



Geotechnical Engineering Report

**Proposed Student Housing
1111 E Artesia Blvd,
Compton, California 90221**

**Prepared for:
Compton Community College District
1111 E Artesia Blvd
Compton, CA 90221**

**April 14, 2023
Project No.: 4230.2200060.0000**



Materials Testing
Geotechnical Engineering
Environmental
Building Sciences & Safety
Inspections & Code Compliance
Virtual Design Consulting

April 14, 2023
Project No. 4230.2200060.0000

Compton Community College District
1111 East Artesia Boulevard
Compton, CA 90221
Attention: Ms. Linda Owens

**Subject: Geotechnical Engineering Report
Proposed Student Housing
1111 E Artesia Blvd,
Compton, California 90221**

Dear Ms. Owens,

In accordance with your request and authorization, we are presenting the results of our geotechnical engineering exploration for the proposed project located at 1111 E Artesia Blvd in Compton, California 90221. The purpose of this investigation has been to evaluate the subsurface conditions at the site and to provide geotechnical engineering recommendations for the proposed construction.

Based on our findings, the proposed project is geotechnically and geologically feasible, provided that the recommendations in this report are incorporated into the design and are implemented during construction of the project.

We appreciate the opportunity to be of service on this project. Should you have any questions regarding this report or if we can be of further service, please do not hesitate to contact the undersigned.

Respectfully submitted,
Universal Engineering Sciences

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1. INTRODUCTION

This report presents the results of our geotechnical engineering exploration performed for the proposed student housing buildings to be located at 1111 E Artesia Blvd, Compton, California (Figure 1 – Site Vicinity Location Map). The purpose of this study has been to evaluate the subsurface conditions at the site and to provide geotechnical recommendations related to the design and construction of the proposed structure. This report was prepared in accordance with the requirements of ASCE 7-16 and the 2022 California Building Code (CBC). This report will also be subject to review under California Code of Regulations (CCR), Title 24, California Building Code (2022 CBC). Our exploration generally followed the guidelines presented in California Geological Survey (CGS) Note 48: Checklist for the Review of Engineering Geology and Seismology Reports for California Public Schools, Hospitals, and Essential Services Buildings (November 2022). The review of our report will fall under the jurisdiction of the Division of State Architect (DSA) and will be performed by CGS.

2. SITE DESCRIPTION AND PROPOSED DEVELOPMENT

The approximate site coordinates are latitude 33.87972°N and longitude 118.20972°W and is located at approximately 63 feet above Mean Sea Level (MSL). Based on our aerial photographic survey, the campus was constructed just before 1952. Prior to that, the area was used for agricultural purposes. The project site is an open space area situated between classroom Buildings E and F, and the main northern parking lot. It is our understanding that the two existing classroom buildings will be demolished prior to the new construction.

The proposed construction will consist of a new 3-story building with roof top patio 250-bed low-income student housing facility on the campus. The proposed structures will consist of modular unit construction. It is anticipated that the structure will be constructed near the existing street grade and will have relatively light loads.

3. SCOPE OF WORK

To prepare this report, we have performed the following tasks:

3.1. Literature Review

We reviewed readily available background data including in-house geophysical data, geologic maps, topographic maps, and aerial photographs relevant to the subject site in preparation of this report. The list of documents reviewed is presented in the “References” section of this report. List of reviewed aerial photographs are presented in Table 1 below.

Table 1
List of Aerial Photographs Reviewed

Source	Flight	Frames	Date	Scale
Fairchild Aerial Surveys	C-300	M-137 – M-139	1/1/1928	1” = 1,500’
Fairchild Aerial Surveys	C-5526	11	12/6/1938	1” = 1,667’
Fairchild Aerial Surveys	C-11351	8-18	6/18/1947	1” = 1,667’
USDA	AXJ-1952	13K-219 & 220	10/19/1953	1” = 3,000’
Fairchild Aerial Surveys	C-22555	23-30, 31 & 32	7/15/1956	1” = 1,000’
PAI	96V	V-18	4/23/1958	1” = 400’
Fairchild Aerial Surveys	C-23870	633, 2204 & 2205	5/8/1960	1” = 1,200’
Fairchild Aerial Surveys	C-24400	5-301	10/1/1962	1” = 1,200’
TG	7600	5-15	3/22/1976	1” = 1,667’
EROS Data Center	NAPP-2C	6858-70	5/31/1994	1” = 3,333’

3.2. Field Exploration

The field exploration, consisting of eight exploratory 8-inch-diameter hollow-stemmed auger borings and six cone penetrometer soundings was conducted at the site between December 22, 2022, and January 17, 2023. Exploration depths varied between 10.0’ and 76.5’ below the existing grades. The approximate locations of the excavations are shown on Figure 2 – Geologic Site Plan and Boring Location Map. Detailed exploration information of soil excavations is presented in Appendix A. UES additionally conducted a ReMi Shear-Wave test. Results can be found in Appendix G.

3.3. Infiltration Testing

Four preliminary percolation tests were performed on January 4, 2023 to evaluate the potential of infiltrating stormwater into the site soils and determine a preliminary design infiltration rate for initial design of the planned BMPs. The borings are shown on the attached Figure 2 – Geologic Site Plan and Boring Location Map and were excavated to depth of 10 feet below the existing grade. The raw infiltration test data are provided in Table 2 below.

Table 2
Preliminary Design Infiltration Rates Summary

Boring No.	Depth Below Existing Grade (feet)	Observed Infiltration Rates (inches/hour)
P-2	10	3.37
P-3	10	2.25
P-4	10	2.25

The percolation rates observed in the field were 3.37 and 2.25 inches per hour. Final infiltration rate should be confirmed once the planned percolation basin design and location is established. Additionally, infiltration system should not be placed less than 10 feet away from any foundations and retaining structures. The details of our percolation testing procedures, results, and calculations are presented in Appendix D, Infiltration Test Result.

3.4. Geotechnical Laboratory Testing

Laboratory tests were performed on selected samples obtained from the borings in order to aid in the soil classification and to evaluate the engineering properties of the foundation soils. Laboratory tests included in-situ moisture and density, sieve analysis, #200 sieve wash, maximum density and optimum moisture content, Atterberg limits, expansion index testing, direct shear tests, consolidations, sand equivalence, corrosion testing, and R values. The detailed laboratory test results are presented in Appendix B.

3.5. Engineering Analyses and Report Preparation

We compiled and analyzed the data collected from our site reconnaissance, subsurface evaluation, and laboratory testing, and prepared this report to present our conclusions and recommendations, including:

- Evaluation of general subsurface conditions and description of types, distribution, and engineering characteristics of subsurface materials.
- Evaluation of site-specific seismic design parameters in accordance with 2022 California Building Code.

- Evaluation of current and historic high groundwater conditions at the site and potential impact on the existing structures and site development.
- Evaluation of project feasibility and suitability of on-site soils for foundation support.
- Evaluation of foundation design parameters including soil bearing capacity, lateral resistance, friction coefficient, and seismic considerations.

4. SITE GEOLOGY AND SUBSURFACE CONDITIONS

4.1. Regional Geologic Setting

The site is generally located in the north central portion of the Peninsular Ranges Geomorphic province, within the Los Angeles Basin (see Figure 4 – Regional Geologic Map). The Peninsular Ranges province extends southeastward from the Santa Monica and San Gabriel mountains to beyond the Mexican border and is subdivided into several structural units, such as the Los Angeles Basin, the Santa Ana Mountains, the Orange County plain, and the California Continental Borderland blocks. The Peninsular Ranges province is generally characterized by northwest oriented valleys and mountain ranges bounded by major right lateral strike-slip fault zones. The San Andreas Fault zone constitutes the eastern provincial boundary, the Patton-Coronado Escarpment constitutes the western provincial boundary, while the San Jacinto, the Elsinore, and the Newport-Inglewood-Rose Canyon Fault zones are located within the center of the province. Rocks of the Peninsular Ranges are typically Cretaceous igneous and marine sedimentary and Paleozoic to Mesozoic metasedimentary rocks. Tertiary marine and non-marine sedimentary and volcanic rock along with shallow to deep Quaternary sediment lies unconformably on either the Cretaceous sedimentary or the older basement rock.

Locally, the site is situated in the central Los Angeles Basin. The Los Angeles Basin consists of a structural low situated between the Whittier and Newport-Inglewood faults northwest of the Santa Mountains and contains up to 30,000 feet of accumulated sediment (Yerkes, et.al, 1965; Ingersol et.al., 1999).

4.2. Site-Specific Geologic and Soil Conditions

Reference to available preliminary geologic maps of the general site area indicate that the site is underlain by Holocene Alluvium (Map Symbol: Qya2) and artificial fill associate with the campus construction. The alluvium material was encountered at all exploratory excavation locations to the maximum depth of exploration (approximately 76.5 feet bgs). Detailed descriptions and information concerning the geologic units encountered are provided in the following paragraphs and on the exploration logs in Appendix A. The subsurface geologic conditions are presented on the attached Geologic Site Map (Figure 2) and Geologic Cross-sections A-A' and B-B' (Figures 3A and 3B respectively).

4.2.1. Undocumented Fill (Afu)

Undocumented utility backfill was encountered just west of Boring P-1 and CPT-6. No documentation for the utility backfill was presented for our review.

4.2.2. Quaternary-age Young Alluvial Deposits (Qya2)

The alluvium encountered consisted of interbedded silty sand, sandy silt, and silty clay to the maximum depth explored (approximately 76.5 feet bgs). In general, the near surface sandy layers are loose to medium dense, becoming dense at depth. The near surface fine grained layers are soft to stiff, becoming very stiff to hard or dense at depth.

4.3. Groundwater Conditions

Groundwater was encountered within the deepest exploratory boring at a depth of approximately 52.8 and 54.2 feet below the existing grade. According to the Seismic Hazard Zone Report for the South Gate 7.5-Minute Quadrangle (1998), the historic high groundwater is approximately 8 feet bgs. Groundwater conditions may vary across the site due to stratigraphic and hydrologic conditions and may change over time as a consequence of seasonal and meteorological fluctuations, or of activities by humans at this and nearby sites. Based on our findings, groundwater is not expected to impact the proposed development.

4.4. Geologic Hazards

4.4.1. Surface Fault Rupture

The subject site is not located within a State of California Alquist-Priolo Earthquake Fault Zone (formerly known as a Special Studies Zone). It is our opinion that the likelihood of fault rupture occurring at the site during the design life of the proposed improvements is low. The closest fault to the site as designated by the California Geological Survey and United States Geological Survey is the Newport-Inglewood fault, located approximately 3.4 kilometers (2.1 miles) to the west.

4.4.2. Local and Regional Faulting

The United States Geological Survey (USGS), with support of State Geological Surveys, and reviewed published work by various researchers, have developed a Quaternary Fault and Fold Database of faults and associated folds that are believed to be sources of earthquakes with magnitudes greater than 6.0 that have occurred during the Quaternary (the past 1.6 million years). The Southern California Earthquake Center (SCEC) has released the SCEC Community Fault Model (Version 5.3, 2022), which is an object-oriented three-dimensional representation of 440 active fault surfaces in southern California and adjacent offshore basins.

Based on our review, the nearest mapped faults to the site are the Newport-Inglewood fault, located approximately 3.4 kilometers (2.1 miles) to the west, and the Compton-Los Alamitos Thrust fault, which underlies the site at an approximate depth of 2.6 kilometers (1.6 miles) beneath the surface (SCEC, 2022). The attached Figures 5 and 6 show regional faults and seismicity with respect to the subject site location.

4.5. Liquefaction Potential

Liquefaction occurs when the pore pressures generated within a soil mass approach the effective overburden pressure. Liquefaction of soils may be caused by cyclic loading such as that imposed by ground shaking during earthquakes. The increase in pore pressure results in a loss of strength, and the soil then can undergo both horizontal and vertical movements, depending on the site conditions. Other phenomena associated with soil liquefaction include sand boils, ground oscillation, and loss of foundation bearing capacity. Liquefaction is generally known to occur in loose, saturated, relatively clean, fine-grained cohesionless soils at depths shallower than approximately 50 feet. Factors to consider in the evaluation of soil liquefaction potential include

groundwater conditions, soil type, grain size distribution, relative density, degree of saturation, and both the intensity and duration of ground motion.

The current standard of practice, as outlined in the “Recommended Procedures for Implementation of DMG Special Publication 117, Guidelines for Analyzing and Mitigating Liquefaction in California” and “Special Publication 117A, Guidelines for Evaluating and Mitigating Seismic Hazards in California” requires liquefaction analysis to a depth of 50 feet below the lowest portion of the proposed structure. Liquefaction typically occurs in areas where the soils below the water table are composed of poorly consolidated, fine to medium-grained, primarily sandy soil. In addition to the requisite soil conditions, the ground acceleration and duration of the earthquake must also be of a sufficient level to induce liquefaction.

A review of the Seismic Hazard Zone Report for the South Gate 7.5-Minute Quadrangle (1998), the Earthquake Zones of Required Investigation South Gate Quadrangle (2006), the City of Compton General Plan (2014) and the County of Los Angeles General Plan (2022) indicate the site is located within an area identified as having a potential for liquefaction. Due to the nature of the alluvial soil encountered in our borings, the groundwater encountered during our investigation at approximately 52 to 54 feet below ground surface (bgs), and historic high groundwater is indicated as high as 8 feet bgs, we have performed an assessment for the potential for seismically induced liquefaction at the site. We anticipate up to approximately 6 inches of liquefaction induced settlement. The full results of our liquefaction analysis can be found in Appendix C.

We have reviewed key historic references that identify ground surface liquefaction manifestations from the 1933 Long Beach earthquake (CDMG, 1998; Barrows, 1974; Hillis, 1933; Wood, 1933). The results of our review indicate that two cracks attributed to liquefaction were reported near the Compton College campus. One of these cracks is illustrated in a photograph from Wood (1933, Plate 5a). These cracks occurred where water, sand, and mud were ejected that formed liquefaction surface features and were reportedly located (CGS, 1998) approximately 0.9 kilometers (0.5 miles) east of the proposed campus construction. These cracks are interpreted to have formed as the result of liquefaction during earthquake ground shaking from the 1933 Long Beach earthquake. Water-soaked ground was also reported in the vicinity of City of Compton during the time of the 1933 earthquake. In the general City of Compton area, reportedly the most severe damage associated with liquefaction failure occurred on “ground formerly marshy in part, along Compton Creek and the former courses of the Los Angeles River, with deep deposits of loose, wet alluvium beneath” (Wood (1933, p. 52). The area of the Compton College campus apparently experienced much less severe ground failure due to liquefaction, because it was outside of the formerly marshy areas along the former courses of the Los Angeles River mentioned above.

4.6. Landslides

Based on our review of the referenced geologic maps, literature, topographic maps, aerial photographs, and our subsurface evaluation, no landslides or related features underlie or are adjacent to the subject site. Due to the relatively level and limited gradient changes of the site and surrounding areas, the potential for landslides at the project site is considered negligible.

4.7. Flooding

The Federal Emergency Management Agency (FEMA) has prepared flood insurance rate maps (FIRMs) for use in administering the National Flood Insurance Program. Based on our review of the FEMA (2021) flood map, the site is outside the 0.2% annual chance (500-year) floodplain (see Figure 7 – FEMA Flood Hazard Map).

4.8. Dam Inundation

Dam Inundation occurs when structural damage to a dam results in a flood. Structural damage to a dam can occur due to earthquakes, liquefaction, landslides, lateral spreading, water overflow and erosion, and design failure. A dam inundation map shows areas that would be susceptible to flooding in the event of dam failure. In 2017, the California Legislature passed a law requiring all state jurisdictional dams, except low hazard dams, to develop inundation maps and emergency action plans. DSOD approves inundation maps, and Cal OES approves emergency action plans. Based on review of the California Department of Water Resources Dam Breach Inundation Maps, City of Compton General Plan, and County of Los Angeles General Plan, the site lies within a potential inundation zone for failure of the Whittier Narrows Dam (19 kilometers, 11.8 miles northeast), the Hansen Dam (44.1 kilometers, 27.5 miles northwest), and the Sepulveda Dam (39.6 kilometers, 24.6 miles northwest). Accordingly, the Project Civil Engineer should consider the effects of Dam Inundation for the proposed development.

4.9. Tsunamis and Seiches

Tsunamis are waves generated by massive landslides near or under sea water. The site is not located on any State of California – Los Angeles County Tsunami Inundation Map for Emergency Planning. The potential for the site to be adversely impacted by earthquake-induced tsunamis is considered negligible because the site is located approximately 12.9 kilometers (8 miles) inland from the Pacific Ocean shore, at an elevation exceeding the maximum height of potential tsunami inundation.

Seiches are standing wave oscillations of an enclosed water body after the original driving force has dissipated. The potential for the site to be adversely impacted by earthquake-induced seiches is considered negligible due to the lack of any significant enclosed bodies of water located in the vicinity of the site.

4.10. Compressible and Expansive Soils

The investigation revealed that the site is underlain by deep alluvial material. The upper six feet of soils at the site as described in Section 5.2 may be subject to slight compression under the anticipated loading. Recommendations for removal and re-compaction of these materials are described in Section 5.2 of this report. If implemented, the recommendations for removal and proper compaction should mitigate the static compressibility potential for the proposed grading and improvements.

Heaving from expansive soils is a major leading cause of damage and damage related claims to structures in the U.S. each year. Clayey soils possess a “sponge-like” hydro-shrink/swell mechanism in which they will expand when provided a water source and will contract when drying. These shrink/swell mechanisms can cause considerable damage to structures, pavements and/or improvements when not properly treated and/or mitigated, particularly when occurring cyclically.

Appropriate laboratory testing was performed on representative samples of the encountered materials to assess their expansion potential characteristics. The test results indicate that these soils exhibit a very low to low expansion potential. Therefore, expansive soils are not considered to be a concern for the proposed development. However, expansive soils may exist elsewhere in the site area. Evaluation of exposed materials should be performed during excavation and grading to verify that conditions are as anticipated.

4.11. Corrosive Soils

The potential for the on-site materials to corrode buried steel and concrete improvements was evaluated. Laboratory testing was performed on representative soil samples to evaluate pH, minimum resistivity, and soluble chloride and sulfate contents. General recommendations to address the corrosion potential of the on-site soils are provided below. Imported fill materials, if used, should be tested to evaluate whether their corrosion potential is more severe than those assumed. Refer to Appendix B for chemical testing results.

4.11.1. Sulfate Exposure

Laboratory test results indicate that near-surface soils at the site with sulfates values are 38.5 and 76.3 ppm (mg/kg) which indicate sulfate exposure is negligible when exposed to Portland cement concrete (2010 CBC; ACI 318, 2014, Table 4.3.1). Any type of cement may be used for concrete structure and pipe.

4.11.2. Ferrous Metals

Soil resistivities were in mildly corrosive category when received. When soils were saturated, the resistivities dropped to moderately corrosive category. Soil pH values are 8.8 and 7.6 which indicate moderately to mildly alkaline. We recommend wrapping buried metal pipes in accordance with manufacturers recommendations.

The laboratory testing program performed for this project does not address the potential for corrosion to copper piping. In this regard, a corrosion engineer should be consulted to perform more detailed testing and develop appropriate mitigation measures (if necessary).

4.12. Seismic Design Parameters and Settlement Evaluation

Our recommendations for seismic design parameters have been developed in accordance with 2022 CBC and ASCE 7-16 (ASCE, 2016) standards. The applicable site class is D based on the results of our field investigation. Table 3 presents the seismic design parameters for the site in accordance with 2022 CBC. These values are intended for the design of structures to resist the

effects of earthquake ground motions for the site coordinates 33.87972° latitude and –118.20972° longitude, as underlain by soils corresponding to site Class D. In addition to the evaluation of seismic design parameters, a site specific ground motion analysis was performed for the subject project and the results of the analysis are presented in Appendix F.

Table 3
2022 California Building Code Design Parameters

Design Parameters	Value
Site Class	D
Mapped Spectral Acceleration Parameter at Period of 0.2-Second, S_s	1.693 g
Mapped Spectral Acceleration Parameter at Period 1-Second, S_l	0.606 g
Site Coefficient, F_a	1.0
Site Coefficient, F_v	1.7
Adjusted MCE_R Spectral Response Acceleration Parameter at Short Period, S_{MS}	1.693 g
1-Second Period Adjusted MCE_R^1 Spectral Response Acceleration Parameter, S_{Ml}	1.03 g
Short Period Design Spectral Response Acceleration Parameter, S_{DS}	1.129 g
1-Second Period Design Spectral Response Acceleration Parameter, S_{Dl}	0.687 g
Peak Ground Acceleration, PGA_M	0.801 g
Seismic Design Category	D

Notes: ¹ long period coefficient (F_v) of 1.7 may be utilized for calculation of T_s , provided that the value of the Seismic Response Coefficient (C_s) is determined by Equation 12.8-2 for values of the fundamental period of the building (T) less than or equal to $1.5T_s$ and taken as 1.5 times the value computed in accordance with either Equation 12.8-3 for T greater than $1.5T_s$ and less than or equal to TL or Equation 12.8-4 for T greater than TL .

4.13. Rippability

Based on our subsurface exploration of the site, the near-surface materials should be generally excavatable with heavy-duty earthwork equipment in good working condition.

4.14. Caving Potential

In general, the near surface soils contain significant amounts of fine grained material and have a low potential for caving. We recommend that the geotechnical engineer should be notified immediately if caving conditions are encountered during excavations to provide further mitigation recommendations.

5. GEOTECHNICAL ENGINEERING RECOMMENDATIONS

5.1. General Considerations

Based on the results of our field exploration and engineering analyses, it is our opinion that the proposed development is feasible from a geotechnical standpoint, provided that the recommendations in this report are incorporated into the design plans and are implemented during construction.

The following is a summary of the geotechnical considerations for this project:

- Groundwater was encountered during subsurface investigation at a depth around 52.8 to 54.2 feet below ground surface. Groundwater is not expected to impact the proposed development.
- The potential for landslide, tsunami and seiches to impact the proposed improvement is considered low.
- The site is not located within an AP Zone, however, it is subject to intense ground shaking during a seismic event.
- The onsite near-surface soils are expected to exhibit a very low to low expansion potential.
- The onsite near-surface soils are considered to have negligible exposure to sulfate and are corrosive to ferrous metals.
- The existing fill soils and disturbed soils should be removed and replaced as compacted fill. Fills should be compacted as recommended in this report.
- The potential for liquefaction and seismically induced settlement exists at the site. The estimated seismically induced settlement of the soils at the site was computed to be on the order of 6 inches, in the event of the design basis level of ground shaking.
- In order to reduce the adverse effects of liquefaction and seismically induced settlement, we recommend that proposed buildings for this project be founded on either 1) ground improvement using Deep Soil Mixing (DSM) and the use of conventional spread footings or 2) rigid mat foundation systems underlain by certified compacted fill or rock layers and high-strength geogrid, (cost effective solution).
- Foundations for small appurtenant structures, such as garden walls, trash enclosures which will not be tied-in to the proposed building, may be supported on conventional foundations bearing in certified compacted fill.
- All runoff from the site should be directed to the street via non-erosive drainage devices. Improve rear site drainage. Eave gutters should be added, all downspouts should discharge directly into pipe drains to the street. Other concentrated drainage should also be collected and discharged to the street in non-erosive devices.

5.2. Site Preparation

We conclude that the proposed development of the site is feasible from a geotechnical standpoint, provided the recommendations in this report are incorporated into the design and construction of the project. Recommendations for the proposed earthwork and improvements are included in the following sections and Appendix E. However, recommendations in the text of this report supersede those presented in Appendix E, should conflicts exist. All recommendations may require modifications or updating as project plans evolve, building locations are modified, or based on the conditions encountered during earthwork or construction.

Following demolition of the existing structures, underground utilities, and irrigation or water structures not to remain, the proposed improvement areas should be cleared of existing debris and deleterious materials. Objectionable materials, such as construction debris, vegetation, and other deleterious materials not suitable for structural backfill should be disposed of offsite at a regulated disposal facility. In the area of the proposed improvements, including structures, roadways, and minor distress-sensitive improvements, existing fill material and any eroded, desiccated, burrowed, disturbed soils from agricultural use, or otherwise loose or disturbed soils should be excavated to the minimum depths of six feet in the areas of proposed buildings, to the depth of suitable native materials, or to a minimum 24 inches below the bottom of all footings, whichever depth is greatest.

Removals should extend at least five feet laterally beyond the perimeter of the proposed structures, where feasible. Exposed subgrade should be moisture conditioned and properly compacted prior to receiving fill. The exposed subgrade may also require scarification. A representative of our office should observe the exposed subgrade to determine if scarification is necessary or practical based on the actual conditions present at the time of grading.

Any existing below ground utilities should be redirected around proposed structures or, alternatively, the conflicting utility backfill material over-excavated to the depth of suitable material with a minimum one-sack cement/sand slurry or compacted fill placed in the resulting void. If present, existing utilities at an elevation to extend through the proposed footings should be sleeved and caulked to minimize the potential for moisture migration below the structure slab. Any existing utility backfill present within the prism created by a 1(H):1(V) plane extending from the outer edges of the footings to suitable material up to ten feet beyond the building perimeter should be over-excavated and one-sack cement/sand slurry or compacted fill soil should be placed in the resulting area, as feasible. Abandoned pipes exposed by grading should be securely capped to prevent moisture from migrating beneath foundation and slab soils.

An engineer or geologist from UES should observe the exposed ground surface prior to scarification, if necessary. Excavation should continue until suitable native materials are encountered as indicated by a representative of our office. Organic and other deleterious materials not suitable for structural backfill should be properly disposed of off-site.

5.3. Site Excavation

Based on UES's observations, shallow excavations at the site should be feasible using standard, well-maintained construction equipment run by experienced operators.

Excessively dense soils or large boulders requiring larger equipment or non-standard methods of excavation are not typically anticipated at the subject site.

5.4. Fill Placement and Compaction

Following removal of existing fill material and loose, disturbed soils, the areas to receive fills, backfill from over-excavations, or improvements should be moisture conditioned, and properly compacted or wetted and proof-rolled, as appropriate. A representative of our office should observe the over-excavated surface or the excavated areas to determine if scarification is required. Fill and backfill should be compacted to a minimum relative compaction of 95 percent at a moisture content at or near optimum moisture contents, as evaluated by ASTM D1557. The optimum lift thickness for fill soil will depend on the type of compaction equipment used; however due to the potential for the relatively shallow groundwater to exhibit upward capillary movement, relatively heavy and/or vibratory compaction equipment may not be effective when backfilling over-excavations or while compacting fill within a few feet of the actual groundwater levels. As such, backfill should generally be placed in uniform, horizontal lifts not exceeding six inches in loose thickness.

5.5. Fill Materials

The on-site existing fill material, materials disturbed for agricultural activities, and native materials are considered suitable for use as fill and backfill material. However, these materials should be screened of organic materials and materials generally greater than three inches in maximum dimension. Irreducible materials greater than three inches in maximum dimension were not identified in the preliminary investigation but may be present due to the variable nature of the materials encountered. If irreducible materials greater than three inches (such as cobbles or boulders) are encountered, they generally should not be used in shallow fills (within six feet of proposed grades). In utility trenches, adequate bedding should surround pipes.

Imported fill beneath structures, pavements and walks should have an Expansion Index of 20 or less (ASTM D4829). Imported fill soils for use in structural or slope areas should be evaluated by the soils engineer before importation to the site. Imported fill soils may be subject to Department of Toxic Substances Control (DTSC) screening requirements, as determined by the owner.

If proposed, any retaining wall backfill located within a 45-degree wedge extending up from the heel of the wall footing should consist of soil having an Expansion Index of 20 or less (ASTM D4829) with less than 30 percent passing the No. 200 sieve. The upper 12 to 18 inches of wall backfill could consist of lower permeability soils, in order to reduce surface water infiltration behind walls. We understand that no basements are proposed at this time.

5.6. Foundation Recommendations

The following recommendations are for preliminary design purposes only. These foundation recommendations should be reviewed after completion of rough grading of the building pad areas. The site is susceptible to settlement and liquefaction during a major seismic event. Analyses of the data obtained from the Cone Penetration Tests indicate that seismic settlement during a major seismic event would be on the order of six inches. As such, seismic settlements should be considered for foundation design. The following are recommendations for mitigating the effects of liquefaction and seismically induced settlements.

5.6.1. Ground Improvement by Deep Soil Mixing (DSM)

The proposed ground improvement system for the project site involves the use of deep soil mixing (DSM) columns arranged in a lattice grid pattern to form overlapping crisscrossing secant panels. The objective of this system is to provide static bearing capacity support and reduce settlement by reinforcing the soil and shielding it from seismic loading. The DSM panels are aligned with the strip footings to ensure effective distribution of the loads. The proposed DSM layout is presented in Appendix H – Ground Improvement Design - Deep Soil Mixing.

The proposed DSM includes the columns diameter of 3 ft with an area replacement ratio (ARR) of 30%. The total length of the DSM should be verified during the construction by the actual depth of coarse-grained materials. However, it is anticipated the total installation depth would be approximately 20 feet below existing grade.

The settlement analysis was conducted based on the minimum average 28-day unconfined compressive strength of 150 psi according to ASTM D1633 "Standard Test Methods for Compressive Strength of Molded Soil-Cement Cylinders". The static settlement analysis estimated a total expected settlement between 0.2 and 0.6 inches, which is well within the allowable settlement value of 1 inch. Thus, the ground improvement system is effective in reducing settlement and providing a stable foundation for the proposed construction.

To evaluate the potential for liquefaction-induced settlements, all six Cone Penetration Tests (CPTs) were analyzed. The post-improvement liquefaction-induced settlements are estimated to be between 0.8 and 0.9 inches, and differential settlements are expected to be half of these values over a horizontal span of 30 feet, which is about 0.5 inches or less. Thus, the post-improvement liquefaction differential settlements meet the allowable maximum value of 1 inch, demonstrating the effectiveness of the DSM ground improvement system. The results of static and seismic settlement calculations are presented in Appendix H.

5.6.2. Rigid Mat Foundation and Certified compacted fill/Crushed Rock Recommendations

In order to provide appropriate foundation support, to reduce the potential for static and dynamic foundation settlement, and to reduce the potential adverse secondary surface effects from liquefaction and seismic settlement on the proposed building foundations, we have concluded that proposed

structures could be supported by a system that includes rigid mat foundations underlain by a high-strength geogrid-reinforced layer of crushed rock.

If utilized, rigid mat foundation systems should be underlain by a minimum two-foot thick layer of geogrid-reinforced certified compacted fill or crushed rock. The following recommendations are provided if the geogrid-reinforced crushed rock and mat foundation system will be utilized at the subject site:

1. The geogrid and certified compacted fill or crushed rock layer should be placed as deep beneath the proposed mat foundation as possible in order to provide a compacted fill zone between the mat foundation and the rock for utility placement and to provide added structural separation between the rock and the foundation.
2. The geogrid and certified compacted soil or crushed rock layer should extend a minimum six feet laterally beyond the building footprint limits.
3. The crushed rock layer should be placed upon a suitable and properly prepared exposed subgrade, and upon a layer of Tensar BX-1200, Tensar TX-160, Hanes TerraGrid RX1200, or Mirafi BXG12, installed as per the manufacturer's specifications.
4. A second layer of geogrid should be properly placed at the approximate mid-point of the minimum two-foot thick certified compacted soil or crushed rock layer.
5. A layer of filter fabric should be placed upon the top surface of the crushed rock layer prior to being backfilled to proposed grade with suitable onsite or imported compacted fill soils.

5.6.2.1. Mat Foundation Specifics

Mat foundations should consist of a structural, moment and shear resisting slab, or an integrated system of structural slabs and moment/shear resisting grade beams. Bearing elements should be embedded a minimum of 24 inches. Mat foundations can be designed with an allowable bearing capacity of 2,000 pounds per square foot (psf). A one-third increase may be used for evaluation of short duration wind loads, not for short term seismic loads. A modulus of subgrade reaction of 120 psi/inch is also considered appropriate. Due to the specialized design required for the rigid mat foundation systems, reinforcement size, spacing, and detailing should be as per the structure engineer of record.

For mat foundations, the maximum total post-construction static settlement is expected to be less than one inch and the maximum differential static settlement is expected to be less than ½ inch. For mat foundations constructed upon a geogrid-reinforced certified compacted soil or crushed rock layer, the estimated total seismic settlement is anticipated to be less than 6 inches, with differential seismic settlements on the order of 4 inches.

5.6.3. Conventional Spread Foundations

As detailed herein, if ground modification is performed as recommended utilizing DSM (as described in Sections above, respectively), conventional continuous and/or spread footings may be suitable. Grade beams should generally be installed across all large entrances or critical areas in the structures. Footings and grade beams should have minimum depths of 24 inches below the lowest adjacent grade. Isolated spread footings should be a minimum of two feet in minimum dimension. Continuous footings and grade beams should be reinforced as required by the structural engineer of record; however, we recommend minimum continuous reinforcement should consist of four No. 5 rebars, two near the top and two near the bottom. Footings may be designed using maximum allowable bearing capacities of 2,000 psf. A one-third increase is also considered acceptable for evaluation of short-term loadings due to wind or seismic forces.

5.6.4. General Foundation Recommendations

The following general recommendations for footings are also provided:

- The structural engineer should provide recommendations for reinforcement of any spread footings and footings with pipe penetrations.
- Footing excavations should generally be maintained at above optimum moisture content until concrete placement.
- All foundation excavations should be observed by soil engineer during excavation, and prior to placement of reinforcing steel or formwork. The foundation excavations should be moistened to at least optimum moisture content.

5.6.5. Foundation Setback

Footings should bear beneath a 1(H):1(V) plane extended up from the nearest bottom edge of adjacent trenches and/or excavations. Deepening of affected footings may be a suitable means of attaining the prescribed setbacks.

5.6.6. Interior Concrete Slabs

Lightly loaded concrete slabs should be designed for the anticipated loadings but measure at least five inches in thickness. If a rigid mat foundation with crushed rock system is utilized, then the minimum thickness of the slab should conform to the recommendations in above Sections of this report. Minimum slab reinforcement should consist of a minimum of number 4 reinforcing bars placed on 18-inch centers, each way, at or above mid-slab height, but with proper concrete cover, or as per the project architect or structural engineer. In moisture-sensitive floor areas, a suitable vapor retarder of at least ten-mil thickness (with all laps or penetrations sealed or taped) overlying a two-inch layer of consolidated aggregate base or sand (with SE of 30 or more) should be installed. A maximum two-inch layer of similar material may be placed above the vapor retarder to protect the membrane during steel and concrete placement. This recommended protection is generally considered typical in the industry. If proposed floor areas or coverings are considered especially

sensitive to moisture emissions, additional recommendations from a specialty consultant could be obtained. UES is not an expert at preventing moisture penetration through slabs. A qualified architect or other experienced professional should be contacted if moisture penetration is a more significant concern.

Slabs subjected to heavier loads may require thicker slab sections and/or increased reinforcement. A 120-pci subgrade modulus is considered suitable for elastic design of minimally embedded improvements such as slabs-on-grade.

Subgrade materials should be maintained near or above optimum moisture content until slab underlayment or concrete are placed.

5.7. Lateral Resistance

Lateral loads acting against structures may be resisted by friction between the footings and the supporting soil or passive pressure acting against structures. If frictional resistance is used, we recommend allowable coefficients of friction of 0.35 (total frictional resistance equals the coefficient of friction multiplied by the dead load) for concrete cast directly against compacted fill. A design passive resistance value of 200 pounds per square foot per foot of depth (with a maximum value of 2,000 pounds per square foot) may be used. The allowable lateral resistance can be taken as the sum of the frictional resistance and the passive resistance, provided the passive resistance does not exceed two-thirds of the total allowable resistance.

5.8. Settlement

The estimated total *seismic* settlement is 6 inches with differential settlements on the order of 4 inches ($\frac{2}{3} \times 6$) in a horizontal distance of approximately 30 feet.

The anticipated total *static* settlement is approximately 1 inch measured between adjacent structural elements. Differential settlements are expected to be less than one-half of an inch, measured between adjacent structural elements or in a distance of 30 feet.

5.9. Exterior Flatwork

To reduce the potential for cracking in exterior flatwork caused by minor movement of subgrade soils and concrete shrinkage, we recommend that such flatwork be installed with crack-control joints at appropriate spacing as designed by the project architect. Additionally, we recommend that flatwork be installed with at least number 3 reinforcing bars at 24-inch centers, each way, at mid-height of slab or other reinforcement per the project consultants. Flatwork, which should be installed with crack control joints, includes driveways, sidewalks, and architectural features. All subgrades should be prepared according to the earthwork recommendations previously given before placing concrete. Positive drainage should be established and maintained next to all flatwork. Subgrade materials shall be maintained or elevated to above optimum moisture content until just before concrete placement.

5.10. Temporary Excavations

The following recommendations for temporary cuts and slopes should be relatively stable against deep-seated failure but may experience a degree of localized sloughing. Surcharging from material stockpiles, grading equipment, or construction materials at tops of cuts and/or slopes should be avoided within a minimum distance equal to the total vertical height of the excavation.

The following criteria should be considered for unbraced / unshored temporary excavations and/or trenches without the use of proper shoring. The on-site soils are considered Type B and C soils with recommended slope ratio as set forth in Table 4.

Table 4
Recommended Temporary Slope Ratio

Soil Type	Slope Ratio	Maximum Height
C (Existing alluvium, fill, or any soils not identified during the investigation)	1.5(H):1(V) (or flatter)	5.0 Feet

Actual field conditions and soil type designations must be verified by a "competent person" while excavations exist, according to Cal-OSHA regulations. In addition, the above sloping recommendations do not allow for surcharge loading at the top of slopes by vehicular traffic, equipment or materials. Appropriate surcharge setbacks must be maintained from the top of all unshored slopes.

Temporary excavations for the demolition, earthwork, footings, retaining walls and utility trenches are expected to be up to 4 feet in height. Due to relatively loose condition of shallow onsite soils, temporary, unsurcharged excavation sides should be sloped no steeper than an inclination of 1.5(H):1(V). Where sloped excavations are created, the tops of the slopes should be barricaded so that vehicles and storage loads do not encroach within 10 feet of the top of the excavated slopes. A greater setback may be necessary when considering heavy vehicles, such as concrete trucks and cranes. UES should be advised of such heavy vehicle loadings so that specific setback requirements can be established. If the temporary construction slopes are to be maintained during the rainy season, berms are recommended to be graded along the tops of the slopes in order to prevent runoff water from entering the excavation and eroding the slope faces.

UES should observe the excavations so that any necessary modifications based on variations in the encountered soil conditions can be made. All applicable safety requirements and regulations, including CalOSHA requirements, should be met.

5.11. Pavement Design

5.11.1. Flexible Pavement Design

Our pavement structural design is in accordance with Chapter 600 of the Caltrans Highway Design Manual, which is based on a relationship between the gravel equivalent (GE) of the pavement structural materials, the traffic index (TI), and the R-value of the underlying subgrade soil. The onsite soils exhibit an R-value of 39 during our testing. Accordingly, our proposed pavement sections are based at an R-value of 30. On this basis, Table 5 provides recommended minimum thicknesses for hot mix asphalt (HMA) and aggregate base sections for different traffic indices.

Table 5
Recommended Minimum HMA and Base Section Thicknesses

Location	Parking Stalls	Drive Aisle	Firelane / Truck Driveway
Traffic Index	4.5	5.5	7.0
HMA Thickness (in)	3.0	3.0	4.0
Aggregate Base Thickness (in)	4.0	7.0	10.0

Prior to construction of the pavement sections provided above, the subgrade for the proposed pavement should be moisture conditioned to a depth of 12 inches and compacted to achieve 95 percent. The aggregate base section should then be placed, moisture conditioned to near optimum moisture content and compacted to achieve 95 percent relative compaction. The HMA section should be in accordance with the City of Compton requirements and should be compacted to 95 percent relative compaction. A representative of UES should be onsite to observe and test the subgrade, base and HMA sections.

5.11.2. Portland Cement Concrete (PCC) Pavement Design

If Portland cement concrete pavement is used, it should have a minimum modulus of rupture (flexural strength) of 600 psi. We estimate that a 4,500 psi 28-day compressive strength concrete would generally provide the minimum required flexural strength; however, other mix designs could also meet the requirements. As such, we recommend that the contractor submit the proposed mix design with necessary documentation to offer a proper level of confidence in the proposed concrete materials. Recommended concrete pavement sections are presented below in Table 6.

Table 6
Portland Cement Concrete (PCC) Pavement Section

Location	Parking Stalls	Drive Aisle	Firelane / Truck Driveway
Traffic Index	4.5	5.5	7.0
Concrete Thickness (in)*	5.0	6.0	7.0
Aggregate Base Thickness (in)	4.0	4.0	4.0

* Design Modulus of Subgrade Reaction = 120 pci

An unreinforced pavement with the minimum thickness indicated above should generally be constructed with maximum joint spacing of 24 times the pavement thickness, in both directions, and in nearly square patterns. As an alternative, the concrete pavement could be constructed with typical minimal reinforcement consisting of #4 bars at 18 inches, on-center, both ways, at or above mid-slab height and with proper concrete cover.

5.12. Drainage Control

Proper surface drainage is critical to the future performance of the project. Saturation of a soil can cause it to lose internal shear strength and increase its compressibility, resulting in a change in the designed engineering properties. Proper site drainage should be always maintained. All site drainage, with the exception of any required to be disposed of onsite by stormwater regulations, should be collected and transferred to the street in non-erosive drainage devices.

The proposed structure should be provided with roof drainage. Discharge from downspouts, roof drains and scuppers should not be permitted on unprotected soils within five feet of the building perimeter. Drainage should not be allowed to pond anywhere on the site, and especially not against any foundation or retaining wall. Drainage should not be allowed to flow uncontrolled over any descending slope. Planters which are located within a distance equal to the depth of a retaining wall should be sealed to prevent moisture adversely affecting the wall. Planters which are located within five feet of a foundation should be sealed to prevent moisture affecting the earth materials supporting the foundation.

6. DESIGN REVIEW AND CONSTRUCTION MONITORING

Geotechnical review of plans and specifications is of paramount importance in engineering practice. The poor performance of many structures has been attributed to inadequate geotechnical review of construction documents. Additionally, observation of excavations will be important to the performance of the proposed development. The following sections present our recommendations relative to the review of construction documents and the monitoring of construction activities.

6.1. Plans and Specifications

The design plans and specifications should be reviewed by UES prior to bidding and construction, as the geotechnical recommendations may need to be reevaluated in the light of the actual design configuration and loads. This review is necessary to evaluate whether the recommendations contained in this report and future reports have been properly incorporated into the project plans and specifications. Based on the work already performed, this office is best qualified to provide such review.

6.2. Construction Monitoring

Site preparation, removal of unsuitable soils, assessment of imported fill materials, fill placement, foundation installation, and other site grading operations should be observed and tested. The substrata exposed during the construction may differ from that encountered in the test excavations. Continuous observation by a representative of UES during construction allows for evaluation of the soil conditions as they are encountered and allows the opportunity to recommend appropriate revisions where necessary.

The project engineer should be notified prior to exposure of subgrades. It is critically important that the engineer be provided with an opportunity to observe all exposed subgrades prior to burial or covering.

7. LIMITATIONS

The recommendations and opinions expressed in this report are based on information obtained from our field exploration for the site. In the event that any of our recommendations conflict with recommendations provided by other design professionals, we should be contacted to aid in resolving the discrepancy.

Due to the limited nature of our field explorations, conditions not observed and described in this report may be present on the site. Uncertainties relative to subsurface conditions can be reduced through additional subsurface exploration. Additional subsurface evaluation and laboratory testing can be performed upon request. It should be understood that conditions different from those anticipated in this report may be encountered during excavation operations, for example, the presence of unsuitable soil, and that additional effort may be required to mitigate them.

Site conditions, including groundwater elevation, can change with time as a result of natural processes or the activities of man at the subject site or at nearby sites. Changes to the applicable laws, regulations, codes, and standards of practice may occur as a result of government action or the broadening of knowledge. The findings of this report may, therefore, be invalidated over time, in part or in whole, by changes over which UES has no control.

UES's recommendations for this site are, to a high degree, dependent upon appropriate quality control of foundation construction. Accordingly, the recommendations are made contingent upon the opportunity for UES to observe foundation excavations for the proposed construction. If parties other than UES are engaged to provide such services, such parties must be notified that they will be required to assume complete responsibility as the geotechnical engineer of record and the engineering geologist of record for the geotechnical phase of the project by concurring with the recommendations in this report and/or by providing alternative recommendations.

This document is intended to be used only in its entirety. No portion of the document, by itself, is designed to completely represent any aspect of the project described herein. UES should be contacted if the reader requires additional information or has questions regarding the content, interpretations presented, or completeness of this document.

This report has been prepared for the exclusive use by the client and its agents for specific application to the proposed design and construction of the project described herein. Any party other than the client who wishes to use this report for an adjacent or nearby project, shall notify UES of such intended use. Land use, site conditions, or other factors may change over time, and additional work may be required with the passage of time. Based on the intended use of this report and the nature of the project, UES may require that additional work be performed and that an updated report be issued. Non-compliance with any of these requirements by the client or any other party will release UES from any liability resulting from the use of this report by any unauthorized party.

UES has endeavored to perform its evaluation using the degree of care and skill ordinarily exercised under similar circumstances by reputable geotechnical professionals with experience in

this area in similar soil conditions. No other warranty, either expressed or implied, is made as to the conclusions and recommendations contained in this report.

8. SELECTED REFERENCES

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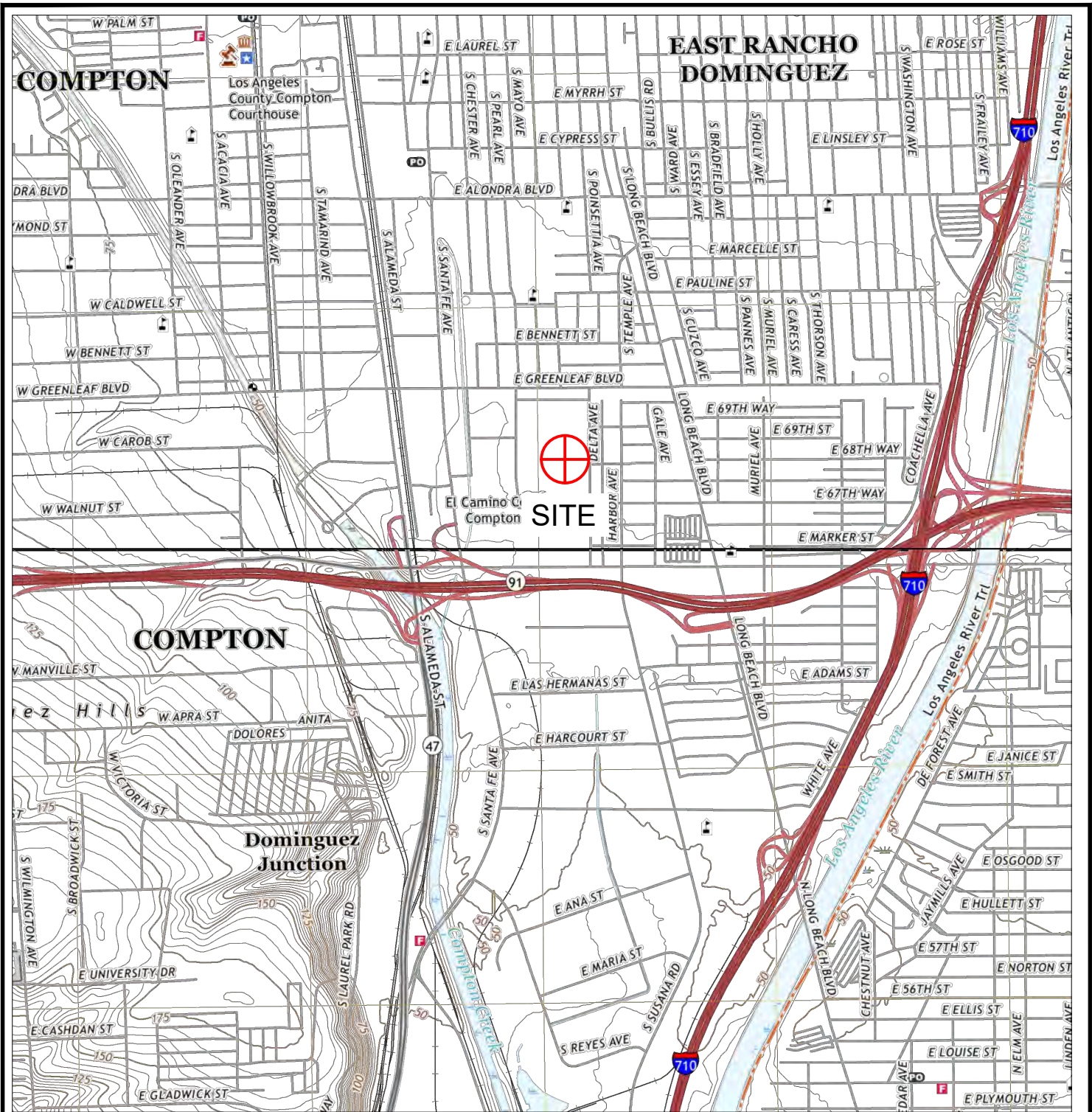
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FIGURES



**APPROXIMATE
SITE LOCATION**



SCALE IN FEET



REFERENCE: USGS "South Gate 7.5-Minute Quadrangle" (2021), USGS "Long Beach 7.5-Minute Quadrangle" (2021)

SITE VICINITY LOCATION MAP

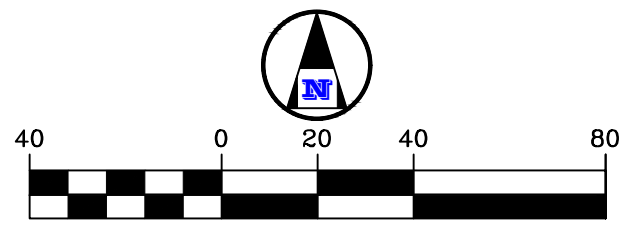
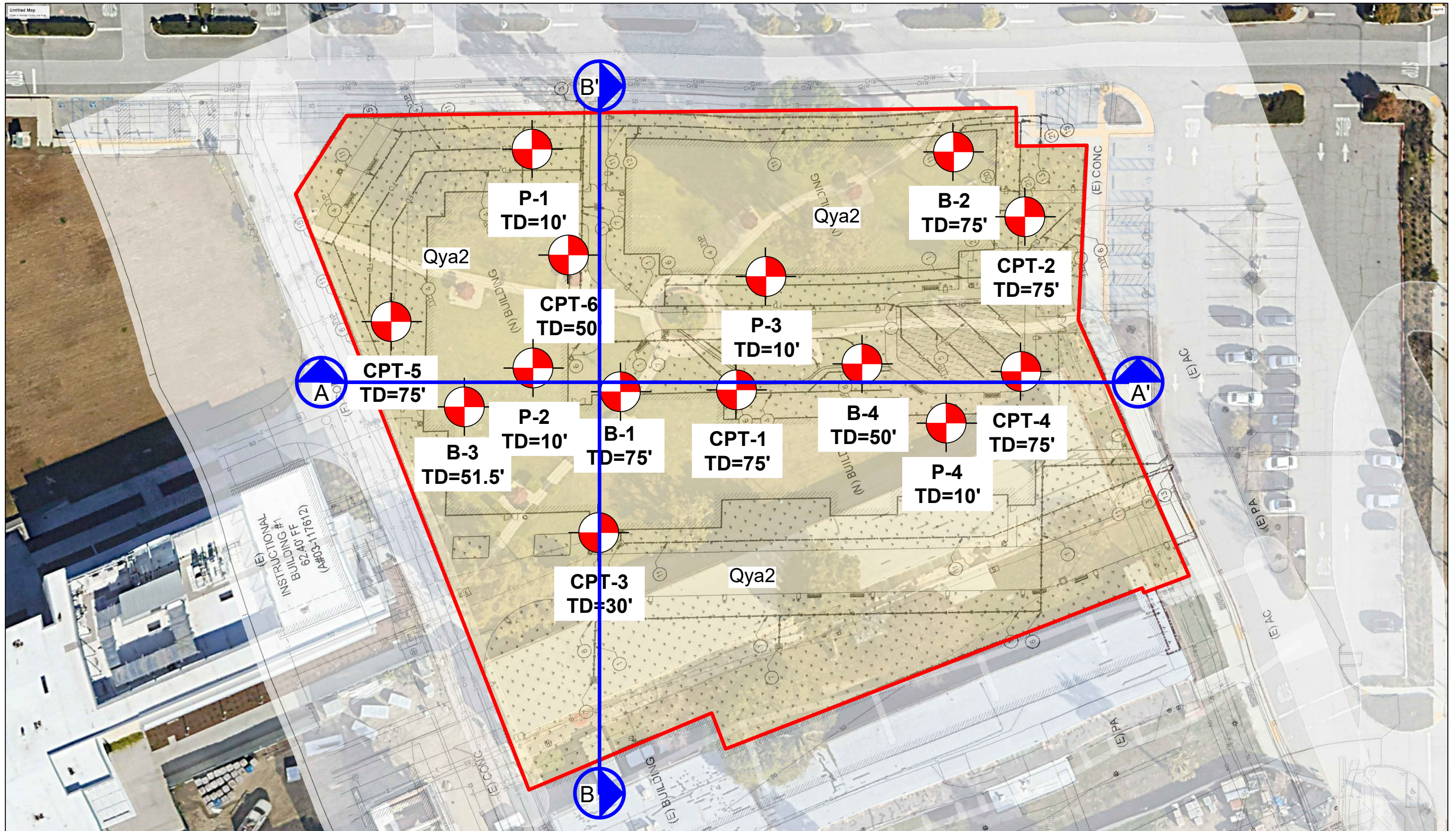
Compton College Student Housing
1111 E. Artesia Blvd.
Compton, California



PROJECT NO.
4230.2200060.0000

REPORT DATE
December 2022

FIGURE 1



- Project Boundary
- Cross Section Location
- Boring Location
- Qya2 Young Alluvium, Unit 2

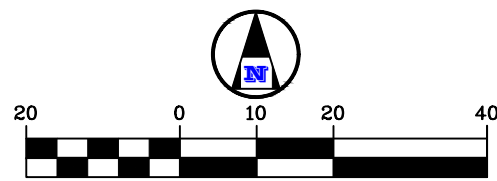
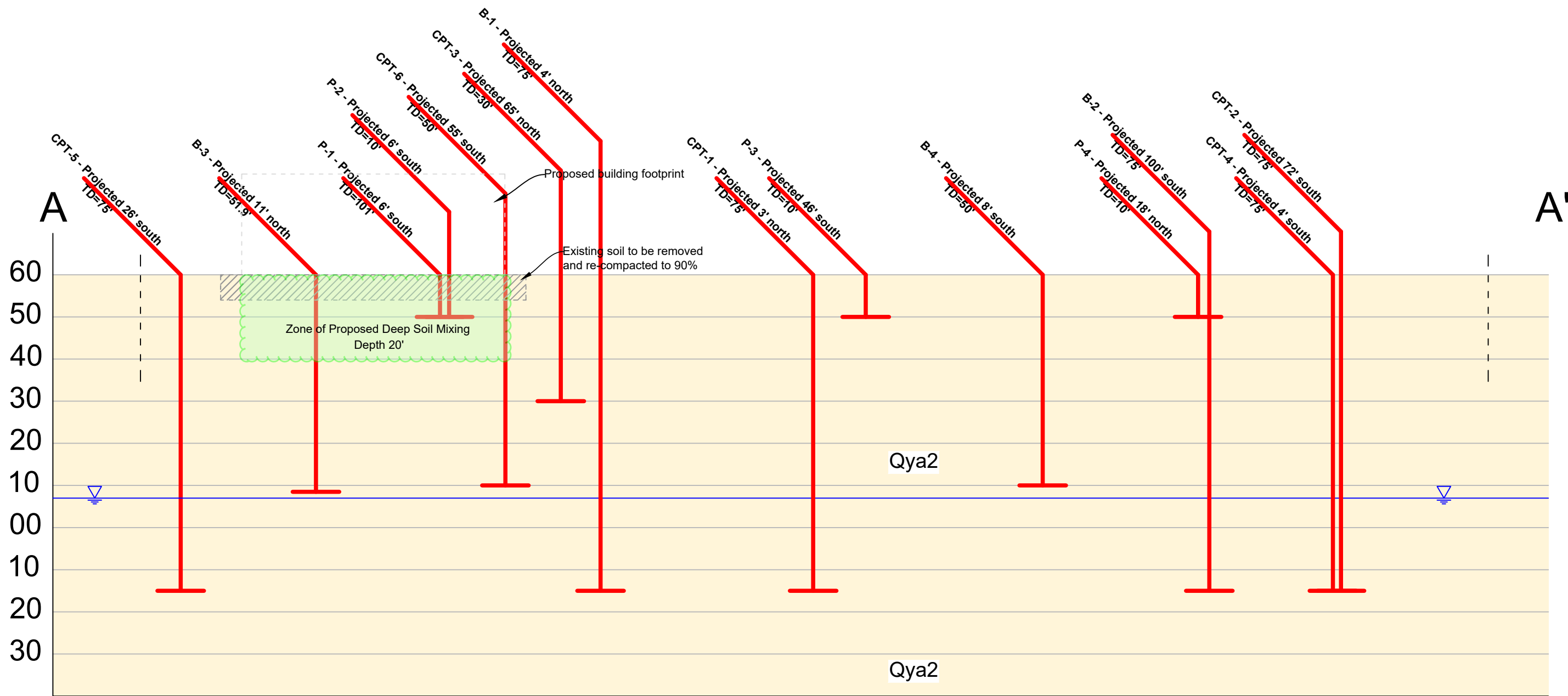


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Geologic Site Plan
Proposed Student Housing
1111 East Artesia Boulevard
Compton, California 90221

Los Angeles County AIN: 7318-006-900 (North East Corner)

Drawn by	BSK
Job No.	4230.2200060.0000
Date	01-28-2023
Scale	1:40
Figure	2

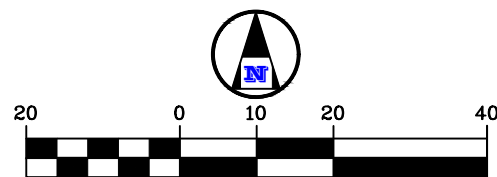
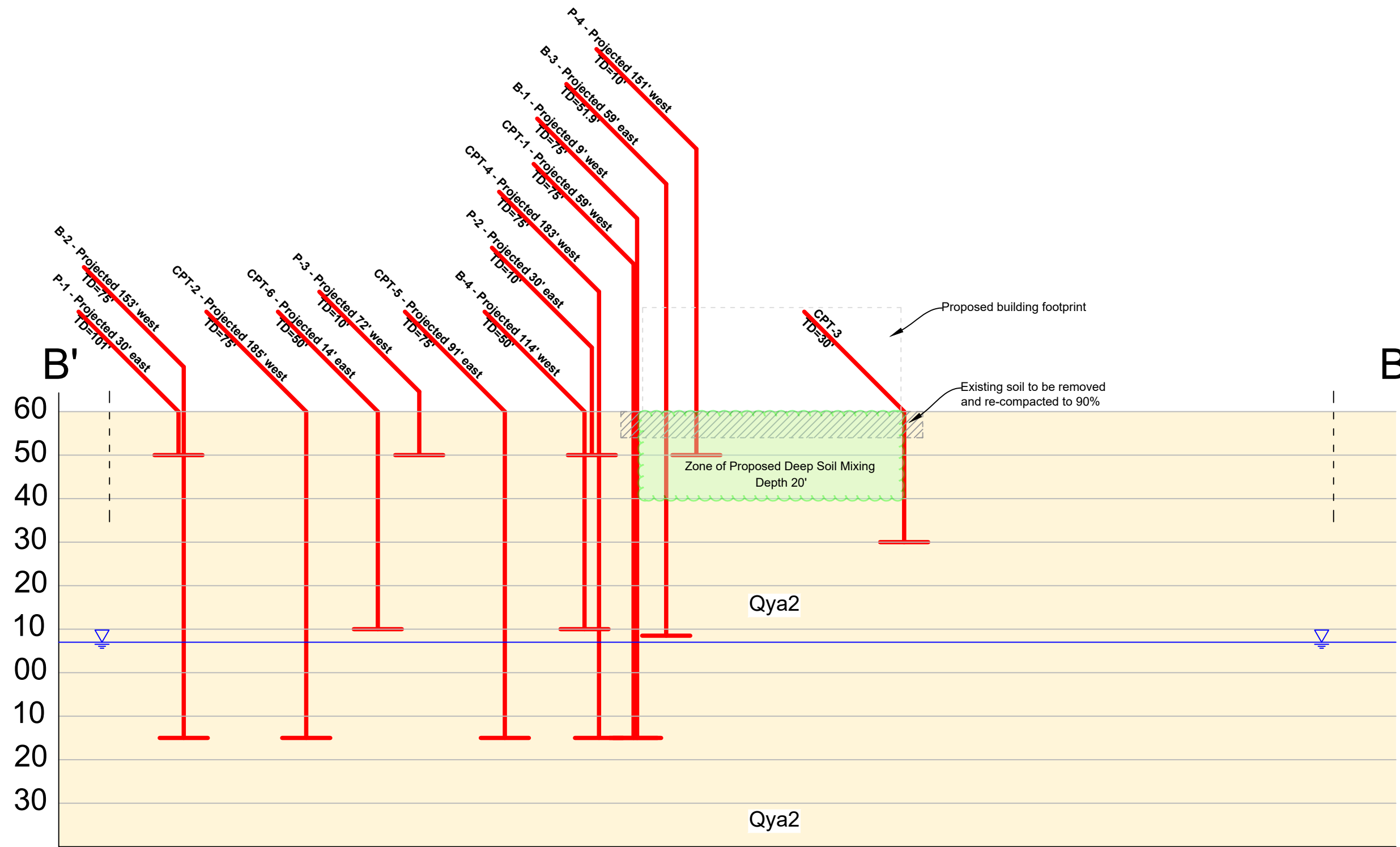


- Qya2 Young alluvium, unit 2
- Depth of Boring
- Ground Water
- Project Boundary

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Cross Section A-A'
Proposed Student Housing
1111 East Artesia Boulevard
Compton, California 90221
Los Angeles County AIN: 7318-006-900 (North East Corner)

Drawn by	BSK
Job No.	4230.2200060.0000
Date	01-28-2023
Scale	1:25
Figure	3A



- Qya2 Young alluvium, unit 2
- Depth of Boring
- Ground Water
- Project Boundary

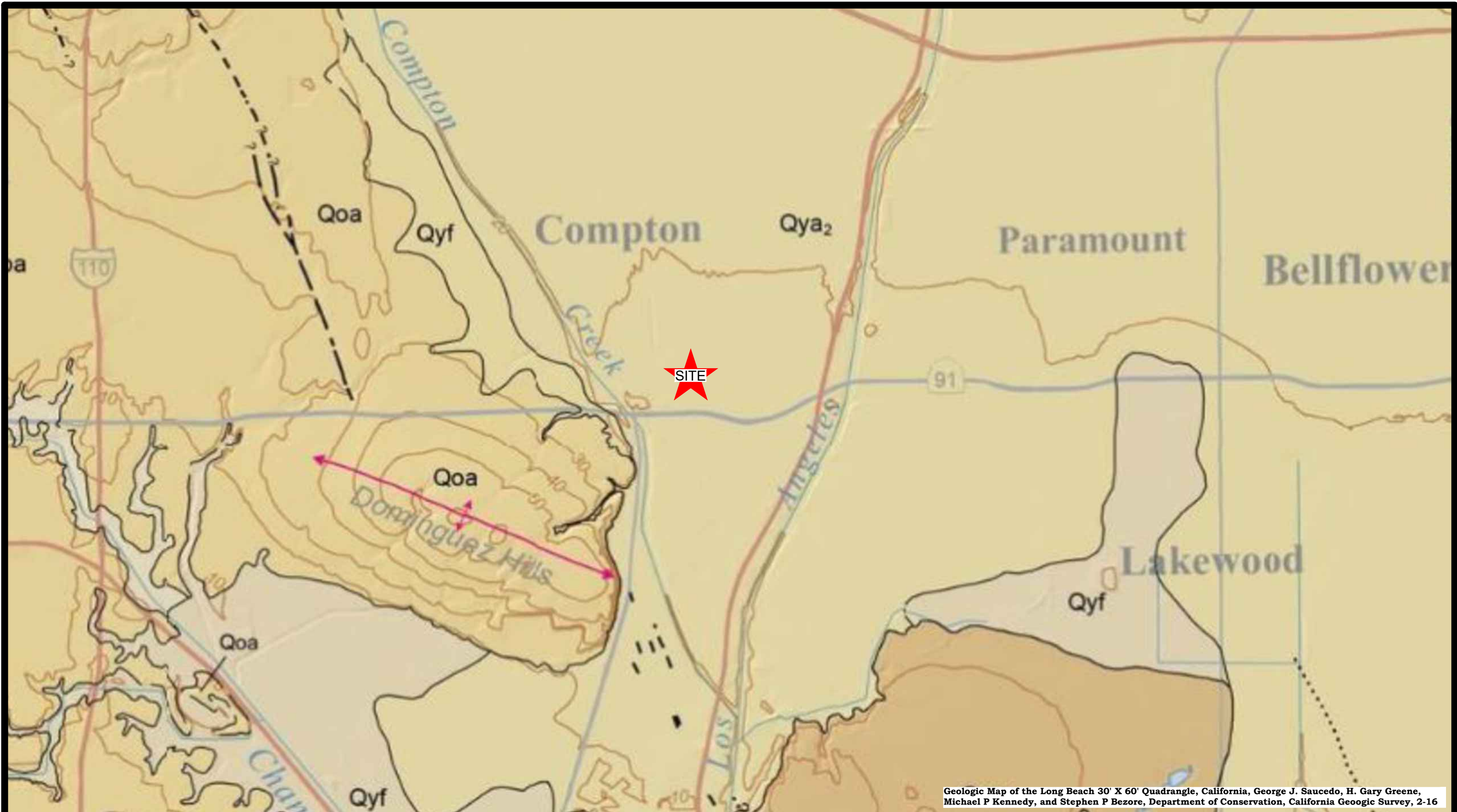


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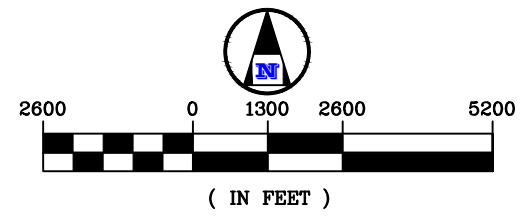
Cross Section B-B'
Proposed Student Housing
1111 East Artesia Boulevard
Compton, California 90221

Los Angeles County AIN: 7318-006-900 (North East Corner)

Drawn by	BSK
Job No.	4230.2200060.0000
Date	01-28-2023
Scale	1:25
Figure	3B



Geologic Map of the Long Beach 30' X 60' Quadrangle, California, George J. Saucedo, H. Gary Greene, Michael P Kennedy, and Stephen P Bezore, Department of Conservation, California Geologic Survey, 2-16



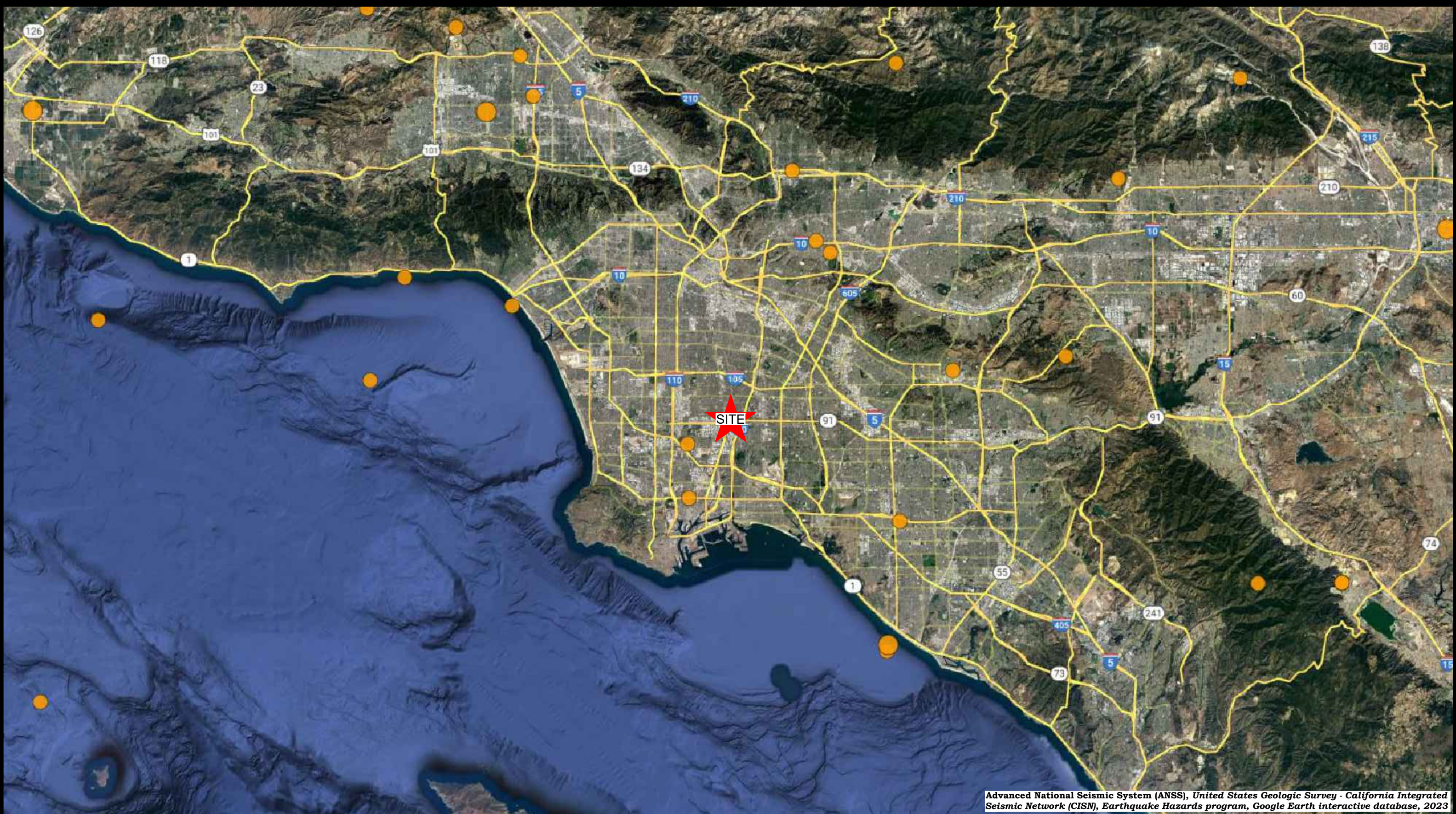
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- Qoa Old alluvium, undivided
- Qyf Young alluvial fan deposits, undivided
- Qom Old shallow marine deposits on wave-cut surface



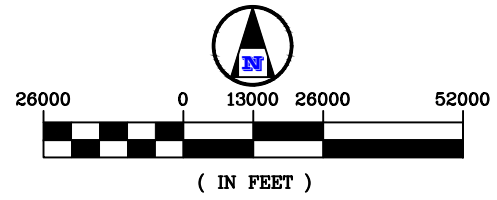
16 Technology Drive Suite 139
Irvine, Ca, 92618 T: (949) 537-3222

Regional Geologic Map
Proposed Student Housing
1111 East Artesia Boulevard
Compton, California 90221
Los Angeles County AIN: 7318-006-900 (North East Corner)

Drawn by	BSK
Job No.	4230.2200060.0000
Date	01-28-2023
Scale	
Figure	4



Advanced National Seismic System (ANSS), United States Geologic Survey - California Integrated Seismic Network (CISN), Earthquake Hazards program, Google Earth interactive database, 2023



Depth (km)	
Orange circle	0 - 33
Yellow circle	33 - 70
Green circle	70 - 150
Blue circle	150 - 300
Purple circle	300 - 500
Red circle	500 - 800

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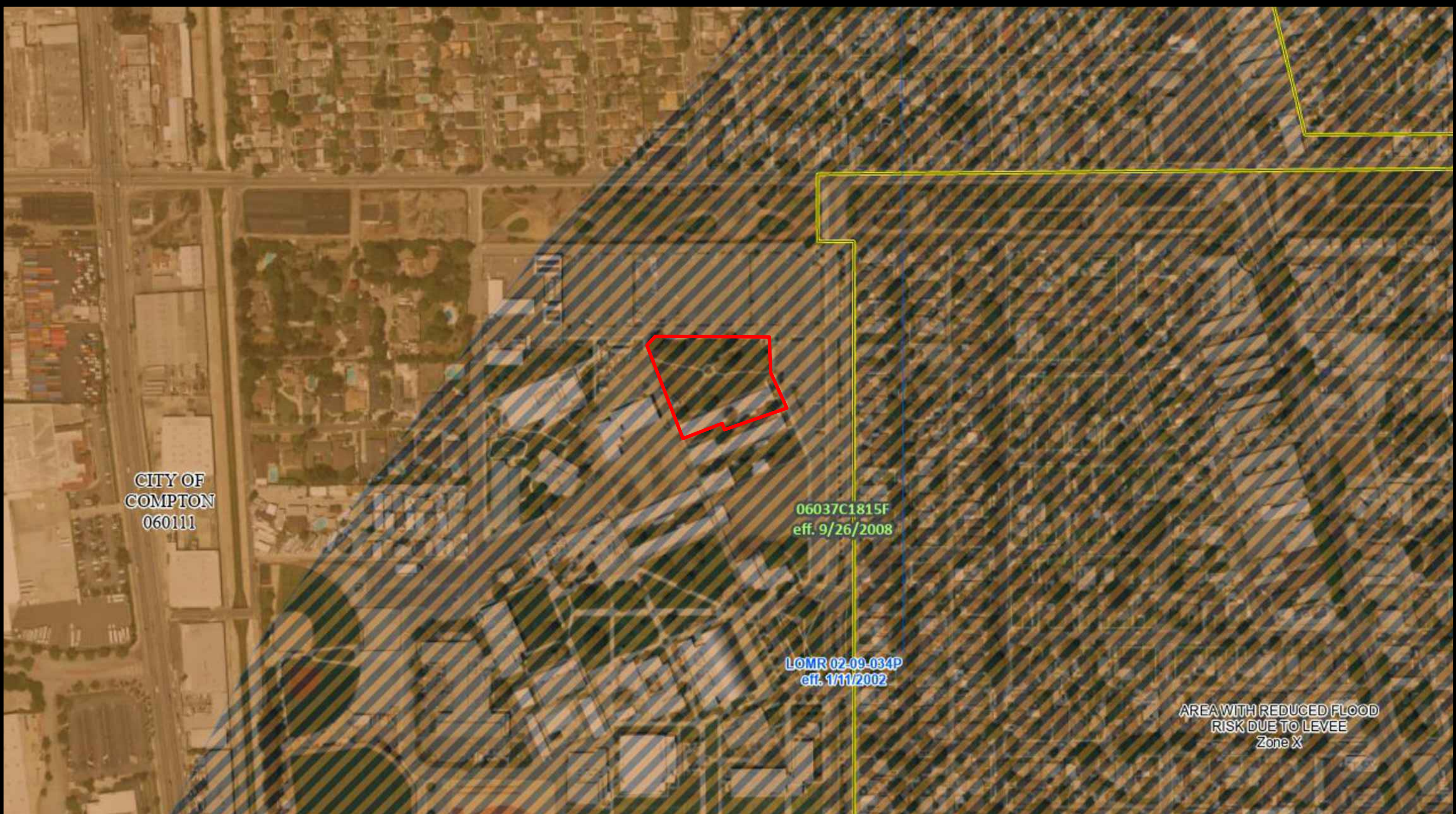
16 Technology Drive Suite 139
Irvine, Ca, 92618 T: (949) 537-3222

Regional Earthquake Epicenter Map

Proposed Student Housing
1111 East Artesia Boulevard
Compton, California 90221

Los Angeles County AIN: 7318-006-900 (North East Corner)

Drawn by	BSK
Job No.	4230.2200060.0000
Date	01-28-2023
Scale	
Figure	6

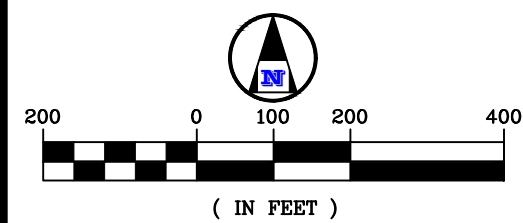


CITY OF
COMPTON
060111

06037C1815F
eff. 9/26/2008

LOMR 02-09-034P
eff. 1/11/2002

AREA WITH REDUCED FLOOD
RISK DUE TO LEVEE
Zone X



— Project Boundary

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FEMA Flood Hazard Map
Zone X: Reduced Flood Risk due to Levee
1111 East Artesia Boulevard
Compton, California 90221
Los Angeles County AIN: 7318-006-900 (North East Corner)

Drawn by	BSK
Job No.	4230.2200060.0000
Date	01-28-2023
Scale	
Figure	7

APPENDIX A

Field Exploration and Boring Logs

Appendix A – Field Exploration and Boring Logs

General

The subsurface exploration program for the proposed project consisted of logging four 8-inch diameter exploratory borings conducted at the site between December 22, 2022, and January 17, 2023. Exploration depths varied between 10.0' and 76.5' below the existing grades. The drilling operation was performed using a limited access track-mounted CME-75 hollow-stem-auger drill rig performed by One Way Drilling, Inc.

Drilling and Sampling

The Boring Logs are presented in the following pages. The log also shows the boring number and drilling date. The borings were logged by a geologist using the Unified Soil Classification System. The boundaries between soil types shown on the logs are approximate because the transition between different soil layers may be gradual. Drive and bulk samples of representative earth materials were obtained from the borings.

Disturbed samples were obtained using a Standard Penetration Sampler (SPT). This sampler consists of a 2-inch O.D., 1.4-inch I.D. split barrel shaft that is advanced into the soil at the bottom of the drilled hole a total of 18 inches. The number of blows required to drive the sampler the final 12 inches is presented on the boring logs. Soil samples obtained by the SPT were retained in plastic bags.

A California modified sampler was used to obtain drive samples of the soil encountered. This sampler consists of a 3-inch outside diameter (O.D.), 2.4-inch inside diameter (I.D.) split barrel shaft that was driven a total of 12-inches into the soil at the bottom of the boring by a safety hammer weighing 140 pounds at a drop height of approximately 30 inches. The soil was retained in brass rings for laboratory testing. Additional soil from each drive remaining in the cutting shoe was usually discarded after visually classifying the soil. The number of blows required to drive the sampler the final 12 inches is presented on the boring logs.

Upon completion of the borings, the boreholes were backfilled with soil from the cuttings.

CONE PENETROMETER TEST SOUNDINGS

Cone Penetrometer Test (CPT) soundings were performed for us at 6 locations by Kehoe Testing & Engineering. The soundings extended to depths of up to approximately 75 feet. The locations of the soundings are shown on Figure 2. The results of the soundings, shear wave velocities (performed on CPT-1, CPT-2, CPT-4, and CPT-5) and the methodology of performing the soundings are presented in the Kehoe Testing & Engineering report in this appendix.



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CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/22/22 **COMPLETED** 12/22/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879695, -118.210009
GROUNDWATER LEVELS Encountered at 52' 9"
BACKFILL Native cuttings

NOTES

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist									
		(SC) Clayey SAND, dark olive brown, loose to med. dense, damp	AU SPT	7-5-5 (10)							
		(CL) Lean CLAY, olive brown, stiff, damp	MC	5-7-12 (19)		94.1	26.2				
10		(ML) Silt with SAND, olive brown, medium soft, damp	SPT	3-3-4 (7)				34	25	9	75.9
		(CL) Lean CLAY, very dark grayish brown, stiff, damp	MC	4-8-12 (20)		102.6	19.2				
		(CL-ML) Sandy silty CLAY, olive brown, stiff, damp	SPT	5-6-7 (13)							61.7
20		Very stiff, moist	MC	6-10-25 (35)		100.0	9.7				
		(CL) Lean CLAY, dark olive brown, stiff, moist	SPT	3-4-5 (9)				39	22	17	86.7
30		(ML) Silt with SAND, olive, fine, stiff, moist, no smell, *CH (bottom two rings)	MC	8-8-9 (17)		100.0	14.4				
		(CL) Lean CLAY, olive gray, stiff, moist,	SPT	4-4-7 (11)							97.7
40		(ML) Silt with SAND, olive gray, hard, moist	MC	10-23-35 (58)		103.9	16.6				
		Wet, fine grained, very stiff	SPT	7-8-8 (16)				29	24	5	74.7
50		(SP-SM) Poorly graded SAND with silt, fine to medium, very dark greenish gray, very dense, wet	MC	17-39-50 (89)		103.1	19.1				
		(SM) Silty SAND, very dark greenish gray, dense, saturated	SPT	10-19-24 (43)							14.0
60		(SP-SM) Poorly graded SAND with silt, fine to medium, very dark greenish gray, very dense, saturated	MC	19-50 (69)		107.0	20.5				
		(SM) Silty SAND, greenish black, medium dense, saturated	SPT	3-6-8 (14)				NP	NP	NP	23.5
70		(SP-SM) Poorly graded SAND with silt, fine, very dark greenish gray, medium dense, saturated	MC	8-11-24 (35)							
		No recovery									
Bottom of borehole at 76.5 feet.											

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CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/22/22 **COMPLETED** 12/22/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879977, -118.209528
GROUNDWATER LEVELS Not encountered
BACKFILL Native cuttings

NOTES

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist	AU								
		(CL) Lean CLAY, dark olive brown, stiff, moist	MC	4-5-6 (11)		101.5	18.0				
		(ML) Sandy SILT, olive brown, stiff, moist	SPT	4-6-6 (12)				29	23	6	60.8
10		Very stiff, fine	MC	5-15-19 (34)		97.5	6.6				
		(CL-ML) Sandy silty CLAY, olive brown, stiff to very stiff, damp	SPT	5-5-10 (15)							
		(ML) Sandy SILT, fine, light olive brown, very stiff, damp	MC	11-17-21 (38)		105.5	6.5				
20		(CL-ML) Sandy silty CLAY, olive, hard, damp	SPT	15-19-23 (42)							
		(CL) Lean CLAY, dark olive brown, very stiff, damp	MC	13-19-22 (41)		89.3	13.6				
30		(CL-ML) Sandy silty CLAY, olive, very stiff, damp	SPT	4-8-8 (16)							
		(CL) Lean CLAY, dark olive gray, very stiff, moist	MC	5-9-19 (28)		92.1	29.4				
40		Gray brown, hard	SPT	13-19-27 (46)							
		(ML) Sandy SILT, olive, hard, moist	MC	14-38-29 (67)		107.3	16.6				
50		(CL-ML) Sandy silty CLAY, light brown, very stiff, moist	SPT	6-9-10 (19)							

Bottom of borehole at 51.5 feet.

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BORING NUMBER B-3

CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/29/22 **COMPLETED** 12/29/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879698, -118.210258
GROUNDWATER LEVELS Not encountered
BACKFILL Native cuttings

NOTES

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, medium soft, moist	AU								
		(ML) Silt with SAND, light olive brown, stiff, damp	SPT	3-3-4 (7)							
		Sandy SILT, olive, stiff, moist	MC	7-11-11 (22)		98.0	6.0				
10		(CL-ML) Sandy silty CLAY, dark olive gray, stiff, moist	SPT	3-4-6 (10)				36	25	11	
		Olive	MC	4-8-12 (20)		113.5	15.7				
		(ML) Sandy SILT with GRAVEL, olive, stiff, moist, *siltstone	SPT	4-5-4 (9)				28	21	7	
20		(CL) Lean CLAY, olive, stiff, moist	MC	12-10-9 (19)		101.3	10.3				
		(CH) Fat CLAY, greenish black, greenish black, stiff to very stiff, moist	SPT	2-3-6 (9)							
30		(ML) Sandy SILT, olive, very stiff, moist	MC	6-12-13 (25)		88.1	31.4				
		Hard	SPT	4-7-10 (17)				38	27	11	
40		(CL) Lean CLAY, grayish brown, very stiff, moist, *trace silt	MC	6-19-34 (53)		104.4	12.1				
		(SC-SM) Silty, clayey SAND, very dark greenish gray, fine to medium, dense, wet	SPT	3-5-12 (17)							
50			MC	28-31-50 (81)		105.3	18.7				

Bottom of borehole at 51.5 feet.



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CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/29/22 **COMPLETED** 12/29/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA
NOTES

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879719, -118.209679
GROUNDWATER LEVELS Encountered at 54' 2"
BACKFILL Native cuttings

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DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, medium soft, moist (CL-ML) Silty CLAY, light olive brown, very stiff, dry	AU	7-9-10 (19)		97.1	7.2				
		Light olive, damp	MC	12-8-9 (17)							
10		(ML) Sandy SILT, fine, light olive brown, stiff, damp	SPT	7-8-13 (21)		94.3	3.4				
		(CL-ML) Silty CLAY, olive, very stiff, damp	MC	5-9-11 (20)							
		Olive brown, stiff, moist	SPT	10-11-13 (24)		105.7	7.8				
20		(CL) Lean CLAY, olive brown, stiff, moist	MC	5-5-6 (11)							89.3
		(ML) Sandy SILT, fine, olive brown, very stiff, moist	SPT	18-19-20 (39)		103.4	4.8				
30		(CL) Lean CLAY, dark olive gray, stiff, moist	MC	3-4-5 (9)							92.7
		Olive, very stiff, damp	SPT	8-12-17 (29)		93.5	26.6				
40		(SM) Silty SAND, dark olive gray, dense	MC	11-8-11 (19)							46.5
		(ML) Sandy SILT, olive, hard, moist	SPT	16-35-44 (79)		108.1	17.3				
50		(SM) Silty SAND, dark greenish gray, dense, moist	MC	9-17-19 (36)							33.0
		(ML) Sandy SILT, greenish black, hard, wet	SPT	9-19-39 (58)		94.5	30.0				
60		(SP-SM) Poorly graded SAND with silt, dark greenish gray, dense, saturated	MC	7-13-26 (39)				NP	NP	NP	8.5
		Fine to coarse, greenish gray	SPT	5-20-20 (40)		117.3	15.0				
70		Dark greenish gray, medium dense	MC	8-8-13 (21)							9.0
		Fine to medium, very dark greenish gray, very dense, less silt	SPT	6-22-50 (72)		111.4	18.8				
Bottom of borehole at 76.5 feet.											

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BORING NUMBER P-2

CLIENT Compton Community College District **PROJECT NAME** New 3-Story Student Housing Facility - Compton College
PROJECT NUMBER 4230.2200060.0000 **PROJECT LOCATION** 1111 E Artesia Blvd, Compton, CA 90221
DATE STARTED 12/23/22 **COMPLETED** 12/23/22 **GROUND ELEVATION** 57 ft MSL **HOLE SIZE** 8 inches
DRILLING CONTRACTOR 2R **COORDINATES** 33.879726, -118.210124
DRILLING METHOD HSA **GROUNDWATER LEVELS** Not encountered
LOGGED BY AM **CHECKED BY** ER & DA **BACKFILL** Native cuttings
NOTES _____

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist	GB								
5		(CL) Lean CLAY, very dark grayish brown, stiff, damp Light brown, *trace silt	MC	4-7		93.0	29.8				
			SPT	3-5-5 (10)							
10		(ML) SILT, olive brown, stiff, damp	MC	6-10-9 (19)		93.1	13.7				

Bottom of borehole at 10.0 feet.

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 Telephone: (949) 537-3222

BORING NUMBER P-3

CLIENT Compton Community College District **PROJECT NAME** New 3-Story Student Housing Facility - Compton College
PROJECT NUMBER 4230.2200060.0000 **PROJECT LOCATION** 1111 E Artesia Blvd, Compton, CA 90221
DATE STARTED 12/29/22 **COMPLETED** 12/29/22 **GROUND ELEVATION** 57 ft MSL **HOLE SIZE** 8 inches
DRILLING CONTRACTOR 2R **COORDINATES** 33.879805, -118.209812
DRILLING METHOD HSA **GROUNDWATER LEVELS** Not encountered
LOGGED BY AM **CHECKED BY** ER & DA **BACKFILL** Native cuttings
NOTES _____

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist	Hand icon GB								
5		(CL) Lean CLAY with sand, olive brown, medium soft, damp	SPT	3-3-3 (6)				32	22	10	69.8
10		(CL-ML) Sandy silty CLAY, olive brown, very stiff, damp	MC	10-17-20 (37)		96.7	22.4				
		Medium soft to stiff	SPT	4-4-4 (8)							

Bottom of borehole at 10.0 feet.

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 Telephone: (949) 537-3222

BORING NUMBER P-4

CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/22/22 **COMPLETED** 12/22/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA
NOTES _____

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879674, -118.209534
GROUNDWATER LEVELS Not encountered
BACKFILL Native cuttings

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist	Hand icon GB								
5		(CL) Lean CLAY with sand, olive, medium soft, dry	SPT	3-4-5 (9)				32	22	10	72.3
10		(CL-ML) Sandy silty CLAY, light olive brown, very stiff, damp	MC	9-18-30 (48)		99.6	6.6				
10		Olive	SPT	8-9-13 (22)							

Bottom of borehole at 10.0 feet.



April 14, 2023
Project No. 4230.2200060.0000

APPENDIX B

Laboratory Testing

Appendix B-Laboratory Testing

ASTM D2488 – Classification

Soils were visually and texturally classified in accordance with the Unified Soil Classification System (USCS) in general accordance with ASTM D2488. Soil classifications are indicated on the logs of the exploratory borings in Appendix A.

ASTM D2937- In-Place Moisture and Density Tests

The moisture content and dry density of relatively undisturbed samples obtained from the exploratory borings were evaluated in general accordance with ASTM D2937. The test results are presented on the logs of the exploratory borings in Appendix A.

ASTM D422 - Gradation Analysis

Gradation analysis tests were performed on selected representative soil samples in general accordance with ASTM D422. These test results were utilized in evaluating the soil classifications in accordance with the USCS.

ASTM D1140 - Wash Sieve

The amount of fines passing the No. 200 sieve was evaluated by the wash sieve. The test procedure was in general accordance with ASTM D1140. The results are presented in Table B-1.

Table B- 1
ASTM D1140 - Wash Sieve

Boring No.	Depth (feet)	Percent Passing #200
B-1	9.0	75.9
B-1	15.0	61.7
B-1	25.0	86.7
B-1	35.0	97.7
B-1	45.0	74.7
B-1	55.0	14.0
B-1	65.0	23.5
B-2	6.0	60.8
B-4	18.0	89.3
B-4	30.0	92.7
B-4	40.0	46.5
B-4	50.0	33.0
B-4	60.0	8.5
B-4	70.0	9.0
P-3	3.0	69.8
P-4	3.0	72.3

ASTM D1557 - Maximum Dry Density and Optimum Moisture Content

The maximum dry density and optimum moisture content of the material of selected bulk samples obtained from the exploratory borings were evaluated in general accordance with the latest version of ASTM D1557 and is shown in Table B-2.

Table B- 2
ASTM D1557 - Maximum Dry Density and Optimum Moisture Content

Boring No.	Depth (feet)	Maximum Dry Density (pcf)	Optimum Moisture Content (Percent)
B-1	0-3	120.4	12.3
B-3	5-10	114.9	13.6

ASTM D4318 - Atterberg Limit

Tests were performed on selected representative fine-grained soil samples to evaluate the liquid limit, plastic limit, and plasticity index in general accordance with ASTM D4318. These test results were utilized to evaluate the soil classification in accordance with the Unified Soil Classification System (USCS). The test results and classifications are shown in Table B-3.

Table B- 3
ASTM D4318 - Atterberg Limit

Boring No.	Depth (feet)	Atterberg Limits		
		Liquid Limit	Plastic Limit	Plasticity Index
B-1	9.0	34	25	9
B-1	25.0	39	22	17
B-1	45.0	29	24	5
B-1	65.0	NP	NP	NP
B-2	6.0	29	23	6
B-3	9.0	36	25	11
B-3	15.0	28	21	7
B-3	35.0	38	27	11
B-4	60.0	NP	NP	NP
B-3	3.0	32	22	10
B-4	3.0	32	22	10

ASTM D4829 - Expansion Index Test

The expansion index of a selected material was evaluated in general accordance with ASTM D4829. The specimen was molded under a specified compactive energy at approximately 50 percent saturation. The prepared 1-inch thick by 4-inch diameter specimen was loaded with a surcharge of 144 pounds per square foot and was inundated with tap water. Readings of volumetric swell were made for a period of 24 hours. The test results and classification are presented in Table B-4.

Table B-4
ASTM D4829 Expansion Index of Soils

Boring No.	Depth (feet)	EI value	Potential Expansion
B-1	0-3	28	Low
B-3	5-10	11	Very Low

ASTM D3080 - Direct Shear Tests

A direct shear test was performed on relatively undisturbed sample in general accordance with ASTM D3080 to evaluate the shear strength characteristics of the selected material. The sample was inundated during shearing to represent adverse field conditions. The results are shown in Table B-5.

Table B-5
ASTM D3080 Direct Shear Test Results

Boring No.	Depth (feet)	Remolded	Peak		Ultimate	
			C (psf)	Phi (deg)	C (psf)	Phi (deg)
B-1	6.0	NO	120.0	28	10.0	28
B-1	6.0	NO	120.0	32	130.0	31

ASTM D2435 - Consolidation Test

A Consolidation tests was performed on a selected driven soil sample in general accordance with the latest version of ASTM D2435. The sample was inundated during testing to represent adverse field conditions. The percent consolidation for each load cycle was recorded as a ratio of the amount of vertical compression to the original height of the sample.

Soil Corrosivity

Soil pH and resistivity tests were performed by **Project X** on a representative soil sample in general

accordance with the latest version of ASTM D4972 and ASTM G187, respectively.

The chloride content of the selected sample was evaluated in general accordance with the latest version of ASTM D4327.

The sulfate content of the selected samples was evaluated in general accordance with the latest version of ASTM D4327. The test results are presented in Table B-6.

Table B- 6
Corrosivity Test Results

Boring No.	Depth (ft)	Water Soluble Sulfate (ppm)	Water Soluble Chloride (ppm)	Minimum Resistivity (ohm-cm)	pH
B-1	0-3	38.5	28.1	2,881	8.8
B-3	5-10	76.3	11.5	5,427	7.6

CT301 - R-value

The resistance value, or R-value, for site soils was evaluated in general accordance with California Test CT301. The sample was prepared and evaluated for exudation pressure and expansion pressure. The equilibrium R-value is reported as the lesser or more conservative of the two calculated results. The test results are presented in Table B-7.

