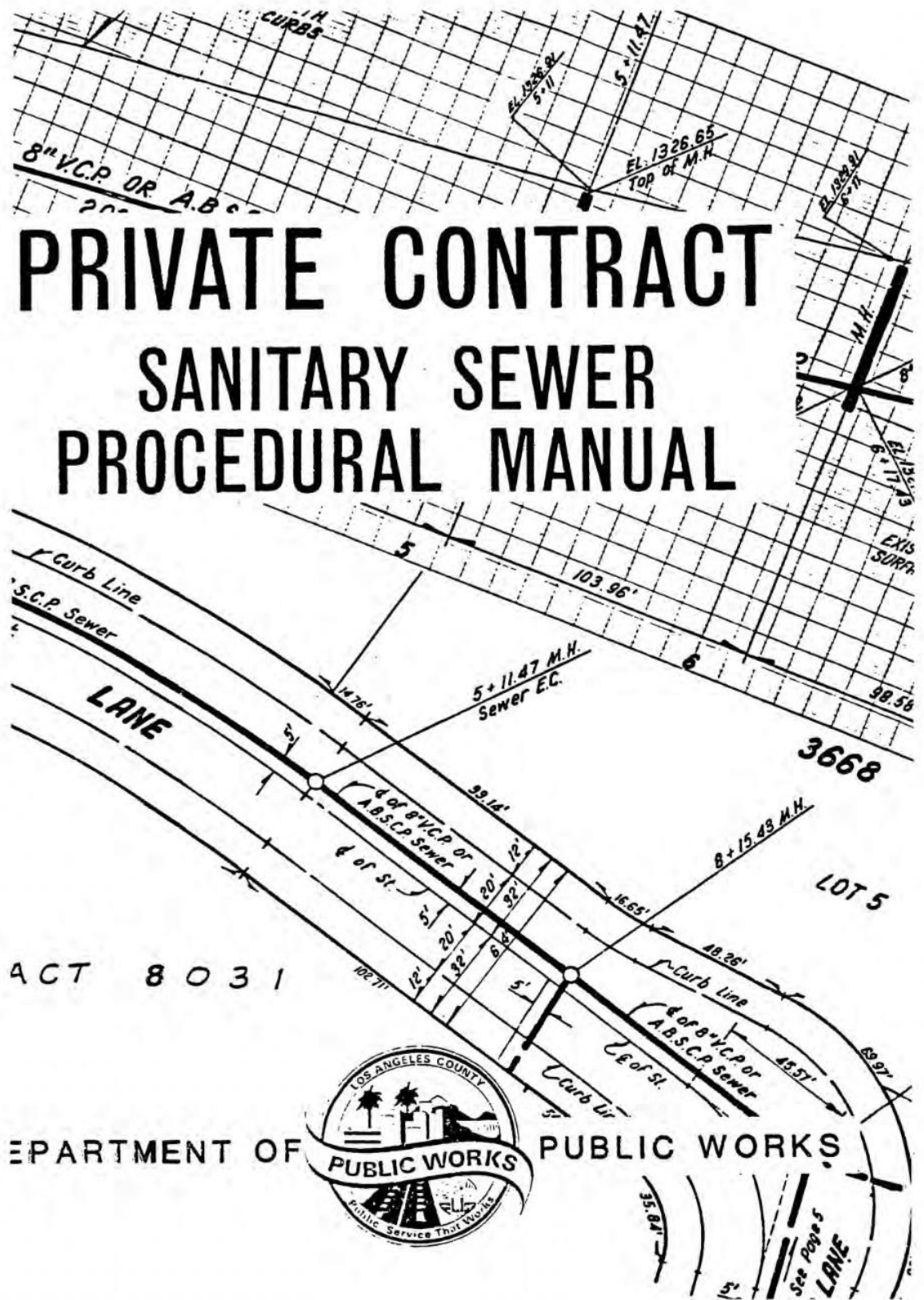
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1041 S Garfield Ave #210, Alhambra CA 91801
Tel: 323-729-6098 ▪ Fax: 323-729-6043
e-mail: vca@vcaeng.com

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www.vcaeng.com

PRIVATE CONTRACT SANITARY SEWER PROCEDURAL MANUAL



DEPARTMENT OF PUBLIC WORKS



Los Angeles
 1041 S Garfield Ave #210, Alhambra CA 91801
 Tel: 323-729-6098 • Fax: 323-729-6043
 e-mail: vca@vcaeng.com

Irvine
 2151 Michelson Dr. # 242, Irvine, CA 92612
 Tel: 949-679-0870 • Fax: 949-679-9370
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