Table B- 7
R-Value Test Results

Boring No.	Depth (feet)	R-Value
B-1	0-3	39
B-3	5-10	48

SUMMARY OF LABORATORY RESULTS



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CLIENT Compton Community College District

PROJECT NAME New 3-Story Student Housing Facility - Compton College

PROJECT NUMBER 4230.2200060.0000

PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221

Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Classification	Water Content (%)	Dry Density (pcf)
B-1	6.0						CL	26.2	94.1
B-1	9.0	34	25	9	<4.75	75.9	ML		
B-1	12.0						CL	19.2	102.6
B-1	15.0				<4.75	61.7	CL-ML		
B-1	18.0						CL-ML	9.7	100.0
B-1	25.0	39	22	17	<4.75	86.7	CL		
B-1	30.0						ML	14.4	100.0
B-1	35.0				<4.75	97.7	CL		
B-1	40.0						ML	16.6	103.9
B-1	45.0	29	24	5	>4.75	74.7	ML		
B-1	50.0						SP-SM	19.1	103.1
B-1	55.0				<4.75	14.0	SM		
B-1	60.0						SP-SM	20.5	107.0
B-1	65.0	NP	NP	NP	>4.75	23.5	SM		
B-1	70.0						SP-SM	17.4	111.8
B-2	3.0						CL	18.0	101.5
B-2	6.0	29	23	6	>4.75	60.8	ML		
B-2	9.0						ML	6.6	97.5
B-2	15.0						ML	6.5	105.5
B-2	25.0						CL	13.6	89.3
B-2	35.0						CL	29.4	92.1
B-2	45.0						ML	16.6	107.3
B-3	6.0						ML	6.0	98.0
B-3	9.0	36	25	11			ML		
B-3	12.0						CL-ML	15.7	113.5
B-3	15.0	28	21	7			CL-ML		
B-3	18.0						ML	10.3	101.3
B-3	30.0						CH	31.4	88.1
B-3	35.0	38	27	11			ML		
B-3	40.0						ML	12.1	104.4
B-3	50.0						SC-SM	18.7	105.3
B-4	3.0						CL-ML	7.2	97.1
B-4	9.0						ML	3.4	94.3
B-4	15.0						CL-ML	7.8	105.7
B-4	18.0				>4.75	89.3	CL		
B-4	25.0						ML	4.8	103.4
B-4	30.0				>4.75	92.7	CL		
B-4	35.0						CL	26.6	93.5
B-4	40.0				<4.75	46.5	SM		
B-4	45.0						ML	17.3	108.1
B-4	50.0				<4.75	33.0	SM		
B-4	55.0						ML	30.0	94.5
B-4	60.0	NP	NP	NP	<4.75	8.5	SP-SM		

LAB SUMMARY - GINT STD US LAB.GDT - 1/30/23 14:05 - S:\PROJECTS\GEO\TECHNICAL\2022\4230.2200060.0000 COMPTON COLLEGE STUDENT HOUSING PROJECT\APPENDIX A - BORING LOGS\LOGS\4230.2200060.0000 COMPTON COLLEGE STUDENT HOUSING





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SUMMARY OF LABORATORY RESULTS

CLIENT Compton Community College District **PROJECT NAME** New 3-Story Student Housing Facility - Compton College
PROJECT NUMBER 4230.2200060.0000 **PROJECT LOCATION** 1111 E Artesia Blvd, Compton, CA 90221

Borehole	Depth	Liquid Limit	Plastic Limit	Plasticity Index	Maximum Size (mm)	%<#200 Sieve	Classification	Water Content (%)	Dry Density (pcf)
B-4	65.0						SP-SM	15.0	117.3
B-4	70.0				>4.75	9.0	SP-SM		
B-4	75.0						SP-SM	18.8	111.4
P-2	3.0						CL	29.8	93.0
P-2	8.5						ML	13.7	93.1
P-3	3.0	32	22	10	12.7	69.8	CL		
P-3	6.0						CL-ML	22.4	96.7
P-4	3.0	32	22	10	19	72.3	CL		
P-4	6.0						CL-ML	6.6	99.6

Boring No.	B-1	B-1	B-1	B-1	B-1	B-1	B-1	B-2
Sample No.								
Depth (ft.)	9	15	25	35	45	55	65	6
Sample Type	SPT	SPT	SPT	SPT	SPT	SPT	SPT	SPT
Visual Soil Classification	Olive Brown Silt with Sand (ML)	Olive Brown Sandy Silty Clay (CL-ML)	Dark Olive Brown Lean Clay (CL)	Olive Gray Lean Clay (CL)	Olive Gray Silt with Sand (ML)	Very Dark Greenish Gray Silty Sand (SM)	Greenish Black Silty Sand (SM)	Olive Brown Sandy Silt (ML)
Total Sample Weight (Coarse Fraction)								
Total Sample Weight (g):	338.64	380.66	282.58	280.54	287.12	374.61	393.56	269.86
Plus #4 Weight (g):	0.0	2.9	0.0	0.0	0.2	0.0	6.4	0.0
Percent Retained Coarse Fraction (+ #4):	0.0	0.8	0.0	0.0	99.8	0.0	1.6	0.0
Weight Before Wash								
Weight of Moist Sample + Container (g):	800.62	582.50	507.81	514.91	517.11	611.35	642.26	464.72
Weight of Dry Sample + Container (g):	751.01	536.18	437.14	432.00	441.80	521.43	545.51	423.11
Weight of Container (g):	412.37	155.52	154.56	151.46	154.68	146.82	151.95	153.25
Moisture Content (%):	14.6	12.2	25.0	29.6	26.2	24.0	24.6	15.4
Container No.:	x	t3	t8	t4	t2	t2	t1	t7
Weight After Wash								
Dry Weight of Sample + Container (g):	494.11	301.14	192.21	157.96	227.18	469.01	452.97	259.11
Weight of Container (g):	412.37	155.52	154.56	151.46	154.68	146.82	151.95	153.25
Dry Weight of Sample (gm):	81.74	145.62	37.65	6.50	72.50	322.19	301.02	105.86
% Retained No. 200 Sieve	24.1	38.3	13.3	2.3	25.3	86.0	76.5	39.2
% Passing No. 200 Sieve	75.9	61.7	86.7	97.7	74.7	14.0	23.5	60.8
	PERCENT PASSING No. 200 SIEVE ASTM D 1140				Project Name: <u>New 3 Story Student Housing Facility - CC</u>			
					Project No.: <u>4230.2200060.0000</u>			
				Client: <u>CCCD</u>				
				Tested By: <u>SE</u> Date: <u>12/28/22</u>				

Boring No.	B-4	B-4	B-4	B-4	B-4	B-4		
Sample No.								
Depth (ft.)	18	30	40	50	60	70		
Sample Type	SPT	SPT	SPT	SPT	SPT	SPT		
Visual Soil Classification	Olive Brown Lean Clay (CL)	Dark Olive Gray Lean Clay (CL)	Dark Olive Gray Silty Sand (SM)	Dark Greenish Gray Silty Sand (SM)	Dark Greenish Gray Poorly Graded Sand with Silt (SP-SM)	Dark Greenish Gray Poorly Graded Sand with Silt (SP-SM)		
Total Sample Weight (Coarse Fraction)								
Total Sample Weight (g):	328.83	274.03	362.04	413.70	401.69	606.90		
Plus #4 Weight (g):	6.99	2.91	0.0	0.0	0.0	2.21		
Percent Retained Coarse Fraction (+ #4):	2.1	1.1	0.0	0.0	0.0	0.4		
Weight Before Wash								
Weight of Moist Sample + Container (g):	556.06	510.15	563.86	682.16	902.02	1218.11		
Weight of Dry Sample + Container (g):	483.64	429.66	513.51	568.30	814.02	1101.29		
Weight of Container (g):	154.81	155.63	151.47	154.60	412.33	494.39		
Moisture Content (%):	22.0	29.4	13.9	27.5	22.0	19.2		
Container No.:	t6	t3	t4	t8	x	gp		
Weight After Wash								
Dry Weight of Sample + Container (g):	190.01	175.61	345.01	431.61	780.03	1046.91		
Weight of Container (g):	154.81	155.63	151.47	154.60	412.33	494.39		
Dry Weight of Sample (gm):	35.20	19.98	193.54	277.01	367.70	552.52		
% Retained No. 200 Sieve	10.7	7.3	53.5	67.0	91.5	91.0		
% Passing No. 200 Sieve	89.3	92.7	46.5	33.0	8.5	9.0		
	PERCENT PASSING No. 200 SIEVE ASTM D 1140				Project Name: <u>New 3 Story Student Housing Facility - CC</u>			
					Project No.: <u>4230.2200060.0000</u>			
				Client: <u>CCCD</u>				
				Tested By: <u>SE</u>		Date: <u>12/28/22</u>		



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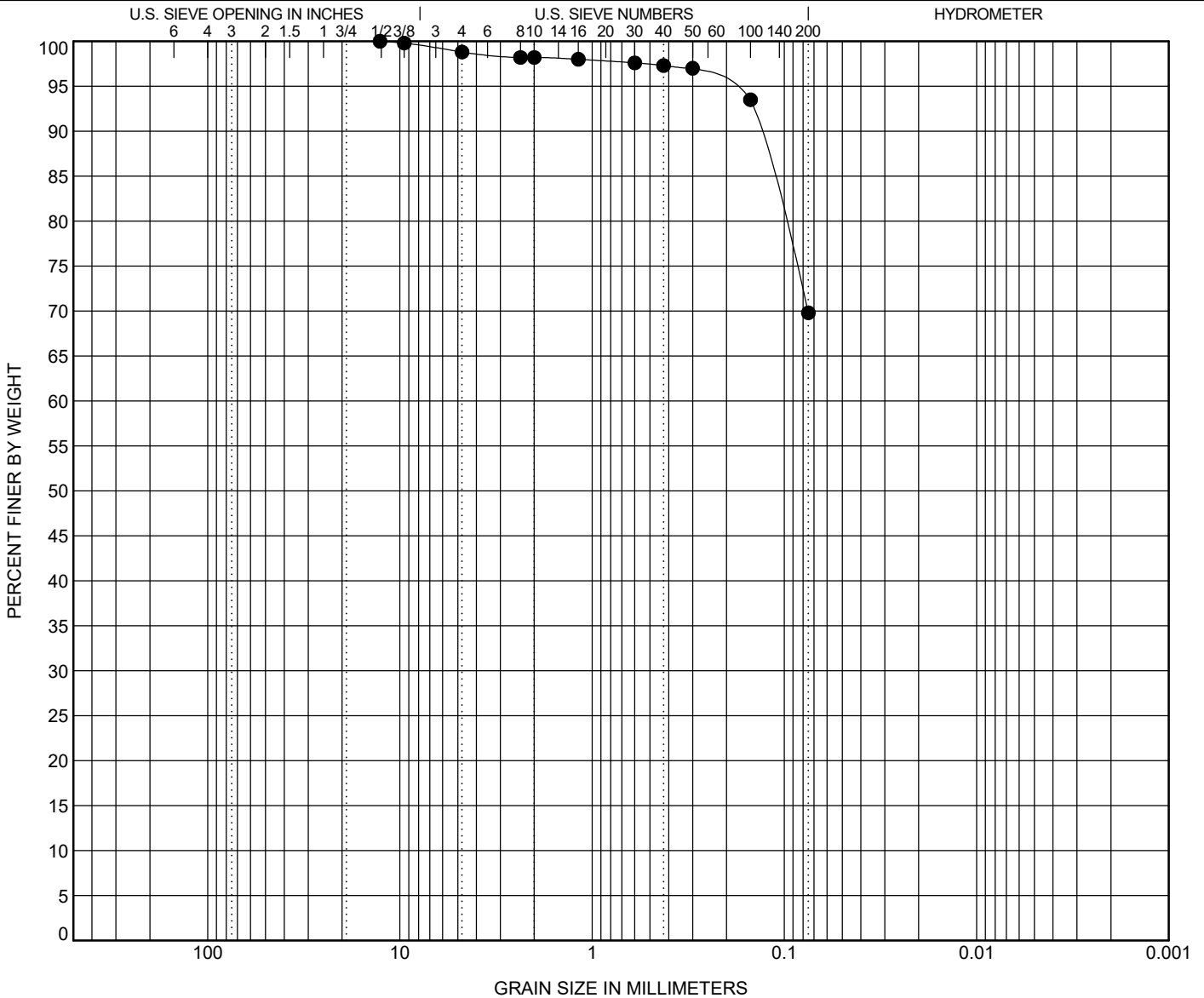
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PROJECT NUMBER 4230.2200060.0000

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COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● P-3	0.0-6.0	(CL) Lean CLAY with SAND, olive brown					32	22	10		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● P-3	0.0-6.0	12.7				1.2	29.0	69.8			

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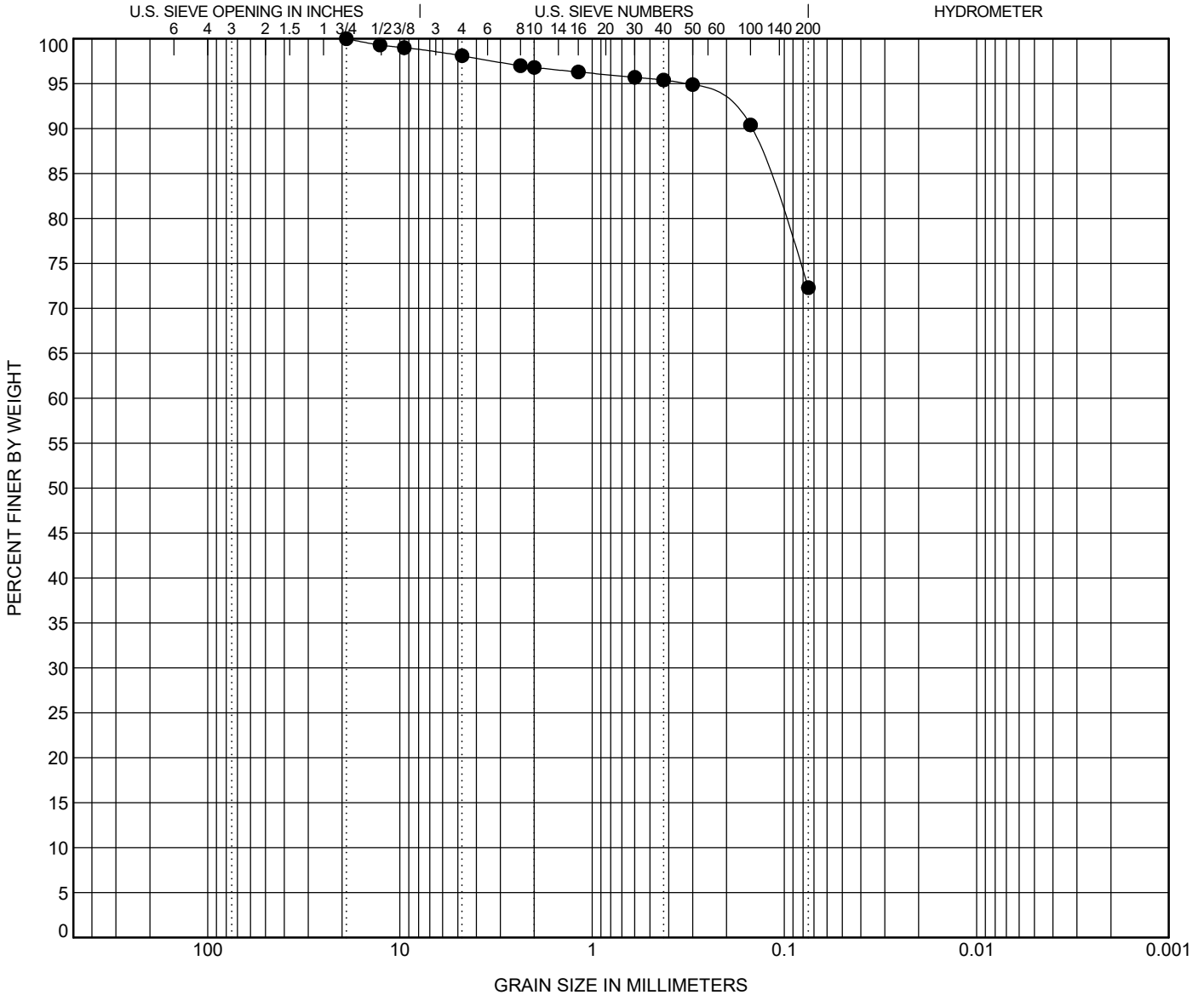
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CLIENT Compton Community College District

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PROJECT NUMBER 4230.2200060.0000

PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

BOREHOLE	DEPTH	Classification					LL	PL	PI	Cc	Cu
● P-4	0.0-5.0	(CL) Lean CLAY with SAND, olive					32	22	10		
BOREHOLE	DEPTH	D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
● P-4	0.0-5.0	19				1.9	25.8	72.3			

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MOISTURE-DENSITY RELATIONSHIP

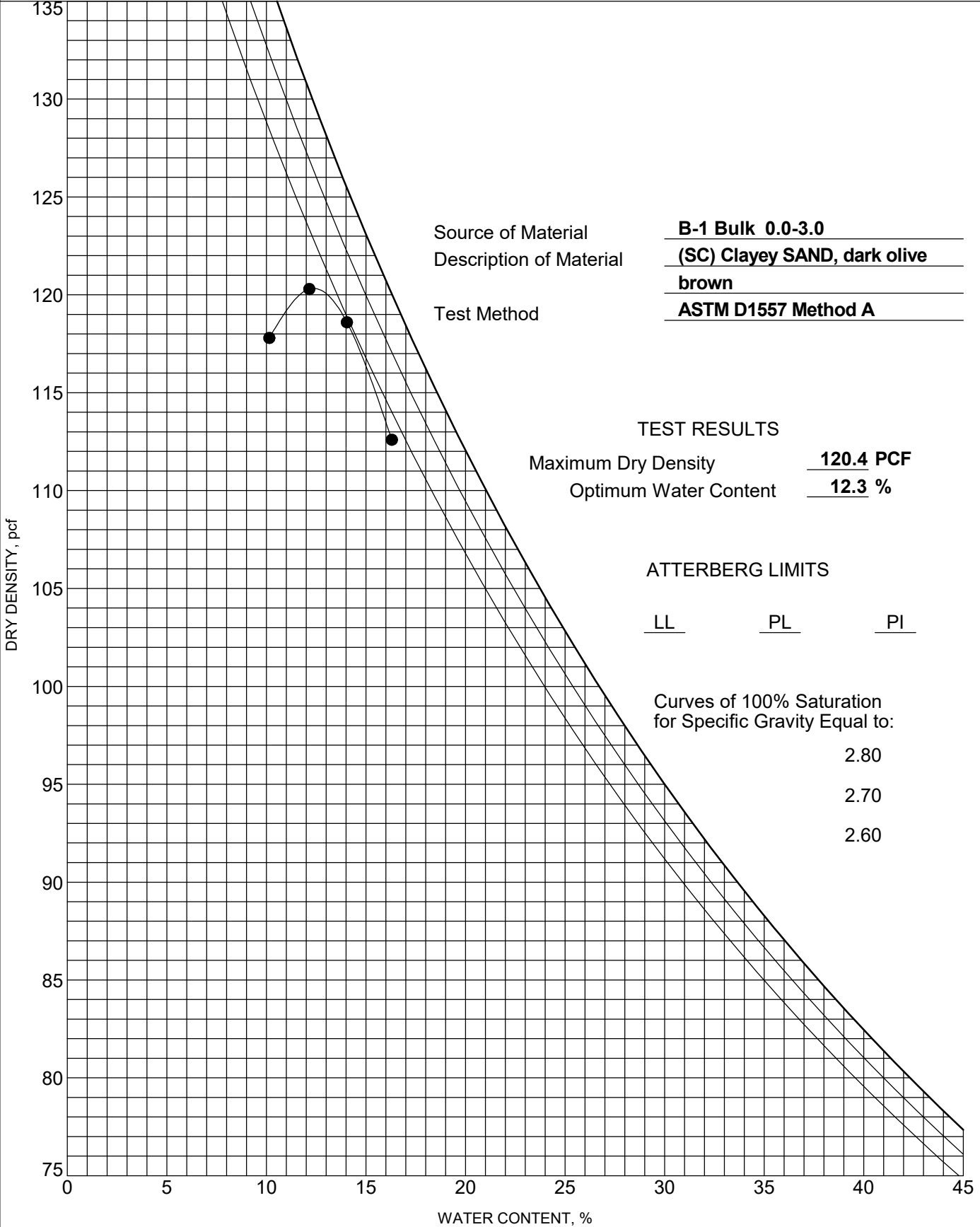
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Source of Material B-1 Bulk 0.0-3.0
 Description of Material (SC) Clayey SAND, dark olive brown
 Test Method ASTM D1557 Method A

TEST RESULTS
 Maximum Dry Density 120.4 PCF
 Optimum Water Content 12.3 %

ATTERBERG LIMITS
LL PL PI

Curves of 100% Saturation
 for Specific Gravity Equal to:
 2.80
 2.70
 2.60



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MOISTURE-DENSITY RELATIONSHIP

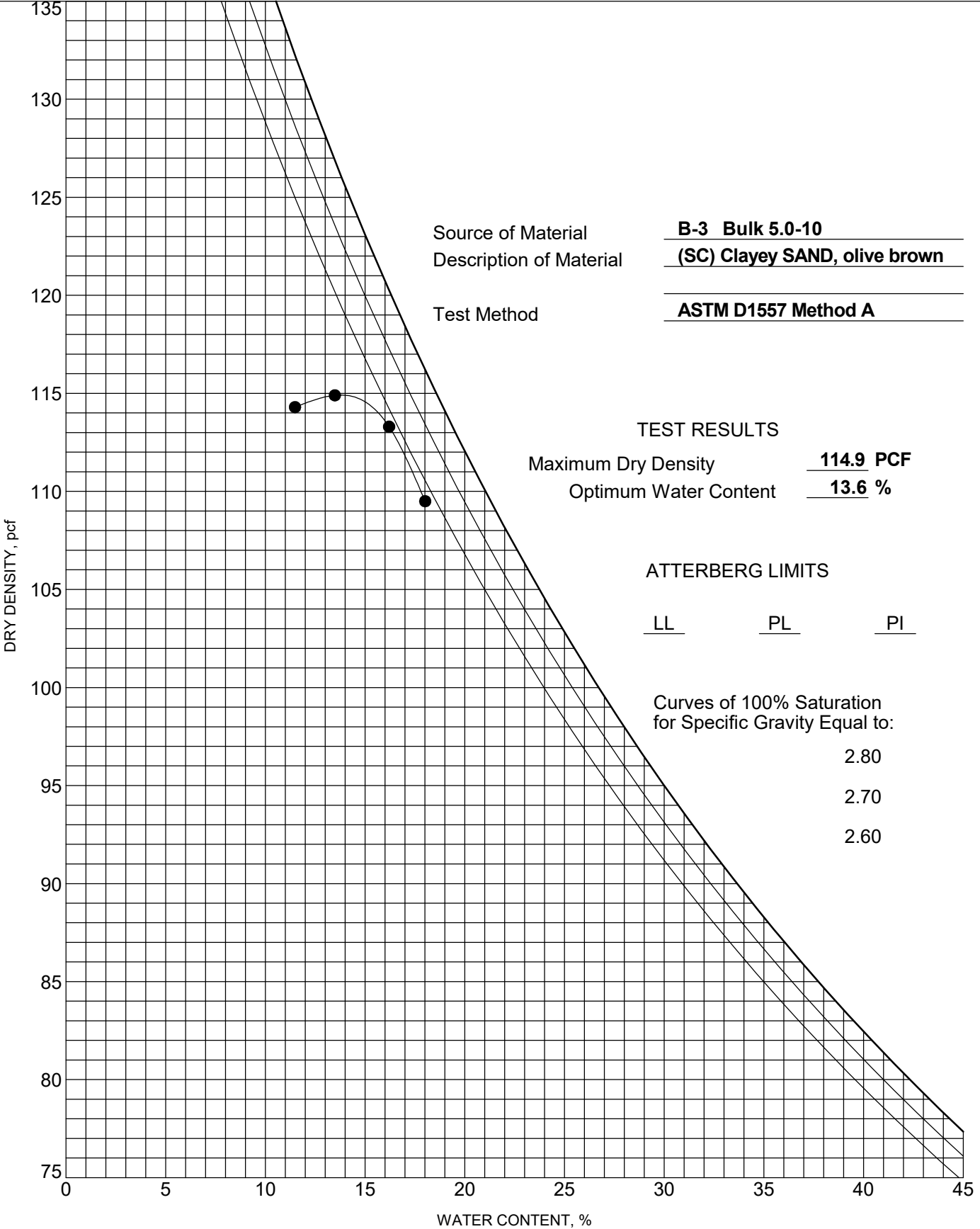
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PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221

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Source of Material B-3 Bulk 5.0-10
 Description of Material (SC) Clayey SAND, olive brown
 Test Method ASTM D1557 Method A

TEST RESULTS
 Maximum Dry Density 114.9 PCF
 Optimum Water Content 13.6 %

ATTERBERG LIMITS
LL PL PI

Curves of 100% Saturation
 for Specific Gravity Equal to:
 2.80
 2.70
 2.60

Expansion Index of Soils - D4829

Project Name:	New 3 Story Student Housing Facility - CC	Date Sampled:	12/22/2022
Project No.:	4230.2200060.0000	Sampled By:	AM
Boring No.:	B-1	Date Tested:	1/13/2023
Sample No.:	Bulk	Tested By:	SE
Depth (ft.):	0-3'		
Sample Prep.:	Dry		
Description:	Dark Olive Brown Clayey Sand (SC)		

Dry Weight of Soil + Cont. (g) (M_t)	2121.9
Dry Weight of Soil (g)	2121.9
Weight Soil Retained on #4 (M_{cf})	95.6
Percent Soil Retained on #4 (M_{cf})	4.5
Weight of Soil Passing (M_p)	2026.3
Sieve Percent Passing #4	95.5%

MOLDED SPECIMEN	Before Test	AFTER TEST
Specimen Diameter (in.)	4.00	
Specimen Height (in.) (H_i)	1.00	
Wt. Comp. Soil + Ring (g) (M_{sr})	775.85	
Wt. of Ring (g)	372.90	
Specific Gravity (Assumed)	2.65	
Ring Factor	0.3014	
Wet Wt. of Soil + Cont. (g)	112.64	
Dry Wt. of Soil + Cont. (g)	102.69	
Wt. of Container (g)	0.00	
Water Content (%) (w)	9.7	21.2
Wet Density (pcf)	121.5	
Dry Density (pcf)	110.7	
Degree of Saturation (%) [S meas]	52.0	

SPECIMEN INUNDATION in distilled water for the period of 24h or expansion rate < 0.0002 in./h

Date	Time	Pressure (psi)	Elapsed Time (min.)	Dial Reading
1/13/2023	0800	1	0	0.000
1/13/2023	0810	1	10	0.000
1/14/2023	0800	1	1440	0.0281

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Expansion Index of Soils - D4829

Project Name:	New 3 Story Student Housing Facility - CC	Date Sampled:	12/28/2022
Project No.:	4230.2200060.0000	Sampled By:	AM
Boring No.:	B-3	Date Tested:	1/13/2023
Sample No.:	Bulk	Tested By:	SE
Depth (ft.):	5-10'		
Sample Prep.:	Dry		
Description:	Olive Brown Clayey Sand (SC)		

Dry Weight of Soil + Cont. (g) (M_t)	1500.2
Dry Weight of Soil (g)	1500.2
Weight Soil Retained on #4 (M_{cf})	19.5
Percent Soil Retained on #4 (M_{cf})	1.3
Weight of Soil Passing (M_p)	1480.7
Sieve Percent Passing #4	98.7%

MOLDED SPECIMEN	Before Test	AFTER TEST
Specimen Diameter (in.)	4.00	
Specimen Height (in.) (H_i)	1.00	
Wt. Comp. Soil + Ring (g) (M_{sr})	762.29	
Wt. of Ring (g)	368.60	
Specific Gravity (Assumed)	2.65	
Ring Factor	0.3014	
Wet Wt. of Soil + Cont. (g)	114.64	
Dry Wt. of Soil + Cont. (g)	103.75	
Wt. of Container (g)	0.00	
Water Content (%) (w)	10.5	22.5
Wet Density (pcf)	118.7	
Dry Density (pcf)	107.4	
Degree of Saturation (%) [S meas]	51.6	

SPECIMEN INUNDATION in distilled water for the period of 24h or expansion rate < 0.0002 in./h

Date	Time	Pressure (psi)	Elapsed Time (min.)	Dial Reading
1/17/2023	0800	1	0	0.000
1/17/2023	0810	1	10	0.000
1/18/2023	0800	1	1440	0.0105

DIRECT SHEAR TEST



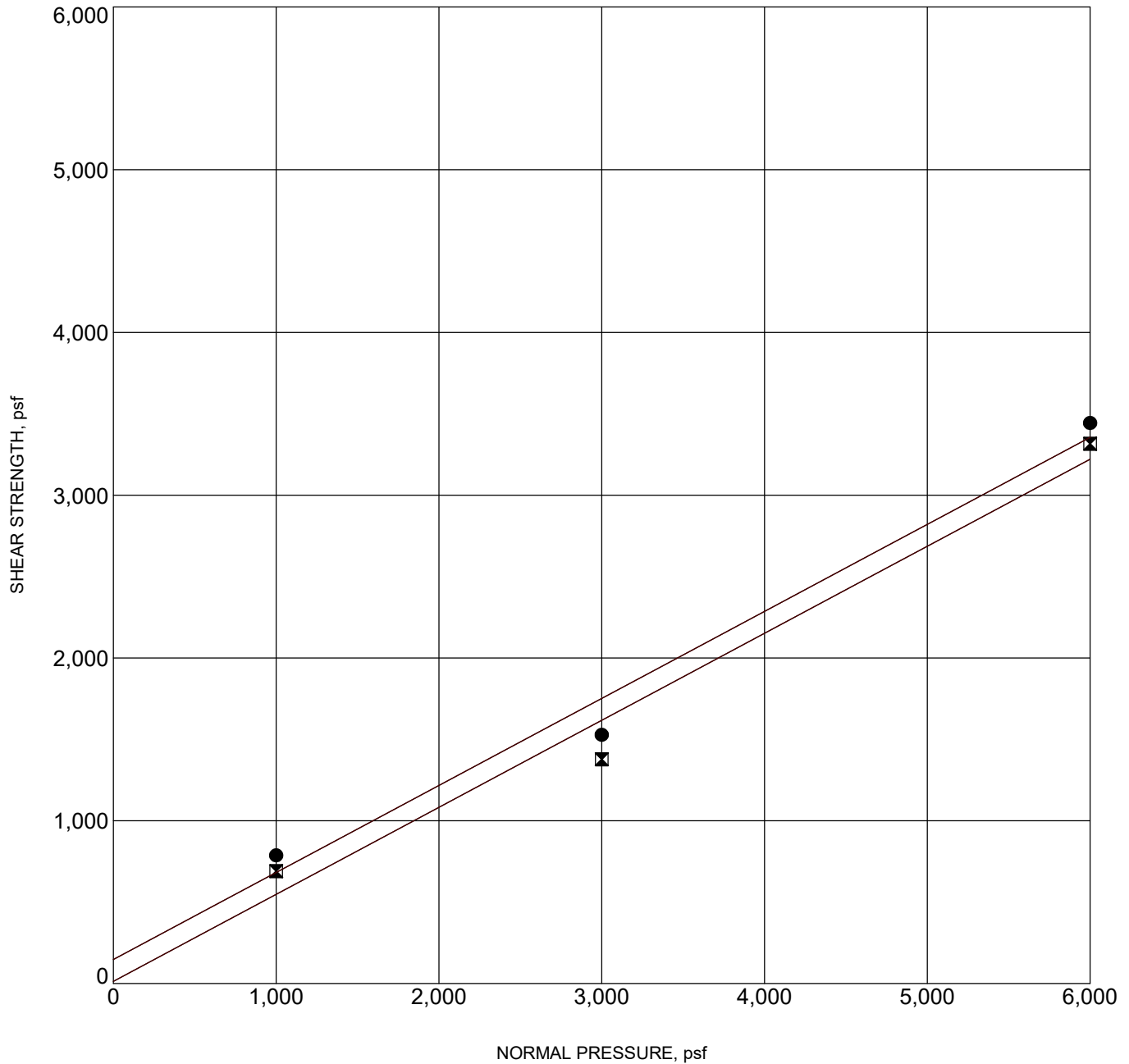
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CLIENT Compton Community College District

PROJECT NAME New 3-Story Student Housing Facility - Compton College

PROJECT NUMBER 4230.2200060.0000

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BOREHOLE	DEPTH	Classification	γ_d	MC%	c	ϕ
● B-1	6.0	(CL) Lean CLAY, olive brown	90.4	26.2	120.0	28
☒ B-1	6.0	(CL) Lean CLAY, olive brown	90.4	26.2	10.0	28

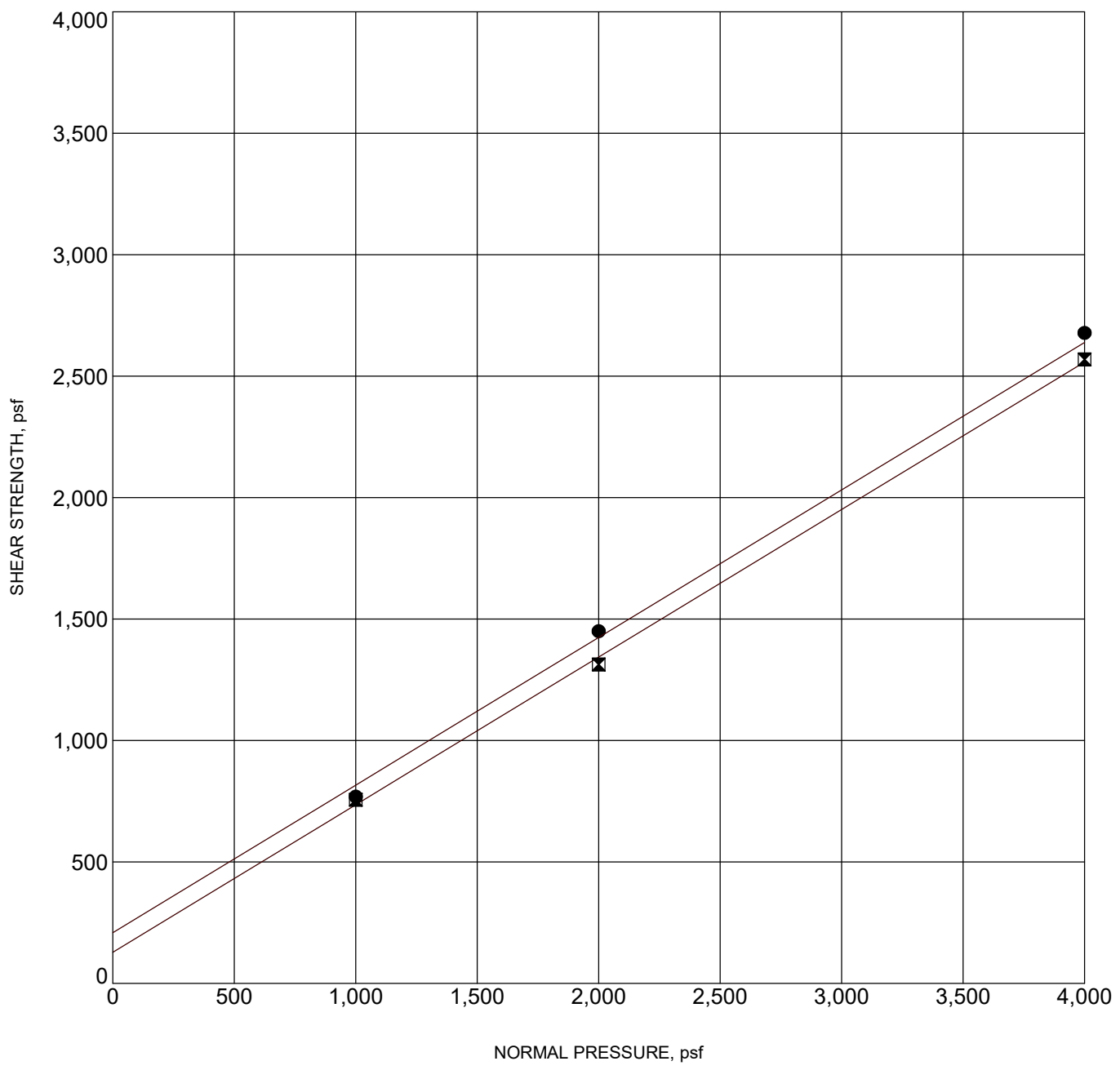
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DIRECT SHEAR TEST

CLIENT Compton Community College District **PROJECT NAME** New 3-Story Student Housing Facility - Compton College
PROJECT NUMBER 4230.2200060.0000 **PROJECT LOCATION** 1111 E Artesia Blvd, Compton, CA 90221



BOREHOLE	DEPTH	Classification	γ_d	MC%	c	ϕ
● B-3	6.0	(ML) Silt with SAND, light olive brown	91.5	7.4	150.0	32
☒ B-3	6.0	(ML) Silt with SAND, light olive brown	91.5	7.4	130.0	31

CONSOLIDATION TEST



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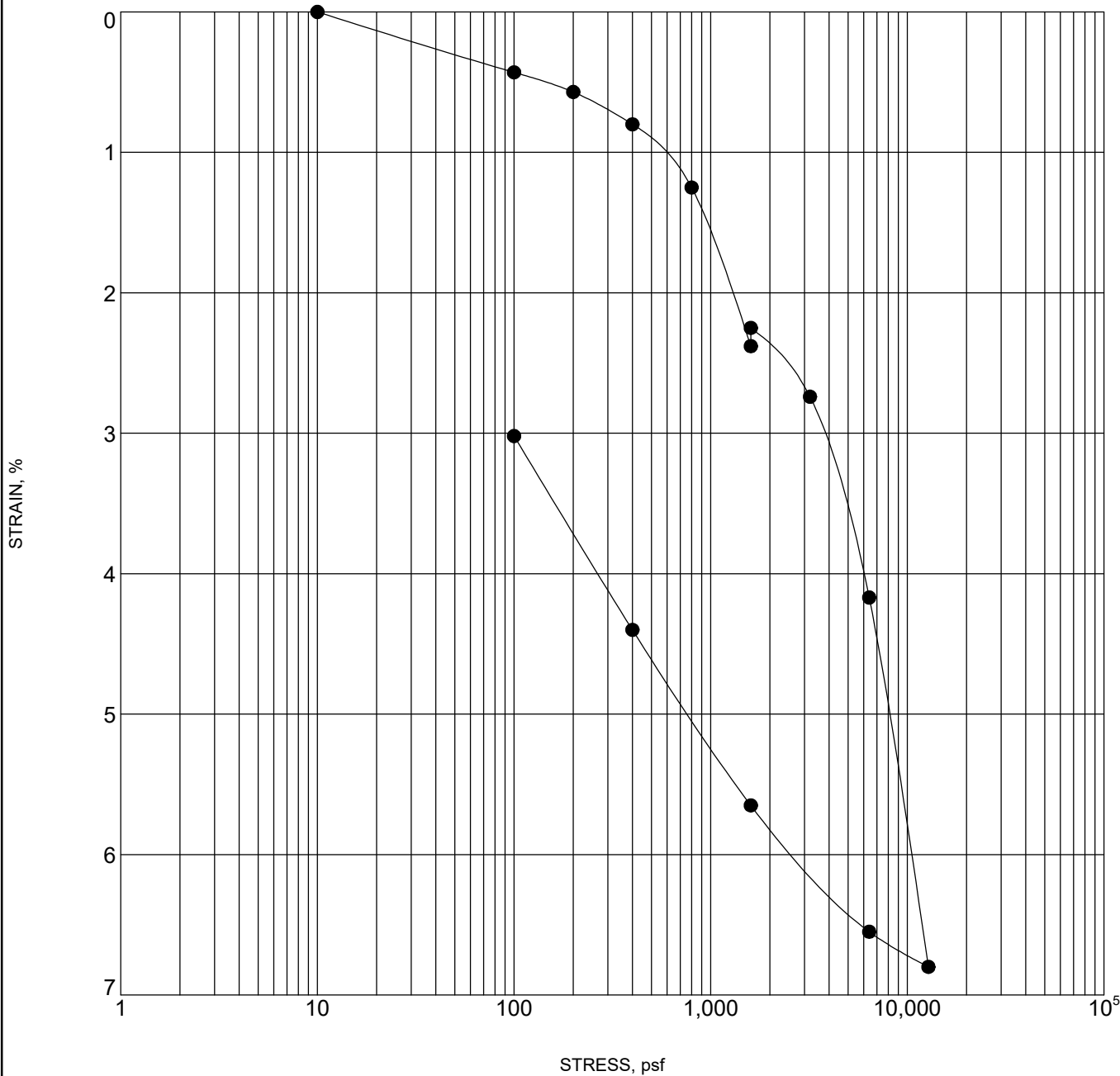
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PROJECT NUMBER 4230.2200060.0000

PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221

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BOREHOLE	DEPTH	Classification	γ_d	MC%
● B-2	3.0	(CL) Lean CLAY, dark olive brown	100.0	20.2

CONSOLIDATION TEST



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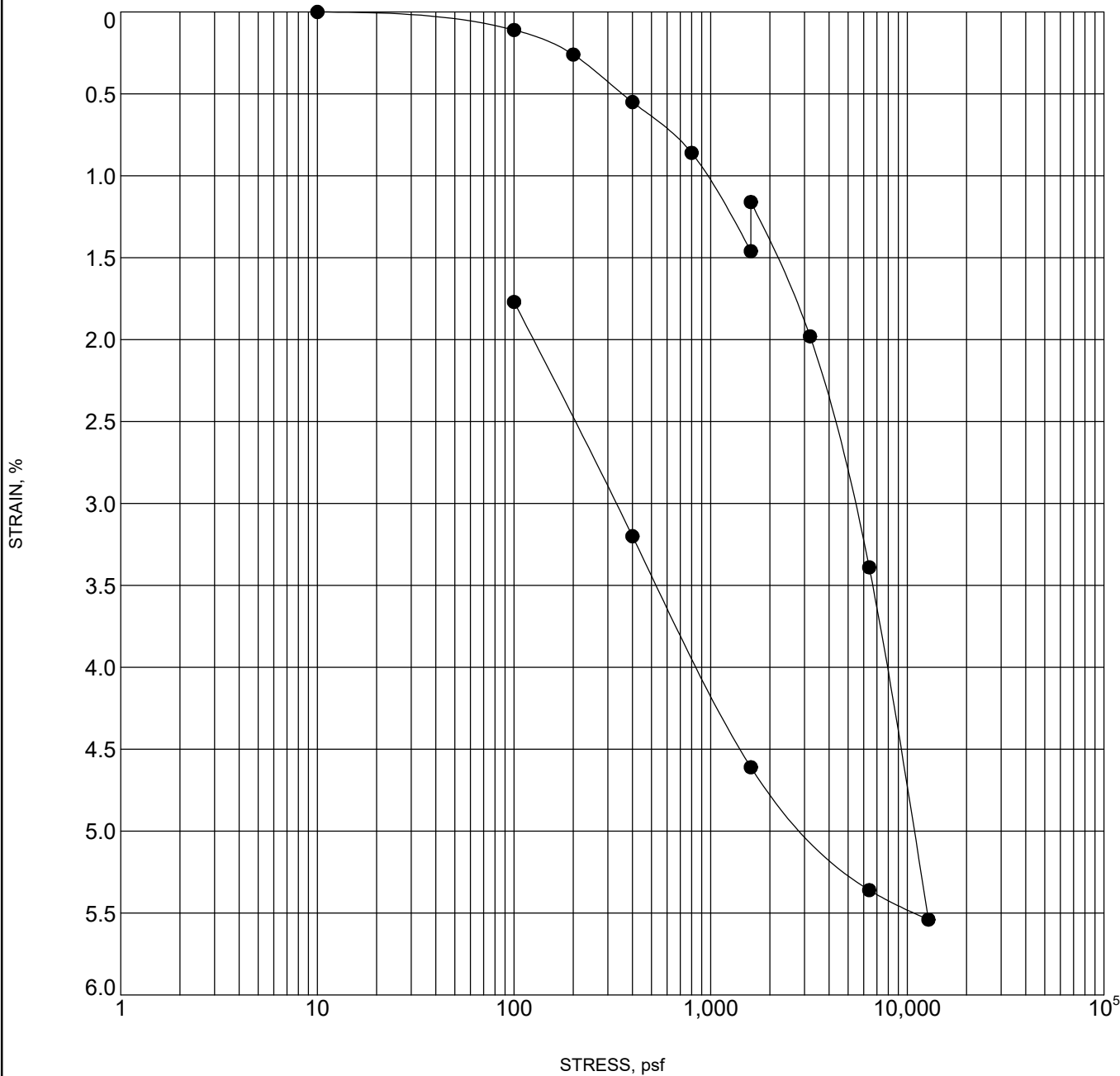
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BOREHOLE	DEPTH	Classification	γ_d	MC%
● B-4	3.0	(CL-ML) Silty CLAY, light olive brown	104.0	8.3



Soil Analysis Lab Results

Client: Universal Engineering
 Job Name: New 3-Story Student Housing Facility - Compton College
 Client Job Number: 4230.2200060.0000
 Project X Job Number: S230103H
 January 4, 2023

	Method	ASTM D4327		ASTM D4327		ASTM G187		ASTM G51
Bore# / Description	Depth	Sulfates SO ₄ ²⁻		Chlorides Cl ⁻		Resistivity As Rec'd Minimum		pH
	(ft)	(mg/kg)	(wt%)	(mg/kg)	(wt%)	(Ohm-cm)	(Ohm-cm)	
B - 1 Bulk	0-3	38.5	0.0039	28.1	0.0028	20,770	2,881	8.8

Cations and Anions, except Sulfide and Bicarbonate, tested with Ion Chromatography
 mg/kg = milligrams per kilogram (parts per million) of dry soil weight
 ND = 0 = Not Detected | NT = Not Tested | Unk = Unknown
 Chemical Analysis performed on 1:3 Soil-To-Water extract
 PPM = mg/kg (soil) = mg/L (Liquid)



Soil Analysis Lab Results

Client: Universal Engineering
 Job Name: New 3-Story Student Housing Facility - Compton College
 Client Job Number: 4230.2200060.0000
 Project X Job Number: S230105D
 January 6, 2023

	Method	ASTM D4327		ASTM D4327		ASTM G187		ASTM G51
Bore# / Description	Depth	Sulfates SO ₄ ²⁻		Chlorides Cl ⁻		Resistivity As Rec'd Minimum		pH
	(ft)	(mg/kg)	(wt%)	(mg/kg)	(wt%)	(Ohm-cm)	(Ohm-cm)	
B-3 BULK	5-10	76.3	0.0076	11.5	0.0012	14,740	5,427	7.6

Cations and Anions, except Sulfide and Bicarbonate, tested with Ion Chromatography
 mg/kg = milligrams per kilogram (parts per million) of dry soil weight
 ND = 0 = Not Detected | NT = Not Tested | Unk = Unknown
 Chemical Analysis performed on 1:3 Soil-To-Water extract
 PPM = mg/kg (soil) = mg/L (Liquid)

January 6, 2023

Mr. Sean Emami
Universal Engineering Sciences
16 Technology Drive, Suite 139
Irvine, California 92618

Project No. 48943

Attention: Sean Emami

Testing of the bulk soil sample delivered to our laboratory on 1/5/2023 has been completed.

Reference: 4230.2200060.0000

Project: New 4 Story Student Housing Facility, Compton College

Sample: B-1, Bulk @ 0'-3', 12/22/2022

Data sheets are attached for your use and file. Any untested portion of the sample will be retained for a period of 60 days prior to disposal. The opportunity to be of service is sincerely appreciated and should you have any questions, kindly call.

Very truly yours,



Steven R. Marvin
RCE 30659

SRM:tw
Enclosure



R - VALUE DATA SHEET

PROJECT No. 48943

DATE: 1/6/2022

BORING NO. B-1 @ 0'-3', Bulk, 12/22/2022

New 4 Story Student Housing Facility, Compton College


P.N. 4230.2200060.0000

SAMPLE DESCRIPTION: Brown Silty Sand

R-VALUE TESTING DATA ASTM D 2844			
	SPECIMEN ID		
	a	b	c
Mold ID Number	4	5	6
Water added, grams	78	58	51
Initial Test Water, %	14.2	12.2	11.5
Compact Gage Pressure, psi	70	250	345
Exudation Pressure, psi	242	444	666
Height Sample, Inches	2.67	2.58	2.56
Gross Weight Mold, grams	3090	3064	3068
Tare Weight Mold, grams	1949	1940	1951
Sample Wet Weight, grams	1141	1124	1117
Expansion, Inches x 10exp-4	32	88	94
Stability 2,000 lbs (160psi)	30 / 61	22 / 43	21 / 41
Turns Displacement	5.90	5.22	5.17
R-Value Uncorrected	41	57	58
R-Value Corrected	45	59	59
Dry Density, pcf	113.4	117.6	118.5

DESIGN CALCULATION DATA

Traffic Index	Assumed:	4.0	4.0	4.0
G. E. by Stability		0.56	0.42	0.42
G. E. by Expansion		1.07	2.93	3.13

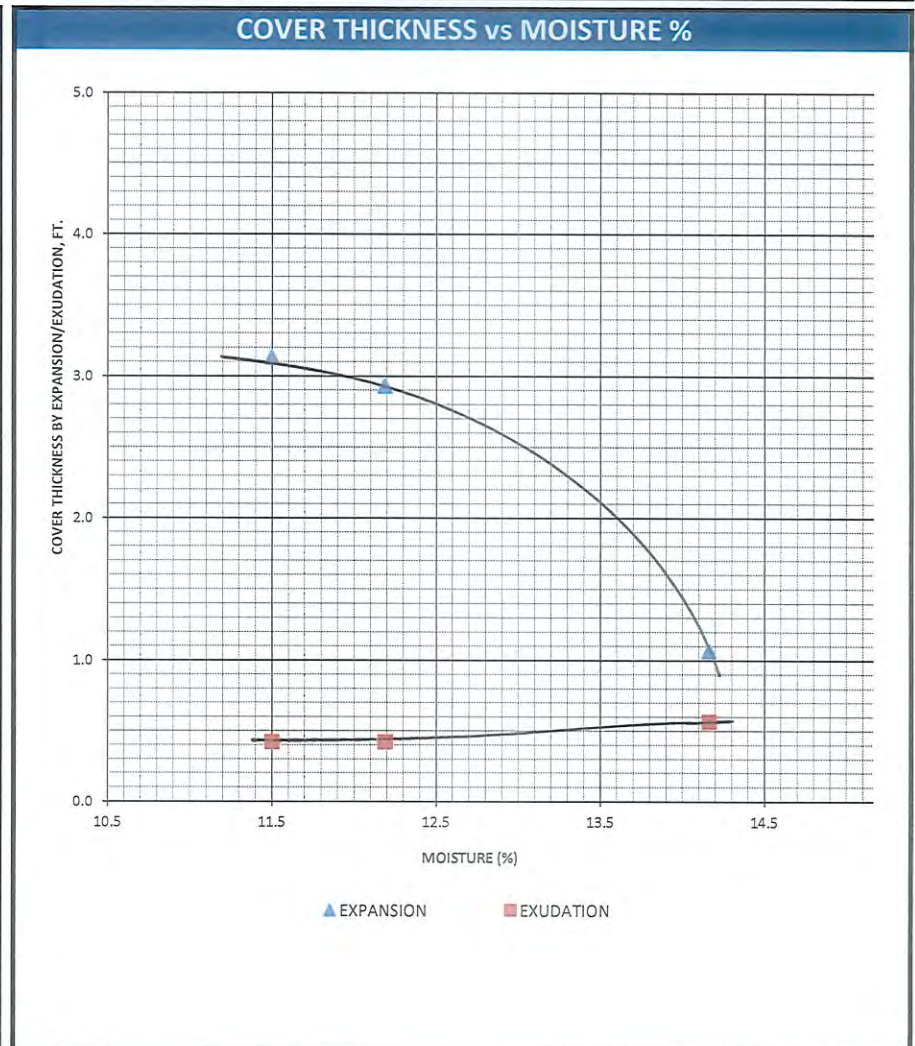
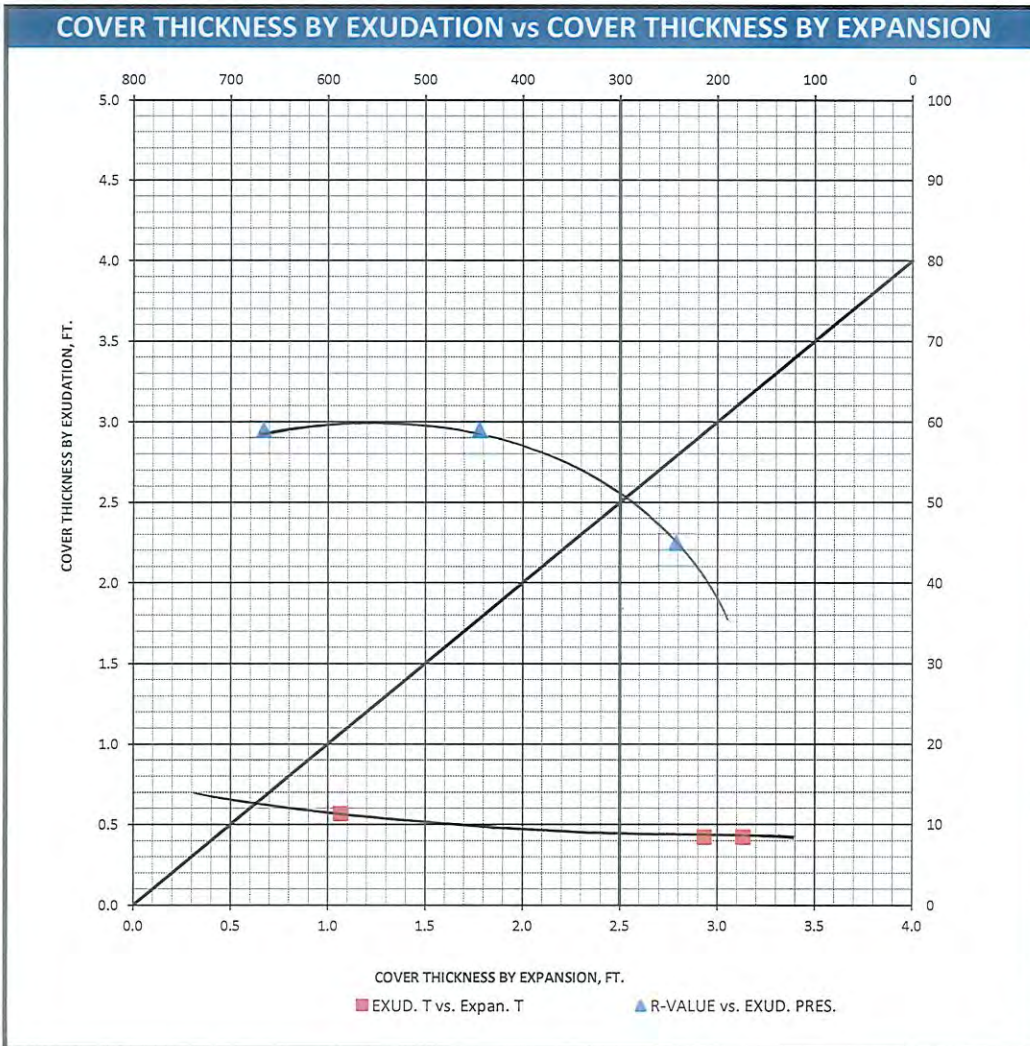
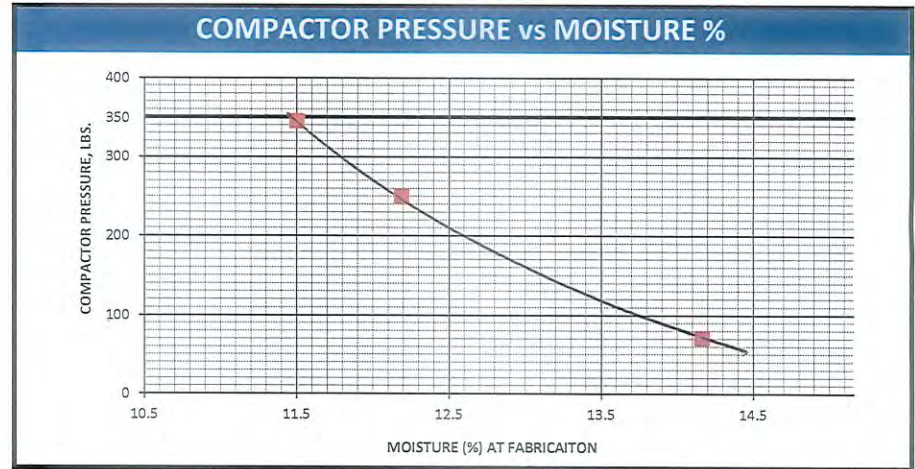
Equilibrium R-Value	39 by EXPANSION	Examined & Checked: <u>1 /6/ 23</u>
REMARKS:	Gf = <u>1.25</u>	
	<u>2.9% Retained on the</u> <u>3/4" Sieve.</u>	
		Steven R. Marvin, RCE 30659

The data above is based upon processing and testing samples as received from the field. Test procedures in accordance with latest revisions to ASTM D 2844.



R-VALUE GRAPHICAL PRESENTATION

PROJECT NO. 48943
 DATE: 1 /6/ 23 REMARKS: _____
 BORING NO. B-1 @ 0'-3', Bulk, 12/22/2022
New 4 Story Student Housing Facility, Compton College
P.N. 4230.2200060.0000



January 6, 2023

Mr. Sean Emami
Universal Engineering Sciences
16 Technology Drive, Suite 139
Irvine, California 92618

Project No. 48944

Attention: Sean Emami

Testing of the bulk soil sample delivered to our laboratory on 1/5/2023 has been completed.

Reference: 4230.2200060.0000

Project: New 4 Story Student Housing Facility, Compton College

Sample: B-3, Bulk @ 5'-10', 12/29/2022

Data sheets are attached for your use and file. Any untested portion of the sample will be retained for a period of 60 days prior to disposal. The opportunity to be of service is sincerely appreciated and should you have any questions, kindly call.

Very truly yours,



Steven R. Marvin
RCE 30659

SRM:tw
Enclosure



R - VALUE DATA SHEET

PROJECT No. 48944

DATE: 1/6/2022

BORING NO. B-3 @ 5'-10', Bulk, 12/29/2022

New 4 Story Student Housing Facility, Compton College

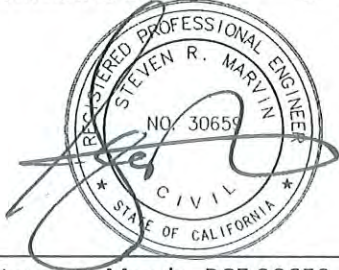
P.N. 4230.2200060.0000

SAMPLE DESCRIPTION: Brown Silty Sand

R-VALUE TESTING DATA ASTM D 2844			
	SPECIMEN ID		
	a	b	c
Mold ID Number	13	14	15
Water added, grams	41	21	14
Initial Test Water, %	15.7	13.6	12.8
Compact Gage Pressure, psi	110	225	315
Exudation Pressure, psi	181	446	599
Height Sample, Inches	2.59	2.52	2.49
Gross Weight Mold, grams	3011	3026	2991
Tare Weight Mold, grams	1935	1965	1940
Sample Wet Weight, grams	1076	1061	1051
Expansion, Inches x 10exp-4	26	37	45
Stability 2,000 lbs (160psi)	25 / 48	23 / 42	22 / 41
Turns Displacement	6.01	5.72	5.38
R-Value Uncorrected	49	55	57
R-Value Corrected	51	55	57
Dry Density, pcf	108.8	112.3	113.3

DESIGN CALCULATION DATA

Traffic Index	Assumed:	4.0	4.0	4.0
G.E. by Stability		0.50	0.46	0.44
G. E. by Expansion		0.87	1.23	1.50

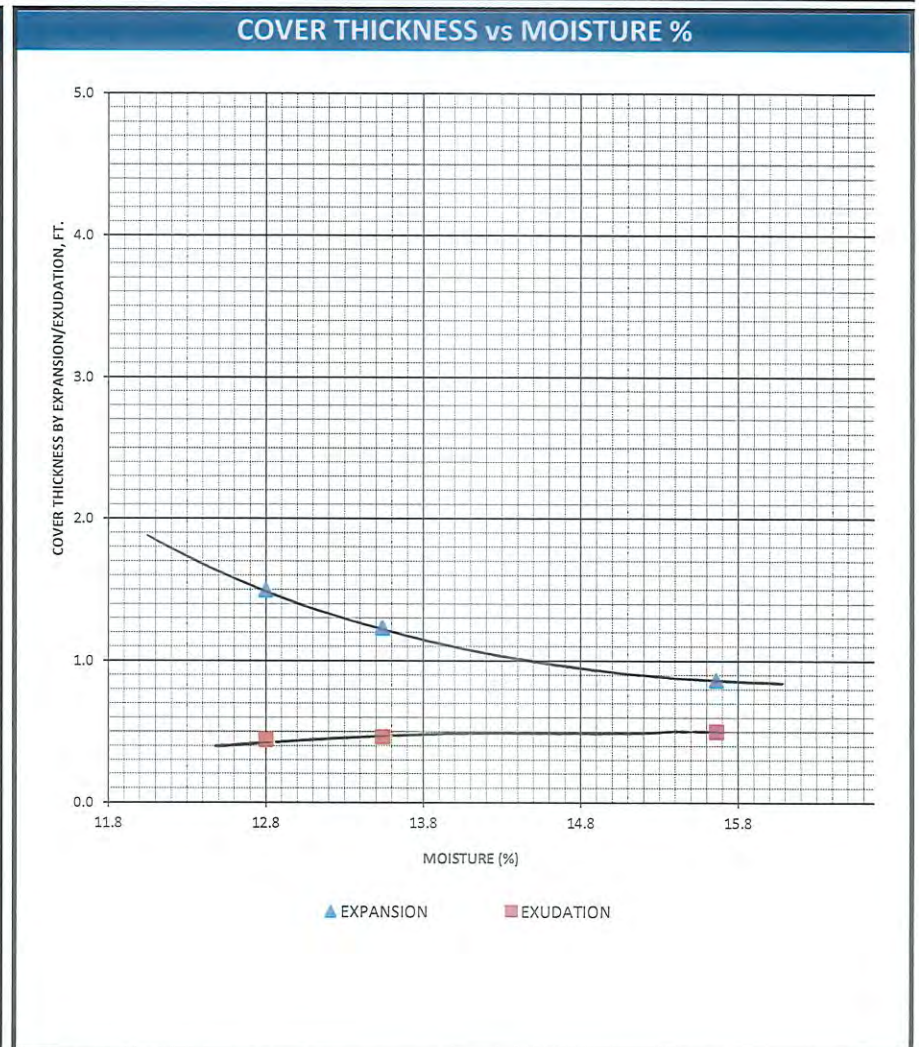
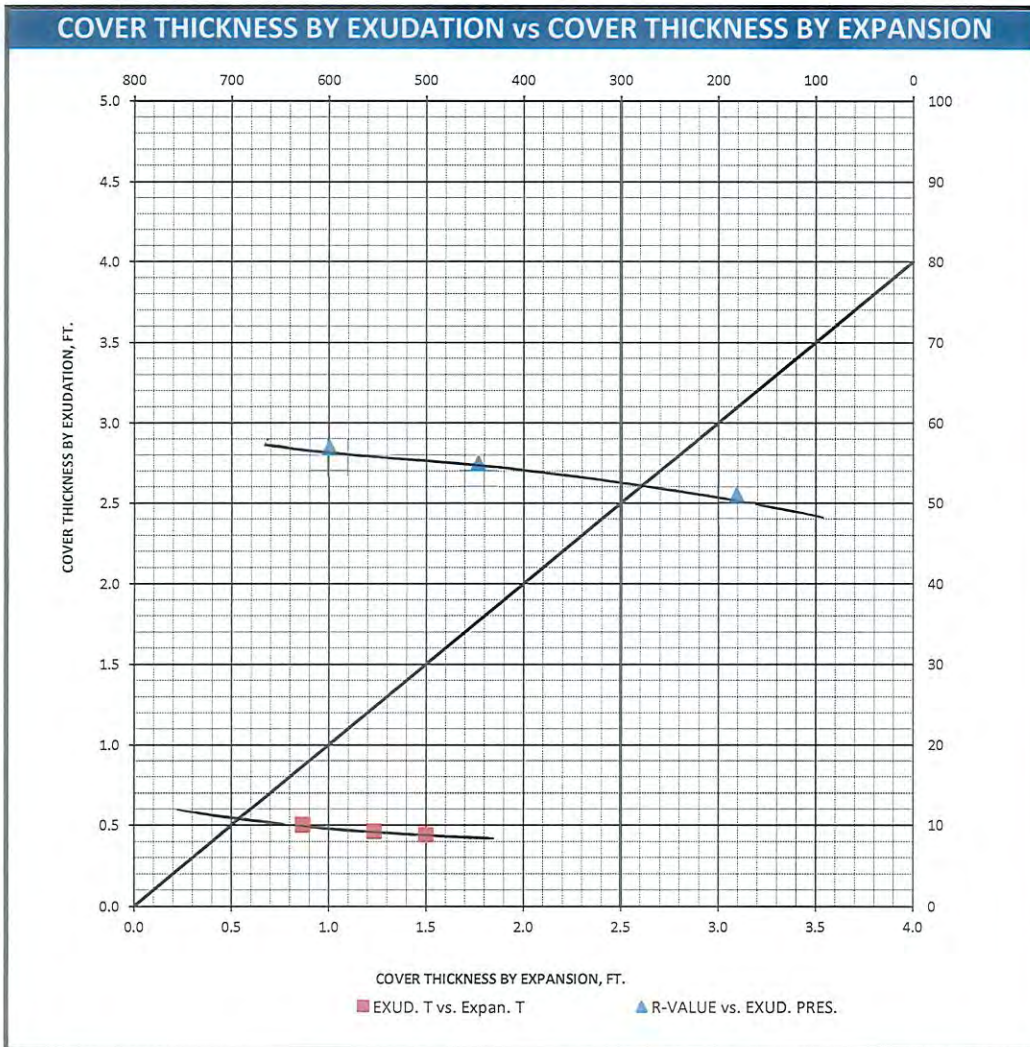
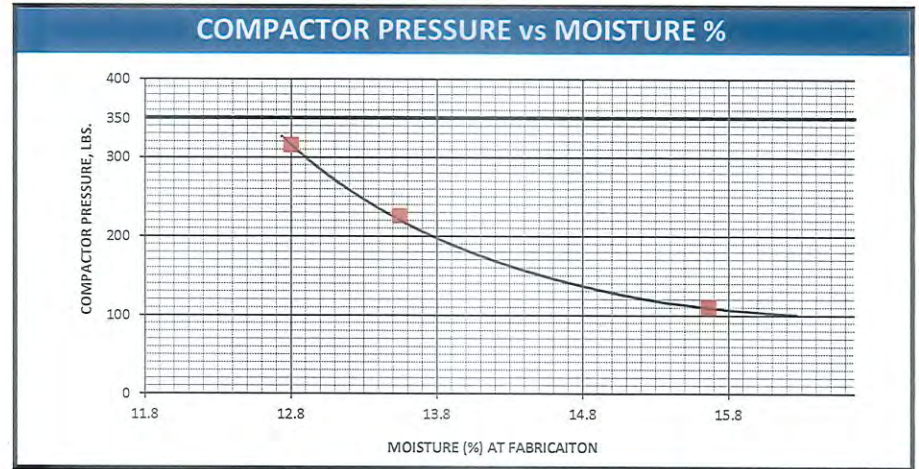
Equilibrium R-Value	48 by EXPANSION	Examined & Checked: <u>1 /6/ 23</u>
REMARKS:	Gf = <u>1.25</u>	 Steven R. Marvin, RCE 30659
	<u>0.0% Retained on the</u> <u>3/4" Sieve.</u>	

The data above is based upon processing and testing samples as received from the field. Test procedures in accordance with latest revisions to ASTM D 2844.



R-VALUE GRAPHICAL PRESENTATION

PROJECT NO. 48944
 DATE: 1 /6/ 23 REMARKS: _____
 BORING NO. B-3 @ 5'-10', Bulk, 12/29/2022
New 4 Story Student Housing Facility, Compton College
P.N. 4230.2200060.0000



APPENDIX C

Liquefaction Analysis

SUMMARY
OF
CONE PENETRATION TEST DATA

Project:

Compton Community College
1111 E. Artesia Blvd.
Compton, CA
January 4 & 17, 2023

Prepared for:

Ms. Bridget Sherman
Universal Engineering Services
16 Technology Drive, Ste 139
Irvine, CA 92618
Office (949) 537-3222

Prepared by:



KEHOE TESTING & ENGINEERING
5415 Industrial Drive
Huntington Beach, CA 92649-1518
Office (714) 901-7270 / Fax (714) 901-7289
www.kehoetesting.com

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- 1. INTRODUCTION**
- 2. SUMMARY OF FIELD WORK**
- 3. FIELD EQUIPMENT & PROCEDURES**
- 4. CONE PENETRATION TEST DATA & INTERPRETATION**

APPENDIX

- CPT Plots
- CPT Classification/Soil Behavior Chart
- Summary of Shear Wave Velocities
- CPT Data Files (sent via email)

SUMMARY OF CONE PENETRATION TEST DATA

1. INTRODUCTION

This report presents the results of a Cone Penetration Test (CPT) program carried out for the Compton Community College project located at 1111 E. Artesia Blvd. in Compton, California. The work was performed by Kehoe Testing & Engineering (KTE) on January 4 & 17, 2023. The scope of work was performed as directed by Universal Engineering Services personnel.

2. SUMMARY OF FIELD WORK

The fieldwork consisted of performing CPT soundings at three locations to determine the soil lithology. A summary is provided in **TABLE 2.1**.

LOCATION	DEPTH OF CPT (ft)	COMMENTS/NOTES:
CPT-1	75	
CPT-2	75	
CPT-3	30	
CPT-4	75	
CPT-5	75	
CPT-6	50	

TABLE 2.1 - Summary of CPT Soundings

3. FIELD EQUIPMENT & PROCEDURES

The CPT soundings were carried out by **KTE** using an integrated electronic cone system manufactured by Vertek. The CPT soundings were performed in accordance with ASTM standards (D5778). The cone penetrometers were pushed using a 30-ton CPT rig. The cone used during the program was a 15 cm² cone with a cone net area ratio of 0.83. The following parameters were recorded at approximately 2.5 cm depth intervals:

- Cone Resistance (qc)
- Sleeve Friction (fs)
- Dynamic Pore Pressure (u)
- Inclination
- Penetration Speed

At locations CPT-1, CPT-2, CPT-4 & CPT-5, shear wave measurements were obtained at various depths. The shear wave is generated using an air-actuated hammer, which is located inside the front jack of the CPT rig. The cone has a triaxial geophone, which recorded the shear wave signal generated by the air hammer.

The above parameters were recorded and viewed in real time using a laptop computer. Data is stored at the KTE office for up to 2 years for future analysis and reference. A complete set of baseline readings was taken prior to each sounding to determine temperature shifts and any zero load offsets. Monitoring base line readings ensures that the cone electronics are operating properly.

4. CONE PENETRATION TEST DATA & INTERPRETATION

The Cone Penetration Test data is presented in graphical form in the attached Appendix. These plots were generated using the CPeT-IT program. Penetration depths are referenced to ground surface. The soil behavior type on the CPT plots is derived from the attached CPT SBT plot (Robertson, "Interpretation of Cone Penetration Test...", 2009) and presents major soil lithologic changes. The stratigraphic interpretation is based on relationships between cone resistance (q_c), sleeve friction (f_s), and penetration pore pressure (u). The friction ratio (R_f), which is sleeve friction divided by cone resistance, is a calculated parameter that is used along with cone resistance to infer soil behavior type. Generally, cohesive soils (clays) have high friction ratios, low cone resistance and generate excess pore water pressures. Cohesionless soils (sands) have lower friction ratios, high cone bearing and generate little (or negative) excess pore water pressures.

The CPT data files have also been provided. These files can be imported in CPeT-IT (software by GeoLogismiki) and other programs to calculate various geotechnical parameters.

It should be noted that it is not always possible to clearly identify a soil type based on q_c , f_s and u . In these situations, experience, judgement and an assessment of the pore pressure data should be used to infer the soil behavior type.

If you have any questions regarding this information, please do not hesitate to call our office at (714) 901-7270.

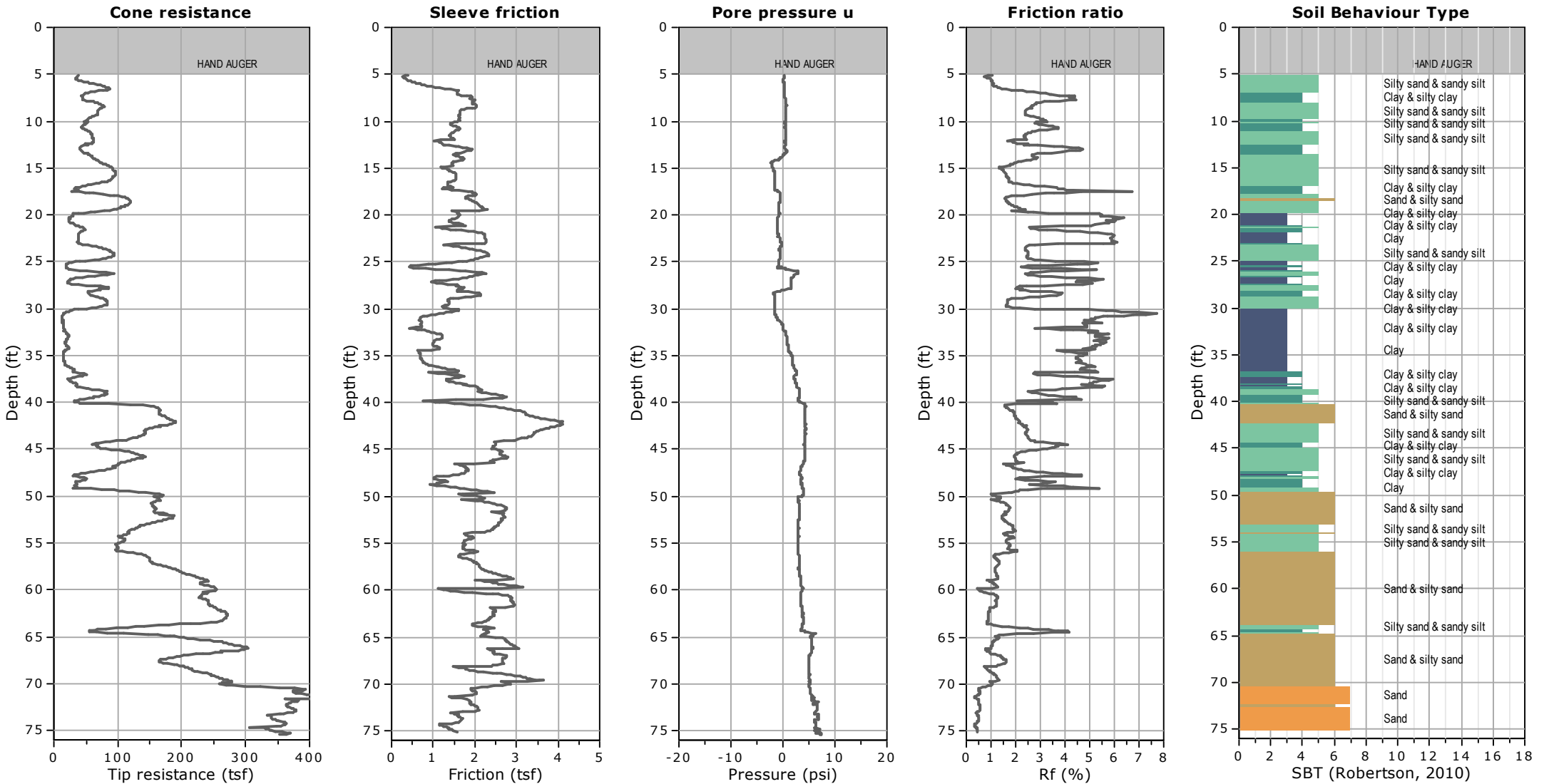
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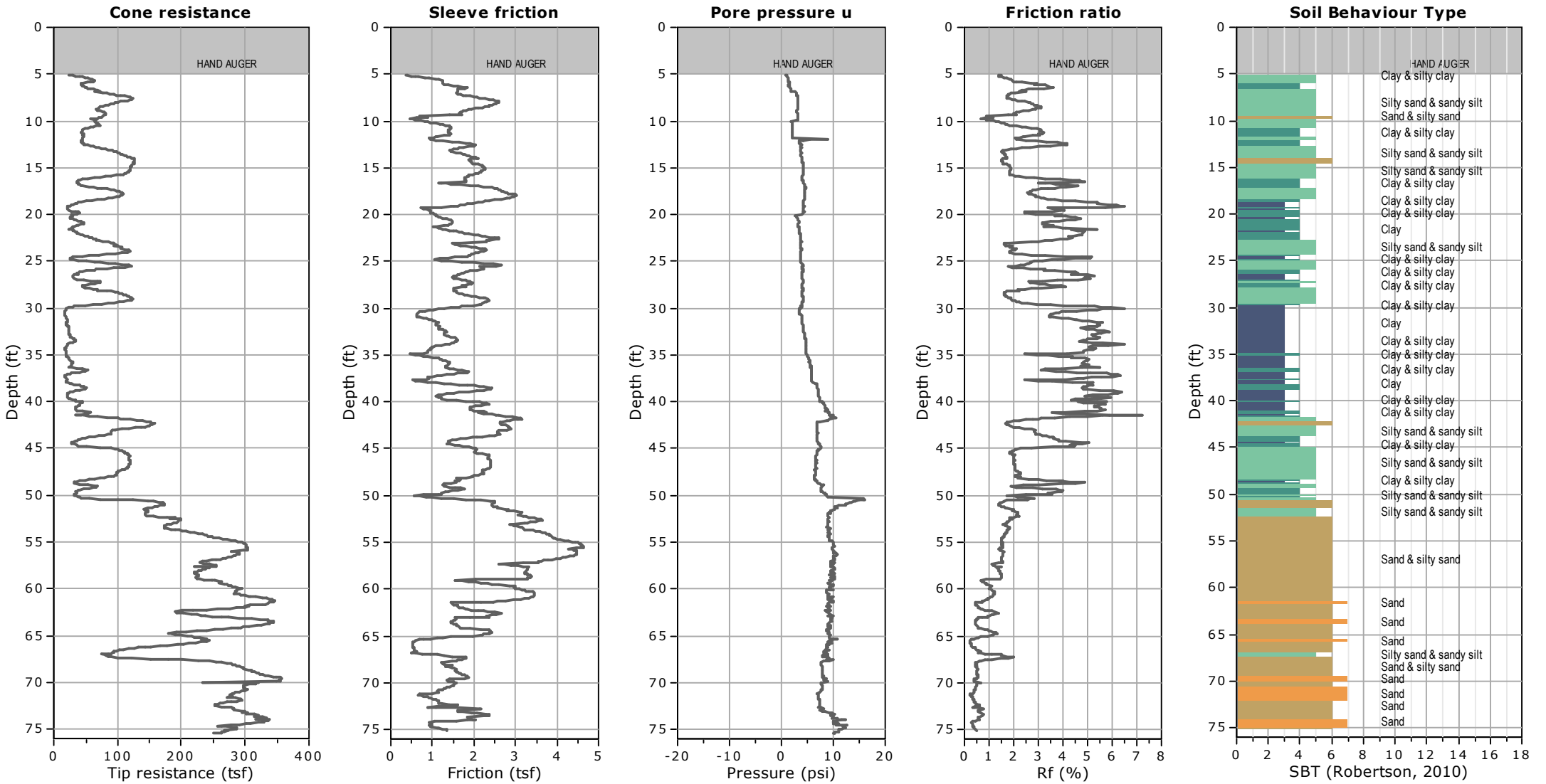
KEHOE TESTING & ENGINEERING

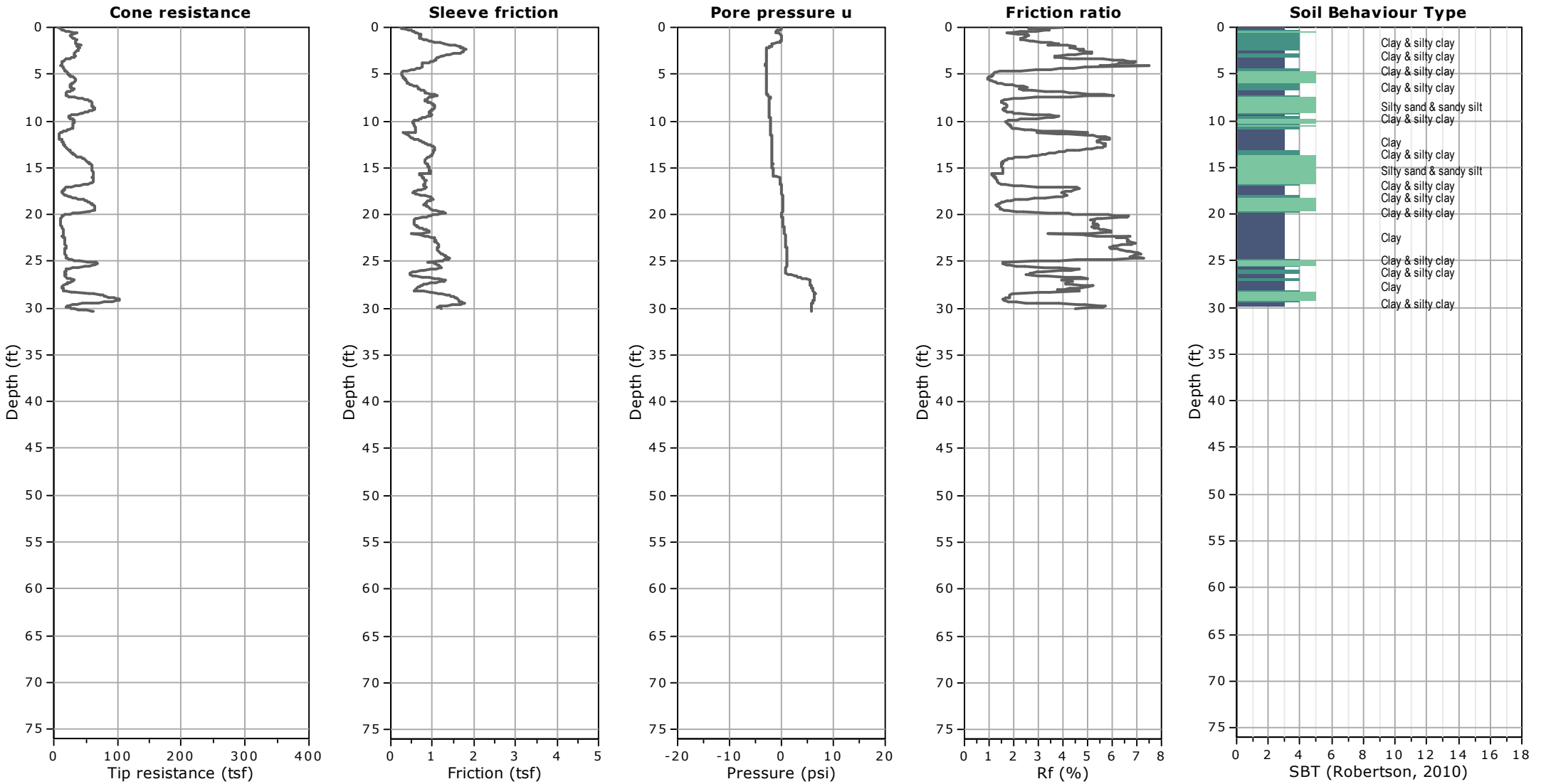


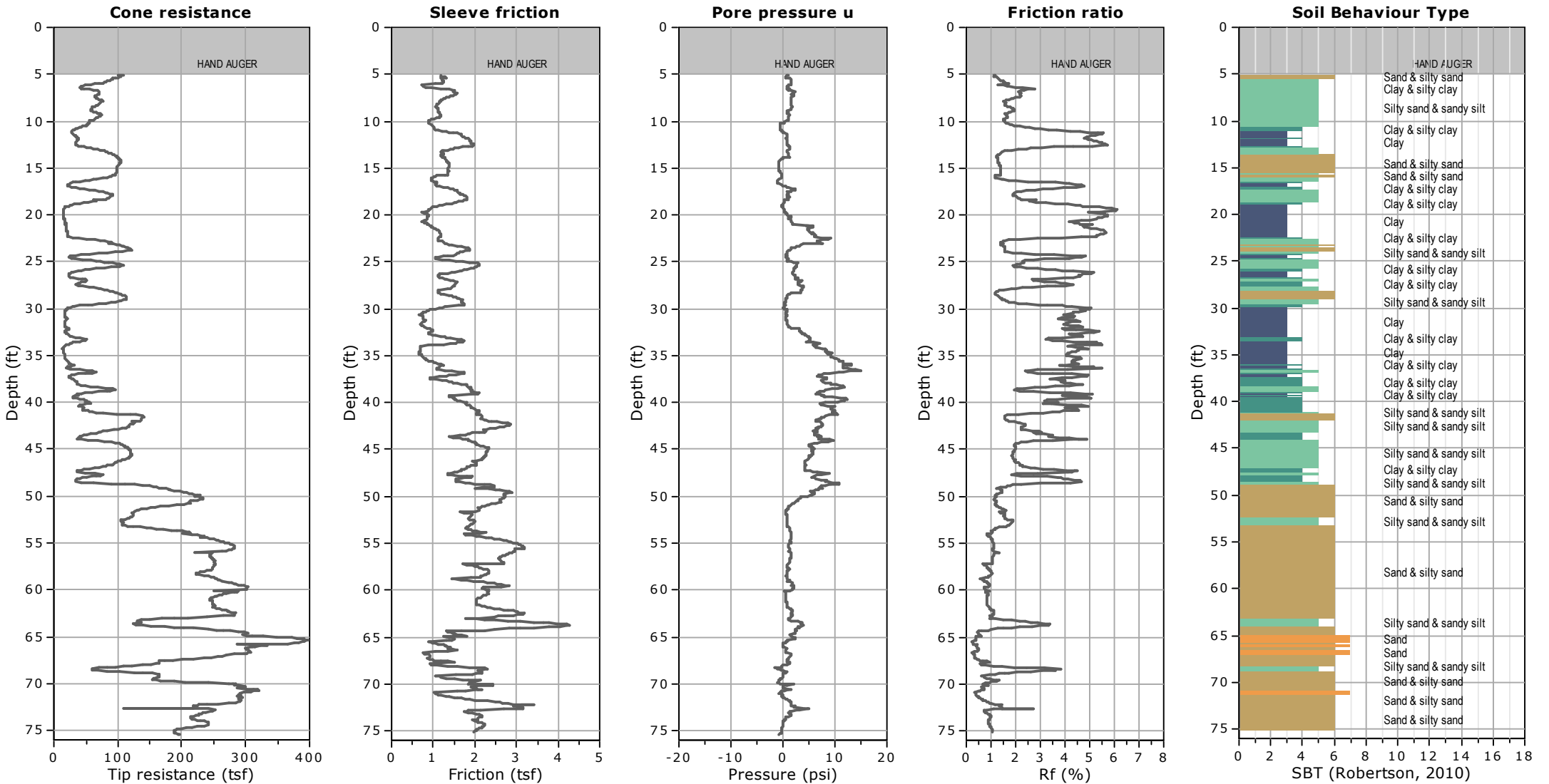
Steven P. Kehoe
President

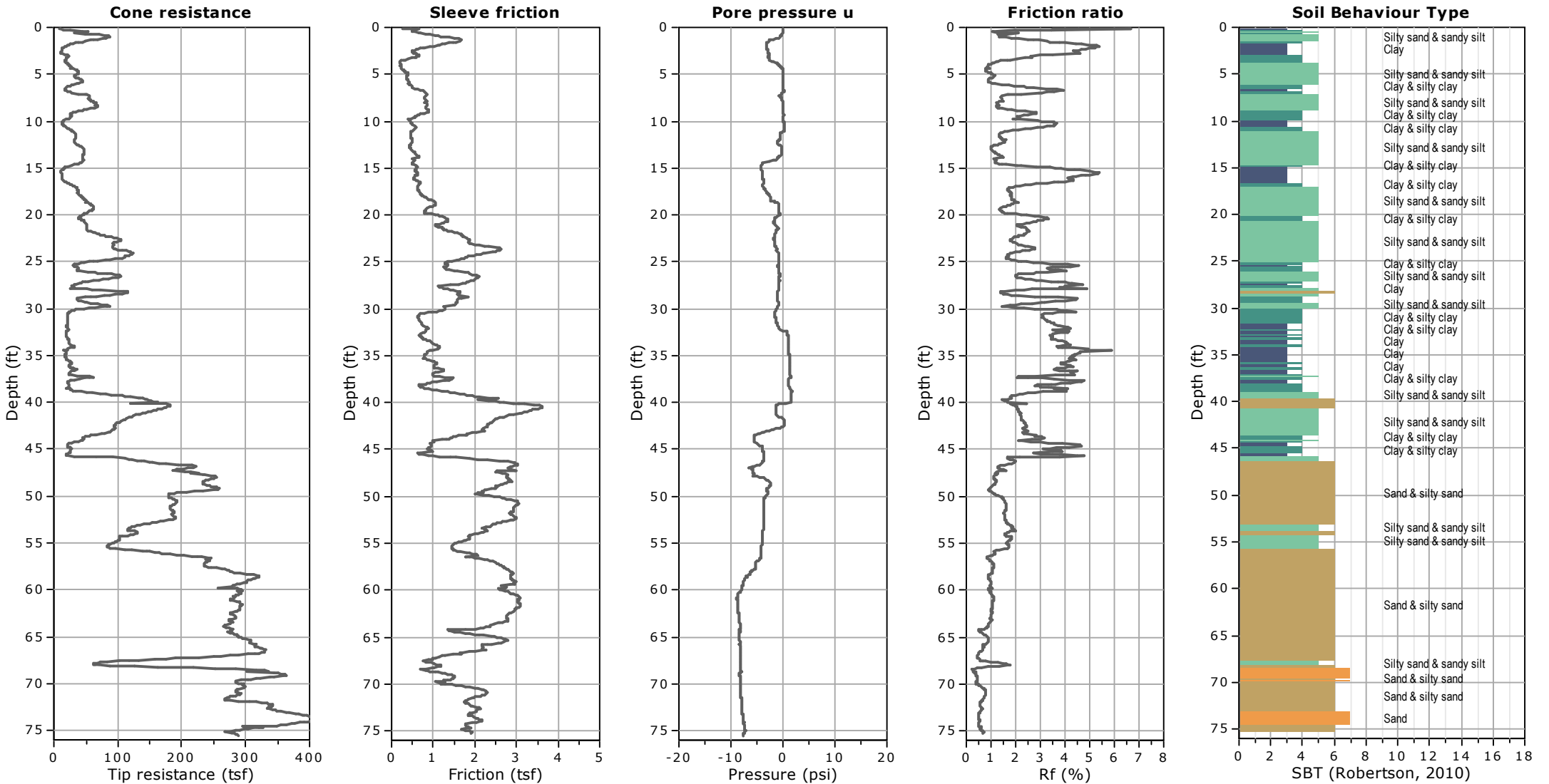
APPENDIX

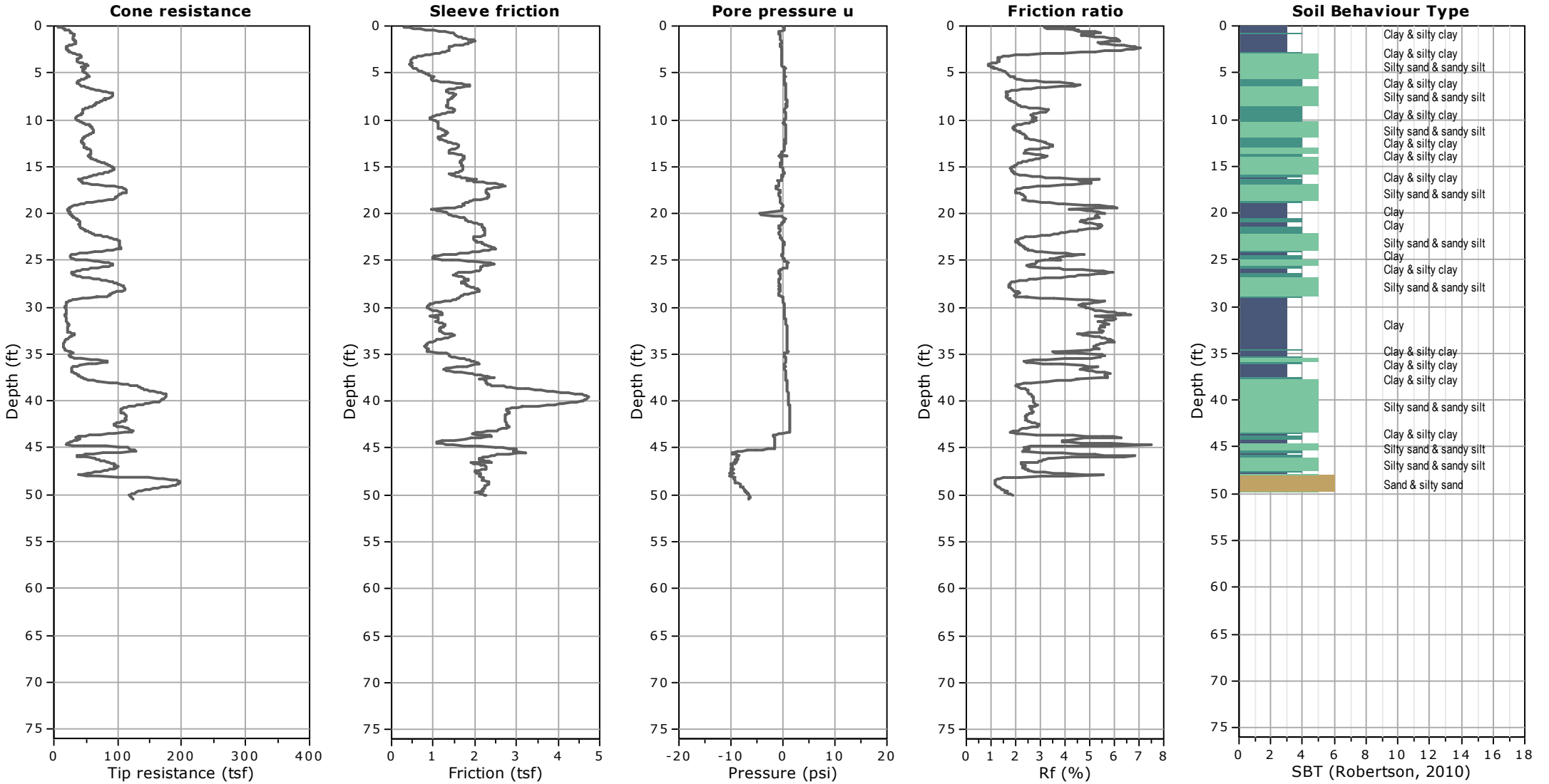


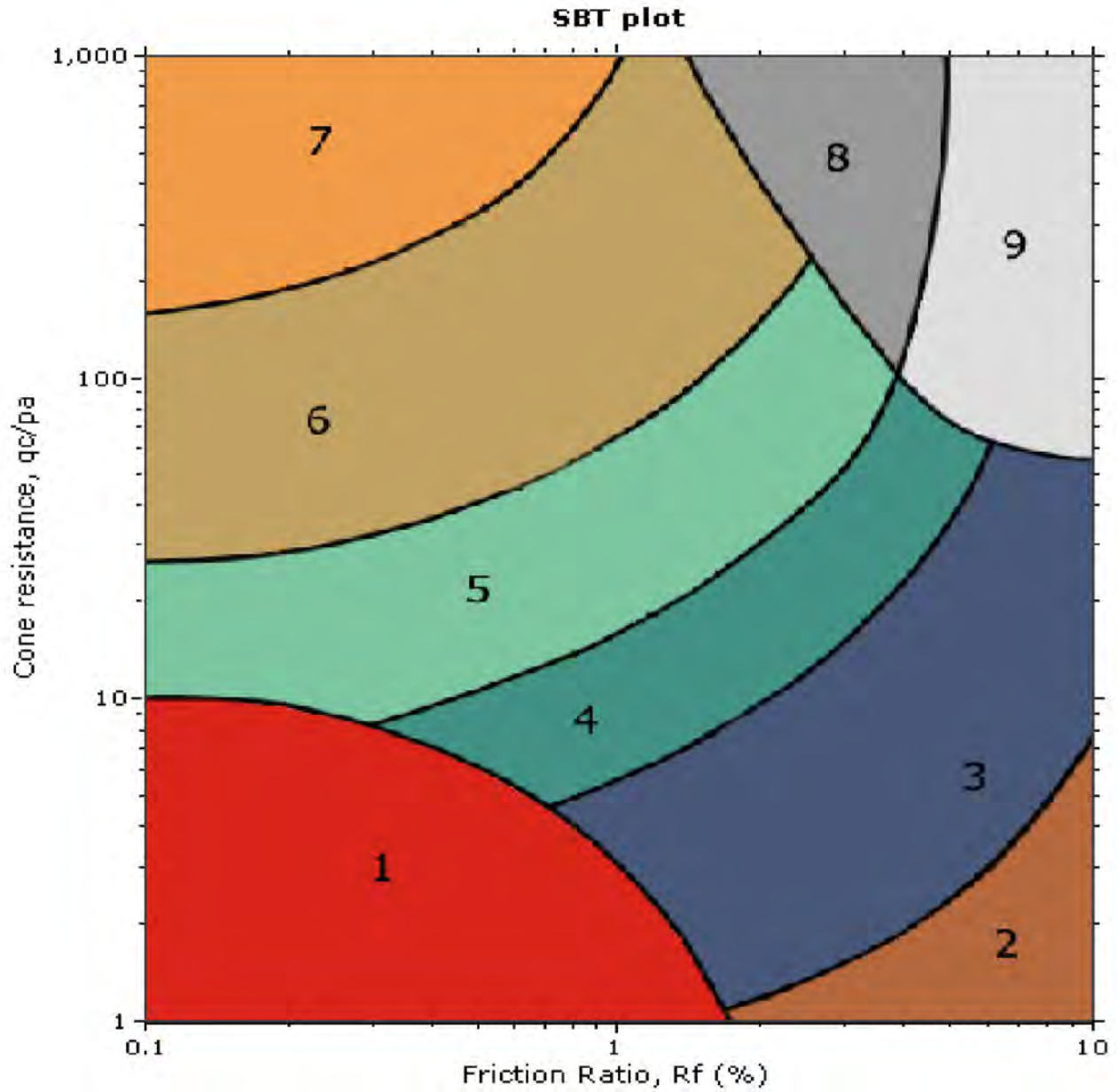












SBT legend

- | | | |
|---|---|---|
| ■ 1. Sensitive fine grained | ■ 4. Clayey silt to silty clay | ■ 7. Gravelly sand to sand |
| ■ 2. Organic material | ■ 5. Silty sand to sandy silt | ■ 8. Very stiff sand to clayey sand |
| ■ 3. Clay to silty clay | ■ 6. Clean sand to silty sand | ■ 9. Very stiff fine grained |

Universal Engineering Services
 Compton Community College
 Compton, CA

CPT Shear Wave Measurements

Location	Tip Depth (ft)	Geophone Depth (ft)	Travel Distance (ft)	S-Wave Arrival (msec)	S-Wave Velocity from Surface (ft/sec)	Interval S-Wave Velocity (ft/sec)
CPT-1	10.04	9.04	9.26	11.64	795	
	20.01	19.01	19.11	24.40	783	772
	30.02	29.02	29.09	36.08	806	854
	40.03	39.03	39.08	51.16	764	663
	50.03	49.03	49.07	62.28	788	898
	60.01	59.01	59.04	73.00	809	930
	70.01	69.01	69.04	84.06	821	904
CPT-2	10.01	9.01	9.23	11.74	786	
	20.01	19.01	19.11	23.76	804	822
	30.02	29.02	29.09	36.40	799	789
	40.03	39.03	39.08	51.80	754	649
	50.03	49.03	49.07	62.08	790	972
	60.01	59.01	59.04	72.34	816	972
	70.01	69.01	69.04	83.52	827	894
CPT-4	10.04	9.04	9.26	11.22	825	
	20.01	19.01	19.11	22.56	847	869
	30.02	29.02	29.09	34.24	850	854
	40.03	39.03	39.08	46.68	837	803
	50.00	49.00	49.04	58.76	835	824
	60.01	59.01	59.04	68.82	858	994
	70.01	69.01	69.04	80.52	857	854
CPT-5	10.04	9.04	9.26	13.60	681	
	20.05	19.05	19.15	29.34	653	629
	30.02	29.02	29.09	42.48	685	756
	40.03	39.03	39.08	56.32	694	722
	50.03	49.03	49.07	67.76	724	873
	60.10	59.10	59.13	78.24	756	960
	70.11	69.11	69.14	88.20	784	1005
	75.09	74.09	74.12	93.46	793	946

Shear Wave Source Offset - 2 ft

S-Wave Velocity from Surface = Travel Distance/S-Wave Arrival
 Interval S-Wave Velocity = (Travel Dist2-Travel Dist1)/(Time2-Time1)

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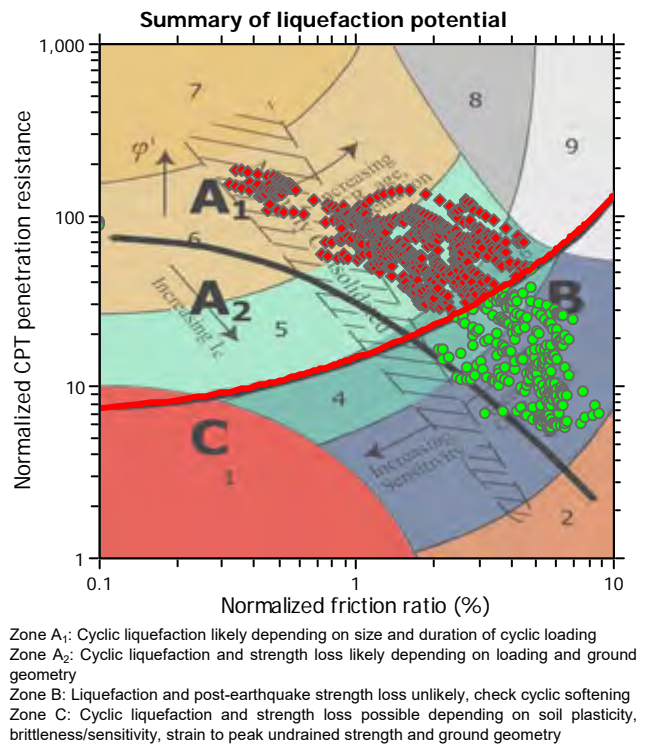
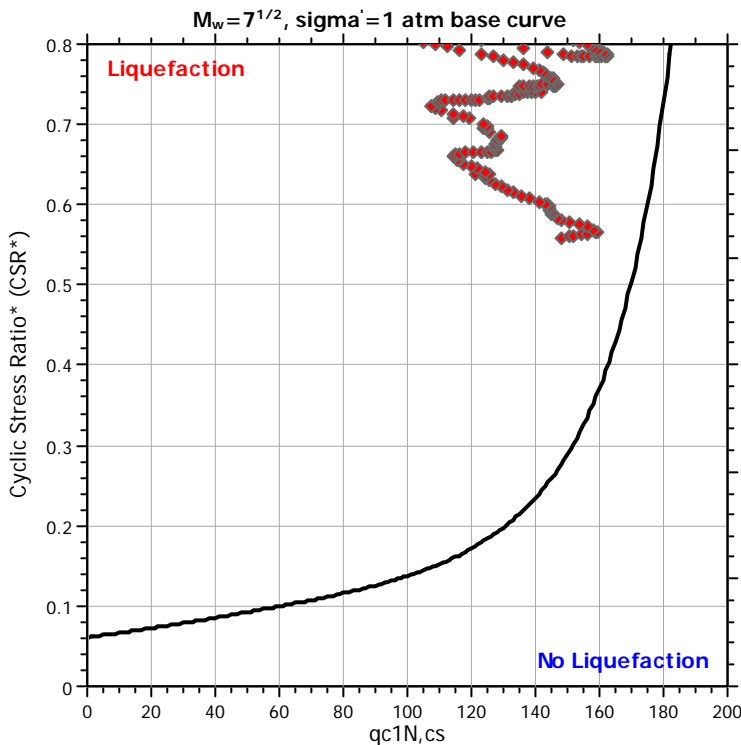
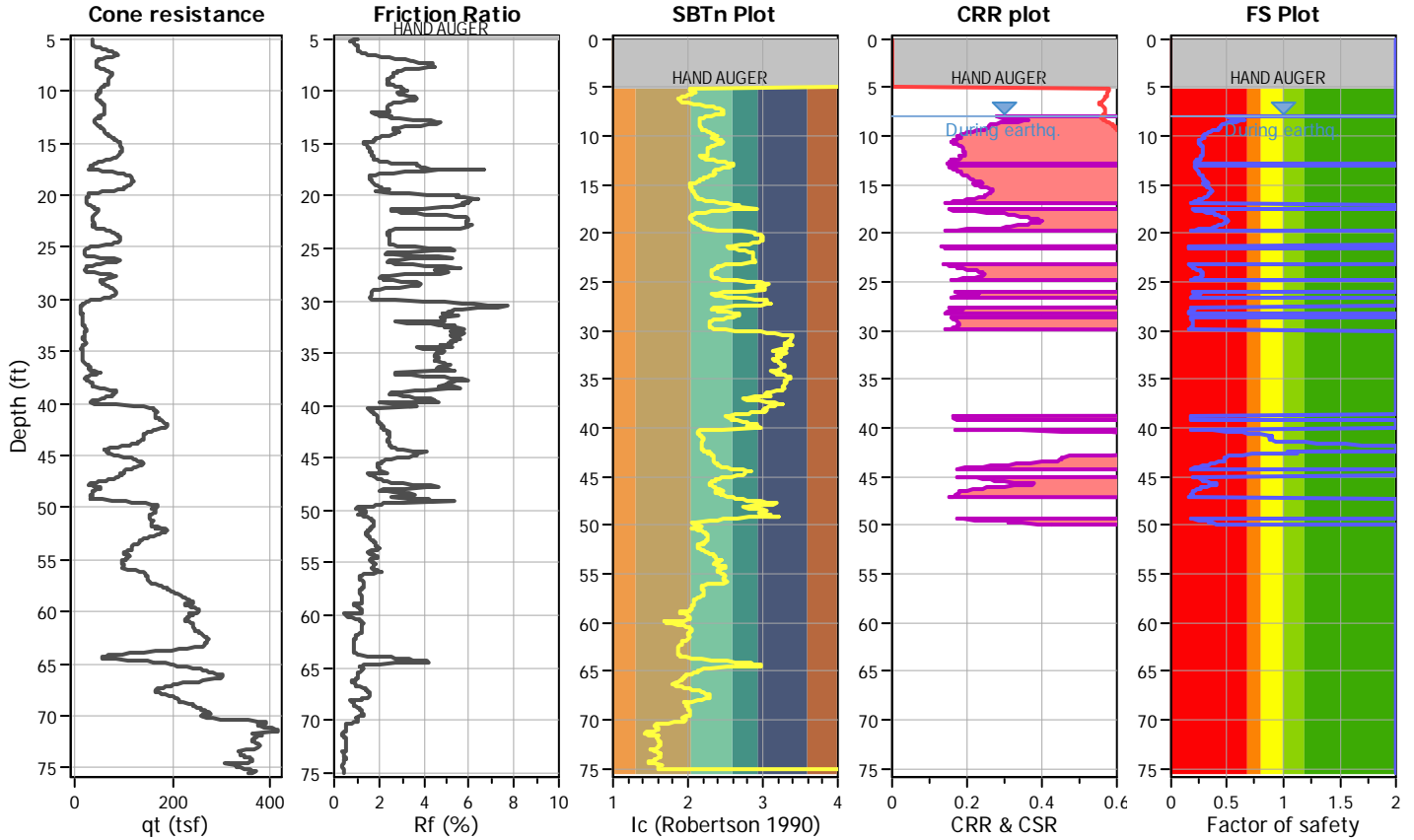
LIQUEFACTION ANALYSIS REPORT

Project title : Universal Engineering Services / Compton
CPT file : CPT-1

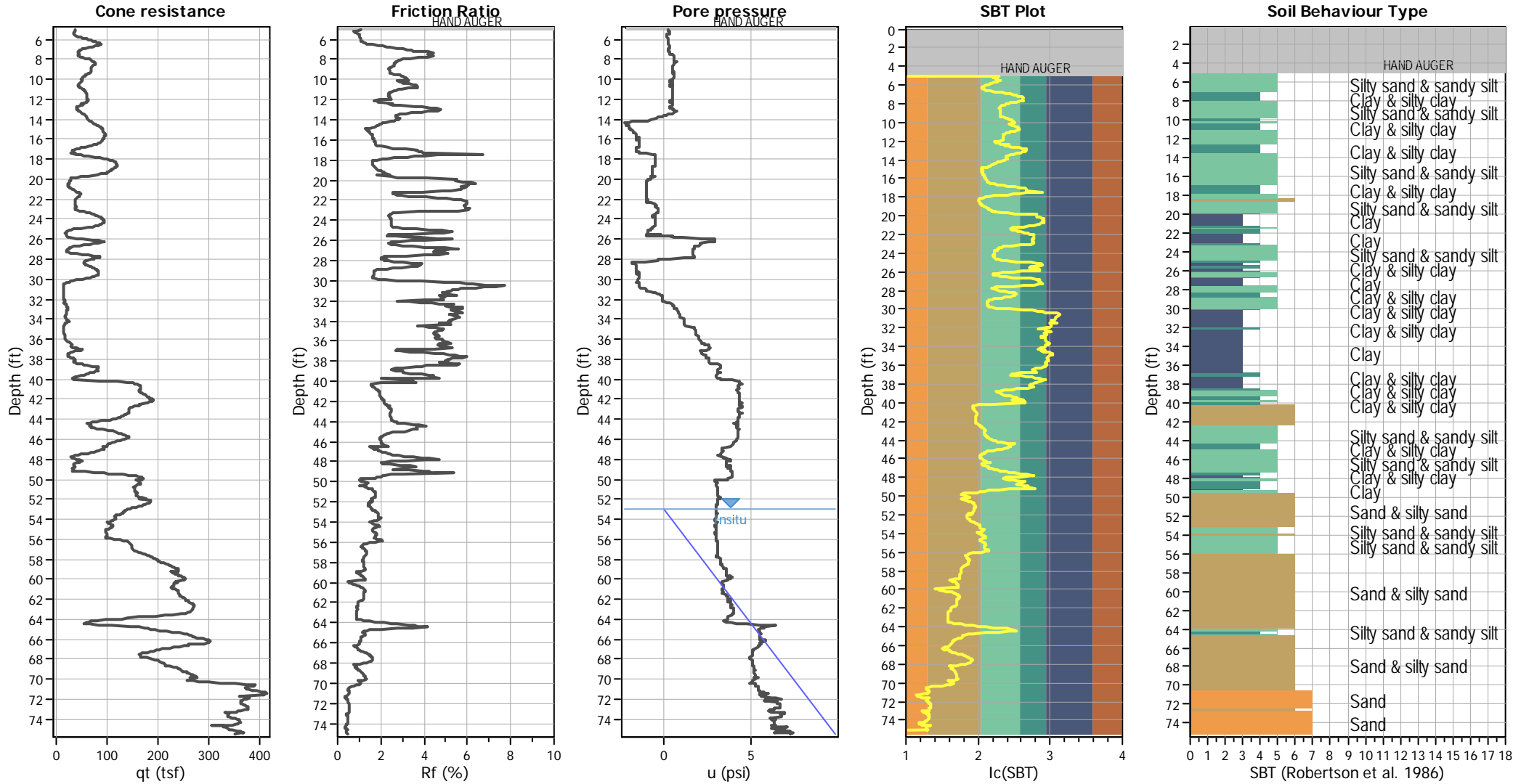
Location : 1111 E. Artesia Blvd, Compton, CA

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	52.90 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	1	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w :	7.30	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method
Peak ground acceleration:	0.77	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



CPT basic interpretation plots



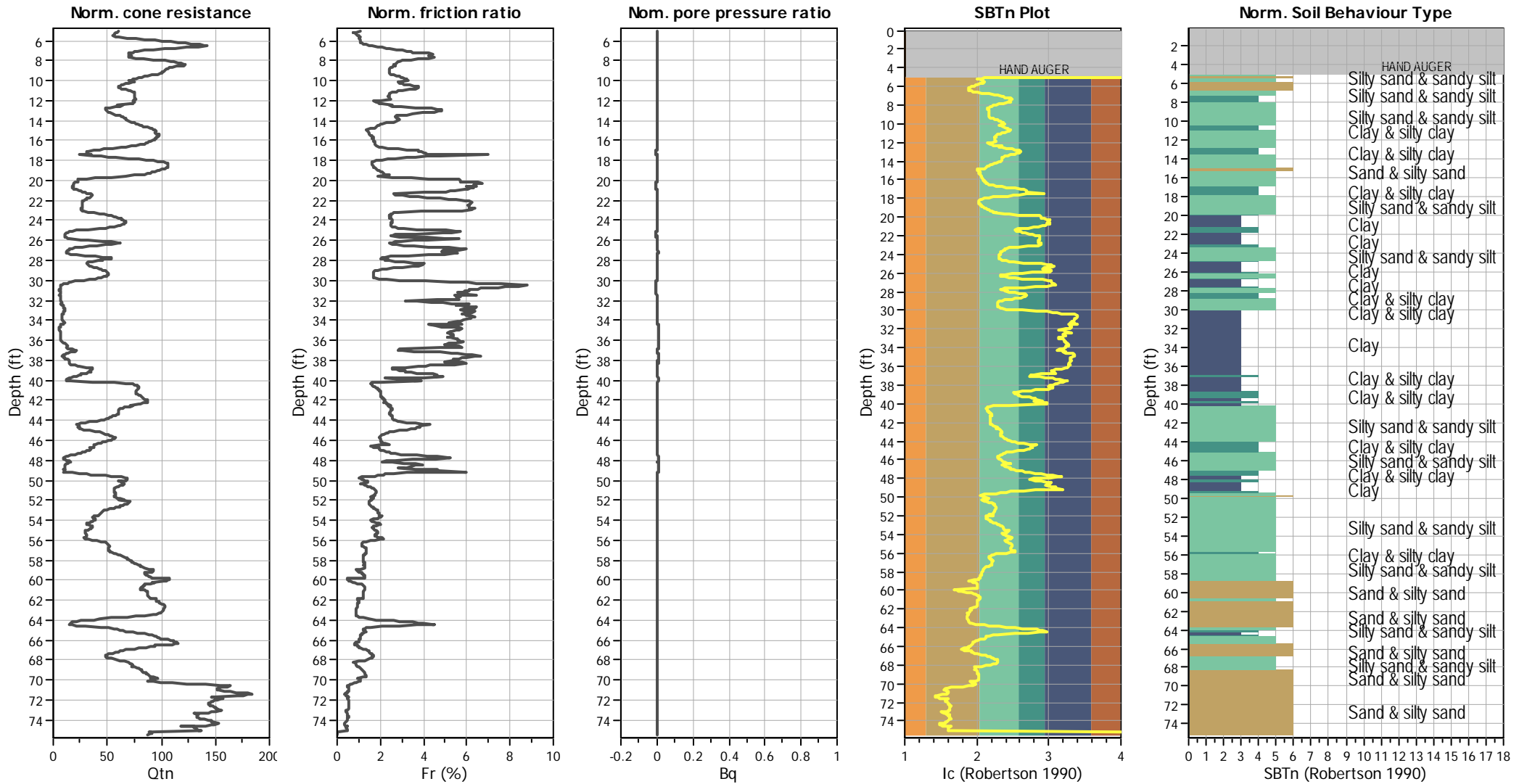
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_G applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

■ 1. Sensitive fine grained	■ 4. Clayey silt to silty	■ 7. Gravely sand to sand
■ 2. Organic material	■ 5. Silty sand to sandy silt	■ 8. Very stiff sand to
■ 3. Clay to silty clay	■ 6. Clean sand to silty sand	■ 9. Very stiff fine grained

CPT basic interpretation plots (normalized)



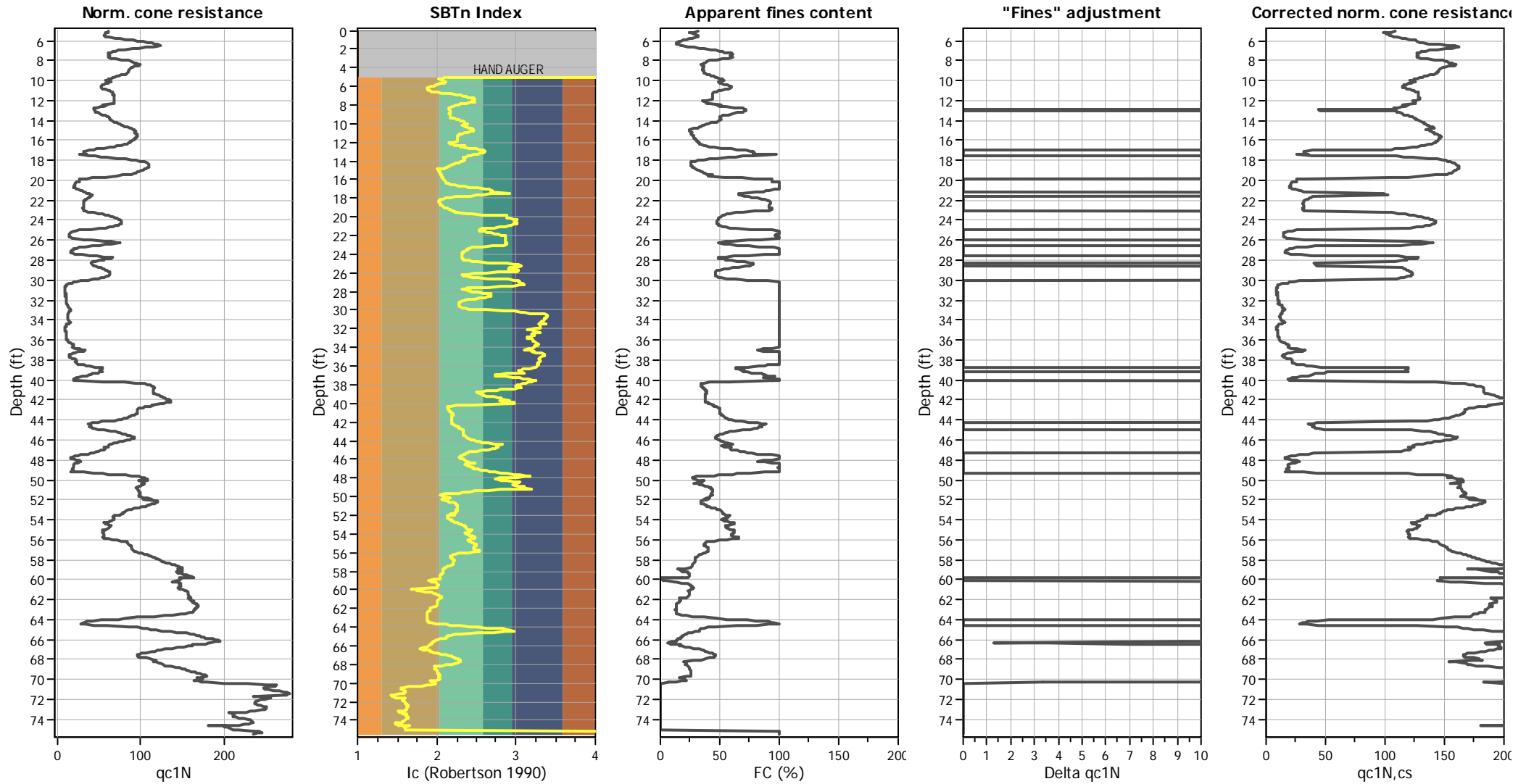
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Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

■ 1. Sensitive fine grained	■ 4. Clayey silt to silty	■ 7. Gravely sand to sand
■ 2. Organic material	■ 5. Silty sand to sandy silt	■ 8. Very stiff sand to
■ 3. Clay to silty clay	■ 6. Clean sand to silty sand	■ 9. Very stiff fine grained

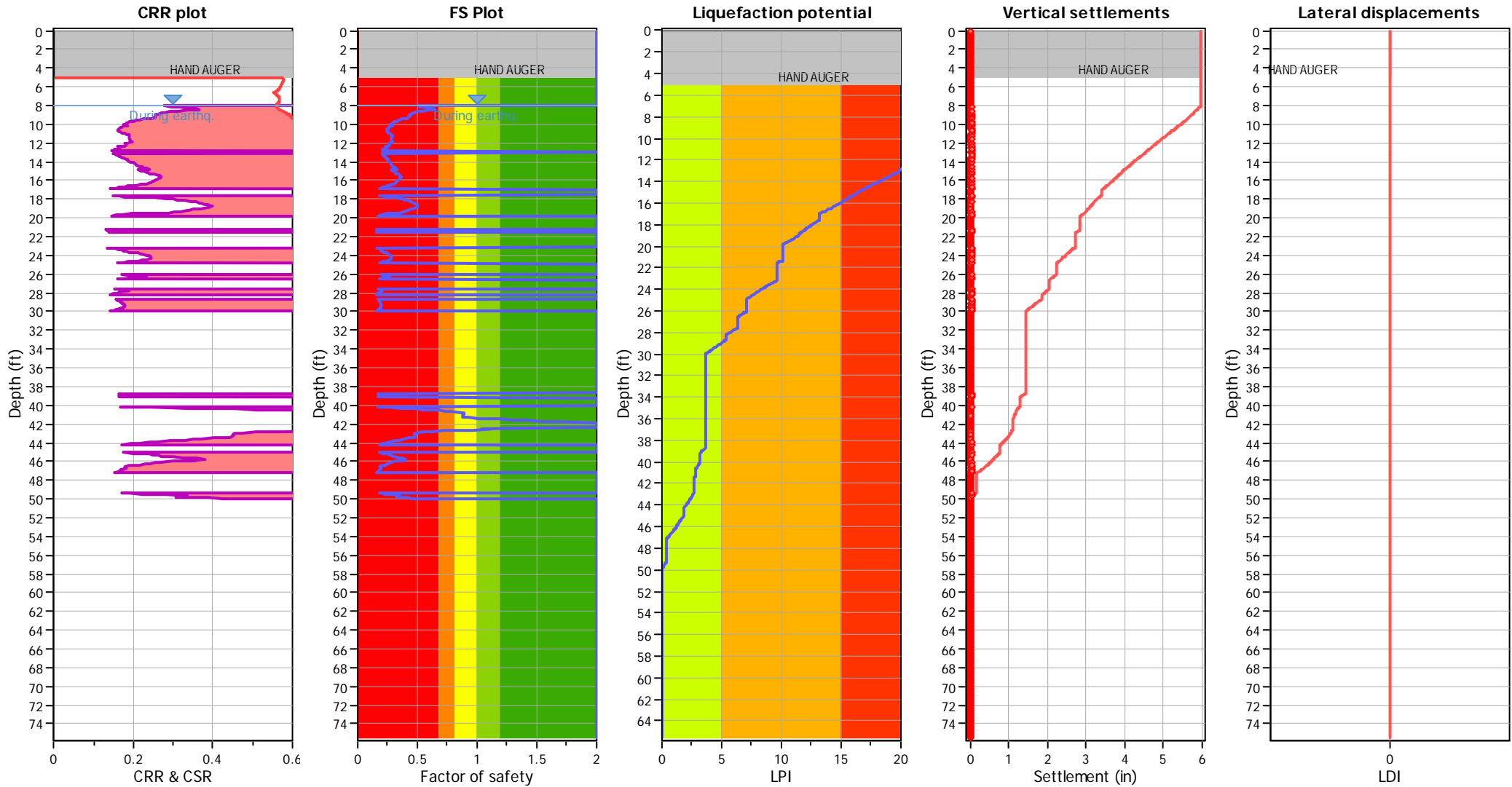
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_q applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

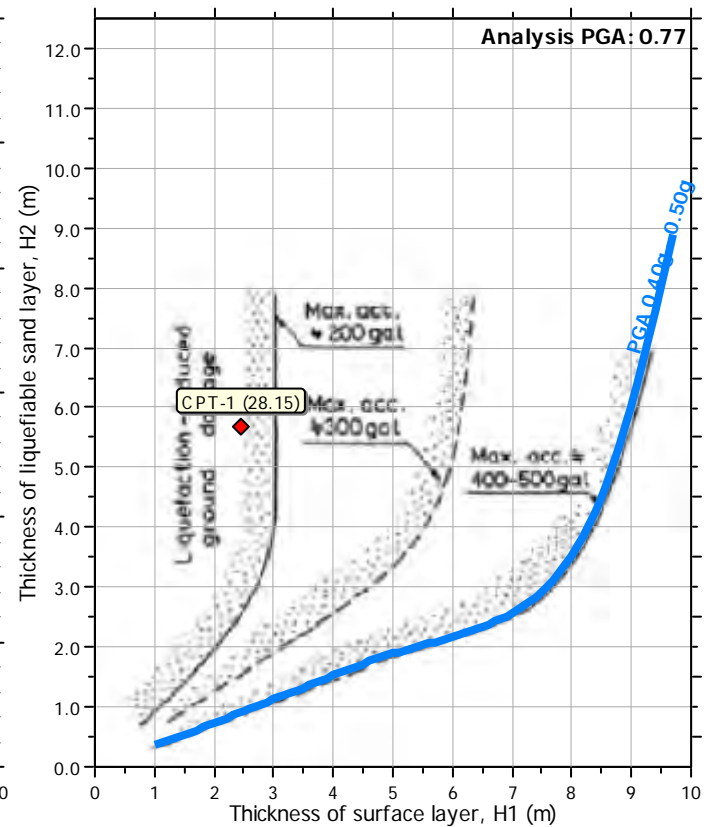
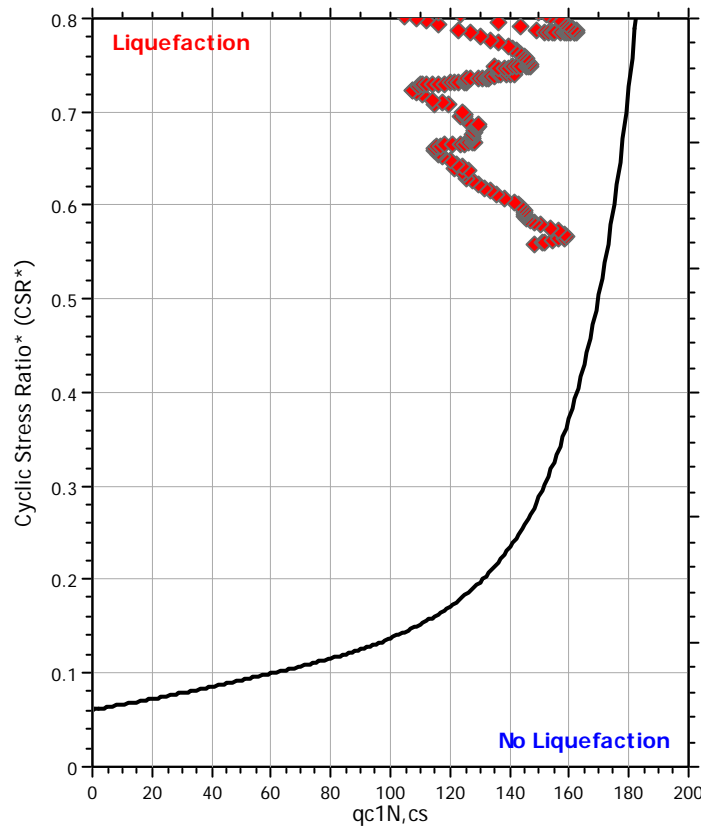
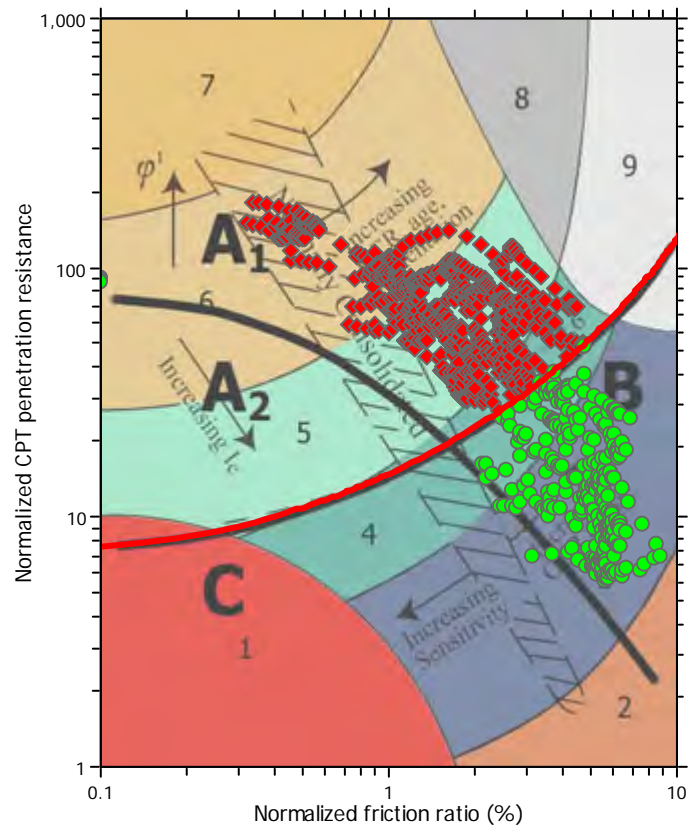
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

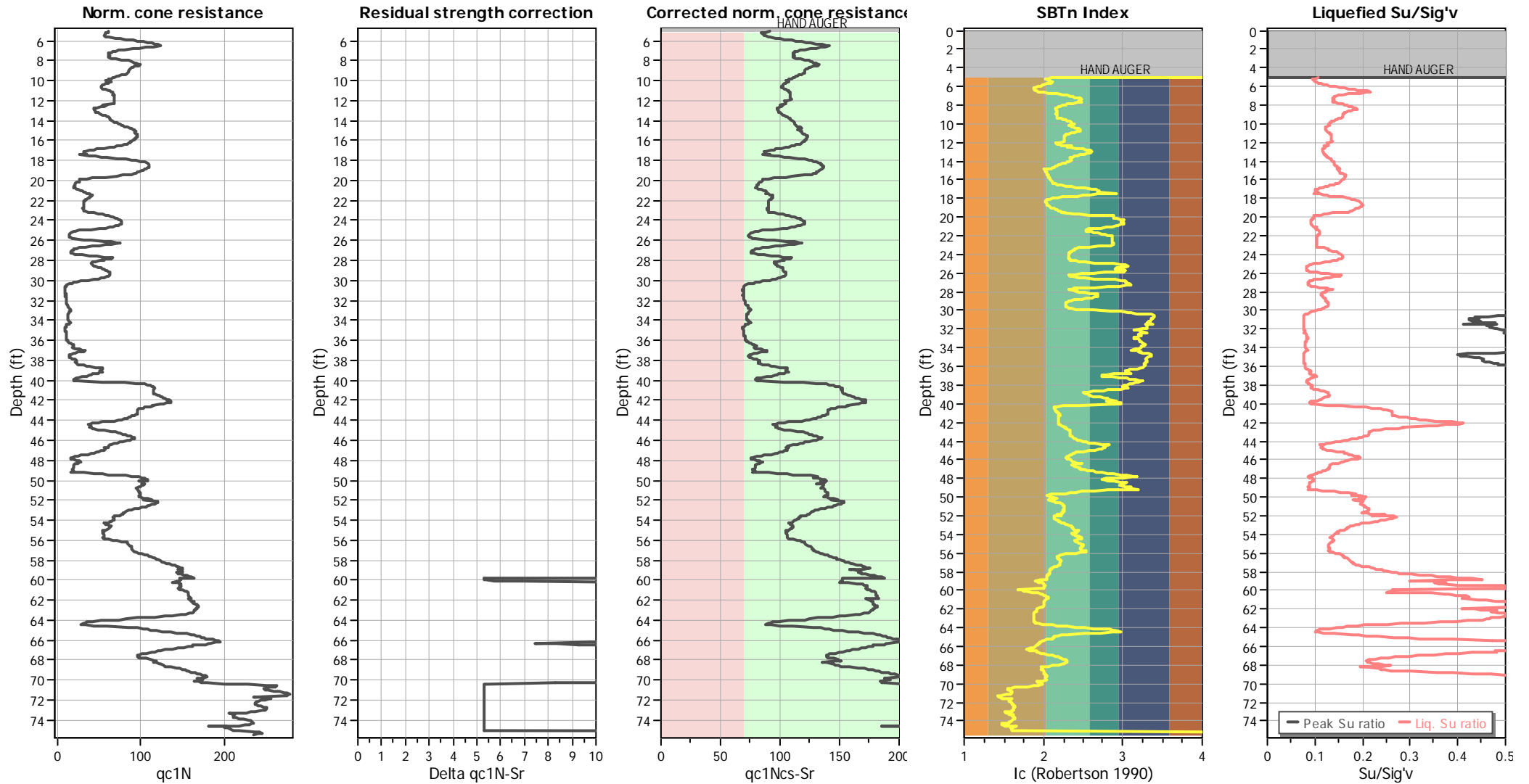
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.07	-9999.00	-9999.00	-9999.00	100.00	120.90
2	0.14	-9999.00	-9999.00	-9999.00	100.00	120.90
3	0.21	-9999.00	-9999.00	-9999.00	100.00	120.90
4	0.28	-9999.00	-9999.00	-9999.00	100.00	120.90
5	0.33	-9999.00	-9999.00	-9999.00	100.00	120.90
6	0.40	-9999.00	-9999.00	-9999.00	100.00	120.90
7	0.47	-9999.00	-9999.00	-9999.00	100.00	120.90
8	0.53	-9999.00	-9999.00	-9999.00	100.00	120.90
9	0.59	-9999.00	-9999.00	-9999.00	100.00	120.90
10	0.67	-9999.00	-9999.00	-9999.00	100.00	120.90
11	0.73	-9999.00	-9999.00	-9999.00	100.00	120.90
12	0.81	-9999.00	-9999.00	-9999.00	100.00	120.90
13	0.87	-9999.00	-9999.00	-9999.00	100.00	120.90
14	0.93	-9999.00	-9999.00	-9999.00	100.00	120.90
15	1.00	-9999.00	-9999.00	-9999.00	100.00	120.90
16	1.06	-9999.00	-9999.00	-9999.00	100.00	120.90
17	1.13	-9999.00	-9999.00	-9999.00	100.00	120.90
18	1.19	-9999.00	-9999.00	-9999.00	100.00	120.90
19	1.26	-9999.00	-9999.00	-9999.00	100.00	120.90
20	1.33	-9999.00	-9999.00	-9999.00	100.00	120.90
21	1.39	-9999.00	-9999.00	-9999.00	100.00	120.90
22	1.45	-9999.00	-9999.00	-9999.00	100.00	120.90
23	1.51	-9999.00	-9999.00	-9999.00	100.00	120.90
24	1.59	-9999.00	-9999.00	-9999.00	100.00	120.90
25	1.64	-9999.00	-9999.00	-9999.00	100.00	120.90
26	1.72	-9999.00	-9999.00	-9999.00	100.00	120.90
27	1.77	-9999.00	-9999.00	-9999.00	100.00	120.90
28	1.84	-9999.00	-9999.00	-9999.00	100.00	120.90
29	1.92	-9999.00	-9999.00	-9999.00	100.00	120.90
30	1.97	-9999.00	-9999.00	-9999.00	100.00	120.90
31	2.05	-9999.00	-9999.00	-9999.00	100.00	120.90
32	2.10	-9999.00	-9999.00	-9999.00	100.00	120.90
33	2.18	-9999.00	-9999.00	-9999.00	100.00	120.90
34	2.24	-9999.00	-9999.00	-9999.00	100.00	120.90
35	2.30	-9999.00	-9999.00	-9999.00	100.00	120.90
36	2.38	-9999.00	-9999.00	-9999.00	100.00	120.90
37	2.44	-9999.00	-9999.00	-9999.00	100.00	120.90
38	2.50	-9999.00	-9999.00	-9999.00	100.00	120.90
39	2.58	-9999.00	-9999.00	-9999.00	100.00	120.90
40	2.64	-9999.00	-9999.00	-9999.00	100.00	120.90
41	2.69	-9999.00	-9999.00	-9999.00	100.00	120.90
42	2.77	-9999.00	-9999.00	-9999.00	100.00	120.90
43	2.83	-9999.00	-9999.00	-9999.00	100.00	120.90
44	2.89	-9999.00	-9999.00	-9999.00	100.00	120.90
45	2.97	-9999.00	-9999.00	-9999.00	100.00	120.90
46	3.03	-9999.00	-9999.00	-9999.00	100.00	120.90
47	3.08	-9999.00	-9999.00	-9999.00	100.00	120.90
48	3.16	-9999.00	-9999.00	-9999.00	100.00	120.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.22	-9999.00	-9999.00	-9999.00	100.00	120.90
50	3.29	-9999.00	-9999.00	-9999.00	100.00	120.90
51	3.36	-9999.00	-9999.00	-9999.00	100.00	120.90
52	3.42	-9999.00	-9999.00	-9999.00	100.00	120.90
53	3.48	-9999.00	-9999.00	-9999.00	100.00	120.90
54	3.55	-9999.00	-9999.00	-9999.00	100.00	120.90
55	3.62	-9999.00	-9999.00	-9999.00	100.00	120.90
56	3.69	-9999.00	-9999.00	-9999.00	100.00	120.90
57	3.75	-9999.00	-9999.00	-9999.00	100.00	120.90
58	3.81	-9999.00	-9999.00	-9999.00	100.00	120.90
59	3.89	-9999.00	-9999.00	-9999.00	100.00	120.90
60	3.95	-9999.00	-9999.00	-9999.00	100.00	120.90
61	4.00	-9999.00	-9999.00	-9999.00	100.00	120.90
62	4.08	-9999.00	-9999.00	-9999.00	100.00	120.90
63	4.14	-9999.00	-9999.00	-9999.00	100.00	120.90
64	4.20	-9999.00	-9999.00	-9999.00	100.00	120.90
65	4.28	-9999.00	-9999.00	-9999.00	100.00	120.90
66	4.33	-9999.00	-9999.00	-9999.00	100.00	120.90
67	4.41	-9999.00	-9999.00	-9999.00	100.00	120.90
68	4.47	-9999.00	-9999.00	-9999.00	100.00	120.90
69	4.53	-9999.00	-9999.00	-9999.00	100.00	120.90
70	4.61	-9999.00	-9999.00	-9999.00	100.00	120.90
71	4.67	-9999.00	-9999.00	-9999.00	100.00	120.90
72	4.74	-9999.00	-9999.00	-9999.00	100.00	120.90
73	4.80	-9999.00	-9999.00	-9999.00	100.00	120.90
74	4.86	-9999.00	-9999.00	-9999.00	100.00	120.90
75	4.94	-9999.00	-9999.00	-9999.00	100.00	120.90
76	5.00	-9999.00	-9999.00	-9999.00	100.00	120.90
77	5.05	37.57	0.39	0.23	15.85	112.32
78	5.13	37.48	0.33	0.23	14.63	111.07
79	5.19	36.91	0.27	0.34	13.41	109.43
80	5.25	36.25	0.28	0.34	13.99	109.70
81	5.33	35.69	0.30	0.34	14.70	110.13
82	5.39	35.31	0.31	0.34	15.20	110.41
83	5.45	35.12	0.32	0.34	15.58	110.68
84	5.53	34.75	0.35	0.11	16.29	111.16
85	5.59	36.16	0.37	0.11	16.08	111.76
86	5.65	38.33	0.40	0.11	15.51	112.38
87	5.72	43.32	0.45	0.11	14.22	113.54
88	5.78	47.74	0.49	0.11	13.29	114.51
89	5.86	52.83	0.56	0.23	12.50	115.64
90	5.92	55.94	0.60	0.23	12.10	116.32
91	5.98	59.14	0.64	0.23	11.76	117.01
92	6.04	63.09	0.68	0.23	11.18	117.60
93	6.12	67.89	0.73	0.23	10.52	118.26
94	6.18	72.23	0.78	0.23	10.07	118.89
95	6.24	75.99	0.84	0.23	9.87	119.60
96	6.31	80.04	0.96	0.23	9.98	120.63

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.37	82.30	1.05	0.23	10.26	121.40
98	6.43	84.66	1.15	0.23	10.51	122.13
99	6.51	87.39	1.28	0.23	10.87	123.01
100	6.57	88.71	1.42	0.23	11.41	123.76
101	6.65	83.53	1.55	0.34	13.16	124.28
102	6.71	77.12	1.61	0.34	14.89	124.37
103	6.77	70.91	1.61	0.34	16.47	124.17
104	6.83	65.07	1.58	0.34	17.90	123.79
105	6.90	58.10	1.59	0.34	20.38	123.59
106	6.96	52.83	1.58	0.23	22.41	123.31
107	7.03	49.25	1.58	0.23	24.00	123.11
108	7.09	46.99	1.60	0.23	25.28	123.08
109	7.17	46.05	1.60	0.23	25.82	123.05
110	7.22	44.45	1.68	0.23	27.35	123.32
111	7.28	43.50	1.81	0.34	28.99	123.83
112	7.36	43.50	1.92	0.34	29.80	124.25
113	7.42	44.07	1.94	0.34	29.62	124.36
114	7.50	45.39	1.89	0.34	28.47	124.25
115	7.55	44.16	1.89	0.46	29.17	124.16
116	7.61	44.26	1.89	0.57	29.10	124.17
117	7.70	44.35	1.97	0.57	29.66	124.48
118	7.75	47.74	1.99	0.57	27.88	124.75
119	7.81	52.36	1.97	0.57	25.35	124.88
120	7.89	58.29	1.96	0.57	22.76	125.12
121	7.95	61.49	1.95	0.57	21.49	125.20
122	8.01	64.98	1.95	0.57	20.27	125.33
123	8.08	68.18	1.95	0.57	19.25	125.45
124	8.14	69.59	1.96	0.57	18.87	125.53
125	8.22	72.13	1.99	0.57	18.36	125.76
126	8.28	74.77	2.03	0.68	17.86	125.96
127	8.34	77.12	2.05	0.57	17.46	126.13
128	8.40	78.35	2.06	0.57	17.23	126.18
129	8.48	77.50	2.04	0.57	17.39	126.08
130	8.54	75.71	2.00	0.57	17.69	125.90
131	8.60	73.83	1.94	0.57	17.88	125.60
132	8.68	71.76	1.83	0.46	17.88	125.10
133	8.74	70.63	1.74	0.46	17.77	124.72
134	8.79	69.78	1.69	0.46	17.75	124.48
135	8.87	69.31	1.65	0.46	17.69	124.28
136	8.93	68.93	1.63	0.46	17.73	124.19
137	8.99	68.74	1.63	0.46	17.82	124.18
138	9.07	68.74	1.65	0.46	17.94	124.23
139	9.13	68.74	1.66	0.46	18.07	124.30
140	9.19	68.65	1.66	0.46	18.12	124.29
141	9.27	68.55	1.64	0.57	18.11	124.21
142	9.33	67.89	1.64	0.46	18.30	124.16
143	9.39	66.11	1.63	0.57	18.80	124.06
144	9.46	62.53	1.62	0.46	19.93	123.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.52	60.08	1.62	0.57	20.78	123.81
146	9.58	57.82	1.66	0.57	21.83	123.86
147	9.66	56.22	1.65	0.57	22.49	123.78
148	9.72	54.43	1.63	0.57	23.06	123.58
149	9.78	52.64	1.63	0.57	23.83	123.49
150	9.86	51.42	1.63	0.57	24.46	123.46
151	9.91	50.47	1.62	0.57	24.88	123.38
152	9.97	50.47	1.60	0.46	24.75	123.26
153	10.04	48.03	1.57	0.46	25.77	123.02
154	10.12	52.92	1.51	0.34	23.15	122.95
155	10.18	52.07	1.45	0.46	23.09	122.61
156	10.25	50.00	1.43	0.34	23.93	122.43
157	10.31	48.21	1.43	0.46	24.78	122.32
158	10.37	46.33	1.40	0.46	25.57	122.11
159	10.45	44.82	1.49	0.46	27.13	122.45
160	10.50	44.26	1.55	0.46	27.98	122.71
161	10.58	43.41	1.58	0.34	28.80	122.81
162	10.64	43.22	1.60	0.46	29.10	122.88
163	10.70	43.69	1.63	0.34	29.13	123.04
164	10.78	44.92	1.66	0.46	28.77	123.26
165	10.84	46.52	1.65	0.46	27.89	123.32
166	10.90	49.06	1.61	0.46	26.34	123.26
167	10.98	52.07	1.55	0.46	24.52	123.11
168	11.04	53.96	1.51	0.46	23.49	123.03
169	11.10	55.65	1.50	0.46	22.73	123.03
170	11.16	57.16	1.49	0.46	22.11	123.04
171	11.22	58.29	1.46	0.46	21.55	122.96
172	11.31	58.57	1.42	0.46	21.18	122.75
173	11.37	58.95	1.40	0.46	20.98	122.69
174	11.43	58.85	1.41	0.46	21.10	122.71
175	11.49	59.14	1.40	0.46	20.97	122.67
176	11.55	59.51	1.40	0.46	20.89	122.69
177	11.64	59.89	1.41	0.46	20.91	122.78
178	11.70	60.08	1.43	0.46	20.98	122.85
179	11.77	60.55	1.44	0.46	20.99	122.96
180	11.82	60.93	1.46	0.46	21.04	123.07
181	11.88	61.49	1.48	0.46	21.04	123.20
182	11.94	61.11	1.50	0.46	21.34	123.28
183	12.03	61.02	1.20	0.46	19.11	121.61
184	12.09	61.68	1.03	0.46	17.57	120.55
185	12.15	61.68	1.12	0.34	18.32	121.13
186	12.21	61.21	1.15	0.46	18.83	121.36
187	12.28	60.83	1.18	0.34	19.22	121.51
188	12.34	59.33	1.21	0.46	19.97	121.61
189	12.42	48.68	1.23	0.46	24.53	121.24
190	12.48	53.49	1.26	0.46	22.73	121.67
191	12.54	51.04	1.30	0.46	24.16	121.77
192	12.60	47.74	1.37	0.46	26.47	122.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.69	43.41	1.53	0.34	30.36	122.59
194	12.75	41.72	1.62	0.34	32.26	122.90
195	12.81	40.21	1.72	0.34	34.23	123.26
196	12.87	40.21	1.82	0.34	35.13	123.68
197	12.93	40.21	1.90	0.46	35.83	124.00
198	13.02	41.06	1.94	0.46	35.61	124.20
199	13.08	41.81	1.92	0.57	34.97	124.16
200	13.14	42.66	1.89	0.57	34.21	124.09
201	13.20	43.60	1.82	0.68	33.10	123.88
202	13.26	45.11	1.76	0.68	31.66	123.68
203	13.35	47.84	1.64	0.57	29.24	123.33
204	13.41	50.19	1.58	0.46	27.57	123.16
205	13.47	52.55	1.53	0.23	26.11	123.06
206	13.53	54.43	1.49	0.23	24.96	122.94
207	13.59	55.94	1.49	0.11	24.35	123.00
208	13.65	57.25	1.53	0.00	24.16	123.25
209	13.74	59.23	1.61	-0.11	24.05	123.73
210	13.80	59.89	1.66	-0.34	24.15	123.96
211	13.86	59.98	1.69	-0.46	24.37	124.10
212	13.92	59.98	1.72	-0.46	24.64	124.24
213	13.98	61.02	1.74	-0.46	24.36	124.33
214	14.07	63.94	1.73	-0.80	23.30	124.43
215	14.13	66.20	1.72	-0.91	22.50	124.48
216	14.19	67.99	1.67	-1.48	21.60	124.31
217	14.25	69.87	1.56	-1.82	20.31	123.88
218	14.31	71.47	1.49	-2.05	19.40	123.60
219	14.37	72.89	1.47	-2.28	18.91	123.55
220	14.46	75.24	1.45	-2.17	18.15	123.50
221	14.52	77.03	1.44	-2.17	17.68	123.54
222	14.58	79.01	1.44	-2.17	17.22	123.60
223	14.64	81.27	1.45	-2.05	16.76	123.71
224	14.70	83.24	1.47	-2.05	16.49	123.89
225	14.79	86.16	1.49	-2.05	16.00	124.06
226	14.85	87.86	1.32	-2.05	14.59	123.20
227	14.91	89.55	1.17	-2.05	13.33	122.38
228	14.97	90.97	1.22	-1.94	13.39	122.70
229	15.03	92.19	1.26	-1.94	13.48	123.00
230	15.09	93.04	1.30	-1.82	13.60	123.25
231	15.18	92.14	1.35	-1.77	14.10	123.49
232	15.23	92.10	1.37	-1.77	14.27	123.61
233	15.29	93.88	1.38	-1.77	14.02	123.72
234	15.38	95.96	1.42	-1.71	13.90	123.97
235	15.44	96.62	1.49	-1.59	14.21	124.33
236	15.50	96.80	1.53	-1.59	14.41	124.52
237	15.56	96.62	1.55	-1.59	14.59	124.62
238	15.62	96.52	1.56	-1.59	14.70	124.68
239	15.71	95.77	1.56	-1.59	14.87	124.65
240	15.77	95.20	1.54	-1.59	14.91	124.56

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.83	94.73	1.55	-1.48	15.06	124.58
242	15.89	93.98	1.55	-1.59	15.25	124.58
243	15.95	93.04	1.55	-1.48	15.44	124.54
244	16.04	91.72	1.54	-1.59	15.70	124.47
245	16.10	90.97	1.54	-1.48	15.87	124.44
246	16.16	90.40	1.54	-1.48	16.00	124.42
247	16.22	89.46	1.53	-1.48	16.17	124.35
248	16.28	88.23	1.51	-1.48	16.36	124.23
249	16.34	86.45	1.48	-1.48	16.57	124.02
250	16.43	82.49	1.43	-1.48	17.16	123.63
251	16.49	78.91	1.39	-1.48	17.83	123.34
252	16.55	74.67	1.36	-1.48	18.75	123.03
253	16.61	70.06	1.34	-1.48	19.98	122.77
254	16.67	65.26	1.34	-1.48	21.54	122.58
255	16.76	57.54	1.34	-1.48	24.55	122.29
256	16.82	52.92	1.35	-1.59	26.76	122.13
257	16.88	48.97	1.36	-1.59	28.99	122.04
258	16.94	44.92	1.41	-1.59	31.88	122.07
259	17.00	40.49	1.49	-1.59	35.79	122.21
260	17.09	34.56	1.26	-1.59	38.37	120.59
261	17.15	32.86	1.23	-1.59	39.72	120.29
262	17.21	32.96	1.28	-1.59	40.30	120.59
263	17.27	33.99	1.34	-1.48	40.08	121.02
264	17.34	35.78	1.45	-1.48	39.69	121.74
265	17.39	37.48	1.63	-1.06	39.96	122.67
266	17.46	27.50	1.84	-1.06	53.66	122.82
267	17.52	41.34	1.93	-0.68	39.54	124.15
268	17.60	48.40	1.95	-0.57	34.81	124.63
269	17.66	55.56	1.99	-0.57	31.06	125.09
270	17.72	62.81	2.01	-0.57	27.89	125.47
271	17.81	77.22	2.04	-0.57	22.98	126.08
272	17.87	86.82	2.01	-0.57	20.21	126.26
273	17.93	94.64	1.94	-0.57	18.08	126.23
274	17.99	101.42	1.85	-0.57	16.24	126.03
275	18.05	106.69	1.78	-0.57	15.00	125.90
276	18.12	111.12	1.77	-0.57	14.23	125.94
277	18.18	112.91	1.79	-0.57	14.04	126.05
278	18.27	115.92	1.83	-0.57	13.82	126.29
279	18.33	117.33	1.87	-0.57	13.82	126.48
280	18.39	117.99	1.90	-0.57	13.86	126.60
281	18.45	118.56	1.92	-0.57	13.89	126.68
282	18.51	119.03	1.95	-0.57	13.97	126.80
283	18.60	119.31	1.99	-0.57	14.14	126.96
284	18.66	119.12	2.02	-0.57	14.31	127.06
285	18.72	118.74	2.04	-0.68	14.50	127.14
286	18.78	117.90	2.06	-0.68	14.72	127.18
287	18.84	116.77	2.07	-0.68	14.98	127.21
288	18.90	115.07	2.09	-0.68	15.35	127.24

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.99	111.87	2.11	-0.68	16.01	127.24
290	19.05	110.18	2.12	-0.68	16.39	127.25
291	19.11	107.73	2.14	-0.68	16.95	127.27
292	19.17	105.56	2.19	-0.68	17.57	127.36
293	19.23	104.24	2.21	-0.68	17.94	127.39
294	19.32	101.61	2.18	-0.68	18.38	127.25
295	19.38	99.06	2.19	-0.68	18.99	127.22
296	19.44	95.01	2.29	-0.68	20.42	127.45
297	19.50	87.95	2.10	-0.68	21.18	126.62
298	19.56	79.10	1.46	-0.68	19.68	123.70
299	19.65	64.41	1.61	-0.68	25.68	123.93
300	19.71	57.35	1.58	-0.75	28.48	123.48
301	19.77	48.03	1.61	-0.57	33.88	123.18
302	19.83	39.08	1.60	-0.82	40.49	122.63
303	19.89	29.57	1.60	-0.82	50.91	121.96
304	19.95	29.85	1.64	-0.82	51.05	122.16
305	20.01	29.43	1.60	-0.92	51.27	121.96
306	20.09	29.29	1.60	-0.92	51.54	121.95
307	20.15	27.69	1.60	-0.92	53.87	121.81
308	20.21	25.71	1.59	-1.02	56.98	121.60
309	20.30	24.48	1.56	-1.02	58.82	121.34
310	20.36	24.58	1.51	-1.02	58.04	121.11
311	20.42	24.67	1.47	-1.02	57.39	120.90
312	20.48	24.11	1.44	-1.02	58.06	120.70
313	20.54	23.26	1.41	-1.02	59.27	120.46
314	20.63	24.25	1.38	-1.02	57.13	120.40
315	20.69	23.17	1.39	-1.02	59.27	120.32
316	20.75	24.39	1.42	-1.02	57.59	120.63
317	20.81	25.61	1.48	-1.02	56.30	121.03
318	20.87	27.12	1.55	-1.02	54.92	121.53
319	20.93	29.00	1.63	-1.02	53.13	122.05
320	21.02	32.49	1.70	-1.02	49.56	122.66
321	21.08	34.56	1.75	-1.02	47.67	123.00
322	21.14	36.63	1.78	-1.02	45.80	123.26
323	21.20	38.61	1.51	-1.02	41.18	122.18
324	21.26	40.96	1.05	-1.02	33.96	119.70
325	21.35	45.11	1.14	-1.02	32.17	120.52
326	21.41	46.80	1.23	-1.02	32.08	121.14
327	21.47	47.74	1.33	-1.02	32.62	121.78
328	21.53	48.31	1.43	-1.02	33.28	122.33
329	21.59	46.61	1.53	-1.02	35.47	122.77
330	21.66	46.33	1.69	-1.02	37.15	123.46
331	21.72	45.11	1.83	-1.02	39.38	124.00
332	21.79	42.85	1.98	-1.02	42.50	124.43
333	21.86	41.53	2.08	-1.02	44.56	124.72
334	21.92	40.40	2.16	-1.02	46.31	124.93
335	22.00	38.61	2.21	-1.02	48.57	124.99
336	22.06	37.67	2.23	-0.91	49.70	124.98

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.13	37.48	2.25	-0.91	50.12	125.03
338	22.18	37.48	2.25	-0.91	50.19	125.04
339	22.26	37.48	2.23	-1.02	50.10	124.97
340	22.32	37.48	2.23	-1.02	50.15	124.97
341	22.39	37.48	2.23	-0.80	50.23	124.98
342	22.46	38.23	2.24	-0.57	49.58	125.05
343	22.52	38.33	2.25	-0.57	49.63	125.10
344	22.60	38.51	2.27	-0.57	49.67	125.16
345	22.64	38.61	2.28	-0.46	49.68	125.20
346	22.71	38.80	2.28	-0.57	49.59	125.22
347	22.77	38.51	2.28	-0.57	49.94	125.21
348	22.84	37.20	2.28	-0.57	51.35	125.12
349	22.93	38.61	2.28	-0.34	49.99	125.22
350	22.98	37.48	2.25	-0.34	50.95	125.05
351	23.04	38.70	2.16	-0.34	48.96	124.81
352	23.12	41.53	1.56	-0.34	40.73	122.60
353	23.17	45.77	1.26	-0.34	34.39	121.30
354	23.26	53.67	1.36	-0.34	30.66	122.25
355	23.32	60.17	1.48	-0.34	28.49	123.13
356	23.38	66.20	1.61	-0.46	26.99	123.99
357	23.44	70.34	1.68	-0.55	25.93	124.44
358	23.49	71.10	1.72	-0.55	25.94	124.62
359	23.56	74.77	1.78	-0.55	25.09	125.00
360	23.63	77.88	1.86	-0.68	24.63	125.44
361	23.69	80.61	1.95	-0.56	24.33	125.85
362	23.75	85.03	2.03	-0.68	23.55	126.30
363	23.84	87.48	2.14	-0.57	23.50	126.75
364	23.89	88.33	2.19	-0.57	23.55	126.93
365	23.96	90.78	2.25	-0.57	23.23	127.19
366	24.02	92.38	2.29	-0.57	23.04	127.37
367	24.10	93.41	2.32	-0.57	22.95	127.48
368	24.16	94.07	2.33	-0.57	22.88	127.54
369	24.23	94.03	2.34	-0.57	22.99	127.59
370	24.29	93.98	2.33	-0.57	22.97	127.55
371	24.36	93.41	2.30	-0.57	22.97	127.43
372	24.41	91.91	2.26	-0.57	23.17	127.25
373	24.50	88.89	2.18	-0.57	23.64	126.92
374	24.56	86.26	2.13	-0.57	24.13	126.68
375	24.62	82.21	2.08	-0.57	25.06	126.37
376	24.68	77.03	2.02	-0.57	26.44	125.99
377	24.75	70.91	1.96	-0.68	28.37	125.59
378	24.80	63.56	1.90	-0.68	31.15	125.10
379	24.89	50.00	1.80	-0.68	38.01	124.12
380	24.95	40.68	1.72	-0.68	44.69	123.28
381	25.01	33.52	1.61	-0.80	51.05	122.31
382	25.07	28.16	1.46	-0.80	56.54	121.19
383	25.14	24.48	1.30	-0.91	60.52	120.00
384	25.22	21.47	1.06	-0.91	62.57	118.16

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.28	19.68	0.89	-0.91	63.31	116.67
386	25.34	18.83	0.63	-0.91	59.10	114.04
387	25.40	18.64	0.46	-0.91	54.47	111.75
388	25.46	18.74	0.44	-1.02	53.44	111.36
389	25.53	18.93	0.43	-0.21	52.67	111.20
390	25.62	19.49	0.52	-1.02	54.55	112.68
391	25.67	18.64	0.65	0.49	60.34	114.23
392	25.73	21.28	0.81	0.34	58.53	116.23
393	25.79	22.60	1.04	0.57	60.45	118.19
394	25.87	25.90	1.37	1.02	59.64	120.52
395	25.94	40.96	1.64	2.16	44.37	122.96
396	25.98	52.17	1.79	2.85	37.18	124.18
397	26.07	70.25	2.04	2.85	29.83	125.86
398	26.14	82.21	2.17	2.85	26.28	126.68
399	26.20	91.15	2.26	2.85	24.14	127.24
400	26.26	94.07	2.27	2.73	23.42	127.35
401	26.32	92.47	2.20	2.51	23.52	127.09
402	26.41	83.15	2.09	2.05	25.64	126.44
403	26.47	74.77	2.02	2.16	28.14	125.94
404	26.53	64.60	1.94	2.05	31.92	125.30
405	26.59	53.77	1.87	2.05	37.22	124.56
406	26.64	44.54	1.80	1.94	43.39	123.84
407	26.73	34.65	1.71	1.71	52.24	122.85
408	26.79	29.95	1.62	1.71	57.39	122.11
409	26.86	26.46	1.48	1.71	61.06	121.11
410	26.92	24.95	1.31	1.71	61.42	120.08
411	26.98	24.01	1.16	1.59	60.93	119.12
412	27.04	23.07	1.04	1.59	60.77	118.24
413	27.12	21.19	0.94	1.59	62.87	117.30
414	27.19	21.19	0.99	1.59	63.82	117.64
415	27.25	21.19	1.09	1.59	65.73	118.33
416	27.30	24.11	1.22	1.59	61.98	119.49
417	27.37	28.81	1.36	1.59	56.17	120.70
418	27.46	38.89	1.56	1.59	46.77	122.47
419	27.52	50.76	1.61	1.59	37.48	123.32
420	27.58	63.28	1.54	1.59	29.92	123.55
421	27.64	73.17	1.57	1.71	26.14	124.06
422	27.70	81.08	1.69	1.71	24.29	124.82
423	27.76	85.32	1.74	1.71	23.35	125.16
424	27.82	84.84	1.69	1.71	23.24	124.96
425	27.89	71.47	1.62	1.14	27.26	124.21
426	27.96	73.73	1.59	0.34	26.22	124.16
427	28.02	68.18	1.62	-0.34	28.68	124.11
428	28.09	60.93	1.58	-0.40	31.69	123.64
429	28.16	56.12	1.68	-0.40	35.24	123.90
430	28.23	54.24	1.86	-1.11	37.96	124.55
431	28.28	53.86	1.99	-1.82	39.35	125.03
432	28.35	54.43	2.11	-1.82	39.95	125.47

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.43	55.65	2.14	-1.82	39.46	125.64
434	28.49	56.12	2.14	-1.71	39.21	125.65
435	28.55	57.91	2.12	-1.59	38.04	125.68
436	28.61	60.83	2.07	-1.59	36.04	125.63
437	28.70	65.73	1.92	-1.59	32.47	125.26
438	28.76	69.21	1.77	-1.59	29.80	124.79
439	28.82	71.94	1.62	-1.59	27.56	124.23
440	28.88	74.20	1.49	-1.59	25.71	123.70
441	28.94	76.56	1.40	-1.59	24.20	123.34
442	29.03	79.57	1.36	-1.59	22.91	123.20
443	29.09	81.08	1.36	-1.59	22.41	123.22
444	29.15	82.30	1.36	-1.59	22.11	123.28
445	29.21	83.15	1.37	-1.59	21.98	123.37
446	29.27	83.53	1.39	-1.48	22.00	123.45
447	29.33	83.71	1.39	-1.59	22.03	123.50
448	29.42	83.81	1.40	-1.48	22.05	123.51
449	29.48	83.62	1.38	-1.59	22.02	123.43
450	29.54	82.77	1.35	-1.48	22.07	123.25
451	29.60	81.55	1.33	-1.48	22.25	123.08
452	29.66	79.85	1.29	-1.48	22.52	122.83
453	29.75	75.80	1.22	-1.48	23.27	122.31
454	29.81	71.94	1.22	-1.48	24.60	122.15
455	29.87	66.76	1.25	-1.48	26.92	122.13
456	29.93	60.08	1.31	-1.48	30.65	122.24
457	29.99	51.42	1.41	-1.52	36.76	122.42
458	30.05	38.99	1.53	-1.52	48.25	122.31
459	30.12	32.49	1.60	-1.52	56.52	122.21
460	30.19	28.25	1.60	-1.50	62.75	121.85
461	30.26	25.90	1.55	-1.59	66.33	121.42
462	30.33	23.07	1.44	-1.48	70.55	120.60
463	30.39	19.21	1.32	-1.48	78.34	119.50
464	30.45	16.39	1.24	-1.48	86.19	118.68
465	30.52	14.97	1.15	-1.48	90.02	117.92
466	30.58	14.60	1.06	-1.48	89.64	117.25
467	30.65	14.13	0.95	-1.41	89.16	116.39
468	30.71	13.37	0.85	-1.41	90.05	115.44
469	30.78	13.65	0.78	-1.41	86.76	114.84
470	30.85	13.37	0.74	-1.37	86.95	114.42
471	30.92	13.18	0.70	-1.37	86.64	113.97
472	30.97	13.18	0.69	-1.13	86.17	113.80
473	31.04	13.18	0.69	-1.02	86.28	113.82
474	31.11	13.47	0.68	-1.02	84.86	113.81
475	31.17	13.47	0.67	-1.02	84.56	113.69
476	31.25	13.94	0.67	-0.91	82.51	113.75
477	31.30	13.65	0.71	-0.63	85.08	114.12
478	31.37	14.78	0.73	-0.52	81.10	114.54
479	31.44	13.00	0.72	-0.34	88.51	114.08
480	31.51	14.97	0.71	-0.30	79.81	114.34

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.57	14.41	0.71	-0.23	82.22	114.29
482	31.63	14.69	0.71	-0.23	81.01	114.29
483	31.70	14.69	0.70	-0.11	80.99	114.26
484	31.79	14.69	0.71	-0.11	81.31	114.33
485	31.85	14.69	0.72	-0.11	81.65	114.43
486	31.91	15.07	0.74	-0.11	80.75	114.67
487	31.97	15.16	0.61	-0.11	76.41	113.26
488	32.03	15.54	0.43	-0.11	68.50	110.76
489	32.09	15.91	0.52	-0.11	70.85	112.23
490	32.18	16.57	0.64	-0.11	72.65	113.80
491	32.24	16.67	0.72	0.00	74.98	114.77
492	32.30	17.04	0.80	0.11	75.80	115.52
493	32.35	15.73	0.84	0.34	81.60	115.74
494	32.43	17.80	0.90	0.46	76.07	116.51
495	32.50	19.59	0.97	0.46	72.52	117.28
496	32.56	19.78	1.02	0.46	73.17	117.69
497	32.62	19.59	1.07	0.46	74.81	118.04
498	32.69	19.68	1.14	0.57	75.87	118.47
499	32.75	20.43	1.17	0.57	74.63	118.81
500	32.83	22.22	1.20	0.57	70.80	119.18
501	32.88	23.45	1.22	0.57	68.44	119.43
502	32.96	23.64	1.23	0.68	68.31	119.52
503	33.02	22.69	1.23	0.68	70.40	119.41
504	33.08	21.66	1.23	0.68	72.76	119.26
505	33.14	21.28	1.22	0.68	73.73	119.21
506	33.23	20.62	1.16	0.80	74.38	118.76
507	33.28	20.15	1.09	0.80	74.21	118.21
508	33.36	19.87	1.03	0.80	73.92	117.79
509	33.41	19.30	1.02	0.80	75.23	117.62
510	33.48	18.93	1.01	0.91	76.29	117.55
511	33.55	18.64	1.02	0.91	77.34	117.55
512	33.61	17.80	1.00	0.91	79.65	117.33
513	33.67	17.80	0.99	0.91	79.32	117.20
514	33.74	18.08	0.98	0.91	78.46	117.22
515	33.80	18.27	0.99	0.91	78.10	117.30
516	33.88	19.21	1.00	1.14	75.55	117.48
517	33.94	19.40	1.01	1.14	75.30	117.58
518	34.00	19.59	1.03	1.14	75.23	117.74
519	34.06	21.00	1.08	1.14	72.52	118.24
520	34.15	22.88	1.16	1.14	69.77	119.01
521	34.21	24.39	1.15	1.14	66.39	119.08
522	34.27	22.98	1.13	1.14	69.01	118.79
523	34.33	21.38	1.12	1.14	72.64	118.57
524	34.39	19.21	0.95	1.14	75.05	117.14
525	34.45	17.23	0.64	1.14	72.75	113.90
526	34.52	16.20	0.65	1.14	76.51	113.87
527	34.61	15.44	0.65	1.25	79.41	113.78
528	34.67	14.50	0.66	1.25	83.38	113.70

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.73	13.94	0.67	1.25	86.19	113.72
530	34.79	14.03	0.69	1.59	86.51	113.96
531	34.85	14.13	0.69	1.71	86.41	114.07
532	34.93	14.31	0.69	1.71	85.61	114.07
533	34.98	14.60	0.69	1.71	84.33	114.08
534	35.07	15.16	0.69	1.82	82.17	114.18
535	35.13	15.44	0.69	1.82	81.32	114.28
536	35.19	15.73	0.70	1.82	80.42	114.37
537	35.25	15.73	0.70	1.82	80.52	114.38
538	35.31	15.73	0.71	1.82	80.80	114.46
539	35.37	15.73	0.71	1.82	81.02	114.51
540	35.43	15.73	0.73	1.82	81.58	114.68
541	35.52	16.01	0.75	1.82	81.22	114.93
542	35.58	16.29	0.76	1.82	80.45	115.03
543	35.64	16.57	0.75	1.94	79.44	115.04
544	35.70	16.86	0.75	1.94	78.55	115.10
545	35.76	16.95	0.77	1.94	78.86	115.31
546	35.85	17.04	0.82	1.94	79.91	115.76
547	35.91	17.42	0.85	1.94	79.33	116.02
548	35.97	17.80	0.88	1.94	78.87	116.32
549	36.03	18.27	0.91	1.94	78.24	116.65
550	36.09	19.02	0.96	2.05	77.21	117.15
551	36.18	20.53	1.07	2.05	75.46	118.15
552	36.24	22.79	1.13	2.16	71.10	118.80
553	36.30	25.52	1.21	2.16	66.75	119.54
554	36.36	27.50	1.28	2.16	64.33	120.15
555	36.42	29.10	1.34	2.28	62.64	120.64
556	36.51	31.55	1.50	2.28	61.11	121.65
557	36.57	31.64	1.59	2.39	62.23	122.11
558	36.63	30.79	1.61	2.51	63.76	122.13
559	36.69	29.38	1.57	2.51	65.47	121.81
560	36.75	29.10	1.28	2.51	62.07	120.32
561	36.81	32.11	0.89	2.51	51.41	117.84
562	36.91	41.15	1.12	2.62	45.49	120.15
563	36.97	46.80	1.27	2.51	42.79	121.41
564	37.03	50.47	1.45	2.51	42.05	122.54
565	37.08	47.93	1.62	2.39	45.70	123.24
566	37.15	44.07	1.74	2.05	50.09	123.56
567	37.21	38.42	1.72	2.05	55.56	123.16
568	37.29	32.39	1.60	2.16	61.73	122.19
569	37.34	29.66	1.52	2.16	64.95	121.63
570	37.43	25.80	1.40	2.16	70.17	120.67
571	37.48	23.45	1.33	2.16	74.05	120.05
572	37.55	22.13	1.32	2.28	77.14	119.88
573	37.62	23.07	1.33	2.39	75.10	120.03
574	37.67	24.20	1.32	2.39	72.36	120.07
575	37.74	26.18	1.38	2.39	69.39	120.61
576	37.81	28.44	1.48	2.39	66.70	121.30

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.86	30.23	1.55	2.39	64.69	121.77
578	37.94	33.24	1.66	2.51	61.70	122.52
579	38.02	35.41	1.80	2.51	60.48	123.28
580	38.07	36.16	1.81	2.51	59.65	123.36
581	38.13	36.25	1.69	2.51	58.35	122.89
582	38.22	35.12	1.89	2.51	61.89	123.60
583	38.28	35.50	1.99	2.51	62.54	124.03
584	38.34	37.38	2.06	2.51	60.92	124.41
585	38.40	40.49	2.06	2.62	57.41	124.60
586	38.47	50.85	2.07	3.08	48.26	125.18
587	38.53	54.33	2.11	3.19	46.15	125.50
588	38.59	59.80	2.16	3.19	43.06	125.89
589	38.68	71.28	2.16	3.19	36.68	126.30
590	38.74	78.53	2.10	3.19	33.03	126.34
591	38.80	82.77	2.07	3.19	31.17	126.38
592	38.85	83.15	2.07	3.19	31.06	126.39
593	38.93	81.08	2.16	3.19	32.48	126.62
594	38.98	80.14	2.27	3.08	33.61	126.95
595	39.04	79.01	2.40	3.08	35.02	127.35
596	39.11	82.49	2.51	3.08	34.24	127.76
597	39.20	78.44	2.61	3.08	36.65	127.93
598	39.26	75.05	2.67	3.08	38.65	128.00
599	39.32	69.59	2.73	3.19	41.84	127.97
600	39.38	64.88	2.77	3.08	44.54	127.89
601	39.44	62.24	2.77	3.08	46.13	127.81
602	39.53	61.02	2.65	3.08	46.16	127.44
603	39.59	55.75	2.43	2.96	48.13	126.59
604	39.65	47.46	2.22	2.96	52.87	125.52
605	39.71	41.06	1.55	2.96	52.48	122.53
606	39.77	36.72	0.75	2.96	45.67	116.97
607	39.86	32.39	0.93	3.08	53.86	118.22
608	39.92	31.36	1.05	3.19	57.35	119.05
609	39.98	33.34	1.17	3.19	56.50	119.95
610	40.04	39.55	1.31	3.30	51.43	121.24
611	40.10	41.25	1.51	3.87	52.08	122.36
612	40.16	84.75	1.68	4.21	28.23	124.91
613	40.22	119.97	1.88	4.33	20.18	126.57
614	40.30	139.65	2.14	4.33	18.00	127.89
615	40.37	152.55	2.37	4.33	17.10	128.86
616	40.43	155.94	2.49	4.44	17.13	129.27
617	40.51	161.03	2.59	4.33	16.83	129.62
618	40.57	163.00	2.68	4.33	16.96	129.92
619	40.63	163.94	2.78	4.21	17.23	130.20
620	40.69	164.98	2.87	4.21	17.44	130.45
621	40.78	167.52	2.98	4.21	17.49	130.74
622	40.84	166.96	3.04	4.21	17.83	130.90
623	40.90	165.73	3.10	4.33	18.19	131.00
624	40.95	164.98	3.14	4.33	18.48	131.11

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.01	164.89	3.20	4.10	18.70	131.23
626	41.10	164.04	3.24	4.10	18.98	131.30
627	41.16	164.23	3.24	4.21	18.97	131.31
628	41.22	164.42	3.23	4.21	18.92	131.29
629	41.28	164.70	3.24	4.21	18.95	131.33
630	41.34	165.92	3.27	4.21	18.90	131.41
631	41.41	168.46	3.31	4.33	18.70	131.53
632	41.49	172.42	3.40	4.33	18.49	131.79
633	41.55	174.59	3.46	4.33	18.41	131.94
634	41.61	176.37	3.52	4.33	18.40	132.10
635	41.68	177.98	3.60	4.33	18.44	132.28
636	41.73	179.58	3.68	4.33	18.50	132.46
637	41.83	182.68	3.82	4.33	18.57	132.79
638	41.89	184.66	3.93	4.33	18.64	133.01
639	41.95	187.30	4.01	4.33	18.58	133.20
640	42.01	189.37	4.09	4.33	18.55	133.36
641	42.06	190.78	4.11	4.33	18.46	133.42
642	42.16	190.12	4.05	4.33	18.41	133.31
643	42.22	187.86	4.08	4.33	18.77	133.32
644	42.28	184.66	4.10	4.33	19.26	133.33
645	42.34	180.99	4.10	4.44	19.73	133.27
646	42.40	177.50	4.06	4.33	20.10	133.15
647	42.48	164.23	3.97	4.33	21.79	132.81
648	42.54	166.96	3.91	4.33	21.20	132.73
649	42.60	163.00	3.86	4.33	21.66	132.58
650	42.66	158.77	3.82	4.33	22.22	132.44
651	42.72	154.43	3.78	4.44	22.81	132.29
652	42.78	150.29	3.71	4.44	23.32	132.09
653	42.87	145.77	3.62	4.44	23.87	131.85
654	42.93	143.42	3.57	4.21	24.13	131.69
655	42.99	142.57	3.52	4.21	24.13	131.58
656	43.05	142.19	3.49	4.21	24.11	131.51
657	43.11	142.29	3.47	4.21	24.02	131.46
658	43.20	142.76	3.43	4.21	23.84	131.40
659	43.26	142.66	3.41	4.33	23.80	131.36
660	43.32	142.66	3.41	4.33	23.80	131.34
661	43.38	142.19	3.41	4.44	23.93	131.34
662	43.44	140.40	3.40	4.33	24.25	131.29
663	43.51	138.33	3.38	4.33	24.61	131.21
664	43.59	134.94	3.34	4.33	25.17	131.07
665	43.65	132.68	3.30	4.33	25.48	130.92
666	43.71	130.04	3.25	4.33	25.87	130.77
667	43.77	127.50	3.19	4.33	26.20	130.58
668	43.83	124.30	3.12	4.21	26.69	130.37
669	43.92	118.37	3.02	4.21	27.69	129.99
670	43.98	113.19	2.95	4.21	28.76	129.73
671	44.05	106.13	2.93	4.21	30.66	129.50
672	44.10	97.84	2.69	4.21	32.08	128.70

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.16	88.71	2.47	4.21	34.09	127.84
674	44.23	80.42	2.49	4.21	37.70	127.65
675	44.32	70.72	2.49	4.16	42.23	127.33
676	44.38	65.92	2.49	4.21	44.75	127.15
677	44.43	60.74	2.49	3.99	47.81	126.96
678	44.49	68.08	2.50	4.21	43.71	127.26
679	44.57	67.71	2.48	4.21	43.82	127.19
680	44.63	68.18	2.47	4.21	43.53	127.18
681	44.70	65.92	2.44	4.10	44.59	127.01
682	44.77	68.27	2.43	4.10	43.32	127.08
683	44.82	69.78	2.44	4.10	42.61	127.15
684	44.88	73.26	2.41	4.10	40.81	127.19
685	44.97	80.42	2.49	4.21	38.10	127.65
686	45.03	90.49	2.55	4.33	34.31	128.12
687	45.10	102.83	2.61	4.21	30.46	128.60
688	45.16	112.15	2.66	4.21	28.07	128.95
689	45.22	116.30	2.68	4.21	27.08	129.09
690	45.28	118.56	2.65	4.21	26.38	129.04
691	45.37	122.32	2.61	4.21	25.31	129.00
692	45.43	124.96	2.60	4.21	24.72	129.05
693	45.49	127.88	2.60	4.21	24.10	129.10
694	45.55	131.08	2.62	4.21	23.53	129.22
695	45.61	135.51	2.67	4.21	22.90	129.44
696	45.67	140.03	2.71	4.21	22.24	129.63
697	45.76	142.95	2.78	4.21	21.99	129.84
698	45.82	142.10	2.78	4.21	22.19	129.85
699	45.88	139.18	2.76	4.21	22.66	129.74
700	45.94	135.60	2.71	4.10	23.15	129.53
701	46.00	131.17	2.63	4.10	23.69	129.23
702	46.09	125.34	2.50	4.10	24.35	128.75
703	46.15	122.51	2.44	4.10	24.72	128.53
704	46.21	119.12	2.40	4.10	25.33	128.35
705	46.27	115.35	2.37	3.99	26.11	128.17
706	46.33	111.02	2.37	3.99	27.26	128.08
707	46.42	104.81	2.46	3.99	29.59	128.22
708	46.48	101.98	1.97	3.99	27.44	126.53
709	46.54	100.10	1.50	3.87	24.64	124.49
710	46.60	99.82	1.59	3.87	25.37	124.87
711	46.66	100.38	1.65	3.76	25.68	125.16
712	46.72	100.01	1.69	3.76	26.17	125.36
713	46.80	92.28	1.74	3.76	28.99	125.36
714	46.86	95.01	1.76	3.42	28.30	125.54
715	46.93	95.39	1.79	3.30	28.36	125.63
716	46.98	94.07	1.81	3.30	28.99	125.70
717	47.07	88.33	1.85	3.30	31.35	125.71
718	47.13	83.53	1.86	3.30	33.29	125.59
719	47.19	79.01	1.83	3.42	35.04	125.36
720	47.25	74.58	1.79	3.30	36.78	125.04

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.31	70.06	1.78	3.30	38.99	124.87
722	47.40	62.90	1.78	3.19	42.68	124.60
723	47.46	57.16	1.78	3.19	46.14	124.36
724	47.52	50.00	1.75	3.19	51.02	123.89
725	47.58	43.32	1.67	3.19	56.27	123.24
726	47.64	37.86	1.61	3.08	61.62	122.64
727	47.73	31.73	1.49	3.30	68.58	121.61
728	47.79	29.19	1.37	3.30	71.23	120.81
729	47.85	30.13	1.23	3.53	67.57	120.12
730	47.91	34.47	1.10	3.42	59.09	119.58
731	47.97	40.40	1.01	3.76	51.01	119.36
732	48.03	46.61	1.01	3.76	45.52	119.70
733	48.12	50.76	1.01	3.76	42.48	119.91
734	48.18	50.85	1.05	3.53	43.00	120.21
735	48.24	48.50	1.16	3.53	46.21	120.85
736	48.30	44.45	1.28	3.53	51.04	121.33
737	48.36	39.93	1.34	3.53	56.29	121.40
738	48.45	34.94	1.27	3.53	61.38	120.70
739	48.51	35.08	1.15	3.53	59.53	120.00
740	48.57	35.08	1.10	3.53	58.75	119.66
741	48.63	35.22	1.10	3.76	58.63	119.68
742	48.69	36.91	1.10	3.53	56.62	119.81
743	48.78	35.31	0.91	3.76	55.35	118.25
744	48.84	33.43	1.10	3.65	61.09	119.54
745	48.90	32.58	1.29	3.76	65.19	120.63
746	48.96	33.52	1.42	3.76	65.64	121.38
747	49.03	34.65	1.50	3.76	65.15	121.87
748	49.09	35.60	1.55	3.76	64.56	122.20
749	49.15	30.89	1.66	3.76	73.08	122.35
750	49.21	57.63	1.75	3.87	46.33	124.25
751	49.30	75.71	1.90	3.87	38.05	125.50
752	49.36	93.60	2.03	3.87	31.72	126.53
753	49.42	103.02	2.17	3.87	29.57	127.26
754	49.48	116.77	2.31	3.87	26.57	128.02
755	49.55	132.49	2.42	3.87	23.55	128.66
756	49.61	143.42	2.47	3.87	21.68	128.99
757	49.70	157.45	1.72	3.87	15.73	126.59
758	49.76	164.23	1.62	3.87	14.31	126.24
759	49.82	168.56	1.74	3.87	14.42	126.84
760	49.88	170.44	1.87	3.65	14.85	127.40
761	49.94	171.29	1.99	3.65	15.32	127.86
762	50.00	169.88	2.09	3.65	15.96	128.19
763	50.07	156.22	2.15	2.85	18.19	128.20
764	50.14	162.16	2.20	2.85	17.58	128.47
765	50.20	163.94	2.25	2.85	17.53	128.63
766	50.27	164.23	2.17	2.96	17.15	128.37
767	50.34	164.70	1.69	2.96	14.75	126.55
768	50.41	166.96	2.02	3.08	16.12	127.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.46	165.17	2.09	2.96	16.69	128.11
770	50.54	161.40	2.17	2.96	17.62	128.33
771	50.61	158.86	2.24	2.96	18.36	128.54
772	50.67	156.55	2.32	2.96	19.09	128.75
773	50.74	151.70	2.42	3.08	20.36	128.99
774	50.79	154.43	2.48	3.08	20.19	129.21
775	50.85	154.62	2.53	3.08	20.39	129.35
776	50.94	154.53	2.62	3.08	20.84	129.61
777	51.01	154.72	2.69	3.08	21.12	129.80
778	51.06	154.81	2.70	3.08	21.19	129.84
779	51.13	155.09	2.71	3.08	21.20	129.87
780	51.18	156.13	2.75	3.08	21.24	130.01
781	51.27	158.11	2.78	3.08	21.03	130.10
782	51.33	159.42	2.76	3.08	20.77	130.08
783	51.38	158.77	2.75	3.08	20.83	130.02
784	51.46	158.39	2.73	3.08	20.82	129.96
785	51.52	158.20	2.72	3.08	20.86	129.95
786	51.58	157.16	2.61	3.08	20.57	129.64
787	51.64	156.51	2.42	3.08	19.82	129.05
788	51.73	159.14	2.61	3.08	20.27	129.65
789	51.79	163.47	2.66	3.19	19.85	129.87
790	51.85	170.07	2.69	3.19	19.00	130.03
791	51.91	177.79	2.67	3.19	17.89	130.10
792	51.98	164.79	2.66	3.08	19.68	129.87
793	52.05	186.54	2.69	3.08	16.89	130.26
794	52.10	187.67	2.71	3.08	16.86	130.34
795	52.18	187.11	2.73	3.08	16.99	130.37
796	52.23	186.64	2.71	3.08	17.00	130.32
797	52.31	186.45	2.66	3.08	16.84	130.18
798	52.36	184.10	2.63	3.08	17.04	130.07
799	52.44	179.48	2.66	3.08	17.75	130.08
800	52.51	174.87	2.65	3.08	18.37	130.01
801	52.57	171.67	2.65	2.96	18.80	129.94
802	52.63	169.69	2.64	2.96	19.07	129.89
803	52.72	162.91	2.63	2.96	20.07	129.77
804	52.77	158.48	2.61	2.96	20.68	129.64
805	52.84	154.25	2.58	2.96	21.27	129.49
806	52.90	150.10	2.57	2.96	21.98	129.40
807	52.95	146.15	2.57	2.96	22.70	129.33
808	53.04	140.31	2.56	2.96	23.79	129.20
809	53.10	137.58	2.55	2.96	24.31	129.13
810	53.16	135.51	2.53	2.96	24.63	129.03
811	53.23	133.81	2.49	2.96	24.84	128.90
812	53.29	132.59	2.48	2.96	25.03	128.83
813	53.35	131.55	2.46	2.96	25.19	128.76
814	53.44	129.29	2.43	3.08	25.55	128.63
815	53.50	126.94	2.42	2.96	26.05	128.56
816	53.56	122.23	2.40	2.96	27.09	128.39

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.62	117.24	2.35	2.96	28.13	128.15
818	53.67	117.57	2.30	2.96	27.76	128.00
819	53.76	115.83	2.22	2.96	27.76	127.70
820	53.82	117.90	2.14	2.96	26.78	127.49
821	53.88	117.80	1.95	2.96	25.61	126.80
822	53.94	117.14	1.74	2.85	24.36	125.94
823	54.00	115.73	1.77	2.85	24.93	126.04
824	54.09	112.44	1.78	2.85	25.87	126.01
825	54.16	109.99	1.81	2.85	26.77	126.07
826	54.22	106.88	1.85	2.96	27.95	126.17
827	54.27	100.19	1.88	2.96	30.25	126.14
828	54.34	101.42	1.93	3.08	30.19	126.34
829	54.41	102.36	1.97	2.96	30.18	126.51
830	54.47	104.81	1.98	2.96	29.51	126.62
831	54.56	109.42	1.91	2.96	27.71	126.46
832	54.62	111.68	1.84	2.85	26.62	126.24
833	54.68	111.31	1.79	2.96	26.33	126.01
834	54.74	110.27	1.76	2.85	26.41	125.86
835	54.80	108.76	1.74	2.96	26.78	125.78
836	54.86	106.79	1.74	2.96	27.31	125.72
837	54.95	103.21	1.73	2.96	28.28	125.57
838	55.01	100.85	1.73	2.96	29.04	125.52
839	55.07	98.22	1.73	2.96	29.92	125.47
840	55.13	96.80	1.74	2.96	30.51	125.49
841	55.19	98.31	1.76	2.96	30.17	125.61
842	55.28	97.84	1.76	2.96	30.32	125.58
843	55.34	98.40	1.72	2.85	29.82	125.42
844	55.40	99.25	1.71	2.96	29.50	125.41
845	55.45	100.38	1.72	2.85	29.23	125.48
846	55.51	100.76	1.71	2.96	29.02	125.44
847	55.60	100.29	1.74	2.96	29.46	125.58
848	55.66	99.25	1.79	2.96	30.19	125.75
849	55.73	98.03	1.88	2.96	31.25	126.07
850	55.79	97.18	1.98	2.96	32.28	126.42
851	55.84	98.59	2.04	2.96	32.28	126.70
852	55.94	107.44	2.08	2.96	29.67	127.03
853	56.00	115.92	1.99	2.96	26.72	126.89
854	56.06	124.77	1.88	2.96	23.87	126.66
855	56.12	131.36	1.74	2.96	21.56	126.21
856	56.18	137.95	1.65	2.96	19.73	125.94
857	56.24	141.72	1.64	3.08	19.01	125.96
858	56.30	143.42	1.61	3.08	18.59	125.89
859	56.39	146.05	1.61	3.08	18.16	125.93
860	56.43	146.01	1.62	3.08	18.23	125.97
861	56.50	145.96	1.66	3.08	18.45	126.12
862	56.56	149.07	1.71	3.08	18.24	126.39
863	56.65	150.01	1.80	3.08	18.62	126.78
864	56.71	149.91	1.86	3.08	19.02	127.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.77	149.44	1.92	3.08	19.41	127.25
866	56.84	149.25	1.95	3.08	19.62	127.36
867	56.89	149.54	1.96	3.08	19.66	127.42
868	56.98	151.04	1.98	3.08	19.51	127.51
869	57.04	152.27	2.00	3.08	19.40	127.59
870	57.10	153.30	2.02	3.08	19.39	127.71
871	57.16	154.53	2.05	3.08	19.34	127.83
872	57.22	156.41	2.08	3.08	19.18	127.94
873	57.31	161.97	2.09	3.08	18.41	128.08
874	57.37	166.39	2.09	3.08	17.77	128.14
875	57.43	171.67	2.10	3.08	17.08	128.24
876	57.49	176.00	2.12	3.08	16.62	128.38
877	57.55	179.48	2.14	3.08	16.29	128.50
878	57.61	182.21	2.15	2.96	15.99	128.57
879	57.70	186.26	2.16	3.08	15.56	128.66
880	57.76	188.43	2.18	2.96	15.39	128.74
881	57.82	190.31	2.21	3.08	15.34	128.89
882	57.88	191.72	2.25	3.19	15.33	129.02
883	57.94	194.08	2.28	3.19	15.22	129.16
884	58.03	197.66	2.34	3.19	15.06	129.38
885	58.09	199.82	2.39	3.19	15.03	129.56
886	58.16	201.52	2.44	3.19	15.06	129.74
887	58.22	204.06	2.50	3.19	15.01	129.94
888	58.28	207.45	2.55	3.19	14.89	130.15
889	58.34	211.59	2.60	3.19	14.63	130.31
890	58.42	217.43	2.65	3.19	14.28	130.54
891	58.48	219.22	2.71	3.30	14.31	130.72
892	58.55	220.63	2.77	3.19	14.37	130.88
893	58.60	222.70	2.82	3.30	14.35	131.03
894	58.67	225.25	2.85	3.30	14.23	131.14
895	58.75	229.67	2.88	3.42	13.93	131.26
896	58.81	232.69	2.94	3.42	13.88	131.46
897	58.87	235.32	2.52	3.42	12.29	130.37
898	58.94	238.34	2.01	3.53	10.23	128.72
899	59.00	240.22	2.13	3.53	10.56	129.19
900	59.06	241.16	2.25	3.53	10.89	129.57
901	59.15	240.31	2.38	3.53	11.43	129.99
902	59.20	227.88	2.45	3.53	12.68	130.06
903	59.27	227.93	2.52	3.53	12.95	130.29
904	59.32	227.98	2.58	3.53	13.15	130.45
905	59.40	231.56	2.69	3.53	13.24	130.81
906	59.46	235.13	2.83	3.53	13.36	131.19
907	59.53	239.56	2.94	3.53	13.37	131.53
908	59.58	242.20	3.00	3.53	13.34	131.71
909	59.66	246.25	3.08	3.76	13.25	131.94
910	59.73	250.01	3.17	3.65	13.21	132.17
911	59.79	252.08	2.62	3.87	11.40	130.81
912	59.86	253.31	1.13	3.65	5.00	124.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.93	254.53	1.24	3.76	5.00	125.35
914	59.98	253.97	1.31	3.65	6.56	125.76
915	60.05	253.03	1.41	3.65	7.02	126.27
916	60.12	250.20	1.54	3.65	7.71	126.88
917	60.19	234.10	1.75	3.30	9.64	127.65
918	60.24	240.78	1.92	3.30	9.86	128.44
919	60.32	238.71	2.26	3.30	11.24	129.58
920	60.38	235.51	2.44	3.30	12.12	130.11
921	60.44	232.31	2.56	3.30	12.84	130.45
922	60.50	231.27	2.67	3.30	13.31	130.75
923	60.59	231.56	2.79	3.42	13.68	131.05
924	60.65	231.27	2.84	3.42	13.88	131.19
925	60.71	229.58	2.88	3.42	14.15	131.26
926	60.77	227.32	2.90	3.42	14.44	131.29
927	60.83	226.28	2.89	3.42	14.52	131.26
928	60.89	227.98	2.87	3.42	14.31	131.24
929	60.98	234.10	2.86	3.30	13.73	131.27
930	61.04	237.77	2.85	3.30	13.40	131.29
931	61.10	240.50	2.87	3.30	13.21	131.35
932	61.16	241.82	2.90	3.30	13.21	131.44
933	61.22	242.10	2.91	3.42	13.24	131.48
934	61.31	242.15	2.91	3.42	13.24	131.47
935	61.37	241.73	2.92	3.30	13.31	131.49
936	61.43	242.20	2.93	3.30	13.32	131.54
937	61.49	242.76	2.95	3.53	13.33	131.58
938	61.55	243.14	2.96	3.53	13.33	131.60
939	61.64	244.27	2.94	3.53	13.20	131.58
940	61.70	245.78	2.92	3.65	13.02	131.54
941	61.76	248.04	2.90	3.65	12.77	131.50
942	61.82	250.20	2.72	3.65	12.06	131.07
943	61.88	252.46	2.36	3.65	10.74	130.06
944	61.94	254.25	2.43	3.65	10.85	130.29
945	62.04	255.38	2.47	3.76	10.88	130.39
946	62.10	256.51	2.48	3.65	10.87	130.46
947	62.16	260.65	2.50	3.76	10.64	130.55
948	62.22	260.89	2.50	3.65	10.63	130.55
949	62.29	261.12	2.46	3.76	10.49	130.43
950	62.34	266.68	2.43	3.76	10.03	130.40
951	62.43	269.60	2.43	3.76	9.83	130.41
952	62.49	270.07	2.43	3.87	9.81	130.42
953	62.55	270.54	2.44	3.87	9.83	130.46
954	62.61	271.48	2.47	3.76	9.87	130.56
955	62.67	272.42	2.47	3.76	9.82	130.57
956	62.73	271.39	2.43	3.76	9.76	130.43
957	62.82	270.16	2.40	3.76	9.76	130.34
958	62.88	269.32	2.39	3.99	9.79	130.31
959	62.94	268.75	2.37	3.99	9.76	130.23
960	63.00	268.75	2.36	3.99	9.72	130.19

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	63.06	268.19	2.35	3.99	9.73	130.16
962	63.12	266.12	2.34	3.99	9.85	130.12
963	63.21	264.33	2.32	3.99	9.90	130.02
964	63.27	262.54	2.28	3.99	9.91	129.90
965	63.33	259.90	2.23	3.99	9.92	129.71
966	63.40	253.97	2.16	3.99	10.09	129.42
967	63.46	246.72	2.08	3.87	10.32	129.08
968	63.55	229.39	1.97	3.87	11.23	128.50
969	63.60	213.95	1.94	3.87	12.42	128.20
970	63.66	196.24	1.96	3.65	14.29	128.08
971	63.73	179.01	1.95	3.65	16.28	127.83
972	63.78	164.32	1.94	3.65	18.22	127.56
973	63.87	141.82	2.07	3.65	22.80	127.68
974	63.94	128.73	2.25	3.65	26.71	128.06
975	63.99	114.60	2.47	3.65	31.78	128.47
976	64.05	97.65	2.45	3.65	36.85	128.00
977	64.12	81.17	2.21	3.42	41.55	126.80
978	64.18	69.21	2.29	3.42	47.95	126.68
979	64.27	64.32	2.28	3.53	50.73	126.45
980	64.33	61.49	2.27	3.76	52.53	126.33
981	64.39	55.75	2.29	4.10	56.80	126.15
982	64.44	55.65	2.33	4.21	57.18	126.26
983	64.51	66.67	2.33	4.67	49.69	126.69
984	64.57	83.62	2.28	5.47	41.07	127.11
985	64.63	109.70	2.23	6.38	31.87	127.59
986	64.72	147.47	2.18	5.81	22.43	128.15
987	64.79	162.81	2.16	5.58	19.75	128.34
988	64.85	173.74	2.12	5.70	17.94	128.36
989	64.91	181.65	2.13	5.58	16.91	128.48
990	64.96	187.30	2.23	5.35	16.66	128.89
991	65.05	196.06	2.48	5.35	16.71	129.80
992	65.11	203.21	2.65	5.47	16.56	130.38
993	65.18	210.27	2.72	5.47	16.05	130.65
994	65.23	219.03	2.73	5.47	15.16	130.75
995	65.29	228.64	2.73	5.47	14.26	130.87
996	65.38	243.14	2.76	5.47	13.11	131.10
997	65.44	251.05	2.77	5.58	12.51	131.20
998	65.50	257.55	2.78	5.47	12.05	131.29
999	65.56	262.35	2.81	5.47	11.78	131.41
1000	65.63	266.30	2.82	5.47	11.55	131.48
1001	65.69	269.13	2.83	5.47	11.40	131.54
1002	65.77	273.65	2.87	5.47	11.20	131.67
1003	65.83	277.23	2.91	5.47	11.08	131.81
1004	65.89	283.25	2.94	5.58	10.79	131.94
1005	65.95	290.50	2.96	5.47	10.40	132.05
1006	66.01	296.15	2.98	5.47	10.11	132.15
1007	66.10	301.81	2.98	5.81	9.80	132.20
1008	66.16	303.69	3.06	5.81	9.89	132.39

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	66.23	303.69	2.67	5.81	8.86	131.40
1010	66.29	300.96	2.31	5.47	7.98	130.30
1011	66.35	297.00	2.36	5.47	8.35	130.44
1012	66.41	292.76	2.40	5.58	8.69	130.52
1013	66.47	288.25	2.44	5.47	9.08	130.61
1014	66.54	261.03	2.46	5.47	10.89	130.44
1015	66.62	262.16	2.46	5.47	10.81	130.44
1016	66.69	253.40	2.43	5.41	11.36	130.28
1017	66.75	244.46	2.45	5.35	12.11	130.25
1018	66.81	233.25	2.53	5.35	13.33	130.37
1019	66.86	222.89	2.61	5.24	14.57	130.49
1020	66.95	209.24	2.73	5.24	16.40	130.65
1021	67.01	202.36	2.78	5.01	17.38	130.70
1022	67.07	196.34	2.78	5.13	18.11	130.63
1023	67.13	191.63	2.75	5.01	18.59	130.49
1024	67.19	186.83	2.72	5.01	19.11	130.34
1025	67.28	179.58	2.67	5.01	19.95	130.13
1026	67.34	174.49	2.67	5.01	20.67	130.04
1027	67.40	170.16	2.66	5.01	21.32	129.96
1028	67.46	166.77	2.66	5.01	21.87	129.91
1029	67.52	164.42	2.66	5.01	22.27	129.88
1030	67.61	167.01	2.67	5.01	21.89	129.94
1031	67.67	164.98	2.67	5.01	22.24	129.91
1032	67.73	167.24	2.67	4.90	21.87	129.94
1033	67.79	171.85	2.69	4.90	21.23	130.05
1034	67.85	177.79	2.67	4.90	20.29	130.10
1035	67.94	187.58	2.53	4.90	18.34	129.83
1036	68.00	193.51	2.45	5.01	17.25	129.66
1037	68.06	197.66	2.39	5.01	16.51	129.53
1038	68.12	200.39	2.01	5.01	14.61	128.32
1039	68.18	202.36	1.49	5.01	11.90	126.13
1040	68.24	204.81	1.60	5.01	12.25	126.70
1041	68.33	208.67	1.77	5.01	12.69	127.49
1042	68.39	212.16	1.79	5.01	12.46	127.60
1043	68.45	215.55	1.80	5.01	12.21	127.70
1044	68.51	215.50	1.88	5.01	12.54	127.98
1045	68.59	215.45	1.98	5.01	13.01	128.39
1046	68.65	219.41	2.07	5.01	13.03	128.76
1047	68.70	223.65	2.21	5.13	13.20	129.28
1048	68.80	232.22	2.43	5.13	13.26	130.06
1049	68.86	236.92	2.53	5.13	13.23	130.41
1050	68.92	240.41	2.64	5.13	13.31	130.74
1051	68.97	243.33	2.76	5.13	13.46	131.09
1052	69.04	245.12	2.88	5.24	13.70	131.42
1053	69.10	246.25	2.97	5.13	13.91	131.66
1054	69.19	250.01	3.08	5.13	13.94	131.96
1055	69.25	253.87	3.15	5.13	13.84	132.16
1056	69.31	256.98	3.21	5.13	13.78	132.34

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	69.36	259.24	3.26	5.13	13.76	132.48
1058	69.42	262.25	3.33	5.13	13.72	132.66
1059	69.51	265.74	3.47	5.24	13.84	132.99
1060	69.57	268.85	3.55	5.24	13.82	133.18
1061	69.63	271.48	3.66	5.24	13.93	133.43
1062	69.69	274.59	3.24	5.24	12.57	132.58
1063	69.75	277.13	2.62	5.13	10.61	131.05
1064	69.84	277.32	2.79	5.35	11.09	131.49
1065	69.89	263.95	2.84	5.35	12.19	131.50
1066	69.96	273.55	2.87	5.13	11.60	131.66
1067	70.02	271.53	2.85	5.24	11.68	131.60
1068	70.08	258.30	2.79	5.01	12.49	131.33
1069	70.15	269.51	2.67	5.01	11.30	131.11
1070	70.21	280.52	2.47	5.01	9.97	130.65
1071	70.28	300.02	2.30	5.01	8.31	130.27
1072	70.35	323.93	2.17	4.90	6.77	130.04
1073	70.41	353.13	2.00	5.24	5.12	129.66
1074	70.48	375.91	1.90	5.24	4.07	129.42
1075	70.55	388.81	1.90	5.24	3.68	129.50
1076	70.61	392.68	1.91	5.24	3.60	129.56
1077	70.68	389.95	1.93	5.24	3.74	129.63
1078	70.74	380.25	1.94	5.35	4.07	129.62
1079	70.81	374.13	2.00	5.35	4.42	129.80
1080	70.88	373.75	2.03	5.35	4.50	129.89
1081	70.95	375.16	2.03	5.35	4.45	129.90
1082	71.00	377.80	2.03	5.35	4.37	129.91
1083	71.08	387.12	2.00	5.35	4.02	129.88
1084	71.14	396.07	1.95	5.47	3.62	129.73
1085	71.20	404.45	1.91	5.47	3.30	129.65
1086	71.29	411.42	1.53	5.70	2.19	128.06
1087	71.35	415.37	1.39	5.58	1.76	127.40
1088	71.41	415.65	1.46	5.47	1.93	127.76
1089	71.47	413.49	1.55	5.92	2.20	128.18
1090	71.53	409.72	1.68	5.47	2.61	128.73
1091	71.59	404.45	1.81	5.81	3.06	129.24
1092	71.66	362.45	1.82	5.58	4.37	129.03
1093	71.72	380.15	1.86	5.58	3.92	129.31
1094	71.79	382.41	1.87	6.15	3.87	129.36
1095	71.86	381.38	1.87	6.38	3.90	129.34
1096	71.92	375.44	1.89	6.72	4.15	129.39
1097	71.98	372.62	1.90	6.49	4.27	129.42
1098	72.06	370.17	1.90	5.81	4.36	129.41
1099	72.13	367.16	1.89	6.49	4.42	129.33
1100	72.19	365.27	1.91	5.70	4.56	129.41
1101	72.26	363.95	1.96	6.49	4.74	129.59
1102	72.32	363.95	2.01	6.49	4.87	129.77
1103	72.38	363.95	2.05	6.49	4.96	129.89
1104	72.45	366.12	2.06	6.61	4.92	129.94

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	72.51	368.57	2.06	6.61	4.84	129.97
1106	72.58	371.68	2.07	6.61	4.76	130.02
1107	72.65	374.78	2.08	6.61	4.70	130.08
1108	72.72	376.86	2.09	6.61	4.65	130.13
1109	72.77	377.70	2.10	6.61	4.65	130.16
1110	72.84	378.27	2.07	6.61	4.57	130.07
1111	72.92	378.65	1.99	6.26	4.36	129.79
1112	72.98	377.14	1.70	6.26	3.63	128.62
1113	73.04	373.47	1.41	6.04	2.95	127.25
1114	73.11	365.46	1.47	5.92	3.36	127.50
1115	73.17	359.15	1.53	5.92	3.72	127.72
1116	73.24	355.39	1.57	6.15	3.97	127.91
1117	73.30	352.00	1.60	6.83	4.18	128.01
1118	73.37	332.97	1.60	6.83	4.88	127.87
1119	73.44	340.70	1.59	6.83	4.57	127.90
1120	73.49	339.47	1.61	6.61	4.68	127.98
1121	73.57	339.52	1.65	6.72	4.79	128.14
1122	73.63	339.09	1.69	6.72	4.93	128.31
1123	73.70	339.57	1.70	6.72	4.96	128.37
1124	73.77	342.30	1.67	6.72	4.77	128.25
1125	73.83	346.06	1.67	6.04	4.62	128.27
1126	73.89	347.85	1.66	6.15	4.55	128.26
1127	73.95	351.34	1.65	6.15	4.41	128.25
1128	74.04	358.40	1.61	6.38	4.02	128.09
1129	74.10	360.94	1.56	6.15	3.80	127.88
1130	74.16	361.79	1.55	6.26	3.74	127.83
1131	74.22	361.88	1.44	6.26	3.43	127.32
1132	74.28	363.48	1.15	6.26	2.50	125.69
1133	74.37	362.35	1.15	6.26	2.54	125.69
1134	74.43	358.87	1.20	6.26	2.80	125.97
1135	74.49	354.07	1.25	6.26	3.09	126.21
1136	74.55	347.76	1.32	6.38	3.51	126.55
1137	74.62	306.80	1.38	6.26	5.00	126.58
1138	74.67	330.34	1.37	6.15	4.30	126.74
1139	74.75	329.30	1.35	6.26	4.27	126.61
1140	74.82	332.13	1.39	7.06	4.31	126.86
1141	74.88	336.84	1.45	6.49	4.33	127.18
1142	74.94	337.31	1.47	6.15	4.37	127.27
1143	75.00	340.88	1.50	6.83	4.33	127.44
1144	75.07	347.48	1.57	6.38	4.34	127.83
1145	75.14	357.46	0.00	7.18	100.00	87.36
1146	75.21	364.52	0.00	7.23	100.00	87.36
1147	75.28	368.29	0.00	6.26	100.00	87.36
1148	75.33	369.98	0.00	7.29	100.00	87.36
1149	75.41	362.73	0.00	7.41	100.00	87.36
1150	75.48	353.50	0.00	7.18	100.00	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.07	0.00	0.00	0.00	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
2	0.14	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
3	0.21	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
4	0.28	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
5	0.33	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
6	0.40	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
7	0.47	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
8	0.53	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
9	0.59	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
10	0.67	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
11	0.73	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
12	0.81	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
13	0.87	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
14	0.93	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
15	1.00	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
16	1.06	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
17	1.13	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
18	1.19	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
19	1.26	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
20	1.33	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
21	1.39	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
22	1.45	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
23	1.51	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
24	1.59	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
25	1.64	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
26	1.72	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
27	1.77	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
28	1.84	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
29	1.92	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
30	1.97	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
31	2.05	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
32	2.10	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
33	2.18	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
34	2.24	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
35	2.30	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
36	2.38	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
37	2.44	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
38	2.50	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
39	2.58	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
40	2.64	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
41	2.69	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
42	2.77	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
43	2.83	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
44	2.89	0.17	0.00	0.17	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
45	2.97	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
46	3.03	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
47	3.08	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
48	3.16	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	3.22	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
50	3.29	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
51	3.36	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
52	3.42	0.21	0.00	0.21	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
53	3.48	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
54	3.55	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
55	3.62	0.22	0.00	0.22	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
56	3.69	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
57	3.75	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
58	3.81	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
59	3.89	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
60	3.95	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
61	4.00	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
62	4.08	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
63	4.14	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
64	4.20	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
65	4.28	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
66	4.33	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
67	4.41	0.27	0.00	0.27	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
68	4.47	0.27	0.00	0.27	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
69	4.53	0.27	0.00	0.27	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
70	4.61	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
71	4.67	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
72	4.74	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
73	4.80	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
74	4.86	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
75	4.94	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
76	5.00	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
77	5.05	0.31	0.00	0.31	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
78	5.13	0.31	0.00	0.31	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
79	5.19	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
80	5.25	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
81	5.33	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
82	5.39	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
83	5.45	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
84	5.53	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
85	5.59	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
86	5.65	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
87	5.72	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
88	5.78	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
89	5.86	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
90	5.92	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
91	5.98	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
92	6.04	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
93	6.12	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
94	6.18	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
95	6.24	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
96	6.31	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	6.37	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
98	6.43	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
99	6.51	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
100	6.57	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
101	6.65	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
102	6.71	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
103	6.77	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
104	6.83	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
105	6.90	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
106	6.96	0.42	0.00	0.42	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
107	7.03	0.42	0.00	0.42	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
108	7.09	0.42	0.00	0.42	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
109	7.17	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
110	7.22	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
111	7.28	0.44	0.00	0.44	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
112	7.36	0.44	0.00	0.44	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
113	7.42	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
114	7.50	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
115	7.55	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
116	7.61	0.46	0.00	0.46	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
117	7.70	0.46	0.00	0.46	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
118	7.75	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
119	7.81	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
120	7.89	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
121	7.95	0.48	0.00	0.48	0.98	0.493	1.05	0.468	1.10	1.30	2.000	No
122	8.01	0.48	0.00	0.48	0.98	0.493	1.05	0.468	1.10	1.30	0.558	No
123	8.08	0.49	0.00	0.48	0.98	0.495	1.05	0.470	1.10	1.30	0.560	No
124	8.14	0.49	0.00	0.49	0.98	0.497	1.05	0.471	1.10	1.30	0.561	No
125	8.22	0.50	0.01	0.49	0.98	0.500	1.05	0.474	1.10	1.30	0.563	No
126	8.28	0.50	0.01	0.49	0.98	0.501	1.05	0.475	1.10	1.30	0.564	No
127	8.34	0.50	0.01	0.49	0.98	0.503	1.05	0.477	1.10	1.30	0.565	No
128	8.40	0.51	0.01	0.49	0.98	0.505	1.05	0.479	1.10	1.30	0.566	No
129	8.48	0.51	0.01	0.50	0.98	0.507	1.05	0.481	1.10	1.30	0.569	No
130	8.54	0.52	0.02	0.50	0.98	0.509	1.05	0.482	1.10	1.30	0.572	No
131	8.60	0.52	0.02	0.50	0.98	0.510	1.05	0.484	1.10	1.30	0.575	No
132	8.68	0.52	0.02	0.50	0.98	0.512	1.05	0.486	1.10	1.30	0.579	No
133	8.74	0.53	0.02	0.50	0.98	0.514	1.05	0.488	1.10	1.30	0.582	No
134	8.79	0.53	0.02	0.51	0.98	0.516	1.05	0.489	1.10	1.30	0.584	No
135	8.87	0.54	0.03	0.51	0.98	0.518	1.05	0.491	1.10	1.30	0.587	No
136	8.93	0.54	0.03	0.51	0.98	0.519	1.05	0.493	1.10	1.30	0.589	No
137	8.99	0.54	0.03	0.51	0.98	0.521	1.05	0.494	1.10	1.30	0.591	No
138	9.07	0.55	0.03	0.52	0.98	0.523	1.05	0.496	1.10	1.30	0.593	No
139	9.13	0.55	0.04	0.52	0.98	0.525	1.05	0.497	1.10	1.30	0.595	No
140	9.19	0.56	0.04	0.52	0.98	0.526	1.05	0.499	1.10	1.30	0.597	No
141	9.27	0.56	0.04	0.52	0.98	0.528	1.05	0.501	1.10	1.30	0.600	No
142	9.33	0.56	0.04	0.52	0.98	0.530	1.05	0.502	1.10	1.30	0.602	No
143	9.39	0.57	0.04	0.53	0.98	0.531	1.05	0.504	1.10	1.30	0.604	No
144	9.46	0.57	0.05	0.53	0.98	0.533	1.05	0.506	1.10	1.30	0.608	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	9.52	0.58	0.05	0.53	0.98	0.534	1.05	0.507	1.10	1.30	0.611	No
146	9.58	0.58	0.05	0.53	0.98	0.536	1.05	0.508	1.10	1.30	0.615	No
147	9.66	0.59	0.05	0.53	0.98	0.538	1.05	0.510	1.09	1.30	0.619	No
148	9.72	0.59	0.05	0.54	0.98	0.539	1.05	0.511	1.09	1.30	0.623	No
149	9.78	0.59	0.06	0.54	0.98	0.541	1.05	0.513	1.09	1.30	0.626	No
150	9.86	0.60	0.06	0.54	0.98	0.543	1.05	0.515	1.09	1.30	0.630	No
151	9.91	0.60	0.06	0.54	0.98	0.544	1.05	0.516	1.09	1.30	0.633	No
152	9.97	0.60	0.06	0.54	0.98	0.545	1.05	0.517	1.09	1.30	0.635	No
153	10.04	0.61	0.06	0.55	0.98	0.547	1.05	0.519	1.08	1.30	0.639	No
154	10.12	0.61	0.07	0.55	0.98	0.549	1.05	0.520	1.09	1.30	0.638	No
155	10.18	0.62	0.07	0.55	0.98	0.550	1.05	0.522	1.08	1.30	0.641	No
156	10.25	0.62	0.07	0.55	0.98	0.552	1.05	0.523	1.08	1.30	0.645	No
157	10.31	0.63	0.07	0.55	0.98	0.553	1.05	0.524	1.08	1.30	0.648	No
158	10.37	0.63	0.07	0.55	0.98	0.554	1.05	0.526	1.08	1.30	0.651	No
159	10.45	0.63	0.08	0.56	0.98	0.556	1.05	0.527	1.08	1.30	0.655	No
160	10.50	0.64	0.08	0.56	0.98	0.557	1.05	0.528	1.08	1.30	0.657	No
161	10.58	0.64	0.08	0.56	0.98	0.559	1.05	0.530	1.08	1.30	0.660	No
162	10.64	0.65	0.08	0.56	0.98	0.560	1.05	0.531	1.08	1.30	0.661	No
163	10.70	0.65	0.08	0.56	0.98	0.561	1.05	0.532	1.08	1.30	0.663	No
164	10.78	0.65	0.09	0.57	0.98	0.563	1.05	0.534	1.08	1.30	0.664	No
165	10.84	0.66	0.09	0.57	0.98	0.564	1.05	0.535	1.08	1.30	0.665	No
166	10.90	0.66	0.09	0.57	0.98	0.566	1.05	0.536	1.08	1.30	0.665	No
167	10.98	0.67	0.09	0.57	0.97	0.567	1.05	0.538	1.08	1.30	0.665	No
168	11.04	0.67	0.09	0.58	0.97	0.568	1.05	0.539	1.08	1.30	0.666	No
169	11.10	0.67	0.10	0.58	0.97	0.570	1.05	0.540	1.08	1.30	0.666	No
170	11.16	0.68	0.10	0.58	0.97	0.571	1.05	0.541	1.08	1.30	0.667	No
171	11.22	0.68	0.10	0.58	0.97	0.572	1.05	0.542	1.08	1.30	0.668	No
172	11.31	0.69	0.10	0.58	0.97	0.574	1.05	0.544	1.08	1.30	0.671	No
173	11.37	0.69	0.11	0.59	0.97	0.575	1.05	0.545	1.08	1.30	0.673	No
174	11.43	0.69	0.11	0.59	0.97	0.576	1.05	0.546	1.08	1.30	0.674	No
175	11.49	0.70	0.11	0.59	0.97	0.577	1.05	0.547	1.08	1.30	0.676	No
176	11.55	0.70	0.11	0.59	0.97	0.578	1.05	0.549	1.08	1.30	0.677	No
177	11.64	0.71	0.11	0.59	0.97	0.580	1.05	0.550	1.08	1.30	0.679	No
178	11.70	0.71	0.12	0.60	0.97	0.581	1.05	0.551	1.08	1.30	0.681	No
179	11.77	0.71	0.12	0.60	0.97	0.582	1.05	0.552	1.08	1.30	0.682	No
180	11.82	0.72	0.12	0.60	0.97	0.583	1.05	0.553	1.08	1.30	0.683	No
181	11.88	0.72	0.12	0.60	0.97	0.585	1.05	0.554	1.08	1.30	0.685	No
182	11.94	0.73	0.12	0.60	0.97	0.586	1.05	0.555	1.08	1.30	0.686	No
183	12.03	0.73	0.13	0.61	0.97	0.587	1.05	0.557	1.07	1.30	0.691	No
184	12.09	0.73	0.13	0.61	0.97	0.588	1.05	0.558	1.07	1.30	0.694	No
185	12.15	0.74	0.13	0.61	0.97	0.589	1.05	0.559	1.07	1.30	0.695	No
186	12.21	0.74	0.13	0.61	0.97	0.590	1.05	0.560	1.07	1.30	0.696	No
187	12.28	0.75	0.13	0.61	0.97	0.592	1.05	0.561	1.07	1.30	0.698	No
188	12.34	0.75	0.14	0.61	0.97	0.593	1.05	0.562	1.07	1.30	0.700	No
189	12.42	0.75	0.14	0.62	0.97	0.594	1.05	0.563	1.06	1.30	0.709	No
190	12.48	0.76	0.14	0.62	0.97	0.595	1.05	0.564	1.07	1.30	0.707	No
191	12.54	0.76	0.14	0.62	0.97	0.596	1.05	0.565	1.07	1.30	0.710	No
192	12.60	0.77	0.14	0.62	0.97	0.597	1.05	0.566	1.06	1.30	0.713	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	12.69	0.77	0.15	0.62	0.97	0.599	1.05	0.568	1.06	1.30	0.718	No
194	12.75	0.77	0.15	0.63	0.97	0.600	1.05	0.569	1.06	1.30	0.720	No
195	12.81	0.78	0.15	0.63	0.97	0.601	1.05	0.570	1.06	1.30	0.723	No
196	12.87	0.78	0.15	0.63	0.97	0.602	1.05	0.570	1.06	1.30	0.724	No
197	12.93	0.79	0.15	0.63	0.97	0.602	1.05	0.571	1.06	1.30	0.725	No
198	13.02	0.79	0.16	0.63	0.97	0.604	1.05	0.573	1.06	1.30	0.727	No
199	13.08	0.79	0.16	0.64	0.97	0.605	1.05	0.574	1.06	1.30	0.728	No
200	13.14	0.80	0.16	0.64	0.97	0.606	1.05	0.574	1.06	1.30	0.728	No
201	13.20	0.80	0.16	0.64	0.97	0.607	1.05	0.575	1.06	1.30	0.729	No
202	13.26	0.81	0.16	0.64	0.97	0.608	1.05	0.576	1.06	1.30	0.730	No
203	13.35	0.81	0.17	0.64	0.97	0.609	1.05	0.578	1.06	1.30	0.730	No
204	13.41	0.82	0.17	0.65	0.97	0.610	1.05	0.578	1.06	1.30	0.730	No
205	13.47	0.82	0.17	0.65	0.97	0.611	1.05	0.579	1.06	1.30	0.730	No
206	13.53	0.82	0.17	0.65	0.97	0.612	1.05	0.580	1.06	1.30	0.731	No
207	13.59	0.83	0.17	0.65	0.97	0.613	1.05	0.581	1.06	1.30	0.731	No
208	13.65	0.83	0.18	0.65	0.97	0.614	1.05	0.582	1.06	1.30	0.731	No
209	13.74	0.84	0.18	0.66	0.97	0.615	1.05	0.583	1.06	1.30	0.732	No
210	13.80	0.84	0.18	0.66	0.96	0.616	1.05	0.584	1.06	1.30	0.732	No
211	13.86	0.84	0.18	0.66	0.96	0.617	1.05	0.585	1.06	1.30	0.734	No
212	13.92	0.85	0.18	0.66	0.96	0.617	1.05	0.586	1.06	1.30	0.735	No
213	13.98	0.85	0.19	0.66	0.96	0.618	1.05	0.586	1.06	1.30	0.735	No
214	14.07	0.86	0.19	0.67	0.96	0.619	1.05	0.587	1.06	1.30	0.735	No
215	14.13	0.86	0.19	0.67	0.96	0.620	1.05	0.588	1.06	1.30	0.735	No
216	14.19	0.86	0.19	0.67	0.96	0.621	1.05	0.589	1.06	1.30	0.736	No
217	14.25	0.87	0.20	0.67	0.96	0.622	1.05	0.590	1.06	1.30	0.736	No
218	14.31	0.87	0.20	0.67	0.96	0.623	1.05	0.591	1.06	1.30	0.737	No
219	14.37	0.88	0.20	0.68	0.96	0.624	1.05	0.591	1.06	1.30	0.738	No
220	14.46	0.88	0.20	0.68	0.96	0.625	1.05	0.593	1.06	1.30	0.739	No
221	14.52	0.88	0.20	0.68	0.96	0.626	1.05	0.593	1.06	1.30	0.739	No
222	14.58	0.89	0.21	0.68	0.96	0.626	1.05	0.594	1.06	1.30	0.739	No
223	14.64	0.89	0.21	0.68	0.96	0.627	1.05	0.595	1.06	1.30	0.739	No
224	14.70	0.90	0.21	0.69	0.96	0.628	1.05	0.596	1.06	1.30	0.739	No
225	14.79	0.90	0.21	0.69	0.96	0.629	1.05	0.597	1.06	1.30	0.740	No
226	14.85	0.90	0.21	0.69	0.96	0.630	1.05	0.597	1.06	1.30	0.743	No
227	14.91	0.91	0.22	0.69	0.96	0.631	1.05	0.598	1.06	1.30	0.748	No
228	14.97	0.91	0.22	0.69	0.96	0.631	1.05	0.599	1.06	1.30	0.748	No
229	15.03	0.92	0.22	0.70	0.96	0.632	1.05	0.600	1.06	1.30	0.747	No
230	15.09	0.92	0.22	0.70	0.96	0.633	1.05	0.600	1.06	1.30	0.747	No
231	15.18	0.92	0.22	0.70	0.96	0.634	1.05	0.601	1.06	1.30	0.748	No
232	15.23	0.93	0.23	0.70	0.96	0.635	1.05	0.602	1.06	1.30	0.749	No
233	15.29	0.93	0.23	0.70	0.96	0.635	1.05	0.603	1.06	1.30	0.749	No
234	15.38	0.94	0.23	0.71	0.96	0.636	1.05	0.603	1.06	1.30	0.749	No
235	15.44	0.94	0.23	0.71	0.96	0.637	1.05	0.604	1.06	1.30	0.749	No
236	15.50	0.94	0.23	0.71	0.96	0.638	1.05	0.605	1.06	1.30	0.749	No
237	15.56	0.95	0.24	0.71	0.96	0.638	1.05	0.605	1.06	1.30	0.750	No
238	15.62	0.95	0.24	0.71	0.96	0.639	1.05	0.606	1.06	1.30	0.751	No
239	15.71	0.96	0.24	0.72	0.96	0.640	1.05	0.607	1.06	1.30	0.753	No
240	15.77	0.96	0.24	0.72	0.96	0.641	1.05	0.608	1.06	1.30	0.754	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	15.83	0.97	0.24	0.72	0.96	0.641	1.05	0.608	1.06	1.30	0.756	No
242	15.89	0.97	0.25	0.72	0.96	0.642	1.05	0.609	1.06	1.30	0.757	No
243	15.95	0.97	0.25	0.72	0.96	0.643	1.05	0.610	1.06	1.30	0.759	No
244	16.04	0.98	0.25	0.73	0.96	0.644	1.05	0.611	1.06	1.30	0.761	No
245	16.10	0.98	0.25	0.73	0.96	0.644	1.05	0.611	1.06	1.30	0.762	No
246	16.16	0.99	0.25	0.73	0.96	0.645	1.05	0.612	1.06	1.30	0.764	No
247	16.22	0.99	0.26	0.73	0.96	0.646	1.05	0.612	1.05	1.30	0.765	No
248	16.28	0.99	0.26	0.73	0.96	0.646	1.05	0.613	1.05	1.30	0.767	No
249	16.34	1.00	0.26	0.74	0.96	0.647	1.05	0.614	1.05	1.30	0.770	No
250	16.43	1.00	0.26	0.74	0.95	0.648	1.05	0.615	1.05	1.30	0.774	No
251	16.49	1.01	0.26	0.74	0.95	0.649	1.05	0.615	1.05	1.30	0.777	No
252	16.55	1.01	0.27	0.74	0.95	0.649	1.05	0.616	1.05	1.30	0.781	No
253	16.61	1.01	0.27	0.75	0.95	0.650	1.05	0.616	1.05	1.30	0.784	No
254	16.67	1.02	0.27	0.75	0.95	0.650	1.05	0.617	1.04	1.30	0.788	No
255	16.76	1.02	0.27	0.75	0.95	0.651	1.05	0.618	1.04	1.30	0.793	No
256	16.82	1.03	0.28	0.75	0.95	0.652	1.05	0.618	1.04	1.30	0.797	No
257	16.88	1.03	0.28	0.75	0.95	0.653	1.05	0.619	1.04	1.30	0.800	No
258	16.94	1.03	0.28	0.75	0.95	0.653	1.05	0.619	1.04	1.30	0.803	No
259	17.00	1.04	0.28	0.76	0.95	0.654	1.05	0.620	1.04	1.30	0.806	No
260	17.09	1.04	0.28	0.76	0.95	0.655	1.05	0.621	1.03	1.30	0.811	No
261	17.15	1.05	0.29	0.76	0.95	0.655	1.05	0.622	1.03	1.30	0.812	No
262	17.21	1.05	0.29	0.76	0.95	0.656	1.05	0.622	1.03	1.30	0.813	No
263	17.27	1.05	0.29	0.76	0.95	0.657	1.05	0.623	1.03	1.30	0.814	No
264	17.34	1.06	0.29	0.77	0.95	0.657	1.05	0.623	1.03	1.30	0.814	No
265	17.39	1.06	0.29	0.77	0.95	0.658	1.05	0.624	1.03	1.30	0.814	No
266	17.46	1.07	0.30	0.77	0.95	0.658	1.05	0.624	1.03	1.30	0.819	No
267	17.52	1.07	0.30	0.77	0.95	0.659	1.05	0.625	1.03	1.30	0.813	No
268	17.60	1.07	0.30	0.77	0.95	0.660	1.05	0.626	1.04	1.30	0.811	No
269	17.66	1.08	0.30	0.78	0.95	0.660	1.05	0.626	1.04	1.30	0.807	No
270	17.72	1.08	0.30	0.78	0.95	0.661	1.05	0.627	1.04	1.30	0.804	No
271	17.81	1.09	0.31	0.78	0.95	0.661	1.05	0.627	1.04	1.30	0.796	No
272	17.87	1.09	0.31	0.78	0.95	0.662	1.05	0.628	1.05	1.30	0.791	No
273	17.93	1.09	0.31	0.79	0.95	0.662	1.05	0.628	1.05	1.30	0.787	No
274	17.99	1.10	0.31	0.79	0.95	0.663	1.05	0.629	1.05	1.30	0.786	No
275	18.05	1.10	0.31	0.79	0.95	0.663	1.05	0.629	1.05	1.30	0.785	No
276	18.12	1.11	0.32	0.79	0.95	0.664	1.05	0.630	1.05	1.30	0.785	No
277	18.18	1.11	0.32	0.79	0.95	0.665	1.05	0.630	1.05	1.30	0.785	No
278	18.27	1.12	0.32	0.80	0.95	0.665	1.05	0.631	1.05	1.30	0.785	No
279	18.33	1.12	0.32	0.80	0.95	0.666	1.05	0.631	1.05	1.30	0.784	No
280	18.39	1.12	0.32	0.80	0.95	0.666	1.05	0.632	1.05	1.30	0.784	No
281	18.45	1.13	0.33	0.80	0.95	0.667	1.05	0.632	1.05	1.30	0.784	No
282	18.51	1.13	0.33	0.80	0.95	0.667	1.05	0.633	1.05	1.30	0.785	No
283	18.60	1.14	0.33	0.81	0.95	0.668	1.05	0.633	1.05	1.30	0.785	No
284	18.66	1.14	0.33	0.81	0.95	0.668	1.05	0.634	1.05	1.30	0.785	No
285	18.72	1.14	0.33	0.81	0.95	0.669	1.05	0.634	1.05	1.30	0.786	No
286	18.78	1.15	0.34	0.81	0.95	0.669	1.05	0.635	1.05	1.30	0.787	No
287	18.84	1.15	0.34	0.81	0.95	0.670	1.05	0.635	1.05	1.30	0.788	No
288	18.90	1.16	0.34	0.82	0.95	0.670	1.05	0.636	1.05	1.30	0.789	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	18.99	1.16	0.34	0.82	0.94	0.671	1.05	0.636	1.04	1.30	0.792	No
290	19.05	1.17	0.34	0.82	0.94	0.671	1.05	0.637	1.04	1.30	0.794	No
291	19.11	1.17	0.35	0.82	0.94	0.672	1.05	0.637	1.04	1.30	0.796	No
292	19.17	1.17	0.35	0.82	0.94	0.672	1.05	0.637	1.04	1.30	0.797	No
293	19.23	1.18	0.35	0.83	0.94	0.672	1.05	0.638	1.04	1.30	0.799	No
294	19.32	1.18	0.35	0.83	0.94	0.673	1.05	0.638	1.04	1.30	0.802	No
295	19.38	1.19	0.35	0.83	0.94	0.674	1.05	0.639	1.04	1.30	0.805	No
296	19.44	1.19	0.36	0.83	0.94	0.674	1.05	0.639	1.04	1.30	0.807	No
297	19.50	1.19	0.36	0.84	0.94	0.674	1.05	0.640	1.04	1.30	0.814	No
298	19.56	1.20	0.36	0.84	0.94	0.675	1.05	0.640	1.03	1.30	0.824	No
299	19.65	1.20	0.36	0.84	0.94	0.675	1.05	0.641	1.03	1.30	0.832	No
300	19.71	1.21	0.37	0.84	0.94	0.676	1.05	0.641	1.03	1.30	0.836	No
301	19.77	1.21	0.37	0.84	0.94	0.676	1.05	0.641	1.03	1.30	0.841	No
302	19.83	1.22	0.37	0.85	0.94	0.677	1.05	0.642	1.02	1.30	0.846	No
303	19.89	1.22	0.37	0.85	0.94	0.677	1.05	0.642	1.02	1.30	0.850	No
304	19.95	1.22	0.37	0.85	0.94	0.678	1.05	0.643	1.02	1.30	0.851	No
305	20.01	1.23	0.37	0.85	0.94	0.678	1.05	0.643	1.02	1.30	0.852	No
306	20.09	1.23	0.38	0.85	0.94	0.679	1.05	0.644	1.02	1.30	0.853	No
307	20.15	1.23	0.38	0.86	0.94	0.679	1.05	0.644	1.02	1.30	0.854	No
308	20.21	1.24	0.38	0.86	0.94	0.679	1.05	0.644	1.02	1.30	0.855	No
309	20.30	1.24	0.38	0.86	0.94	0.680	1.05	0.645	1.02	1.30	0.857	No
310	20.36	1.25	0.39	0.86	0.94	0.680	1.05	0.645	1.02	1.30	0.857	No
311	20.42	1.25	0.39	0.86	0.94	0.681	1.05	0.646	1.02	1.30	0.858	No
312	20.48	1.25	0.39	0.86	0.94	0.681	1.05	0.646	1.02	1.30	0.859	No
313	20.54	1.26	0.39	0.87	0.94	0.682	1.05	0.646	1.02	1.30	0.860	No
314	20.63	1.26	0.39	0.87	0.94	0.682	1.05	0.647	1.02	1.30	0.861	No
315	20.69	1.27	0.40	0.87	0.94	0.683	1.05	0.647	1.02	1.30	0.862	No
316	20.75	1.27	0.40	0.87	0.94	0.683	1.05	0.648	1.02	1.30	0.862	No
317	20.81	1.27	0.40	0.87	0.94	0.683	1.05	0.648	1.02	1.30	0.862	No
318	20.87	1.28	0.40	0.88	0.94	0.684	1.05	0.649	1.02	1.30	0.862	No
319	20.93	1.28	0.40	0.88	0.94	0.684	1.05	0.649	1.02	1.30	0.862	No
320	21.02	1.29	0.41	0.88	0.94	0.685	1.05	0.649	1.02	1.30	0.862	No
321	21.08	1.29	0.41	0.88	0.94	0.685	1.05	0.650	1.02	1.30	0.862	No
322	21.14	1.29	0.41	0.88	0.94	0.685	1.05	0.650	1.02	1.30	0.862	No
323	21.20	1.30	0.41	0.89	0.94	0.686	1.05	0.650	1.02	1.30	0.862	No
324	21.26	1.30	0.41	0.89	0.94	0.686	1.05	0.651	1.02	1.30	0.862	No
325	21.35	1.31	0.42	0.89	0.93	0.687	1.05	0.651	1.02	1.30	0.862	No
326	21.41	1.31	0.42	0.89	0.93	0.687	1.05	0.652	1.02	1.30	0.862	No
327	21.47	1.31	0.42	0.89	0.93	0.687	1.05	0.652	1.02	1.30	0.862	No
328	21.53	1.32	0.42	0.90	0.93	0.688	1.05	0.652	1.02	1.30	0.862	No
329	21.59	1.32	0.42	0.90	0.93	0.688	1.05	0.653	1.02	1.30	0.863	No
330	21.66	1.33	0.43	0.90	0.93	0.689	1.05	0.653	1.02	1.30	0.864	No
331	21.72	1.33	0.43	0.90	0.93	0.689	1.05	0.653	1.02	1.30	0.865	No
332	21.79	1.33	0.43	0.90	0.93	0.689	1.05	0.654	1.02	1.30	0.866	No
333	21.86	1.34	0.43	0.91	0.93	0.690	1.05	0.654	1.02	1.30	0.867	No
334	21.92	1.34	0.43	0.91	0.93	0.690	1.05	0.654	1.02	1.30	0.868	No
335	22.00	1.35	0.44	0.91	0.93	0.690	1.05	0.655	1.02	1.30	0.870	No
336	22.06	1.35	0.44	0.91	0.93	0.691	1.05	0.655	1.02	1.30	0.871	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	22.13	1.36	0.44	0.91	0.93	0.691	1.05	0.655	1.01	1.30	0.871	No
338	22.18	1.36	0.44	0.92	0.93	0.691	1.05	0.656	1.01	1.30	0.872	No
339	22.26	1.36	0.44	0.92	0.93	0.692	1.05	0.656	1.01	1.30	0.873	No
340	22.32	1.37	0.45	0.92	0.93	0.692	1.05	0.656	1.01	1.30	0.873	No
341	22.39	1.37	0.45	0.92	0.93	0.692	1.05	0.657	1.01	1.30	0.874	No
342	22.46	1.38	0.45	0.92	0.93	0.693	1.05	0.657	1.01	1.30	0.874	No
343	22.52	1.38	0.45	0.93	0.93	0.693	1.05	0.657	1.01	1.30	0.875	No
344	22.60	1.38	0.46	0.93	0.93	0.693	1.05	0.657	1.01	1.30	0.875	No
345	22.64	1.39	0.46	0.93	0.93	0.693	1.05	0.658	1.01	1.30	0.876	No
346	22.71	1.39	0.46	0.93	0.93	0.694	1.05	0.658	1.01	1.30	0.876	No
347	22.77	1.40	0.46	0.93	0.93	0.694	1.05	0.658	1.01	1.30	0.877	No
348	22.84	1.40	0.46	0.94	0.93	0.694	1.05	0.659	1.01	1.30	0.878	No
349	22.93	1.41	0.47	0.94	0.93	0.695	1.05	0.659	1.01	1.30	0.878	No
350	22.98	1.41	0.47	0.94	0.93	0.695	1.05	0.659	1.01	1.30	0.879	No
351	23.04	1.41	0.47	0.94	0.93	0.695	1.05	0.659	1.01	1.30	0.879	No
352	23.12	1.42	0.47	0.95	0.93	0.696	1.05	0.660	1.01	1.30	0.880	No
353	23.17	1.42	0.47	0.95	0.93	0.696	1.05	0.660	1.01	1.30	0.879	No
354	23.26	1.43	0.48	0.95	0.93	0.696	1.05	0.660	1.01	1.30	0.877	No
355	23.32	1.43	0.48	0.95	0.93	0.697	1.05	0.661	1.01	1.30	0.875	No
356	23.38	1.43	0.48	0.95	0.93	0.697	1.05	0.661	1.01	1.30	0.873	No
357	23.44	1.44	0.48	0.96	0.93	0.697	1.05	0.661	1.01	1.30	0.871	No
358	23.49	1.44	0.48	0.96	0.93	0.697	1.05	0.661	1.01	1.30	0.872	No
359	23.56	1.44	0.49	0.96	0.93	0.698	1.05	0.662	1.01	1.30	0.870	No
360	23.63	1.45	0.49	0.96	0.92	0.698	1.05	0.662	1.01	1.30	0.869	No
361	23.69	1.45	0.49	0.96	0.92	0.698	1.05	0.662	1.01	1.30	0.868	No
362	23.75	1.46	0.49	0.97	0.92	0.698	1.05	0.662	1.01	1.30	0.867	No
363	23.84	1.46	0.49	0.97	0.92	0.699	1.05	0.663	1.01	1.30	0.866	No
364	23.89	1.46	0.50	0.97	0.92	0.699	1.05	0.663	1.01	1.30	0.866	No
365	23.96	1.47	0.50	0.97	0.92	0.699	1.05	0.663	1.01	1.30	0.865	No
366	24.02	1.47	0.50	0.97	0.92	0.699	1.05	0.663	1.01	1.30	0.864	No
367	24.10	1.48	0.50	0.98	0.92	0.700	1.05	0.663	1.01	1.30	0.864	No
368	24.16	1.48	0.50	0.98	0.92	0.700	1.05	0.664	1.01	1.30	0.865	No
369	24.23	1.49	0.51	0.98	0.92	0.700	1.05	0.664	1.01	1.30	0.865	No
370	24.29	1.49	0.51	0.98	0.92	0.700	1.05	0.664	1.01	1.30	0.866	No
371	24.36	1.49	0.51	0.98	0.92	0.700	1.05	0.664	1.01	1.30	0.867	No
372	24.41	1.50	0.51	0.99	0.92	0.701	1.05	0.665	1.01	1.30	0.868	No
373	24.50	1.50	0.51	0.99	0.92	0.701	1.05	0.665	1.01	1.30	0.871	No
374	24.56	1.51	0.52	0.99	0.92	0.701	1.05	0.665	1.01	1.30	0.873	No
375	24.62	1.51	0.52	0.99	0.92	0.701	1.05	0.665	1.01	1.30	0.876	No
376	24.68	1.52	0.52	1.00	0.92	0.702	1.05	0.665	1.01	1.30	0.879	No
377	24.75	1.52	0.52	1.00	0.92	0.702	1.05	0.666	1.01	1.30	0.882	No
378	24.80	1.52	0.52	1.00	0.92	0.702	1.05	0.666	1.01	1.30	0.885	No
379	24.89	1.53	0.53	1.00	0.92	0.702	1.05	0.666	1.01	1.30	0.891	No
380	24.95	1.53	0.53	1.00	0.92	0.702	1.05	0.666	1.01	1.30	0.894	No
381	25.01	1.54	0.53	1.01	0.92	0.703	1.05	0.666	1.00	1.30	0.897	No
382	25.07	1.54	0.53	1.01	0.92	0.703	1.05	0.667	1.00	1.30	0.898	No
383	25.14	1.54	0.53	1.01	0.92	0.703	1.05	0.667	1.00	1.30	0.900	No
384	25.22	1.55	0.54	1.01	0.92	0.704	1.05	0.667	1.00	1.30	0.901	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	25.28	1.55	0.54	1.01	0.92	0.704	1.05	0.667	1.00	1.30	0.902	No
386	25.34	1.56	0.54	1.01	0.92	0.704	1.05	0.668	1.00	1.30	0.902	No
387	25.40	1.56	0.54	1.02	0.92	0.704	1.05	0.668	1.00	1.30	0.903	No
388	25.46	1.56	0.54	1.02	0.92	0.705	1.05	0.668	1.00	1.30	0.903	No
389	25.53	1.57	0.55	1.02	0.92	0.705	1.05	0.669	1.00	1.30	0.904	No
390	25.62	1.57	0.55	1.02	0.92	0.705	1.05	0.669	1.00	1.30	0.904	No
391	25.67	1.57	0.55	1.02	0.92	0.706	1.05	0.669	1.00	1.30	0.905	No
392	25.73	1.58	0.55	1.02	0.92	0.706	1.05	0.669	1.00	1.30	0.905	No
393	25.79	1.58	0.56	1.03	0.92	0.706	1.05	0.670	1.00	1.30	0.905	No
394	25.87	1.59	0.56	1.03	0.91	0.706	1.05	0.670	1.00	1.30	0.905	No
395	25.94	1.59	0.56	1.03	0.91	0.706	1.05	0.670	1.00	1.30	0.902	No
396	25.98	1.59	0.56	1.03	0.91	0.707	1.05	0.670	1.00	1.30	0.899	No
397	26.07	1.60	0.56	1.03	0.91	0.707	1.05	0.670	1.00	1.30	0.893	No
398	26.14	1.60	0.57	1.04	0.91	0.707	1.05	0.671	1.00	1.30	0.888	No
399	26.20	1.61	0.57	1.04	0.91	0.707	1.05	0.671	1.00	1.30	0.885	No
400	26.26	1.61	0.57	1.04	0.91	0.707	1.05	0.671	1.00	1.30	0.884	No
401	26.32	1.61	0.57	1.04	0.91	0.707	1.05	0.671	1.00	1.30	0.885	No
402	26.41	1.62	0.57	1.05	0.91	0.708	1.05	0.671	1.00	1.30	0.890	No
403	26.47	1.62	0.58	1.05	0.91	0.708	1.05	0.671	1.00	1.30	0.894	No
404	26.53	1.63	0.58	1.05	0.91	0.708	1.05	0.671	1.00	1.30	0.898	No
405	26.59	1.63	0.58	1.05	0.91	0.708	1.05	0.672	1.00	1.30	0.902	No
406	26.64	1.63	0.58	1.05	0.91	0.708	1.05	0.672	1.00	1.30	0.905	No
407	26.73	1.64	0.58	1.06	0.91	0.709	1.05	0.672	1.00	1.30	0.908	No
408	26.79	1.64	0.59	1.06	0.91	0.709	1.05	0.672	1.00	1.30	0.910	No
409	26.86	1.65	0.59	1.06	0.91	0.709	1.05	0.672	1.00	1.30	0.911	No
410	26.92	1.65	0.59	1.06	0.91	0.709	1.05	0.672	1.00	1.30	0.911	No
411	26.98	1.65	0.59	1.06	0.91	0.709	1.05	0.673	1.00	1.30	0.912	No
412	27.04	1.66	0.59	1.06	0.91	0.709	1.05	0.673	1.00	1.30	0.912	No
413	27.12	1.66	0.60	1.07	0.91	0.710	1.05	0.673	1.00	1.30	0.913	No
414	27.19	1.67	0.60	1.07	0.91	0.710	1.05	0.673	1.00	1.30	0.914	No
415	27.25	1.67	0.60	1.07	0.91	0.710	1.05	0.673	1.00	1.30	0.914	No
416	27.30	1.67	0.60	1.07	0.91	0.710	1.05	0.674	1.00	1.30	0.914	No
417	27.37	1.68	0.60	1.07	0.91	0.710	1.05	0.674	1.00	1.30	0.913	No
418	27.46	1.68	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.912	No
419	27.52	1.69	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.909	No
420	27.58	1.69	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.907	No
421	27.64	1.69	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.904	No
422	27.70	1.70	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.901	No
423	27.76	1.70	0.62	1.09	0.91	0.711	1.05	0.675	1.00	1.30	0.900	No
424	27.82	1.71	0.62	1.09	0.91	0.711	1.05	0.675	1.00	1.30	0.901	No
425	27.89	1.71	0.62	1.09	0.91	0.712	1.05	0.675	1.00	1.30	0.906	No
426	27.96	1.71	0.62	1.09	0.91	0.712	1.05	0.675	1.00	1.30	0.906	No
427	28.02	1.72	0.62	1.09	0.91	0.712	1.05	0.675	1.00	1.30	0.908	No
428	28.09	1.72	0.63	1.10	0.90	0.712	1.05	0.675	1.00	1.30	0.910	No
429	28.16	1.73	0.63	1.10	0.90	0.712	1.05	0.675	1.00	1.30	0.912	No
430	28.23	1.73	0.63	1.10	0.90	0.712	1.05	0.675	1.00	1.30	0.912	No
431	28.28	1.73	0.63	1.10	0.90	0.712	1.05	0.676	1.00	1.30	0.913	No
432	28.35	1.74	0.63	1.10	0.90	0.712	1.05	0.676	1.00	1.30	0.913	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	28.43	1.74	0.64	1.11	0.90	0.713	1.05	0.676	1.00	1.30	0.913	No
434	28.49	1.75	0.64	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.913	No
435	28.55	1.75	0.64	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.913	No
436	28.61	1.76	0.64	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.913	No
437	28.70	1.76	0.65	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.912	No
438	28.76	1.76	0.65	1.12	0.90	0.713	1.05	0.676	0.99	1.30	0.911	No
439	28.82	1.77	0.65	1.12	0.90	0.713	1.05	0.676	0.99	1.30	0.911	No
440	28.88	1.77	0.65	1.12	0.90	0.713	1.05	0.676	0.99	1.30	0.911	No
441	28.94	1.78	0.65	1.12	0.90	0.713	1.05	0.677	0.99	1.30	0.911	No
442	29.03	1.78	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.911	No
443	29.09	1.78	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.911	No
444	29.15	1.79	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.911	No
445	29.21	1.79	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.911	No
446	29.27	1.80	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.911	No
447	29.33	1.80	0.67	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.911	No
448	29.42	1.81	0.67	1.14	0.90	0.714	1.05	0.677	0.99	1.30	0.912	No
449	29.48	1.81	0.67	1.14	0.90	0.714	1.05	0.677	0.99	1.30	0.912	No
450	29.54	1.81	0.67	1.14	0.90	0.714	1.05	0.677	0.99	1.30	0.913	No
451	29.60	1.82	0.67	1.14	0.90	0.714	1.05	0.678	0.99	1.30	0.914	No
452	29.66	1.82	0.68	1.14	0.90	0.715	1.05	0.678	0.99	1.30	0.914	No
453	29.75	1.83	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.916	No
454	29.81	1.83	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.917	No
455	29.87	1.83	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.919	No
456	29.93	1.84	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.920	No
457	29.99	1.84	0.69	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.922	No
458	30.05	1.84	0.69	1.16	0.90	0.715	1.05	0.678	0.99	1.30	0.924	No
459	30.12	1.85	0.69	1.16	0.90	0.715	1.05	0.678	0.99	1.30	0.926	No
460	30.19	1.85	0.69	1.16	0.90	0.715	1.05	0.678	0.99	1.30	0.927	No
461	30.26	1.86	0.69	1.16	0.89	0.715	1.05	0.678	0.99	1.30	0.927	No
462	30.33	1.86	0.70	1.16	0.89	0.716	1.05	0.679	0.99	1.30	0.928	No
463	30.39	1.86	0.70	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.928	No
464	30.45	1.87	0.70	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.929	No
465	30.52	1.87	0.70	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.929	No
466	30.58	1.88	0.70	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.930	No
467	30.65	1.88	0.71	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.930	No
468	30.71	1.88	0.71	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.930	No
469	30.78	1.89	0.71	1.18	0.89	0.716	1.05	0.679	0.99	1.30	0.931	No
470	30.85	1.89	0.71	1.18	0.89	0.716	1.05	0.680	0.99	1.30	0.931	No
471	30.92	1.89	0.71	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.931	No
472	30.97	1.90	0.72	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.931	No
473	31.04	1.90	0.72	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.932	No
474	31.11	1.91	0.72	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.932	No
475	31.17	1.91	0.72	1.19	0.89	0.717	1.05	0.680	0.99	1.30	0.932	No
476	31.25	1.91	0.73	1.19	0.89	0.717	1.05	0.680	0.99	1.30	0.933	No
477	31.30	1.92	0.73	1.19	0.89	0.717	1.05	0.680	0.99	1.30	0.933	No
478	31.37	1.92	0.73	1.19	0.89	0.718	1.05	0.681	0.99	1.30	0.933	No
479	31.44	1.92	0.73	1.19	0.89	0.718	1.05	0.681	0.99	1.30	0.933	No
480	31.51	1.93	0.73	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
481	31.57	1.93	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
482	31.63	1.94	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
483	31.70	1.94	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
484	31.79	1.94	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.935	No
485	31.85	1.95	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.935	No
486	31.91	1.95	0.75	1.21	0.89	0.718	1.05	0.681	0.99	1.30	0.935	No
487	31.97	1.95	0.75	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.935	No
488	32.03	1.96	0.75	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.936	No
489	32.09	1.96	0.75	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.936	No
490	32.18	1.97	0.75	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.936	No
491	32.24	1.97	0.76	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.936	No
492	32.30	1.97	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
493	32.35	1.98	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
494	32.43	1.98	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
495	32.50	1.99	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
496	32.56	1.99	0.77	1.22	0.88	0.720	1.05	0.682	0.99	1.30	0.937	No
497	32.62	1.99	0.77	1.22	0.88	0.720	1.05	0.682	0.99	1.30	0.938	No
498	32.69	2.00	0.77	1.23	0.88	0.720	1.05	0.683	0.99	1.30	0.938	No
499	32.75	2.00	0.77	1.23	0.88	0.720	1.05	0.683	0.99	1.30	0.938	No
500	32.83	2.00	0.77	1.23	0.88	0.720	1.05	0.683	0.99	1.30	0.938	No
501	32.88	2.01	0.78	1.23	0.88	0.720	1.05	0.683	0.99	1.30	0.938	No
502	32.96	2.01	0.78	1.23	0.88	0.720	1.05	0.683	0.99	1.30	0.938	No
503	33.02	2.02	0.78	1.24	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
504	33.08	2.02	0.78	1.24	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
505	33.14	2.02	0.78	1.24	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
506	33.23	2.03	0.79	1.24	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
507	33.28	2.03	0.79	1.24	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
508	33.36	2.04	0.79	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
509	33.41	2.04	0.79	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
510	33.48	2.04	0.79	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
511	33.55	2.05	0.80	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
512	33.61	2.05	0.80	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.941	No
513	33.67	2.05	0.80	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.941	No
514	33.74	2.06	0.80	1.26	0.88	0.721	1.05	0.683	0.99	1.30	0.941	No
515	33.80	2.06	0.81	1.26	0.88	0.721	1.05	0.683	0.99	1.30	0.941	No
516	33.88	2.07	0.81	1.26	0.88	0.721	1.05	0.683	0.99	1.30	0.941	No
517	33.94	2.07	0.81	1.26	0.88	0.721	1.05	0.683	0.99	1.30	0.941	No
518	34.00	2.07	0.81	1.26	0.88	0.721	1.05	0.684	0.99	1.30	0.942	No
519	34.06	2.08	0.81	1.26	0.88	0.721	1.05	0.684	0.98	1.30	0.942	No
520	34.15	2.08	0.82	1.27	0.88	0.721	1.05	0.684	0.98	1.30	0.942	No
521	34.21	2.09	0.82	1.27	0.88	0.721	1.05	0.684	0.98	1.30	0.942	No
522	34.27	2.09	0.82	1.27	0.88	0.721	1.05	0.684	0.98	1.30	0.942	No
523	34.33	2.09	0.82	1.27	0.88	0.721	1.05	0.684	0.98	1.30	0.942	No
524	34.39	2.10	0.82	1.27	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
525	34.45	2.10	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
526	34.52	2.10	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
527	34.61	2.11	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
528	34.67	2.11	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
529	34.73	2.12	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
530	34.79	2.12	0.84	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
531	34.85	2.12	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
532	34.93	2.13	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
533	34.98	2.13	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
534	35.07	2.14	0.84	1.29	0.87	0.722	1.05	0.684	0.98	1.30	0.944	No
535	35.13	2.14	0.85	1.29	0.87	0.722	1.05	0.684	0.98	1.30	0.945	No
536	35.19	2.14	0.85	1.29	0.87	0.722	1.05	0.684	0.98	1.30	0.945	No
537	35.25	2.15	0.85	1.30	0.87	0.722	1.05	0.684	0.98	1.30	0.945	No
538	35.31	2.15	0.85	1.30	0.87	0.722	1.05	0.684	0.98	1.30	0.945	No
539	35.37	2.15	0.85	1.30	0.87	0.722	1.05	0.685	0.98	1.30	0.945	No
540	35.43	2.16	0.86	1.30	0.87	0.722	1.05	0.685	0.98	1.30	0.945	No
541	35.52	2.16	0.86	1.30	0.87	0.722	1.05	0.685	0.98	1.30	0.946	No
542	35.58	2.17	0.86	1.30	0.87	0.722	1.05	0.685	0.98	1.30	0.946	No
543	35.64	2.17	0.86	1.31	0.87	0.722	1.05	0.685	0.98	1.30	0.946	No
544	35.70	2.17	0.86	1.31	0.87	0.722	1.05	0.685	0.98	1.30	0.946	No
545	35.76	2.18	0.87	1.31	0.87	0.722	1.05	0.685	0.98	1.30	0.946	No
546	35.85	2.18	0.87	1.31	0.87	0.722	1.05	0.685	0.98	1.30	0.946	No
547	35.91	2.18	0.87	1.31	0.87	0.722	1.05	0.685	0.98	1.30	0.946	No
548	35.97	2.19	0.87	1.32	0.87	0.722	1.05	0.685	0.98	1.30	0.947	No
549	36.03	2.19	0.87	1.32	0.87	0.722	1.05	0.685	0.98	1.30	0.947	No
550	36.09	2.19	0.88	1.32	0.87	0.722	1.05	0.685	0.98	1.30	0.947	No
551	36.18	2.20	0.88	1.32	0.87	0.722	1.05	0.685	0.98	1.30	0.947	No
552	36.24	2.20	0.88	1.32	0.87	0.722	1.05	0.685	0.98	1.30	0.947	No
553	36.30	2.21	0.88	1.32	0.87	0.722	1.05	0.685	0.98	1.30	0.947	No
554	36.36	2.21	0.88	1.33	0.87	0.722	1.05	0.685	0.98	1.30	0.947	No
555	36.42	2.21	0.89	1.33	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
556	36.51	2.22	0.89	1.33	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
557	36.57	2.22	0.89	1.33	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
558	36.63	2.23	0.89	1.33	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
559	36.69	2.23	0.90	1.34	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
560	36.75	2.23	0.90	1.34	0.86	0.722	1.05	0.685	0.98	1.30	0.948	No
561	36.81	2.24	0.90	1.34	0.86	0.722	1.05	0.685	0.98	1.30	0.948	No
562	36.91	2.24	0.90	1.34	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
563	36.97	2.25	0.90	1.34	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
564	37.03	2.25	0.91	1.35	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
565	37.08	2.25	0.91	1.35	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
566	37.15	2.26	0.91	1.35	0.86	0.722	1.05	0.685	0.98	1.30	0.947	No
567	37.21	2.26	0.91	1.35	0.86	0.722	1.05	0.684	0.98	1.30	0.948	No
568	37.29	2.27	0.91	1.35	0.86	0.722	1.05	0.684	0.98	1.30	0.948	No
569	37.34	2.27	0.92	1.36	0.86	0.722	1.05	0.684	0.98	1.30	0.948	No
570	37.43	2.28	0.92	1.36	0.86	0.722	1.05	0.684	0.98	1.30	0.948	No
571	37.48	2.28	0.92	1.36	0.86	0.722	1.05	0.684	0.98	1.30	0.949	No
572	37.55	2.28	0.92	1.36	0.86	0.722	1.05	0.684	0.98	1.30	0.949	No
573	37.62	2.29	0.92	1.36	0.86	0.722	1.05	0.684	0.98	1.30	0.949	No
574	37.67	2.29	0.93	1.36	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
575	37.74	2.29	0.93	1.37	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
576	37.81	2.30	0.93	1.37	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
577	37.86	2.30	0.93	1.37	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
578	37.94	2.31	0.93	1.37	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
579	38.02	2.31	0.94	1.37	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
580	38.07	2.31	0.94	1.38	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
581	38.13	2.32	0.94	1.38	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
582	38.22	2.32	0.94	1.38	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
583	38.28	2.33	0.94	1.38	0.86	0.721	1.05	0.684	0.98	1.30	0.949	No
584	38.34	2.33	0.95	1.38	0.86	0.721	1.05	0.684	0.97	1.30	0.949	No
585	38.40	2.34	0.95	1.39	0.86	0.721	1.05	0.684	0.97	1.30	0.949	No
586	38.47	2.34	0.95	1.39	0.85	0.721	1.05	0.684	0.97	1.30	0.949	No
587	38.53	2.34	0.95	1.39	0.85	0.721	1.05	0.684	0.97	1.30	0.948	No
588	38.59	2.35	0.95	1.39	0.85	0.721	1.05	0.683	0.97	1.30	0.948	No
589	38.68	2.35	0.96	1.40	0.85	0.721	1.05	0.683	0.97	1.30	0.947	No
590	38.74	2.36	0.96	1.40	0.85	0.720	1.05	0.683	0.97	1.30	0.946	No
591	38.80	2.36	0.96	1.40	0.85	0.720	1.05	0.683	0.97	1.30	0.946	No
592	38.85	2.36	0.96	1.40	0.85	0.720	1.05	0.683	0.97	1.30	0.946	No
593	38.93	2.37	0.96	1.40	0.85	0.720	1.05	0.683	0.97	1.30	0.946	No
594	38.98	2.37	0.97	1.40	0.85	0.720	1.05	0.683	0.97	1.30	0.946	No
595	39.04	2.38	0.97	1.41	0.85	0.720	1.05	0.683	0.97	1.30	0.946	No
596	39.11	2.38	0.97	1.41	0.85	0.720	1.05	0.683	0.96	1.30	0.946	No
597	39.20	2.39	0.97	1.41	0.85	0.720	1.05	0.683	0.96	1.30	0.946	No
598	39.26	2.39	0.98	1.41	0.85	0.720	1.05	0.683	0.97	1.30	0.947	No
599	39.32	2.39	0.98	1.42	0.85	0.720	1.05	0.682	0.97	1.30	0.947	No
600	39.38	2.40	0.98	1.42	0.85	0.719	1.05	0.682	0.97	1.30	0.948	No
601	39.44	2.40	0.98	1.42	0.85	0.719	1.05	0.682	0.97	1.30	0.948	No
602	39.53	2.41	0.98	1.42	0.85	0.719	1.05	0.682	0.97	1.30	0.948	No
603	39.59	2.41	0.99	1.42	0.85	0.719	1.05	0.682	0.97	1.30	0.949	No
604	39.65	2.41	0.99	1.43	0.85	0.719	1.05	0.682	0.97	1.30	0.949	No
605	39.71	2.42	0.99	1.43	0.85	0.719	1.05	0.682	0.97	1.30	0.949	No
606	39.77	2.42	0.99	1.43	0.85	0.719	1.05	0.682	0.97	1.30	0.950	No
607	39.86	2.43	0.99	1.43	0.85	0.719	1.05	0.682	0.97	1.30	0.950	No
608	39.92	2.43	1.00	1.43	0.85	0.719	1.05	0.682	0.97	1.30	0.950	No
609	39.98	2.43	1.00	1.44	0.85	0.719	1.05	0.682	0.97	1.30	0.950	No
610	40.04	2.44	1.00	1.44	0.85	0.719	1.05	0.682	0.97	1.30	0.950	No
611	40.10	2.44	1.00	1.44	0.85	0.719	1.05	0.682	0.97	1.30	0.950	No
612	40.16	2.44	1.00	1.44	0.85	0.719	1.05	0.682	0.96	1.30	0.947	No
613	40.22	2.45	1.01	1.44	0.85	0.718	1.05	0.681	0.95	1.30	0.942	No
614	40.30	2.45	1.01	1.45	0.85	0.718	1.05	0.681	0.95	1.30	0.938	No
615	40.37	2.46	1.01	1.45	0.85	0.718	1.05	0.681	0.94	1.30	0.935	No
616	40.43	2.46	1.01	1.45	0.85	0.718	1.05	0.681	0.94	1.30	0.934	No
617	40.51	2.47	1.01	1.45	0.84	0.718	1.05	0.681	0.94	1.30	0.933	No
618	40.57	2.47	1.02	1.46	0.84	0.718	1.05	0.681	0.93	1.30	0.933	No
619	40.63	2.48	1.02	1.46	0.84	0.718	1.05	0.681	0.93	1.30	0.932	No
620	40.69	2.48	1.02	1.46	0.84	0.718	1.05	0.681	0.93	1.30	0.932	No
621	40.78	2.49	1.02	1.46	0.84	0.717	1.05	0.680	0.93	1.30	0.931	No
622	40.84	2.49	1.02	1.46	0.84	0.717	1.05	0.680	0.93	1.30	0.931	No
623	40.90	2.49	1.03	1.47	0.84	0.717	1.05	0.680	0.93	1.30	0.932	No
624	40.95	2.50	1.03	1.47	0.84	0.717	1.05	0.680	0.93	1.30	0.932	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
625	41.01	2.50	1.03	1.47	0.84	0.717	1.05	0.680	0.93	1.30	0.932	No
626	41.10	2.51	1.03	1.47	0.84	0.717	1.05	0.680	0.93	1.30	0.932	No
627	41.16	2.51	1.03	1.48	0.84	0.717	1.05	0.680	0.93	1.30	0.932	No
628	41.22	2.51	1.04	1.48	0.84	0.716	1.05	0.679	0.93	1.30	0.932	No
629	41.28	2.52	1.04	1.48	0.84	0.716	1.05	0.679	0.93	1.30	0.932	No
630	41.34	2.52	1.04	1.48	0.84	0.716	1.05	0.679	0.93	1.30	0.932	No
631	41.41	2.53	1.04	1.48	0.84	0.716	1.05	0.679	0.92	1.30	0.932	No
632	41.49	2.53	1.05	1.49	0.84	0.716	1.05	0.679	0.92	1.30	0.935	No
633	41.55	2.54	1.05	1.49	0.84	0.716	1.05	0.679	0.92	1.30	0.937	No
634	41.61	2.54	1.05	1.49	0.84	0.716	1.05	0.679	0.92	1.30	0.939	No
635	41.68	2.54	1.05	1.49	0.84	0.715	1.05	0.678	0.91	1.30	0.940	No
636	41.73	2.55	1.05	1.50	0.84	0.715	1.05	0.678	0.91	1.30	0.942	No
637	41.83	2.55	1.06	1.50	0.84	0.715	1.05	0.678	0.91	1.30	0.946	No
638	41.89	2.56	1.06	1.50	0.84	0.715	1.05	0.678	0.91	1.30	0.949	No
639	41.95	2.56	1.06	1.50	0.84	0.715	1.05	0.678	0.90	1.30	0.952	No
640	42.01	2.57	1.06	1.50	0.84	0.715	1.05	0.678	0.90	1.30	0.955	No
641	42.06	2.57	1.06	1.51	0.84	0.714	1.05	0.678	0.90	1.30	0.957	No
642	42.16	2.58	1.07	1.51	0.84	0.714	1.05	0.677	0.90	1.30	0.956	No
643	42.22	2.58	1.07	1.51	0.84	0.714	1.05	0.677	0.90	1.30	0.954	No
644	42.28	2.58	1.07	1.51	0.84	0.714	1.05	0.677	0.90	1.30	0.952	No
645	42.34	2.59	1.07	1.52	0.84	0.714	1.05	0.677	0.90	1.30	0.948	No
646	42.40	2.59	1.07	1.52	0.84	0.714	1.05	0.677	0.91	1.30	0.945	No
647	42.48	2.60	1.08	1.52	0.84	0.713	1.05	0.677	0.92	1.30	0.935	No
648	42.54	2.60	1.08	1.52	0.83	0.713	1.05	0.676	0.92	1.30	0.936	No
649	42.60	2.61	1.08	1.53	0.83	0.713	1.05	0.676	0.92	1.30	0.935	No
650	42.66	2.61	1.08	1.53	0.83	0.713	1.05	0.676	0.92	1.30	0.935	No
651	42.72	2.61	1.08	1.53	0.83	0.713	1.05	0.676	0.92	1.30	0.936	No
652	42.78	2.62	1.09	1.53	0.83	0.713	1.05	0.676	0.93	1.30	0.937	No
653	42.87	2.62	1.09	1.54	0.83	0.712	1.05	0.676	0.93	1.30	0.938	No
654	42.93	2.63	1.09	1.54	0.83	0.712	1.05	0.676	0.93	1.30	0.938	No
655	42.99	2.63	1.09	1.54	0.83	0.712	1.05	0.675	0.93	1.30	0.939	No
656	43.05	2.64	1.09	1.54	0.83	0.712	1.05	0.675	0.93	1.30	0.939	No
657	43.11	2.64	1.10	1.54	0.83	0.712	1.05	0.675	0.93	1.30	0.939	No
658	43.20	2.65	1.10	1.55	0.83	0.712	1.05	0.675	0.93	1.30	0.939	No
659	43.26	2.65	1.10	1.55	0.83	0.711	1.05	0.675	0.93	1.30	0.939	No
660	43.32	2.65	1.10	1.55	0.83	0.711	1.05	0.675	0.93	1.30	0.939	No
661	43.38	2.66	1.10	1.55	0.83	0.711	1.05	0.674	0.93	1.30	0.939	No
662	43.44	2.66	1.11	1.56	0.83	0.711	1.05	0.674	0.93	1.30	0.940	No
663	43.51	2.67	1.11	1.56	0.83	0.711	1.05	0.674	0.93	1.30	0.940	No
664	43.59	2.67	1.11	1.56	0.83	0.711	1.05	0.674	0.93	1.30	0.941	No
665	43.65	2.67	1.11	1.56	0.83	0.710	1.05	0.674	0.93	1.30	0.941	No
666	43.71	2.68	1.11	1.56	0.83	0.710	1.05	0.674	0.93	1.30	0.941	No
667	43.77	2.68	1.12	1.57	0.83	0.710	1.05	0.674	0.94	1.30	0.942	No
668	43.83	2.69	1.12	1.57	0.83	0.710	1.05	0.673	0.94	1.30	0.942	No
669	43.92	2.69	1.12	1.57	0.83	0.710	1.05	0.673	0.94	1.30	0.943	No
670	43.98	2.70	1.12	1.57	0.83	0.710	1.05	0.673	0.94	1.30	0.944	No
671	44.05	2.70	1.12	1.58	0.83	0.710	1.05	0.673	0.94	1.30	0.944	No
672	44.10	2.70	1.13	1.58	0.83	0.709	1.05	0.673	0.95	1.30	0.945	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
673	44.16	2.71	1.13	1.58	0.83	0.709	1.05	0.673	0.95	1.30	0.946	No
674	44.23	2.71	1.13	1.58	0.83	0.709	1.05	0.673	0.95	1.30	0.946	No
675	44.32	2.72	1.13	1.58	0.83	0.709	1.05	0.672	0.95	1.30	0.946	No
676	44.38	2.72	1.13	1.59	0.83	0.709	1.05	0.672	0.96	1.30	0.946	No
677	44.43	2.72	1.14	1.59	0.83	0.709	1.05	0.672	0.96	1.30	0.946	No
678	44.49	2.73	1.14	1.59	0.83	0.709	1.05	0.672	0.95	1.30	0.946	No
679	44.57	2.73	1.14	1.59	0.82	0.708	1.05	0.672	0.95	1.30	0.946	No
680	44.63	2.74	1.14	1.59	0.82	0.708	1.05	0.672	0.95	1.30	0.946	No
681	44.70	2.74	1.15	1.60	0.82	0.708	1.05	0.672	0.96	1.30	0.946	No
682	44.77	2.75	1.15	1.60	0.82	0.708	1.05	0.671	0.95	1.30	0.946	No
683	44.82	2.75	1.15	1.60	0.82	0.708	1.05	0.671	0.95	1.30	0.946	No
684	44.88	2.75	1.15	1.60	0.82	0.708	1.05	0.671	0.95	1.30	0.946	No
685	44.97	2.76	1.15	1.61	0.82	0.708	1.05	0.671	0.95	1.30	0.946	No
686	45.03	2.76	1.16	1.61	0.82	0.707	1.05	0.671	0.95	1.30	0.945	No
687	45.10	2.77	1.16	1.61	0.82	0.707	1.05	0.671	0.94	1.30	0.945	No
688	45.16	2.77	1.16	1.61	0.82	0.707	1.05	0.671	0.94	1.30	0.944	No
689	45.22	2.78	1.16	1.61	0.82	0.707	1.05	0.670	0.94	1.30	0.944	No
690	45.28	2.78	1.16	1.62	0.82	0.707	1.05	0.670	0.94	1.30	0.943	No
691	45.37	2.78	1.17	1.62	0.82	0.707	1.05	0.670	0.93	1.30	0.943	No
692	45.43	2.79	1.17	1.62	0.82	0.706	1.05	0.670	0.93	1.30	0.943	No
693	45.49	2.79	1.17	1.62	0.82	0.706	1.05	0.670	0.93	1.30	0.943	No
694	45.55	2.80	1.17	1.62	0.82	0.706	1.05	0.670	0.93	1.30	0.943	No
695	45.61	2.80	1.17	1.63	0.82	0.706	1.05	0.670	0.93	1.30	0.942	No
696	45.67	2.80	1.18	1.63	0.82	0.706	1.05	0.669	0.93	1.30	0.942	No
697	45.76	2.81	1.18	1.63	0.82	0.706	1.05	0.669	0.92	1.30	0.942	No
698	45.82	2.81	1.18	1.63	0.82	0.705	1.05	0.669	0.92	1.30	0.942	No
699	45.88	2.82	1.18	1.64	0.82	0.705	1.05	0.669	0.93	1.30	0.942	No
700	45.94	2.82	1.18	1.64	0.82	0.705	1.05	0.669	0.93	1.30	0.942	No
701	46.00	2.83	1.19	1.64	0.82	0.705	1.05	0.669	0.93	1.30	0.943	No
702	46.09	2.83	1.19	1.64	0.82	0.705	1.05	0.668	0.93	1.30	0.943	No
703	46.15	2.84	1.19	1.65	0.82	0.705	1.05	0.668	0.93	1.30	0.943	No
704	46.21	2.84	1.19	1.65	0.82	0.704	1.05	0.668	0.93	1.30	0.943	No
705	46.27	2.84	1.19	1.65	0.82	0.704	1.05	0.668	0.94	1.30	0.944	No
706	46.33	2.85	1.20	1.65	0.82	0.704	1.05	0.668	0.94	1.30	0.944	No
707	46.42	2.85	1.20	1.65	0.82	0.704	1.05	0.668	0.94	1.30	0.944	No
708	46.48	2.86	1.20	1.66	0.82	0.704	1.05	0.667	0.94	1.30	0.944	No
709	46.54	2.86	1.20	1.66	0.81	0.704	1.05	0.667	0.94	1.30	0.944	No
710	46.60	2.86	1.20	1.66	0.81	0.704	1.05	0.667	0.94	1.30	0.944	No
711	46.66	2.87	1.21	1.66	0.81	0.703	1.05	0.667	0.94	1.30	0.944	No
712	46.72	2.87	1.21	1.66	0.81	0.703	1.05	0.667	0.94	1.30	0.944	No
713	46.80	2.88	1.21	1.67	0.81	0.703	1.05	0.667	0.94	1.30	0.944	No
714	46.86	2.88	1.21	1.67	0.81	0.703	1.05	0.667	0.94	1.30	0.944	No
715	46.93	2.88	1.21	1.67	0.81	0.703	1.05	0.667	0.94	1.30	0.944	No
716	46.98	2.89	1.22	1.67	0.81	0.703	1.05	0.666	0.94	1.30	0.944	No
717	47.07	2.89	1.22	1.67	0.81	0.702	1.05	0.666	0.94	1.30	0.944	No
718	47.13	2.90	1.22	1.68	0.81	0.702	1.05	0.666	0.95	1.30	0.944	No
719	47.19	2.90	1.22	1.68	0.81	0.702	1.05	0.666	0.95	1.30	0.944	No
720	47.25	2.90	1.22	1.68	0.81	0.702	1.05	0.666	0.95	1.30	0.943	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
721	47.31	2.91	1.23	1.68	0.81	0.702	1.05	0.666	0.95	1.30	0.943	No
722	47.40	2.91	1.23	1.68	0.81	0.702	1.05	0.666	0.95	1.30	0.943	No
723	47.46	2.92	1.23	1.69	0.81	0.702	1.05	0.665	0.95	1.30	0.943	No
724	47.52	2.92	1.23	1.69	0.81	0.701	1.05	0.665	0.95	1.30	0.942	No
725	47.58	2.93	1.23	1.69	0.81	0.701	1.05	0.665	0.96	1.30	0.941	No
726	47.64	2.93	1.24	1.69	0.81	0.701	1.05	0.665	0.96	1.30	0.941	No
727	47.73	2.93	1.24	1.69	0.81	0.701	1.05	0.665	0.96	1.30	0.940	No
728	47.79	2.94	1.24	1.70	0.81	0.701	1.05	0.665	0.96	1.30	0.940	No
729	47.85	2.94	1.24	1.70	0.81	0.701	1.05	0.665	0.96	1.30	0.940	No
730	47.91	2.95	1.25	1.70	0.81	0.701	1.05	0.665	0.96	1.30	0.940	No
731	47.97	2.95	1.25	1.70	0.81	0.701	1.05	0.664	0.96	1.30	0.941	No
732	48.03	2.95	1.25	1.70	0.81	0.700	1.05	0.664	0.95	1.30	0.941	No
733	48.12	2.96	1.25	1.71	0.81	0.700	1.05	0.664	0.95	1.30	0.941	No
734	48.18	2.96	1.25	1.71	0.81	0.700	1.05	0.664	0.95	1.30	0.941	No
735	48.24	2.97	1.26	1.71	0.81	0.700	1.05	0.664	0.95	1.30	0.941	No
736	48.30	2.97	1.26	1.71	0.81	0.700	1.05	0.664	0.95	1.30	0.941	No
737	48.36	2.97	1.26	1.71	0.81	0.700	1.05	0.664	0.96	1.30	0.940	No
738	48.45	2.98	1.26	1.72	0.81	0.700	1.05	0.664	0.96	1.30	0.940	No
739	48.51	2.98	1.26	1.72	0.81	0.700	1.05	0.663	0.96	1.30	0.940	No
740	48.57	2.99	1.27	1.72	0.80	0.699	1.05	0.663	0.96	1.30	0.940	No
741	48.63	2.99	1.27	1.72	0.80	0.699	1.05	0.663	0.96	1.30	0.940	No
742	48.69	2.99	1.27	1.72	0.80	0.699	1.05	0.663	0.96	1.30	0.940	No
743	48.78	3.00	1.27	1.73	0.80	0.699	1.05	0.663	0.96	1.30	0.939	No
744	48.84	3.00	1.27	1.73	0.80	0.699	1.05	0.663	0.96	1.30	0.939	No
745	48.90	3.00	1.28	1.73	0.80	0.699	1.05	0.663	0.96	1.30	0.939	No
746	48.96	3.01	1.28	1.73	0.80	0.699	1.05	0.663	0.96	1.30	0.939	No
747	49.03	3.01	1.28	1.73	0.80	0.698	1.05	0.662	0.96	1.30	0.939	No
748	49.09	3.02	1.28	1.73	0.80	0.698	1.05	0.662	0.96	1.30	0.939	No
749	49.15	3.02	1.28	1.74	0.80	0.698	1.05	0.662	0.96	1.30	0.938	No
750	49.21	3.02	1.29	1.74	0.80	0.698	1.05	0.662	0.95	1.30	0.941	No
751	49.30	3.03	1.29	1.74	0.80	0.698	1.05	0.662	0.94	1.30	0.942	No
752	49.36	3.03	1.29	1.74	0.80	0.698	1.05	0.662	0.94	1.30	0.942	No
753	49.42	3.04	1.29	1.74	0.80	0.698	1.05	0.662	0.93	1.30	0.943	No
754	49.48	3.04	1.29	1.75	0.80	0.697	1.05	0.661	0.93	1.30	0.943	No
755	49.55	3.05	1.30	1.75	0.80	0.697	1.05	0.661	0.92	1.30	0.943	No
756	49.61	3.05	1.30	1.75	0.80	0.697	1.05	0.661	0.91	1.30	0.943	No
757	49.70	3.05	1.30	1.75	0.80	0.697	1.05	0.661	0.92	1.30	0.943	No
758	49.76	3.06	1.30	1.76	0.80	0.697	1.05	0.661	0.92	1.30	0.943	No
759	49.82	3.06	1.30	1.76	0.80	0.696	1.05	0.661	0.91	1.30	0.943	No
760	49.88	3.07	1.31	1.76	0.80	0.696	1.05	0.660	0.91	1.30	0.943	No
761	49.94	3.07	1.31	1.76	0.80	0.696	1.05	0.660	0.91	1.30	0.943	No
762	50.00	3.07	1.31	1.76	0.80	0.696	1.05	0.660	0.91	1.30	2.000	No
763	50.07	3.08	1.31	1.77	0.80	0.696	1.05	0.660	0.91	1.30	2.000	No
764	50.14	3.08	1.31	1.77	0.80	0.696	1.05	0.660	0.91	1.30	2.000	No
765	50.20	3.09	1.32	1.77	0.80	0.695	1.05	0.660	0.90	1.30	2.000	No
766	50.27	3.09	1.32	1.77	0.80	0.695	1.05	0.659	0.91	1.30	2.000	No
767	50.34	3.10	1.32	1.77	0.80	0.695	1.05	0.659	0.91	1.30	2.000	No
768	50.41	3.10	1.32	1.78	0.80	0.695	1.05	0.659	0.91	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
769	50.46	3.10	1.32	1.78	0.80	0.695	1.05	0.659	0.91	1.30	2.000	No
770	50.54	3.11	1.33	1.78	0.80	0.694	1.05	0.659	0.91	1.30	2.000	No
771	50.61	3.11	1.33	1.78	0.79	0.694	1.05	0.658	0.91	1.30	2.000	No
772	50.67	3.12	1.33	1.79	0.79	0.694	1.05	0.658	0.91	1.30	2.000	No
773	50.74	3.12	1.33	1.79	0.79	0.694	1.05	0.658	0.91	1.30	2.000	No
774	50.79	3.12	1.34	1.79	0.79	0.694	1.05	0.658	0.91	1.30	2.000	No
775	50.85	3.13	1.34	1.79	0.79	0.694	1.05	0.658	0.91	1.30	2.000	No
776	50.94	3.13	1.34	1.79	0.79	0.693	1.05	0.658	0.90	1.30	2.000	No
777	51.01	3.14	1.34	1.80	0.79	0.693	1.05	0.657	0.90	1.30	2.000	No
778	51.06	3.14	1.34	1.80	0.79	0.693	1.05	0.657	0.90	1.30	2.000	No
779	51.13	3.15	1.35	1.80	0.79	0.693	1.05	0.657	0.90	1.30	2.000	No
780	51.18	3.15	1.35	1.80	0.79	0.693	1.05	0.657	0.90	1.30	2.000	No
781	51.27	3.16	1.35	1.81	0.79	0.692	1.05	0.657	0.90	1.30	2.000	No
782	51.33	3.16	1.35	1.81	0.79	0.692	1.05	0.656	0.90	1.30	2.000	No
783	51.38	3.16	1.35	1.81	0.79	0.692	1.05	0.656	0.90	1.30	2.000	No
784	51.46	3.17	1.36	1.81	0.79	0.692	1.05	0.656	0.90	1.30	2.000	No
785	51.52	3.17	1.36	1.81	0.79	0.692	1.05	0.656	0.90	1.30	2.000	No
786	51.58	3.18	1.36	1.82	0.79	0.691	1.05	0.656	0.90	1.30	2.000	No
787	51.64	3.18	1.36	1.82	0.79	0.691	1.05	0.656	0.90	1.30	2.000	No
788	51.73	3.19	1.36	1.82	0.79	0.691	1.05	0.655	0.90	1.30	2.000	No
789	51.79	3.19	1.37	1.82	0.79	0.691	1.05	0.655	0.90	1.30	2.000	No
790	51.85	3.19	1.37	1.83	0.79	0.691	1.05	0.655	0.89	1.30	2.000	No
791	51.91	3.20	1.37	1.83	0.79	0.690	1.05	0.655	0.89	1.30	2.000	No
792	51.98	3.20	1.37	1.83	0.79	0.690	1.05	0.655	0.89	1.30	2.000	No
793	52.05	3.21	1.37	1.83	0.79	0.690	1.05	0.654	0.88	1.30	2.000	No
794	52.10	3.21	1.38	1.83	0.79	0.690	1.05	0.654	0.88	1.30	2.000	No
795	52.18	3.21	1.38	1.84	0.79	0.690	1.05	0.654	0.88	1.30	2.000	No
796	52.23	3.22	1.38	1.84	0.79	0.689	1.05	0.654	0.88	1.30	2.000	No
797	52.31	3.22	1.38	1.84	0.79	0.689	1.05	0.654	0.88	1.30	2.000	No
798	52.36	3.23	1.38	1.84	0.79	0.689	1.05	0.654	0.88	1.30	2.000	No
799	52.44	3.23	1.39	1.85	0.79	0.689	1.05	0.653	0.88	1.30	2.000	No
800	52.51	3.24	1.39	1.85	0.79	0.689	1.05	0.653	0.89	1.30	2.000	No
801	52.57	3.24	1.39	1.85	0.79	0.688	1.05	0.653	0.89	1.30	2.000	No
802	52.63	3.24	1.39	1.85	0.78	0.688	1.05	0.653	0.89	1.30	2.000	No
803	52.72	3.25	1.40	1.85	0.78	0.688	1.05	0.652	0.89	1.30	2.000	No
804	52.77	3.25	1.40	1.86	0.78	0.688	1.05	0.652	0.90	1.30	2.000	No
805	52.84	3.26	1.40	1.86	0.78	0.688	1.05	0.652	0.90	1.30	2.000	No
806	52.90	3.26	1.40	1.86	0.78	0.687	1.05	0.652	0.90	1.30	2.000	No
807	52.95	3.27	1.40	1.86	0.78	0.687	1.05	0.652	0.90	1.30	2.000	No
808	53.04	3.27	1.41	1.87	0.78	0.687	1.05	0.652	0.91	1.30	2.000	No
809	53.10	3.27	1.41	1.87	0.78	0.687	1.05	0.651	0.91	1.30	2.000	No
810	53.16	3.28	1.41	1.87	0.78	0.687	1.05	0.651	0.91	1.30	2.000	No
811	53.23	3.28	1.41	1.87	0.78	0.686	1.05	0.651	0.91	1.30	2.000	No
812	53.29	3.29	1.41	1.87	0.78	0.686	1.05	0.651	0.91	1.30	2.000	No
813	53.35	3.29	1.41	1.88	0.78	0.686	1.05	0.651	0.91	1.30	2.000	No
814	53.44	3.30	1.42	1.88	0.78	0.686	1.05	0.650	0.91	1.30	2.000	No
815	53.50	3.30	1.42	1.88	0.78	0.686	1.05	0.650	0.91	1.30	2.000	No
816	53.56	3.30	1.42	1.88	0.78	0.685	1.05	0.650	0.92	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
817	53.62	3.31	1.42	1.88	0.78	0.685	1.05	0.650	0.92	1.30	2.000	No
818	53.67	3.31	1.43	1.89	0.78	0.685	1.05	0.650	0.92	1.30	2.000	No
819	53.76	3.32	1.43	1.89	0.78	0.685	1.05	0.650	0.92	1.30	2.000	No
820	53.82	3.32	1.43	1.89	0.78	0.685	1.05	0.649	0.92	1.30	2.000	No
821	53.88	3.32	1.43	1.89	0.78	0.685	1.05	0.649	0.92	1.30	2.000	No
822	53.94	3.33	1.43	1.90	0.78	0.684	1.05	0.649	0.92	1.30	2.000	No
823	54.00	3.33	1.44	1.90	0.78	0.684	1.05	0.649	0.92	1.30	2.000	No
824	54.09	3.34	1.44	1.90	0.78	0.684	1.05	0.649	0.92	1.30	2.000	No
825	54.16	3.34	1.44	1.90	0.78	0.684	1.05	0.648	0.92	1.30	2.000	No
826	54.22	3.35	1.44	1.90	0.78	0.684	1.05	0.648	0.92	1.30	2.000	No
827	54.27	3.35	1.44	1.91	0.78	0.683	1.05	0.648	0.93	1.30	2.000	No
828	54.34	3.35	1.45	1.91	0.78	0.683	1.05	0.648	0.93	1.30	2.000	No
829	54.41	3.36	1.45	1.91	0.78	0.683	1.05	0.648	0.92	1.30	2.000	No
830	54.47	3.36	1.45	1.91	0.78	0.683	1.05	0.648	0.92	1.30	2.000	No
831	54.56	3.37	1.45	1.91	0.78	0.683	1.05	0.647	0.92	1.30	2.000	No
832	54.62	3.37	1.45	1.92	0.78	0.682	1.05	0.647	0.92	1.30	2.000	No
833	54.68	3.37	1.46	1.92	0.77	0.682	1.05	0.647	0.92	1.30	2.000	No
834	54.74	3.38	1.46	1.92	0.77	0.682	1.05	0.647	0.92	1.30	2.000	No
835	54.80	3.38	1.46	1.92	0.77	0.682	1.05	0.647	0.92	1.30	2.000	No
836	54.86	3.39	1.46	1.92	0.77	0.682	1.05	0.647	0.92	1.30	2.000	No
837	54.95	3.39	1.46	1.93	0.77	0.682	1.05	0.646	0.92	1.30	2.000	No
838	55.01	3.40	1.47	1.93	0.77	0.681	1.05	0.646	0.92	1.30	2.000	No
839	55.07	3.40	1.47	1.93	0.77	0.681	1.05	0.646	0.93	1.30	2.000	No
840	55.13	3.40	1.47	1.93	0.77	0.681	1.05	0.646	0.93	1.30	2.000	No
841	55.19	3.41	1.47	1.93	0.77	0.681	1.05	0.646	0.93	1.30	2.000	No
842	55.28	3.41	1.48	1.94	0.77	0.681	1.05	0.645	0.93	1.30	2.000	No
843	55.34	3.42	1.48	1.94	0.77	0.680	1.05	0.645	0.92	1.30	2.000	No
844	55.40	3.42	1.48	1.94	0.77	0.680	1.05	0.645	0.92	1.30	2.000	No
845	55.45	3.42	1.48	1.94	0.77	0.680	1.05	0.645	0.92	1.30	2.000	No
846	55.51	3.43	1.48	1.94	0.77	0.680	1.05	0.645	0.92	1.30	2.000	No
847	55.60	3.43	1.49	1.95	0.77	0.680	1.05	0.645	0.92	1.30	2.000	No
848	55.66	3.44	1.49	1.95	0.77	0.680	1.05	0.644	0.92	1.30	2.000	No
849	55.73	3.44	1.49	1.95	0.77	0.679	1.05	0.644	0.92	1.30	2.000	No
850	55.79	3.44	1.49	1.95	0.77	0.679	1.05	0.644	0.92	1.30	2.000	No
851	55.84	3.45	1.49	1.96	0.77	0.679	1.05	0.644	0.92	1.30	2.000	No
852	55.94	3.45	1.50	1.96	0.77	0.679	1.05	0.644	0.92	1.30	2.000	No
853	56.00	3.46	1.50	1.96	0.77	0.679	1.05	0.644	0.92	1.30	2.000	No
854	56.06	3.46	1.50	1.96	0.77	0.678	1.05	0.643	0.91	1.30	2.000	No
855	56.12	3.47	1.50	1.96	0.77	0.678	1.05	0.643	0.91	1.30	2.000	No
856	56.18	3.47	1.50	1.97	0.77	0.678	1.05	0.643	0.91	1.30	2.000	No
857	56.24	3.47	1.51	1.97	0.77	0.678	1.05	0.643	0.91	1.30	2.000	No
858	56.30	3.48	1.51	1.97	0.77	0.678	1.05	0.643	0.91	1.30	2.000	No
859	56.39	3.48	1.51	1.97	0.77	0.677	1.05	0.642	0.90	1.30	2.000	No
860	56.43	3.49	1.51	1.97	0.77	0.677	1.05	0.642	0.90	1.30	2.000	No
861	56.50	3.49	1.51	1.98	0.77	0.677	1.05	0.642	0.90	1.30	2.000	No
862	56.56	3.49	1.52	1.98	0.77	0.677	1.05	0.642	0.90	1.30	2.000	No
863	56.65	3.50	1.52	1.98	0.77	0.677	1.05	0.642	0.90	1.30	2.000	No
864	56.71	3.50	1.52	1.98	0.77	0.676	1.05	0.642	0.90	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
865	56.77	3.51	1.52	1.99	0.76	0.676	1.05	0.641	0.90	1.30	2.000	No
866	56.84	3.51	1.52	1.99	0.76	0.676	1.05	0.641	0.90	1.30	2.000	No
867	56.89	3.51	1.53	1.99	0.76	0.676	1.05	0.641	0.90	1.30	2.000	No
868	56.98	3.52	1.53	1.99	0.76	0.676	1.05	0.641	0.90	1.30	2.000	No
869	57.04	3.52	1.53	1.99	0.76	0.675	1.05	0.641	0.89	1.30	2.000	No
870	57.10	3.53	1.53	2.00	0.76	0.675	1.05	0.640	0.89	1.30	2.000	No
871	57.16	3.53	1.53	2.00	0.76	0.675	1.05	0.640	0.89	1.30	2.000	No
872	57.22	3.54	1.54	2.00	0.76	0.675	1.05	0.640	0.89	1.30	2.000	No
873	57.31	3.54	1.54	2.00	0.76	0.675	1.05	0.640	0.89	1.30	2.000	No
874	57.37	3.55	1.54	2.00	0.76	0.674	1.05	0.640	0.89	1.30	2.000	No
875	57.43	3.55	1.54	2.01	0.76	0.674	1.05	0.640	0.88	1.30	2.000	No
876	57.49	3.55	1.54	2.01	0.76	0.674	1.05	0.639	0.88	1.30	2.000	No
877	57.55	3.56	1.55	2.01	0.76	0.674	1.05	0.639	0.88	1.30	2.000	No
878	57.61	3.56	1.55	2.01	0.76	0.674	1.05	0.639	0.87	1.30	2.000	No
879	57.70	3.57	1.55	2.02	0.76	0.673	1.05	0.639	0.87	1.30	2.000	No
880	57.76	3.57	1.55	2.02	0.76	0.673	1.05	0.639	0.87	1.30	2.000	No
881	57.82	3.57	1.55	2.02	0.76	0.673	1.05	0.638	0.87	1.30	2.000	No
882	57.88	3.58	1.56	2.02	0.76	0.673	1.05	0.638	0.87	1.30	2.000	No
883	57.94	3.58	1.56	2.02	0.76	0.673	1.05	0.638	0.86	1.30	2.000	No
884	58.03	3.59	1.56	2.03	0.76	0.672	1.05	0.638	0.86	1.30	2.000	No
885	58.09	3.59	1.56	2.03	0.76	0.672	1.05	0.638	0.86	1.30	2.000	No
886	58.16	3.60	1.56	2.03	0.76	0.672	1.05	0.637	0.85	1.30	2.000	No
887	58.22	3.60	1.57	2.03	0.76	0.672	1.05	0.637	0.85	1.30	2.000	No
888	58.28	3.60	1.57	2.03	0.76	0.672	1.05	0.637	0.85	1.30	2.000	No
889	58.34	3.61	1.57	2.04	0.76	0.671	1.05	0.637	0.84	1.30	2.000	No
890	58.42	3.61	1.57	2.04	0.76	0.671	1.05	0.637	0.84	1.30	2.000	No
891	58.48	3.62	1.58	2.04	0.76	0.671	1.05	0.636	0.83	1.30	2.000	No
892	58.55	3.62	1.58	2.04	0.76	0.671	1.05	0.636	0.83	1.30	2.000	No
893	58.60	3.63	1.58	2.05	0.76	0.671	1.05	0.636	0.82	1.30	2.000	No
894	58.67	3.63	1.58	2.05	0.76	0.670	1.05	0.636	0.82	1.30	2.000	No
895	58.75	3.63	1.58	2.05	0.76	0.670	1.05	0.636	0.81	1.30	2.000	No
896	58.81	3.64	1.59	2.05	0.76	0.670	1.05	0.635	0.81	1.30	2.000	No
897	58.87	3.64	1.59	2.06	0.75	0.670	1.05	0.635	0.83	1.30	2.000	No
898	58.94	3.65	1.59	2.06	0.75	0.669	1.05	0.635	0.87	1.30	2.000	No
899	59.00	3.65	1.59	2.06	0.75	0.669	1.05	0.635	0.86	1.30	2.000	No
900	59.06	3.65	1.59	2.06	0.75	0.669	1.05	0.635	0.86	1.30	2.000	No
901	59.15	3.66	1.60	2.06	0.75	0.669	1.05	0.634	0.84	1.30	2.000	No
902	59.20	3.66	1.60	2.07	0.75	0.669	1.05	0.634	0.84	1.30	2.000	No
903	59.27	3.67	1.60	2.07	0.75	0.668	1.05	0.634	0.83	1.30	2.000	No
904	59.32	3.67	1.60	2.07	0.75	0.668	1.05	0.634	0.83	1.30	2.000	No
905	59.40	3.68	1.60	2.07	0.75	0.668	1.05	0.634	0.82	1.30	2.000	No
906	59.46	3.68	1.61	2.08	0.75	0.668	1.05	0.633	0.81	1.30	2.000	No
907	59.53	3.69	1.61	2.08	0.75	0.668	1.05	0.633	0.80	1.30	2.000	No
908	59.58	3.69	1.61	2.08	0.75	0.667	1.05	0.633	0.80	1.30	2.000	No
909	59.66	3.69	1.61	2.08	0.75	0.667	1.05	0.633	0.80	1.30	2.000	No
910	59.73	3.70	1.61	2.08	0.75	0.667	1.05	0.632	0.80	1.30	2.000	No
911	59.79	3.70	1.62	2.09	0.75	0.667	1.05	0.632	0.82	1.30	2.000	No
912	59.86	3.71	1.62	2.09	0.75	0.666	1.05	0.632	0.89	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
913	59.93	3.71	1.62	2.09	0.75	0.666	1.05	0.632	0.89	1.30	2.000	No
914	59.98	3.71	1.62	2.09	0.75	0.666	1.05	0.632	0.89	1.30	2.000	No
915	60.05	3.72	1.62	2.09	0.75	0.666	1.05	0.632	0.89	1.30	2.000	No
916	60.12	3.72	1.63	2.10	0.75	0.666	1.05	0.631	0.90	1.30	2.000	No
917	60.19	3.73	1.63	2.10	0.75	0.665	1.05	0.631	0.89	1.30	2.000	No
918	60.24	3.73	1.63	2.10	0.75	0.665	1.05	0.631	0.88	1.30	2.000	No
919	60.32	3.74	1.63	2.10	0.75	0.665	1.05	0.631	0.85	1.30	2.000	No
920	60.38	3.74	1.63	2.11	0.75	0.665	1.05	0.631	0.83	1.30	2.000	No
921	60.44	3.74	1.64	2.11	0.75	0.665	1.05	0.630	0.82	1.30	2.000	No
922	60.50	3.75	1.64	2.11	0.75	0.664	1.05	0.630	0.82	1.30	2.000	No
923	60.59	3.75	1.64	2.11	0.75	0.664	1.05	0.630	0.81	1.30	2.000	No
924	60.65	3.76	1.64	2.12	0.75	0.664	1.05	0.630	0.81	1.30	2.000	No
925	60.71	3.76	1.64	2.12	0.75	0.664	1.05	0.630	0.80	1.30	2.000	No
926	60.77	3.77	1.65	2.12	0.75	0.664	1.05	0.629	0.81	1.30	2.000	No
927	60.83	3.77	1.65	2.12	0.75	0.663	1.05	0.629	0.81	1.30	2.000	No
928	60.89	3.77	1.65	2.12	0.75	0.663	1.05	0.629	0.81	1.30	2.000	No
929	60.98	3.78	1.65	2.13	0.75	0.663	1.05	0.629	0.80	1.30	2.000	No
930	61.04	3.78	1.65	2.13	0.74	0.663	1.05	0.629	0.80	1.30	2.000	No
931	61.10	3.79	1.66	2.13	0.74	0.663	1.05	0.628	0.80	1.30	2.000	No
932	61.16	3.79	1.66	2.13	0.74	0.662	1.05	0.628	0.79	1.30	2.000	No
933	61.22	3.80	1.66	2.13	0.74	0.662	1.05	0.628	0.79	1.30	2.000	No
934	61.31	3.80	1.66	2.14	0.74	0.662	1.05	0.628	0.79	1.30	2.000	No
935	61.37	3.81	1.67	2.14	0.74	0.662	1.05	0.627	0.79	1.30	2.000	No
936	61.43	3.81	1.67	2.14	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
937	61.49	3.81	1.67	2.14	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
938	61.55	3.82	1.67	2.15	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
939	61.64	3.82	1.67	2.15	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
940	61.70	3.83	1.68	2.15	0.74	0.660	1.05	0.626	0.79	1.30	2.000	No
941	61.76	3.83	1.68	2.15	0.74	0.660	1.05	0.626	0.79	1.30	2.000	No
942	61.82	3.83	1.68	2.16	0.74	0.660	1.05	0.626	0.80	1.30	2.000	No
943	61.88	3.84	1.68	2.16	0.74	0.660	1.05	0.626	0.84	1.30	2.000	No
944	61.94	3.84	1.68	2.16	0.74	0.660	1.05	0.626	0.83	1.30	2.000	No
945	62.04	3.85	1.69	2.16	0.74	0.659	1.05	0.625	0.83	1.30	2.000	No
946	62.10	3.85	1.69	2.16	0.74	0.659	1.05	0.625	0.82	1.30	2.000	No
947	62.16	3.86	1.69	2.17	0.74	0.659	1.05	0.625	0.82	1.30	2.000	No
948	62.22	3.86	1.69	2.17	0.74	0.659	1.05	0.625	0.82	1.30	2.000	No
949	62.29	3.86	1.69	2.17	0.74	0.659	1.05	0.625	0.83	1.30	2.000	No
950	62.34	3.87	1.70	2.17	0.74	0.658	1.05	0.624	0.83	1.30	2.000	No
951	62.43	3.87	1.70	2.18	0.74	0.658	1.05	0.624	0.83	1.30	2.000	No
952	62.49	3.88	1.70	2.18	0.74	0.658	1.05	0.624	0.83	1.30	2.000	No
953	62.55	3.88	1.70	2.18	0.74	0.658	1.05	0.624	0.83	1.30	2.000	No
954	62.61	3.89	1.70	2.18	0.74	0.658	1.05	0.624	0.83	1.30	2.000	No
955	62.67	3.89	1.71	2.18	0.74	0.657	1.05	0.623	0.83	1.30	2.000	No
956	62.73	3.89	1.71	2.19	0.74	0.657	1.05	0.623	0.83	1.30	2.000	No
957	62.82	3.90	1.71	2.19	0.74	0.657	1.05	0.623	0.84	1.30	2.000	No
958	62.88	3.90	1.71	2.19	0.74	0.657	1.05	0.623	0.84	1.30	2.000	No
959	62.94	3.91	1.71	2.19	0.74	0.656	1.05	0.623	0.84	1.30	2.000	No
960	63.00	3.91	1.72	2.20	0.74	0.656	1.05	0.622	0.84	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
961	63.06	3.92	1.72	2.20	0.74	0.656	1.05	0.622	0.84	1.30	2.000	No
962	63.12	3.92	1.72	2.20	0.74	0.656	1.05	0.622	0.84	1.30	2.000	No
963	63.21	3.93	1.72	2.20	0.73	0.656	1.05	0.622	0.84	1.30	2.000	No
964	63.27	3.93	1.72	2.20	0.73	0.655	1.05	0.622	0.84	1.30	2.000	No
965	63.33	3.93	1.73	2.21	0.73	0.655	1.05	0.621	0.84	1.30	2.000	No
966	63.40	3.94	1.73	2.21	0.73	0.655	1.05	0.621	0.85	1.30	2.000	No
967	63.46	3.94	1.73	2.21	0.73	0.655	1.05	0.621	0.85	1.30	2.000	No
968	63.55	3.95	1.73	2.21	0.73	0.655	1.05	0.621	0.85	1.30	2.000	No
969	63.60	3.95	1.73	2.22	0.73	0.654	1.05	0.621	0.85	1.30	2.000	No
970	63.66	3.95	1.74	2.22	0.73	0.654	1.05	0.620	0.86	1.30	2.000	No
971	63.73	3.96	1.74	2.22	0.73	0.654	1.05	0.620	0.86	1.30	2.000	No
972	63.78	3.96	1.74	2.22	0.73	0.654	1.05	0.620	0.87	1.30	2.000	No
973	63.87	3.97	1.74	2.22	0.73	0.653	1.05	0.620	0.88	1.30	2.000	No
974	63.94	3.97	1.75	2.23	0.73	0.653	1.05	0.620	0.89	1.30	2.000	No
975	63.99	3.98	1.75	2.23	0.73	0.653	1.05	0.619	0.90	1.30	2.000	No
976	64.05	3.98	1.75	2.23	0.73	0.653	1.05	0.619	0.91	1.30	2.000	No
977	64.12	3.98	1.75	2.23	0.73	0.653	1.05	0.619	0.92	1.30	2.000	No
978	64.18	3.99	1.75	2.23	0.73	0.653	1.05	0.619	0.92	1.30	2.000	No
979	64.27	3.99	1.76	2.24	0.73	0.652	1.05	0.619	0.92	1.30	2.000	No
980	64.33	4.00	1.76	2.24	0.73	0.652	1.05	0.618	0.92	1.30	2.000	No
981	64.39	4.00	1.76	2.24	0.73	0.652	1.05	0.618	0.93	1.30	2.000	No
982	64.44	4.00	1.76	2.24	0.73	0.652	1.05	0.618	0.93	1.30	2.000	No
983	64.51	4.01	1.76	2.25	0.73	0.652	1.05	0.618	0.92	1.30	2.000	No
984	64.57	4.01	1.77	2.25	0.73	0.651	1.05	0.618	0.91	1.30	2.000	No
985	64.63	4.02	1.77	2.25	0.73	0.651	1.05	0.618	0.90	1.30	2.000	No
986	64.72	4.02	1.77	2.25	0.73	0.651	1.05	0.617	0.88	1.30	2.000	No
987	64.79	4.03	1.77	2.25	0.73	0.651	1.05	0.617	0.87	1.30	2.000	No
988	64.85	4.03	1.77	2.26	0.73	0.651	1.05	0.617	0.86	1.30	2.000	No
989	64.91	4.03	1.78	2.26	0.73	0.650	1.05	0.617	0.85	1.30	2.000	No
990	64.96	4.04	1.78	2.26	0.73	0.650	1.05	0.617	0.85	1.30	2.000	No
991	65.05	4.04	1.78	2.26	0.73	0.650	1.05	0.616	0.83	1.30	2.000	No
992	65.11	4.05	1.78	2.27	0.73	0.650	1.05	0.616	0.82	1.30	2.000	No
993	65.18	4.05	1.78	2.27	0.73	0.649	1.05	0.616	0.81	1.30	2.000	No
994	65.23	4.05	1.79	2.27	0.73	0.649	1.05	0.616	0.80	1.30	2.000	No
995	65.29	4.06	1.79	2.27	0.73	0.649	1.05	0.616	0.79	1.30	2.000	No
996	65.38	4.06	1.79	2.27	0.73	0.649	1.05	0.615	0.78	1.30	2.000	No
997	65.44	4.07	1.79	2.28	0.73	0.649	1.05	0.615	0.77	1.30	2.000	No
998	65.50	4.07	1.79	2.28	0.72	0.648	1.05	0.615	0.77	1.30	2.000	No
999	65.56	4.08	1.80	2.28	0.72	0.648	1.05	0.615	0.77	1.30	2.000	No
1000	65.63	4.08	1.80	2.28	0.72	0.648	1.05	0.615	0.77	1.30	2.000	No
1001	65.69	4.08	1.80	2.28	0.72	0.648	1.05	0.614	0.77	1.30	2.000	No
1002	65.77	4.09	1.80	2.29	0.72	0.647	1.05	0.614	0.77	1.30	2.000	No
1003	65.83	4.09	1.80	2.29	0.72	0.647	1.05	0.614	0.77	1.30	2.000	No
1004	65.89	4.10	1.81	2.29	0.72	0.647	1.05	0.614	0.77	1.30	2.000	No
1005	65.95	4.10	1.81	2.29	0.72	0.647	1.05	0.614	0.77	1.30	2.000	No
1006	66.01	4.11	1.81	2.30	0.72	0.647	1.05	0.613	0.77	1.30	2.000	No
1007	66.10	4.11	1.81	2.30	0.72	0.646	1.05	0.613	0.77	1.30	2.000	No
1008	66.16	4.12	1.81	2.30	0.72	0.646	1.05	0.613	0.77	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1009	66.23	4.12	1.82	2.30	0.72	0.646	1.05	0.613	0.80	1.30	2.000	No
1010	66.29	4.12	1.82	2.31	0.72	0.646	1.05	0.612	0.83	1.30	2.000	No
1011	66.35	4.13	1.82	2.31	0.72	0.646	1.05	0.612	0.83	1.30	2.000	No
1012	66.41	4.13	1.82	2.31	0.72	0.645	1.05	0.612	0.83	1.30	2.000	No
1013	66.47	4.14	1.82	2.31	0.72	0.645	1.05	0.612	0.82	1.30	2.000	No
1014	66.54	4.14	1.83	2.31	0.72	0.645	1.05	0.612	0.80	1.30	2.000	No
1015	66.62	4.15	1.83	2.32	0.72	0.645	1.05	0.611	0.80	1.30	2.000	No
1016	66.69	4.15	1.83	2.32	0.72	0.644	1.05	0.611	0.80	1.30	2.000	No
1017	66.75	4.15	1.83	2.32	0.72	0.644	1.05	0.611	0.80	1.30	2.000	No
1018	66.81	4.16	1.83	2.32	0.72	0.644	1.05	0.611	0.80	1.30	2.000	No
1019	66.86	4.16	1.84	2.33	0.72	0.644	1.05	0.611	0.80	1.30	2.000	No
1020	66.95	4.17	1.84	2.33	0.72	0.644	1.05	0.610	0.81	1.30	2.000	No
1021	67.01	4.17	1.84	2.33	0.72	0.643	1.05	0.610	0.81	1.30	2.000	No
1022	67.07	4.18	1.84	2.33	0.72	0.643	1.05	0.610	0.82	1.30	2.000	No
1023	67.13	4.18	1.84	2.33	0.72	0.643	1.05	0.610	0.83	1.30	2.000	No
1024	67.19	4.18	1.85	2.34	0.72	0.643	1.05	0.610	0.83	1.30	2.000	No
1025	67.28	4.19	1.85	2.34	0.72	0.643	1.05	0.609	0.84	1.30	2.000	No
1026	67.34	4.19	1.85	2.34	0.72	0.642	1.05	0.609	0.84	1.30	2.000	No
1027	67.40	4.20	1.85	2.34	0.72	0.642	1.05	0.609	0.85	1.30	2.000	No
1028	67.46	4.20	1.86	2.35	0.72	0.642	1.05	0.609	0.85	1.30	2.000	No
1029	67.52	4.20	1.86	2.35	0.72	0.642	1.05	0.609	0.85	1.30	2.000	No
1030	67.61	4.21	1.86	2.35	0.72	0.642	1.05	0.608	0.85	1.30	2.000	No
1031	67.67	4.21	1.86	2.35	0.72	0.641	1.05	0.608	0.85	1.30	2.000	No
1032	67.73	4.22	1.86	2.35	0.72	0.641	1.05	0.608	0.85	1.30	2.000	No
1033	67.79	4.22	1.87	2.36	0.71	0.641	1.05	0.608	0.85	1.30	2.000	No
1034	67.85	4.23	1.87	2.36	0.71	0.641	1.05	0.608	0.84	1.30	2.000	No
1035	67.94	4.23	1.87	2.36	0.71	0.640	1.05	0.607	0.83	1.30	2.000	No
1036	68.00	4.24	1.87	2.36	0.71	0.640	1.05	0.607	0.83	1.30	2.000	No
1037	68.06	4.24	1.87	2.37	0.71	0.640	1.05	0.607	0.83	1.30	2.000	No
1038	68.12	4.24	1.88	2.37	0.71	0.640	1.05	0.607	0.84	1.30	2.000	No
1039	68.18	4.25	1.88	2.37	0.71	0.640	1.05	0.607	0.87	1.30	2.000	No
1040	68.24	4.25	1.88	2.37	0.71	0.640	1.05	0.607	0.86	1.30	2.000	No
1041	68.33	4.26	1.88	2.37	0.71	0.639	1.05	0.606	0.85	1.30	2.000	No
1042	68.39	4.26	1.88	2.38	0.71	0.639	1.05	0.606	0.85	1.30	2.000	No
1043	68.45	4.26	1.89	2.38	0.71	0.639	1.05	0.606	0.85	1.30	2.000	No
1044	68.51	4.27	1.89	2.38	0.71	0.639	1.05	0.606	0.84	1.30	2.000	No
1045	68.59	4.27	1.89	2.38	0.71	0.638	1.05	0.606	0.83	1.30	2.000	No
1046	68.65	4.28	1.89	2.38	0.71	0.638	1.05	0.605	0.83	1.30	2.000	No
1047	68.70	4.28	1.89	2.39	0.71	0.638	1.05	0.605	0.82	1.30	2.000	No
1048	68.80	4.29	1.90	2.39	0.71	0.638	1.05	0.605	0.80	1.30	2.000	No
1049	68.86	4.29	1.90	2.39	0.71	0.638	1.05	0.605	0.79	1.30	2.000	No
1050	68.92	4.29	1.90	2.39	0.71	0.637	1.05	0.605	0.77	1.30	2.000	No
1051	68.97	4.30	1.90	2.40	0.71	0.637	1.05	0.604	0.76	1.30	2.000	No
1052	69.04	4.30	1.90	2.40	0.71	0.637	1.05	0.604	0.75	1.30	2.000	No
1053	69.10	4.31	1.91	2.40	0.71	0.637	1.05	0.604	0.75	1.30	2.000	No
1054	69.19	4.31	1.91	2.40	0.71	0.637	1.05	0.604	0.75	1.30	2.000	No
1055	69.25	4.32	1.91	2.41	0.71	0.636	1.05	0.604	0.75	1.30	2.000	No
1056	69.31	4.32	1.91	2.41	0.71	0.636	1.05	0.603	0.75	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1057	69.36	4.32	1.91	2.41	0.71	0.636	1.05	0.603	0.75	1.30	2.000	No
1058	69.42	4.33	1.92	2.41	0.71	0.636	1.05	0.603	0.75	1.30	2.000	No
1059	69.51	4.33	1.92	2.41	0.71	0.636	1.05	0.603	0.75	1.30	2.000	No
1060	69.57	4.34	1.92	2.42	0.71	0.635	1.05	0.603	0.75	1.30	2.000	No
1061	69.63	4.34	1.92	2.42	0.71	0.635	1.05	0.602	0.75	1.30	2.000	No
1062	69.69	4.35	1.92	2.42	0.71	0.635	1.05	0.602	0.75	1.30	2.000	No
1063	69.75	4.35	1.93	2.42	0.71	0.635	1.05	0.602	0.77	1.30	2.000	No
1064	69.84	4.36	1.93	2.43	0.71	0.634	1.05	0.602	0.75	1.30	2.000	No
1065	69.89	4.36	1.93	2.43	0.71	0.634	1.05	0.602	0.75	1.30	2.000	No
1066	69.96	4.36	1.93	2.43	0.71	0.634	1.05	0.601	0.75	1.30	2.000	No
1067	70.02	4.37	1.93	2.43	0.71	0.634	1.05	0.601	0.75	1.30	2.000	No
1068	70.08	4.37	1.94	2.43	0.71	0.634	1.05	0.601	0.75	1.30	2.000	No
1069	70.15	4.38	1.94	2.44	0.70	0.633	1.05	0.601	0.76	1.30	2.000	No
1070	70.21	4.38	1.94	2.44	0.70	0.633	1.05	0.601	0.79	1.30	2.000	No
1071	70.28	4.38	1.94	2.44	0.70	0.633	1.05	0.600	0.82	1.30	2.000	No
1072	70.35	4.39	1.95	2.44	0.70	0.633	1.05	0.600	0.78	1.30	2.000	No
1073	70.41	4.39	1.95	2.45	0.70	0.633	1.05	0.600	0.75	1.30	2.000	No
1074	70.48	4.40	1.95	2.45	0.70	0.632	1.05	0.600	0.75	1.30	2.000	No
1075	70.55	4.40	1.95	2.45	0.70	0.632	1.05	0.600	0.75	1.30	2.000	No
1076	70.61	4.41	1.95	2.45	0.70	0.632	1.05	0.599	0.75	1.30	2.000	No
1077	70.68	4.41	1.96	2.45	0.70	0.632	1.05	0.599	0.75	1.30	2.000	No
1078	70.74	4.41	1.96	2.46	0.70	0.632	1.05	0.599	0.75	1.30	2.000	No
1079	70.81	4.42	1.96	2.46	0.70	0.631	1.05	0.599	0.75	1.30	2.000	No
1080	70.88	4.42	1.96	2.46	0.70	0.631	1.05	0.599	0.75	1.30	2.000	No
1081	70.95	4.43	1.96	2.46	0.70	0.631	1.05	0.598	0.75	1.30	2.000	No
1082	71.00	4.43	1.97	2.47	0.70	0.631	1.05	0.598	0.75	1.30	2.000	No
1083	71.08	4.44	1.97	2.47	0.70	0.631	1.05	0.598	0.75	1.30	2.000	No
1084	71.14	4.44	1.97	2.47	0.70	0.630	1.05	0.598	0.75	1.30	2.000	No
1085	71.20	4.44	1.97	2.47	0.70	0.630	1.05	0.598	0.75	1.30	2.000	No
1086	71.29	4.45	1.97	2.48	0.70	0.630	1.05	0.597	0.75	1.30	2.000	No
1087	71.35	4.45	1.98	2.48	0.70	0.630	1.05	0.597	0.74	1.30	2.000	No
1088	71.41	4.46	1.98	2.48	0.70	0.630	1.05	0.597	0.74	1.30	2.000	No
1089	71.47	4.46	1.98	2.48	0.70	0.629	1.05	0.597	0.74	1.30	2.000	No
1090	71.53	4.47	1.98	2.48	0.70	0.629	1.05	0.597	0.74	1.30	2.000	No
1091	71.59	4.47	1.98	2.49	0.70	0.629	1.05	0.597	0.74	1.30	2.000	No
1092	71.66	4.47	1.99	2.49	0.70	0.629	1.05	0.596	0.74	1.30	2.000	No
1093	71.72	4.48	1.99	2.49	0.70	0.629	1.05	0.596	0.74	1.30	2.000	No
1094	71.79	4.48	1.99	2.49	0.70	0.628	1.05	0.596	0.74	1.30	2.000	No
1095	71.86	4.49	1.99	2.49	0.70	0.628	1.05	0.596	0.74	1.30	2.000	No
1096	71.92	4.49	1.99	2.50	0.70	0.628	1.05	0.596	0.74	1.30	2.000	No
1097	71.98	4.49	2.00	2.50	0.70	0.628	1.05	0.595	0.74	1.30	2.000	No
1098	72.06	4.50	2.00	2.50	0.70	0.628	1.05	0.595	0.74	1.30	2.000	No
1099	72.13	4.50	2.00	2.50	0.70	0.627	1.05	0.595	0.74	1.30	2.000	No
1100	72.19	4.51	2.00	2.51	0.70	0.627	1.05	0.595	0.74	1.30	2.000	No
1101	72.26	4.51	2.00	2.51	0.70	0.627	1.05	0.595	0.74	1.30	2.000	No
1102	72.32	4.52	2.01	2.51	0.70	0.627	1.05	0.594	0.74	1.30	2.000	No
1103	72.38	4.52	2.01	2.51	0.70	0.627	1.05	0.594	0.74	1.30	2.000	No
1104	72.45	4.53	2.01	2.51	0.70	0.626	1.05	0.594	0.74	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1105	72.51	4.53	2.01	2.52	0.70	0.626	1.05	0.594	0.74	1.30	2.000	No
1106	72.58	4.53	2.01	2.52	0.69	0.626	1.05	0.594	0.74	1.30	2.000	No
1107	72.65	4.54	2.02	2.52	0.69	0.626	1.05	0.593	0.74	1.30	2.000	No
1108	72.72	4.54	2.02	2.52	0.69	0.626	1.05	0.593	0.74	1.30	2.000	No
1109	72.77	4.55	2.02	2.52	0.69	0.625	1.05	0.593	0.74	1.30	2.000	No
1110	72.84	4.55	2.02	2.53	0.69	0.625	1.05	0.593	0.74	1.30	2.000	No
1111	72.92	4.56	2.03	2.53	0.69	0.625	1.05	0.593	0.74	1.30	2.000	No
1112	72.98	4.56	2.03	2.53	0.69	0.625	1.05	0.593	0.74	1.30	2.000	No
1113	73.04	4.56	2.03	2.53	0.69	0.625	1.05	0.592	0.74	1.30	2.000	No
1114	73.11	4.57	2.03	2.54	0.69	0.624	1.05	0.592	0.74	1.30	2.000	No
1115	73.17	4.57	2.03	2.54	0.69	0.624	1.05	0.592	0.74	1.30	2.000	No
1116	73.24	4.58	2.04	2.54	0.69	0.624	1.05	0.592	0.74	1.30	2.000	No
1117	73.30	4.58	2.04	2.54	0.69	0.624	1.05	0.592	0.74	1.30	2.000	No
1118	73.37	4.58	2.04	2.54	0.69	0.624	1.05	0.591	0.75	1.30	2.000	No
1119	73.44	4.59	2.04	2.55	0.69	0.623	1.05	0.591	0.74	1.30	2.000	No
1120	73.49	4.59	2.04	2.55	0.69	0.623	1.05	0.591	0.74	1.30	2.000	No
1121	73.57	4.60	2.05	2.55	0.69	0.623	1.05	0.591	0.74	1.30	2.000	No
1122	73.63	4.60	2.05	2.55	0.69	0.623	1.05	0.591	0.74	1.30	2.000	No
1123	73.70	4.61	2.05	2.56	0.69	0.623	1.05	0.591	0.74	1.30	2.000	No
1124	73.77	4.61	2.05	2.56	0.69	0.622	1.05	0.590	0.74	1.30	2.000	No
1125	73.83	4.61	2.05	2.56	0.69	0.622	1.05	0.590	0.73	1.30	2.000	No
1126	73.89	4.62	2.06	2.56	0.69	0.622	1.05	0.590	0.73	1.30	2.000	No
1127	73.95	4.62	2.06	2.56	0.69	0.622	1.05	0.590	0.73	1.30	2.000	No
1128	74.04	4.63	2.06	2.57	0.69	0.622	1.05	0.590	0.73	1.30	2.000	No
1129	74.10	4.63	2.06	2.57	0.69	0.621	1.05	0.589	0.73	1.30	2.000	No
1130	74.16	4.63	2.06	2.57	0.69	0.621	1.05	0.589	0.73	1.30	2.000	No
1131	74.22	4.64	2.07	2.57	0.69	0.621	1.05	0.589	0.73	1.30	2.000	No
1132	74.28	4.64	2.07	2.57	0.69	0.621	1.05	0.589	0.73	1.30	2.000	No
1133	74.37	4.65	2.07	2.58	0.69	0.621	1.05	0.589	0.73	1.30	2.000	No
1134	74.43	4.65	2.07	2.58	0.69	0.621	1.05	0.589	0.73	1.30	2.000	No
1135	74.49	4.66	2.07	2.58	0.69	0.620	1.05	0.588	0.73	1.30	2.000	No
1136	74.55	4.66	2.08	2.58	0.69	0.620	1.05	0.588	0.73	1.30	2.000	No
1137	74.62	4.66	2.08	2.59	0.69	0.620	1.05	0.588	0.81	1.30	2.000	No
1138	74.67	4.67	2.08	2.59	0.69	0.620	1.05	0.588	0.76	1.30	2.000	No
1139	74.75	4.67	2.08	2.59	0.69	0.620	1.05	0.588	0.76	1.30	2.000	No
1140	74.82	4.68	2.08	2.59	0.69	0.619	1.05	0.588	0.75	1.30	2.000	No
1141	74.88	4.68	2.09	2.59	0.69	0.619	1.05	0.587	0.74	1.30	2.000	No
1142	74.94	4.68	2.09	2.60	0.69	0.619	1.05	0.587	0.74	1.30	2.000	No
1143	75.00	4.69	2.09	2.60	0.69	0.619	1.05	0.587	0.73	1.30	2.000	No
1144	75.07	4.69	2.09	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1145	75.14	4.70	2.09	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1146	75.21	4.70	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1147	75.28	4.70	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1148	75.33	4.70	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1149	75.41	4.71	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1150	75.48	4.71	2.11	2.60	0.68	0.618	1.05	0.587	0.73	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR_{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.07	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
2	0.14	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
3	0.21	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
4	0.28	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
5	0.33	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
6	0.40	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
7	0.47	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
8	0.53	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
9	0.59	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
10	0.67	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
11	0.73	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
12	0.81	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
13	0.87	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
14	0.93	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
15	1.00	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
16	1.06	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
17	1.13	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
18	1.19	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
19	1.26	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
20	1.33	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
21	1.39	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
22	1.45	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
23	1.51	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
24	1.59	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
25	1.64	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
26	1.72	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
27	1.77	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
28	1.84	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
29	1.92	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
30	1.97	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
31	2.05	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
32	2.10	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
33	2.18	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
34	2.24	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
35	2.30	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
36	2.38	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
37	2.44	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
38	2.50	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
39	2.58	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
40	2.64	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
41	2.69	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
42	2.77	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
43	2.83	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
44	2.89	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
45	2.97	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
46	3.03	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
47	3.08	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
48	3.16	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	3.22	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
50	3.29	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
51	3.36	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
52	3.42	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
53	3.48	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
54	3.55	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
55	3.62	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
56	3.69	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
57	3.75	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
58	3.81	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
59	3.89	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
60	3.95	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
61	4.00	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
62	4.08	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
63	4.14	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
64	4.20	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
65	4.28	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
66	4.33	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
67	4.41	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
68	4.47	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
69	4.53	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
70	4.61	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
71	4.67	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
72	4.74	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
73	4.80	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
74	4.86	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
75	4.94	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
76	5.00	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
77	5.05	37.57	31.11	2.10	0.48	1.70	60.36	48.76	109.12	4.000	No	No	2.00
78	5.13	37.48	27.81	2.06	0.49	1.70	60.22	44.76	104.98	4.000	No	No	2.00
79	5.19	36.91	24.34	2.02	0.50	1.70	59.30	39.52	98.82	4.000	No	No	2.00
80	5.25	36.25	26.02	2.04	0.50	1.70	58.24	41.91	100.15	4.000	No	No	2.00
81	5.33	35.69	28.01	2.06	0.49	1.70	57.34	44.46	101.81	4.000	No	No	2.00
82	5.39	35.31	29.36	2.08	0.49	1.70	56.73	46.02	102.75	4.000	No	No	2.00
83	5.45	35.12	30.39	2.09	0.49	1.70	56.43	47.15	103.58	4.000	No	No	2.00
84	5.53	34.75	32.27	2.12	0.49	1.70	55.83	49.02	104.85	4.000	No	No	2.00
85	5.59	36.16	31.72	2.11	0.48	1.70	58.10	48.94	107.03	4.000	No	No	2.00
86	5.65	38.33	30.21	2.09	0.48	1.70	61.58	47.99	109.58	4.000	No	No	2.00
87	5.72	43.32	26.66	2.05	0.47	1.70	69.41	44.89	114.30	4.000	No	No	2.00
88	5.78	47.74	24.01	2.01	0.46	1.68	75.67	41.71	117.38	4.000	No	No	2.00
89	5.86	52.83	21.65	1.98	0.46	1.66	82.67	38.29	120.96	4.000	No	No	2.00
90	5.92	55.94	20.45	1.97	0.45	1.64	86.82	36.26	123.08	4.000	No	No	2.00
91	5.98	59.14	19.41	1.96	0.45	1.62	90.77	34.33	125.10	4.000	No	No	2.00
92	6.04	63.09	17.56	1.93	0.44	1.61	96.16	30.18	126.34	4.000	No	No	2.00
93	6.12	67.89	15.43	1.91	0.44	1.60	102.67	24.61	127.28	4.000	No	No	2.00
94	6.18	72.23	13.90	1.89	0.44	1.59	108.47	20.23	128.70	4.000	No	No	2.00
95	6.24	75.99	13.24	1.88	0.43	1.57	113.04	18.37	131.41	4.000	No	No	2.00
96	6.31	80.04	13.63	1.88	0.42	1.55	117.16	19.94	137.11	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	6.37	82.30	14.56	1.89	0.42	1.53	118.93	23.17	142.10	4.000	No	No	2.00
98	6.43	84.66	15.40	1.90	0.41	1.51	120.83	26.11	146.94	4.000	No	No	2.00
99	6.51	87.39	16.55	1.92	0.40	1.49	122.88	30.04	152.92	4.000	No	No	2.00
100	6.57	88.71	18.30	1.94	0.39	1.47	123.16	35.40	158.56	4.000	No	No	2.00
101	6.65	83.53	23.61	2.01	0.38	1.45	114.79	47.42	162.21	4.000	No	No	2.00
102	6.71	77.12	28.53	2.07	0.39	1.45	105.91	54.62	160.53	4.000	No	No	2.00
103	6.77	70.91	32.72	2.12	0.39	1.46	97.69	58.49	156.18	4.000	No	No	2.00
104	6.83	65.07	36.35	2.17	0.40	1.47	90.10	60.57	150.66	4.000	No	No	2.00
105	6.90	58.10	42.23	2.24	0.41	1.47	80.93	63.03	143.96	4.000	No	No	2.00
106	6.96	52.83	46.75	2.30	0.42	1.48	74.03	64.00	138.03	4.000	No	No	2.00
107	7.03	49.25	50.13	2.34	0.43	1.49	69.23	64.40	133.63	4.000	No	No	2.00
108	7.09	46.99	52.76	2.37	0.44	1.49	66.11	64.69	130.81	4.000	No	No	2.00
109	7.17	46.05	53.82	2.39	0.44	1.49	64.71	64.73	129.45	4.000	No	No	2.00
110	7.22	44.45	56.83	2.42	0.44	1.49	62.42	65.20	127.61	4.000	No	No	2.00
111	7.28	43.50	59.91	2.46	0.45	1.48	60.94	65.77	126.71	4.000	No	No	2.00
112	7.36	43.50	61.41	2.48	0.44	1.47	60.63	66.13	126.76	4.000	No	No	2.00
113	7.42	44.07	61.08	2.48	0.44	1.47	61.14	66.18	127.32	4.000	No	No	2.00
114	7.50	45.39	58.95	2.45	0.44	1.46	62.57	65.93	128.50	4.000	No	No	2.00
115	7.55	44.17	60.24	2.47	0.45	1.46	60.83	65.84	126.67	4.000	No	No	2.00
116	7.61	44.27	60.13	2.46	0.45	1.45	60.76	65.79	126.55	4.000	No	No	2.00
117	7.70	44.36	61.15	2.48	0.45	1.45	60.58	66.04	126.62	4.000	No	No	2.00
118	7.75	47.75	57.83	2.44	0.44	1.43	64.59	66.13	130.72	4.000	No	No	2.00
119	7.81	52.37	52.90	2.37	0.43	1.41	70.01	65.80	135.81	4.000	No	No	2.00
120	7.89	58.30	47.52	2.31	0.42	1.40	76.91	65.15	142.06	4.000	No	No	2.00
121	7.95	61.50	44.73	2.27	0.41	1.39	80.55	64.52	145.07	4.000	No	No	2.00
122	8.01	64.99	41.99	2.24	0.41	1.38	84.50	63.75	148.25	0.278	No	No	0.50
123	8.08	68.19	39.61	2.21	0.40	1.37	88.01	62.86	150.87	0.295	No	No	0.53
124	8.14	69.60	38.71	2.20	0.40	1.36	89.44	62.48	151.91	0.302	No	No	0.54
125	8.22	72.14	37.47	2.18	0.40	1.35	92.07	62.05	154.12	0.319	No	No	0.57
126	8.28	74.78	36.24	2.17	0.39	1.34	94.89	61.56	156.45	0.338	No	No	0.60
127	8.34	77.13	35.24	2.15	0.39	1.34	97.35	61.14	158.50	0.357	No	No	0.63
128	8.40	78.36	34.68	2.15	0.39	1.33	98.52	60.83	159.35	0.365	No	No	0.64
129	8.48	77.51	35.08	2.15	0.39	1.33	97.22	60.95	158.17	0.354	No	No	0.62
130	8.54	75.72	35.81	2.16	0.39	1.33	94.93	61.16	156.09	0.335	No	No	0.59
131	8.60	73.84	36.29	2.17	0.40	1.33	92.57	61.08	153.66	0.315	No	No	0.55
132	8.68	71.77	36.29	2.17	0.40	1.33	89.96	60.48	150.45	0.292	No	No	0.50
133	8.74	70.64	36.01	2.16	0.41	1.33	88.50	59.89	148.39	0.279	No	No	0.48
134	8.79	69.79	35.98	2.16	0.41	1.32	87.34	59.59	146.93	0.270	No	No	0.46
135	8.87	69.32	35.82	2.16	0.41	1.32	86.55	59.26	145.80	0.263	No	No	0.45
136	8.93	68.94	35.92	2.16	0.41	1.32	85.90	59.20	145.10	0.260	No	No	0.44
137	8.99	68.75	36.15	2.16	0.41	1.32	85.46	59.32	144.77	0.258	No	No	0.44
138	9.07	68.75	36.44	2.17	0.41	1.31	85.16	59.52	144.68	0.257	No	No	0.43
139	9.13	68.75	36.77	2.17	0.41	1.31	84.92	59.76	144.68	0.257	No	No	0.43
140	9.19	68.66	36.90	2.17	0.41	1.30	84.61	59.80	144.40	0.256	No	No	0.43
141	9.27	68.56	36.85	2.17	0.41	1.30	84.22	59.67	143.90	0.253	No	No	0.42
142	9.33	67.90	37.33	2.18	0.41	1.30	83.25	59.86	143.12	0.249	No	No	0.41
143	9.39	66.12	38.54	2.19	0.42	1.30	81.06	60.35	141.41	0.241	No	No	0.40
144	9.46	62.54	41.20	2.23	0.42	1.30	76.67	61.28	137.95	0.226	No	No	0.37

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	9.52	60.09	43.15	2.25	0.43	1.30	73.66	61.82	135.48	0.216	No	No	0.35
146	9.58	57.83	45.50	2.28	0.43	1.30	70.85	62.50	133.35	0.209	No	No	0.34
147	9.66	56.23	46.93	2.30	0.44	1.29	68.77	62.73	131.50	0.202	No	No	0.33
148	9.72	54.44	48.15	2.31	0.44	1.29	66.56	62.77	129.32	0.196	No	No	0.31
149	9.78	52.65	49.78	2.33	0.44	1.29	64.33	62.95	127.28	0.190	No	No	0.30
150	9.86	51.43	51.08	2.35	0.45	1.29	62.71	63.09	125.80	0.186	No	No	0.29
151	9.91	50.48	51.94	2.36	0.45	1.29	61.47	63.11	124.58	0.182	No	No	0.29
152	9.97	50.48	51.67	2.36	0.45	1.29	61.32	62.96	124.28	0.182	No	No	0.29
153	10.04	48.04	53.73	2.38	0.45	1.29	58.36	62.97	121.33	0.174	No	No	0.27
154	10.12	52.92	48.34	2.32	0.45	1.28	63.77	62.13	125.90	0.186	No	No	0.29
155	10.18	52.08	48.22	2.32	0.45	1.27	62.67	61.78	124.46	0.182	No	No	0.28
156	10.25	50.00	49.98	2.34	0.45	1.27	60.13	61.92	122.05	0.176	No	No	0.27
157	10.31	48.22	51.73	2.36	0.46	1.27	57.94	62.08	120.02	0.171	No	No	0.26
158	10.37	46.34	53.33	2.38	0.46	1.27	55.67	62.09	117.76	0.167	No	No	0.26
159	10.45	44.83	56.39	2.42	0.46	1.27	53.74	62.65	116.39	0.164	No	No	0.25
160	10.50	44.27	58.02	2.44	0.46	1.27	52.96	62.96	115.92	0.163	No	No	0.25
161	10.58	43.41	59.57	2.46	0.47	1.26	51.81	63.11	114.92	0.161	No	No	0.24
162	10.64	43.23	60.12	2.46	0.47	1.26	51.46	63.18	114.64	0.160	No	No	0.24
163	10.70	43.69	60.18	2.46	0.47	1.26	51.86	63.31	115.17	0.161	No	No	0.24
164	10.78	44.93	59.50	2.46	0.46	1.25	53.07	63.45	116.52	0.164	No	No	0.25
165	10.84	46.53	57.85	2.44	0.46	1.25	54.74	63.40	118.14	0.167	No	No	0.25
166	10.90	49.07	54.86	2.40	0.46	1.24	57.44	63.14	120.57	0.173	No	No	0.26
167	10.98	52.08	51.20	2.35	0.45	1.23	60.61	62.57	123.18	0.179	No	No	0.27
168	11.04	53.97	49.06	2.33	0.45	1.23	62.57	62.15	124.72	0.183	No	No	0.27
169	11.10	55.66	47.45	2.31	0.45	1.22	64.30	61.84	126.13	0.186	No	No	0.28
170	11.16	57.17	46.11	2.29	0.44	1.22	65.82	61.54	127.35	0.190	No	No	0.28
171	11.22	58.30	44.87	2.27	0.44	1.21	66.91	61.14	128.06	0.192	No	No	0.29
172	11.31	58.58	44.06	2.26	0.44	1.21	67.02	60.70	127.72	0.191	No	No	0.28
173	11.37	58.96	43.61	2.26	0.44	1.21	67.29	60.50	127.79	0.191	No	No	0.28
174	11.43	58.86	43.86	2.26	0.44	1.21	67.02	60.59	127.61	0.191	No	No	0.28
175	11.49	59.15	43.58	2.26	0.44	1.20	67.19	60.46	127.65	0.191	No	No	0.28
176	11.55	59.52	43.39	2.25	0.44	1.20	67.44	60.41	127.86	0.191	No	No	0.28
177	11.64	59.90	43.44	2.26	0.44	1.19	67.63	60.49	128.12	0.192	No	No	0.28
178	11.70	60.09	43.61	2.26	0.44	1.19	67.68	60.60	128.28	0.192	No	No	0.28
179	11.77	60.56	43.62	2.26	0.44	1.19	68.03	60.70	128.73	0.194	No	No	0.28
180	11.82	60.94	43.73	2.26	0.44	1.19	68.28	60.82	129.10	0.195	No	No	0.29
181	11.88	61.50	43.73	2.26	0.44	1.18	68.72	60.94	129.66	0.197	No	No	0.29
182	11.94	61.12	44.41	2.27	0.44	1.18	68.16	61.19	129.36	0.196	No	No	0.29
183	12.03	61.03	39.28	2.20	0.45	1.18	68.01	57.82	125.82	0.186	No	No	0.27
184	12.09	61.69	35.52	2.16	0.45	1.18	68.69	54.93	123.62	0.180	No	No	0.26
185	12.15	61.68	37.38	2.18	0.45	1.17	68.48	56.46	124.94	0.183	No	No	0.26
186	12.21	61.22	38.61	2.20	0.45	1.17	67.80	57.26	125.06	0.184	No	No	0.26
187	12.28	60.83	39.53	2.21	0.45	1.17	67.23	57.81	125.04	0.184	No	No	0.26
188	12.34	59.34	41.29	2.23	0.45	1.17	65.46	58.59	124.06	0.181	No	No	0.26
189	12.42	48.69	51.24	2.35	0.47	1.17	53.88	60.79	114.68	0.160	No	No	0.23
190	12.48	53.50	47.46	2.31	0.46	1.17	58.90	60.43	119.33	0.170	No	No	0.24
191	12.54	51.05	50.47	2.34	0.46	1.16	56.15	61.08	117.23	0.166	No	No	0.23
192	12.60	47.75	55.11	2.40	0.47	1.16	52.50	61.88	114.38	0.160	No	No	0.22

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	12.69	43.41	62.41	2.49	0.48	1.16	47.70	62.75	110.44	0.153	No	No	0.21
194	12.75	41.72	65.78	2.53	0.48	1.16	45.78	63.03	108.82	0.150	No	No	0.21
195	12.81	40.21	69.13	2.58	0.48	1.16	44.07	63.27	107.34	0.148	No	No	0.20
196	12.87	40.21	70.62	2.60	0.48	1.16	43.96	63.55	107.51	0.148	No	No	0.20
197	12.93	40.22	71.78	2.61	0.48	1.15	43.86	0.00	43.86	4.000	No	Yes	2.00
198	13.02	41.07	71.41	2.61	0.48	1.15	44.61	0.00	44.61	4.000	No	Yes	2.00
199	13.08	41.82	70.36	2.59	0.48	1.15	45.31	63.89	109.20	0.151	No	No	0.21
200	13.14	42.67	69.09	2.58	0.48	1.14	46.11	63.86	109.97	0.152	No	No	0.21
201	13.20	43.61	67.22	2.55	0.48	1.14	47.00	63.71	110.71	0.153	No	No	0.21
202	13.26	45.12	64.74	2.52	0.47	1.14	48.48	63.56	112.04	0.156	No	No	0.21
203	13.35	47.85	60.39	2.47	0.47	1.13	51.18	63.18	114.36	0.160	No	No	0.22
204	13.41	50.20	57.24	2.43	0.46	1.13	53.52	62.87	116.40	0.164	No	No	0.22
205	13.47	52.55	54.40	2.39	0.46	1.12	55.86	62.54	118.41	0.168	No	No	0.23
206	13.53	54.43	52.11	2.36	0.46	1.12	57.70	62.17	119.87	0.171	No	No	0.23
207	13.59	55.94	50.85	2.35	0.45	1.12	59.14	62.04	121.18	0.174	No	No	0.24
208	13.65	57.25	50.47	2.34	0.45	1.12	60.37	62.20	122.57	0.177	No	No	0.24
209	13.74	59.23	50.24	2.34	0.45	1.11	62.21	62.59	124.79	0.183	No	No	0.25
210	13.80	59.89	50.45	2.34	0.45	1.11	62.75	62.82	125.58	0.185	No	No	0.25
211	13.86	59.97	50.91	2.35	0.45	1.11	62.72	63.01	125.74	0.185	No	No	0.25
212	13.92	59.97	51.45	2.36	0.45	1.10	62.60	63.21	125.81	0.186	No	No	0.25
213	13.98	61.01	50.88	2.35	0.44	1.10	63.53	63.22	126.75	0.188	No	No	0.26
214	14.07	63.93	48.66	2.32	0.44	1.10	66.32	62.95	129.27	0.195	No	No	0.27
215	14.13	66.19	46.96	2.30	0.44	1.09	68.48	62.67	131.15	0.201	No	No	0.27
216	14.19	67.97	44.98	2.27	0.43	1.09	70.17	62.03	132.20	0.205	No	No	0.28
217	14.25	69.85	42.08	2.24	0.43	1.09	71.96	60.72	132.67	0.206	No	No	0.28
218	14.31	71.44	39.97	2.21	0.43	1.09	73.46	59.63	133.09	0.208	No	No	0.28
219	14.37	72.86	38.79	2.20	0.43	1.09	74.77	59.06	133.83	0.210	No	No	0.28
220	14.46	75.21	36.96	2.17	0.43	1.08	76.94	58.08	135.02	0.214	No	No	0.29
221	14.52	77.00	35.81	2.16	0.43	1.08	78.60	57.44	136.04	0.218	No	No	0.30
222	14.58	78.98	34.65	2.15	0.43	1.08	80.44	56.76	137.20	0.223	No	No	0.30
223	14.64	81.24	33.48	2.13	0.42	1.07	82.57	56.04	138.61	0.229	No	No	0.31
224	14.70	83.21	32.78	2.12	0.42	1.07	84.38	55.69	140.07	0.235	No	No	0.32
225	14.79	86.13	31.50	2.11	0.42	1.07	87.07	54.80	141.87	0.243	No	No	0.33
226	14.85	87.83	27.71	2.06	0.42	1.07	88.71	50.06	138.78	0.229	No	No	0.31
227	14.91	89.52	24.12	2.01	0.43	1.07	90.36	44.37	134.73	0.213	No	No	0.29
228	14.97	90.95	24.31	2.02	0.43	1.07	91.59	44.93	136.52	0.220	No	No	0.29
229	15.03	92.17	24.56	2.02	0.42	1.06	92.62	45.58	138.19	0.227	No	No	0.30
230	15.09	93.02	24.90	2.02	0.42	1.06	93.28	46.30	139.58	0.233	No	No	0.31
231	15.18	92.12	26.31	2.04	0.42	1.06	92.14	48.52	140.66	0.238	No	No	0.32
232	15.23	92.08	26.80	2.05	0.42	1.06	91.94	49.26	141.20	0.240	No	No	0.32
233	15.29	93.86	26.11	2.04	0.42	1.05	93.55	48.44	141.99	0.244	No	No	0.33
234	15.38	95.94	25.76	2.03	0.41	1.05	95.37	48.18	143.55	0.251	No	No	0.34
235	15.44	96.60	26.62	2.05	0.41	1.05	95.83	49.70	145.53	0.262	No	No	0.35
236	15.50	96.78	27.20	2.05	0.41	1.05	95.83	50.64	146.47	0.267	No	No	0.36
237	15.56	96.60	27.69	2.06	0.41	1.05	95.49	51.32	146.81	0.269	No	No	0.36
238	15.62	96.50	28.00	2.06	0.41	1.04	95.24	51.74	146.98	0.270	No	No	0.36
239	15.71	95.75	28.47	2.07	0.41	1.04	94.28	52.26	146.54	0.268	No	No	0.36
240	15.77	95.18	28.57	2.07	0.41	1.04	93.57	52.26	145.84	0.264	No	No	0.35

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	15.83	94.71	28.99	2.07	0.41	1.04	92.96	52.74	145.70	0.263	No	No	0.35
242	15.89	93.96	29.50	2.08	0.41	1.04	92.08	53.27	145.35	0.261	No	No	0.34
243	15.95	93.02	30.01	2.09	0.41	1.04	91.03	53.74	144.77	0.258	No	No	0.34
244	16.04	91.70	30.70	2.10	0.41	1.03	89.54	54.33	143.87	0.253	No	No	0.33
245	16.10	90.95	31.16	2.10	0.41	1.03	88.67	54.72	143.38	0.251	No	No	0.33
246	16.16	90.38	31.50	2.11	0.42	1.03	87.98	54.98	142.96	0.248	No	No	0.33
247	16.22	89.44	31.96	2.11	0.42	1.03	86.94	55.31	142.24	0.245	No	No	0.32
248	16.28	88.21	32.43	2.12	0.42	1.03	85.62	55.57	141.19	0.240	No	No	0.31
249	16.34	86.43	32.98	2.12	0.42	1.03	83.77	55.78	139.55	0.233	No	No	0.30
250	16.43	82.47	34.49	2.14	0.43	1.02	79.77	56.46	136.23	0.219	No	No	0.28
251	16.49	78.89	36.18	2.16	0.43	1.02	76.21	57.23	133.44	0.209	No	No	0.27
252	16.55	74.65	38.41	2.19	0.44	1.02	72.02	58.11	130.13	0.198	No	No	0.25
253	16.61	70.04	41.33	2.23	0.44	1.02	67.49	59.12	126.60	0.188	No	No	0.24
254	16.67	65.24	44.84	2.27	0.45	1.02	62.78	60.08	122.86	0.178	No	No	0.23
255	16.76	57.52	51.26	2.35	0.46	1.02	55.24	61.17	116.41	0.164	No	No	0.21
256	16.82	52.90	55.67	2.41	0.47	1.01	50.73	61.59	112.32	0.156	No	No	0.20
257	16.88	48.95	59.92	2.46	0.48	1.01	46.88	61.84	108.72	0.150	No	No	0.19
258	16.94	44.90	65.12	2.53	0.49	1.01	42.94	62.06	105.00	0.144	No	No	0.18
259	17.00	40.47	71.71	2.61	0.50	1.01	38.64	0.00	38.64	4.000	No	Yes	2.00
260	17.09	34.54	75.82	2.66	0.51	1.01	32.90	0.00	32.90	4.000	No	Yes	2.00
261	17.15	32.84	77.90	2.69	0.52	1.01	31.23	0.00	31.23	4.000	No	Yes	2.00
262	17.21	32.94	78.77	2.70	0.52	1.00	31.27	0.00	31.27	4.000	No	Yes	2.00
263	17.27	33.97	78.44	2.69	0.51	1.00	32.19	0.00	32.19	4.000	No	Yes	2.00
264	17.34	35.76	77.84	2.69	0.51	1.00	33.82	0.00	33.82	4.000	No	Yes	2.00
265	17.39	37.47	78.25	2.69	0.50	1.00	35.37	0.00	35.37	4.000	No	Yes	2.00
266	17.46	27.49	97.11	2.93	0.53	1.00	25.90	0.00	25.90	4.000	No	Yes	2.00
267	17.52	41.33	77.62	2.68	0.49	0.99	38.87	0.00	38.87	4.000	No	Yes	2.00
268	17.60	48.39	70.10	2.59	0.48	0.99	45.42	63.87	109.28	0.151	No	No	0.19
269	17.66	55.55	63.67	2.51	0.46	0.99	52.05	64.31	116.37	0.164	No	No	0.20
270	17.72	62.80	57.85	2.44	0.45	0.99	58.77	64.53	123.30	0.179	No	No	0.22
271	17.81	77.21	47.98	2.31	0.43	0.99	72.14	64.14	136.27	0.219	No	No	0.28
272	17.87	86.81	41.84	2.24	0.41	0.99	81.02	62.79	143.81	0.253	No	No	0.32
273	17.93	94.63	36.78	2.17	0.41	0.99	88.21	60.53	148.74	0.281	No	No	0.36
274	17.99	101.41	32.13	2.11	0.40	0.99	94.42	57.10	151.51	0.299	No	No	0.38
275	18.05	106.68	28.83	2.07	0.40	0.98	99.19	53.74	152.93	0.309	No	No	0.39
276	18.12	111.11	26.68	2.05	0.40	0.98	103.17	51.15	154.32	0.320	No	No	0.41
277	18.18	112.90	26.16	2.04	0.39	0.98	104.69	50.54	155.24	0.328	No	No	0.42
278	18.27	115.91	25.53	2.03	0.39	0.98	107.29	49.89	157.17	0.344	No	No	0.44
279	18.33	117.32	25.52	2.03	0.39	0.98	108.46	50.09	158.55	0.357	No	No	0.46
280	18.39	117.98	25.65	2.03	0.39	0.98	108.93	50.40	159.33	0.365	No	No	0.47
281	18.45	118.55	25.72	2.03	0.39	0.98	109.32	50.60	159.92	0.371	No	No	0.47
282	18.51	119.02	25.95	2.04	0.39	0.97	109.62	51.06	160.68	0.379	No	No	0.48
283	18.60	119.30	26.44	2.04	0.38	0.97	109.68	51.93	161.61	0.389	No	No	0.50
284	18.66	119.11	26.92	2.05	0.38	0.97	109.37	52.71	162.08	0.394	No	No	0.50
285	18.72	118.73	27.44	2.06	0.38	0.97	108.89	53.47	162.36	0.397	No	No	0.51
286	18.78	117.89	28.06	2.06	0.38	0.97	107.98	54.29	162.27	0.396	No	No	0.50
287	18.84	116.76	28.77	2.07	0.38	0.97	106.80	55.16	161.96	0.393	No	No	0.50
288	18.90	115.06	29.78	2.08	0.39	0.97	105.10	56.29	161.39	0.386	No	No	0.49

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	18.99	111.86	31.52	2.11	0.39	0.96	101.96	57.95	159.91	0.371	No	No	0.47
290	19.05	110.17	32.51	2.12	0.39	0.96	100.28	58.80	159.08	0.362	No	No	0.46
291	19.11	107.72	33.96	2.14	0.39	0.96	97.91	59.93	157.84	0.351	No	No	0.44
292	19.17	105.55	35.52	2.16	0.39	0.96	95.80	61.07	156.87	0.342	No	No	0.43
293	19.23	104.23	36.45	2.17	0.39	0.96	94.47	61.67	156.13	0.335	No	No	0.42
294	19.32	101.60	37.53	2.18	0.40	0.96	91.87	62.05	153.92	0.317	No	No	0.40
295	19.38	99.05	39.00	2.20	0.40	0.96	89.42	62.71	152.14	0.304	No	No	0.38
296	19.44	95.00	42.32	2.24	0.40	0.95	85.62	64.25	149.88	0.288	No	No	0.36
297	19.50	87.94	44.05	2.26	0.42	0.95	79.04	63.73	142.77	0.248	No	No	0.30
298	19.56	79.09	40.62	2.22	0.44	0.95	70.80	59.44	130.25	0.198	No	No	0.24
299	19.65	64.40	53.55	2.38	0.46	0.94	57.39	62.64	120.04	0.171	No	No	0.21
300	19.71	57.34	58.96	2.45	0.47	0.94	50.94	62.69	113.64	0.159	No	No	0.19
301	19.77	48.02	68.54	2.57	0.49	0.94	42.50	62.70	105.20	0.145	No	No	0.17
302	19.83	39.07	79.06	2.70	0.51	0.93	34.44	0.00	34.44	4.000	No	Yes	2.00
303	19.89	29.56	93.60	2.88	0.53	0.93	25.94	0.00	25.94	4.000	No	Yes	2.00
304	19.95	29.84	93.79	2.88	0.53	0.93	26.14	0.00	26.14	4.000	No	Yes	2.00
305	20.01	29.42	94.07	2.89	0.53	0.93	25.73	0.00	25.73	4.000	No	Yes	2.00
306	20.09	29.28	94.42	2.89	0.53	0.92	25.56	0.00	25.56	4.000	No	Yes	2.00
307	20.15	27.68	97.37	2.93	0.53	0.92	24.11	0.00	24.11	4.000	No	Yes	2.00
308	20.21	25.70	100.00	2.98	0.54	0.92	22.33	0.00	22.33	4.000	No	Yes	2.00
309	20.30	24.47	100.00	3.01	0.54	0.92	21.20	0.00	21.20	4.000	No	Yes	2.00
310	20.36	24.57	100.00	2.99	0.54	0.91	21.25	0.00	21.25	4.000	No	Yes	2.00
311	20.42	24.66	100.00	2.98	0.54	0.91	21.30	0.00	21.30	4.000	No	Yes	2.00
312	20.48	24.10	100.00	2.99	0.54	0.91	20.77	0.00	20.77	4.000	No	Yes	2.00
313	20.54	23.25	100.00	3.01	0.55	0.91	20.00	0.00	20.00	4.000	No	Yes	2.00
314	20.63	24.24	100.00	2.98	0.54	0.91	20.81	0.00	20.81	4.000	No	Yes	2.00
315	20.69	23.16	100.00	3.01	0.55	0.91	19.84	0.00	19.84	4.000	No	Yes	2.00
316	20.75	24.38	100.00	2.99	0.54	0.91	20.87	0.00	20.87	4.000	No	Yes	2.00
317	20.81	25.60	100.00	2.97	0.54	0.90	21.89	0.00	21.89	4.000	No	Yes	2.00
318	20.87	27.11	98.68	2.95	0.54	0.90	23.17	0.00	23.17	4.000	No	Yes	2.00
319	20.93	28.99	96.44	2.92	0.53	0.90	24.76	0.00	24.76	4.000	No	Yes	2.00
320	21.02	32.48	91.82	2.86	0.52	0.90	27.72	0.00	27.72	4.000	No	Yes	2.00
321	21.08	34.55	89.29	2.83	0.52	0.90	29.47	0.00	29.47	4.000	No	Yes	2.00
322	21.14	36.62	86.74	2.80	0.51	0.90	31.22	0.00	31.22	4.000	No	Yes	2.00
323	21.20	38.60	80.08	2.71	0.51	0.90	32.88	0.00	32.88	4.000	No	Yes	2.00
324	21.26	40.95	68.68	2.57	0.51	0.90	34.84	60.50	95.34	0.132	No	No	0.15
325	21.35	45.10	65.62	2.53	0.50	0.90	38.36	60.86	99.22	0.136	No	No	0.16
326	21.41	46.79	65.46	2.53	0.50	0.90	39.77	61.23	101.01	0.139	No	No	0.16
327	21.47	47.73	66.39	2.54	0.49	0.90	40.53	61.66	102.20	0.140	No	No	0.16
328	21.53	48.30	67.54	2.56	0.49	0.90	40.98	62.04	103.02	0.142	No	No	0.16
329	21.59	46.60	71.18	2.60	0.49	0.90	39.46	0.00	39.46	4.000	No	Yes	2.00
330	21.66	46.32	73.89	2.64	0.49	0.89	39.16	0.00	39.16	4.000	No	Yes	2.00
331	21.72	45.10	77.37	2.68	0.50	0.89	38.06	0.00	38.06	4.000	No	Yes	2.00
332	21.79	42.84	82.03	2.74	0.50	0.89	36.06	0.00	36.06	4.000	No	Yes	2.00
333	21.86	41.52	84.99	2.77	0.50	0.89	34.88	0.00	34.88	4.000	No	Yes	2.00
334	21.92	40.39	87.44	2.81	0.50	0.89	33.86	0.00	33.86	4.000	No	Yes	2.00
335	22.00	38.60	90.51	2.84	0.51	0.88	32.27	0.00	32.27	4.000	No	Yes	2.00
336	22.06	37.66	92.02	2.86	0.51	0.88	31.43	0.00	31.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	22.13	37.47	92.57	2.87	0.51	0.88	31.21	0.00	31.21	4.000	No	Yes	2.00
338	22.18	37.47	92.65	2.87	0.51	0.88	31.17	0.00	31.17	4.000	No	Yes	2.00
339	22.26	37.47	92.53	2.87	0.51	0.88	31.11	0.00	31.11	4.000	No	Yes	2.00
340	22.32	37.47	92.61	2.87	0.51	0.88	31.06	0.00	31.06	4.000	No	Yes	2.00
341	22.39	37.47	92.71	2.87	0.51	0.88	31.02	0.00	31.02	4.000	No	Yes	2.00
342	22.46	38.22	91.85	2.86	0.51	0.87	31.60	0.00	31.60	4.000	No	Yes	2.00
343	22.52	38.32	91.92	2.86	0.51	0.87	31.64	0.00	31.64	4.000	No	Yes	2.00
344	22.60	38.50	91.98	2.86	0.51	0.87	31.73	0.00	31.73	4.000	No	Yes	2.00
345	22.64	38.60	91.99	2.86	0.51	0.87	31.78	0.00	31.78	4.000	No	Yes	2.00
346	22.71	38.79	91.86	2.86	0.51	0.87	31.90	0.00	31.90	4.000	No	Yes	2.00
347	22.77	38.50	92.32	2.87	0.51	0.87	31.60	0.00	31.60	4.000	No	Yes	2.00
348	22.84	37.19	94.17	2.89	0.51	0.87	30.45	0.00	30.45	4.000	No	Yes	2.00
349	22.93	38.61	92.39	2.87	0.51	0.87	31.57	0.00	31.57	4.000	No	Yes	2.00
350	22.98	37.48	93.65	2.88	0.51	0.86	30.58	0.00	30.58	4.000	No	Yes	2.00
351	23.04	38.70	91.03	2.85	0.51	0.86	31.56	0.00	31.56	4.000	No	Yes	2.00
352	23.12	41.53	79.42	2.71	0.51	0.86	33.84	0.00	33.84	4.000	No	Yes	2.00
353	23.17	45.77	69.40	2.58	0.50	0.86	37.32	61.37	98.70	0.136	No	No	0.15
354	23.26	53.67	62.95	2.50	0.49	0.87	43.89	61.81	105.69	0.145	No	No	0.17
355	23.32	60.17	58.98	2.45	0.47	0.87	49.32	62.24	111.56	0.155	No	No	0.18
356	23.38	66.19	56.13	2.41	0.46	0.87	54.38	62.74	117.12	0.165	No	No	0.19
357	23.44	70.33	54.04	2.39	0.46	0.87	57.84	62.95	120.78	0.173	No	No	0.20
358	23.49	71.09	54.06	2.39	0.45	0.87	58.42	63.11	121.54	0.175	No	No	0.20
359	23.56	74.76	52.36	2.37	0.45	0.87	61.48	63.29	124.76	0.183	No	No	0.21
360	23.63	77.87	51.43	2.36	0.44	0.87	64.05	63.59	127.65	0.191	No	No	0.22
361	23.69	80.60	50.82	2.35	0.44	0.87	66.32	63.94	130.25	0.198	No	No	0.23
362	23.75	85.02	49.20	2.33	0.43	0.87	70.03	64.18	134.21	0.212	No	No	0.24
363	23.84	87.47	49.09	2.33	0.43	0.87	72.04	64.66	136.70	0.221	No	No	0.26
364	23.89	88.32	49.19	2.33	0.42	0.87	72.71	64.88	137.59	0.224	No	No	0.26
365	23.96	90.77	48.51	2.32	0.42	0.87	74.72	65.08	139.80	0.234	No	No	0.27
366	24.02	92.37	48.11	2.31	0.42	0.87	76.02	65.22	141.24	0.240	No	No	0.28
367	24.10	93.40	47.91	2.31	0.42	0.87	76.79	65.32	142.11	0.244	No	No	0.28
368	24.16	94.06	47.76	2.31	0.42	0.87	77.27	65.37	142.64	0.247	No	No	0.29
369	24.23	94.02	48.00	2.31	0.42	0.87	77.15	65.46	142.61	0.247	No	No	0.29
370	24.29	93.97	47.97	2.31	0.42	0.87	77.00	65.40	142.41	0.246	No	No	0.28
371	24.36	93.40	47.97	2.31	0.42	0.87	76.42	65.25	141.67	0.242	No	No	0.28
372	24.41	91.90	48.39	2.32	0.42	0.86	75.05	65.10	140.15	0.235	No	No	0.27
373	24.50	88.88	49.38	2.33	0.43	0.86	72.34	64.87	137.21	0.223	No	No	0.26
374	24.56	86.25	50.40	2.34	0.43	0.86	70.01	64.73	134.74	0.213	No	No	0.24
375	24.62	82.20	52.31	2.37	0.44	0.86	66.50	64.62	131.11	0.201	No	No	0.23
376	24.68	77.02	55.05	2.40	0.44	0.85	62.05	64.47	126.52	0.188	No	No	0.21
377	24.75	70.90	58.76	2.45	0.45	0.85	56.85	64.28	121.12	0.174	No	No	0.20
378	24.80	63.55	63.83	2.51	0.47	0.84	50.66	63.95	114.62	0.160	No	No	0.18
379	24.89	49.99	75.25	2.65	0.49	0.83	39.41	0.00	39.41	4.000	No	Yes	2.00
380	24.95	40.67	85.17	2.78	0.51	0.83	31.81	0.00	31.81	4.000	No	Yes	2.00
381	25.01	33.51	93.78	2.88	0.53	0.82	26.03	0.00	26.03	4.000	No	Yes	2.00
382	25.07	28.15	100.00	2.97	0.54	0.82	21.73	0.00	21.73	4.000	No	Yes	2.00
383	25.14	24.47	100.00	3.03	0.55	0.81	18.80	0.00	18.80	4.000	No	Yes	2.00
384	25.22	21.46	100.00	3.06	0.56	0.81	16.40	0.00	16.40	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	25.28	19.67	100.00	3.07	0.56	0.81	14.99	0.00	14.99	4.000	No	Yes	2.00
386	25.34	18.82	100.00	3.01	0.57	0.80	14.31	0.00	14.31	4.000	No	Yes	2.00
387	25.40	18.63	98.13	2.94	0.57	0.80	14.14	0.00	14.14	4.000	No	Yes	2.00
388	25.46	18.73	96.84	2.92	0.57	0.80	14.20	0.00	14.20	4.000	No	Yes	2.00
389	25.53	18.93	95.86	2.91	0.57	0.80	14.33	0.00	14.33	4.000	No	Yes	2.00
390	25.62	19.48	98.23	2.94	0.56	0.80	14.73	0.00	14.73	4.000	No	Yes	2.00
391	25.67	18.65	100.00	3.03	0.57	0.80	14.07	0.00	14.07	4.000	No	Yes	2.00
392	25.73	21.28	100.00	3.00	0.56	0.80	16.09	0.00	16.09	4.000	No	Yes	2.00
393	25.79	22.61	100.00	3.03	0.56	0.80	17.08	0.00	17.08	4.000	No	Yes	2.00
394	25.87	25.91	100.00	3.02	0.55	0.80	19.62	0.00	19.62	4.000	No	Yes	2.00
395	25.94	40.99	84.72	2.77	0.51	0.81	31.41	0.00	31.41	4.000	No	Yes	2.00
396	25.98	52.20	73.94	2.64	0.49	0.82	40.33	0.00	40.33	4.000	No	Yes	2.00
397	26.07	70.28	61.46	2.48	0.46	0.83	54.97	64.55	119.51	0.170	No	No	0.19
398	26.14	82.24	54.75	2.40	0.44	0.83	64.77	65.10	129.87	0.197	No	No	0.22
399	26.20	91.18	50.42	2.34	0.42	0.84	72.15	65.31	137.45	0.224	No	No	0.25
400	26.26	94.10	48.92	2.32	0.42	0.84	74.50	65.22	139.73	0.233	No	No	0.26
401	26.32	92.50	49.14	2.33	0.42	0.84	73.07	64.95	138.03	0.226	No	No	0.26
402	26.41	83.18	53.47	2.38	0.44	0.83	65.21	64.73	129.94	0.197	No	No	0.22
403	26.47	74.80	58.32	2.44	0.45	0.82	58.25	64.53	122.77	0.178	No	No	0.20
404	26.53	64.63	65.18	2.53	0.47	0.82	49.90	64.07	113.97	0.159	No	No	0.18
405	26.59	53.80	74.01	2.64	0.49	0.81	41.14	0.00	41.14	4.000	No	Yes	2.00
406	26.64	44.56	83.32	2.75	0.51	0.80	33.78	0.00	33.78	4.000	No	Yes	2.00
407	26.73	34.67	95.31	2.90	0.53	0.79	25.99	0.00	25.99	4.000	No	Yes	2.00
408	26.79	29.97	100.00	2.98	0.54	0.79	22.33	0.00	22.33	4.000	No	Yes	2.00
409	26.86	26.48	100.00	3.04	0.55	0.78	19.63	0.00	19.63	4.000	No	Yes	2.00
410	26.92	24.97	100.00	3.04	0.55	0.78	18.45	0.00	18.45	4.000	No	Yes	2.00
411	26.98	24.03	100.00	3.04	0.55	0.78	17.72	0.00	17.72	4.000	No	Yes	2.00
412	27.04	23.09	100.00	3.03	0.56	0.78	16.98	0.00	16.98	4.000	No	Yes	2.00
413	27.12	21.21	100.00	3.06	0.56	0.78	15.54	0.00	15.54	4.000	No	Yes	2.00
414	27.19	21.21	100.00	3.08	0.56	0.77	15.52	0.00	15.52	4.000	No	Yes	2.00
415	27.25	21.21	100.00	3.10	0.56	0.77	15.50	0.00	15.50	4.000	No	Yes	2.00
416	27.30	24.13	100.00	3.05	0.55	0.78	17.67	0.00	17.67	4.000	No	Yes	2.00
417	27.37	28.83	100.00	2.97	0.54	0.78	21.21	0.00	21.21	4.000	No	Yes	2.00
418	27.46	38.91	88.07	2.81	0.52	0.79	28.87	0.00	28.87	4.000	No	Yes	2.00
419	27.52	50.78	74.41	2.64	0.50	0.79	38.05	0.00	38.05	4.000	No	Yes	2.00
420	27.58	63.30	61.63	2.48	0.48	0.80	47.85	62.58	110.43	0.153	No	No	0.17
421	27.64	73.19	54.47	2.39	0.46	0.81	55.67	62.51	118.19	0.167	No	No	0.19
422	27.70	81.10	50.74	2.35	0.45	0.81	61.99	62.75	124.74	0.183	No	No	0.20
423	27.76	85.34	48.77	2.32	0.44	0.81	65.36	62.75	128.12	0.192	No	No	0.21
424	27.82	84.86	48.53	2.32	0.44	0.81	64.89	62.51	127.41	0.190	No	No	0.21
425	27.89	71.48	56.65	2.42	0.46	0.80	54.09	62.83	116.92	0.165	No	No	0.18
426	27.96	73.73	54.63	2.40	0.46	0.80	55.81	62.61	118.43	0.168	No	No	0.19
427	28.02	68.18	59.33	2.45	0.47	0.80	51.35	62.92	114.27	0.160	No	No	0.18
428	28.09	60.93	64.78	2.52	0.48	0.79	45.57	62.74	108.30	0.149	No	No	0.16
429	28.16	56.12	70.81	2.60	0.49	0.79	41.77	62.94	104.71	0.144	No	No	0.16
430	28.23	54.23	75.16	2.65	0.49	0.79	40.26	0.00	40.26	4.000	No	Yes	2.00
431	28.28	53.84	77.32	2.68	0.49	0.78	39.93	0.00	39.93	4.000	No	Yes	2.00
432	28.35	54.41	78.24	2.69	0.49	0.78	40.35	0.00	40.35	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	28.43	55.63	77.50	2.68	0.49	0.78	41.24	0.00	41.24	4.000	No	Yes	2.00
434	28.49	56.10	77.10	2.68	0.49	0.78	41.56	0.00	41.56	4.000	No	Yes	2.00
435	28.55	57.89	75.29	2.65	0.48	0.78	42.90	0.00	42.90	4.000	No	Yes	2.00
436	28.61	60.81	72.12	2.61	0.48	0.78	45.13	0.00	45.13	4.000	No	Yes	2.00
437	28.70	65.71	66.15	2.54	0.47	0.79	48.87	64.01	112.88	0.157	No	No	0.17
438	28.76	69.19	61.41	2.48	0.47	0.79	51.52	63.56	115.08	0.161	No	No	0.18
439	28.82	71.92	57.22	2.43	0.46	0.79	53.58	62.88	116.46	0.164	No	No	0.18
440	28.88	74.18	53.62	2.38	0.46	0.79	55.26	62.09	117.35	0.166	No	No	0.18
441	28.94	76.54	50.55	2.34	0.46	0.79	57.02	61.35	118.36	0.168	No	No	0.18
442	29.03	79.55	47.83	2.31	0.46	0.79	59.27	60.71	119.99	0.171	No	No	0.19
443	29.09	81.06	46.77	2.30	0.46	0.79	60.40	60.48	120.88	0.173	No	No	0.19
444	29.15	82.28	46.11	2.29	0.45	0.79	61.29	60.38	121.67	0.175	No	No	0.19
445	29.21	83.13	45.82	2.29	0.45	0.79	61.91	60.38	122.29	0.177	No	No	0.19
446	29.27	83.51	45.86	2.29	0.45	0.79	62.15	60.46	122.61	0.177	No	No	0.19
447	29.33	83.69	45.93	2.29	0.45	0.79	62.24	60.53	122.76	0.178	No	No	0.20
448	29.42	83.79	45.98	2.29	0.45	0.79	62.22	60.55	122.77	0.178	No	No	0.20
449	29.48	83.60	45.90	2.29	0.45	0.78	62.01	60.45	122.46	0.177	No	No	0.19
450	29.54	82.75	46.01	2.29	0.45	0.78	61.26	60.32	121.58	0.175	No	No	0.19
451	29.60	81.53	46.42	2.29	0.46	0.78	60.24	60.26	120.50	0.173	No	No	0.19
452	29.66	79.83	46.99	2.30	0.46	0.78	58.84	60.19	119.03	0.169	No	No	0.19
453	29.75	75.78	48.61	2.32	0.47	0.78	55.58	60.11	115.69	0.162	No	No	0.18
454	29.81	71.92	51.37	2.35	0.47	0.77	52.55	60.49	113.04	0.157	No	No	0.17
455	29.87	66.74	56.00	2.41	0.48	0.77	48.53	61.09	109.62	0.152	No	No	0.16
456	29.93	60.06	62.94	2.50	0.49	0.76	43.41	61.66	105.07	0.144	No	No	0.16
457	29.99	51.40	73.26	2.63	0.50	0.76	36.83	0.00	36.83	4.000	No	Yes	2.00
458	30.05	38.97	90.08	2.84	0.52	0.75	27.55	0.00	27.55	4.000	No	Yes	2.00
459	30.12	32.47	100.00	2.97	0.54	0.74	22.77	0.00	22.77	4.000	No	Yes	2.00
460	30.19	28.23	100.00	3.06	0.55	0.74	19.65	0.00	19.65	4.000	No	Yes	2.00
461	30.26	25.88	100.00	3.11	0.55	0.73	17.94	0.00	17.94	4.000	No	Yes	2.00
462	30.33	23.05	100.00	3.17	0.56	0.73	15.89	0.00	15.89	4.000	No	Yes	2.00
463	30.39	19.19	100.00	3.27	0.57	0.72	13.14	0.00	13.14	4.000	No	Yes	2.00
464	30.45	16.37	100.00	3.36	0.58	0.72	11.15	0.00	11.15	4.000	No	Yes	2.00
465	30.52	14.95	100.00	3.40	0.58	0.72	10.15	0.00	10.15	4.000	No	Yes	2.00
466	30.58	14.58	100.00	3.40	0.58	0.72	9.88	0.00	9.88	4.000	No	Yes	2.00
467	30.65	14.11	100.00	3.39	0.58	0.71	9.55	0.00	9.55	4.000	No	Yes	2.00
468	30.71	13.35	100.00	3.40	0.59	0.71	9.01	0.00	9.01	4.000	No	Yes	2.00
469	30.78	13.63	100.00	3.37	0.59	0.71	9.19	0.00	9.19	4.000	No	Yes	2.00
470	30.85	13.35	100.00	3.37	0.59	0.71	8.99	0.00	8.99	4.000	No	Yes	2.00
471	30.92	13.16	100.00	3.37	0.59	0.71	8.85	0.00	8.85	4.000	No	Yes	2.00
472	30.97	13.17	100.00	3.36	0.59	0.71	8.84	0.00	8.84	4.000	No	Yes	2.00
473	31.04	13.17	100.00	3.36	0.59	0.71	8.83	0.00	8.83	4.000	No	Yes	2.00
474	31.11	13.46	100.00	3.34	0.59	0.71	9.02	0.00	9.02	4.000	No	Yes	2.00
475	31.17	13.46	100.00	3.34	0.59	0.71	9.01	0.00	9.01	4.000	No	Yes	2.00
476	31.25	13.93	100.00	3.32	0.58	0.71	9.32	0.00	9.32	4.000	No	Yes	2.00
477	31.30	13.64	100.00	3.35	0.59	0.71	9.11	0.00	9.11	4.000	No	Yes	2.00
478	31.37	14.77	100.00	3.30	0.58	0.71	9.87	0.00	9.87	4.000	No	Yes	2.00
479	31.44	13.00	100.00	3.39	0.59	0.70	8.64	0.00	8.64	4.000	No	Yes	2.00
480	31.51	14.97	100.00	3.28	0.58	0.70	9.97	0.00	9.97	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	31.57	14.41	100.00	3.31	0.58	0.70	9.58	0.00	9.58	4.000	No	Yes	2.00
482	31.63	14.69	100.00	3.30	0.58	0.70	9.76	0.00	9.76	4.000	No	Yes	2.00
483	31.70	14.69	100.00	3.30	0.58	0.70	9.75	0.00	9.75	4.000	No	Yes	2.00
484	31.79	14.69	100.00	3.30	0.58	0.70	9.73	0.00	9.73	4.000	No	Yes	2.00
485	31.85	14.69	100.00	3.31	0.58	0.70	9.72	0.00	9.72	4.000	No	Yes	2.00
486	31.91	15.07	100.00	3.30	0.58	0.70	9.97	0.00	9.97	4.000	No	Yes	2.00
487	31.97	15.16	100.00	3.24	0.58	0.70	10.02	0.00	10.02	4.000	No	Yes	2.00
488	32.03	15.54	100.00	3.14	0.58	0.70	10.27	0.00	10.27	4.000	No	Yes	2.00
489	32.09	15.91	100.00	3.17	0.58	0.70	10.51	0.00	10.51	4.000	No	Yes	2.00
490	32.18	16.57	100.00	3.20	0.58	0.70	10.94	0.00	10.94	4.000	No	Yes	2.00
491	32.24	16.67	100.00	3.23	0.58	0.70	11.00	0.00	11.00	4.000	No	Yes	2.00
492	32.30	17.04	100.00	3.24	0.58	0.70	11.24	0.00	11.24	4.000	No	Yes	2.00
493	32.35	15.73	100.00	3.31	0.58	0.70	10.34	0.00	10.34	4.000	No	Yes	2.00
494	32.43	17.81	100.00	3.24	0.58	0.70	11.72	0.00	11.72	4.000	No	Yes	2.00
495	32.50	19.60	100.00	3.19	0.57	0.70	12.92	0.00	12.92	4.000	No	Yes	2.00
496	32.56	19.79	100.00	3.20	0.57	0.70	13.04	0.00	13.04	4.000	No	Yes	2.00
497	32.62	19.60	100.00	3.22	0.57	0.70	12.90	0.00	12.90	4.000	No	Yes	2.00
498	32.69	19.69	100.00	3.24	0.57	0.70	12.94	0.00	12.94	4.000	No	Yes	2.00
499	32.75	20.44	100.00	3.22	0.57	0.70	13.44	0.00	13.44	4.000	No	Yes	2.00
500	32.83	22.23	100.00	3.17	0.56	0.70	14.64	0.00	14.64	4.000	No	Yes	2.00
501	32.88	23.46	100.00	3.14	0.56	0.70	15.47	0.00	15.47	4.000	No	Yes	2.00
502	32.96	23.65	100.00	3.14	0.56	0.70	15.57	0.00	15.57	4.000	No	Yes	2.00
503	33.02	22.70	100.00	3.17	0.56	0.70	14.91	0.00	14.91	4.000	No	Yes	2.00
504	33.08	21.67	100.00	3.20	0.57	0.69	14.19	0.00	14.19	4.000	No	Yes	2.00
505	33.14	21.29	100.00	3.21	0.57	0.69	13.92	0.00	13.92	4.000	No	Yes	2.00
506	33.23	20.63	100.00	3.22	0.57	0.69	13.45	0.00	13.45	4.000	No	Yes	2.00
507	33.28	20.16	100.00	3.22	0.57	0.69	13.13	0.00	13.13	4.000	No	Yes	2.00
508	33.36	19.88	100.00	3.21	0.57	0.69	12.92	0.00	12.92	4.000	No	Yes	2.00
509	33.41	19.31	100.00	3.23	0.57	0.69	12.53	0.00	12.53	4.000	No	Yes	2.00
510	33.48	18.94	100.00	3.24	0.57	0.69	12.27	0.00	12.27	4.000	No	Yes	2.00
511	33.55	18.65	100.00	3.25	0.57	0.68	12.06	0.00	12.06	4.000	No	Yes	2.00
512	33.61	17.81	100.00	3.28	0.58	0.68	11.49	0.00	11.49	4.000	No	Yes	2.00
513	33.67	17.81	100.00	3.28	0.58	0.68	11.47	0.00	11.47	4.000	No	Yes	2.00
514	33.74	18.09	100.00	3.27	0.58	0.68	11.65	0.00	11.65	4.000	No	Yes	2.00
515	33.80	18.28	100.00	3.26	0.58	0.68	11.76	0.00	11.76	4.000	No	Yes	2.00
516	33.88	19.22	100.00	3.23	0.57	0.68	12.37	0.00	12.37	4.000	No	Yes	2.00
517	33.94	19.41	100.00	3.23	0.57	0.68	12.48	0.00	12.48	4.000	No	Yes	2.00
518	34.00	19.60	100.00	3.23	0.57	0.68	12.60	0.00	12.60	4.000	No	Yes	2.00
519	34.06	21.01	100.00	3.19	0.57	0.68	13.52	0.00	13.52	4.000	No	Yes	2.00
520	34.15	22.89	100.00	3.16	0.56	0.68	14.76	0.00	14.76	4.000	No	Yes	2.00
521	34.21	24.40	100.00	3.11	0.56	0.68	15.75	0.00	15.75	4.000	No	Yes	2.00
522	34.27	22.99	100.00	3.15	0.56	0.68	14.79	0.00	14.79	4.000	No	Yes	2.00
523	34.33	21.39	100.00	3.20	0.57	0.68	13.71	0.00	13.71	4.000	No	Yes	2.00
524	34.39	19.22	100.00	3.23	0.57	0.68	12.26	0.00	12.26	4.000	No	Yes	2.00
525	34.45	17.24	100.00	3.20	0.58	0.67	10.95	0.00	10.95	4.000	No	Yes	2.00
526	34.52	16.21	100.00	3.24	0.58	0.67	10.27	0.00	10.27	4.000	No	Yes	2.00
527	34.61	15.46	100.00	3.28	0.58	0.67	9.76	0.00	9.76	4.000	No	Yes	2.00
528	34.67	14.52	100.00	3.33	0.59	0.67	9.14	0.00	9.14	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	34.73	13.96	100.00	3.36	0.59	0.67	8.77	0.00	8.77	4.000	No	Yes	2.00
530	34.79	14.05	100.00	3.36	0.59	0.67	8.82	0.00	8.82	4.000	No	Yes	2.00
531	34.85	14.15	100.00	3.36	0.59	0.66	8.88	0.00	8.88	4.000	No	Yes	2.00
532	34.93	14.33	100.00	3.35	0.59	0.66	8.98	0.00	8.98	4.000	No	Yes	2.00
533	34.98	14.62	100.00	3.34	0.59	0.66	9.16	0.00	9.16	4.000	No	Yes	2.00
534	35.07	15.18	100.00	3.31	0.58	0.66	9.51	0.00	9.51	4.000	No	Yes	2.00
535	35.13	15.46	100.00	3.30	0.58	0.66	9.68	0.00	9.68	4.000	No	Yes	2.00
536	35.19	15.75	100.00	3.29	0.58	0.66	9.85	0.00	9.85	4.000	No	Yes	2.00
537	35.25	15.75	100.00	3.29	0.58	0.66	9.84	0.00	9.84	4.000	No	Yes	2.00
538	35.31	15.75	100.00	3.30	0.58	0.66	9.83	0.00	9.83	4.000	No	Yes	2.00
539	35.37	15.75	100.00	3.30	0.58	0.66	9.82	0.00	9.82	4.000	No	Yes	2.00
540	35.43	15.75	100.00	3.31	0.58	0.66	9.82	0.00	9.82	4.000	No	Yes	2.00
541	35.52	16.03	100.00	3.30	0.58	0.66	9.98	0.00	9.98	4.000	No	Yes	2.00
542	35.58	16.31	100.00	3.29	0.58	0.66	10.15	0.00	10.15	4.000	No	Yes	2.00
543	35.64	16.59	100.00	3.28	0.58	0.66	10.32	0.00	10.32	4.000	No	Yes	2.00
544	35.70	16.88	100.00	3.27	0.58	0.66	10.50	0.00	10.50	4.000	No	Yes	2.00
545	35.76	16.97	100.00	3.27	0.58	0.66	10.54	0.00	10.54	4.000	No	Yes	2.00
546	35.85	17.06	100.00	3.29	0.58	0.66	10.59	0.00	10.59	4.000	No	Yes	2.00
547	35.91	17.44	100.00	3.28	0.58	0.66	10.82	0.00	10.82	4.000	No	Yes	2.00
548	35.97	17.82	100.00	3.27	0.58	0.66	11.05	0.00	11.05	4.000	No	Yes	2.00
549	36.03	18.29	100.00	3.27	0.58	0.66	11.34	0.00	11.34	4.000	No	Yes	2.00
550	36.09	19.05	100.00	3.25	0.58	0.66	11.81	0.00	11.81	4.000	No	Yes	2.00
551	36.18	20.56	100.00	3.23	0.57	0.66	12.77	0.00	12.77	4.000	No	Yes	2.00
552	36.24	22.82	100.00	3.18	0.57	0.66	14.22	0.00	14.22	4.000	No	Yes	2.00
553	36.30	25.55	100.00	3.12	0.56	0.66	15.98	0.00	15.98	4.000	No	Yes	2.00
554	36.36	27.53	100.00	3.08	0.56	0.66	17.26	0.00	17.26	4.000	No	Yes	2.00
555	36.42	29.13	100.00	3.06	0.55	0.67	18.30	0.00	18.30	4.000	No	Yes	2.00
556	36.51	31.58	100.00	3.04	0.55	0.67	19.89	0.00	19.89	4.000	No	Yes	2.00
557	36.57	31.67	100.00	3.05	0.55	0.67	19.94	0.00	19.94	4.000	No	Yes	2.00
558	36.63	30.82	100.00	3.08	0.55	0.67	19.35	0.00	19.35	4.000	No	Yes	2.00
559	36.69	29.41	100.00	3.10	0.55	0.66	18.41	0.00	18.41	4.000	No	Yes	2.00
560	36.75	29.13	100.00	3.05	0.55	0.66	18.20	0.00	18.20	4.000	No	Yes	2.00
561	36.81	32.14	94.25	2.89	0.55	0.66	20.15	0.00	20.15	4.000	No	Yes	2.00
562	36.91	41.18	86.30	2.79	0.53	0.67	26.13	0.00	26.13	4.000	No	Yes	2.00
563	36.97	46.83	82.45	2.74	0.52	0.68	29.94	0.00	29.94	4.000	No	Yes	2.00
564	37.03	50.50	81.37	2.73	0.51	0.68	32.43	0.00	32.43	4.000	No	Yes	2.00
565	37.08	47.96	86.59	2.79	0.51	0.68	30.69	0.00	30.69	4.000	No	Yes	2.00
566	37.15	44.10	92.53	2.87	0.52	0.67	28.05	0.00	28.05	4.000	No	Yes	2.00
567	37.21	38.45	99.47	2.96	0.53	0.67	24.24	0.00	24.24	4.000	No	Yes	2.00
568	37.29	32.42	100.00	3.05	0.55	0.66	20.21	0.00	20.21	4.000	No	Yes	2.00
569	37.34	29.69	100.00	3.09	0.55	0.66	18.40	0.00	18.40	4.000	No	Yes	2.00
570	37.43	25.83	100.00	3.16	0.56	0.65	15.88	0.00	15.88	4.000	No	Yes	2.00
571	37.48	23.48	100.00	3.21	0.57	0.65	14.36	0.00	14.36	4.000	No	Yes	2.00
572	37.55	22.16	100.00	3.25	0.57	0.65	13.50	0.00	13.50	4.000	No	Yes	2.00
573	37.62	23.10	100.00	3.23	0.57	0.65	14.09	0.00	14.09	4.000	No	Yes	2.00
574	37.67	24.23	100.00	3.19	0.56	0.65	14.80	0.00	14.80	4.000	No	Yes	2.00
575	37.74	26.21	100.00	3.15	0.56	0.65	16.04	0.00	16.04	4.000	No	Yes	2.00
576	37.81	28.47	100.00	3.12	0.55	0.65	17.48	0.00	17.48	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
577	37.86	30.26	100.00	3.09	0.55	0.65	18.63	0.00	18.63	4.000	No	Yes	2.00
578	37.94	33.27	100.00	3.05	0.54	0.65	20.56	0.00	20.56	4.000	No	Yes	2.00
579	38.02	35.44	100.00	3.03	0.54	0.66	21.96	0.00	21.96	4.000	No	Yes	2.00
580	38.07	36.19	100.00	3.02	0.54	0.66	22.44	0.00	22.44	4.000	No	Yes	2.00
581	38.13	36.28	100.00	3.00	0.54	0.66	22.48	0.00	22.48	4.000	No	Yes	2.00
582	38.22	35.15	100.00	3.05	0.54	0.65	21.70	0.00	21.70	4.000	No	Yes	2.00
583	38.28	35.53	100.00	3.06	0.54	0.65	21.93	0.00	21.93	4.000	No	Yes	2.00
584	38.34	37.41	100.00	3.04	0.54	0.66	23.15	0.00	23.15	4.000	No	Yes	2.00
585	38.40	40.52	100.00	2.98	0.53	0.66	25.18	0.00	25.18	4.000	No	Yes	2.00
586	38.47	50.89	90.09	2.84	0.51	0.67	32.09	0.00	32.09	4.000	No	Yes	2.00
587	38.53	54.37	87.22	2.80	0.50	0.67	34.42	0.00	34.42	4.000	No	Yes	2.00
588	38.59	59.84	82.85	2.75	0.49	0.67	38.12	0.00	38.12	4.000	No	Yes	2.00
589	38.68	71.32	73.15	2.63	0.48	0.68	46.07	0.00	46.07	4.000	No	Yes	2.00
590	38.74	78.57	67.10	2.55	0.46	0.69	51.15	64.88	116.04	0.163	No	No	0.17
591	38.80	82.81	63.88	2.51	0.46	0.69	54.13	64.96	119.09	0.169	No	No	0.18
592	38.85	83.19	63.67	2.51	0.46	0.69	54.36	64.97	119.33	0.170	No	No	0.18
593	38.93	81.12	66.16	2.54	0.46	0.69	52.85	65.15	118.01	0.167	No	No	0.18
594	38.98	80.18	68.09	2.56	0.46	0.69	52.17	65.40	117.57	0.166	No	No	0.18
595	39.04	79.05	70.45	2.59	0.46	0.69	51.35	65.67	117.02	0.165	No	No	0.17
596	39.11	82.53	69.15	2.58	0.46	0.69	53.81	66.11	119.92	0.171	No	No	0.18
597	39.20	78.48	73.09	2.63	0.46	0.69	50.87	0.00	50.87	4.000	No	Yes	2.00
598	39.26	75.09	76.25	2.67	0.47	0.68	48.44	0.00	48.44	4.000	No	Yes	2.00
599	39.32	69.63	81.07	2.73	0.48	0.68	44.57	0.00	44.57	4.000	No	Yes	2.00
600	39.38	64.92	84.97	2.77	0.48	0.67	41.26	0.00	41.26	4.000	No	Yes	2.00
601	39.44	62.28	87.18	2.80	0.49	0.67	39.40	0.00	39.40	4.000	No	Yes	2.00
602	39.53	61.06	87.23	2.80	0.49	0.67	38.48	0.00	38.48	4.000	No	Yes	2.00
603	39.59	55.79	89.92	2.84	0.50	0.66	34.87	0.00	34.87	4.000	No	Yes	2.00
604	39.65	47.50	96.12	2.91	0.52	0.65	29.29	0.00	29.29	4.000	No	Yes	2.00
605	39.71	41.10	95.62	2.91	0.53	0.65	25.04	0.00	25.04	4.000	No	Yes	2.00
606	39.77	36.76	86.54	2.79	0.54	0.64	22.16	0.00	22.16	4.000	No	Yes	2.00
607	39.86	32.43	97.37	2.93	0.55	0.63	19.42	0.00	19.42	4.000	No	Yes	2.00
608	39.92	31.40	100.00	2.98	0.55	0.63	18.76	0.00	18.76	4.000	No	Yes	2.00
609	39.98	33.38	100.00	2.97	0.55	0.63	20.00	0.00	20.00	4.000	No	Yes	2.00
610	40.04	39.59	94.27	2.89	0.53	0.64	23.94	0.00	23.94	4.000	No	Yes	2.00
611	40.10	41.30	95.10	2.90	0.53	0.64	25.03	0.00	25.03	4.000	No	Yes	2.00
612	40.16	84.80	58.50	2.44	0.46	0.68	54.43	63.52	117.96	0.167	No	No	0.18
613	40.22	120.02	41.78	2.23	0.42	0.71	79.96	62.49	142.45	0.246	No	No	0.26
614	40.30	139.70	36.58	2.17	0.39	0.72	94.85	61.88	156.73	0.340	No	No	0.36
615	40.37	152.60	34.35	2.14	0.38	0.73	104.90	61.90	166.81	0.454	No	No	0.49
616	40.43	155.99	34.43	2.14	0.37	0.73	107.64	62.60	170.24	0.508	No	No	0.54
617	40.51	161.08	33.66	2.13	0.37	0.73	111.63	62.61	174.24	0.584	No	No	0.63
618	40.57	163.05	33.98	2.14	0.36	0.74	113.25	63.34	176.59	0.637	No	No	0.68
619	40.63	163.99	34.67	2.15	0.36	0.74	114.09	64.30	178.39	0.682	No	No	0.73
620	40.69	165.03	35.19	2.15	0.36	0.74	114.98	65.06	180.04	0.728	No	No	0.78
621	40.78	167.57	35.33	2.15	0.35	0.74	117.03	65.68	182.72	0.813	No	No	0.87
622	40.84	167.01	36.16	2.16	0.35	0.74	116.63	66.47	183.10	0.826	No	No	0.89
623	40.90	165.78	37.06	2.18	0.35	0.74	115.67	67.15	182.81	0.816	No	No	0.88
624	40.95	165.03	37.77	2.18	0.35	0.74	115.08	67.69	182.77	0.814	No	No	0.87

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	41.01	164.94	38.29	2.19	0.35	0.74	115.01	68.16	183.17	0.828	No	No	0.89
626	41.10	164.09	38.96	2.20	0.35	0.74	114.28	68.60	182.88	0.818	No	No	0.88
627	41.16	164.28	38.94	2.20	0.35	0.74	114.36	68.60	182.96	0.821	No	No	0.88
628	41.22	164.47	38.83	2.20	0.35	0.74	114.43	68.52	182.95	0.820	No	No	0.88
629	41.28	164.75	38.91	2.20	0.35	0.74	114.60	68.63	183.22	0.830	No	No	0.89
630	41.34	165.97	38.77	2.20	0.35	0.74	115.52	68.72	184.25	0.867	No	No	0.93
631	41.41	168.51	38.29	2.19	0.35	0.74	117.51	68.76	186.27	0.948	No	No	1.02
632	41.49	172.47	37.80	2.18	0.34	0.74	120.68	69.04	189.71	1.110	No	No	1.19
633	41.55	174.64	37.60	2.18	0.34	0.74	122.41	69.25	191.66	1.220	No	No	1.30
634	41.61	176.42	37.57	2.18	0.34	0.74	123.85	69.55	193.41	1.331	No	No	1.42
635	41.68	178.03	37.67	2.18	0.34	0.74	125.17	69.97	195.14	1.454	No	No	1.55
636	41.73	179.63	37.82	2.19	0.33	0.75	126.50	70.42	196.92	1.597	No	No	1.69
637	41.83	182.73	37.99	2.19	0.33	0.75	129.08	71.19	200.28	1.921	No	No	2.00
638	41.89	184.71	38.16	2.19	0.33	0.75	130.75	71.75	202.50	2.184	No	No	2.00
639	41.95	187.35	38.01	2.19	0.32	0.75	132.94	72.13	205.07	2.548	No	No	2.00
640	42.01	189.42	37.94	2.19	0.32	0.75	134.66	72.45	207.11	2.893	No	No	2.00
641	42.06	190.83	37.71	2.18	0.32	0.75	135.77	72.48	208.25	3.111	No	No	2.00
642	42.16	190.17	37.61	2.18	0.32	0.75	135.04	72.21	207.25	2.919	No	No	2.00
643	42.22	187.91	38.45	2.19	0.32	0.75	133.14	72.61	205.75	2.656	No	No	2.00
644	42.28	184.71	39.64	2.21	0.33	0.75	130.48	73.09	203.56	2.326	No	No	2.00
645	42.34	181.04	40.74	2.22	0.33	0.74	127.39	73.31	200.70	1.968	No	No	2.00
646	42.40	177.55	41.61	2.23	0.33	0.74	124.44	73.30	197.74	1.669	No	No	1.77
647	42.48	164.28	45.40	2.28	0.35	0.73	113.54	73.34	186.88	0.974	No	No	1.04
648	42.54	167.01	44.09	2.26	0.35	0.73	115.61	72.97	188.58	1.053	No	No	1.12
649	42.60	163.05	45.12	2.28	0.35	0.73	112.33	72.85	185.17	0.903	No	No	0.97
650	42.66	158.82	46.35	2.29	0.36	0.73	108.86	72.75	181.60	0.776	No	No	0.83
651	42.72	154.48	47.63	2.31	0.36	0.72	105.32	72.59	177.92	0.670	No	No	0.72
652	42.78	150.34	48.71	2.32	0.37	0.72	101.95	72.32	174.27	0.585	No	No	0.62
653	42.87	145.82	49.85	2.34	0.37	0.71	98.27	71.96	170.23	0.508	No	No	0.54
654	42.93	143.47	50.40	2.34	0.38	0.71	96.35	71.72	168.07	0.473	No	No	0.50
655	42.99	142.62	50.40	2.34	0.38	0.71	95.60	71.53	167.13	0.459	No	No	0.49
656	43.05	142.24	50.35	2.34	0.38	0.71	95.23	71.40	166.63	0.452	No	No	0.48
657	43.11	142.34	50.17	2.34	0.38	0.71	95.23	71.31	166.54	0.451	No	No	0.48
658	43.20	142.81	49.79	2.33	0.38	0.71	95.48	71.19	166.67	0.452	No	No	0.48
659	43.26	142.71	49.72	2.33	0.38	0.71	95.33	71.11	166.44	0.449	No	No	0.48
660	43.32	142.71	49.72	2.33	0.38	0.71	95.27	71.10	166.36	0.448	No	No	0.48
661	43.38	142.24	49.98	2.34	0.38	0.71	94.84	71.11	165.96	0.443	No	No	0.47
662	43.44	140.45	50.65	2.35	0.38	0.70	93.40	71.07	164.47	0.423	No	No	0.45
663	43.51	138.38	51.39	2.35	0.38	0.70	91.74	70.98	162.72	0.402	No	No	0.43
664	43.59	134.99	52.53	2.37	0.39	0.70	89.05	70.78	159.83	0.370	No	No	0.39
665	43.65	132.73	53.16	2.38	0.39	0.70	87.25	70.57	157.82	0.350	No	No	0.37
666	43.71	130.09	53.94	2.39	0.39	0.69	85.18	70.34	155.52	0.330	No	No	0.35
667	43.77	127.55	54.58	2.39	0.40	0.69	83.19	70.06	153.24	0.312	No	No	0.33
668	43.83	124.35	55.54	2.41	0.40	0.69	80.71	69.76	150.47	0.292	No	No	0.31
669	43.92	118.42	57.47	2.43	0.41	0.68	76.20	69.23	145.43	0.261	No	No	0.28
670	43.98	113.24	59.48	2.46	0.42	0.68	72.33	68.83	141.16	0.240	No	No	0.25
671	44.05	106.18	62.95	2.50	0.43	0.67	67.09	68.39	135.48	0.216	No	No	0.23
672	44.10	97.89	65.46	2.53	0.44	0.66	61.09	67.35	128.44	0.193	No	No	0.20

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
673	44.16	88.76	68.90	2.57	0.46	0.65	54.64	66.30	120.94	0.174	No	No	0.18
674	44.23	80.47	74.77	2.65	0.47	0.64	48.95	0.00	48.95	4.000	No	Yes	2.00
675	44.32	70.77	81.64	2.73	0.48	0.63	42.40	0.00	42.40	4.000	No	Yes	2.00
676	44.38	65.97	85.26	2.78	0.49	0.63	39.18	0.00	39.18	4.000	No	Yes	2.00
677	44.43	60.79	89.49	2.83	0.50	0.62	35.82	0.00	35.82	4.000	No	Yes	2.00
678	44.49	68.13	83.78	2.76	0.49	0.63	40.57	0.00	40.57	4.000	No	Yes	2.00
679	44.57	67.76	83.94	2.76	0.49	0.63	40.29	0.00	40.29	4.000	No	Yes	2.00
680	44.63	68.23	83.52	2.76	0.49	0.63	40.56	0.00	40.56	4.000	No	Yes	2.00
681	44.70	65.97	85.04	2.78	0.49	0.63	39.01	0.00	39.01	4.000	No	Yes	2.00
682	44.77	68.32	83.23	2.75	0.49	0.63	40.55	0.00	40.55	4.000	No	Yes	2.00
683	44.82	69.83	82.19	2.74	0.48	0.63	41.51	0.00	41.51	4.000	No	Yes	2.00
684	44.88	73.31	79.54	2.71	0.48	0.63	43.77	0.00	43.77	4.000	No	Yes	2.00
685	44.97	80.47	75.39	2.65	0.47	0.64	48.51	0.00	48.51	4.000	No	Yes	2.00
686	45.03	90.54	69.27	2.58	0.45	0.65	55.32	66.58	121.90	0.176	No	No	0.19
687	45.10	102.88	62.61	2.50	0.44	0.66	63.86	67.38	131.24	0.202	No	No	0.21
688	45.16	112.20	58.19	2.44	0.42	0.66	70.42	67.87	138.29	0.227	No	No	0.24
689	45.22	116.35	56.30	2.42	0.42	0.67	73.47	68.05	141.52	0.242	No	No	0.26
690	45.28	118.61	54.93	2.40	0.42	0.67	75.03	67.97	143.01	0.249	No	No	0.26
691	45.37	122.37	52.80	2.37	0.41	0.67	77.66	67.83	145.49	0.262	No	No	0.28
692	45.43	125.01	51.62	2.36	0.41	0.67	79.53	67.81	147.34	0.272	No	No	0.29
693	45.49	127.93	50.33	2.34	0.40	0.68	81.61	67.78	149.38	0.285	No	No	0.30
694	45.55	131.13	49.15	2.33	0.40	0.68	83.91	67.81	151.72	0.301	No	No	0.32
695	45.61	135.56	47.80	2.31	0.40	0.68	87.16	67.96	155.12	0.327	No	No	0.35
696	45.67	140.08	46.38	2.29	0.39	0.68	90.49	68.03	158.52	0.357	No	No	0.38
697	45.76	143.00	45.85	2.29	0.39	0.69	92.64	68.28	160.91	0.381	No	No	0.40
698	45.82	142.15	46.29	2.29	0.39	0.68	91.95	68.36	160.31	0.375	No	No	0.40
699	45.88	139.23	47.31	2.30	0.39	0.68	89.70	68.35	158.06	0.353	No	No	0.37
700	45.94	135.65	48.34	2.32	0.40	0.68	86.96	68.19	155.15	0.327	No	No	0.35
701	46.00	131.22	49.48	2.33	0.40	0.67	83.59	67.89	151.48	0.299	No	No	0.32
702	46.09	125.39	50.85	2.35	0.41	0.67	79.17	67.37	146.54	0.268	No	No	0.28
703	46.15	122.56	51.61	2.36	0.41	0.67	77.04	67.15	144.19	0.255	No	No	0.27
704	46.21	119.17	52.85	2.37	0.42	0.66	74.54	67.00	141.54	0.242	No	No	0.26
705	46.27	115.40	54.40	2.39	0.42	0.66	71.79	66.88	138.67	0.229	No	No	0.24
706	46.33	111.07	56.65	2.42	0.43	0.65	68.58	66.83	135.42	0.216	No	No	0.23
707	46.42	104.86	61.02	2.48	0.44	0.65	64.23	67.03	131.26	0.202	No	No	0.21
708	46.48	102.03	56.99	2.42	0.44	0.64	62.00	65.13	127.14	0.189	No	No	0.20
709	46.54	100.15	51.45	2.36	0.45	0.64	60.36	62.61	122.97	0.178	No	No	0.19
710	46.60	99.87	52.94	2.37	0.45	0.64	60.20	63.17	123.37	0.179	No	No	0.19
711	46.66	100.43	53.56	2.38	0.45	0.64	60.58	63.51	124.09	0.181	No	No	0.19
712	46.72	100.06	54.52	2.39	0.45	0.64	60.33	63.80	124.13	0.181	No	No	0.19
713	46.80	92.33	59.92	2.46	0.46	0.63	55.12	64.14	119.26	0.170	No	No	0.18
714	46.86	95.05	58.63	2.45	0.46	0.63	56.92	64.26	121.17	0.174	No	No	0.18
715	46.93	95.43	58.74	2.45	0.45	0.63	57.14	64.35	121.50	0.175	No	No	0.19
716	46.98	94.11	59.92	2.46	0.46	0.63	56.24	64.46	120.70	0.173	No	No	0.18
717	47.07	88.37	64.19	2.51	0.46	0.63	52.38	64.54	116.91	0.165	No	No	0.17
718	47.13	83.57	67.54	2.56	0.47	0.62	49.18	64.41	113.59	0.158	No	No	0.17
719	47.19	79.05	70.47	2.59	0.48	0.62	46.18	64.17	110.35	0.153	No	No	0.16
720	47.25	74.62	73.31	2.63	0.48	0.61	43.28	0.00	43.28	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	47.31	70.10	76.76	2.67	0.49	0.61	40.31	0.00	40.31	4.000	No	Yes	2.00
722	47.40	62.94	82.30	2.74	0.50	0.60	35.80	0.00	35.80	4.000	No	Yes	2.00
723	47.46	57.20	87.20	2.80	0.51	0.60	32.24	0.00	32.24	4.000	No	Yes	2.00
724	47.52	50.04	93.74	2.88	0.52	0.59	27.82	0.00	27.82	4.000	No	Yes	2.00
725	47.58	43.36	100.00	2.97	0.53	0.58	23.81	0.00	23.81	4.000	No	Yes	2.00
726	47.64	37.90	100.00	3.05	0.54	0.57	20.57	0.00	20.57	4.000	No	Yes	2.00
727	47.73	31.77	100.00	3.14	0.56	0.57	17.01	0.00	17.01	4.000	No	Yes	2.00
728	47.79	29.23	100.00	3.18	0.56	0.56	15.55	0.00	15.55	4.000	No	Yes	2.00
729	47.85	30.17	100.00	3.13	0.56	0.56	16.07	0.00	16.07	4.000	No	Yes	2.00
730	47.91	34.51	100.00	3.01	0.55	0.57	18.54	0.00	18.54	4.000	No	Yes	2.00
731	47.97	40.45	93.72	2.88	0.54	0.57	21.94	0.00	21.94	4.000	No	Yes	2.00
732	48.03	46.66	86.34	2.79	0.53	0.58	25.55	0.00	25.55	4.000	No	Yes	2.00
733	48.12	50.81	82.01	2.74	0.52	0.58	27.99	0.00	27.99	4.000	No	Yes	2.00
734	48.18	50.89	82.76	2.75	0.52	0.58	28.03	0.00	28.03	4.000	No	Yes	2.00
735	48.24	48.54	87.30	2.80	0.53	0.58	26.63	0.00	26.63	4.000	No	Yes	2.00
736	48.30	44.49	93.77	2.88	0.53	0.58	24.24	0.00	24.24	4.000	No	Yes	2.00
737	48.36	39.97	100.00	2.97	0.54	0.57	21.60	0.00	21.60	4.000	No	Yes	2.00
738	48.45	34.98	100.00	3.04	0.55	0.57	18.69	0.00	18.69	4.000	No	Yes	2.00
739	48.51	35.12	100.00	3.02	0.55	0.57	18.76	0.00	18.76	4.000	No	Yes	2.00
740	48.57	35.12	100.00	3.00	0.55	0.57	18.74	0.00	18.74	4.000	No	Yes	2.00
741	48.63	35.27	100.00	3.00	0.55	0.57	18.81	0.00	18.81	4.000	No	Yes	2.00
742	48.69	36.95	100.00	2.97	0.55	0.57	19.77	0.00	19.77	4.000	No	Yes	2.00
743	48.78	35.36	99.21	2.95	0.55	0.56	18.82	0.00	18.82	4.000	No	Yes	2.00
744	48.84	33.47	100.00	3.04	0.55	0.56	17.74	0.00	17.74	4.000	No	Yes	2.00
745	48.90	32.63	100.00	3.10	0.56	0.56	17.25	0.00	17.25	4.000	No	Yes	2.00
746	48.96	33.57	100.00	3.10	0.55	0.56	17.77	0.00	17.77	4.000	No	Yes	2.00
747	49.03	34.70	100.00	3.10	0.55	0.56	18.40	0.00	18.40	4.000	No	Yes	2.00
748	49.09	35.65	100.00	3.09	0.55	0.56	18.93	0.00	18.93	4.000	No	Yes	2.00
749	49.15	30.94	100.00	3.20	0.56	0.56	16.25	0.00	16.25	4.000	No	Yes	2.00
750	49.21	57.68	87.47	2.81	0.51	0.59	31.89	0.00	31.89	4.000	No	Yes	2.00
751	49.30	75.76	75.30	2.65	0.48	0.60	43.06	0.00	43.06	4.000	No	Yes	2.00
752	49.36	93.65	64.83	2.52	0.46	0.62	54.64	65.34	119.98	0.171	No	No	0.18
753	49.42	103.07	60.99	2.47	0.44	0.63	60.93	66.09	127.03	0.189	No	No	0.20
754	49.48	116.82	55.32	2.40	0.43	0.64	70.46	66.87	137.33	0.223	No	No	0.24
755	49.55	132.54	49.20	2.33	0.41	0.65	81.54	67.21	148.75	0.281	No	No	0.30
756	49.61	143.47	45.16	2.28	0.39	0.66	89.38	67.02	156.40	0.338	No	No	0.36
757	49.70	157.50	30.79	2.10	0.40	0.66	97.59	56.11	153.70	0.315	No	No	0.33
758	49.76	164.28	26.91	2.05	0.40	0.65	101.58	51.23	152.81	0.309	No	No	0.33
759	49.82	168.61	27.24	2.05	0.39	0.66	105.02	52.41	157.44	0.347	No	No	0.37
760	49.88	170.48	28.42	2.07	0.39	0.66	106.86	54.63	161.49	0.388	No	No	0.41
761	49.94	171.33	29.70	2.08	0.38	0.67	107.89	56.72	164.61	0.425	No	No	0.45
762	50.00	169.92	31.41	2.11	0.38	0.67	107.21	58.91	166.12	4.000	No	No	2.00
763	50.07	156.25	37.05	2.18	0.39	0.66	97.67	62.96	160.63	4.000	No	No	2.00
764	50.14	162.19	35.55	2.16	0.38	0.67	101.96	62.50	164.45	4.000	No	No	2.00
765	50.20	163.97	35.43	2.16	0.38	0.67	103.28	62.68	165.96	4.000	No	No	2.00
766	50.27	164.27	34.46	2.14	0.38	0.67	103.22	61.65	164.87	4.000	No	No	2.00
767	50.34	164.74	28.13	2.06	0.40	0.65	101.75	53.19	154.95	4.000	No	No	2.00
768	50.41	167.00	31.82	2.11	0.38	0.66	104.58	58.87	163.45	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
769	50.46	165.21	33.28	2.13	0.38	0.66	103.49	60.40	163.88	4.000	No	No	2.00
770	50.54	161.44	35.64	2.16	0.38	0.66	100.97	62.37	163.34	4.000	No	No	2.00
771	50.61	158.90	37.48	2.18	0.38	0.66	99.28	63.73	163.00	4.000	No	No	2.00
772	50.67	156.59	39.23	2.20	0.38	0.66	97.73	64.88	162.60	4.000	No	No	2.00
773	50.74	151.74	42.19	2.24	0.39	0.66	94.34	66.32	160.67	4.000	No	No	2.00
774	50.79	154.47	41.80	2.24	0.38	0.66	96.36	66.54	162.90	4.000	No	No	2.00
775	50.85	154.66	42.25	2.24	0.38	0.66	96.51	66.90	163.42	4.000	No	No	2.00
776	50.94	154.57	43.29	2.25	0.38	0.66	96.50	67.62	164.12	4.000	No	No	2.00
777	51.01	154.76	43.92	2.26	0.38	0.66	96.67	68.08	164.76	4.000	No	No	2.00
778	51.06	154.85	44.07	2.26	0.38	0.66	96.71	68.19	164.90	4.000	No	No	2.00
779	51.13	155.13	44.09	2.26	0.38	0.66	96.87	68.25	165.12	4.000	No	No	2.00
780	51.18	156.17	44.18	2.26	0.38	0.66	97.64	68.50	166.14	4.000	No	No	2.00
781	51.27	158.15	43.72	2.26	0.38	0.66	99.05	68.55	167.60	4.000	No	No	2.00
782	51.33	159.46	43.14	2.25	0.38	0.66	99.94	68.38	168.32	4.000	No	No	2.00
783	51.38	158.81	43.26	2.25	0.38	0.66	99.39	68.32	167.72	4.000	No	No	2.00
784	51.46	158.43	43.25	2.25	0.38	0.66	99.02	68.22	167.24	4.000	No	No	2.00
785	51.52	158.24	43.32	2.25	0.38	0.66	98.82	68.23	167.04	4.000	No	No	2.00
786	51.58	157.20	42.68	2.25	0.38	0.66	97.86	67.54	165.40	4.000	No	No	2.00
787	51.64	156.55	40.94	2.22	0.38	0.66	97.03	66.07	163.10	4.000	No	No	2.00
788	51.73	159.18	41.99	2.24	0.38	0.66	99.16	67.37	166.53	4.000	No	No	2.00
789	51.79	163.51	41.02	2.23	0.37	0.66	102.36	67.43	169.79	4.000	No	No	2.00
790	51.85	170.11	39.02	2.20	0.37	0.67	107.19	66.96	174.16	4.000	No	No	2.00
791	51.91	177.83	36.33	2.17	0.36	0.67	112.79	65.76	178.55	4.000	No	No	2.00
792	51.98	164.83	40.62	2.22	0.37	0.66	103.15	67.31	170.46	4.000	No	No	2.00
793	52.05	186.58	33.80	2.13	0.35	0.68	119.15	64.42	183.57	4.000	No	No	2.00
794	52.10	187.71	33.73	2.13	0.35	0.68	120.00	64.52	184.53	4.000	No	No	2.00
795	52.18	187.15	34.07	2.14	0.35	0.68	119.56	64.84	184.39	4.000	No	No	2.00
796	52.23	186.68	34.08	2.14	0.35	0.68	119.11	64.74	183.85	4.000	No	No	2.00
797	52.31	186.49	33.69	2.13	0.35	0.67	118.76	64.21	182.97	4.000	No	No	2.00
798	52.36	184.14	34.19	2.14	0.36	0.67	116.91	64.39	181.30	4.000	No	No	2.00
799	52.44	179.52	35.98	2.16	0.36	0.67	113.52	65.57	179.09	4.000	No	No	2.00
800	52.51	174.91	37.49	2.18	0.36	0.67	110.06	66.26	176.32	4.000	No	No	2.00
801	52.57	171.71	38.54	2.19	0.37	0.66	107.65	66.65	174.30	4.000	No	No	2.00
802	52.63	169.73	39.17	2.20	0.37	0.66	106.13	66.84	172.97	4.000	No	No	2.00
803	52.72	162.95	41.53	2.23	0.37	0.66	101.10	67.51	168.60	4.000	No	No	2.00
804	52.77	158.52	42.93	2.25	0.38	0.65	97.79	67.69	165.48	4.000	No	No	2.00
805	52.84	154.29	44.26	2.27	0.38	0.65	94.64	67.80	162.44	4.000	No	No	2.00
806	52.90	150.14	45.81	2.29	0.39	0.65	91.60	67.98	159.58	4.000	No	No	2.00
807	52.95	146.19	47.38	2.30	0.39	0.64	88.74	68.14	156.89	4.000	No	No	2.00
808	53.04	140.35	49.69	2.33	0.40	0.64	84.54	68.25	152.79	4.000	No	No	2.00
809	53.10	137.62	50.77	2.35	0.40	0.64	82.58	68.24	150.83	4.000	No	No	2.00
810	53.16	135.55	51.44	2.36	0.41	0.63	81.08	68.15	149.23	4.000	No	No	2.00
811	53.23	133.85	51.86	2.36	0.41	0.63	79.84	68.00	147.85	4.000	No	No	2.00
812	53.29	132.63	52.25	2.37	0.41	0.63	78.95	67.94	146.89	4.000	No	No	2.00
813	53.35	131.59	52.57	2.37	0.41	0.63	78.19	67.87	146.06	4.000	No	No	2.00
814	53.44	129.33	53.29	2.38	0.41	0.63	76.57	67.74	144.30	4.000	No	No	2.00
815	53.50	126.98	54.30	2.39	0.42	0.62	74.91	67.69	142.60	4.000	No	No	2.00
816	53.56	122.27	56.32	2.42	0.42	0.62	71.64	67.56	139.20	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	53.62	117.28	58.31	2.44	0.43	0.62	68.20	67.29	135.49	4.000	No	No	2.00
818	53.67	117.61	57.62	2.43	0.43	0.62	68.37	67.11	135.48	4.000	No	No	2.00
819	53.76	115.87	57.61	2.43	0.43	0.61	66.99	66.72	133.71	4.000	No	No	2.00
820	53.82	117.94	55.72	2.41	0.43	0.61	68.44	66.46	134.90	4.000	No	No	2.00
821	53.88	117.84	53.40	2.38	0.43	0.61	68.07	65.48	133.55	4.000	No	No	2.00
822	53.94	117.17	50.89	2.35	0.44	0.61	67.42	64.26	131.68	4.000	No	No	2.00
823	54.00	115.76	52.05	2.36	0.44	0.61	66.50	64.51	131.01	4.000	No	No	2.00
824	54.09	112.47	53.93	2.39	0.44	0.61	64.33	64.67	129.00	4.000	No	No	2.00
825	54.16	110.02	55.69	2.41	0.44	0.60	62.73	64.89	127.62	4.000	No	No	2.00
826	54.22	106.92	57.96	2.44	0.45	0.60	60.72	65.10	125.82	4.000	No	No	2.00
827	54.27	100.23	62.23	2.49	0.45	0.60	56.40	65.16	121.57	4.000	No	No	2.00
828	54.34	101.46	62.11	2.49	0.45	0.60	57.20	65.36	122.56	4.000	No	No	2.00
829	54.41	102.40	62.10	2.49	0.45	0.60	57.81	65.53	123.33	4.000	No	No	2.00
830	54.47	104.85	60.88	2.47	0.45	0.60	59.38	65.62	125.00	4.000	No	No	2.00
831	54.56	109.46	57.51	2.43	0.44	0.60	62.31	65.39	127.71	4.000	No	No	2.00
832	54.62	111.71	55.41	2.41	0.44	0.60	63.72	65.06	128.78	4.000	No	No	2.00
833	54.68	111.35	54.85	2.40	0.44	0.60	63.42	64.77	128.18	4.000	No	No	2.00
834	54.74	110.30	54.99	2.40	0.44	0.60	62.70	64.62	127.32	4.000	No	No	2.00
835	54.80	108.80	55.71	2.41	0.45	0.60	61.69	64.61	126.30	4.000	No	No	2.00
836	54.86	106.83	56.75	2.42	0.45	0.60	60.40	64.61	125.01	4.000	No	No	2.00
837	54.95	103.25	58.60	2.44	0.45	0.60	58.06	64.56	122.62	4.000	No	No	2.00
838	55.01	100.89	60.01	2.46	0.46	0.59	56.53	64.57	121.10	4.000	No	No	2.00
839	55.07	98.26	61.63	2.48	0.46	0.59	54.84	64.56	119.40	4.000	No	No	2.00
840	55.13	96.84	62.69	2.50	0.46	0.59	53.93	64.59	118.52	4.000	No	No	2.00
841	55.19	98.35	62.07	2.49	0.46	0.59	54.89	64.69	119.58	4.000	No	No	2.00
842	55.28	97.88	62.34	2.49	0.46	0.59	54.56	64.67	119.24	4.000	No	No	2.00
843	55.34	98.43	61.44	2.48	0.46	0.59	54.88	64.51	119.39	4.000	No	No	2.00
844	55.40	99.29	60.87	2.47	0.46	0.59	55.40	64.50	119.90	4.000	No	No	2.00
845	55.45	100.41	60.35	2.47	0.46	0.59	56.11	64.55	120.66	4.000	No	No	2.00
846	55.51	100.80	59.98	2.46	0.46	0.59	56.33	64.50	120.83	4.000	No	No	2.00
847	55.60	100.33	60.79	2.47	0.46	0.59	56.02	64.65	120.68	4.000	No	No	2.00
848	55.66	99.29	62.11	2.49	0.46	0.59	55.37	64.84	120.21	4.000	No	No	2.00
849	55.73	98.07	64.02	2.51	0.46	0.59	54.63	65.13	119.76	4.000	No	No	2.00
850	55.79	97.22	65.82	2.54	0.46	0.59	54.11	65.43	119.55	4.000	No	No	2.00
851	55.84	98.63	65.81	2.54	0.46	0.59	55.02	65.69	120.72	4.000	No	No	2.00
852	55.94	107.48	61.18	2.48	0.45	0.60	60.72	66.09	126.80	4.000	No	No	2.00
853	56.00	115.96	55.60	2.41	0.44	0.60	66.19	65.80	131.99	4.000	No	No	2.00
854	56.06	124.81	49.86	2.34	0.43	0.61	72.09	65.03	137.12	4.000	No	No	2.00
855	56.12	131.40	44.89	2.27	0.42	0.61	76.29	63.53	139.82	4.000	No	No	2.00
856	56.18	137.99	40.74	2.22	0.42	0.62	80.50	61.89	142.39	4.000	No	No	2.00
857	56.24	141.76	39.04	2.20	0.41	0.62	82.97	61.20	144.17	4.000	No	No	2.00
858	56.30	143.46	38.03	2.19	0.41	0.62	84.02	60.63	144.65	4.000	No	No	2.00
859	56.39	146.09	36.98	2.17	0.41	0.62	85.73	60.13	145.86	4.000	No	No	2.00
860	56.43	146.05	37.16	2.18	0.41	0.62	85.71	60.28	146.00	4.000	No	No	2.00
861	56.50	146.00	37.68	2.18	0.41	0.62	85.74	60.74	146.49	4.000	No	No	2.00
862	56.56	149.11	37.18	2.18	0.41	0.62	87.93	60.82	148.75	4.000	No	No	2.00
863	56.65	150.05	38.10	2.19	0.40	0.63	88.75	61.80	150.56	4.000	No	No	2.00
864	56.71	149.95	39.07	2.20	0.40	0.63	88.82	62.63	151.45	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	56.77	149.48	39.98	2.21	0.40	0.63	88.60	63.28	151.88	4.000	No	No	2.00
866	56.84	149.29	40.47	2.22	0.40	0.63	88.51	63.64	152.15	4.000	No	No	2.00
867	56.89	149.58	40.57	2.22	0.40	0.63	88.72	63.76	152.48	4.000	No	No	2.00
868	56.98	151.08	40.21	2.22	0.40	0.63	89.74	63.74	153.48	4.000	No	No	2.00
869	57.04	152.31	39.96	2.21	0.40	0.63	90.60	63.76	154.36	4.000	No	No	2.00
870	57.10	153.34	39.94	2.21	0.40	0.63	91.35	63.92	155.27	4.000	No	No	2.00
871	57.16	154.57	39.83	2.21	0.39	0.63	92.23	64.05	156.28	4.000	No	No	2.00
872	57.22	156.45	39.43	2.21	0.39	0.63	93.56	64.05	157.61	4.000	No	No	2.00
873	57.31	162.01	37.59	2.18	0.39	0.64	97.41	63.39	160.80	4.000	No	No	2.00
874	57.37	166.43	36.02	2.16	0.38	0.64	100.45	62.63	163.08	4.000	No	No	2.00
875	57.43	171.71	34.29	2.14	0.38	0.64	104.11	61.66	165.77	4.000	No	No	2.00
876	57.49	176.04	33.13	2.13	0.38	0.64	107.16	61.01	168.17	4.000	No	No	2.00
877	57.55	179.52	32.25	2.12	0.37	0.65	109.62	60.48	170.10	4.000	No	No	2.00
878	57.61	182.25	31.48	2.11	0.37	0.65	111.51	59.91	171.42	4.000	No	No	2.00
879	57.70	186.30	30.35	2.09	0.37	0.65	114.31	58.95	173.26	4.000	No	No	2.00
880	57.76	188.47	29.88	2.09	0.37	0.65	115.85	58.60	174.45	4.000	No	No	2.00
881	57.82	190.35	29.74	2.08	0.36	0.65	117.28	58.67	175.95	4.000	No	No	2.00
882	57.88	191.76	29.71	2.08	0.36	0.65	118.37	58.85	177.23	4.000	No	No	2.00
883	57.94	194.12	29.41	2.08	0.36	0.65	120.14	58.76	178.90	4.000	No	No	2.00
884	58.03	197.70	29.00	2.07	0.36	0.66	122.85	58.66	181.51	4.000	No	No	2.00
885	58.09	199.86	28.90	2.07	0.35	0.66	124.55	58.85	183.39	4.000	No	No	2.00
886	58.16	201.56	28.99	2.07	0.35	0.66	125.95	59.27	185.22	4.000	No	No	2.00
887	58.22	204.10	28.86	2.07	0.35	0.66	127.97	59.46	187.43	4.000	No	No	2.00
888	58.28	207.49	28.53	2.07	0.34	0.67	130.61	59.43	190.05	4.000	No	No	2.00
889	58.34	211.63	27.81	2.06	0.34	0.67	133.72	58.83	192.55	4.000	No	No	2.00
890	58.42	217.47	26.83	2.05	0.34	0.67	138.11	57.88	195.99	4.000	No	No	2.00
891	58.48	219.26	26.92	2.05	0.33	0.67	139.65	58.35	198.00	4.000	No	No	2.00
892	58.55	220.67	27.09	2.05	0.33	0.68	140.91	58.88	199.80	4.000	No	No	2.00
893	58.60	222.74	27.03	2.05	0.33	0.68	142.63	59.11	201.74	4.000	No	No	2.00
894	58.67	225.29	26.68	2.05	0.33	0.68	144.60	58.81	203.40	4.000	No	No	2.00
895	58.75	229.71	25.85	2.04	0.32	0.68	147.89	57.76	205.65	4.000	No	No	2.00
896	58.81	232.73	25.69	2.03	0.32	0.68	150.39	57.89	208.28	4.000	No	No	2.00
897	58.87	235.36	21.04	1.98	0.34	0.67	149.12	46.55	195.68	4.000	No	No	2.00
898	58.94	238.38	14.46	1.89	0.37	0.64	144.52	24.84	169.36	4.000	No	No	2.00
899	59.00	240.26	15.56	1.91	0.36	0.65	147.43	29.05	176.48	4.000	No	No	2.00
900	59.06	241.20	16.64	1.92	0.36	0.66	149.48	33.02	182.51	4.000	No	No	2.00
901	59.15	240.35	18.36	1.94	0.35	0.66	150.63	38.85	189.48	4.000	No	No	2.00
902	59.20	227.92	22.19	1.99	0.34	0.67	143.48	48.74	192.22	4.000	No	No	2.00
903	59.27	227.97	23.01	2.00	0.34	0.67	144.10	50.83	194.93	4.000	No	No	2.00
904	59.32	228.02	23.60	2.01	0.34	0.67	144.54	52.29	196.83	4.000	No	No	2.00
905	59.40	231.60	23.85	2.01	0.33	0.68	147.76	53.39	201.15	4.000	No	No	2.00
906	59.46	235.17	24.22	2.02	0.32	0.68	151.10	54.80	205.89	4.000	No	No	2.00
907	59.53	239.60	24.23	2.02	0.32	0.68	154.96	55.48	210.45	4.000	No	No	2.00
908	59.58	242.24	24.16	2.01	0.31	0.69	157.74	55.78	213.52	4.000	No	No	2.00
909	59.66	246.30	23.90	2.01	0.31	0.69	161.14	55.74	216.88	4.000	No	No	2.00
910	59.73	250.05	23.75	2.01	0.30	0.70	164.40	55.93	220.33	4.000	No	No	2.00
911	59.79	252.13	18.26	1.94	0.33	0.67	160.29	39.69	199.99	4.000	No	No	2.00
912	59.86	253.35	0.00	1.68	0.41	0.61	146.71	0.00	146.71	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
913	59.93	254.58	0.00	1.71	0.41	0.61	147.65	0.00	147.65	4.000	No	No	2.00
914	59.98	254.01	0.87	1.72	0.41	0.61	147.16	0.00	147.16	4.000	No	No	2.00
915	60.05	253.07	2.73	1.75	0.41	0.61	146.34	0.00	146.34	4.000	No	No	2.00
916	60.12	250.24	5.45	1.78	0.41	0.61	144.14	0.36	144.50	4.000	No	No	2.00
917	60.19	234.14	12.44	1.87	0.40	0.62	137.52	17.05	154.57	4.000	No	No	2.00
918	60.24	240.82	13.22	1.88	0.38	0.63	143.96	20.24	164.21	4.000	No	No	2.00
919	60.32	238.75	17.74	1.93	0.35	0.66	147.77	36.53	184.30	4.000	No	No	2.00
920	60.38	235.55	20.52	1.97	0.34	0.66	147.81	44.94	192.75	4.000	No	No	2.00
921	60.44	232.35	22.68	2.00	0.34	0.67	146.85	50.47	197.32	4.000	No	No	2.00
922	60.50	231.31	24.07	2.01	0.33	0.67	146.96	53.77	200.72	4.000	No	No	2.00
923	60.59	231.60	25.12	2.03	0.33	0.68	147.87	56.23	204.10	4.000	No	No	2.00
924	60.65	231.31	25.70	2.03	0.32	0.68	147.96	57.46	205.42	4.000	No	No	2.00
925	60.71	229.62	26.47	2.04	0.32	0.68	146.94	58.84	205.78	4.000	No	No	2.00
926	60.77	227.36	27.28	2.05	0.32	0.68	145.41	60.08	205.49	4.000	No	No	2.00
927	60.83	226.32	27.50	2.06	0.33	0.68	144.59	60.34	204.94	4.000	No	No	2.00
928	60.89	228.02	26.92	2.05	0.33	0.68	145.70	59.47	205.17	4.000	No	No	2.00
929	60.98	234.14	25.29	2.03	0.32	0.68	149.95	56.95	206.90	4.000	No	No	2.00
930	61.04	237.81	24.32	2.02	0.32	0.68	152.45	55.25	207.71	4.000	No	No	2.00
931	61.10	240.54	23.78	2.01	0.32	0.68	154.41	54.34	208.75	4.000	No	No	2.00
932	61.16	241.86	23.77	2.01	0.32	0.68	155.53	54.51	210.04	4.000	No	No	2.00
933	61.22	242.14	23.86	2.01	0.32	0.68	156.33	54.84	211.18	4.000	No	No	2.00
934	61.31	242.19	23.85	2.01	0.32	0.68	156.31	54.82	211.13	4.000	No	No	2.00
935	61.37	241.77	24.05	2.01	0.32	0.68	156.05	55.24	211.29	4.000	No	No	2.00
936	61.43	242.24	24.10	2.01	0.31	0.68	156.47	55.44	211.91	4.000	No	No	2.00
937	61.49	242.80	24.11	2.01	0.31	0.68	156.94	55.55	212.49	4.000	No	No	2.00
938	61.55	243.18	24.11	2.01	0.31	0.68	157.24	55.58	212.82	4.000	No	No	2.00
939	61.64	244.31	23.74	2.01	0.31	0.68	157.90	54.82	212.72	4.000	No	No	2.00
940	61.70	245.82	23.21	2.00	0.31	0.68	158.78	53.67	212.45	4.000	No	No	2.00
941	61.76	248.08	22.46	1.99	0.31	0.68	160.12	51.98	212.11	4.000	No	No	2.00
942	61.82	250.24	20.33	1.97	0.32	0.68	159.97	46.09	206.06	4.000	No	No	2.00
943	61.88	252.50	16.14	1.91	0.35	0.66	156.48	31.96	188.44	4.000	No	No	2.00
944	61.94	254.29	16.50	1.92	0.34	0.66	158.46	33.45	191.91	4.000	No	No	2.00
945	62.04	255.43	16.60	1.92	0.34	0.66	159.51	33.93	193.44	4.000	No	No	2.00
946	62.10	256.55	16.56	1.92	0.34	0.66	160.39	33.85	194.24	4.000	No	No	2.00
947	62.16	260.70	15.83	1.91	0.34	0.66	162.99	31.46	194.45	4.000	No	No	2.00
948	62.22	260.93	15.79	1.91	0.34	0.66	163.09	31.32	194.41	4.000	No	No	2.00
949	62.29	261.17	15.31	1.90	0.34	0.66	162.58	29.51	192.09	4.000	No	No	2.00
950	62.34	266.73	13.80	1.88	0.35	0.66	165.16	23.88	189.04	4.000	No	No	2.00
951	62.43	269.65	13.12	1.88	0.35	0.65	166.60	21.33	187.93	4.000	No	No	2.00
952	62.49	270.12	13.05	1.88	0.35	0.65	166.85	21.05	187.90	4.000	No	No	2.00
953	62.55	270.59	13.09	1.88	0.35	0.65	167.28	21.24	188.52	4.000	No	No	2.00
954	62.61	271.53	13.25	1.88	0.35	0.66	168.30	21.94	190.25	4.000	No	No	2.00
955	62.67	272.47	13.06	1.88	0.35	0.66	168.78	21.22	190.01	4.000	No	No	2.00
956	62.73	271.44	12.86	1.87	0.35	0.65	167.51	20.33	187.83	4.000	No	No	2.00
957	62.82	270.21	12.87	1.87	0.35	0.65	166.38	20.32	186.70	4.000	No	No	2.00
958	62.88	269.37	12.97	1.87	0.35	0.65	165.76	20.66	186.42	4.000	No	No	2.00
959	62.94	268.80	12.87	1.87	0.35	0.65	165.07	20.25	185.32	4.000	No	No	2.00
960	63.00	268.80	12.73	1.87	0.35	0.65	164.79	19.67	184.46	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	63.06	268.24	12.78	1.87	0.35	0.65	164.33	19.82	184.15	4.000	No	No	2.00
962	63.12	266.17	13.18	1.88	0.35	0.65	163.12	21.33	184.45	4.000	No	No	2.00
963	63.21	264.38	13.34	1.88	0.35	0.65	161.74	21.84	183.58	4.000	No	No	2.00
964	63.27	262.59	13.39	1.88	0.36	0.65	160.23	21.96	182.19	4.000	No	No	2.00
965	63.33	259.95	13.41	1.88	0.36	0.64	157.94	21.87	179.82	4.000	No	No	2.00
966	63.40	254.02	13.99	1.89	0.36	0.64	153.70	23.80	177.50	4.000	No	No	2.00
967	63.46	246.77	14.76	1.90	0.37	0.64	148.61	26.28	174.90	4.000	No	No	2.00
968	63.55	229.44	17.72	1.93	0.37	0.64	137.71	35.31	173.02	4.000	No	No	2.00
969	63.60	214.00	21.41	1.98	0.37	0.64	128.43	44.52	172.96	4.000	No	No	2.00
970	63.66	196.28	26.85	2.05	0.37	0.63	117.53	54.10	171.63	4.000	No	No	2.00
971	63.73	179.05	32.23	2.12	0.38	0.63	106.07	59.70	165.77	4.000	No	No	2.00
972	63.78	164.36	37.13	2.18	0.39	0.62	96.08	62.67	158.74	4.000	No	No	2.00
973	63.87	141.86	47.59	2.31	0.41	0.60	81.06	66.26	147.32	4.000	No	No	2.00
974	63.94	128.77	55.58	2.41	0.42	0.60	72.45	67.51	139.97	4.000	No	No	2.00
975	63.99	114.64	64.94	2.52	0.44	0.58	63.13	67.80	130.93	4.000	No	No	2.00
976	64.05	97.69	73.41	2.63	0.46	0.57	52.35	0.00	52.35	4.000	No	Yes	2.00
977	64.12	81.21	80.64	2.72	0.48	0.55	42.26	0.00	42.26	4.000	No	Yes	2.00
978	64.18	69.25	89.68	2.83	0.50	0.54	35.28	0.00	35.28	4.000	No	Yes	2.00
979	64.27	64.36	93.36	2.88	0.51	0.53	32.52	0.00	32.52	4.000	No	Yes	2.00
980	64.33	61.54	95.67	2.91	0.51	0.53	30.89	0.00	30.89	4.000	No	Yes	2.00
981	64.39	55.80	100.00	2.97	0.52	0.53	27.69	0.00	27.69	4.000	No	Yes	2.00
982	64.44	55.70	100.00	2.98	0.52	0.53	27.63	0.00	27.63	4.000	No	Yes	2.00
983	64.51	66.73	92.00	2.86	0.50	0.54	33.80	0.00	33.80	4.000	No	Yes	2.00
984	64.57	83.69	79.92	2.71	0.48	0.55	43.64	0.00	43.64	4.000	No	Yes	2.00
985	64.63	109.78	65.11	2.53	0.45	0.58	59.70	66.86	126.57	4.000	No	No	2.00
986	64.72	147.54	46.81	2.30	0.40	0.61	84.75	66.80	151.54	4.000	No	No	2.00
987	64.79	162.88	40.77	2.22	0.39	0.62	95.23	65.50	160.73	4.000	No	No	2.00
988	64.85	173.81	36.45	2.17	0.38	0.63	102.64	63.54	166.18	4.000	No	No	2.00
989	64.91	181.72	33.85	2.14	0.37	0.63	108.06	62.05	170.11	4.000	No	No	2.00
990	64.96	187.37	33.22	2.13	0.37	0.63	112.30	62.24	174.54	4.000	No	No	2.00
991	65.05	196.13	33.34	2.13	0.35	0.64	119.33	63.91	183.24	4.000	No	No	2.00
992	65.11	203.28	32.96	2.12	0.35	0.65	125.02	64.69	189.71	4.000	No	No	2.00
993	65.18	210.34	31.64	2.11	0.34	0.66	130.36	64.08	194.44	4.000	No	No	2.00
994	65.23	219.10	29.25	2.08	0.33	0.66	136.64	61.80	198.44	4.000	No	No	2.00
995	65.29	228.71	26.78	2.05	0.33	0.66	143.47	58.78	202.26	4.000	No	No	2.00
996	65.38	243.21	23.47	2.01	0.32	0.67	154.25	53.57	207.82	4.000	No	No	2.00
997	65.44	251.12	21.68	1.98	0.32	0.67	159.66	49.85	209.51	4.000	No	No	2.00
998	65.50	257.62	20.29	1.97	0.32	0.67	164.03	46.53	210.57	4.000	No	No	2.00
999	65.56	262.42	19.47	1.96	0.32	0.68	167.39	44.46	211.85	4.000	No	No	2.00
1000	65.63	266.37	18.74	1.95	0.31	0.68	170.05	42.45	212.51	4.000	No	No	2.00
1001	65.69	269.20	18.25	1.94	0.31	0.68	171.96	41.05	213.01	4.000	No	No	2.00
1002	65.77	273.72	17.63	1.93	0.31	0.68	175.20	39.26	214.45	4.000	No	No	2.00
1003	65.83	277.30	17.25	1.93	0.31	0.68	177.91	38.19	216.09	4.000	No	No	2.00
1004	65.89	283.32	16.31	1.92	0.31	0.68	182.01	35.09	217.10	4.000	No	No	2.00
1005	65.95	290.57	15.03	1.90	0.31	0.68	186.61	30.45	217.06	4.000	No	No	2.00
1006	66.01	296.22	14.07	1.89	0.31	0.68	190.17	26.78	216.95	4.000	No	No	2.00
1007	66.10	301.88	13.01	1.88	0.31	0.68	193.44	22.51	215.95	4.000	No	No	2.00
1008	66.16	303.76	13.31	1.88	0.31	0.68	195.74	23.95	219.69	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1009	66.23	303.76	9.72	1.83	0.33	0.66	189.11	9.23	198.34	4.000	No	No	2.00
1010	66.29	301.03	6.46	1.79	0.35	0.64	182.87	1.26	184.13	4.000	No	No	2.00
1011	66.35	297.07	7.84	1.81	0.35	0.64	180.40	3.62	184.02	4.000	No	No	2.00
1012	66.41	292.83	9.10	1.83	0.35	0.64	178.12	6.94	185.06	4.000	No	No	2.00
1013	66.47	288.32	10.49	1.84	0.35	0.65	176.18	11.59	187.77	4.000	No	No	2.00
1014	66.54	261.10	16.63	1.92	0.34	0.66	161.84	34.26	196.09	4.000	No	No	2.00
1015	66.62	262.23	16.38	1.92	0.34	0.66	162.43	33.42	195.85	4.000	No	No	2.00
1016	66.69	253.47	18.13	1.94	0.34	0.65	156.40	38.80	195.20	4.000	No	No	2.00
1017	66.75	244.53	20.49	1.97	0.34	0.65	151.22	45.33	196.55	4.000	No	No	2.00
1018	66.81	233.32	24.11	2.01	0.33	0.66	144.69	53.48	198.17	4.000	No	No	2.00
1019	66.86	222.95	27.65	2.06	0.34	0.66	138.11	59.38	197.49	4.000	No	No	2.00
1020	66.95	209.30	32.55	2.12	0.34	0.65	128.86	64.99	193.84	4.000	No	No	2.00
1021	67.01	202.42	35.04	2.15	0.34	0.65	124.00	66.93	190.93	4.000	No	No	2.00
1022	67.07	196.40	36.85	2.17	0.35	0.64	119.57	67.85	187.42	4.000	No	No	2.00
1023	67.13	191.69	38.04	2.19	0.35	0.64	116.04	68.18	184.21	4.000	No	No	2.00
1024	67.19	186.89	39.27	2.20	0.36	0.64	112.45	68.44	180.89	4.000	No	No	2.00
1025	67.28	179.64	41.24	2.23	0.36	0.63	107.09	68.75	175.84	4.000	No	No	2.00
1026	67.34	174.55	42.90	2.25	0.37	0.63	103.40	69.07	172.47	4.000	No	No	2.00
1027	67.40	170.22	44.37	2.27	0.37	0.62	100.27	69.29	169.56	4.000	No	No	2.00
1028	67.46	166.83	45.59	2.28	0.38	0.62	97.83	69.44	167.28	4.000	No	No	2.00
1029	67.52	164.48	46.46	2.29	0.38	0.62	96.15	69.54	165.68	4.000	No	No	2.00
1030	67.61	167.07	45.63	2.28	0.38	0.62	97.96	69.50	167.46	4.000	No	No	2.00
1031	67.67	165.04	46.38	2.29	0.38	0.62	96.50	69.58	166.08	4.000	No	No	2.00
1032	67.73	167.30	45.59	2.28	0.38	0.62	98.08	69.51	167.58	4.000	No	No	2.00
1033	67.79	171.91	44.15	2.26	0.37	0.62	101.36	69.42	170.79	4.000	No	No	2.00
1034	67.85	177.85	42.03	2.24	0.37	0.63	105.58	68.99	174.56	4.000	No	No	2.00
1035	67.94	187.64	37.42	2.18	0.36	0.63	112.23	66.70	178.93	4.000	No	No	2.00
1036	68.00	193.57	34.73	2.15	0.36	0.64	116.18	64.83	181.01	4.000	No	No	2.00
1037	68.06	197.72	32.84	2.12	0.36	0.64	118.86	63.20	182.06	4.000	No	No	2.00
1038	68.12	200.45	27.74	2.06	0.37	0.63	118.89	55.87	174.76	4.000	No	No	2.00
1039	68.18	202.42	19.84	1.96	0.40	0.60	115.29	38.64	153.93	4.000	No	No	2.00
1040	68.24	204.87	20.90	1.97	0.39	0.61	118.03	41.73	159.76	4.000	No	No	2.00
1041	68.33	208.73	22.24	1.99	0.38	0.62	122.05	45.57	167.62	4.000	No	No	2.00
1042	68.39	212.22	21.53	1.98	0.38	0.62	124.26	44.19	168.45	4.000	No	No	2.00
1043	68.45	215.61	20.79	1.97	0.38	0.62	126.33	42.63	168.96	4.000	No	No	2.00
1044	68.51	215.56	21.78	1.98	0.37	0.62	127.08	45.23	172.30	4.000	No	No	2.00
1045	68.59	215.51	23.18	2.00	0.36	0.63	128.05	48.65	176.70	4.000	No	No	2.00
1046	68.65	219.47	23.24	2.00	0.36	0.63	131.31	49.32	180.62	4.000	No	No	2.00
1047	68.70	223.71	23.74	2.01	0.35	0.64	135.15	51.06	186.21	4.000	No	No	2.00
1048	68.80	232.28	23.93	2.01	0.34	0.65	142.45	52.70	195.15	4.000	No	No	2.00
1049	68.86	236.98	23.82	2.01	0.33	0.65	146.36	53.11	199.47	4.000	No	No	2.00
1050	68.92	240.47	24.05	2.01	0.32	0.66	150.09	54.25	204.33	4.000	No	No	2.00
1051	68.97	243.39	24.50	2.02	0.32	0.67	153.00	55.76	208.76	4.000	No	No	2.00
1052	69.04	245.18	25.19	2.03	0.31	0.67	155.09	57.64	212.74	4.000	No	No	2.00
1053	69.10	246.31	25.78	2.03	0.31	0.67	156.52	59.17	215.70	4.000	No	No	2.00
1054	69.19	250.07	25.88	2.04	0.30	0.68	159.94	59.98	219.92	4.000	No	No	2.00
1055	69.25	253.93	25.58	2.03	0.30	0.68	163.20	59.93	223.12	4.000	No	No	2.00
1056	69.31	257.04	25.42	2.03	0.30	0.68	165.89	60.05	225.94	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1057	69.36	259.30	25.37	2.03	0.29	0.69	167.90	60.29	228.19	4.000	No	No	2.00
1058	69.42	262.31	25.26	2.03	0.29	0.69	170.57	60.52	231.08	4.000	No	No	2.00
1059	69.51	265.80	25.59	2.03	0.29	0.69	174.07	61.88	235.94	4.000	No	No	2.00
1060	69.57	268.91	25.53	2.03	0.28	0.70	176.92	62.25	239.17	4.000	No	No	2.00
1061	69.63	271.54	25.83	2.04	0.28	0.70	179.65	63.42	243.07	4.000	No	No	2.00
1062	69.69	274.65	21.89	1.99	0.29	0.69	178.68	53.28	231.96	4.000	No	No	2.00
1063	69.75	277.19	15.71	1.91	0.32	0.66	172.55	31.89	204.44	4.000	No	No	2.00
1064	69.84	277.39	17.27	1.93	0.31	0.67	175.08	37.94	213.02	4.000	No	No	2.00
1065	69.89	264.02	20.72	1.97	0.31	0.67	167.34	48.26	215.59	4.000	No	No	2.00
1066	69.96	273.61	18.88	1.95	0.31	0.67	173.81	43.38	217.19	4.000	No	No	2.00
1067	70.02	271.59	19.16	1.95	0.31	0.67	172.29	44.10	216.39	4.000	No	No	2.00
1068	70.08	258.36	21.64	1.98	0.31	0.67	163.08	50.26	213.34	4.000	No	No	2.00
1069	70.15	269.57	17.95	1.94	0.32	0.66	168.71	39.62	208.34	4.000	No	No	2.00
1070	70.21	280.58	13.60	1.88	0.34	0.65	171.70	23.54	195.24	4.000	No	No	2.00
1071	70.28	300.08	7.71	1.81	0.35	0.63	179.58	3.33	182.91	4.000	No	No	2.00
1072	70.35	323.99	1.73	1.73	0.33	0.65	199.60	0.00	199.60	4.000	No	No	2.00
1073	70.41	353.19	0.00	1.64	0.30	0.68	227.61	0.00	227.61	4.000	No	No	2.00
1074	70.48	375.97	0.00	1.58	0.27	0.71	250.67	0.00	250.67	4.000	No	No	2.00
1075	70.55	388.87	0.00	1.56	0.26	0.71	261.27	0.00	261.27	4.000	No	No	2.00
1076	70.61	392.74	0.00	1.55	0.26	0.71	263.83	0.00	263.83	4.000	No	No	2.00
1077	70.68	390.01	0.00	1.56	0.26	0.71	261.95	0.00	261.95	4.000	No	No	2.00
1078	70.74	380.32	0.00	1.58	0.27	0.71	254.95	0.00	254.95	4.000	No	No	2.00
1079	70.81	374.20	0.00	1.60	0.27	0.70	248.52	0.00	248.52	4.000	No	No	2.00
1080	70.88	373.82	0.00	1.61	0.27	0.70	248.05	0.00	248.05	4.000	No	No	2.00
1081	70.95	375.23	0.00	1.61	0.27	0.70	249.45	0.00	249.45	4.000	No	No	2.00
1082	71.00	377.87	0.00	1.60	0.27	0.71	252.14	0.00	252.14	4.000	No	No	2.00
1083	71.08	387.19	0.00	1.58	0.26	0.71	259.81	0.00	259.81	4.000	No	No	2.00
1084	71.14	396.14	0.00	1.55	0.26	0.71	265.79	0.00	265.79	4.000	No	No	2.00
1085	71.20	404.52	0.00	1.53	0.26	0.71	271.37	0.00	271.37	4.000	No	No	2.00
1086	71.29	411.49	0.00	1.45	0.26	0.71	275.99	0.00	275.99	4.000	No	No	2.00
1087	71.35	415.44	0.00	1.42	0.26	0.71	278.60	0.00	278.60	4.000	No	No	2.00
1088	71.41	415.72	0.00	1.43	0.26	0.71	278.75	0.00	278.75	4.000	No	No	2.00
1089	71.47	413.56	0.00	1.45	0.26	0.71	277.27	0.00	277.27	4.000	No	No	2.00
1090	71.53	409.79	0.00	1.48	0.26	0.71	274.70	0.00	274.70	4.000	No	No	2.00
1091	71.59	404.52	0.00	1.52	0.26	0.71	271.13	0.00	271.13	4.000	No	No	2.00
1092	71.66	362.52	0.00	1.60	0.29	0.69	235.78	0.00	235.78	4.000	No	No	2.00
1093	71.72	380.22	0.00	1.57	0.27	0.71	253.93	0.00	253.93	4.000	No	No	2.00
1094	71.79	382.49	0.00	1.57	0.26	0.71	256.23	0.00	256.23	4.000	No	No	2.00
1095	71.86	381.46	0.00	1.57	0.27	0.71	255.08	0.00	255.08	4.000	No	No	2.00
1096	71.92	375.52	0.00	1.59	0.27	0.70	248.83	0.00	248.83	4.000	No	No	2.00
1097	71.98	372.70	0.00	1.59	0.28	0.70	245.86	0.00	245.86	4.000	No	No	2.00
1098	72.06	370.24	0.00	1.60	0.28	0.70	243.26	0.00	243.26	4.000	No	No	2.00
1099	72.13	367.24	0.00	1.60	0.28	0.69	240.12	0.00	240.12	4.000	No	No	2.00
1100	72.19	365.34	0.00	1.61	0.28	0.69	238.14	0.00	238.14	4.000	No	No	2.00
1101	72.26	364.03	0.00	1.62	0.29	0.69	236.74	0.00	236.74	4.000	No	No	2.00
1102	72.32	364.03	0.00	1.63	0.29	0.69	236.68	0.00	236.68	4.000	No	No	2.00
1103	72.38	364.03	0.00	1.64	0.29	0.69	236.63	0.00	236.63	4.000	No	No	2.00
1104	72.45	366.20	0.00	1.63	0.28	0.69	238.76	0.00	238.76	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1105	72.51	368.65	0.00	1.63	0.28	0.69	241.21	0.00	241.21	4.000	No	No	2.00
1106	72.58	371.76	0.00	1.62	0.28	0.70	244.33	0.00	244.33	4.000	No	No	2.00
1107	72.65	374.86	0.00	1.62	0.27	0.70	247.46	0.00	247.46	4.000	No	No	2.00
1108	72.72	376.94	0.00	1.62	0.27	0.70	249.55	0.00	249.55	4.000	No	No	2.00
1109	72.77	377.78	0.00	1.62	0.27	0.70	250.38	0.00	250.38	4.000	No	No	2.00
1110	72.84	378.35	0.00	1.61	0.27	0.70	250.90	0.00	250.90	4.000	No	No	2.00
1111	72.92	378.73	0.00	1.60	0.27	0.70	251.23	0.00	251.23	4.000	No	No	2.00
1112	72.98	377.22	0.00	1.55	0.27	0.70	249.60	0.00	249.60	4.000	No	No	2.00
1113	73.04	373.54	0.00	1.51	0.28	0.70	245.74	0.00	245.74	4.000	No	No	2.00
1114	73.11	365.53	0.00	1.54	0.29	0.69	237.48	0.00	237.48	4.000	No	No	2.00
1115	73.17	359.22	0.00	1.56	0.29	0.68	231.07	0.00	231.07	4.000	No	No	2.00
1116	73.24	355.47	0.00	1.58	0.30	0.68	227.26	0.00	227.26	4.000	No	No	2.00
1117	73.30	352.08	0.00	1.59	0.30	0.67	223.86	0.00	223.86	4.000	No	No	2.00
1118	73.37	333.05	0.00	1.63	0.32	0.65	205.42	0.00	205.42	4.000	No	No	2.00
1119	73.44	340.78	0.00	1.61	0.31	0.66	212.73	0.00	212.73	4.000	No	No	2.00
1120	73.49	339.55	0.00	1.62	0.32	0.66	211.50	0.00	211.50	4.000	No	No	2.00
1121	73.57	339.60	0.00	1.63	0.32	0.66	211.48	0.00	211.48	4.000	No	No	2.00
1122	73.63	339.17	0.00	1.63	0.32	0.66	211.02	0.00	211.02	4.000	No	No	2.00
1123	73.70	339.65	0.00	1.64	0.32	0.66	211.42	0.00	211.42	4.000	No	No	2.00
1124	73.77	342.38	0.00	1.62	0.31	0.66	213.98	0.00	213.98	4.000	No	No	2.00
1125	73.83	346.13	0.00	1.62	0.31	0.67	217.57	0.00	217.57	4.000	No	No	2.00
1126	73.89	347.93	0.00	1.61	0.31	0.67	219.26	0.00	219.26	4.000	No	No	2.00
1127	73.95	351.42	0.00	1.60	0.30	0.67	222.62	0.00	222.62	4.000	No	No	2.00
1128	74.04	358.48	0.00	1.58	0.29	0.68	229.54	0.00	229.54	4.000	No	No	2.00
1129	74.10	361.02	0.00	1.56	0.29	0.68	232.03	0.00	232.03	4.000	No	No	2.00
1130	74.16	361.87	0.00	1.56	0.29	0.68	232.83	0.00	232.83	4.000	No	No	2.00
1131	74.22	361.96	0.00	1.54	0.29	0.68	232.87	0.00	232.87	4.000	No	No	2.00
1132	74.28	363.56	0.00	1.48	0.29	0.68	234.43	0.00	234.43	4.000	No	No	2.00
1133	74.37	362.43	0.00	1.48	0.29	0.68	233.21	0.00	233.21	4.000	No	No	2.00
1134	74.43	358.95	0.00	1.50	0.29	0.68	229.67	0.00	229.67	4.000	No	No	2.00
1135	74.49	354.15	0.00	1.52	0.30	0.67	224.84	0.00	224.84	4.000	No	No	2.00
1136	74.55	347.84	0.00	1.55	0.31	0.67	218.60	0.00	218.60	4.000	No	No	2.00
1137	74.62	306.88	0.00	1.65	0.36	0.62	180.37	0.00	180.37	4.000	No	No	2.00
1138	74.67	330.42	0.00	1.60	0.33	0.65	201.83	0.00	201.83	4.000	No	No	2.00
1139	74.75	329.38	0.00	1.59	0.33	0.65	200.79	0.00	200.79	4.000	No	No	2.00
1140	74.82	332.22	0.00	1.60	0.33	0.65	203.39	0.00	203.39	4.000	No	No	2.00
1141	74.88	336.92	0.00	1.60	0.32	0.65	207.80	0.00	207.80	4.000	No	No	2.00
1142	74.94	337.39	0.00	1.60	0.32	0.65	208.19	0.00	208.19	4.000	No	No	2.00
1143	75.00	340.96	0.00	1.60	0.32	0.66	211.56	0.00	211.56	4.000	No	No	2.00
1144	75.07	347.56	0.00	1.60	0.31	0.66	217.88	0.00	217.88	4.000	No	No	2.00
1145	75.14	357.55	100.00	4.06	0.26	0.70	237.79	0.00	237.79	4.000	No	Yes	2.00
1146	75.21	364.61	100.00	4.06	0.26	0.70	242.47	0.00	242.47	4.000	No	Yes	2.00
1147	75.28	368.37	100.00	4.06	0.26	0.70	244.96	0.00	244.96	4.000	No	Yes	2.00
1148	75.33	370.07	100.00	4.06	0.26	0.70	246.08	0.00	246.08	4.000	No	Yes	2.00
1149	75.41	362.82	100.00	4.06	0.26	0.70	241.24	0.00	241.24	4.000	No	Yes	2.00
1150	75.48	353.59	100.00	4.06	0.26	0.70	235.09	0.00	235.09	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
$CRR_{7.5}$:	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.07	2.00	0.00	0.00	0.00	0.00	0.14	2.00	0.00	0.00	0.00	0.00
0.21	2.00	0.00	0.00	0.00	0.00	0.28	2.00	0.00	0.00	0.00	0.00
0.33	2.00	0.00	0.00	0.00	0.00	0.40	2.00	0.00	0.00	0.00	0.00
0.47	2.00	0.00	0.00	0.00	0.00	0.53	2.00	0.00	0.00	0.00	0.00
0.59	2.00	0.00	0.00	0.00	0.00	0.67	2.00	0.00	0.00	0.00	0.00
0.73	2.00	0.00	0.00	0.00	0.00	0.81	2.00	0.00	0.00	0.00	0.00
0.87	2.00	0.00	0.00	0.00	0.00	0.93	2.00	0.00	0.00	0.00	0.00
1.00	2.00	0.00	0.00	0.00	0.00	1.06	2.00	0.00	0.00	0.00	0.00
1.13	2.00	0.00	0.00	0.00	0.00	1.19	2.00	0.00	0.00	0.00	0.00
1.26	2.00	0.00	0.00	0.00	0.00	1.33	2.00	0.00	0.00	0.00	0.00
1.39	2.00	0.00	0.00	0.00	0.00	1.45	2.00	0.00	0.00	0.00	0.00
1.51	2.00	0.00	0.00	0.00	0.00	1.59	2.00	0.00	0.00	0.00	0.00
1.64	2.00	0.00	0.00	0.00	0.00	1.72	2.00	0.00	0.00	0.00	0.00
1.77	2.00	0.00	0.00	0.00	0.00	1.84	2.00	0.00	0.00	0.00	0.00
1.92	2.00	0.00	0.00	0.00	0.00	1.97	2.00	0.00	0.00	0.00	0.00
2.05	2.00	0.00	0.00	0.00	0.00	2.10	2.00	0.00	0.00	0.00	0.00
2.18	2.00	0.00	0.00	0.00	0.00	2.24	2.00	0.00	0.00	0.00	0.00
2.30	2.00	0.00	0.00	0.00	0.00	2.38	2.00	0.00	0.00	0.00	0.00
2.44	2.00	0.00	0.00	0.00	0.00	2.50	2.00	0.00	0.00	0.00	0.00
2.58	2.00	0.00	0.00	0.00	0.00	2.64	2.00	0.00	0.00	0.00	0.00
2.69	2.00	0.00	0.00	0.00	0.00	2.77	2.00	0.00	0.00	0.00	0.00
2.83	2.00	0.00	0.00	0.00	0.00	2.89	2.00	0.00	0.00	0.00	0.00
2.97	2.00	0.00	0.00	0.00	0.00	3.03	2.00	0.00	0.00	0.00	0.00
3.08	2.00	0.00	0.00	0.00	0.00	3.16	2.00	0.00	0.00	0.00	0.00
3.22	2.00	0.00	0.00	0.00	0.00	3.29	2.00	0.00	0.00	0.00	0.00
3.36	2.00	0.00	0.00	0.00	0.00	3.42	2.00	0.00	0.00	0.00	0.00
3.48	2.00	0.00	0.00	0.00	0.00	3.55	2.00	0.00	0.00	0.00	0.00
3.62	2.00	0.00	0.00	0.00	0.00	3.69	2.00	0.00	0.00	0.00	0.00
3.75	2.00	0.00	0.00	0.00	0.00	3.81	2.00	0.00	0.00	0.00	0.00
3.89	2.00	0.00	0.00	0.00	0.00	3.95	2.00	0.00	0.00	0.00	0.00
4.00	2.00	0.00	0.00	0.00	0.00	4.08	2.00	0.00	0.00	0.00	0.00
4.14	2.00	0.00	0.00	0.00	0.00	4.20	2.00	0.00	0.00	0.00	0.00
4.28	2.00	0.00	0.00	0.00	0.00	4.33	2.00	0.00	0.00	0.00	0.00
4.41	2.00	0.00	0.00	0.00	0.00	4.47	2.00	0.00	0.00	0.00	0.00
4.53	2.00	0.00	0.00	0.00	0.00	4.61	2.00	0.00	0.00	0.00	0.00
4.67	2.00	0.00	0.00	0.00	0.00	4.74	2.00	0.00	0.00	0.00	0.00
4.80	2.00	0.00	0.00	0.00	0.00	4.86	2.00	0.00	0.00	0.00	0.00
4.94	2.00	0.00	0.00	0.00	0.00	5.00	2.00	0.00	0.00	0.00	0.00
5.05	2.00	0.00	0.00	0.06	0.00	5.13	2.00	0.00	0.00	0.08	0.00
5.19	2.00	0.00	0.00	0.06	0.00	5.25	2.00	0.00	0.00	0.06	0.00
5.33	2.00	0.00	0.00	0.08	0.00	5.39	2.00	0.00	0.00	0.06	0.00
5.45	2.00	0.00	0.00	0.06	0.00	5.53	2.00	0.00	0.00	0.08	0.00
5.59	2.00	0.00	0.00	0.06	0.00	5.65	2.00	0.00	0.00	0.06	0.00
5.72	2.00	0.00	0.00	0.08	0.00	5.78	2.00	0.00	0.00	0.06	0.00
5.86	2.00	0.00	0.00	0.08	0.00	5.92	2.00	0.00	0.00	0.06	0.00
5.98	2.00	0.00	0.00	0.06	0.00	6.04	2.00	0.00	0.00	0.06	0.00
6.12	2.00	0.00	0.00	0.08	0.00	6.18	2.00	0.00	0.00	0.06	0.00
6.24	2.00	0.00	0.00	0.06	0.00	6.31	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
6.37	2.00	0.00	0.00	0.06	0.00	6.43	2.00	0.00	0.00	0.06	0.00
6.51	2.00	0.00	0.00	0.08	0.00	6.57	2.00	0.00	0.00	0.06	0.00
6.65	2.00	0.00	0.00	0.08	0.00	6.71	2.00	0.00	0.00	0.06	0.00
6.77	2.00	0.00	0.00	0.06	0.00	6.83	2.00	0.00	0.00	0.06	0.00
6.90	2.00	0.00	0.00	0.08	0.00	6.96	2.00	0.00	0.00	0.06	0.00
7.03	2.00	0.00	0.00	0.07	0.00	7.09	2.00	0.00	0.00	0.06	0.00
7.17	2.00	0.00	0.00	0.08	0.00	7.22	2.00	0.00	0.00	0.06	0.00
7.28	2.00	0.00	0.00	0.06	0.00	7.36	2.00	0.00	0.00	0.08	0.00
7.42	2.00	0.00	0.00	0.06	0.00	7.50	2.00	0.00	0.00	0.08	0.00
7.55	2.00	0.00	0.00	0.06	0.00	7.61	2.00	0.00	0.00	0.06	0.00
7.70	2.00	0.00	0.00	0.08	0.00	7.75	2.00	0.00	0.00	0.06	0.00
7.81	2.00	0.00	0.00	0.06	0.00	7.89	2.00	0.00	0.00	0.08	0.00
7.95	2.00	0.00	0.00	0.06	0.00	8.01	0.50	0.50	0.48	0.06	0.08
8.08	0.53	0.47	0.51	0.08	0.10	8.14	0.54	0.46	0.53	0.06	0.07
8.22	0.57	0.43	0.57	0.08	0.09	8.28	0.60	0.40	0.63	0.06	0.06
8.34	0.63	0.37	0.70	0.06	0.06	8.40	0.64	0.36	0.73	0.06	0.06
8.48	0.62	0.38	0.68	0.08	0.08	8.54	0.59	0.41	0.60	0.06	0.07
8.60	0.55	0.45	0.54	0.06	0.07	8.68	0.50	0.50	0.48	0.08	0.11
8.74	0.48	0.52	0.46	0.06	0.08	8.79	0.46	0.54	0.44	0.06	0.08
8.87	0.45	0.55	0.43	0.08	0.11	8.93	0.44	0.56	0.42	0.06	0.09
8.99	0.44	0.56	0.41	0.06	0.09	9.07	0.43	0.57	0.41	0.08	0.11
9.13	0.43	0.57	0.41	0.06	0.09	9.19	0.43	0.57	0.41	0.06	0.09
9.27	0.42	0.58	0.40	0.08	0.12	9.33	0.41	0.59	0.40	0.06	0.09
9.39	0.40	0.60	0.38	0.06	0.09	9.46	0.37	0.63	0.37	0.08	0.13
9.52	0.35	0.65	0.35	0.06	0.10	9.58	0.34	0.66	0.34	0.06	0.10
9.66	0.33	0.67	0.34	0.08	0.14	9.72	0.31	0.69	0.33	0.06	0.11
9.78	0.30	0.70	0.32	0.06	0.10	9.86	0.29	0.71	0.32	0.08	0.14
9.91	0.29	0.71	0.32	0.06	0.10	9.97	0.29	0.71	0.32	0.06	0.11
10.04	0.27	0.73	0.31	0.07	0.12	10.12	0.29	0.71	0.32	0.08	0.14
10.18	0.28	0.72	0.31	0.06	0.11	10.25	0.27	0.73	0.31	0.08	0.14
10.31	0.26	0.74	0.30	0.06	0.11	10.37	0.26	0.74	0.30	0.06	0.11
10.45	0.25	0.75	0.30	0.08	0.15	10.50	0.25	0.75	0.30	0.06	0.11
10.58	0.24	0.76	0.30	0.08	0.15	10.64	0.24	0.76	0.29	0.06	0.11
10.70	0.24	0.76	0.30	0.06	0.11	10.78	0.25	0.75	0.30	0.08	0.15
10.84	0.25	0.75	0.30	0.06	0.11	10.90	0.26	0.74	0.30	0.07	0.12
10.98	0.27	0.73	0.31	0.08	0.15	11.04	0.27	0.73	0.31	0.06	0.11
11.10	0.28	0.72	0.31	0.06	0.11	11.16	0.28	0.72	0.31	0.06	0.11
11.22	0.29	0.71	0.32	0.06	0.11	11.31	0.28	0.72	0.31	0.09	0.16
11.37	0.28	0.72	0.31	0.06	0.11	11.43	0.28	0.72	0.31	0.06	0.11
11.49	0.28	0.72	0.31	0.06	0.11	11.55	0.28	0.72	0.31	0.06	0.11
11.64	0.28	0.72	0.31	0.09	0.16	11.70	0.28	0.72	0.31	0.06	0.11
11.77	0.28	0.72	0.31	0.06	0.11	11.82	0.29	0.71	0.31	0.06	0.11
11.88	0.29	0.71	0.32	0.06	0.11	11.94	0.29	0.71	0.31	0.06	0.11
12.03	0.27	0.73	0.31	0.09	0.16	12.09	0.26	0.74	0.30	0.06	0.11
12.15	0.26	0.74	0.30	0.06	0.11	12.21	0.26	0.74	0.30	0.06	0.11
12.28	0.26	0.74	0.30	0.06	0.11	12.34	0.26	0.74	0.30	0.06	0.11
12.42	0.23	0.77	0.29	0.08	0.16	12.48	0.24	0.76	0.29	0.06	0.11
12.54	0.23	0.77	0.29	0.06	0.11	12.60	0.22	0.78	0.29	0.06	0.11

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
12.69	0.21	0.79	0.28	0.09	0.18	12.75	0.21	0.79	0.28	0.06	0.12
12.81	0.20	0.80	0.28	0.06	0.12	12.87	0.20	0.80	0.28	0.06	0.11
12.93	2.00	0.00	0.00	0.06	0.00	13.02	2.00	0.00	0.00	0.09	0.00
13.08	0.21	0.79	0.28	0.06	0.11	13.14	0.21	0.79	0.28	0.06	0.12
13.20	0.21	0.79	0.28	0.06	0.12	13.26	0.21	0.79	0.28	0.06	0.11
13.35	0.22	0.78	0.28	0.09	0.18	13.41	0.22	0.78	0.29	0.06	0.11
13.47	0.23	0.77	0.29	0.06	0.12	13.53	0.23	0.77	0.29	0.06	0.11
13.59	0.24	0.76	0.29	0.06	0.11	13.65	0.24	0.76	0.29	0.06	0.11
13.74	0.25	0.75	0.30	0.09	0.16	13.80	0.25	0.75	0.30	0.06	0.11
13.86	0.25	0.75	0.30	0.06	0.11	13.92	0.25	0.75	0.30	0.06	0.11
13.98	0.26	0.74	0.30	0.06	0.11	14.07	0.27	0.73	0.31	0.09	0.16
14.13	0.27	0.73	0.31	0.06	0.11	14.19	0.28	0.72	0.31	0.06	0.11
14.25	0.28	0.72	0.31	0.06	0.10	14.31	0.28	0.72	0.31	0.06	0.10
14.37	0.28	0.72	0.31	0.06	0.10	14.46	0.29	0.71	0.32	0.09	0.15
14.52	0.30	0.70	0.32	0.06	0.10	14.58	0.30	0.70	0.32	0.06	0.10
14.64	0.31	0.69	0.33	0.06	0.10	14.70	0.32	0.68	0.33	0.06	0.10
14.79	0.33	0.67	0.34	0.09	0.14	14.85	0.31	0.69	0.33	0.06	0.10
14.91	0.29	0.71	0.31	0.06	0.10	14.97	0.29	0.71	0.32	0.06	0.10
15.03	0.30	0.70	0.32	0.06	0.10	15.09	0.31	0.69	0.33	0.06	0.10
15.18	0.32	0.68	0.33	0.08	0.13	15.23	0.32	0.68	0.33	0.06	0.09
15.29	0.33	0.67	0.34	0.06	0.09	15.38	0.34	0.66	0.34	0.08	0.13
15.44	0.35	0.65	0.35	0.06	0.09	15.50	0.36	0.64	0.36	0.06	0.09
15.56	0.36	0.64	0.36	0.06	0.09	15.62	0.36	0.64	0.36	0.06	0.09
15.71	0.36	0.64	0.35	0.09	0.13	15.77	0.35	0.65	0.35	0.06	0.09
15.83	0.35	0.65	0.35	0.06	0.09	15.89	0.34	0.66	0.35	0.06	0.09
15.95	0.34	0.66	0.34	0.06	0.09	16.04	0.33	0.67	0.34	0.09	0.14
16.10	0.33	0.67	0.34	0.06	0.10	16.16	0.33	0.67	0.34	0.06	0.09
16.22	0.32	0.68	0.33	0.06	0.09	16.28	0.31	0.69	0.33	0.06	0.09
16.34	0.30	0.70	0.32	0.06	0.10	16.43	0.28	0.72	0.31	0.09	0.15
16.49	0.27	0.73	0.31	0.06	0.10	16.55	0.25	0.75	0.30	0.06	0.10
16.61	0.24	0.76	0.29	0.06	0.10	16.67	0.23	0.77	0.29	0.06	0.10
16.76	0.21	0.79	0.28	0.09	0.16	16.82	0.20	0.80	0.28	0.06	0.11
16.88	0.19	0.81	0.27	0.06	0.11	16.94	0.18	0.82	0.27	0.06	0.11
17.00	2.00	0.00	0.00	0.06	0.00	17.09	2.00	0.00	0.00	0.09	0.00
17.15	2.00	0.00	0.00	0.06	0.00	17.21	2.00	0.00	0.00	0.06	0.00
17.27	2.00	0.00	0.00	0.06	0.00	17.34	2.00	0.00	0.00	0.06	0.00
17.39	2.00	0.00	0.00	0.06	0.00	17.46	2.00	0.00	0.00	0.06	0.00
17.52	2.00	0.00	0.00	0.07	0.00	17.60	0.19	0.81	0.27	0.08	0.14
17.66	0.20	0.80	0.28	0.07	0.12	17.72	0.22	0.78	0.29	0.06	0.10
17.81	0.28	0.72	0.31	0.09	0.14	17.87	0.32	0.68	0.33	0.06	0.09
17.93	0.36	0.64	0.36	0.06	0.09	17.99	0.38	0.62	0.37	0.06	0.08
18.05	0.39	0.61	0.38	0.06	0.09	18.12	0.41	0.59	0.39	0.06	0.08
18.18	0.42	0.58	0.40	0.06	0.08	18.27	0.44	0.56	0.42	0.09	0.11
18.33	0.46	0.54	0.43	0.06	0.07	18.39	0.47	0.53	0.44	0.06	0.07
18.45	0.47	0.53	0.45	0.06	0.07	18.51	0.48	0.52	0.46	0.06	0.07
18.60	0.50	0.50	0.47	0.09	0.10	18.66	0.50	0.50	0.48	0.06	0.06
18.72	0.51	0.49	0.49	0.06	0.06	18.78	0.50	0.50	0.48	0.06	0.06
18.84	0.50	0.50	0.48	0.06	0.07	18.90	0.49	0.51	0.47	0.06	0.07

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
18.99	0.47	0.53	0.44	0.09	0.10	19.05	0.46	0.54	0.43	0.06	0.07
19.11	0.44	0.56	0.42	0.06	0.07	19.17	0.43	0.57	0.41	0.06	0.08
19.23	0.42	0.58	0.40	0.06	0.08	19.32	0.40	0.60	0.38	0.09	0.12
19.38	0.38	0.62	0.37	0.06	0.08	19.44	0.36	0.64	0.36	0.06	0.08
19.50	0.30	0.70	0.32	0.06	0.09	19.56	0.24	0.76	0.29	0.06	0.10
19.65	0.21	0.79	0.28	0.09	0.16	19.71	0.19	0.81	0.27	0.06	0.10
19.77	0.17	0.83	0.27	0.06	0.11	19.83	2.00	0.00	0.00	0.06	0.00
19.89	2.00	0.00	0.00	0.06	0.00	19.95	2.00	0.00	0.00	0.06	0.00
20.01	2.00	0.00	0.00	0.06	0.00	20.09	2.00	0.00	0.00	0.08	0.00
20.15	2.00	0.00	0.00	0.06	0.00	20.21	2.00	0.00	0.00	0.07	0.00
20.30	2.00	0.00	0.00	0.09	0.00	20.36	2.00	0.00	0.00	0.06	0.00
20.42	2.00	0.00	0.00	0.06	0.00	20.48	2.00	0.00	0.00	0.06	0.00
20.54	2.00	0.00	0.00	0.06	0.00	20.63	2.00	0.00	0.00	0.09	0.00
20.69	2.00	0.00	0.00	0.06	0.00	20.75	2.00	0.00	0.00	0.06	0.00
20.81	2.00	0.00	0.00	0.06	0.00	20.87	2.00	0.00	0.00	0.06	0.00
20.93	2.00	0.00	0.00	0.06	0.00	21.02	2.00	0.00	0.00	0.09	0.00
21.08	2.00	0.00	0.00	0.06	0.00	21.14	2.00	0.00	0.00	0.06	0.00
21.20	2.00	0.00	0.00	0.06	0.00	21.26	0.15	0.85	0.26	0.06	0.11
21.35	0.16	0.84	0.26	0.09	0.16	21.41	0.16	0.84	0.26	0.06	0.10
21.47	0.16	0.84	0.26	0.06	0.10	21.53	0.16	0.84	0.26	0.06	0.10
21.59	2.00	0.00	0.00	0.06	0.00	21.66	2.00	0.00	0.00	0.07	0.00
21.72	2.00	0.00	0.00	0.06	0.00	21.79	2.00	0.00	0.00	0.07	0.00
21.86	2.00	0.00	0.00	0.07	0.00	21.92	2.00	0.00	0.00	0.06	0.00
22.00	2.00	0.00	0.00	0.08	0.00	22.06	2.00	0.00	0.00	0.06	0.00
22.13	2.00	0.00	0.00	0.07	0.00	22.18	2.00	0.00	0.00	0.05	0.00
22.26	2.00	0.00	0.00	0.08	0.00	22.32	2.00	0.00	0.00	0.06	0.00
22.39	2.00	0.00	0.00	0.06	0.00	22.46	2.00	0.00	0.00	0.07	0.00
22.52	2.00	0.00	0.00	0.06	0.00	22.60	2.00	0.00	0.00	0.08	0.00
22.64	2.00	0.00	0.00	0.04	0.00	22.71	2.00	0.00	0.00	0.06	0.00
22.77	2.00	0.00	0.00	0.06	0.00	22.84	2.00	0.00	0.00	0.07	0.00
22.93	2.00	0.00	0.00	0.09	0.00	22.98	2.00	0.00	0.00	0.06	0.00
23.04	2.00	0.00	0.00	0.05	0.00	23.12	2.00	0.00	0.00	0.08	0.00
23.17	0.15	0.85	0.26	0.05	0.09	23.26	0.17	0.83	0.26	0.08	0.14
23.32	0.18	0.82	0.27	0.06	0.10	23.38	0.19	0.81	0.27	0.06	0.10
23.44	0.20	0.80	0.28	0.06	0.09	23.49	0.20	0.80	0.28	0.06	0.09
23.56	0.21	0.79	0.28	0.06	0.10	23.63	0.22	0.78	0.28	0.07	0.11
23.69	0.23	0.77	0.29	0.06	0.10	23.75	0.24	0.76	0.30	0.06	0.09
23.84	0.26	0.74	0.30	0.08	0.12	23.89	0.26	0.74	0.30	0.05	0.07
23.96	0.27	0.73	0.31	0.07	0.10	24.02	0.28	0.72	0.31	0.06	0.08
24.10	0.28	0.72	0.31	0.09	0.12	24.16	0.29	0.71	0.31	0.06	0.08
24.23	0.29	0.71	0.31	0.06	0.09	24.29	0.28	0.72	0.31	0.07	0.09
24.36	0.28	0.72	0.31	0.06	0.08	24.41	0.27	0.73	0.31	0.06	0.08
24.50	0.26	0.74	0.30	0.09	0.13	24.56	0.24	0.76	0.30	0.06	0.09
24.62	0.23	0.77	0.29	0.06	0.09	24.68	0.21	0.79	0.28	0.06	0.09
24.75	0.20	0.80	0.28	0.06	0.09	24.80	0.18	0.82	0.27	0.06	0.09
24.89	2.00	0.00	0.00	0.09	0.00	24.95	2.00	0.00	0.00	0.06	0.00
25.01	2.00	0.00	0.00	0.06	0.00	25.07	2.00	0.00	0.00	0.06	0.00
25.14	2.00	0.00	0.00	0.06	0.00	25.22	2.00	0.00	0.00	0.09	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
25.28	2.00	0.00	0.00	0.06	0.00	25.34	2.00	0.00	0.00	0.06	0.00
25.40	2.00	0.00	0.00	0.06	0.00	25.46	2.00	0.00	0.00	0.06	0.00
25.53	2.00	0.00	0.00	0.06	0.00	25.62	2.00	0.00	0.00	0.09	0.00
25.67	2.00	0.00	0.00	0.05	0.00	25.73	2.00	0.00	0.00	0.06	0.00
25.79	2.00	0.00	0.00	0.07	0.00	25.87	2.00	0.00	0.00	0.07	0.00
25.94	2.00	0.00	0.00	0.07	0.00	25.98	2.00	0.00	0.00	0.05	0.00
26.07	0.19	0.81	0.27	0.09	0.13	26.14	0.22	0.78	0.29	0.06	0.09
26.20	0.25	0.75	0.30	0.06	0.08	26.26	0.26	0.74	0.30	0.06	0.08
26.32	0.26	0.74	0.30	0.06	0.08	26.41	0.22	0.78	0.29	0.09	0.13
26.47	0.20	0.80	0.28	0.06	0.09	26.53	0.18	0.82	0.27	0.06	0.09
26.59	2.00	0.00	0.00	0.06	0.00	26.64	2.00	0.00	0.00	0.06	0.00
26.73	2.00	0.00	0.00	0.09	0.00	26.79	2.00	0.00	0.00	0.06	0.00
26.86	2.00	0.00	0.00	0.06	0.00	26.92	2.00	0.00	0.00	0.06	0.00
26.98	2.00	0.00	0.00	0.06	0.00	27.04	2.00	0.00	0.00	0.06	0.00
27.12	2.00	0.00	0.00	0.09	0.00	27.19	2.00	0.00	0.00	0.06	0.00
27.25	2.00	0.00	0.00	0.06	0.00	27.30	2.00	0.00	0.00	0.06	0.00
27.37	2.00	0.00	0.00	0.06	0.00	27.46	2.00	0.00	0.00	0.09	0.00
27.52	2.00	0.00	0.00	0.06	0.00	27.58	0.17	0.83	0.27	0.06	0.09
27.64	0.19	0.81	0.27	0.06	0.09	27.70	0.20	0.80	0.28	0.06	0.09
27.76	0.21	0.79	0.28	0.06	0.08	27.82	0.21	0.79	0.28	0.06	0.08
27.89	0.18	0.82	0.27	0.07	0.09	27.96	0.19	0.81	0.27	0.07	0.10
28.02	0.18	0.82	0.27	0.06	0.09	28.09	0.16	0.84	0.26	0.07	0.10
28.16	0.16	0.84	0.26	0.06	0.10	28.23	2.00	0.00	0.00	0.07	0.00
28.28	2.00	0.00	0.00	0.06	0.00	28.35	2.00	0.00	0.00	0.07	0.00
28.43	2.00	0.00	0.00	0.08	0.00	28.49	2.00	0.00	0.00	0.06	0.00
28.55	2.00	0.00	0.00	0.06	0.00	28.61	2.00	0.00	0.00	0.06	0.00
28.70	0.17	0.83	0.27	0.09	0.12	28.76	0.18	0.82	0.27	0.06	0.09
28.82	0.18	0.82	0.27	0.06	0.08	28.88	0.18	0.82	0.27	0.06	0.09
28.94	0.18	0.82	0.27	0.06	0.08	29.03	0.19	0.81	0.27	0.09	0.12
29.09	0.19	0.81	0.27	0.06	0.08	29.15	0.19	0.81	0.27	0.06	0.08
29.21	0.19	0.81	0.27	0.06	0.08	29.27	0.19	0.81	0.27	0.06	0.08
29.33	0.20	0.80	0.28	0.06	0.08	29.42	0.20	0.80	0.28	0.09	0.12
29.48	0.19	0.81	0.27	0.06	0.08	29.54	0.19	0.81	0.27	0.06	0.08
29.60	0.19	0.81	0.27	0.06	0.08	29.66	0.19	0.81	0.27	0.06	0.08
29.75	0.18	0.82	0.27	0.09	0.12	29.81	0.17	0.83	0.27	0.06	0.08
29.87	0.16	0.84	0.26	0.06	0.08	29.93	0.16	0.84	0.26	0.06	0.08
29.99	2.00	0.00	0.00	0.06	0.00	30.05	2.00	0.00	0.00	0.06	0.00
30.12	2.00	0.00	0.00	0.07	0.00	30.19	2.00	0.00	0.00	0.07	0.00
30.26	2.00	0.00	0.00	0.07	0.00	30.33	2.00	0.00	0.00	0.06	0.00
30.39	2.00	0.00	0.00	0.06	0.00	30.45	2.00	0.00	0.00	0.06	0.00
30.52	2.00	0.00	0.00	0.07	0.00	30.58	2.00	0.00	0.00	0.06	0.00
30.65	2.00	0.00	0.00	0.07	0.00	30.71	2.00	0.00	0.00	0.06	0.00
30.78	2.00	0.00	0.00	0.07	0.00	30.85	2.00	0.00	0.00	0.07	0.00
30.92	2.00	0.00	0.00	0.07	0.00	30.97	2.00	0.00	0.00	0.06	0.00
31.04	2.00	0.00	0.00	0.07	0.00	31.11	2.00	0.00	0.00	0.07	0.00
31.17	2.00	0.00	0.00	0.06	0.00	31.25	2.00	0.00	0.00	0.07	0.00
31.30	2.00	0.00	0.00	0.05	0.00	31.37	2.00	0.00	0.00	0.07	0.00
31.44	2.00	0.00	0.00	0.07	0.00	31.51	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
31.57	2.00	0.00	0.00	0.07	0.00	31.63	2.00	0.00	0.00	0.06	0.00
31.70	2.00	0.00	0.00	0.07	0.00	31.79	2.00	0.00	0.00	0.09	0.00
31.85	2.00	0.00	0.00	0.06	0.00	31.91	2.00	0.00	0.00	0.06	0.00
31.97	2.00	0.00	0.00	0.06	0.00	32.03	2.00	0.00	0.00	0.06	0.00
32.09	2.00	0.00	0.00	0.06	0.00	32.18	2.00	0.00	0.00	0.09	0.00
32.24	2.00	0.00	0.00	0.06	0.00	32.30	2.00	0.00	0.00	0.06	0.00
32.35	2.00	0.00	0.00	0.05	0.00	32.43	2.00	0.00	0.00	0.07	0.00
32.50	2.00	0.00	0.00	0.07	0.00	32.56	2.00	0.00	0.00	0.06	0.00
32.62	2.00	0.00	0.00	0.06	0.00	32.69	2.00	0.00	0.00	0.06	0.00
32.75	2.00	0.00	0.00	0.06	0.00	32.83	2.00	0.00	0.00	0.08	0.00
32.88	2.00	0.00	0.00	0.05	0.00	32.96	2.00	0.00	0.00	0.08	0.00
33.02	2.00	0.00	0.00	0.06	0.00	33.08	2.00	0.00	0.00	0.06	0.00
33.14	2.00	0.00	0.00	0.06	0.00	33.23	2.00	0.00	0.00	0.09	0.00
33.28	2.00	0.00	0.00	0.05	0.00	33.36	2.00	0.00	0.00	0.08	0.00
33.41	2.00	0.00	0.00	0.05	0.00	33.48	2.00	0.00	0.00	0.07	0.00
33.55	2.00	0.00	0.00	0.08	0.00	33.61	2.00	0.00	0.00	0.06	0.00
33.67	2.00	0.00	0.00	0.06	0.00	33.74	2.00	0.00	0.00	0.07	0.00
33.80	2.00	0.00	0.00	0.07	0.00	33.88	2.00	0.00	0.00	0.08	0.00
33.94	2.00	0.00	0.00	0.06	0.00	34.00	2.00	0.00	0.00	0.06	0.00
34.06	2.00	0.00	0.00	0.06	0.00	34.15	2.00	0.00	0.00	0.09	0.00
34.21	2.00	0.00	0.00	0.06	0.00	34.27	2.00	0.00	0.00	0.06	0.00
34.33	2.00	0.00	0.00	0.06	0.00	34.39	2.00	0.00	0.00	0.06	0.00
34.45	2.00	0.00	0.00	0.06	0.00	34.52	2.00	0.00	0.00	0.06	0.00
34.61	2.00	0.00	0.00	0.09	0.00	34.67	2.00	0.00	0.00	0.06	0.00
34.73	2.00	0.00	0.00	0.06	0.00	34.79	2.00	0.00	0.00	0.06	0.00
34.85	2.00	0.00	0.00	0.06	0.00	34.93	2.00	0.00	0.00	0.08	0.00
34.98	2.00	0.00	0.00	0.05	0.00	35.07	2.00	0.00	0.00	0.09	0.00
35.13	2.00	0.00	0.00	0.06	0.00	35.19	2.00	0.00	0.00	0.06	0.00
35.25	2.00	0.00	0.00	0.06	0.00	35.31	2.00	0.00	0.00	0.06	0.00
35.37	2.00	0.00	0.00	0.06	0.00	35.43	2.00	0.00	0.00	0.06	0.00
35.52	2.00	0.00	0.00	0.09	0.00	35.58	2.00	0.00	0.00	0.06	0.00
35.64	2.00	0.00	0.00	0.06	0.00	35.70	2.00	0.00	0.00	0.06	0.00
35.76	2.00	0.00	0.00	0.06	0.00	35.85	2.00	0.00	0.00	0.09	0.00
35.91	2.00	0.00	0.00	0.06	0.00	35.97	2.00	0.00	0.00	0.06	0.00
36.03	2.00	0.00	0.00	0.06	0.00	36.09	2.00	0.00	0.00	0.06	0.00
36.18	2.00	0.00	0.00	0.09	0.00	36.24	2.00	0.00	0.00	0.06	0.00
36.30	2.00	0.00	0.00	0.06	0.00	36.36	2.00	0.00	0.00	0.06	0.00
36.42	2.00	0.00	0.00	0.06	0.00	36.51	2.00	0.00	0.00	0.09	0.00
36.57	2.00	0.00	0.00	0.06	0.00	36.63	2.00	0.00	0.00	0.06	0.00
36.69	2.00	0.00	0.00	0.06	0.00	36.75	2.00	0.00	0.00	0.06	0.00
36.81	2.00	0.00	0.00	0.06	0.00	36.91	2.00	0.00	0.00	0.09	0.00
36.97	2.00	0.00	0.00	0.06	0.00	37.03	2.00	0.00	0.00	0.06	0.00
37.08	2.00	0.00	0.00	0.05	0.00	37.15	2.00	0.00	0.00	0.06	0.00
37.21	2.00	0.00	0.00	0.06	0.00	37.29	2.00	0.00	0.00	0.08	0.00
37.34	2.00	0.00	0.00	0.05	0.00	37.43	2.00	0.00	0.00	0.08	0.00
37.48	2.00	0.00	0.00	0.05	0.00	37.55	2.00	0.00	0.00	0.07	0.00
37.62	2.00	0.00	0.00	0.07	0.00	37.67	2.00	0.00	0.00	0.05	0.00
37.74	2.00	0.00	0.00	0.07	0.00	37.81	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
37.86	2.00	0.00	0.00	0.05	0.00	37.94	2.00	0.00	0.00	0.07	0.00
38.02	2.00	0.00	0.00	0.08	0.00	38.07	2.00	0.00	0.00	0.05	0.00
38.13	2.00	0.00	0.00	0.06	0.00	38.22	2.00	0.00	0.00	0.09	0.00
38.28	2.00	0.00	0.00	0.06	0.00	38.34	2.00	0.00	0.00	0.06	0.00
38.40	2.00	0.00	0.00	0.06	0.00	38.47	2.00	0.00	0.00	0.07	0.00
38.53	2.00	0.00	0.00	0.06	0.00	38.59	2.00	0.00	0.00	0.06	0.00
38.68	2.00	0.00	0.00	0.09	0.00	38.74	0.17	0.83	0.27	0.06	0.06
38.80	0.18	0.82	0.27	0.06	0.06	38.85	0.18	0.82	0.27	0.06	0.06
38.93	0.18	0.82	0.27	0.07	0.07	38.98	0.18	0.82	0.27	0.05	0.05
39.04	0.17	0.83	0.27	0.07	0.07	39.11	0.18	0.82	0.27	0.07	0.07
39.20	2.00	0.00	0.00	0.09	0.00	39.26	2.00	0.00	0.00	0.06	0.00
39.32	2.00	0.00	0.00	0.06	0.00	39.38	2.00	0.00	0.00	0.06	0.00
39.44	2.00	0.00	0.00	0.06	0.00	39.53	2.00	0.00	0.00	0.09	0.00
39.59	2.00	0.00	0.00	0.06	0.00	39.65	2.00	0.00	0.00	0.06	0.00
39.71	2.00	0.00	0.00	0.06	0.00	39.77	2.00	0.00	0.00	0.06	0.00
39.86	2.00	0.00	0.00	0.09	0.00	39.92	2.00	0.00	0.00	0.06	0.00
39.98	2.00	0.00	0.00	0.06	0.00	40.04	2.00	0.00	0.00	0.06	0.00
40.10	2.00	0.00	0.00	0.06	0.00	40.16	0.18	0.82	0.27	0.06	0.06
40.22	0.26	0.74	0.30	0.07	0.06	40.30	0.36	0.64	0.36	0.07	0.06
40.37	0.49	0.51	0.46	0.07	0.05	40.43	0.54	0.46	0.54	0.06	0.03
40.51	0.63	0.37	0.69	0.07	0.03	40.57	0.68	0.32	0.85	0.06	0.02
40.63	0.73	0.27	1.07	0.06	0.02	40.69	0.78	0.00	0.00	0.06	0.02
40.78	0.87	0.00	0.00	0.09	0.01	40.84	0.89	0.00	0.00	0.06	0.01
40.90	0.88	0.00	0.00	0.06	0.01	40.95	0.87	0.00	0.00	0.06	0.01
41.01	0.89	0.00	0.00	0.06	0.01	41.10	0.88	0.00	0.00	0.09	0.01
41.16	0.88	0.00	0.00	0.06	0.01	41.22	0.88	0.00	0.00	0.06	0.01
41.28	0.89	0.00	0.00	0.06	0.01	41.34	0.93	0.00	0.00	0.06	0.00
41.41	1.02	0.00	0.00	0.06	0.00	41.49	1.19	0.00	0.00	0.09	0.00
41.55	1.30	0.00	0.00	0.06	0.00	41.61	1.42	0.00	0.00	0.06	0.00
41.68	1.55	0.00	0.00	0.06	0.00	41.73	1.69	0.00	0.00	0.06	0.00
41.83	2.00	0.00	0.00	0.09	0.00	41.89	2.00	0.00	0.00	0.06	0.00
41.95	2.00	0.00	0.00	0.06	0.00	42.01	2.00	0.00	0.00	0.06	0.00
42.06	2.00	0.00	0.00	0.06	0.00	42.16	2.00	0.00	0.00	0.09	0.00
42.22	2.00	0.00	0.00	0.06	0.00	42.28	2.00	0.00	0.00	0.06	0.00
42.34	2.00	0.00	0.00	0.06	0.00	42.40	1.77	0.00	0.00	0.06	0.00
42.48	1.04	0.00	0.00	0.08	0.00	42.54	1.12	0.00	0.00	0.06	0.00
42.60	0.97	0.00	0.00	0.06	0.00	42.66	0.83	0.00	0.00	0.06	0.01
42.72	0.72	0.28	0.99	0.06	0.02	42.78	0.62	0.38	0.68	0.06	0.02
42.87	0.54	0.46	0.53	0.09	0.04	42.93	0.50	0.50	0.48	0.06	0.03
42.99	0.49	0.51	0.47	0.06	0.03	43.05	0.48	0.52	0.46	0.06	0.03
43.11	0.48	0.52	0.46	0.06	0.03	43.20	0.48	0.52	0.46	0.09	0.05
43.26	0.48	0.52	0.46	0.06	0.03	43.32	0.48	0.52	0.45	0.06	0.03
43.38	0.47	0.53	0.45	0.06	0.03	43.44	0.45	0.55	0.43	0.06	0.03
43.51	0.43	0.57	0.41	0.06	0.04	43.59	0.39	0.61	0.38	0.09	0.06
43.65	0.37	0.63	0.37	0.06	0.04	43.71	0.35	0.65	0.35	0.06	0.04
43.77	0.33	0.67	0.34	0.06	0.04	43.83	0.31	0.69	0.33	0.06	0.04
43.92	0.28	0.72	0.31	0.09	0.07	43.98	0.25	0.75	0.30	0.06	0.05
44.05	0.23	0.77	0.29	0.06	0.05	44.10	0.20	0.80	0.28	0.06	0.05

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
44.16	0.18	0.82	0.27	0.06	0.05	44.23	2.00	0.00	0.00	0.06	0.00
44.32	2.00	0.00	0.00	0.09	0.00	44.38	2.00	0.00	0.00	0.06	0.00
44.43	2.00	0.00	0.00	0.05	0.00	44.49	2.00	0.00	0.00	0.06	0.00
44.57	2.00	0.00	0.00	0.08	0.00	44.63	2.00	0.00	0.00	0.06	0.00
44.70	2.00	0.00	0.00	0.07	0.00	44.77	2.00	0.00	0.00	0.07	0.00
44.82	2.00	0.00	0.00	0.05	0.00	44.88	2.00	0.00	0.00	0.06	0.00
44.97	2.00	0.00	0.00	0.09	0.00	45.03	0.19	0.81	0.27	0.06	0.05
45.10	0.21	0.79	0.28	0.07	0.05	45.16	0.24	0.76	0.29	0.06	0.04
45.22	0.26	0.74	0.30	0.06	0.04	45.28	0.26	0.74	0.30	0.06	0.04
45.37	0.28	0.72	0.31	0.09	0.06	45.43	0.29	0.71	0.32	0.06	0.04
45.49	0.30	0.70	0.32	0.06	0.04	45.55	0.32	0.68	0.33	0.06	0.04
45.61	0.35	0.65	0.35	0.06	0.04	45.67	0.38	0.62	0.37	0.06	0.03
45.76	0.40	0.60	0.39	0.09	0.05	45.82	0.40	0.60	0.38	0.06	0.03
45.88	0.37	0.63	0.37	0.06	0.03	45.94	0.35	0.65	0.35	0.06	0.04
46.00	0.32	0.68	0.33	0.06	0.04	46.09	0.28	0.72	0.31	0.09	0.06
46.15	0.27	0.73	0.31	0.06	0.04	46.21	0.26	0.74	0.30	0.06	0.04
46.27	0.24	0.76	0.29	0.06	0.04	46.33	0.23	0.77	0.29	0.06	0.04
46.42	0.21	0.79	0.28	0.09	0.06	46.48	0.20	0.80	0.28	0.06	0.04
46.54	0.19	0.81	0.27	0.06	0.04	46.60	0.19	0.81	0.27	0.06	0.04
46.66	0.19	0.81	0.27	0.06	0.04	46.72	0.19	0.81	0.27	0.06	0.04
46.80	0.18	0.82	0.27	0.08	0.05	46.86	0.18	0.82	0.27	0.07	0.05
46.93	0.19	0.81	0.27	0.06	0.05	46.98	0.18	0.82	0.27	0.05	0.04
47.07	0.17	0.83	0.27	0.09	0.06	47.13	0.17	0.83	0.27	0.06	0.04
47.19	0.16	0.84	0.26	0.06	0.04	47.25	2.00	0.00	0.00	0.06	0.00
47.31	2.00	0.00	0.00	0.06	0.00	47.40	2.00	0.00	0.00	0.09	0.00
47.46	2.00	0.00	0.00	0.06	0.00	47.52	2.00	0.00	0.00	0.06	0.00
47.58	2.00	0.00	0.00	0.06	0.00	47.64	2.00	0.00	0.00	0.06	0.00
47.73	2.00	0.00	0.00	0.09	0.00	47.79	2.00	0.00	0.00	0.06	0.00
47.85	2.00	0.00	0.00	0.06	0.00	47.91	2.00	0.00	0.00	0.06	0.00
47.97	2.00	0.00	0.00	0.06	0.00	48.03	2.00	0.00	0.00	0.06	0.00
48.12	2.00	0.00	0.00	0.09	0.00	48.18	2.00	0.00	0.00	0.06	0.00
48.24	2.00	0.00	0.00	0.06	0.00	48.30	2.00	0.00	0.00	0.06	0.00
48.36	2.00	0.00	0.00	0.06	0.00	48.45	2.00	0.00	0.00	0.09	0.00
48.51	2.00	0.00	0.00	0.06	0.00	48.57	2.00	0.00	0.00	0.06	0.00
48.63	2.00	0.00	0.00	0.06	0.00	48.69	2.00	0.00	0.00	0.06	0.00
48.78	2.00	0.00	0.00	0.09	0.00	48.84	2.00	0.00	0.00	0.06	0.00
48.90	2.00	0.00	0.00	0.06	0.00	48.96	2.00	0.00	0.00	0.06	0.00
49.03	2.00	0.00	0.00	0.06	0.00	49.09	2.00	0.00	0.00	0.06	0.00
49.15	2.00	0.00	0.00	0.06	0.00	49.21	2.00	0.00	0.00	0.07	0.00
49.30	2.00	0.00	0.00	0.08	0.00	49.36	0.18	0.82	0.27	0.07	0.04
49.42	0.20	0.80	0.28	0.05	0.03	49.48	0.24	0.76	0.29	0.06	0.03
49.55	0.30	0.70	0.32	0.08	0.04	49.61	0.36	0.64	0.36	0.06	0.03
49.70	0.33	0.67	0.34	0.09	0.04	49.76	0.33	0.67	0.34	0.06	0.03
49.82	0.37	0.63	0.36	0.06	0.03	49.88	0.41	0.59	0.39	0.06	0.03
49.94	0.45	0.55	0.43	0.06	0.02	50.00	2.00	0.00	0.00	0.06	0.00
50.07	2.00	0.00	0.00	0.07	0.00	50.14	2.00	0.00	0.00	0.07	0.00
50.20	2.00	0.00	0.00	0.06	0.00	50.27	2.00	0.00	0.00	0.07	0.00
50.34	2.00	0.00	0.00	0.07	0.00	50.41	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
50.46	2.00	0.00	0.00	0.06	0.00	50.54	2.00	0.00	0.00	0.08	0.00
50.61	2.00	0.00	0.00	0.07	0.00	50.67	2.00	0.00	0.00	0.06	0.00
50.74	2.00	0.00	0.00	0.07	0.00	50.79	2.00	0.00	0.00	0.05	0.00
50.85	2.00	0.00	0.00	0.06	0.00	50.94	2.00	0.00	0.00	0.09	0.00
51.01	2.00	0.00	0.00	0.06	0.00	51.06	2.00	0.00	0.00	0.06	0.00
51.13	2.00	0.00	0.00	0.06	0.00	51.18	2.00	0.00	0.00	0.06	0.00
51.27	2.00	0.00	0.00	0.09	0.00	51.33	2.00	0.00	0.00	0.06	0.00
51.38	2.00	0.00	0.00	0.05	0.00	51.46	2.00	0.00	0.00	0.08	0.00
51.52	2.00	0.00	0.00	0.06	0.00	51.58	2.00	0.00	0.00	0.06	0.00
51.64	2.00	0.00	0.00	0.06	0.00	51.73	2.00	0.00	0.00	0.09	0.00
51.79	2.00	0.00	0.00	0.06	0.00	51.85	2.00	0.00	0.00	0.06	0.00
51.91	2.00	0.00	0.00	0.06	0.00	51.98	2.00	0.00	0.00	0.07	0.00
52.05	2.00	0.00	0.00	0.07	0.00	52.10	2.00	0.00	0.00	0.05	0.00
52.18	2.00	0.00	0.00	0.07	0.00	52.23	2.00	0.00	0.00	0.06	0.00
52.31	2.00	0.00	0.00	0.07	0.00	52.36	2.00	0.00	0.00	0.06	0.00
52.44	2.00	0.00	0.00	0.08	0.00	52.51	2.00	0.00	0.00	0.07	0.00
52.57	2.00	0.00	0.00	0.06	0.00	52.63	2.00	0.00	0.00	0.06	0.00
52.72	2.00	0.00	0.00	0.09	0.00	52.77	2.00	0.00	0.00	0.06	0.00
52.84	2.00	0.00	0.00	0.06	0.00	52.90	2.00	0.00	0.00	0.06	0.00
52.95	2.00	0.00	0.00	0.06	0.00	53.04	2.00	0.00	0.00	0.09	0.00
53.10	2.00	0.00	0.00	0.06	0.00	53.16	2.00	0.00	0.00	0.06	0.00
53.23	2.00	0.00	0.00	0.06	0.00	53.29	2.00	0.00	0.00	0.06	0.00
53.35	2.00	0.00	0.00	0.06	0.00	53.44	2.00	0.00	0.00	0.09	0.00
53.50	2.00	0.00	0.00	0.06	0.00	53.56	2.00	0.00	0.00	0.06	0.00
53.62	2.00	0.00	0.00	0.06	0.00	53.67	2.00	0.00	0.00	0.06	0.00
53.76	2.00	0.00	0.00	0.09	0.00	53.82	2.00	0.00	0.00	0.06	0.00
53.88	2.00	0.00	0.00	0.06	0.00	53.94	2.00	0.00	0.00	0.06	0.00
54.00	2.00	0.00	0.00	0.06	0.00	54.09	2.00	0.00	0.00	0.09	0.00
54.16	2.00	0.00	0.00	0.06	0.00	54.22	2.00	0.00	0.00	0.06	0.00
54.27	2.00	0.00	0.00	0.05	0.00	54.34	2.00	0.00	0.00	0.07	0.00
54.41	2.00	0.00	0.00	0.07	0.00	54.47	2.00	0.00	0.00	0.06	0.00
54.56	2.00	0.00	0.00	0.09	0.00	54.62	2.00	0.00	0.00	0.06	0.00
54.68	2.00	0.00	0.00	0.06	0.00	54.74	2.00	0.00	0.00	0.06	0.00
54.80	2.00	0.00	0.00	0.06	0.00	54.86	2.00	0.00	0.00	0.06	0.00
54.95	2.00	0.00	0.00	0.09	0.00	55.01	2.00	0.00	0.00	0.06	0.00
55.07	2.00	0.00	0.00	0.06	0.00	55.13	2.00	0.00	0.00	0.06	0.00
55.19	2.00	0.00	0.00	0.06	0.00	55.28	2.00	0.00	0.00	0.09	0.00
55.34	2.00	0.00	0.00	0.06	0.00	55.40	2.00	0.00	0.00	0.06	0.00
55.45	2.00	0.00	0.00	0.06	0.00	55.51	2.00	0.00	0.00	0.06	0.00
55.60	2.00	0.00	0.00	0.09	0.00	55.66	2.00	0.00	0.00	0.06	0.00
55.73	2.00	0.00	0.00	0.06	0.00	55.79	2.00	0.00	0.00	0.06	0.00
55.84	2.00	0.00	0.00	0.06	0.00	55.94	2.00	0.00	0.00	0.09	0.00
56.00	2.00	0.00	0.00	0.06	0.00	56.06	2.00	0.00	0.00	0.06	0.00
56.12	2.00	0.00	0.00	0.06	0.00	56.18	2.00	0.00	0.00	0.06	0.00
56.24	2.00	0.00	0.00	0.06	0.00	56.30	2.00	0.00	0.00	0.06	0.00
56.39	2.00	0.00	0.00	0.09	0.00	56.43	2.00	0.00	0.00	0.04	0.00
56.50	2.00	0.00	0.00	0.07	0.00	56.56	2.00	0.00	0.00	0.06	0.00
56.65	2.00	0.00	0.00	0.09	0.00	56.71	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
56.77	2.00	0.00	0.00	0.06	0.00	56.84	2.00	0.00	0.00	0.06	0.00
56.89	2.00	0.00	0.00	0.06	0.00	56.98	2.00	0.00	0.00	0.09	0.00
57.04	2.00	0.00	0.00	0.06	0.00	57.10	2.00	0.00	0.00	0.06	0.00
57.16	2.00	0.00	0.00	0.06	0.00	57.22	2.00	0.00	0.00	0.06	0.00
57.31	2.00	0.00	0.00	0.09	0.00	57.37	2.00	0.00	0.00	0.06	0.00
57.43	2.00	0.00	0.00	0.06	0.00	57.49	2.00	0.00	0.00	0.06	0.00
57.55	2.00	0.00	0.00	0.06	0.00	57.61	2.00	0.00	0.00	0.06	0.00
57.70	2.00	0.00	0.00	0.09	0.00	57.76	2.00	0.00	0.00	0.06	0.00
57.82	2.00	0.00	0.00	0.06	0.00	57.88	2.00	0.00	0.00	0.06	0.00
57.94	2.00	0.00	0.00	0.06	0.00	58.03	2.00	0.00	0.00	0.09	0.00
58.09	2.00	0.00	0.00	0.06	0.00	58.16	2.00	0.00	0.00	0.06	0.00
58.22	2.00	0.00	0.00	0.06	0.00	58.28	2.00	0.00	0.00	0.06	0.00
58.34	2.00	0.00	0.00	0.06	0.00	58.42	2.00	0.00	0.00	0.09	0.00
58.48	2.00	0.00	0.00	0.06	0.00	58.55	2.00	0.00	0.00	0.06	0.00
58.60	2.00	0.00	0.00	0.06	0.00	58.67	2.00	0.00	0.00	0.06	0.00
58.75	2.00	0.00	0.00	0.09	0.00	58.81	2.00	0.00	0.00	0.06	0.00
58.87	2.00	0.00	0.00	0.06	0.00	58.94	2.00	0.00	0.00	0.06	0.00
59.00	2.00	0.00	0.00	0.06	0.00	59.06	2.00	0.00	0.00	0.06	0.00
59.15	2.00	0.00	0.00	0.09	0.00	59.20	2.00	0.00	0.00	0.05	0.00
59.27	2.00	0.00	0.00	0.07	0.00	59.32	2.00	0.00	0.00	0.06	0.00
59.40	2.00	0.00	0.00	0.08	0.00	59.46	2.00	0.00	0.00	0.06	0.00
59.53	2.00	0.00	0.00	0.07	0.00	59.58	2.00	0.00	0.00	0.05	0.00
59.66	2.00	0.00	0.00	0.08	0.00	59.73	2.00	0.00	0.00	0.08	0.00
59.79	2.00	0.00	0.00	0.05	0.00	59.86	2.00	0.00	0.00	0.07	0.00
59.93	2.00	0.00	0.00	0.07	0.00	59.98	2.00	0.00	0.00	0.05	0.00
60.05	2.00	0.00	0.00	0.07	0.00	60.12	2.00	0.00	0.00	0.08	0.00
60.19	2.00	0.00	0.00	0.07	0.00	60.24	2.00	0.00	0.00	0.05	0.00
60.32	2.00	0.00	0.00	0.08	0.00	60.38	2.00	0.00	0.00	0.06	0.00
60.44	2.00	0.00	0.00	0.06	0.00	60.50	2.00	0.00	0.00	0.06	0.00
60.59	2.00	0.00	0.00	0.09	0.00	60.65	2.00	0.00	0.00	0.06	0.00
60.71	2.00	0.00	0.00	0.06	0.00	60.77	2.00	0.00	0.00	0.06	0.00
60.83	2.00	0.00	0.00	0.06	0.00	60.89	2.00	0.00	0.00	0.06	0.00
60.98	2.00	0.00	0.00	0.09	0.00	61.04	2.00	0.00	0.00	0.06	0.00
61.10	2.00	0.00	0.00	0.06	0.00	61.16	2.00	0.00	0.00	0.06	0.00
61.22	2.00	0.00	0.00	0.06	0.00	61.31	2.00	0.00	0.00	0.09	0.00
61.37	2.00	0.00	0.00	0.06	0.00	61.43	2.00	0.00	0.00	0.06	0.00
61.49	2.00	0.00	0.00	0.06	0.00	61.55	2.00	0.00	0.00	0.06	0.00
61.64	2.00	0.00	0.00	0.09	0.00	61.70	2.00	0.00	0.00	0.06	0.00
61.76	2.00	0.00	0.00	0.06	0.00	61.82	2.00	0.00	0.00	0.06	0.00
61.88	2.00	0.00	0.00	0.06	0.00	61.94	2.00	0.00	0.00	0.06	0.00
62.04	2.00	0.00	0.00	0.09	0.00	62.10	2.00	0.00	0.00	0.06	0.00
62.16	2.00	0.00	0.00	0.06	0.00	62.22	2.00	0.00	0.00	0.06	0.00
62.29	2.00	0.00	0.00	0.07	0.00	62.34	2.00	0.00	0.00	0.05	0.00
62.43	2.00	0.00	0.00	0.09	0.00	62.49	2.00	0.00	0.00	0.06	0.00
62.55	2.00	0.00	0.00	0.06	0.00	62.61	2.00	0.00	0.00	0.06	0.00
62.67	2.00	0.00	0.00	0.06	0.00	62.73	2.00	0.00	0.00	0.06	0.00
62.82	2.00	0.00	0.00	0.09	0.00	62.88	2.00	0.00	0.00	0.06	0.00
62.94	2.00	0.00	0.00	0.06	0.00	63.00	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
63.06	2.00	0.00	0.00	0.06	0.00	63.12	2.00	0.00	0.00	0.06	0.00
63.21	2.00	0.00	0.00	0.09	0.00	63.27	2.00	0.00	0.00	0.06	0.00
63.33	2.00	0.00	0.00	0.06	0.00	63.40	2.00	0.00	0.00	0.06	0.00
63.46	2.00	0.00	0.00	0.06	0.00	63.55	2.00	0.00	0.00	0.09	0.00
63.60	2.00	0.00	0.00	0.06	0.00	63.66	2.00	0.00	0.00	0.06	0.00
63.73	2.00	0.00	0.00	0.06	0.00	63.78	2.00	0.00	0.00	0.06	0.00
63.87	2.00	0.00	0.00	0.09	0.00	63.94	2.00	0.00	0.00	0.06	0.00
63.99	2.00	0.00	0.00	0.06	0.00	64.05	2.00	0.00	0.00	0.06	0.00
64.12	2.00	0.00	0.00	0.06	0.00	64.18	2.00	0.00	0.00	0.06	0.00
64.27	2.00	0.00	0.00	0.09	0.00	64.33	2.00	0.00	0.00	0.06	0.00
64.39	2.00	0.00	0.00	0.06	0.00	64.44	2.00	0.00	0.00	0.05	0.00
64.51	2.00	0.00	0.00	0.07	0.00	64.57	2.00	0.00	0.00	0.06	0.00
64.63	2.00	0.00	0.00	0.06	0.00	64.72	2.00	0.00	0.00	0.09	0.00
64.79	2.00	0.00	0.00	0.06	0.00	64.85	2.00	0.00	0.00	0.06	0.00
64.91	2.00	0.00	0.00	0.06	0.00	64.96	2.00	0.00	0.00	0.06	0.00
65.05	2.00	0.00	0.00	0.09	0.00	65.11	2.00	0.00	0.00	0.06	0.00
65.18	2.00	0.00	0.00	0.06	0.00	65.23	2.00	0.00	0.00	0.06	0.00
65.29	2.00	0.00	0.00	0.06	0.00	65.38	2.00	0.00	0.00	0.09	0.00
65.44	2.00	0.00	0.00	0.06	0.00	65.50	2.00	0.00	0.00	0.06	0.00
65.56	2.00	0.00	0.00	0.06	0.00	65.63	2.00	0.00	0.00	0.06	0.00
65.69	2.00	0.00	0.00	0.06	0.00	65.77	2.00	0.00	0.00	0.09	0.00
65.83	2.00	0.00	0.00	0.06	0.00	65.89	2.00	0.00	0.00	0.06	0.00
65.95	2.00	0.00	0.00	0.06	0.00	66.01	2.00	0.00	0.00	0.06	0.00
66.10	2.00	0.00	0.00	0.09	0.00	66.16	2.00	0.00	0.00	0.06	0.00
66.23	2.00	0.00	0.00	0.06	0.00	66.29	2.00	0.00	0.00	0.06	0.00
66.35	2.00	0.00	0.00	0.06	0.00	66.41	2.00	0.00	0.00	0.06	0.00
66.47	2.00	0.00	0.00	0.06	0.00	66.54	2.00	0.00	0.00	0.07	0.00
66.62	2.00	0.00	0.00	0.08	0.00	66.69	2.00	0.00	0.00	0.07	0.00
66.75	2.00	0.00	0.00	0.06	0.00	66.81	2.00	0.00	0.00	0.06	0.00
66.86	2.00	0.00	0.00	0.06	0.00	66.95	2.00	0.00	0.00	0.09	0.00
67.01	2.00	0.00	0.00	0.06	0.00	67.07	2.00	0.00	0.00	0.06	0.00
67.13	2.00	0.00	0.00	0.06	0.00	67.19	2.00	0.00	0.00	0.06	0.00
67.28	2.00	0.00	0.00	0.09	0.00	67.34	2.00	0.00	0.00	0.06	0.00
67.40	2.00	0.00	0.00	0.06	0.00	67.46	2.00	0.00	0.00	0.06	0.00
67.52	2.00	0.00	0.00	0.06	0.00	67.61	2.00	0.00	0.00	0.09	0.00
67.67	2.00	0.00	0.00	0.06	0.00	67.73	2.00	0.00	0.00	0.06	0.00
67.79	2.00	0.00	0.00	0.06	0.00	67.85	2.00	0.00	0.00	0.06	0.00
67.94	2.00	0.00	0.00	0.09	0.00	68.00	2.00	0.00	0.00	0.06	0.00
68.06	2.00	0.00	0.00	0.06	0.00	68.12	2.00	0.00	0.00	0.06	0.00
68.18	2.00	0.00	0.00	0.06	0.00	68.24	2.00	0.00	0.00	0.06	0.00
68.33	2.00	0.00	0.00	0.09	0.00	68.39	2.00	0.00	0.00	0.06	0.00
68.45	2.00	0.00	0.00	0.06	0.00	68.51	2.00	0.00	0.00	0.06	0.00
68.59	2.00	0.00	0.00	0.08	0.00	68.65	2.00	0.00	0.00	0.06	0.00
68.70	2.00	0.00	0.00	0.06	0.00	68.80	2.00	0.00	0.00	0.09	0.00
68.86	2.00	0.00	0.00	0.06	0.00	68.92	2.00	0.00	0.00	0.06	0.00
68.97	2.00	0.00	0.00	0.06	0.00	69.04	2.00	0.00	0.00	0.06	0.00
69.10	2.00	0.00	0.00	0.06	0.00	69.19	2.00	0.00	0.00	0.09	0.00
69.25	2.00	0.00	0.00	0.06	0.00	69.31	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
69.36	2.00	0.00	0.00	0.06	0.00	69.42	2.00	0.00	0.00	0.06	0.00
69.51	2.00	0.00	0.00	0.09	0.00	69.57	2.00	0.00	0.00	0.06	0.00
69.63	2.00	0.00	0.00	0.06	0.00	69.69	2.00	0.00	0.00	0.06	0.00
69.75	2.00	0.00	0.00	0.06	0.00	69.84	2.00	0.00	0.00	0.09	0.00
69.89	2.00	0.00	0.00	0.05	0.00	69.96	2.00	0.00	0.00	0.07	0.00
70.02	2.00	0.00	0.00	0.05	0.00	70.08	2.00	0.00	0.00	0.07	0.00
70.15	2.00	0.00	0.00	0.06	0.00	70.21	2.00	0.00	0.00	0.06	0.00
70.28	2.00	0.00	0.00	0.07	0.00	70.35	2.00	0.00	0.00	0.06	0.00
70.41	2.00	0.00	0.00	0.06	0.00	70.48	2.00	0.00	0.00	0.07	0.00
70.55	2.00	0.00	0.00	0.07	0.00	70.61	2.00	0.00	0.00	0.07	0.00
70.68	2.00	0.00	0.00	0.07	0.00	70.74	2.00	0.00	0.00	0.06	0.00
70.81	2.00	0.00	0.00	0.06	0.00	70.88	2.00	0.00	0.00	0.07	0.00
70.95	2.00	0.00	0.00	0.07	0.00	71.00	2.00	0.00	0.00	0.05	0.00
71.08	2.00	0.00	0.00	0.08	0.00	71.14	2.00	0.00	0.00	0.06	0.00
71.20	2.00	0.00	0.00	0.06	0.00	71.29	2.00	0.00	0.00	0.09	0.00
71.35	2.00	0.00	0.00	0.06	0.00	71.41	2.00	0.00	0.00	0.06	0.00
71.47	2.00	0.00	0.00	0.06	0.00	71.53	2.00	0.00	0.00	0.06	0.00
71.59	2.00	0.00	0.00	0.06	0.00	71.66	2.00	0.00	0.00	0.07	0.00
71.72	2.00	0.00	0.00	0.06	0.00	71.79	2.00	0.00	0.00	0.07	0.00
71.86	2.00	0.00	0.00	0.07	0.00	71.92	2.00	0.00	0.00	0.06	0.00
71.98	2.00	0.00	0.00	0.06	0.00	72.06	2.00	0.00	0.00	0.08	0.00
72.13	2.00	0.00	0.00	0.06	0.00	72.19	2.00	0.00	0.00	0.07	0.00
72.26	2.00	0.00	0.00	0.07	0.00	72.32	2.00	0.00	0.00	0.06	0.00
72.38	2.00	0.00	0.00	0.06	0.00	72.45	2.00	0.00	0.00	0.07	0.00
72.51	2.00	0.00	0.00	0.05	0.00	72.58	2.00	0.00	0.00	0.07	0.00
72.65	2.00	0.00	0.00	0.07	0.00	72.72	2.00	0.00	0.00	0.07	0.00
72.77	2.00	0.00	0.00	0.05	0.00	72.84	2.00	0.00	0.00	0.07	0.00
72.92	2.00	0.00	0.00	0.08	0.00	72.98	2.00	0.00	0.00	0.06	0.00
73.04	2.00	0.00	0.00	0.06	0.00	73.11	2.00	0.00	0.00	0.08	0.00
73.17	2.00	0.00	0.00	0.06	0.00	73.24	2.00	0.00	0.00	0.07	0.00
73.30	2.00	0.00	0.00	0.05	0.00	73.37	2.00	0.00	0.00	0.08	0.00
73.44	2.00	0.00	0.00	0.06	0.00	73.49	2.00	0.00	0.00	0.06	0.00
73.57	2.00	0.00	0.00	0.08	0.00	73.63	2.00	0.00	0.00	0.06	0.00
73.70	2.00	0.00	0.00	0.07	0.00	73.77	2.00	0.00	0.00	0.08	0.00
73.83	2.00	0.00	0.00	0.06	0.00	73.89	2.00	0.00	0.00	0.06	0.00
73.95	2.00	0.00	0.00	0.06	0.00	74.04	2.00	0.00	0.00	0.09	0.00
74.10	2.00	0.00	0.00	0.06	0.00	74.16	2.00	0.00	0.00	0.06	0.00
74.22	2.00	0.00	0.00	0.06	0.00	74.28	2.00	0.00	0.00	0.06	0.00
74.37	2.00	0.00	0.00	0.09	0.00	74.43	2.00	0.00	0.00	0.06	0.00
74.49	2.00	0.00	0.00	0.06	0.00	74.55	2.00	0.00	0.00	0.06	0.00
74.62	2.00	0.00	0.00	0.07	0.00	74.67	2.00	0.00	0.00	0.06	0.00
74.75	2.00	0.00	0.00	0.08	0.00	74.82	2.00	0.00	0.00	0.07	0.00
74.88	2.00	0.00	0.00	0.06	0.00	74.94	2.00	0.00	0.00	0.07	0.00
75.00	2.00	0.00	0.00	0.06	0.00	75.07	2.00	0.00	0.00	0.06	0.00
75.14	2.00	0.00	0.00	0.07	0.00	75.21	2.00	0.00	0.00	0.07	0.00
75.28	2.00	0.00	0.00	0.07	0.00	75.33	2.00	0.00	0.00	0.05	0.00
75.41	2.00	0.00	0.00	0.07	0.00	75.48	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}	Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}

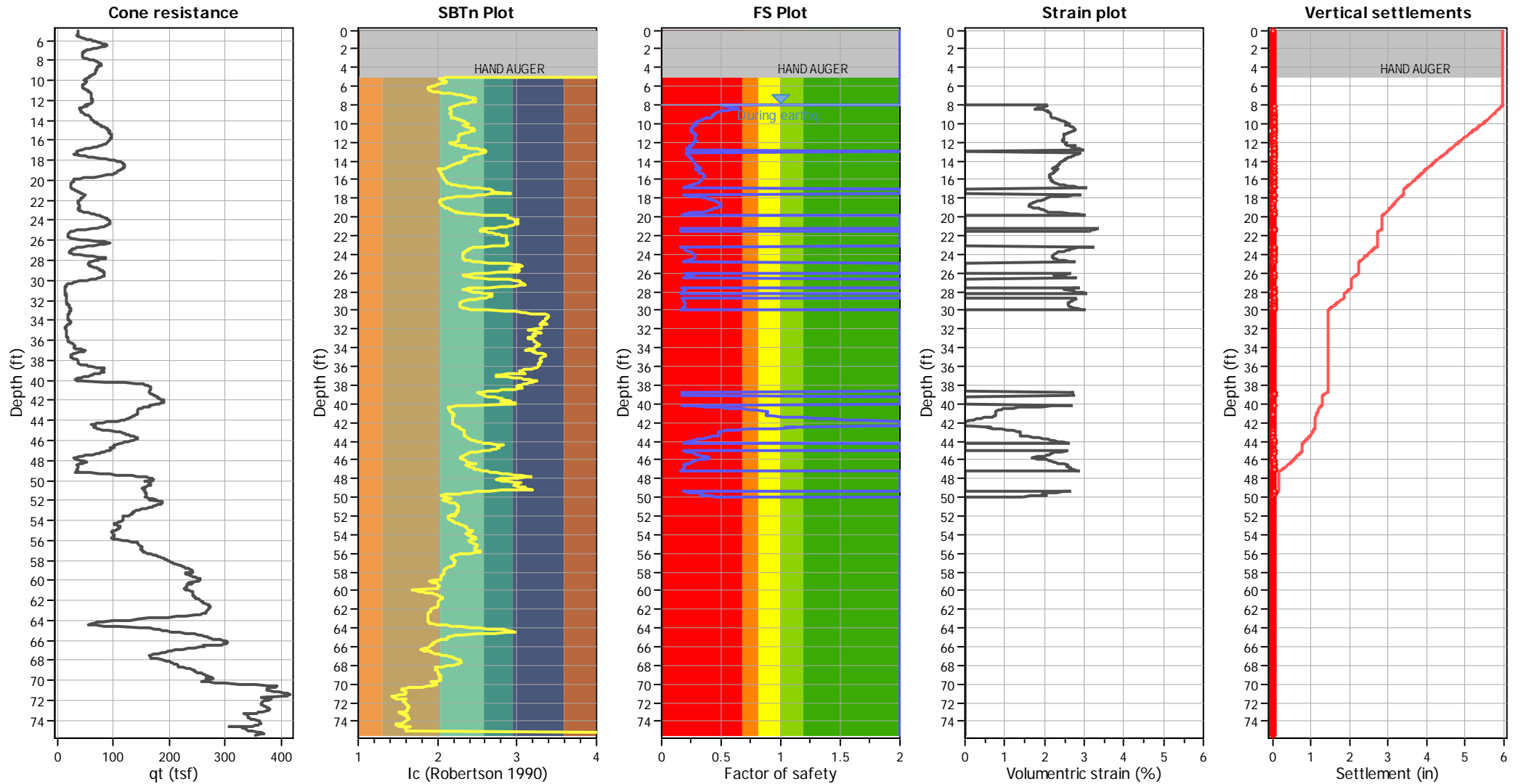
Overall liquefaction potential: 28.15

$LPI_{ISH} > 5.0$ - Liquefaction manifestation is expected

Abbreviations

- FS: Calculated factor of safety for test point
- d_z : Layer thickness (ft)
- LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_t : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement due to soil liquefaction ::											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.01	148.25	0.50	2.10	1.00	0.01	8.08	150.87	0.53	2.06	1.00	0.02
8.14	151.91	0.54	2.05	1.00	0.01	8.22	154.12	0.57	2.01	1.00	0.02
8.28	156.45	0.60	1.95	1.00	0.01	8.34	158.50	0.63	1.82	1.00	0.01
8.40	159.35	0.64	1.76	1.00	0.01	8.48	158.17	0.62	1.84	1.00	0.02
8.54	156.09	0.59	1.97	1.00	0.01	8.60	153.66	0.55	2.02	1.00	0.01
8.68	150.45	0.50	2.07	1.00	0.02	8.74	148.39	0.48	2.10	1.00	0.02
8.79	146.93	0.46	2.12	1.00	0.01	8.87	145.80	0.45	2.14	1.00	0.02
8.93	145.10	0.44	2.15	1.00	0.02	8.99	144.77	0.44	2.16	1.00	0.02
9.07	144.68	0.43	2.16	1.00	0.02	9.13	144.68	0.43	2.16	1.00	0.02
9.19	144.40	0.43	2.17	1.00	0.02	9.27	143.90	0.42	2.18	1.00	0.02
9.33	143.12	0.41	2.19	1.00	0.02	9.39	141.41	0.40	2.22	1.00	0.02
9.46	137.95	0.37	2.28	1.00	0.02	9.52	135.48	0.35	2.33	1.00	0.02
9.58	133.35	0.34	2.37	1.00	0.02	9.66	131.50	0.33	2.40	1.00	0.02
9.72	129.32	0.31	2.45	1.00	0.02	9.78	127.28	0.30	2.49	1.00	0.02
9.86	125.80	0.29	2.52	1.00	0.02	9.91	124.58	0.29	2.55	1.00	0.02
9.97	124.28	0.29	2.56	1.00	0.02	10.04	121.33	0.27	2.62	1.00	0.02
10.12	125.90	0.29	2.52	1.00	0.02	10.18	124.46	0.28	2.55	1.00	0.02
10.25	122.05	0.27	2.61	1.00	0.02	10.31	120.02	0.26	2.65	1.00	0.02
10.37	117.76	0.26	2.71	1.00	0.02	10.45	116.39	0.25	2.74	1.00	0.03
10.50	115.92	0.25	2.75	1.00	0.02	10.58	114.92	0.24	2.78	1.00	0.03
10.64	114.64	0.24	2.79	1.00	0.02	10.70	115.17	0.24	2.77	1.00	0.02
10.78	116.52	0.25	2.74	1.00	0.03	10.84	118.14	0.25	2.70	1.00	0.02
10.90	120.57	0.26	2.64	1.00	0.02	10.98	123.18	0.27	2.58	1.00	0.03
11.04	124.72	0.27	2.55	1.00	0.02	11.10	126.13	0.28	2.52	1.00	0.02
11.16	127.35	0.28	2.49	1.00	0.02	11.22	128.06	0.29	2.47	1.00	0.02
11.31	127.72	0.28	2.48	1.00	0.03	11.37	127.79	0.28	2.48	1.00	0.02
11.43	127.61	0.28	2.48	1.00	0.02	11.49	127.65	0.28	2.48	1.00	0.02
11.55	127.86	0.28	2.48	1.00	0.02	11.64	128.12	0.28	2.47	1.00	0.03
11.70	128.28	0.28	2.47	1.00	0.02	11.77	128.73	0.28	2.46	1.00	0.02
11.82	129.10	0.29	2.45	1.00	0.02	11.88	129.66	0.29	2.44	1.00	0.02
11.94	129.36	0.29	2.45	1.00	0.02	12.03	125.82	0.27	2.52	1.00	0.03
12.09	123.62	0.26	2.57	1.00	0.02	12.15	124.94	0.26	2.54	1.00	0.02
12.21	125.06	0.26	2.54	1.00	0.02	12.28	125.04	0.26	2.54	1.00	0.02
12.34	124.06	0.26	2.56	1.00	0.02	12.42	114.68	0.23	2.79	1.00	0.03
12.48	119.33	0.24	2.67	1.00	0.02	12.54	117.23	0.23	2.72	1.00	0.02
12.60	114.38	0.22	2.79	1.00	0.02	12.69	110.44	0.21	2.90	1.00	0.03
12.75	108.82	0.21	2.94	1.00	0.02	12.81	107.34	0.20	2.99	1.00	0.02
12.87	107.51	0.20	2.98	1.00	0.02	12.93	43.86	2.00	0.00	1.00	0.00
13.02	44.61	2.00	0.00	1.00	0.00	13.08	109.20	0.21	2.93	1.00	0.02
13.14	109.97	0.21	2.91	1.00	0.02	13.20	110.71	0.21	2.89	1.00	0.02
13.26	112.04	0.21	2.86	1.00	0.02	13.35	114.36	0.22	2.79	1.00	0.03
13.41	116.40	0.22	2.74	1.00	0.02	13.47	118.41	0.23	2.69	1.00	0.02
13.53	119.87	0.23	2.66	1.00	0.02	13.59	121.18	0.24	2.63	1.00	0.02
13.65	122.57	0.24	2.60	1.00	0.02	13.74	124.79	0.25	2.55	1.00	0.03
13.80	125.58	0.25	2.53	1.00	0.02	13.86	125.74	0.25	2.52	1.00	0.02
13.92	125.81	0.25	2.52	1.00	0.02	13.98	126.75	0.26	2.50	1.00	0.02
14.07	129.27	0.27	2.45	1.00	0.03	14.13	131.15	0.27	2.41	1.00	0.02
14.19	132.20	0.28	2.39	1.00	0.02	14.25	132.67	0.28	2.38	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
14.31	133.09	0.28	2.37	1.00	0.02	14.37	133.83	0.28	2.36	1.00	0.02
14.46	135.02	0.29	2.34	1.00	0.02	14.52	136.04	0.30	2.32	1.00	0.02
14.58	137.20	0.30	2.29	1.00	0.02	14.64	138.61	0.31	2.27	1.00	0.02
14.70	140.07	0.32	2.24	1.00	0.02	14.79	141.87	0.33	2.21	1.00	0.02
14.85	138.78	0.31	2.27	1.00	0.02	14.91	134.73	0.29	2.34	1.00	0.02
14.97	136.52	0.29	2.31	1.00	0.02	15.03	138.19	0.30	2.28	1.00	0.02
15.09	139.58	0.31	2.25	1.00	0.02	15.18	140.66	0.32	2.23	1.00	0.02
15.23	141.20	0.32	2.22	1.00	0.02	15.29	141.99	0.33	2.21	1.00	0.02
15.38	143.55	0.34	2.18	1.00	0.02	15.44	145.53	0.35	2.15	1.00	0.02
15.50	146.47	0.36	2.13	1.00	0.02	15.56	146.81	0.36	2.13	1.00	0.02
15.62	146.98	0.36	2.12	1.00	0.02	15.71	146.54	0.36	2.13	1.00	0.02
15.77	145.84	0.35	2.14	1.00	0.02	15.83	145.70	0.35	2.14	1.00	0.02
15.89	145.35	0.34	2.15	1.00	0.02	15.95	144.77	0.34	2.16	1.00	0.02
16.04	143.87	0.33	2.18	1.00	0.02	16.10	143.38	0.33	2.18	1.00	0.02
16.16	142.96	0.33	2.19	1.00	0.02	16.22	142.24	0.32	2.20	1.00	0.02
16.28	141.19	0.31	2.22	1.00	0.02	16.34	139.55	0.30	2.25	1.00	0.02
16.43	136.23	0.28	2.31	1.00	0.02	16.49	133.44	0.27	2.37	1.00	0.02
16.55	130.13	0.25	2.43	1.00	0.02	16.61	126.60	0.24	2.51	1.00	0.02
16.67	122.86	0.23	2.59	1.00	0.02	16.76	116.41	0.21	2.74	1.00	0.03
16.82	112.32	0.20	2.85	1.00	0.02	16.88	108.72	0.19	2.95	1.00	0.02
16.94	105.00	0.18	3.06	1.00	0.02	17.00	38.64	2.00	0.00	1.00	0.00
17.09	32.90	2.00	0.00	1.00	0.00	17.15	31.23	2.00	0.00	1.00	0.00
17.21	31.27	2.00	0.00	1.00	0.00	17.27	32.19	2.00	0.00	1.00	0.00
17.34	33.82	2.00	0.00	1.00	0.00	17.39	35.37	2.00	0.00	1.00	0.00
17.46	25.90	2.00	0.00	1.00	0.00	17.52	38.87	2.00	0.00	1.00	0.00
17.60	109.28	0.19	2.93	1.00	0.03	17.66	116.37	0.20	2.74	1.00	0.02
17.72	123.30	0.22	2.58	1.00	0.02	17.81	136.27	0.28	2.31	1.00	0.02
17.87	143.81	0.32	2.18	1.00	0.02	17.93	148.74	0.36	2.10	1.00	0.02
17.99	151.51	0.38	2.05	1.00	0.01	18.05	152.93	0.39	2.03	1.00	0.02
18.12	154.32	0.41	2.01	1.00	0.01	18.18	155.24	0.42	2.00	1.00	0.01
18.27	157.17	0.44	1.90	1.00	0.02	18.33	158.55	0.46	1.81	1.00	0.01
18.39	159.33	0.47	1.77	1.00	0.01	18.45	159.92	0.47	1.73	1.00	0.01
18.51	160.68	0.48	1.69	1.00	0.01	18.60	161.61	0.50	1.63	1.00	0.02
18.66	162.08	0.50	1.61	1.00	0.01	18.72	162.36	0.51	1.59	1.00	0.01
18.78	162.27	0.50	1.60	1.00	0.01	18.84	161.96	0.50	1.61	1.00	0.01
18.90	161.39	0.49	1.65	1.00	0.01	18.99	159.91	0.47	1.73	1.00	0.02
19.05	159.08	0.46	1.78	1.00	0.01	19.11	157.84	0.44	1.86	1.00	0.01
19.17	156.87	0.43	1.92	1.00	0.01	19.23	156.13	0.42	1.97	1.00	0.01
19.32	153.92	0.40	2.02	1.00	0.02	19.38	152.14	0.38	2.04	1.00	0.01
19.44	149.88	0.36	2.08	1.00	0.01	19.50	142.77	0.30	2.19	1.00	0.02
19.56	130.25	0.24	2.43	1.00	0.02	19.65	120.04	0.21	2.65	1.00	0.03
19.71	113.64	0.19	2.81	1.00	0.02	19.77	105.20	0.17	3.05	1.00	0.02
19.83	34.44	2.00	0.00	1.00	0.00	19.89	25.94	2.00	0.00	1.00	0.00
19.95	26.14	2.00	0.00	1.00	0.00	20.01	25.73	2.00	0.00	1.00	0.00
20.09	25.56	2.00	0.00	1.00	0.00	20.15	24.11	2.00	0.00	1.00	0.00
20.21	22.33	2.00	0.00	1.00	0.00	20.30	21.20	2.00	0.00	1.00	0.00
20.36	21.25	2.00	0.00	1.00	0.00	20.42	21.30	2.00	0.00	1.00	0.00
20.48	20.77	2.00	0.00	1.00	0.00	20.54	20.00	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
20.63	20.81	2.00	0.00	1.00	0.00	20.69	19.84	2.00	0.00	1.00	0.00
20.75	20.87	2.00	0.00	1.00	0.00	20.81	21.89	2.00	0.00	1.00	0.00
20.87	23.17	2.00	0.00	1.00	0.00	20.93	24.76	2.00	0.00	1.00	0.00
21.02	27.72	2.00	0.00	1.00	0.00	21.08	29.47	2.00	0.00	1.00	0.00
21.14	31.22	2.00	0.00	1.00	0.00	21.20	32.88	2.00	0.00	1.00	0.00
21.26	95.34	0.15	3.37	1.00	0.02	21.35	99.22	0.16	3.24	1.00	0.03
21.41	101.01	0.16	3.18	1.00	0.02	21.47	102.20	0.16	3.14	1.00	0.02
21.53	103.02	0.16	3.12	1.00	0.02	21.59	39.46	2.00	0.00	1.00	0.00
21.66	39.16	2.00	0.00	1.00	0.00	21.72	38.06	2.00	0.00	1.00	0.00
21.79	36.06	2.00	0.00	1.00	0.00	21.86	34.88	2.00	0.00	1.00	0.00
21.92	33.86	2.00	0.00	1.00	0.00	22.00	32.27	2.00	0.00	1.00	0.00
22.06	31.43	2.00	0.00	1.00	0.00	22.13	31.21	2.00	0.00	1.00	0.00
22.18	31.17	2.00	0.00	1.00	0.00	22.26	31.11	2.00	0.00	1.00	0.00
22.32	31.06	2.00	0.00	1.00	0.00	22.39	31.02	2.00	0.00	1.00	0.00
22.46	31.60	2.00	0.00	1.00	0.00	22.52	31.64	2.00	0.00	1.00	0.00
22.60	31.73	2.00	0.00	1.00	0.00	22.64	31.78	2.00	0.00	1.00	0.00
22.71	31.90	2.00	0.00	1.00	0.00	22.77	31.60	2.00	0.00	1.00	0.00
22.84	30.45	2.00	0.00	1.00	0.00	22.93	31.57	2.00	0.00	1.00	0.00
22.98	30.58	2.00	0.00	1.00	0.00	23.04	31.56	2.00	0.00	1.00	0.00
23.12	33.84	2.00	0.00	1.00	0.00	23.17	98.70	0.15	3.26	1.00	0.02
23.26	105.69	0.17	3.04	1.00	0.03	23.32	111.56	0.18	2.87	1.00	0.02
23.38	117.12	0.19	2.72	1.00	0.02	23.44	120.78	0.20	2.64	1.00	0.02
23.49	121.54	0.20	2.62	1.00	0.02	23.56	124.76	0.21	2.55	1.00	0.02
23.63	127.65	0.22	2.48	1.00	0.02	23.69	130.25	0.23	2.43	1.00	0.02
23.75	134.21	0.24	2.35	1.00	0.02	23.84	136.70	0.26	2.30	1.00	0.02
23.89	137.59	0.26	2.29	1.00	0.01	23.96	139.80	0.27	2.25	1.00	0.02
24.02	141.24	0.28	2.22	1.00	0.02	24.10	142.11	0.28	2.21	1.00	0.02
24.16	142.64	0.29	2.20	1.00	0.02	24.23	142.61	0.29	2.20	1.00	0.02
24.29	142.41	0.28	2.20	1.00	0.02	24.36	141.67	0.28	2.21	1.00	0.02
24.41	140.15	0.27	2.24	1.00	0.02	24.50	137.21	0.26	2.29	1.00	0.02
24.56	134.74	0.24	2.34	1.00	0.02	24.62	131.11	0.23	2.41	1.00	0.02
24.68	126.52	0.21	2.51	1.00	0.02	24.75	121.12	0.20	2.63	1.00	0.02
24.80	114.62	0.18	2.79	1.00	0.02	24.89	39.41	2.00	0.00	1.00	0.00
24.95	31.81	2.00	0.00	1.00	0.00	25.01	26.03	2.00	0.00	1.00	0.00
25.07	21.73	2.00	0.00	1.00	0.00	25.14	18.80	2.00	0.00	1.00	0.00
25.22	16.40	2.00	0.00	1.00	0.00	25.28	14.99	2.00	0.00	1.00	0.00
25.34	14.31	2.00	0.00	1.00	0.00	25.40	14.14	2.00	0.00	1.00	0.00
25.46	14.20	2.00	0.00	1.00	0.00	25.53	14.33	2.00	0.00	1.00	0.00
25.62	14.73	2.00	0.00	1.00	0.00	25.67	14.07	2.00	0.00	1.00	0.00
25.73	16.09	2.00	0.00	1.00	0.00	25.79	17.08	2.00	0.00	1.00	0.00
25.87	19.62	2.00	0.00	1.00	0.00	25.94	31.41	2.00	0.00	1.00	0.00
25.98	40.33	2.00	0.00	1.00	0.00	26.07	119.51	0.19	2.67	1.00	0.03
26.14	129.87	0.22	2.44	1.00	0.02	26.20	137.45	0.25	2.29	1.00	0.02
26.26	139.73	0.26	2.25	1.00	0.02	26.32	138.03	0.26	2.28	1.00	0.02
26.41	129.94	0.22	2.44	1.00	0.03	26.47	122.77	0.20	2.59	1.00	0.02
26.53	113.97	0.18	2.80	1.00	0.02	26.59	41.14	2.00	0.00	1.00	0.00
26.64	33.78	2.00	0.00	1.00	0.00	26.73	25.99	2.00	0.00	1.00	0.00
26.79	22.33	2.00	0.00	1.00	0.00	26.86	19.63	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
26.92	18.45	2.00	0.00	1.00	0.00	26.98	17.72	2.00	0.00	1.00	0.00
27.04	16.98	2.00	0.00	1.00	0.00	27.12	15.54	2.00	0.00	1.00	0.00
27.19	15.52	2.00	0.00	1.00	0.00	27.25	15.50	2.00	0.00	1.00	0.00
27.30	17.67	2.00	0.00	1.00	0.00	27.37	21.21	2.00	0.00	1.00	0.00
27.46	28.87	2.00	0.00	1.00	0.00	27.52	38.05	2.00	0.00	1.00	0.00
27.58	110.43	0.17	2.90	1.00	0.02	27.64	118.19	0.19	2.70	1.00	0.02
27.70	124.74	0.20	2.55	1.00	0.02	27.76	128.12	0.21	2.47	1.00	0.02
27.82	127.41	0.21	2.49	1.00	0.02	27.89	116.92	0.18	2.73	1.00	0.02
27.96	118.43	0.19	2.69	1.00	0.02	28.02	114.27	0.18	2.80	1.00	0.02
28.09	108.30	0.16	2.96	1.00	0.03	28.16	104.71	0.16	3.06	1.00	0.02
28.23	40.26	2.00	0.00	1.00	0.00	28.28	39.93	2.00	0.00	1.00	0.00
28.35	40.35	2.00	0.00	1.00	0.00	28.43	41.24	2.00	0.00	1.00	0.00
28.49	41.56	2.00	0.00	1.00	0.00	28.55	42.90	2.00	0.00	1.00	0.00
28.61	45.13	2.00	0.00	1.00	0.00	28.70	112.88	0.17	2.83	1.00	0.03
28.76	115.08	0.18	2.78	1.00	0.02	28.82	116.46	0.18	2.74	1.00	0.02
28.88	117.35	0.18	2.72	1.00	0.02	28.94	118.36	0.18	2.69	1.00	0.02
29.03	119.99	0.19	2.66	1.00	0.03	29.09	120.88	0.19	2.63	1.00	0.02
29.15	121.67	0.19	2.62	1.00	0.02	29.21	122.29	0.19	2.60	1.00	0.02
29.27	122.61	0.19	2.59	1.00	0.02	29.33	122.76	0.20	2.59	1.00	0.02
29.42	122.77	0.20	2.59	1.00	0.03	29.48	122.46	0.19	2.60	1.00	0.02
29.54	121.58	0.19	2.62	1.00	0.02	29.60	120.50	0.19	2.64	1.00	0.02
29.66	119.03	0.19	2.68	1.00	0.02	29.75	115.69	0.18	2.76	1.00	0.03
29.81	113.04	0.17	2.83	1.00	0.02	29.87	109.62	0.16	2.92	1.00	0.02
29.93	105.07	0.16	3.05	1.00	0.02	29.99	36.83	2.00	0.00	1.00	0.00
30.05	27.55	2.00	0.00	1.00	0.00	30.12	22.77	2.00	0.00	1.00	0.00
30.19	19.65	2.00	0.00	1.00	0.00	30.26	17.94	2.00	0.00	1.00	0.00
30.33	15.89	2.00	0.00	1.00	0.00	30.39	13.14	2.00	0.00	1.00	0.00
30.45	11.15	2.00	0.00	1.00	0.00	30.52	10.15	2.00	0.00	1.00	0.00
30.58	9.88	2.00	0.00	1.00	0.00	30.65	9.55	2.00	0.00	1.00	0.00
30.71	9.01	2.00	0.00	1.00	0.00	30.78	9.19	2.00	0.00	1.00	0.00
30.85	8.99	2.00	0.00	1.00	0.00	30.92	8.85	2.00	0.00	1.00	0.00
30.97	8.84	2.00	0.00	1.00	0.00	31.04	8.83	2.00	0.00	1.00	0.00
31.11	9.02	2.00	0.00	1.00	0.00	31.17	9.01	2.00	0.00	1.00	0.00
31.25	9.32	2.00	0.00	1.00	0.00	31.30	9.11	2.00	0.00	1.00	0.00
31.37	9.87	2.00	0.00	1.00	0.00	31.44	8.64	2.00	0.00	1.00	0.00
31.51	9.97	2.00	0.00	1.00	0.00	31.57	9.58	2.00	0.00	1.00	0.00
31.63	9.76	2.00	0.00	1.00	0.00	31.70	9.75	2.00	0.00	1.00	0.00
31.79	9.73	2.00	0.00	1.00	0.00	31.85	9.72	2.00	0.00	1.00	0.00
31.91	9.97	2.00	0.00	1.00	0.00	31.97	10.02	2.00	0.00	1.00	0.00
32.03	10.27	2.00	0.00	1.00	0.00	32.09	10.51	2.00	0.00	1.00	0.00
32.18	10.94	2.00	0.00	1.00	0.00	32.24	11.00	2.00	0.00	1.00	0.00
32.30	11.24	2.00	0.00	1.00	0.00	32.35	10.34	2.00	0.00	1.00	0.00
32.43	11.72	2.00	0.00	1.00	0.00	32.50	12.92	2.00	0.00	1.00	0.00
32.56	13.04	2.00	0.00	1.00	0.00	32.62	12.90	2.00	0.00	1.00	0.00
32.69	12.94	2.00	0.00	1.00	0.00	32.75	13.44	2.00	0.00	1.00	0.00
32.83	14.64	2.00	0.00	1.00	0.00	32.88	15.47	2.00	0.00	1.00	0.00
32.96	15.57	2.00	0.00	1.00	0.00	33.02	14.91	2.00	0.00	1.00	0.00
33.08	14.19	2.00	0.00	1.00	0.00	33.14	13.92	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
33.23	13.45	2.00	0.00	1.00	0.00	33.28	13.13	2.00	0.00	1.00	0.00
33.36	12.92	2.00	0.00	1.00	0.00	33.41	12.53	2.00	0.00	1.00	0.00
33.48	12.27	2.00	0.00	1.00	0.00	33.55	12.06	2.00	0.00	1.00	0.00
33.61	11.49	2.00	0.00	1.00	0.00	33.67	11.47	2.00	0.00	1.00	0.00
33.74	11.65	2.00	0.00	1.00	0.00	33.80	11.76	2.00	0.00	1.00	0.00
33.88	12.37	2.00	0.00	1.00	0.00	33.94	12.48	2.00	0.00	1.00	0.00
34.00	12.60	2.00	0.00	1.00	0.00	34.06	13.52	2.00	0.00	1.00	0.00
34.15	14.76	2.00	0.00	1.00	0.00	34.21	15.75	2.00	0.00	1.00	0.00
34.27	14.79	2.00	0.00	1.00	0.00	34.33	13.71	2.00	0.00	1.00	0.00
34.39	12.26	2.00	0.00	1.00	0.00	34.45	10.95	2.00	0.00	1.00	0.00
34.52	10.27	2.00	0.00	1.00	0.00	34.61	9.76	2.00	0.00	1.00	0.00
34.67	9.14	2.00	0.00	1.00	0.00	34.73	8.77	2.00	0.00	1.00	0.00
34.79	8.82	2.00	0.00	1.00	0.00	34.85	8.88	2.00	0.00	1.00	0.00
34.93	8.98	2.00	0.00	1.00	0.00	34.98	9.16	2.00	0.00	1.00	0.00
35.07	9.51	2.00	0.00	1.00	0.00	35.13	9.68	2.00	0.00	1.00	0.00
35.19	9.85	2.00	0.00	1.00	0.00	35.25	9.84	2.00	0.00	1.00	0.00
35.31	9.83	2.00	0.00	1.00	0.00	35.37	9.82	2.00	0.00	1.00	0.00
35.43	9.82	2.00	0.00	1.00	0.00	35.52	9.98	2.00	0.00	1.00	0.00
35.58	10.15	2.00	0.00	1.00	0.00	35.64	10.32	2.00	0.00	1.00	0.00
35.70	10.50	2.00	0.00	1.00	0.00	35.76	10.54	2.00	0.00	1.00	0.00
35.85	10.59	2.00	0.00	1.00	0.00	35.91	10.82	2.00	0.00	1.00	0.00
35.97	11.05	2.00	0.00	1.00	0.00	36.03	11.34	2.00	0.00	1.00	0.00
36.09	11.81	2.00	0.00	1.00	0.00	36.18	12.77	2.00	0.00	1.00	0.00
36.24	14.22	2.00	0.00	1.00	0.00	36.30	15.98	2.00	0.00	1.00	0.00
36.36	17.26	2.00	0.00	1.00	0.00	36.42	18.30	2.00	0.00	1.00	0.00
36.51	19.89	2.00	0.00	1.00	0.00	36.57	19.94	2.00	0.00	1.00	0.00
36.63	19.35	2.00	0.00	1.00	0.00	36.69	18.41	2.00	0.00	1.00	0.00
36.75	18.20	2.00	0.00	1.00	0.00	36.81	20.15	2.00	0.00	1.00	0.00
36.91	26.13	2.00	0.00	1.00	0.00	36.97	29.94	2.00	0.00	1.00	0.00
37.03	32.43	2.00	0.00	1.00	0.00	37.08	30.69	2.00	0.00	1.00	0.00
37.15	28.05	2.00	0.00	1.00	0.00	37.21	24.24	2.00	0.00	1.00	0.00
37.29	20.21	2.00	0.00	1.00	0.00	37.34	18.40	2.00	0.00	1.00	0.00
37.43	15.88	2.00	0.00	1.00	0.00	37.48	14.36	2.00	0.00	1.00	0.00
37.55	13.50	2.00	0.00	1.00	0.00	37.62	14.09	2.00	0.00	1.00	0.00
37.67	14.80	2.00	0.00	1.00	0.00	37.74	16.04	2.00	0.00	1.00	0.00
37.81	17.48	2.00	0.00	1.00	0.00	37.86	18.63	2.00	0.00	1.00	0.00
37.94	20.56	2.00	0.00	1.00	0.00	38.02	21.96	2.00	0.00	1.00	0.00
38.07	22.44	2.00	0.00	1.00	0.00	38.13	22.48	2.00	0.00	1.00	0.00
38.22	21.70	2.00	0.00	1.00	0.00	38.28	21.93	2.00	0.00	1.00	0.00
38.34	23.15	2.00	0.00	1.00	0.00	38.40	25.18	2.00	0.00	1.00	0.00
38.47	32.09	2.00	0.00	1.00	0.00	38.53	34.42	2.00	0.00	1.00	0.00
38.59	38.12	2.00	0.00	1.00	0.00	38.68	46.07	2.00	0.00	1.00	0.00
38.74	116.04	0.17	2.75	1.00	0.02	38.80	119.09	0.18	2.68	1.00	0.02
38.85	119.33	0.18	2.67	1.00	0.02	38.93	118.01	0.18	2.70	1.00	0.02
38.98	117.57	0.18	2.71	1.00	0.02	39.04	117.02	0.17	2.73	1.00	0.02
39.11	119.92	0.18	2.66	1.00	0.02	39.20	50.87	2.00	0.00	1.00	0.00
39.26	48.44	2.00	0.00	1.00	0.00	39.32	44.57	2.00	0.00	1.00	0.00
39.38	41.26	2.00	0.00	1.00	0.00	39.44	39.40	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
39.53	38.48	2.00	0.00	1.00	0.00	39.59	34.87	2.00	0.00	1.00	0.00
39.65	29.29	2.00	0.00	1.00	0.00	39.71	25.04	2.00	0.00	1.00	0.00
39.77	22.16	2.00	0.00	1.00	0.00	39.86	19.42	2.00	0.00	1.00	0.00
39.92	18.76	2.00	0.00	1.00	0.00	39.98	20.00	2.00	0.00	1.00	0.00
40.04	23.94	2.00	0.00	1.00	0.00	40.10	25.03	2.00	0.00	1.00	0.00
40.16	117.96	0.18	2.70	1.00	0.02	40.22	142.45	0.26	2.20	1.00	0.02
40.30	156.73	0.36	1.93	1.00	0.02	40.37	166.81	0.49	1.37	1.00	0.01
40.43	170.24	0.54	1.21	1.00	0.01	40.51	174.24	0.63	1.05	1.00	0.01
40.57	176.59	0.68	0.97	1.00	0.01	40.63	178.39	0.73	0.91	1.00	0.01
40.69	180.04	0.78	0.86	1.00	0.01	40.78	182.72	0.87	0.78	1.00	0.01
40.84	183.10	0.89	0.77	1.00	0.01	40.90	182.81	0.88	0.77	1.00	0.01
40.95	182.77	0.87	0.78	1.00	0.01	41.01	183.17	0.89	0.76	1.00	0.01
41.10	182.88	0.88	0.77	1.00	0.01	41.16	182.96	0.88	0.77	1.00	0.01
41.22	182.95	0.88	0.77	1.00	0.01	41.28	183.22	0.89	0.76	1.00	0.01
41.34	184.25	0.93	0.73	1.00	0.01	41.41	186.27	1.02	0.68	1.00	0.01
41.49	189.71	1.19	0.49	1.00	0.01	41.55	191.66	1.30	0.39	1.00	0.00
41.61	193.41	1.42	0.30	1.00	0.00	41.68	195.14	1.55	0.22	1.00	0.00
41.73	196.92	1.69	0.13	1.00	0.00	41.83	200.28	2.00	0.00	1.00	0.00
41.89	202.50	2.00	0.00	1.00	0.00	41.95	205.07	2.00	0.00	1.00	0.00
42.01	207.11	2.00	0.00	1.00	0.00	42.06	208.25	2.00	0.00	1.00	0.00
42.16	207.25	2.00	0.00	1.00	0.00	42.22	205.75	2.00	0.00	1.00	0.00
42.28	203.56	2.00	0.00	1.00	0.00	42.34	200.70	2.00	0.00	1.00	0.00
42.40	197.74	1.77	0.10	1.00	0.00	42.48	186.88	1.04	0.65	1.00	0.01
42.54	188.58	1.12	0.55	1.00	0.00	42.60	185.17	0.97	0.71	1.00	0.01
42.66	181.60	0.83	0.81	1.00	0.01	42.72	177.92	0.72	0.92	1.00	0.01
42.78	174.27	0.62	1.05	1.00	0.01	42.87	170.23	0.54	1.21	1.00	0.01
42.93	168.07	0.50	1.31	1.00	0.01	42.99	167.13	0.49	1.35	1.00	0.01
43.05	166.63	0.48	1.38	1.00	0.01	43.11	166.54	0.48	1.38	1.00	0.01
43.20	166.67	0.48	1.37	1.00	0.01	43.26	166.44	0.48	1.38	1.00	0.01
43.32	166.36	0.48	1.39	1.00	0.01	43.38	165.96	0.47	1.41	1.00	0.01
43.44	164.47	0.45	1.48	1.00	0.01	43.51	162.72	0.43	1.57	1.00	0.01
43.59	159.83	0.39	1.74	1.00	0.02	43.65	157.82	0.37	1.86	1.00	0.01
43.71	155.52	0.35	1.99	1.00	0.01	43.77	153.24	0.33	2.03	1.00	0.01
43.83	150.47	0.31	2.07	1.00	0.01	43.92	145.43	0.28	2.15	1.00	0.02
43.98	141.16	0.25	2.22	1.00	0.02	44.05	135.48	0.23	2.33	1.00	0.02
44.10	128.44	0.20	2.47	1.00	0.02	44.16	120.94	0.18	2.63	1.00	0.02
44.23	48.95	2.00	0.00	1.00	0.00	44.32	42.40	2.00	0.00	1.00	0.00
44.38	39.18	2.00	0.00	1.00	0.00	44.43	35.82	2.00	0.00	1.00	0.00
44.49	40.57	2.00	0.00	1.00	0.00	44.57	40.29	2.00	0.00	1.00	0.00
44.63	40.56	2.00	0.00	1.00	0.00	44.70	39.01	2.00	0.00	1.00	0.00
44.77	40.55	2.00	0.00	1.00	0.00	44.82	41.51	2.00	0.00	1.00	0.00
44.88	43.77	2.00	0.00	1.00	0.00	44.97	48.51	2.00	0.00	1.00	0.00
45.03	121.90	0.19	2.61	1.00	0.02	45.10	131.24	0.21	2.41	1.00	0.02
45.16	138.29	0.24	2.27	1.00	0.02	45.22	141.52	0.26	2.22	1.00	0.02
45.28	143.01	0.26	2.19	1.00	0.02	45.37	145.49	0.28	2.15	1.00	0.02
45.43	147.34	0.29	2.12	1.00	0.02	45.49	149.38	0.30	2.09	1.00	0.02
45.55	151.72	0.32	2.05	1.00	0.01	45.61	155.12	0.35	2.00	1.00	0.01
45.67	158.52	0.38	1.81	1.00	0.01	45.76	160.91	0.40	1.67	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
45.82	160.31	0.40	1.71	1.00	0.01	45.88	158.06	0.37	1.84	1.00	0.01
45.94	155.15	0.35	2.00	1.00	0.01	46.00	151.48	0.32	2.05	1.00	0.01
46.09	146.54	0.28	2.13	1.00	0.02	46.15	144.19	0.27	2.17	1.00	0.02
46.21	141.54	0.26	2.22	1.00	0.02	46.27	138.67	0.24	2.27	1.00	0.02
46.33	135.42	0.23	2.33	1.00	0.02	46.42	131.26	0.21	2.41	1.00	0.03
46.48	127.14	0.20	2.49	1.00	0.02	46.54	122.97	0.19	2.59	1.00	0.02
46.60	123.37	0.19	2.58	1.00	0.02	46.66	124.09	0.19	2.56	1.00	0.02
46.72	124.13	0.19	2.56	1.00	0.02	46.80	119.26	0.18	2.67	1.00	0.02
46.86	121.17	0.18	2.63	1.00	0.02	46.93	121.50	0.19	2.62	1.00	0.02
46.98	120.70	0.18	2.64	1.00	0.02	47.07	116.91	0.17	2.73	1.00	0.03
47.13	113.59	0.17	2.81	1.00	0.02	47.19	110.35	0.16	2.90	1.00	0.02
47.25	43.28	2.00	0.00	1.00	0.00	47.31	40.31	2.00	0.00	1.00	0.00
47.40	35.80	2.00	0.00	1.00	0.00	47.46	32.24	2.00	0.00	1.00	0.00
47.52	27.82	2.00	0.00	1.00	0.00	47.58	23.81	2.00	0.00	1.00	0.00
47.64	20.57	2.00	0.00	1.00	0.00	47.73	17.01	2.00	0.00	1.00	0.00
47.79	15.55	2.00	0.00	1.00	0.00	47.85	16.07	2.00	0.00	1.00	0.00
47.91	18.54	2.00	0.00	1.00	0.00	47.97	21.94	2.00	0.00	1.00	0.00
48.03	25.55	2.00	0.00	1.00	0.00	48.12	27.99	2.00	0.00	1.00	0.00
48.18	28.03	2.00	0.00	1.00	0.00	48.24	26.63	2.00	0.00	1.00	0.00
48.30	24.24	2.00	0.00	1.00	0.00	48.36	21.60	2.00	0.00	1.00	0.00
48.45	18.69	2.00	0.00	1.00	0.00	48.51	18.76	2.00	0.00	1.00	0.00
48.57	18.74	2.00	0.00	1.00	0.00	48.63	18.81	2.00	0.00	1.00	0.00
48.69	19.77	2.00	0.00	1.00	0.00	48.78	18.82	2.00	0.00	1.00	0.00
48.84	17.74	2.00	0.00	1.00	0.00	48.90	17.25	2.00	0.00	1.00	0.00
48.96	17.77	2.00	0.00	1.00	0.00	49.03	18.40	2.00	0.00	1.00	0.00
49.09	18.93	2.00	0.00	1.00	0.00	49.15	16.25	2.00	0.00	1.00	0.00
49.21	31.89	2.00	0.00	1.00	0.00	49.30	43.06	2.00	0.00	1.00	0.00
49.36	119.98	0.18	2.66	1.00	0.02	49.42	127.03	0.20	2.50	1.00	0.02
49.48	137.33	0.24	2.29	1.00	0.02	49.55	148.75	0.30	2.10	1.00	0.02
49.61	156.40	0.36	1.95	1.00	0.01	49.70	153.70	0.33	2.02	1.00	0.02
49.76	152.81	0.33	2.03	1.00	0.01	49.82	157.44	0.37	1.88	1.00	0.01
49.88	161.49	0.41	1.64	1.00	0.01	49.94	164.61	0.45	1.47	1.00	0.01
50.00	166.12	2.00	0.00	1.00	0.00	50.07	160.63	2.00	0.00	1.00	0.00
50.14	164.45	2.00	0.00	1.00	0.00	50.20	165.96	2.00	0.00	1.00	0.00
50.27	164.87	2.00	0.00	1.00	0.00	50.34	154.95	2.00	0.00	1.00	0.00
50.41	163.45	2.00	0.00	1.00	0.00	50.46	163.88	2.00	0.00	1.00	0.00
50.54	163.34	2.00	0.00	1.00	0.00	50.61	163.00	2.00	0.00	1.00	0.00
50.67	162.60	2.00	0.00	1.00	0.00	50.74	160.67	2.00	0.00	1.00	0.00
50.79	162.90	2.00	0.00	1.00	0.00	50.85	163.42	2.00	0.00	1.00	0.00
50.94	164.12	2.00	0.00	1.00	0.00	51.01	164.76	2.00	0.00	1.00	0.00
51.06	164.90	2.00	0.00	1.00	0.00	51.13	165.12	2.00	0.00	1.00	0.00
51.18	166.14	2.00	0.00	1.00	0.00	51.27	167.60	2.00	0.00	1.00	0.00
51.33	168.32	2.00	0.00	1.00	0.00	51.38	167.72	2.00	0.00	1.00	0.00
51.46	167.24	2.00	0.00	1.00	0.00	51.52	167.04	2.00	0.00	1.00	0.00
51.58	165.40	2.00	0.00	1.00	0.00	51.64	163.10	2.00	0.00	1.00	0.00
51.73	166.53	2.00	0.00	1.00	0.00	51.79	169.79	2.00	0.00	1.00	0.00
51.85	174.16	2.00	0.00	1.00	0.00	51.91	178.55	2.00	0.00	1.00	0.00
51.98	170.46	2.00	0.00	1.00	0.00	52.05	183.57	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
52.10	184.53	2.00	0.00	1.00	0.00	52.18	184.39	2.00	0.00	1.00	0.00
52.23	183.85	2.00	0.00	1.00	0.00	52.31	182.97	2.00	0.00	1.00	0.00
52.36	181.30	2.00	0.00	1.00	0.00	52.44	179.09	2.00	0.00	1.00	0.00
52.51	176.32	2.00	0.00	1.00	0.00	52.57	174.30	2.00	0.00	1.00	0.00
52.63	172.97	2.00	0.00	1.00	0.00	52.72	168.60	2.00	0.00	1.00	0.00
52.77	165.48	2.00	0.00	1.00	0.00	52.84	162.44	2.00	0.00	1.00	0.00
52.90	159.58	2.00	0.00	1.00	0.00	52.95	156.89	2.00	0.00	1.00	0.00
53.04	152.79	2.00	0.00	1.00	0.00	53.10	150.83	2.00	0.00	1.00	0.00
53.16	149.23	2.00	0.00	1.00	0.00	53.23	147.85	2.00	0.00	1.00	0.00
53.29	146.89	2.00	0.00	1.00	0.00	53.35	146.06	2.00	0.00	1.00	0.00
53.44	144.30	2.00	0.00	1.00	0.00	53.50	142.60	2.00	0.00	1.00	0.00
53.56	139.20	2.00	0.00	1.00	0.00	53.62	135.49	2.00	0.00	1.00	0.00
53.67	135.48	2.00	0.00	1.00	0.00	53.76	133.71	2.00	0.00	1.00	0.00
53.82	134.90	2.00	0.00	1.00	0.00	53.88	133.55	2.00	0.00	1.00	0.00
53.94	131.68	2.00	0.00	1.00	0.00	54.00	131.01	2.00	0.00	1.00	0.00
54.09	129.00	2.00	0.00	1.00	0.00	54.16	127.62	2.00	0.00	1.00	0.00
54.22	125.82	2.00	0.00	1.00	0.00	54.27	121.57	2.00	0.00	1.00	0.00
54.34	122.56	2.00	0.00	1.00	0.00	54.41	123.33	2.00	0.00	1.00	0.00
54.47	125.00	2.00	0.00	1.00	0.00	54.56	127.71	2.00	0.00	1.00	0.00
54.62	128.78	2.00	0.00	1.00	0.00	54.68	128.18	2.00	0.00	1.00	0.00
54.74	127.32	2.00	0.00	1.00	0.00	54.80	126.30	2.00	0.00	1.00	0.00
54.86	125.01	2.00	0.00	1.00	0.00	54.95	122.62	2.00	0.00	1.00	0.00
55.01	121.10	2.00	0.00	1.00	0.00	55.07	119.40	2.00	0.00	1.00	0.00
55.13	118.52	2.00	0.00	1.00	0.00	55.19	119.58	2.00	0.00	1.00	0.00
55.28	119.24	2.00	0.00	1.00	0.00	55.34	119.39	2.00	0.00	1.00	0.00
55.40	119.90	2.00	0.00	1.00	0.00	55.45	120.66	2.00	0.00	1.00	0.00
55.51	120.83	2.00	0.00	1.00	0.00	55.60	120.68	2.00	0.00	1.00	0.00
55.66	120.21	2.00	0.00	1.00	0.00	55.73	119.76	2.00	0.00	1.00	0.00
55.79	119.55	2.00	0.00	1.00	0.00	55.84	120.72	2.00	0.00	1.00	0.00
55.94	126.80	2.00	0.00	1.00	0.00	56.00	131.99	2.00	0.00	1.00	0.00
56.06	137.12	2.00	0.00	1.00	0.00	56.12	139.82	2.00	0.00	1.00	0.00
56.18	142.39	2.00	0.00	1.00	0.00	56.24	144.17	2.00	0.00	1.00	0.00
56.30	144.65	2.00	0.00	1.00	0.00	56.39	145.86	2.00	0.00	1.00	0.00
56.43	146.00	2.00	0.00	1.00	0.00	56.50	146.49	2.00	0.00	1.00	0.00
56.56	148.75	2.00	0.00	1.00	0.00	56.65	150.56	2.00	0.00	1.00	0.00
56.71	151.45	2.00	0.00	1.00	0.00	56.77	151.88	2.00	0.00	1.00	0.00
56.84	152.15	2.00	0.00	1.00	0.00	56.89	152.48	2.00	0.00	1.00	0.00
56.98	153.48	2.00	0.00	1.00	0.00	57.04	154.36	2.00	0.00	1.00	0.00
57.10	155.27	2.00	0.00	1.00	0.00	57.16	156.28	2.00	0.00	1.00	0.00
57.22	157.61	2.00	0.00	1.00	0.00	57.31	160.80	2.00	0.00	1.00	0.00
57.37	163.08	2.00	0.00	1.00	0.00	57.43	165.77	2.00	0.00	1.00	0.00
57.49	168.17	2.00	0.00	1.00	0.00	57.55	170.10	2.00	0.00	1.00	0.00
57.61	171.42	2.00	0.00	1.00	0.00	57.70	173.26	2.00	0.00	1.00	0.00
57.76	174.45	2.00	0.00	1.00	0.00	57.82	175.95	2.00	0.00	1.00	0.00
57.88	177.23	2.00	0.00	1.00	0.00	57.94	178.90	2.00	0.00	1.00	0.00
58.03	181.51	2.00	0.00	1.00	0.00	58.09	183.39	2.00	0.00	1.00	0.00
58.16	185.22	2.00	0.00	1.00	0.00	58.22	187.43	2.00	0.00	1.00	0.00
58.28	190.05	2.00	0.00	1.00	0.00	58.34	192.55	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
58.42	195.99	2.00	0.00	1.00	0.00	58.48	198.00	2.00	0.00	1.00	0.00
58.55	199.80	2.00	0.00	1.00	0.00	58.60	201.74	2.00	0.00	1.00	0.00
58.67	203.40	2.00	0.00	1.00	0.00	58.75	205.65	2.00	0.00	1.00	0.00
58.81	208.28	2.00	0.00	1.00	0.00	58.87	195.68	2.00	0.00	1.00	0.00
58.94	169.36	2.00	0.00	1.00	0.00	59.00	176.48	2.00	0.00	1.00	0.00
59.06	182.51	2.00	0.00	1.00	0.00	59.15	189.48	2.00	0.00	1.00	0.00
59.20	192.22	2.00	0.00	1.00	0.00	59.27	194.93	2.00	0.00	1.00	0.00
59.32	196.83	2.00	0.00	1.00	0.00	59.40	201.15	2.00	0.00	1.00	0.00
59.46	205.89	2.00	0.00	1.00	0.00	59.53	210.45	2.00	0.00	1.00	0.00
59.58	213.52	2.00	0.00	1.00	0.00	59.66	216.88	2.00	0.00	1.00	0.00
59.73	220.33	2.00	0.00	1.00	0.00	59.79	199.99	2.00	0.00	1.00	0.00
59.86	146.71	2.00	0.00	1.00	0.00	59.93	147.65	2.00	0.00	1.00	0.00
59.98	147.16	2.00	0.00	1.00	0.00	60.05	146.34	2.00	0.00	1.00	0.00
60.12	144.50	2.00	0.00	1.00	0.00	60.19	154.57	2.00	0.00	1.00	0.00
60.24	164.21	2.00	0.00	1.00	0.00	60.32	184.30	2.00	0.00	1.00	0.00
60.38	192.75	2.00	0.00	1.00	0.00	60.44	197.32	2.00	0.00	1.00	0.00
60.50	200.72	2.00	0.00	1.00	0.00	60.59	204.10	2.00	0.00	1.00	0.00
60.65	205.42	2.00	0.00	1.00	0.00	60.71	205.78	2.00	0.00	1.00	0.00
60.77	205.49	2.00	0.00	1.00	0.00	60.83	204.94	2.00	0.00	1.00	0.00
60.89	205.17	2.00	0.00	1.00	0.00	60.98	206.90	2.00	0.00	1.00	0.00
61.04	207.71	2.00	0.00	1.00	0.00	61.10	208.75	2.00	0.00	1.00	0.00
61.16	210.04	2.00	0.00	1.00	0.00	61.22	211.18	2.00	0.00	1.00	0.00
61.31	211.13	2.00	0.00	1.00	0.00	61.37	211.29	2.00	0.00	1.00	0.00
61.43	211.91	2.00	0.00	1.00	0.00	61.49	212.49	2.00	0.00	1.00	0.00
61.55	212.82	2.00	0.00	1.00	0.00	61.64	212.72	2.00	0.00	1.00	0.00
61.70	212.45	2.00	0.00	1.00	0.00	61.76	212.11	2.00	0.00	1.00	0.00
61.82	206.06	2.00	0.00	1.00	0.00	61.88	188.44	2.00	0.00	1.00	0.00
61.94	191.91	2.00	0.00	1.00	0.00	62.04	193.44	2.00	0.00	1.00	0.00
62.10	194.24	2.00	0.00	1.00	0.00	62.16	194.45	2.00	0.00	1.00	0.00
62.22	194.41	2.00	0.00	1.00	0.00	62.29	192.09	2.00	0.00	1.00	0.00
62.34	189.04	2.00	0.00	1.00	0.00	62.43	187.93	2.00	0.00	1.00	0.00
62.49	187.90	2.00	0.00	1.00	0.00	62.55	188.52	2.00	0.00	1.00	0.00
62.61	190.25	2.00	0.00	1.00	0.00	62.67	190.01	2.00	0.00	1.00	0.00
62.73	187.83	2.00	0.00	1.00	0.00	62.82	186.70	2.00	0.00	1.00	0.00
62.88	186.42	2.00	0.00	1.00	0.00	62.94	185.32	2.00	0.00	1.00	0.00
63.00	184.46	2.00	0.00	1.00	0.00	63.06	184.15	2.00	0.00	1.00	0.00
63.12	184.45	2.00	0.00	1.00	0.00	63.21	183.58	2.00	0.00	1.00	0.00
63.27	182.19	2.00	0.00	1.00	0.00	63.33	179.82	2.00	0.00	1.00	0.00
63.40	177.50	2.00	0.00	1.00	0.00	63.46	174.90	2.00	0.00	1.00	0.00
63.55	173.02	2.00	0.00	1.00	0.00	63.60	172.96	2.00	0.00	1.00	0.00
63.66	171.63	2.00	0.00	1.00	0.00	63.73	165.77	2.00	0.00	1.00	0.00
63.78	158.74	2.00	0.00	1.00	0.00	63.87	147.32	2.00	0.00	1.00	0.00
63.94	139.97	2.00	0.00	1.00	0.00	63.99	130.93	2.00	0.00	1.00	0.00
64.05	52.35	2.00	0.00	1.00	0.00	64.12	42.26	2.00	0.00	1.00	0.00
64.18	35.28	2.00	0.00	1.00	0.00	64.27	32.52	2.00	0.00	1.00	0.00
64.33	30.89	2.00	0.00	1.00	0.00	64.39	27.69	2.00	0.00	1.00	0.00
64.44	27.63	2.00	0.00	1.00	0.00	64.51	33.80	2.00	0.00	1.00	0.00
64.57	43.64	2.00	0.00	1.00	0.00	64.63	126.57	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
64.72	151.54	2.00	0.00	1.00	0.00	64.79	160.73	2.00	0.00	1.00	0.00
64.85	166.18	2.00	0.00	1.00	0.00	64.91	170.11	2.00	0.00	1.00	0.00
64.96	174.54	2.00	0.00	1.00	0.00	65.05	183.24	2.00	0.00	1.00	0.00
65.11	189.71	2.00	0.00	1.00	0.00	65.18	194.44	2.00	0.00	1.00	0.00
65.23	198.44	2.00	0.00	1.00	0.00	65.29	202.26	2.00	0.00	1.00	0.00
65.38	207.82	2.00	0.00	1.00	0.00	65.44	209.51	2.00	0.00	1.00	0.00
65.50	210.57	2.00	0.00	1.00	0.00	65.56	211.85	2.00	0.00	1.00	0.00
65.63	212.51	2.00	0.00	1.00	0.00	65.69	213.01	2.00	0.00	1.00	0.00
65.77	214.45	2.00	0.00	1.00	0.00	65.83	216.09	2.00	0.00	1.00	0.00
65.89	217.10	2.00	0.00	1.00	0.00	65.95	217.06	2.00	0.00	1.00	0.00
66.01	216.95	2.00	0.00	1.00	0.00	66.10	215.95	2.00	0.00	1.00	0.00
66.16	219.69	2.00	0.00	1.00	0.00	66.23	198.34	2.00	0.00	1.00	0.00
66.29	184.13	2.00	0.00	1.00	0.00	66.35	184.02	2.00	0.00	1.00	0.00
66.41	185.06	2.00	0.00	1.00	0.00	66.47	187.77	2.00	0.00	1.00	0.00
66.54	196.09	2.00	0.00	1.00	0.00	66.62	195.85	2.00	0.00	1.00	0.00
66.69	195.20	2.00	0.00	1.00	0.00	66.75	196.55	2.00	0.00	1.00	0.00
66.81	198.17	2.00	0.00	1.00	0.00	66.86	197.49	2.00	0.00	1.00	0.00
66.95	193.84	2.00	0.00	1.00	0.00	67.01	190.93	2.00	0.00	1.00	0.00
67.07	187.42	2.00	0.00	1.00	0.00	67.13	184.21	2.00	0.00	1.00	0.00
67.19	180.89	2.00	0.00	1.00	0.00	67.28	175.84	2.00	0.00	1.00	0.00
67.34	172.47	2.00	0.00	1.00	0.00	67.40	169.56	2.00	0.00	1.00	0.00
67.46	167.28	2.00	0.00	1.00	0.00	67.52	165.68	2.00	0.00	1.00	0.00
67.61	167.46	2.00	0.00	1.00	0.00	67.67	166.08	2.00	0.00	1.00	0.00
67.73	167.58	2.00	0.00	1.00	0.00	67.79	170.79	2.00	0.00	1.00	0.00
67.85	174.56	2.00	0.00	1.00	0.00	67.94	178.93	2.00	0.00	1.00	0.00
68.00	181.01	2.00	0.00	1.00	0.00	68.06	182.06	2.00	0.00	1.00	0.00
68.12	174.76	2.00	0.00	1.00	0.00	68.18	153.93	2.00	0.00	1.00	0.00
68.24	159.76	2.00	0.00	1.00	0.00	68.33	167.62	2.00	0.00	1.00	0.00
68.39	168.45	2.00	0.00	1.00	0.00	68.45	168.96	2.00	0.00	1.00	0.00
68.51	172.30	2.00	0.00	1.00	0.00	68.59	176.70	2.00	0.00	1.00	0.00
68.65	180.62	2.00	0.00	1.00	0.00	68.70	186.21	2.00	0.00	1.00	0.00
68.80	195.15	2.00	0.00	1.00	0.00	68.86	199.47	2.00	0.00	1.00	0.00
68.92	204.33	2.00	0.00	1.00	0.00	68.97	208.76	2.00	0.00	1.00	0.00
69.04	212.74	2.00	0.00	1.00	0.00	69.10	215.70	2.00	0.00	1.00	0.00
69.19	219.92	2.00	0.00	1.00	0.00	69.25	223.12	2.00	0.00	1.00	0.00
69.31	225.94	2.00	0.00	1.00	0.00	69.36	228.19	2.00	0.00	1.00	0.00
69.42	231.08	2.00	0.00	1.00	0.00	69.51	235.94	2.00	0.00	1.00	0.00
69.57	239.17	2.00	0.00	1.00	0.00	69.63	243.07	2.00	0.00	1.00	0.00
69.69	231.96	2.00	0.00	1.00	0.00	69.75	204.44	2.00	0.00	1.00	0.00
69.84	213.02	2.00	0.00	1.00	0.00	69.89	215.59	2.00	0.00	1.00	0.00
69.96	217.19	2.00	0.00	1.00	0.00	70.02	216.39	2.00	0.00	1.00	0.00
70.08	213.34	2.00	0.00	1.00	0.00	70.15	208.34	2.00	0.00	1.00	0.00
70.21	195.24	2.00	0.00	1.00	0.00	70.28	182.91	2.00	0.00	1.00	0.00
70.35	199.60	2.00	0.00	1.00	0.00	70.41	227.61	2.00	0.00	1.00	0.00
70.48	250.67	2.00	0.00	1.00	0.00	70.55	261.27	2.00	0.00	1.00	0.00
70.61	263.83	2.00	0.00	1.00	0.00	70.68	261.95	2.00	0.00	1.00	0.00
70.74	254.95	2.00	0.00	1.00	0.00	70.81	248.52	2.00	0.00	1.00	0.00
70.88	248.05	2.00	0.00	1.00	0.00	70.95	249.45	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
71.00	252.14	2.00	0.00	1.00	0.00	71.08	259.81	2.00	0.00	1.00	0.00
71.14	265.79	2.00	0.00	1.00	0.00	71.20	271.37	2.00	0.00	1.00	0.00
71.29	275.99	2.00	0.00	1.00	0.00	71.35	278.60	2.00	0.00	1.00	0.00
71.41	278.75	2.00	0.00	1.00	0.00	71.47	277.27	2.00	0.00	1.00	0.00
71.53	274.70	2.00	0.00	1.00	0.00	71.59	271.13	2.00	0.00	1.00	0.00
71.66	235.78	2.00	0.00	1.00	0.00	71.72	253.93	2.00	0.00	1.00	0.00
71.79	256.23	2.00	0.00	1.00	0.00	71.86	255.08	2.00	0.00	1.00	0.00
71.92	248.83	2.00	0.00	1.00	0.00	71.98	245.86	2.00	0.00	1.00	0.00
72.06	243.26	2.00	0.00	1.00	0.00	72.13	240.12	2.00	0.00	1.00	0.00
72.19	238.14	2.00	0.00	1.00	0.00	72.26	236.74	2.00	0.00	1.00	0.00
72.32	236.68	2.00	0.00	1.00	0.00	72.38	236.63	2.00	0.00	1.00	0.00
72.45	238.76	2.00	0.00	1.00	0.00	72.51	241.21	2.00	0.00	1.00	0.00
72.58	244.33	2.00	0.00	1.00	0.00	72.65	247.46	2.00	0.00	1.00	0.00
72.72	249.55	2.00	0.00	1.00	0.00	72.77	250.38	2.00	0.00	1.00	0.00
72.84	250.90	2.00	0.00	1.00	0.00	72.92	251.23	2.00	0.00	1.00	0.00
72.98	249.60	2.00	0.00	1.00	0.00	73.04	245.74	2.00	0.00	1.00	0.00
73.11	237.48	2.00	0.00	1.00	0.00	73.17	231.07	2.00	0.00	1.00	0.00
73.24	227.26	2.00	0.00	1.00	0.00	73.30	223.86	2.00	0.00	1.00	0.00
73.37	205.42	2.00	0.00	1.00	0.00	73.44	212.73	2.00	0.00	1.00	0.00
73.49	211.50	2.00	0.00	1.00	0.00	73.57	211.48	2.00	0.00	1.00	0.00
73.63	211.02	2.00	0.00	1.00	0.00	73.70	211.42	2.00	0.00	1.00	0.00
73.77	213.98	2.00	0.00	1.00	0.00	73.83	217.57	2.00	0.00	1.00	0.00
73.89	219.26	2.00	0.00	1.00	0.00	73.95	222.62	2.00	0.00	1.00	0.00
74.04	229.54	2.00	0.00	1.00	0.00	74.10	232.03	2.00	0.00	1.00	0.00
74.16	232.83	2.00	0.00	1.00	0.00	74.22	232.87	2.00	0.00	1.00	0.00
74.28	234.43	2.00	0.00	1.00	0.00	74.37	233.21	2.00	0.00	1.00	0.00
74.43	229.67	2.00	0.00	1.00	0.00	74.49	224.84	2.00	0.00	1.00	0.00
74.55	218.60	2.00	0.00	1.00	0.00	74.62	180.37	2.00	0.00	1.00	0.00
74.67	201.83	2.00	0.00	1.00	0.00	74.75	200.79	2.00	0.00	1.00	0.00
74.82	203.39	2.00	0.00	1.00	0.00	74.88	207.80	2.00	0.00	1.00	0.00
74.94	208.19	2.00	0.00	1.00	0.00	75.00	211.56	2.00	0.00	1.00	0.00
75.07	217.88	2.00	0.00	1.00	0.00	75.14	237.79	2.00	0.00	1.00	0.00
75.21	242.47	2.00	0.00	1.00	0.00	75.28	244.96	2.00	0.00	1.00	0.00
75.33	246.08	2.00	0.00	1.00	0.00	75.41	241.24	2.00	0.00	1.00	0.00
75.48	235.09	2.00	0.00	1.00	0.00						

Total estimated settlement: 5.98

Abbreviations

- Q_{tn,cs}: Equivalent clean sand normalized cone resistance
- FS: Factor of safety against liquefaction
- e_v (%): Post-liquefaction volumetric strain
- DF: e_v depth weighting factor
- Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ _v	S _{u(peak)} /σ _v
0.07	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.14	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.21	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.28	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.33	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.40	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.47	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.53	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.59	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.67	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.73	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.81	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.87	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.93	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.00	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.06	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.13	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.19	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.26	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.33	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.39	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.45	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.51	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.59	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.64	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.72	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.77	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.84	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.92	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.97	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.05	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.10	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.18	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.24	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.30	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.38	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.44	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.50	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.58	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.64	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.69	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.77	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.83	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.89	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.97	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.03	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.08	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.16	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
3.22	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.29	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.36	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.42	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.48	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.55	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.62	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.69	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.75	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.81	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.89	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.95	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.00	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.08	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.14	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.20	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.28	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.33	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.41	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.47	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.53	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.61	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.67	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.74	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.80	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.86	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.94	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
5.00	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
5.05	37.57	59.88	1.42	85.07	2.10	0.11	0.76
5.13	37.48	59.72	1.37	81.61	2.06	0.10	0.76
5.19	36.91	58.81	1.32	77.72	2.02	0.10	0.75
5.25	36.25	57.74	1.34	77.48	2.04	0.10	0.75
5.33	35.69	56.83	1.37	77.82	2.06	0.10	0.75
5.39	35.31	56.22	1.39	78.16	2.08	0.10	0.75
5.45	35.12	55.91	1.41	78.71	2.09	0.10	0.75
5.53	34.75	55.30	1.44	79.81	2.12	0.10	0.76
5.59	36.16	57.56	1.43	82.45	2.11	0.10	0.76
5.65	38.33	61.04	1.40	85.74	2.09	0.11	0.77
5.72	43.32	69.05	1.35	93.24	2.05	0.11	0.77
5.78	47.74	76.15	1.32	100.36	2.01	0.12	0.78
5.86	52.83	84.32	1.29	109.09	1.98	0.13	0.78
5.92	55.94	89.31	1.28	114.56	1.97	0.13	0.79
5.98	59.14	94.45	1.27	120.28	1.96	0.14	0.79
6.04	63.09	100.79	1.26	126.79	1.93	0.14	0.79
6.12	67.89	108.49	1.24	134.59	1.91	0.15	0.79
6.18	72.23	115.46	1.23	141.74	1.89	0.16	0.80
6.24	75.99	121.49	1.22	148.45	1.88	0.17	0.80
6.31	80.04	127.99	1.23	156.83	1.88	0.18	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
6.37	82.30	131.62	1.23	162.31	1.89	0.19	0.82
6.43	84.66	135.41	1.24	167.93	1.90	0.20	0.82
6.51	87.39	139.78	1.25	174.69	1.92	0.21	0.83
6.57	88.71	141.90	1.26	179.38	1.94	0.22	0.84
6.65	83.53	133.57	1.31	175.46	2.01	0.21	0.84
6.71	77.12	123.27	1.38	169.77	2.07	0.19	0.84
6.77	70.91	113.28	1.45	164.54	2.12	0.18	0.84
6.83	65.07	103.89	1.54	159.78	2.17	0.17	0.83
6.90	58.10	92.69	1.72	159.79	2.24	0.16	0.82
6.96	52.83	84.21	1.91	161.09	2.30	0.15	0.81
7.03	49.25	78.45	2.08	163.39	2.34	0.14	0.80
7.09	46.99	74.82	2.23	167.04	2.37	0.14	0.80
7.17	46.05	73.30	2.30	168.46	2.39	0.14	0.80
7.22	44.45	70.72	2.50	176.66	2.42	0.14	0.79
7.28	43.50	69.19	2.73	188.60	2.46	0.14	0.79
7.36	43.50	69.19	2.85	196.86	2.48	0.14	0.79
7.42	44.07	70.10	2.82	197.54	2.48	0.14	0.79
7.50	45.39	72.21	2.65	191.51	2.45	0.14	0.80
7.55	44.17	70.23	2.75	193.23	2.47	0.14	0.79
7.61	44.27	70.39	2.74	193.05	2.46	0.14	0.79
7.70	44.36	70.52	2.82	199.18	2.48	0.14	0.79
7.75	47.75	75.96	2.57	195.15	2.44	0.14	0.80
7.81	52.37	83.38	2.24	186.89	2.37	0.15	0.81
7.89	58.30	92.90	1.95	181.09	2.31	0.16	0.82
7.95	61.50	98.04	1.82	178.76	2.27	0.16	0.82
8.01	64.99	103.64	1.72	177.77	2.24	0.17	0.82
8.08	68.19	108.77	1.63	177.67	2.21	0.17	0.83
8.14	69.60	111.03	1.61	178.21	2.20	0.17	0.83
8.22	72.14	115.10	1.57	180.57	2.18	0.18	0.83
8.28	74.78	118.64	1.54	182.12	2.17	0.18	0.84
8.34	77.13	121.35	1.51	183.19	2.15	0.19	0.84
8.40	78.36	122.44	1.50	183.16	2.15	0.19	0.84
8.48	77.51	120.47	1.51	181.39	2.15	0.19	0.84
8.54	75.72	117.38	1.52	178.88	2.16	0.18	0.84
8.60	73.84	114.08	1.54	175.26	2.17	0.18	0.83
8.68	71.77	110.12	1.54	169.19	2.17	0.17	0.83
8.74	70.64	107.74	1.53	164.75	2.16	0.17	0.82
8.79	69.79	105.93	1.53	161.88	2.16	0.16	0.82
8.87	69.32	104.50	1.52	159.27	2.16	0.16	0.82
8.93	68.94	103.48	1.53	157.97	2.16	0.16	0.82
8.99	68.75	102.78	1.53	157.52	2.16	0.16	0.82
9.07	68.75	102.26	1.54	157.53	2.17	0.16	0.82
9.13	68.75	101.89	1.55	157.85	2.17	0.16	0.82
9.19	68.66	101.33	1.55	157.32	2.17	0.16	0.82
9.27	68.56	100.55	1.55	156.00	2.17	0.16	0.82
9.33	67.90	99.20	1.56	155.22	2.18	0.16	0.82
9.39	66.12	96.49	1.60	154.37	2.19	0.15	0.82
9.46	62.54	91.38	1.69	154.15	2.23	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
9.52	60.09	87.87	1.76	154.57	2.25	0.14	0.81
9.58	57.83	84.74	1.86	157.30	2.28	0.14	0.80
9.66	56.23	82.15	1.92	157.84	2.30	0.14	0.80
9.72	54.44	79.41	1.98	157.24	2.31	0.14	0.80
9.78	52.65	76.77	2.06	158.43	2.33	0.14	0.79
9.86	51.43	74.77	2.14	159.64	2.35	0.13	0.79
9.91	50.48	73.21	2.18	159.92	2.36	0.13	0.79
9.97	50.48	72.80	2.17	157.88	2.36	0.13	0.79
10.04	48.04	69.26	2.29	158.76	2.38	0.13	0.78
10.12	52.92	74.87	1.99	148.95	2.32	0.13	0.79
10.18	52.08	73.31	1.98	145.41	2.32	0.13	0.79
10.25	50.00	70.27	2.07	145.78	2.34	0.13	0.79
10.31	48.22	67.73	2.17	147.12	2.36	0.13	0.78
10.37	46.34	65.03	2.27	147.45	2.38	0.12	0.78
10.45	44.83	62.98	2.47	155.38	2.42	0.12	0.78
10.50	44.27	62.15	2.58	160.54	2.44	0.12	0.78
10.58	43.41	60.80	2.70	164.10	2.46	0.12	0.77
10.64	43.23	60.33	2.74	165.44	2.46	0.12	0.77
10.70	43.69	60.73	2.75	166.83	2.46	0.12	0.77
10.78	44.93	62.00	2.69	167.02	2.46	0.12	0.78
10.84	46.53	63.71	2.57	163.76	2.44	0.13	0.78
10.90	49.07	66.45	2.36	157.11	2.40	0.13	0.78
10.98	52.08	69.59	2.14	149.04	2.35	0.13	0.79
11.04	53.97	71.51	2.03	144.90	2.33	0.13	0.79
11.10	55.66	73.22	1.95	142.50	2.31	0.13	0.79
11.16	57.17	74.71	1.88	140.72	2.29	0.13	0.79
11.22	58.30	75.69	1.83	138.46	2.27	0.13	0.80
11.31	58.58	75.48	1.80	135.53	2.26	0.13	0.79
11.37	58.96	75.60	1.78	134.36	2.26	0.13	0.80
11.43	58.86	75.21	1.79	134.43	2.26	0.13	0.79
11.49	59.15	75.25	1.78	133.63	2.26	0.13	0.79
11.55	59.52	75.40	1.77	133.36	2.25	0.13	0.80
11.64	59.90	75.46	1.77	133.60	2.26	0.13	0.80
11.70	60.09	75.43	1.78	134.05	2.26	0.13	0.80
11.77	60.56	75.73	1.78	134.64	2.26	0.13	0.80
11.82	60.94	75.94	1.78	135.32	2.26	0.14	0.80
11.88	61.50	76.35	1.78	136.06	2.26	0.14	0.80
11.94	61.12	75.68	1.81	136.97	2.27	0.14	0.80
12.03	61.03	74.48	1.62	120.88	2.20	0.13	0.79
12.09	61.69	74.53	1.52	113.04	2.16	0.13	0.79
12.15	61.68	74.51	1.57	116.69	2.18	0.13	0.79
12.21	61.22	73.82	1.60	118.27	2.20	0.13	0.79
12.28	60.83	73.21	1.63	119.38	2.21	0.13	0.79
12.34	59.34	71.33	1.69	120.53	2.23	0.13	0.79
12.42	48.69	59.02	2.14	126.54	2.35	0.12	0.77
12.48	53.50	64.32	1.95	125.18	2.31	0.12	0.78
12.54	51.05	61.39	2.10	128.99	2.34	0.12	0.78
12.60	47.75	57.56	2.38	137.06	2.40	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
12.69	43.41	52.52	2.93	153.81	2.49	0.12	0.77
12.75	41.72	50.49	3.23	162.95	2.53	0.12	0.76
12.81	40.21	48.66	3.56	173.01	2.58	0.12	0.76
12.87	40.21	48.56	3.71	180.25	2.60	0.12	0.76
12.93	40.22	48.44	3.84	185.89	2.61	0.12	0.62
13.02	41.07	49.16	3.80	186.67	2.61	0.12	0.62
13.08	41.82	49.80	3.68	183.44	2.59	0.12	0.76
13.14	42.67	50.54	3.55	179.50	2.58	0.12	0.77
13.20	43.61	51.33	3.37	172.76	2.55	0.12	0.77
13.26	45.12	52.76	3.13	165.25	2.52	0.12	0.77
13.35	47.85	55.37	2.76	152.98	2.47	0.12	0.77
13.41	50.20	57.68	2.53	145.75	2.43	0.12	0.78
13.47	52.55	60.00	2.33	140.09	2.39	0.12	0.78
13.53	54.43	61.78	2.19	135.57	2.36	0.13	0.78
13.59	55.94	63.20	2.12	134.14	2.35	0.13	0.78
13.65	57.25	64.45	2.10	135.42	2.34	0.13	0.79
13.74	59.23	66.35	2.09	138.56	2.34	0.13	0.79
13.80	59.89	66.87	2.10	140.42	2.34	0.13	0.79
13.86	59.97	66.78	2.13	141.93	2.35	0.13	0.79
13.92	59.97	66.59	2.16	143.57	2.36	0.13	0.79
13.98	61.01	67.48	2.12	143.32	2.35	0.13	0.79
14.07	63.93	70.23	2.01	140.87	2.32	0.14	0.80
14.13	66.19	72.37	1.92	139.16	2.30	0.14	0.80
14.19	67.97	73.95	1.83	135.64	2.27	0.14	0.80
14.25	69.85	75.56	1.72	129.86	2.24	0.14	0.80
14.31	71.44	76.92	1.65	126.54	2.21	0.14	0.80
14.37	72.86	78.13	1.61	125.62	2.20	0.14	0.80
14.46	75.21	80.19	1.55	124.64	2.17	0.14	0.81
14.52	77.00	81.79	1.52	124.63	2.16	0.14	0.81
14.58	78.98	83.58	1.50	124.97	2.15	0.15	0.81
14.64	81.24	85.66	1.47	125.81	2.13	0.15	0.81
14.70	83.21	87.45	1.45	127.13	2.12	0.15	0.81
14.79	86.13	90.08	1.43	128.65	2.11	0.15	0.82
14.85	87.83	91.35	1.36	124.69	2.06	0.15	0.81
14.91	89.52	92.62	1.32	122.19	2.01	0.15	0.81
14.97	90.95	93.87	1.32	124.03	2.02	0.15	0.81
15.03	92.17	94.90	1.32	125.67	2.02	0.15	0.81
15.09	93.02	95.55	1.33	126.91	2.02	0.15	0.81
15.18	92.12	94.35	1.35	126.97	2.04	0.15	0.81
15.23	92.08	94.09	1.35	127.22	2.05	0.15	0.81
15.29	93.86	95.63	1.34	128.45	2.04	0.16	0.82
15.38	95.94	97.40	1.34	130.38	2.03	0.16	0.82
15.44	96.60	97.85	1.35	132.08	2.05	0.16	0.82
15.50	96.78	97.80	1.36	132.79	2.05	0.16	0.82
15.56	96.60	97.38	1.36	132.88	2.06	0.16	0.82
15.62	96.50	97.03	1.37	132.84	2.06	0.16	0.82
15.71	95.75	95.90	1.38	131.99	2.07	0.16	0.82
15.77	95.18	95.07	1.38	130.98	2.07	0.16	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
15.83	94.71	94.35	1.38	130.61	2.07	0.16	0.82
15.89	93.96	93.36	1.39	130.02	2.08	0.16	0.82
15.95	93.02	92.20	1.40	129.19	2.09	0.16	0.82
16.04	91.70	90.54	1.41	127.96	2.10	0.16	0.82
16.10	90.95	89.56	1.42	127.33	2.10	0.16	0.82
16.16	90.38	88.77	1.43	126.77	2.11	0.16	0.82
16.22	89.44	87.62	1.44	125.91	2.11	0.15	0.82
16.28	88.21	86.18	1.45	124.67	2.12	0.15	0.81
16.34	86.43	84.21	1.46	122.77	2.12	0.15	0.81
16.43	82.47	80.02	1.49	119.36	2.14	0.14	0.81
16.49	78.89	76.32	1.53	117.03	2.16	0.14	0.80
16.55	74.65	72.01	1.60	114.94	2.19	0.14	0.80
16.61	70.04	67.36	1.69	113.92	2.23	0.13	0.79
16.67	65.24	62.55	1.83	114.34	2.27	0.13	0.79
16.76	57.52	54.85	2.15	117.68	2.35	0.12	0.78
16.82	52.90	50.25	2.42	121.54	2.41	0.12	0.77
16.88	48.95	46.32	2.73	126.29	2.46	0.11	0.76
16.94	44.90	42.30	3.17	133.96	2.53	0.11	0.76
17.00	40.47	37.93	3.83	145.26	2.61	0.11	0.62
17.09	34.54	32.08	4.30	138.08	2.66	0.10	0.62
17.15	32.84	30.35	4.56	138.52	2.69	0.10	0.62
17.21	32.94	30.35	4.68	141.91	2.70	0.10	0.62
17.27	33.97	31.22	4.63	144.68	2.69	0.10	0.62
17.34	35.76	32.81	4.56	149.52	2.69	0.10	0.62
17.39	37.47	34.31	4.61	158.15	2.69	0.11	0.62
17.46	27.49	24.80	7.60	188.45	2.93	0.10	0.62
17.52	41.33	37.68	4.53	170.64	2.68	0.11	0.62
17.60	48.39	44.13	3.66	161.39	2.59	0.12	0.76
17.66	55.55	50.66	3.04	153.84	2.51	0.12	0.78
17.72	62.80	57.28	2.57	147.24	2.44	0.13	0.79
17.81	77.21	70.43	1.97	138.86	2.31	0.15	0.81
17.87	86.81	79.16	1.71	135.35	2.24	0.16	0.82
17.93	94.63	86.22	1.55	133.61	2.17	0.17	0.83
17.99	101.41	92.32	1.44	132.98	2.11	0.17	0.83
18.05	106.68	96.97	1.38	134.00	2.07	0.18	0.83
18.12	111.11	100.84	1.35	136.19	2.05	0.18	0.83
18.18	112.90	102.24	1.34	137.38	2.04	0.18	0.83
18.27	115.91	104.64	1.34	139.77	2.03	0.19	0.84
18.33	117.32	105.68	1.34	141.16	2.03	0.19	0.84
18.39	117.98	106.03	1.34	141.78	2.03	0.19	0.84
18.45	118.55	106.29	1.34	142.23	2.03	0.20	0.84
18.51	119.02	106.45	1.34	142.76	2.04	0.20	0.84
18.60	119.30	106.33	1.35	143.26	2.04	0.20	0.84
18.66	119.11	105.89	1.35	143.36	2.05	0.20	0.84
18.72	118.73	105.29	1.36	143.30	2.06	0.20	0.84
18.78	117.89	104.27	1.37	142.85	2.06	0.20	0.84
18.84	116.76	102.98	1.38	142.21	2.07	0.20	0.84
18.90	115.06	101.18	1.40	141.39	2.08	0.20	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
18.99	111.86	97.92	1.43	139.89	2.11	0.19	0.84
19.05	110.17	96.15	1.45	139.24	2.12	0.19	0.84
19.11	107.72	93.71	1.48	138.63	2.14	0.19	0.84
19.17	105.55	91.50	1.52	138.77	2.16	0.18	0.84
19.23	104.23	90.08	1.54	138.78	2.17	0.18	0.84
19.32	101.60	87.42	1.57	137.28	2.18	0.18	0.83
19.38	99.05	84.92	1.61	137.07	2.20	0.17	0.83
19.44	95.00	81.06	1.73	140.02	2.24	0.17	0.83
19.50	87.94	74.70	1.79	134.07	2.26	0.16	0.82
19.56	79.09	67.05	1.67	111.75	2.22	0.14	0.80
19.65	64.40	53.77	2.28	122.67	2.38	0.13	0.78
19.71	57.34	47.48	2.65	125.96	2.45	0.12	0.77
19.77	48.02	39.24	3.50	137.19	2.57	0.11	0.76
19.83	39.07	31.43	4.71	148.18	2.70	0.10	0.62
19.89	29.56	23.26	6.95	161.69	2.88	0.10	0.62
19.95	29.84	23.41	6.99	163.54	2.88	0.10	0.62
20.01	29.42	22.99	7.04	161.81	2.89	0.10	0.62
20.09	29.28	22.79	7.10	161.80	2.89	0.10	0.62
20.15	27.68	21.43	7.65	163.88	2.93	0.10	0.62
20.21	25.70	19.75	8.41	166.08	2.98	0.09	0.62
20.30	24.47	18.68	8.87	165.64	3.01	0.09	1.33
20.36	24.57	18.70	8.67	162.18	2.99	0.09	0.62
20.42	24.66	18.71	8.51	159.24	2.98	0.09	0.62
20.48	24.10	18.21	8.68	158.00	2.99	0.09	0.62
20.54	23.25	17.48	8.98	157.02	3.01	0.09	1.25
20.63	24.24	18.18	8.45	153.56	2.98	0.09	0.62
20.69	23.16	17.28	8.98	155.17	3.01	0.09	1.23
20.75	24.38	18.18	8.56	155.62	2.99	0.09	0.62
20.81	25.60	19.09	8.24	157.28	2.97	0.09	0.62
20.87	27.11	20.21	7.90	159.71	2.95	0.09	0.62
20.93	28.99	21.62	7.47	161.54	2.92	0.10	0.62
21.02	32.48	24.23	6.64	160.96	2.86	0.10	0.62
21.08	34.55	25.82	6.22	160.58	2.83	0.10	0.62
21.14	36.62	27.42	5.81	159.34	2.80	0.10	0.62
21.20	38.60	29.05	4.85	140.92	2.71	0.10	0.62
21.26	40.95	31.15	3.51	109.31	2.57	0.10	0.74
21.35	45.10	34.38	3.21	110.45	2.53	0.10	0.75
21.41	46.79	35.62	3.20	113.92	2.53	0.11	0.75
21.47	47.73	36.23	3.29	119.03	2.54	0.11	0.75
21.53	48.30	36.54	3.40	124.08	2.56	0.11	0.75
21.59	46.60	34.99	3.77	131.99	2.60	0.11	0.62
21.66	46.32	34.57	4.08	140.91	2.64	0.11	0.62
21.72	45.10	33.41	4.50	150.25	2.68	0.11	0.62
21.79	42.84	31.42	5.12	160.81	2.74	0.11	0.62
21.86	41.52	30.23	5.55	167.68	2.77	0.11	0.62
21.92	40.39	29.21	5.92	172.98	2.81	0.11	0.62
22.00	38.60	27.67	6.42	177.62	2.84	0.11	0.62
22.06	37.66	26.88	6.68	179.45	2.86	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
22.13	37.47	26.65	6.77	180.46	2.87	0.10	0.62
22.18	37.47	26.58	6.79	180.38	2.87	0.10	0.62
22.26	37.47	26.48	6.77	179.14	2.87	0.10	0.62
22.32	37.47	26.40	6.78	178.96	2.87	0.10	0.62
22.39	37.47	26.32	6.80	178.88	2.87	0.10	0.62
22.46	38.22	26.78	6.65	178.03	2.86	0.10	0.62
22.52	38.32	26.78	6.66	178.35	2.86	0.10	0.62
22.60	38.50	26.81	6.67	178.78	2.86	0.10	0.62
22.64	38.60	26.83	6.67	178.93	2.86	0.10	0.62
22.71	38.79	26.88	6.65	178.74	2.86	0.11	0.62
22.77	38.50	26.59	6.73	178.93	2.87	0.10	0.62
22.84	37.19	25.57	7.05	180.41	2.89	0.10	0.62
22.93	38.61	26.48	6.74	178.45	2.87	0.10	0.62
22.98	37.48	25.60	6.96	178.22	2.88	0.10	0.62
23.04	38.70	26.40	6.51	171.82	2.85	0.10	0.62
23.12	41.53	28.74	4.76	136.86	2.71	0.10	0.62
23.17	45.77	32.15	3.58	115.23	2.58	0.11	0.75
23.26	53.67	38.10	2.97	113.32	2.50	0.11	0.76
23.32	60.17	42.98	2.65	114.08	2.45	0.12	0.77
23.38	66.19	47.47	2.45	116.26	2.41	0.12	0.78
23.44	70.33	50.55	2.31	116.86	2.39	0.13	0.78
23.49	71.09	50.99	2.31	117.96	2.39	0.13	0.79
23.56	74.76	53.69	2.21	118.61	2.37	0.13	0.79
23.63	77.87	55.89	2.16	120.45	2.36	0.14	0.79
23.69	80.60	57.80	2.12	122.59	2.35	0.14	0.80
23.75	85.02	61.04	2.03	124.11	2.33	0.15	0.80
23.84	87.47	62.65	2.03	127.04	2.33	0.15	0.81
23.89	88.32	63.15	2.03	128.38	2.33	0.15	0.81
23.96	90.77	64.83	2.00	129.52	2.32	0.15	0.81
24.02	92.37	65.89	1.98	130.33	2.31	0.16	0.81
24.10	93.40	66.45	1.97	130.81	2.31	0.16	0.82
24.16	94.06	66.80	1.96	130.99	2.31	0.16	0.82
24.23	94.02	66.59	1.97	131.38	2.31	0.16	0.82
24.29	93.97	66.39	1.97	130.88	2.31	0.16	0.82
24.36	93.40	65.84	1.97	129.79	2.31	0.16	0.82
24.41	91.90	64.58	1.99	128.65	2.32	0.15	0.81
24.50	88.88	62.13	2.04	126.90	2.33	0.15	0.81
24.56	86.25	60.02	2.10	125.88	2.34	0.15	0.81
24.62	82.20	56.84	2.21	125.41	2.37	0.14	0.80
24.68	77.02	52.83	2.38	125.58	2.40	0.14	0.79
24.75	70.90	48.13	2.64	126.95	2.45	0.13	0.78
24.80	63.55	42.56	3.05	129.84	2.51	0.12	0.77
24.89	49.99	32.49	4.24	137.62	2.65	0.11	0.62
24.95	40.67	25.73	5.57	143.36	2.78	0.10	0.62
25.01	33.51	20.82	6.98	145.40	2.88	0.10	0.62
25.07	28.15	17.28	8.30	143.41	2.97	0.09	0.62
25.14	24.47	14.85	9.30	138.18	3.03	0.09	1.06
25.22	21.46	12.86	9.84	126.46	3.06	0.09	0.92

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
25.28	19.67	11.67	10.03	117.11	3.07	0.08	0.83
25.34	18.82	11.10	8.94	99.20	3.01	0.08	0.79
25.40	18.63	10.95	7.79	85.34	2.94	0.08	0.62
25.46	18.73	10.99	7.55	82.92	2.92	0.08	0.62
25.53	18.93	11.09	7.36	81.64	2.91	0.08	0.62
25.62	19.48	11.40	7.81	89.06	2.94	0.08	0.62
25.67	18.65	10.85	9.26	100.41	3.03	0.08	0.77
25.73	21.28	12.49	8.80	109.90	3.00	0.09	0.89
25.79	22.61	13.30	9.29	123.48	3.03	0.09	0.95
25.87	25.91	15.34	9.08	139.27	3.02	0.09	1.10
25.94	40.99	24.97	5.51	137.48	2.77	0.10	0.62
25.98	52.20	32.70	4.08	133.46	2.64	0.11	0.62
26.07	70.28	45.32	2.85	129.15	2.48	0.13	0.78
26.14	82.24	53.80	2.36	126.82	2.40	0.14	0.80
26.20	91.18	60.15	2.10	126.22	2.34	0.15	0.81
26.26	94.10	62.17	2.02	125.51	2.32	0.15	0.81
26.32	92.50	60.94	2.03	123.71	2.33	0.15	0.81
26.41	83.18	54.04	2.28	123.02	2.38	0.14	0.80
26.47	74.80	47.92	2.61	124.82	2.44	0.13	0.79
26.53	64.63	40.59	3.17	128.76	2.53	0.12	0.77
26.59	53.80	32.94	4.09	134.71	2.64	0.11	0.62
26.64	44.56	26.53	5.30	140.64	2.75	0.11	0.62
26.73	34.67	20.14	7.26	146.25	2.90	0.10	0.62
26.79	29.97	17.24	8.51	146.65	2.98	0.09	0.62
26.86	26.48	15.08	9.44	142.34	3.04	0.09	1.08
26.92	24.97	14.13	9.54	134.70	3.04	0.09	1.01
26.98	24.03	13.52	9.41	127.24	3.04	0.09	0.97
27.04	23.09	12.93	9.37	121.08	3.03	0.09	0.92
27.12	21.21	11.75	9.92	116.53	3.06	0.08	0.84
27.19	21.21	11.72	10.17	119.23	3.08	0.08	0.84
27.25	21.21	11.70	10.68	124.95	3.10	0.08	0.84
27.30	24.13	13.41	9.68	129.89	3.05	0.09	0.96
27.37	28.83	16.18	8.21	132.84	2.97	0.09	0.62
27.46	38.91	22.12	6.02	133.16	2.81	0.10	0.62
27.52	50.78	29.97	4.14	123.99	2.64	0.11	0.62
27.58	63.30	38.61	2.86	110.57	2.48	0.12	0.77
27.64	73.19	45.44	2.34	106.29	2.39	0.12	0.78
27.70	81.10	50.79	2.12	107.49	2.35	0.13	0.79
27.76	85.34	53.65	2.01	107.92	2.32	0.14	0.80
27.82	84.86	53.27	2.00	106.49	2.32	0.13	0.79
27.89	71.48	43.77	2.48	108.78	2.42	0.12	0.78
27.96	73.73	45.29	2.35	106.42	2.40	0.12	0.78
28.02	68.18	41.26	2.68	110.62	2.45	0.12	0.77
28.09	60.93	36.21	3.14	113.56	2.52	0.12	0.76
28.16	56.12	32.73	3.73	122.17	2.60	0.11	0.76
28.23	54.23	31.20	4.23	131.85	2.65	0.11	0.62
28.28	53.84	30.75	4.49	138.09	2.68	0.11	0.62
28.35	54.41	30.94	4.61	142.58	2.69	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
28.43	55.63	31.62	4.51	142.68	2.68	0.11	0.62
28.49	56.10	31.85	4.46	142.15	2.68	0.11	0.62
28.55	57.89	32.97	4.24	139.82	2.65	0.12	0.62
28.61	60.81	34.87	3.87	135.11	2.61	0.12	0.62
28.70	65.71	38.19	3.26	124.61	2.54	0.12	0.77
28.76	69.19	40.65	2.85	115.67	2.48	0.12	0.77
28.82	71.92	42.65	2.53	107.69	2.43	0.12	0.78
28.88	74.18	44.32	2.29	101.30	2.38	0.12	0.78
28.94	76.54	46.04	2.11	96.96	2.34	0.12	0.78
29.03	79.55	48.09	1.96	94.47	2.31	0.12	0.78
29.09	81.06	49.07	1.91	93.90	2.30	0.13	0.78
29.15	82.28	49.81	1.88	93.83	2.29	0.13	0.79
29.21	83.13	50.28	1.87	94.06	2.29	0.13	0.79
29.27	83.51	50.42	1.87	94.40	2.29	0.13	0.79
29.33	83.69	50.43	1.88	94.59	2.29	0.13	0.79
29.42	83.79	50.35	1.88	94.54	2.29	0.13	0.79
29.48	83.60	50.15	1.87	94.00	2.29	0.13	0.79
29.54	82.75	49.53	1.88	93.08	2.29	0.13	0.79
29.60	81.53	48.65	1.90	92.31	2.29	0.12	0.78
29.66	79.83	47.45	1.92	91.30	2.30	0.12	0.78
29.75	75.78	44.68	2.00	89.50	2.32	0.12	0.78
29.81	71.92	41.97	2.15	90.30	2.35	0.12	0.77
29.87	66.74	38.32	2.44	93.52	2.41	0.11	0.77
29.93	60.06	33.70	2.97	100.18	2.50	0.11	0.76
29.99	51.40	27.86	4.00	111.55	2.63	0.11	0.62
30.05	38.97	20.13	6.35	127.81	2.84	0.10	0.62
30.12	32.47	16.57	8.29	137.42	2.97	0.09	0.62
30.19	28.23	14.24	9.88	140.76	3.06	0.09	1.02
30.26	25.88	12.94	10.85	140.33	3.11	0.09	0.92
30.33	23.05	11.39	12.02	136.96	3.17	0.08	0.81
30.39	19.19	9.29	14.34	133.23	3.27	0.08	0.66
30.45	16.37	7.76	16.85	130.79	3.36	0.08	0.55
30.52	14.95	6.99	18.14	126.75	3.40	0.08	0.50
30.58	14.58	6.77	18.01	122.01	3.40	0.08	0.48
30.65	14.11	6.51	17.85	116.15	3.39	0.08	0.46
30.71	13.35	6.09	18.15	110.56	3.40	0.08	0.44
30.78	13.63	6.22	17.04	106.01	3.37	0.08	0.44
30.85	13.35	6.06	17.10	103.65	3.37	0.08	0.43
30.92	13.16	5.95	17.00	101.07	3.37	0.08	0.42
30.97	13.17	5.94	16.84	99.96	3.36	0.08	0.42
31.04	13.17	5.92	16.88	99.97	3.36	0.08	0.42
31.11	13.46	6.06	16.41	99.44	3.34	0.08	0.43
31.17	13.46	6.05	16.31	98.64	3.34	0.08	0.43
31.25	13.93	6.28	15.65	98.24	3.32	0.08	0.45
31.30	13.64	6.12	16.48	100.80	3.35	0.08	0.44
31.37	14.77	6.69	15.20	101.69	3.30	0.08	0.48
31.44	13.00	5.75	17.63	101.39	3.39	0.08	0.41
31.51	14.97	6.76	14.79	100.00	3.28	0.08	0.48

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
31.57	14.41	6.46	15.55	100.41	3.31	0.08	0.46
31.63	14.69	6.59	15.17	99.93	3.30	0.08	0.47
31.70	14.69	6.57	15.16	99.66	3.30	0.08	0.47
31.79	14.69	6.55	15.26	100.02	3.30	0.08	0.47
31.85	14.69	6.54	15.37	100.54	3.31	0.08	0.47
31.91	15.07	6.72	15.08	101.40	3.30	0.08	0.48
31.97	15.16	6.75	13.75	92.85	3.24	0.08	0.48
32.03	15.54	6.93	11.45	79.38	3.14	0.08	0.50
32.09	15.91	7.11	12.11	86.10	3.17	0.08	0.51
32.18	16.57	7.42	12.63	93.78	3.20	0.08	0.53
32.24	16.67	7.46	13.32	99.35	3.23	0.08	0.53
32.30	17.04	7.63	13.56	103.54	3.24	0.08	0.55
32.35	15.73	6.96	15.36	106.86	3.31	0.08	0.50
32.43	17.81	7.99	13.64	108.97	3.24	0.08	0.57
32.50	19.60	8.87	12.59	111.71	3.19	0.08	0.63
32.56	19.79	8.95	12.78	114.38	3.20	0.08	0.64
32.62	19.60	8.83	13.27	117.20	3.22	0.08	0.63
32.69	19.69	8.86	13.58	120.38	3.24	0.08	0.63
32.75	20.44	9.22	13.21	121.80	3.22	0.08	0.66
32.83	22.23	10.09	12.10	122.03	3.17	0.08	0.72
32.88	23.46	10.68	11.43	122.12	3.14	0.08	0.76
32.96	23.65	10.75	11.39	122.47	3.14	0.08	0.77
33.02	22.70	10.26	11.98	122.92	3.17	0.08	0.73
33.08	21.67	9.73	12.66	123.18	3.20	0.08	0.69
33.14	21.29	9.52	12.95	123.26	3.21	0.08	0.68
33.23	20.63	9.17	13.14	120.47	3.22	0.08	0.65
33.28	20.16	8.92	13.09	116.77	3.22	0.08	0.64
33.36	19.88	8.76	13.00	113.95	3.21	0.08	0.63
33.41	19.31	8.47	13.39	113.43	3.23	0.08	0.60
33.48	18.94	8.27	13.71	113.38	3.24	0.08	0.59
33.55	18.65	8.11	14.03	113.76	3.25	0.08	0.58
33.61	17.81	7.68	14.74	113.27	3.28	0.08	0.55
33.67	17.81	7.67	14.64	112.24	3.28	0.08	0.55
33.74	18.09	7.79	14.37	111.93	3.27	0.08	0.56
33.80	18.28	7.86	14.26	112.15	3.26	0.08	0.56
33.88	19.22	8.30	13.49	111.95	3.23	0.08	0.59
33.94	19.41	8.38	13.41	112.34	3.23	0.08	0.60
34.00	19.60	8.45	13.39	113.19	3.23	0.08	0.60
34.06	21.01	9.11	12.59	114.77	3.19	0.08	0.65
34.15	22.89	9.99	11.80	117.94	3.16	0.08	0.71
34.21	24.40	10.70	10.86	116.20	3.11	0.08	0.76
34.27	22.99	10.00	11.59	115.90	3.15	0.08	0.71
34.33	21.39	9.22	12.63	116.41	3.20	0.08	0.66
34.39	19.22	8.17	13.34	108.93	3.23	0.08	0.58
34.45	17.24	7.21	12.66	91.25	3.20	0.08	0.51
34.52	16.21	6.71	13.78	92.37	3.24	0.08	0.48
34.61	15.46	6.33	14.67	92.79	3.28	0.08	0.45
34.67	14.52	5.87	15.93	93.48	3.33	0.08	0.42

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
34.73	13.96	5.59	16.85	94.25	3.36	0.08	0.40
34.79	14.05	5.63	16.95	95.40	3.36	0.08	0.40
34.85	14.15	5.67	16.92	95.86	3.36	0.08	0.40
34.93	14.33	5.74	16.65	95.52	3.35	0.08	0.41
34.98	14.62	5.86	16.23	95.17	3.34	0.08	0.42
35.07	15.18	6.11	15.54	94.91	3.31	0.08	0.44
35.13	15.46	6.23	15.27	95.07	3.30	0.08	0.44
35.19	15.75	6.35	14.98	95.15	3.29	0.08	0.45
35.25	15.75	6.34	15.01	95.18	3.29	0.08	0.45
35.31	15.75	6.33	15.10	95.56	3.30	0.08	0.45
35.37	15.75	6.32	15.17	95.82	3.30	0.08	0.45
35.43	15.75	6.30	15.35	96.76	3.31	0.08	0.45
35.52	16.03	6.42	15.24	97.75	3.30	0.08	0.46
35.58	16.31	6.53	14.99	97.96	3.29	0.08	0.47
35.64	16.59	6.65	14.68	97.62	3.28	0.08	0.48
35.70	16.88	6.77	14.40	97.53	3.27	0.08	0.48
35.76	16.97	6.80	14.49	98.59	3.27	0.08	0.49
35.85	17.06	6.82	14.82	101.16	3.29	0.08	0.49
35.91	17.44	6.99	14.64	102.28	3.28	0.08	0.50
35.97	17.82	7.15	14.50	103.63	3.27	0.08	0.51
36.03	18.29	7.35	14.30	105.12	3.27	0.08	0.52
36.09	19.05	7.68	13.99	107.39	3.25	0.08	0.55
36.18	20.56	8.34	13.46	112.30	3.23	0.08	0.60
36.24	22.82	9.35	12.18	113.95	3.18	0.08	0.67
36.30	25.55	10.57	10.96	115.90	3.12	0.08	0.76
36.36	27.53	11.45	10.30	117.99	3.08	0.09	0.82
36.42	29.13	12.15	9.86	119.77	3.06	0.09	0.87
36.51	31.58	13.22	9.46	125.05	3.04	0.09	0.94
36.57	31.67	13.24	9.75	129.07	3.05	0.09	0.95
36.63	30.82	12.84	10.15	130.33	3.08	0.09	0.92
36.69	29.41	12.18	10.61	129.29	3.10	0.09	0.87
36.75	29.13	12.04	9.70	116.81	3.05	0.09	0.86
36.81	32.14	13.36	7.07	94.44	2.89	0.09	0.62
36.91	41.18	17.35	5.74	99.68	2.79	0.10	0.62
36.97	46.83	19.84	5.18	102.69	2.74	0.10	0.62
37.03	50.50	21.49	5.03	107.98	2.73	0.10	0.62
37.08	47.96	20.27	5.79	117.34	2.79	0.10	0.62
37.15	44.10	18.52	6.76	125.28	2.87	0.10	0.62
37.21	38.45	15.99	8.06	128.88	2.96	0.10	0.62
37.29	32.42	13.30	9.62	127.87	3.05	0.09	0.95
37.34	29.69	12.07	10.47	126.43	3.09	0.09	0.86
37.43	25.83	10.35	11.92	123.33	3.16	0.08	0.74
37.48	23.48	9.30	13.04	121.33	3.21	0.08	0.66
37.55	22.16	8.71	13.97	121.61	3.25	0.08	0.62
37.62	23.10	9.10	13.35	121.51	3.23	0.08	0.65
37.67	24.23	9.58	12.55	120.21	3.19	0.08	0.68
37.74	26.21	10.42	11.70	121.92	3.15	0.08	0.74
37.81	28.47	11.38	10.95	124.63	3.12	0.09	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
37.86	30.26	12.15	10.40	126.35	3.09	0.09	0.87
37.94	33.27	13.43	9.61	129.02	3.05	0.09	0.96
38.02	35.44	14.33	9.29	133.21	3.03	0.09	1.02
38.07	36.19	14.64	9.08	132.91	3.02	0.09	1.05
38.13	36.28	14.65	8.75	128.18	3.00	0.09	0.62
38.22	35.15	14.13	9.66	136.45	3.05	0.09	1.01
38.28	35.53	14.26	9.83	140.22	3.06	0.09	1.02
38.34	37.41	15.05	9.41	141.52	3.04	0.09	1.07
38.40	40.52	16.35	8.51	139.24	2.98	0.10	0.62
38.47	50.89	20.75	6.35	131.77	2.84	0.10	0.62
38.53	54.37	22.20	5.89	130.69	2.80	0.11	0.62
38.59	59.84	24.50	5.23	128.20	2.75	0.11	0.62
38.68	71.32	30.21	3.99	120.56	2.63	0.12	0.62
38.74	78.57	34.10	3.35	114.35	2.55	0.13	0.78
38.80	82.81	36.38	3.05	111.13	2.51	0.13	0.78
38.85	83.19	36.52	3.04	110.89	2.51	0.13	0.78
38.93	81.12	35.18	3.26	114.81	2.54	0.13	0.78
38.98	80.18	34.46	3.45	118.89	2.56	0.13	0.78
39.04	79.05	33.59	3.69	124.07	2.59	0.13	0.78
39.11	82.53	35.22	3.56	125.32	2.58	0.13	0.78
39.20	78.48	32.85	3.98	130.89	2.63	0.13	0.63
39.26	75.09	30.96	4.36	134.88	2.67	0.13	0.62
39.32	69.63	28.09	4.98	140.02	2.73	0.12	0.62
39.38	64.92	26.08	5.54	144.56	2.77	0.12	0.62
39.44	62.28	24.94	5.88	146.68	2.80	0.12	0.62
39.53	61.06	24.37	5.89	143.50	2.80	0.11	0.62
39.59	55.79	22.14	6.32	139.97	2.84	0.11	0.62
39.65	47.50	18.67	7.41	138.40	2.91	0.10	0.62
39.71	41.10	16.00	7.32	117.09	2.91	0.10	0.62
39.77	36.76	14.18	5.78	81.99	2.79	0.09	0.62
39.86	32.43	12.36	7.65	94.55	2.93	0.09	0.62
39.92	31.40	11.92	8.50	101.32	2.98	0.09	0.62
39.98	33.38	12.71	8.29	105.37	2.97	0.09	0.62
40.04	39.59	15.24	7.07	107.80	2.89	0.09	0.62
40.10	41.30	15.92	7.22	114.98	2.90	0.10	0.62
40.16	84.80	36.73	2.62	96.16	2.44	0.13	0.78
40.22	120.02	55.96	1.71	95.55	2.23	0.16	0.82
40.30	139.70	66.58	1.54	102.81	2.17	0.18	0.84
40.37	152.60	73.36	1.49	109.19	2.14	0.21	0.85
40.43	155.99	74.89	1.49	111.60	2.14	0.22	0.85
40.51	161.08	77.48	1.47	114.11	2.13	0.23	0.86
40.57	163.05	78.22	1.48	115.76	2.14	0.24	0.86
40.63	163.99	78.35	1.50	117.20	2.15	0.25	0.86
40.69	165.03	78.57	1.51	118.51	2.15	0.25	0.86
40.78	167.57	79.59	1.51	120.33	2.15	0.26	0.87
40.84	167.01	78.94	1.53	121.01	2.16	0.26	0.87
40.90	165.78	77.95	1.56	121.38	2.18	0.26	0.87
40.95	165.03	77.26	1.58	121.85	2.18	0.26	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
41.01	164.94	76.95	1.59	122.53	2.19	0.26	0.87
41.10	164.09	76.17	1.61	122.84	2.20	0.26	0.87
41.16	164.28	76.16	1.61	122.77	2.20	0.26	0.87
41.22	164.47	76.17	1.61	122.54	2.20	0.26	0.87
41.28	164.75	76.17	1.61	122.71	2.20	0.26	0.87
41.34	165.97	76.67	1.61	123.20	2.20	0.27	0.87
41.41	168.51	77.90	1.59	124.05	2.19	0.28	0.87
41.49	172.47	79.75	1.58	125.85	2.18	0.29	0.88
41.55	174.64	80.72	1.57	126.91	2.18	0.30	0.88
41.61	176.42	81.45	1.57	127.99	2.18	0.31	0.88
41.68	178.03	82.04	1.57	129.17	2.18	0.32	0.88
41.73	179.63	82.62	1.58	130.44	2.19	0.33	0.88
41.83	182.73	83.83	1.58	132.75	2.19	0.35	0.89
41.89	184.71	84.57	1.59	134.33	2.19	0.37	0.89
41.95	187.35	85.72	1.58	135.80	2.19	0.39	0.89
42.01	189.42	86.59	1.58	136.98	2.19	0.40	0.89
42.06	190.83	87.20	1.58	137.37	2.18	0.41	0.90
42.16	190.17	86.74	1.57	136.39	2.18	0.40	0.89
42.22	187.91	85.26	1.60	136.20	2.19	0.39	0.89
42.28	184.71	83.25	1.63	136.05	2.21	0.38	0.89
42.34	181.04	81.07	1.67	135.46	2.22	0.36	0.89
42.40	177.55	79.08	1.70	134.53	2.23	0.34	0.88
42.48	164.28	71.76	1.85	132.91	2.28	0.28	0.87
42.54	167.01	73.27	1.80	131.64	2.26	0.29	0.87
42.60	163.05	71.09	1.84	130.80	2.28	0.28	0.87
42.66	158.82	68.74	1.89	130.24	2.29	0.26	0.87
42.72	154.48	66.37	1.95	129.72	2.31	0.25	0.86
42.78	150.34	64.17	2.01	128.84	2.32	0.24	0.86
42.87	145.82	61.76	2.07	127.70	2.34	0.22	0.85
42.93	143.47	60.51	2.10	126.89	2.34	0.22	0.85
42.99	142.62	60.05	2.10	125.96	2.34	0.22	0.85
43.05	142.24	59.81	2.09	125.29	2.34	0.21	0.85
43.11	142.34	59.81	2.08	124.70	2.34	0.21	0.85
43.20	142.81	59.98	2.06	123.83	2.33	0.21	0.85
43.26	142.71	59.87	2.06	123.39	2.33	0.21	0.85
43.32	142.71	59.78	2.06	123.20	2.33	0.21	0.85
43.38	142.24	59.42	2.07	123.27	2.34	0.21	0.85
43.44	140.45	58.40	2.11	123.30	2.35	0.21	0.85
43.51	138.38	57.25	2.15	123.23	2.35	0.20	0.84
43.59	134.99	55.42	2.22	122.97	2.37	0.20	0.84
43.65	132.73	54.24	2.26	122.42	2.38	0.19	0.84
43.71	130.09	52.87	2.31	121.90	2.39	0.19	0.83
43.77	127.55	51.60	2.35	121.06	2.39	0.18	0.83
43.83	124.35	49.98	2.41	120.44	2.41	0.18	0.83
43.92	118.42	46.99	2.54	119.51	2.43	0.17	0.82
43.98	113.24	44.42	2.69	119.62	2.46	0.16	0.81
44.05	106.18	40.89	2.97	121.63	2.50	0.15	0.81
44.10	97.89	37.15	3.20	118.78	2.53	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
44.16	88.76	33.02	3.53	116.64	2.57	0.13	0.78
44.23	80.47	29.03	4.18	121.30	2.65	0.13	0.62
44.32	70.77	25.04	5.06	126.77	2.73	0.12	0.62
44.38	65.97	23.24	5.59	129.82	2.78	0.11	0.62
44.43	60.79	21.31	6.25	133.22	2.83	0.11	0.62
44.49	68.13	23.97	5.37	128.64	2.76	0.12	0.62
44.57	67.76	23.79	5.39	128.22	2.76	0.12	0.62
44.63	68.23	23.93	5.33	127.51	2.76	0.12	0.62
44.70	65.97	23.06	5.55	128.05	2.78	0.11	0.62
44.77	68.32	23.88	5.29	126.25	2.75	0.12	0.62
44.82	69.83	24.40	5.14	125.39	2.74	0.12	0.62
44.88	73.31	25.62	4.78	122.42	2.71	0.12	0.62
44.97	80.47	28.36	4.25	120.61	2.65	0.13	0.62
45.03	90.54	32.90	3.57	117.47	2.58	0.13	0.79
45.10	102.88	38.61	2.95	113.70	2.50	0.15	0.80
45.16	112.20	42.99	2.60	111.57	2.44	0.16	0.81
45.22	116.35	44.98	2.46	110.71	2.42	0.16	0.82
45.28	118.61	46.10	2.37	109.23	2.40	0.16	0.82
45.37	122.37	47.96	2.24	107.22	2.37	0.17	0.82
45.43	125.01	49.22	2.17	106.59	2.36	0.17	0.82
45.49	127.93	50.62	2.09	105.98	2.34	0.17	0.83
45.55	131.13	52.13	2.03	105.86	2.33	0.18	0.83
45.61	135.56	54.19	1.96	106.37	2.31	0.18	0.83
45.67	140.08	56.32	1.90	106.78	2.29	0.19	0.84
45.76	143.00	57.54	1.87	107.72	2.29	0.20	0.84
45.82	142.15	56.99	1.89	107.82	2.29	0.19	0.84
45.88	139.23	55.46	1.94	107.54	2.30	0.19	0.84
45.94	135.65	53.67	1.99	106.77	2.32	0.18	0.83
46.00	131.22	51.53	2.05	105.55	2.33	0.18	0.83
46.09	125.39	48.78	2.12	103.50	2.35	0.17	0.82
46.15	122.56	47.41	2.17	102.67	2.36	0.16	0.82
46.21	119.17	45.74	2.24	102.38	2.37	0.16	0.82
46.27	115.40	43.87	2.33	102.44	2.39	0.15	0.81
46.33	111.07	41.68	2.49	103.59	2.42	0.15	0.81
46.42	104.86	38.37	2.81	107.97	2.48	0.15	0.80
46.48	102.03	38.00	2.51	95.35	2.42	0.14	0.79
46.54	100.15	38.22	2.16	82.39	2.36	0.13	0.79
46.60	99.87	37.78	2.24	84.77	2.37	0.13	0.79
46.66	100.43	37.84	2.28	86.34	2.38	0.13	0.79
46.72	100.06	37.47	2.34	87.78	2.39	0.13	0.79
46.80	92.33	33.52	2.73	91.40	2.46	0.13	0.78
46.86	95.05	34.70	2.63	91.20	2.45	0.13	0.78
46.93	95.43	34.77	2.64	91.68	2.45	0.13	0.79
46.98	94.11	34.04	2.73	92.82	2.46	0.13	0.78
47.07	88.37	31.20	3.08	96.17	2.51	0.13	0.78
47.13	83.57	28.94	3.40	98.29	2.56	0.12	0.77
47.19	79.05	26.90	3.70	99.44	2.59	0.12	0.77
47.25	74.62	24.93	4.01	99.96	2.63	0.12	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
47.31	70.10	23.10	4.42	102.13	2.67	0.11	0.62
47.40	62.94	20.60	5.16	106.18	2.74	0.11	0.62
47.46	57.20	18.60	5.88	109.46	2.80	0.10	0.62
47.52	50.04	16.13	6.98	112.52	2.88	0.10	0.62
47.58	43.36	13.82	8.23	113.79	2.97	0.10	0.62
47.64	37.90	11.94	9.59	114.46	3.05	0.09	0.85
47.73	31.77	9.83	11.47	112.70	3.14	0.09	0.70
47.79	29.23	8.95	12.22	109.36	3.18	0.08	0.64
47.85	30.17	9.26	11.19	103.57	3.13	0.08	0.66
47.91	34.51	10.72	8.94	95.79	3.01	0.09	0.77
47.97	40.45	12.72	6.97	88.69	2.88	0.09	0.62
48.03	46.66	14.80	5.75	85.12	2.79	0.09	0.62
48.12	50.81	16.18	5.11	82.73	2.74	0.10	0.62
48.18	50.89	16.18	5.22	84.50	2.75	0.10	0.62
48.24	48.54	15.37	5.90	90.69	2.80	0.10	0.62
48.30	44.49	13.99	6.98	97.68	2.88	0.09	0.62
48.36	39.97	12.45	8.24	102.51	2.97	0.09	0.62
48.45	34.98	10.75	9.53	102.39	3.04	0.09	0.77
48.51	35.12	10.78	9.05	97.56	3.02	0.09	0.77
48.57	35.12	10.77	8.85	95.29	3.00	0.09	0.77
48.63	35.27	10.80	8.82	95.26	3.00	0.09	0.77
48.69	36.95	11.35	8.32	94.42	2.97	0.09	0.62
48.78	35.36	10.79	8.01	86.43	2.95	0.09	0.62
48.84	33.47	10.15	9.45	95.95	3.04	0.09	0.73
48.90	32.63	9.86	10.54	103.87	3.10	0.09	0.70
48.96	33.57	10.16	10.66	108.26	3.10	0.09	0.73
49.03	34.70	10.52	10.52	110.70	3.10	0.09	0.75
49.09	35.65	10.82	10.37	112.17	3.09	0.09	0.77
49.15	30.94	9.24	12.76	117.94	3.20	0.09	0.66
49.21	57.68	18.07	5.93	107.10	2.81	0.10	0.62
49.30	75.76	24.01	4.24	101.87	2.65	0.12	0.62
49.36	93.65	31.31	3.14	98.34	2.52	0.13	0.78
49.42	103.07	35.19	2.81	98.91	2.47	0.14	0.79
49.48	116.82	41.16	2.39	98.56	2.40	0.15	0.81
49.55	132.54	48.23	2.03	98.06	2.33	0.17	0.83
49.61	143.47	53.30	1.84	98.15	2.28	0.19	0.84
49.70	157.50	62.90	1.42	89.01	2.10	0.18	0.83
49.76	164.28	66.88	1.35	90.53	2.05	0.18	0.83
49.82	168.61	68.48	1.36	93.01	2.05	0.19	0.84
49.88	170.48	68.76	1.38	94.58	2.07	0.20	0.84
49.94	171.33	68.59	1.40	95.74	2.08	0.20	0.85
50.00	169.92	67.34	1.43	96.06	2.11	0.21	0.85
50.07	156.25	60.00	1.56	93.41	2.18	0.19	0.84
50.14	162.19	62.71	1.52	95.15	2.16	0.20	0.85
50.20	163.97	63.37	1.51	95.97	2.16	0.21	0.85
50.27	164.27	63.71	1.49	94.99	2.14	0.20	0.85
50.34	164.74	65.89	1.37	90.34	2.06	0.18	0.83
50.41	167.00	65.49	1.43	93.93	2.11	0.20	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
50.46	165.21	64.21	1.46	94.04	2.13	0.20	0.85
50.54	161.44	61.87	1.52	94.02	2.16	0.20	0.84
50.61	158.90	60.22	1.57	94.47	2.18	0.20	0.84
50.67	156.59	58.73	1.62	95.20	2.20	0.20	0.84
50.74	151.74	55.93	1.72	96.34	2.24	0.19	0.84
50.79	154.47	57.00	1.71	97.38	2.24	0.20	0.84
50.85	154.66	56.87	1.72	98.09	2.24	0.20	0.84
50.94	154.57	56.42	1.76	99.56	2.25	0.20	0.85
51.01	154.76	56.24	1.79	100.64	2.26	0.21	0.85
51.06	154.85	56.16	1.80	100.83	2.26	0.21	0.85
51.13	155.13	56.18	1.80	100.94	2.26	0.21	0.85
51.18	156.17	56.47	1.80	101.65	2.26	0.21	0.85
51.27	158.15	57.22	1.78	101.96	2.26	0.21	0.85
51.33	159.46	57.81	1.76	101.66	2.25	0.21	0.85
51.38	158.81	57.47	1.76	101.34	2.25	0.21	0.85
51.46	158.43	57.23	1.76	100.90	2.25	0.21	0.85
51.52	158.24	57.07	1.77	100.77	2.25	0.21	0.85
51.58	157.20	56.80	1.74	98.90	2.25	0.21	0.85
51.64	156.55	57.01	1.68	95.64	2.22	0.20	0.84
51.73	159.18	57.56	1.72	98.72	2.24	0.21	0.85
51.79	163.51	59.38	1.68	99.79	2.23	0.22	0.85
51.85	170.11	62.40	1.61	100.75	2.20	0.23	0.86
51.91	177.83	66.13	1.54	101.67	2.17	0.25	0.86
51.98	164.83	59.76	1.67	99.60	2.22	0.22	0.85
52.05	186.58	70.18	1.48	103.57	2.13	0.27	0.87
52.10	187.71	70.56	1.47	104.02	2.13	0.27	0.87
52.18	187.15	70.11	1.48	103.91	2.14	0.27	0.87
52.23	186.68	69.85	1.48	103.53	2.14	0.27	0.87
52.31	186.49	69.82	1.47	102.87	2.13	0.26	0.87
52.36	184.14	68.66	1.48	101.95	2.14	0.26	0.87
52.44	179.52	66.18	1.53	101.14	2.16	0.25	0.86
52.51	174.91	63.83	1.57	100.17	2.18	0.24	0.86
52.57	171.71	62.22	1.60	99.55	2.19	0.23	0.86
52.63	169.73	61.21	1.62	99.13	2.20	0.23	0.86
52.72	162.95	57.88	1.70	98.31	2.23	0.21	0.85
52.77	158.52	55.79	1.75	97.65	2.25	0.21	0.85
52.84	154.29	53.81	1.80	97.06	2.27	0.20	0.84
52.90	150.14	51.84	1.87	96.94	2.29	0.19	0.84
52.95	146.19	49.99	1.94	97.09	2.30	0.19	0.84
53.04	140.35	47.31	2.06	97.40	2.33	0.18	0.83
53.10	137.62	46.06	2.12	97.55	2.35	0.18	0.83
53.16	135.55	45.16	2.16	97.34	2.36	0.17	0.83
53.23	133.85	44.45	2.18	96.88	2.36	0.17	0.82
53.29	132.63	43.91	2.20	96.72	2.37	0.17	0.82
53.35	131.59	43.45	2.22	96.53	2.37	0.17	0.82
53.44	129.33	42.48	2.27	96.23	2.38	0.16	0.82
53.50	126.98	41.43	2.33	96.47	2.39	0.16	0.82
53.56	122.27	39.35	2.46	96.88	2.42	0.16	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
53.62	117.28	37.27	2.60	97.07	2.44	0.15	0.81
53.67	117.61	37.49	2.55	95.74	2.43	0.15	0.81
53.76	115.87	36.89	2.55	94.17	2.43	0.15	0.80
53.82	117.94	37.92	2.42	91.81	2.41	0.15	0.81
53.88	117.84	38.39	2.27	87.22	2.38	0.15	0.80
53.94	117.17	38.66	2.12	82.12	2.35	0.14	0.80
54.00	115.76	37.92	2.19	83.06	2.36	0.14	0.80
54.09	112.47	36.40	2.30	83.89	2.39	0.14	0.80
54.16	110.02	35.17	2.42	85.10	2.41	0.14	0.79
54.22	106.92	33.71	2.58	86.94	2.44	0.14	0.79
54.27	100.23	30.81	2.91	89.74	2.49	0.13	0.79
54.34	101.46	31.20	2.90	90.57	2.49	0.13	0.79
54.41	102.40	31.47	2.90	91.34	2.49	0.13	0.79
54.47	104.85	32.44	2.80	90.90	2.47	0.14	0.79
54.56	109.46	34.49	2.55	87.81	2.43	0.14	0.79
54.62	111.71	35.60	2.40	85.46	2.41	0.14	0.80
54.68	111.35	35.61	2.36	84.17	2.40	0.14	0.80
54.74	110.30	35.22	2.37	83.58	2.40	0.14	0.79
54.80	108.80	34.51	2.42	83.55	2.41	0.14	0.79
54.86	106.83	33.66	2.49	83.87	2.42	0.13	0.79
54.95	103.25	32.14	2.63	84.38	2.44	0.13	0.79
55.01	100.89	31.12	2.73	85.07	2.46	0.13	0.78
55.07	98.26	30.00	2.86	85.91	2.48	0.13	0.78
55.13	96.84	29.36	2.95	86.68	2.50	0.13	0.78
55.19	98.35	29.92	2.90	86.76	2.49	0.13	0.78
55.28	97.88	29.70	2.92	86.79	2.49	0.13	0.78
55.34	98.43	30.00	2.85	85.42	2.48	0.13	0.78
55.40	99.29	30.34	2.80	84.98	2.47	0.13	0.78
55.45	100.41	30.76	2.76	84.91	2.47	0.13	0.78
55.51	100.80	30.92	2.73	84.44	2.46	0.13	0.78
55.60	100.33	30.61	2.80	85.55	2.47	0.13	0.78
55.66	99.29	30.05	2.90	87.22	2.49	0.13	0.78
55.73	98.07	29.34	3.07	89.99	2.51	0.13	0.78
55.79	97.22	28.77	3.23	92.98	2.54	0.13	0.78
55.84	98.63	29.19	3.23	94.29	2.54	0.13	0.78
55.94	107.48	32.68	2.83	92.35	2.48	0.14	0.79
56.00	115.96	36.39	2.41	87.83	2.41	0.14	0.80
56.06	124.81	40.54	2.07	83.85	2.34	0.15	0.81
56.12	131.40	43.90	1.83	80.34	2.27	0.15	0.81
56.18	137.99	47.19	1.67	78.86	2.22	0.16	0.82
56.24	141.76	48.94	1.62	79.06	2.20	0.16	0.82
56.30	143.46	49.79	1.58	78.90	2.19	0.16	0.82
56.39	146.09	50.97	1.55	79.26	2.17	0.16	0.82
56.43	146.05	50.89	1.56	79.37	2.18	0.16	0.82
56.50	146.00	50.69	1.57	79.81	2.18	0.16	0.82
56.56	149.11	51.90	1.56	81.00	2.18	0.17	0.83
56.65	150.05	51.93	1.59	82.39	2.19	0.17	0.83
56.71	149.95	51.58	1.62	83.37	2.20	0.17	0.83

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
56.77	149.48	51.13	1.65	84.12	2.21	0.17	0.83
56.84	149.29	50.89	1.66	84.57	2.22	0.17	0.83
56.89	149.58	50.93	1.67	84.81	2.22	0.17	0.83
56.98	151.08	51.51	1.65	85.14	2.22	0.18	0.83
57.04	152.31	51.98	1.64	85.49	2.21	0.18	0.83
57.10	153.34	52.31	1.64	86.01	2.21	0.18	0.83
57.16	154.57	52.74	1.64	86.52	2.21	0.18	0.84
57.22	156.45	53.48	1.63	87.05	2.21	0.19	0.84
57.31	162.01	55.95	1.57	87.94	2.18	0.19	0.84
57.37	166.43	57.97	1.53	88.66	2.16	0.20	0.84
57.43	171.71	60.39	1.49	89.80	2.14	0.21	0.85
57.49	176.04	62.31	1.46	91.04	2.13	0.21	0.85
57.55	179.52	63.84	1.44	92.11	2.12	0.22	0.85
57.61	182.25	65.07	1.43	92.90	2.11	0.22	0.85
57.70	186.30	66.90	1.41	94.14	2.09	0.23	0.86
57.76	188.47	67.83	1.40	94.90	2.09	0.23	0.86
57.82	190.35	68.54	1.40	95.71	2.08	0.24	0.86
57.88	191.76	69.02	1.40	96.36	2.08	0.24	0.86
57.94	194.12	69.96	1.39	97.33	2.08	0.25	0.86
58.03	197.70	71.38	1.38	98.82	2.07	0.26	0.87
58.09	199.86	72.17	1.38	99.80	2.07	0.27	0.87
58.16	201.56	72.71	1.38	100.66	2.07	0.28	0.87
58.22	204.10	73.65	1.38	101.81	2.07	0.29	0.87
58.28	207.49	74.99	1.38	103.27	2.07	0.30	0.88
58.34	211.63	76.77	1.37	104.91	2.06	0.32	0.88
58.42	217.47	79.30	1.35	107.25	2.05	0.34	0.88
58.48	219.26	79.87	1.35	108.13	2.05	0.36	0.88
58.55	220.67	80.27	1.36	108.85	2.05	0.37	0.89
58.60	222.74	81.01	1.36	109.80	2.05	0.38	0.89
58.67	225.29	82.06	1.35	110.84	2.05	0.40	0.89
58.75	229.71	84.02	1.34	112.57	2.04	0.43	0.89
58.81	232.73	85.16	1.34	113.93	2.03	0.45	0.90
58.87	235.36	88.37	1.29	113.82	1.98	0.39	0.88
58.94	238.38	92.83	1.23	114.41	1.89	0.30	0.85
59.00	240.26	92.95	1.24	115.40	1.91	0.33	0.86
59.06	241.20	92.70	1.25	115.92	1.92	0.35	0.87
59.15	240.35	91.40	1.26	115.59	1.94	0.38	0.88
59.20	227.92	84.71	1.30	110.05	1.99	0.35	0.88
59.27	227.97	84.29	1.31	110.19	2.00	0.36	0.88
59.32	228.02	83.98	1.31	110.31	2.01	0.37	0.88
59.40	231.60	85.13	1.32	112.06	2.01	0.40	0.89
59.46	235.17	86.24	1.32	113.86	2.02	0.44	0.89
59.53	239.60	87.82	1.32	115.96	2.02	0.49	0.90
59.58	242.24	88.79	1.32	117.18	2.01	0.53	0.90
59.66	246.30	90.37	1.32	118.99	2.01	0.58	0.90
59.73	250.05	91.77	1.32	120.70	2.01	0.64	0.91
59.79	252.13	95.41	1.26	120.58	1.94	0.48	0.89
59.86	253.35	107.60	1.00	107.60	1.68	0.26	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
59.93	254.58	107.02	1.00	107.02	1.71	0.27	0.82
59.98	254.01	105.89	1.04	109.73	1.72	0.27	0.82
60.05	253.07	104.33	1.08	112.57	1.75	0.26	0.82
60.12	250.24	101.51	1.13	114.65	1.78	0.26	0.82
60.19	234.14	91.13	1.21	110.69	1.87	0.25	0.83
60.24	240.82	93.33	1.22	114.01	1.88	0.29	0.85
60.32	238.75	90.10	1.26	113.48	1.93	0.35	0.87
60.38	235.55	87.43	1.28	112.20	1.97	0.37	0.88
60.44	232.35	85.13	1.30	110.99	2.00	0.38	0.88
60.50	231.31	84.02	1.32	110.80	2.01	0.40	0.89
60.59	231.60	83.55	1.33	111.19	2.03	0.42	0.89
60.65	231.31	83.12	1.34	111.20	2.03	0.42	0.89
60.71	229.62	82.09	1.35	110.65	2.04	0.42	0.89
60.77	227.36	80.85	1.36	109.85	2.05	0.41	0.89
60.83	226.32	80.32	1.36	109.39	2.06	0.41	0.89
60.89	228.02	81.15	1.35	109.87	2.05	0.41	0.89
60.98	234.14	84.08	1.33	112.06	2.03	0.44	0.89
61.04	237.81	85.84	1.32	113.43	2.02	0.46	0.89
61.10	240.54	87.06	1.32	114.52	2.01	0.48	0.90
61.16	241.86	87.49	1.32	115.09	2.01	0.49	0.90
61.22	242.14	87.50	1.32	115.18	2.01	0.51	0.90
61.31	242.19	87.45	1.32	115.10	2.01	0.50	0.90
61.37	241.77	87.14	1.32	114.89	2.01	0.50	0.90
61.43	242.24	87.23	1.32	115.06	2.01	0.51	0.90
61.49	242.80	87.38	1.32	115.27	2.01	0.52	0.90
61.55	243.18	87.47	1.32	115.38	2.01	0.52	0.90
61.64	244.31	87.99	1.32	115.71	2.01	0.53	0.90
61.70	245.82	88.76	1.31	116.22	2.00	0.53	0.90
61.76	248.08	89.93	1.30	117.06	1.99	0.54	0.90
61.82	250.24	91.78	1.28	117.63	1.97	0.50	0.89
61.88	252.50	94.83	1.25	118.19	1.91	0.41	0.87
61.94	254.29	95.26	1.25	119.01	1.92	0.43	0.88
62.04	255.43	95.55	1.25	119.45	1.92	0.45	0.88
62.10	256.55	95.95	1.25	119.92	1.92	0.46	0.88
62.16	260.70	97.88	1.24	121.74	1.91	0.48	0.88
62.22	260.93	97.94	1.24	121.78	1.91	0.48	0.88
62.29	261.17	98.23	1.24	121.76	1.90	0.47	0.88
62.34	266.73	101.18	1.23	124.12	1.88	0.48	0.87
62.43	269.65	102.62	1.22	125.28	1.88	0.49	0.87
62.49	270.12	102.79	1.22	125.42	1.88	0.50	0.87
62.55	270.59	102.89	1.22	125.58	1.88	0.50	0.87
62.61	271.53	103.10	1.22	125.98	1.88	0.52	0.88
62.67	272.47	103.52	1.22	126.31	1.88	0.52	0.88
62.73	271.44	103.18	1.22	125.72	1.87	0.50	0.87
62.82	270.21	102.62	1.22	125.04	1.87	0.49	0.87
62.88	269.37	102.18	1.22	124.60	1.87	0.48	0.87
62.94	268.80	101.96	1.22	124.24	1.87	0.47	0.87
63.00	268.80	101.99	1.22	124.15	1.87	0.47	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
63.06	268.24	101.69	1.22	123.82	1.87	0.46	0.87
63.12	266.17	100.60	1.22	122.86	1.88	0.45	0.87
63.21	264.38	99.74	1.22	121.95	1.88	0.44	0.87
63.27	262.59	98.97	1.22	121.06	1.88	0.42	0.87
63.33	259.95	97.90	1.22	119.76	1.88	0.40	0.86
63.40	254.02	95.25	1.23	117.00	1.89	0.36	0.86
63.46	246.77	92.02	1.23	113.64	1.90	0.33	0.86
63.55	229.44	83.93	1.26	105.69	1.93	0.28	0.86
63.60	214.00	76.47	1.29	98.76	1.98	0.25	0.86
63.66	196.28	67.80	1.35	91.72	2.05	0.23	0.85
63.73	179.05	59.78	1.44	86.23	2.12	0.21	0.85
63.78	164.36	53.19	1.56	82.93	2.18	0.19	0.84
63.87	141.86	42.98	1.95	83.93	2.31	0.17	0.82
63.94	128.77	37.05	2.41	89.37	2.41	0.16	0.81
63.99	114.64	31.11	3.15	98.02	2.52	0.15	0.80
64.05	97.69	25.81	4.02	103.76	2.63	0.13	0.63
64.12	81.21	21.26	4.93	104.69	2.72	0.12	0.62
64.18	69.25	17.95	6.28	112.79	2.83	0.11	0.62
64.27	64.36	16.59	6.91	114.66	2.88	0.11	0.62
64.33	61.54	15.81	7.33	115.86	2.91	0.10	0.62
64.39	55.80	14.22	8.36	118.95	2.97	0.10	0.62
64.44	55.70	14.19	8.46	119.98	2.98	0.10	0.62
64.51	66.73	17.20	6.67	114.77	2.86	0.11	0.62
64.57	83.69	21.84	4.83	105.47	2.71	0.12	0.62
64.63	109.78	29.51	3.17	93.40	2.53	0.14	0.79
64.72	147.54	44.56	1.92	85.37	2.30	0.18	0.83
64.79	162.88	51.07	1.67	85.39	2.22	0.19	0.84
64.85	173.81	55.96	1.54	86.21	2.17	0.21	0.85
64.91	181.72	59.43	1.48	87.78	2.14	0.22	0.85
64.96	187.37	61.51	1.46	90.00	2.13	0.23	0.86
65.05	196.13	64.35	1.47	94.32	2.13	0.26	0.87
65.11	203.28	66.86	1.46	97.45	2.12	0.29	0.88
65.18	210.34	69.73	1.43	99.77	2.11	0.32	0.88
65.23	219.10	73.68	1.39	102.30	2.08	0.35	0.89
65.29	228.71	78.06	1.35	105.52	2.05	0.39	0.89
65.38	243.21	84.66	1.31	111.09	2.01	0.47	0.90
65.44	251.12	88.34	1.29	114.32	1.98	0.52	0.90
65.50	257.62	91.36	1.28	117.05	1.97	0.57	0.90
65.56	262.42	93.49	1.27	119.11	1.96	0.61	0.90
65.63	266.37	95.27	1.27	120.79	1.95	0.65	0.90
65.69	269.20	96.52	1.26	121.98	1.94	0.68	0.90
65.77	273.72	98.45	1.26	123.91	1.93	0.73	0.90
65.83	277.30	99.93	1.26	125.45	1.93	0.79	0.90
65.89	283.32	102.65	1.25	128.07	1.92	0.83	0.90
65.95	290.57	106.06	1.24	131.21	1.90	0.84	0.90
66.01	296.22	108.70	1.23	133.60	1.89	0.84	0.90
66.10	301.88	111.42	1.22	135.90	1.88	0.84	0.90
66.16	303.76	111.86	1.22	136.74	1.88	0.84	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
66.23	303.76	114.20	1.19	135.56	1.83	0.85	0.89
66.29	301.03	115.31	1.15	132.03	1.79	0.68	0.87
66.35	297.07	112.78	1.16	131.31	1.81	0.65	0.87
66.41	292.83	110.25	1.18	130.09	1.83	0.62	0.87
66.47	288.32	107.58	1.20	128.60	1.84	0.61	0.87
66.54	261.10	93.72	1.25	117.19	1.92	0.48	0.88
66.62	262.23	94.20	1.25	117.60	1.92	0.48	0.88
66.69	253.47	90.00	1.26	113.65	1.94	0.43	0.88
66.75	244.53	85.52	1.28	109.72	1.97	0.40	0.88
66.81	233.32	79.74	1.32	105.19	2.01	0.38	0.88
66.86	222.95	74.50	1.36	101.62	2.06	0.35	0.88
66.95	209.30	67.78	1.45	98.21	2.12	0.32	0.88
67.01	202.42	64.50	1.50	97.05	2.15	0.30	0.88
67.07	196.40	61.83	1.55	95.92	2.17	0.28	0.87
67.13	191.69	59.85	1.59	94.86	2.19	0.27	0.87
67.19	186.89	57.85	1.62	93.87	2.20	0.25	0.87
67.28	179.64	54.86	1.69	92.61	2.23	0.24	0.86
67.34	174.55	52.70	1.75	92.20	2.25	0.23	0.86
67.40	170.22	50.88	1.81	92.00	2.27	0.22	0.85
67.46	166.83	49.45	1.86	91.98	2.28	0.21	0.85
67.52	164.48	48.45	1.90	92.03	2.29	0.21	0.85
67.61	167.07	49.43	1.86	92.04	2.28	0.21	0.85
67.67	165.04	48.56	1.90	92.07	2.29	0.21	0.85
67.73	167.30	49.45	1.86	91.99	2.28	0.21	0.85
67.79	171.91	51.26	1.80	92.22	2.26	0.22	0.85
67.85	177.85	53.72	1.72	92.23	2.24	0.23	0.86
67.94	187.64	58.29	1.57	91.36	2.18	0.25	0.86
68.00	193.57	61.12	1.50	91.52	2.15	0.25	0.87
68.06	197.72	63.14	1.45	91.87	2.12	0.26	0.87
68.12	200.45	65.99	1.37	90.10	2.06	0.24	0.86
68.18	202.42	69.86	1.28	89.22	1.96	0.20	0.83
68.24	204.87	70.23	1.29	90.37	1.97	0.21	0.84
68.33	208.73	70.95	1.30	92.20	1.99	0.23	0.85
68.39	212.22	72.43	1.29	93.63	1.98	0.23	0.85
68.45	215.61	73.91	1.29	95.02	1.97	0.24	0.85
68.51	215.56	73.41	1.30	95.07	1.98	0.25	0.86
68.59	215.51	72.72	1.31	95.20	2.00	0.26	0.86
68.65	219.47	74.02	1.31	96.95	2.00	0.28	0.87
68.70	223.71	75.21	1.32	98.91	2.01	0.30	0.87
68.80	232.28	78.00	1.32	102.73	2.01	0.36	0.88
68.86	236.98	79.61	1.32	104.77	2.01	0.39	0.89
68.92	240.47	80.65	1.32	106.33	2.01	0.43	0.89
68.97	243.39	81.38	1.32	107.71	2.02	0.47	0.90
69.04	245.18	81.60	1.33	108.66	2.03	0.51	0.90
69.10	246.31	81.64	1.34	109.31	2.03	0.54	0.90
69.19	250.07	82.79	1.34	110.95	2.04	0.60	0.91
69.25	253.93	84.19	1.34	112.52	2.03	0.65	0.91
69.31	257.04	85.28	1.33	113.80	2.03	0.71	0.91

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
69.36	259.30	86.02	1.33	114.73	2.03	0.75	0.92
69.42	262.31	87.04	1.33	115.98	2.03	0.81	0.92
69.51	265.80	87.96	1.34	117.56	2.03	0.81	0.92
69.57	268.91	88.99	1.34	118.87	2.03	0.81	0.93
69.63	271.54	89.66	1.34	120.10	2.04	0.81	0.93
69.69	274.65	92.85	1.30	120.34	1.99	0.82	0.92
69.75	277.19	97.26	1.24	120.87	1.91	0.63	0.89
69.84	277.39	96.33	1.26	120.95	1.93	0.72	0.90
69.89	264.02	89.66	1.29	115.23	1.97	0.63	0.90
69.96	273.61	93.96	1.27	119.24	1.95	0.73	0.90
70.02	271.59	93.05	1.27	118.30	1.95	0.70	0.90
70.08	258.36	87.06	1.29	112.63	1.98	0.57	0.90
70.15	269.57	92.92	1.26	117.19	1.94	0.60	0.90
70.21	280.58	99.32	1.22	121.67	1.88	0.58	0.88
70.28	300.08	110.16	1.16	128.07	1.81	0.63	0.87
70.35	323.99	123.43	1.06	130.44	1.73	0.86	0.89
70.41	353.19	140.64	1.00	140.64	1.64	0.88	0.91
70.48	375.97	154.42	1.00	154.42	1.58	0.89	0.94
70.55	388.87	161.65	1.00	161.65	1.56	0.90	0.95
70.61	392.74	163.63	1.00	163.63	1.55	0.90	0.95
70.68	390.01	161.68	1.00	161.68	1.56	0.90	0.95
70.74	380.32	155.92	1.00	155.92	1.58	0.89	0.94
70.81	374.20	151.70	1.00	151.70	1.60	0.89	0.93
70.88	373.82	151.09	1.00	151.09	1.61	0.89	0.93
70.95	375.23	151.78	1.00	151.78	1.61	0.89	0.94
71.00	377.87	153.18	1.00	153.18	1.60	0.89	0.94
71.08	387.19	158.59	1.00	158.59	1.58	0.89	0.94
71.14	396.14	164.26	1.00	164.26	1.55	0.90	0.95
71.20	404.52	169.45	1.00	169.45	1.53	0.90	0.95
71.29	411.49	179.54	1.00	179.54	1.45	0.91	0.96
71.35	415.44	184.23	1.00	184.23	1.42	0.92	0.96
71.41	415.72	183.03	1.00	183.03	1.43	0.92	0.96
71.47	413.56	180.12	1.00	180.12	1.45	0.91	0.96
71.53	409.79	175.76	1.00	175.76	1.48	0.91	0.96
71.59	404.52	170.66	1.00	170.66	1.52	0.91	0.95
71.66	362.52	146.13	1.00	146.13	1.60	0.88	0.92
71.72	380.22	155.44	1.00	155.44	1.57	0.89	0.94
71.79	382.49	156.50	1.00	156.50	1.57	0.89	0.94
71.86	381.46	155.87	1.00	155.87	1.57	0.89	0.94
71.92	375.52	152.17	1.00	152.17	1.59	0.89	0.93
71.98	372.70	150.35	1.00	150.35	1.59	0.89	0.93
72.06	370.24	148.86	1.00	148.86	1.60	0.88	0.93
72.13	367.24	147.28	1.00	147.28	1.60	0.88	0.93
72.19	365.34	145.85	1.00	145.85	1.61	0.88	0.93
72.26	364.03	144.46	1.00	144.46	1.62	0.88	0.92
72.32	364.03	143.85	1.00	143.85	1.63	0.88	0.92
72.38	364.03	143.40	1.00	143.40	1.64	0.88	0.92
72.45	366.20	144.36	1.00	144.36	1.63	0.88	0.93

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
72.51	368.65	145.60	1.00	145.60	1.63	0.88	0.93
72.58	371.76	147.11	1.00	147.11	1.62	0.88	0.93
72.65	374.86	148.56	1.00	148.56	1.62	0.88	0.93
72.72	376.94	149.50	1.00	149.50	1.62	0.89	0.94
72.77	377.78	149.79	1.00	149.79	1.62	0.89	0.94
72.84	378.35	150.31	1.00	150.31	1.61	0.89	0.94
72.92	378.73	151.31	1.00	151.31	1.60	0.89	0.94
72.98	377.22	154.41	1.00	154.41	1.55	0.89	0.94
73.04	373.54	156.36	1.00	156.36	1.51	0.89	0.93
73.11	365.53	150.74	1.00	150.74	1.54	0.89	0.92
73.17	359.22	146.30	1.00	146.30	1.56	0.88	0.92
73.24	355.47	143.50	1.00	143.50	1.58	0.88	0.91
73.30	352.08	140.85	1.00	140.85	1.59	0.88	0.91
73.37	333.05	130.32	1.00	130.32	1.63	0.87	0.89
73.44	340.78	134.53	1.00	134.53	1.61	0.87	0.90
73.49	339.55	133.54	1.00	133.54	1.62	0.87	0.90
73.57	339.60	133.06	1.00	133.06	1.63	0.87	0.90
73.63	339.17	132.27	1.00	132.27	1.63	0.87	0.90
73.70	339.65	132.31	1.00	132.31	1.64	0.87	0.90
73.77	342.38	134.05	1.00	134.05	1.62	0.87	0.90
73.83	346.13	136.06	1.00	136.06	1.62	0.87	0.91
73.89	347.93	137.02	1.00	137.02	1.61	0.87	0.91
73.95	351.42	138.94	1.00	138.94	1.60	0.87	0.91
74.04	358.48	143.66	1.00	143.66	1.58	0.88	0.92
74.10	361.02	145.66	1.00	145.66	1.56	0.88	0.92
74.16	361.87	146.22	1.00	146.22	1.56	0.88	0.92
74.22	361.96	147.67	1.00	147.67	1.54	0.88	0.92
74.28	363.56	153.17	1.00	153.17	1.48	0.89	0.92
74.37	362.43	152.37	1.00	152.37	1.48	0.89	0.92
74.43	358.95	149.43	1.00	149.43	1.50	0.89	0.92
74.49	354.15	145.84	1.00	145.84	1.52	0.88	0.91
74.55	347.84	141.14	1.00	141.14	1.55	0.88	0.91
74.62	306.88	117.46	1.00	117.46	1.65	0.59	0.86
74.67	330.42	130.47	1.00	130.47	1.60	0.87	0.89
74.75	329.38	130.12	1.00	130.12	1.59	0.86	0.89
74.82	332.22	131.02	1.00	131.02	1.60	0.87	0.89
74.88	336.92	132.78	1.00	132.78	1.60	0.87	0.90
74.94	337.39	132.72	1.00	132.72	1.60	0.87	0.90
75.00	340.96	134.24	1.00	134.24	1.60	0.87	0.90
75.07	347.56	136.50	1.00	136.50	1.60	0.87	0.91
75.14	357.55	88.18	54.25	4783.80	4.06	0.81	6.30
75.21	364.61	89.93	54.25	4878.37	4.06	0.81	6.42
75.28	368.37	90.84	54.25	4928.14	4.06	0.81	6.49
75.33	370.07	91.25	54.25	4950.43	4.06	0.81	6.52
75.41	362.82	89.42	54.25	4851.05	4.06	0.81	6.39
75.48	353.59	87.10	54.25	4724.85	4.06	0.81	6.22

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
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Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

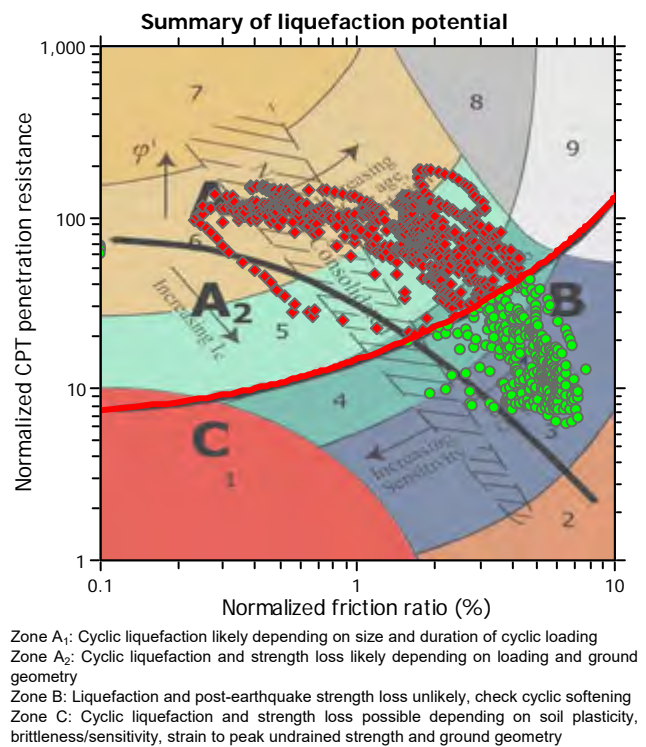
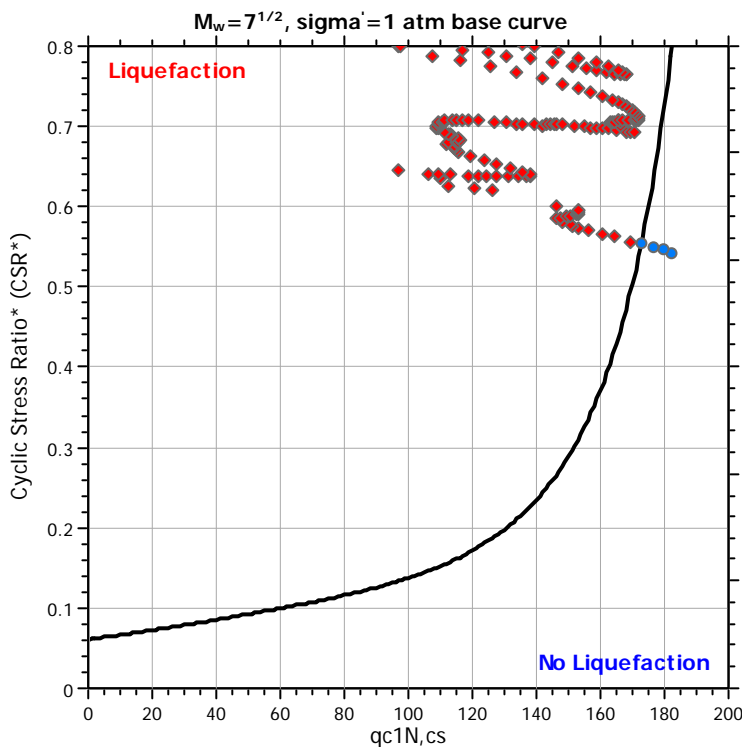
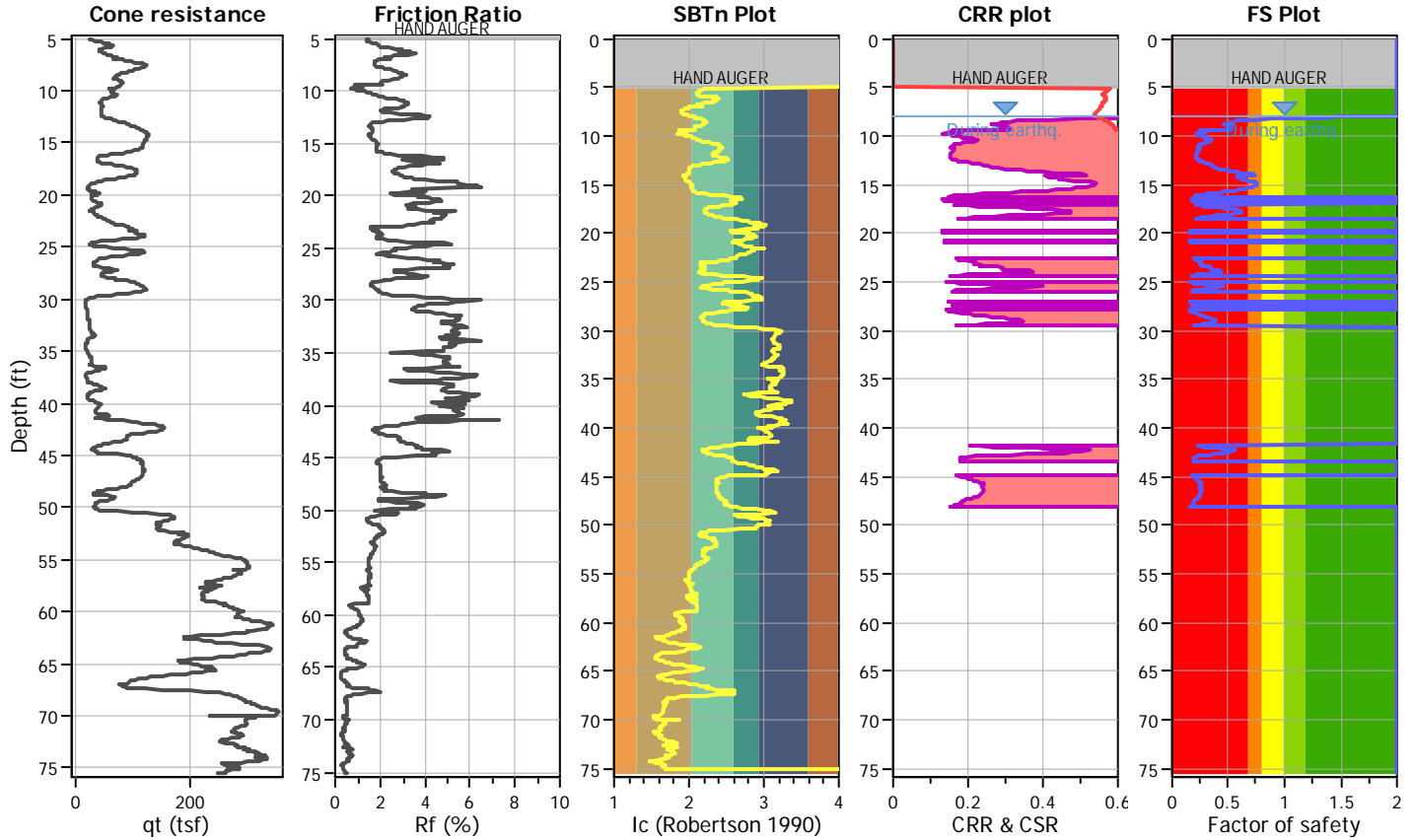
LIQUEFACTION ANALYSIS REPORT

Project title : Universal Engineering Services / Compton
CPT file : CPT-2

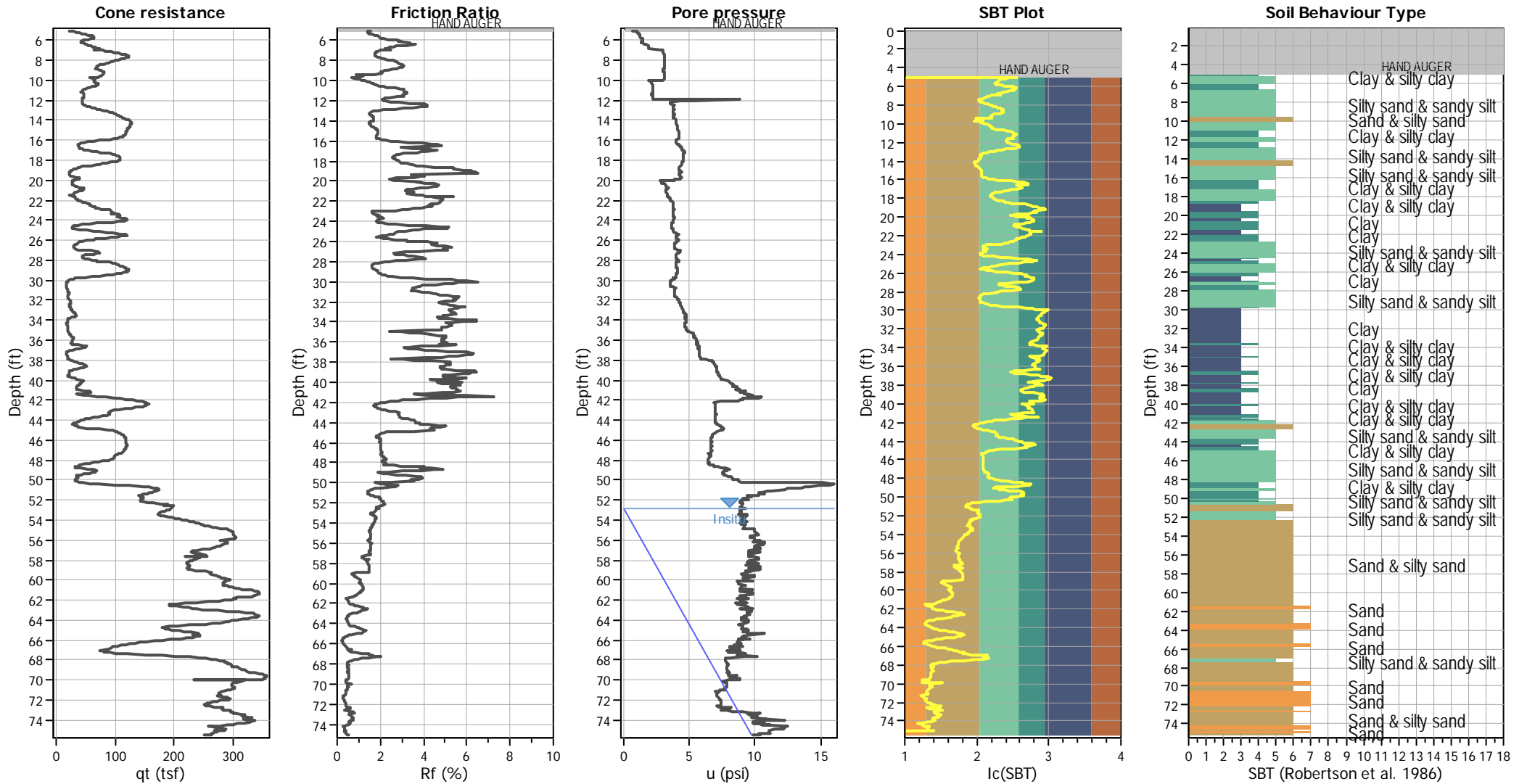
Location : 1111 E. Artesia Blvd, Compton, CA

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	52.90 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	1	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w :	7.30	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method
Peak ground acceleration:	0.77	Unit weight calculation:	Based on SBT	K_g applied:	Yes		



CPT basic interpretation plots



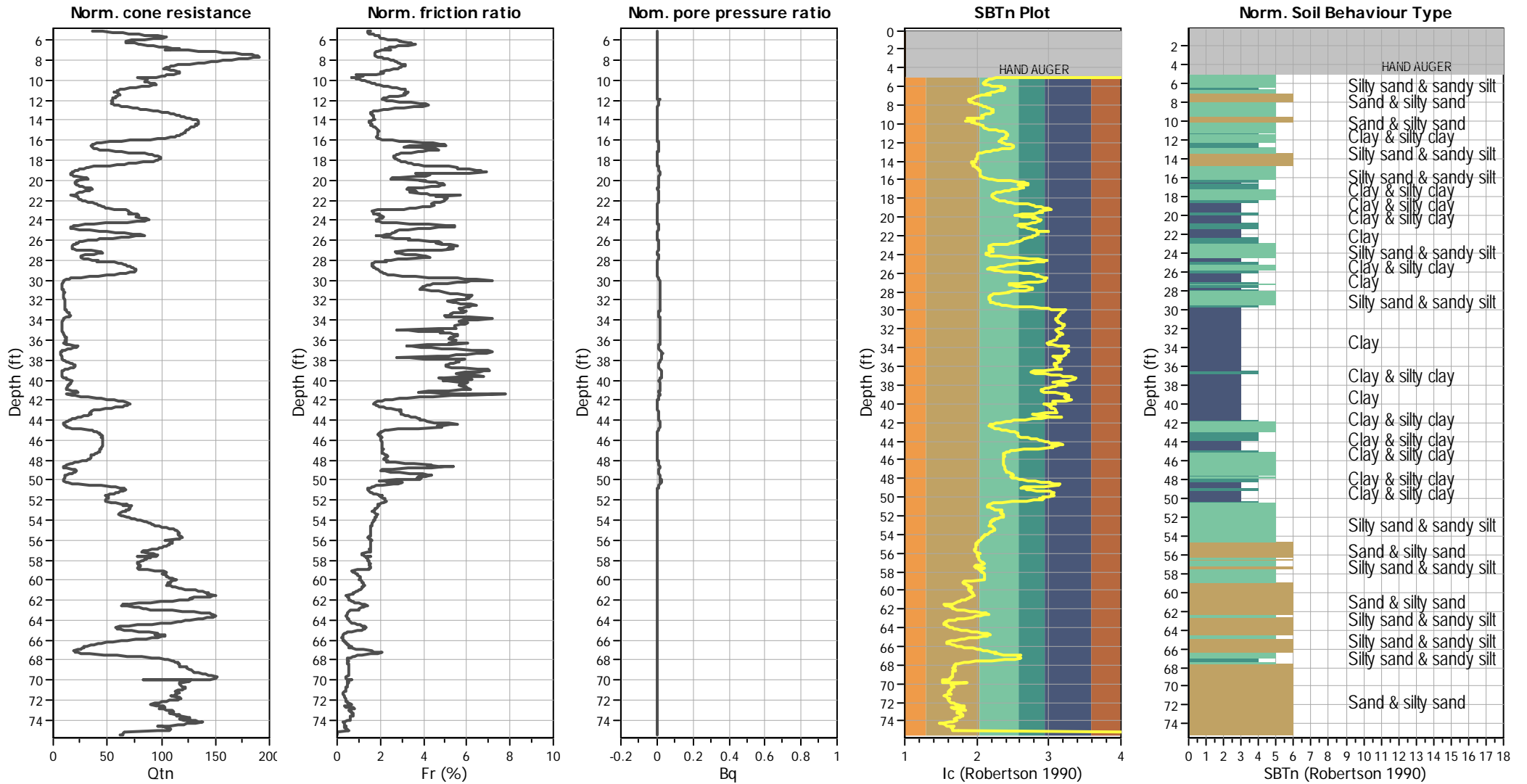
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

■ 1. Sensitive fine grained	■ 4. Clayey silt to silty	■ 7. Gravely sand to sand
■ 2. Organic material	■ 5. Silty sand to sandy silt	■ 8. Very stiff sand to
■ 3. Clay to silty clay	■ 6. Clean sand to silty sand	■ 9. Very stiff fine grained

CPT basic interpretation plots (normalized)



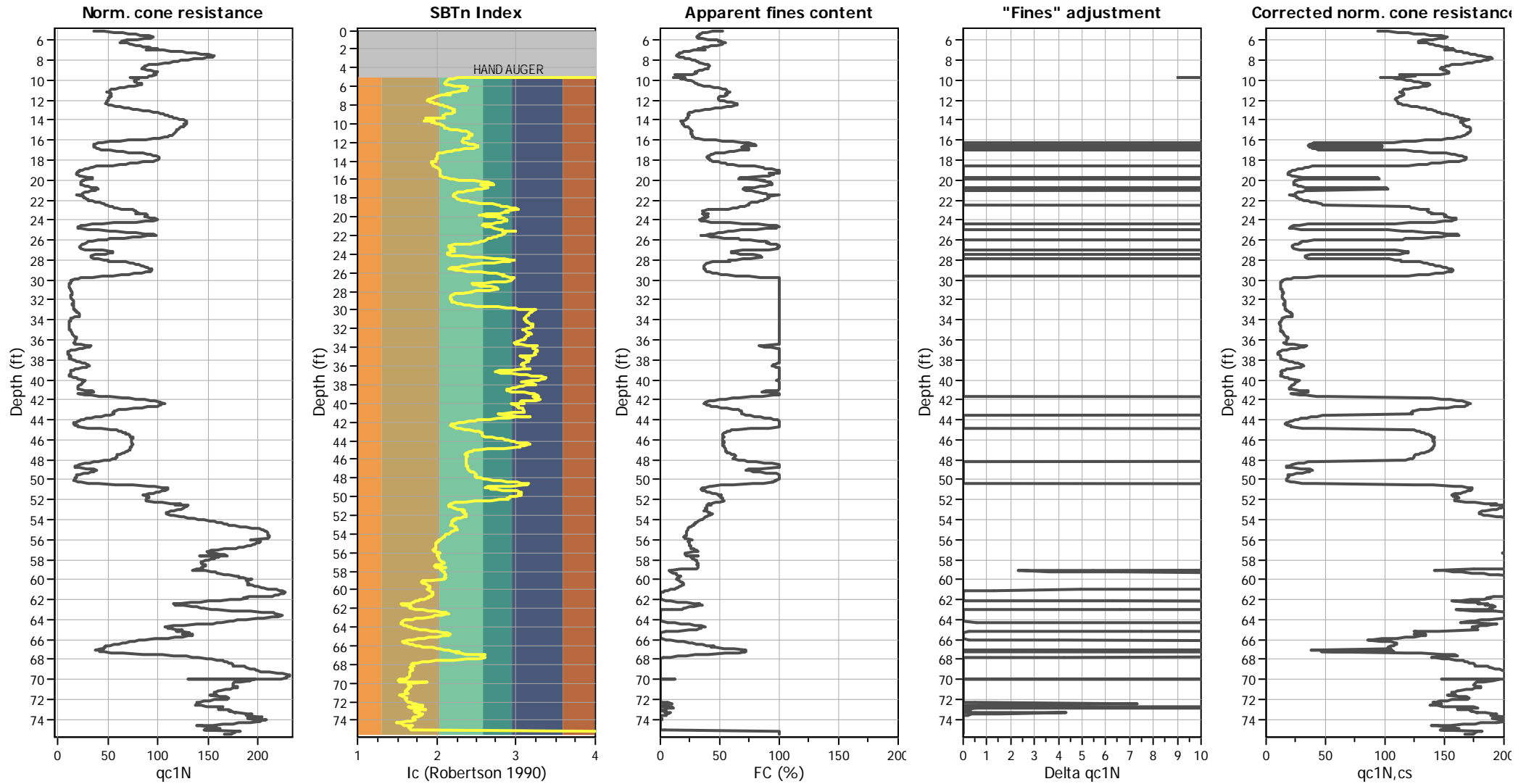
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

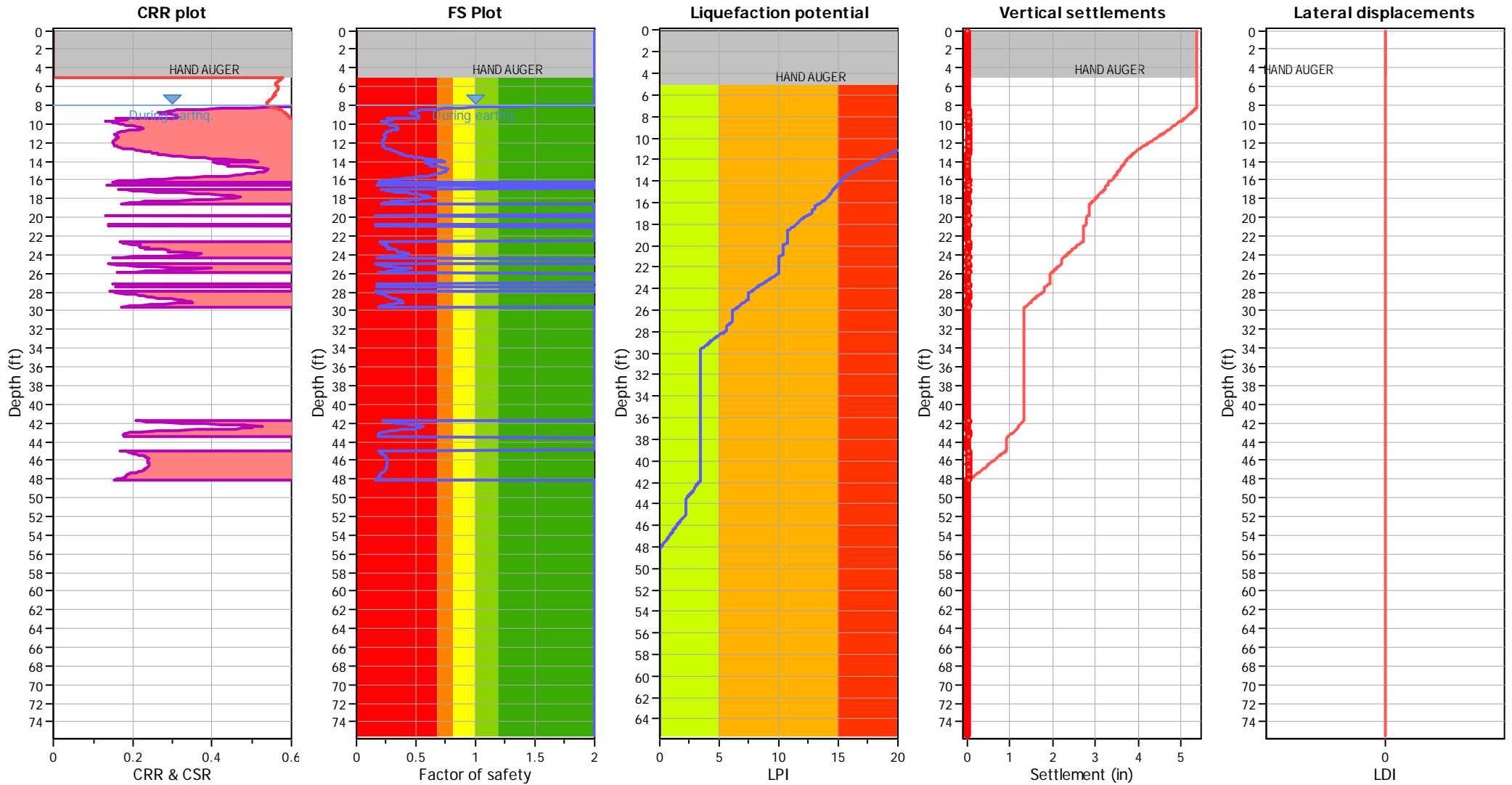
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

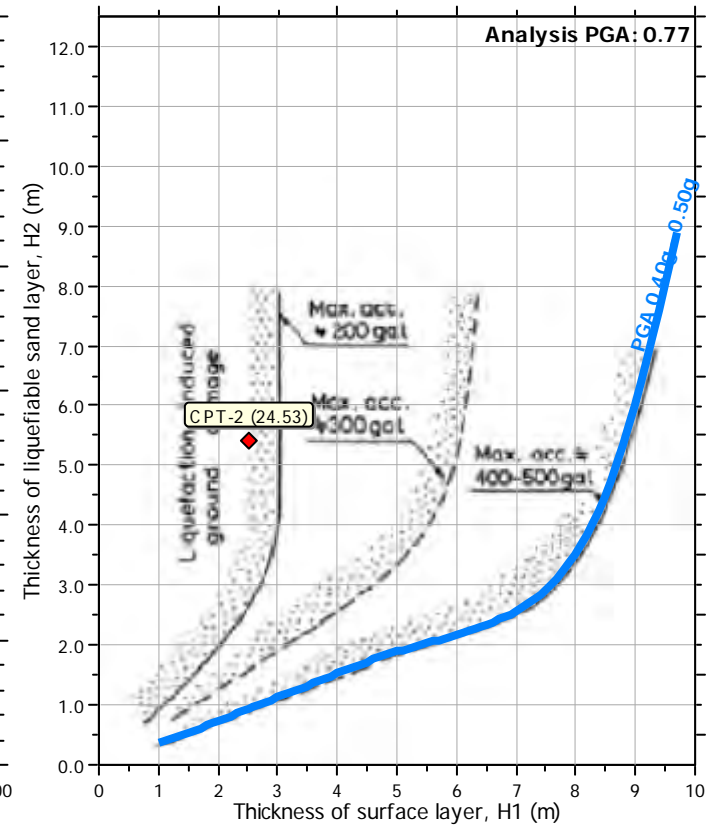
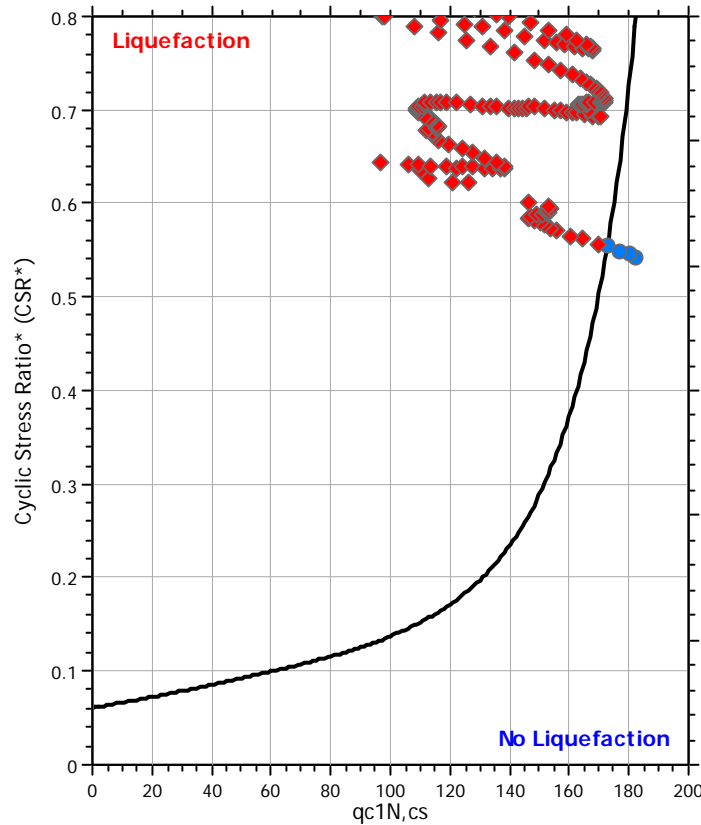
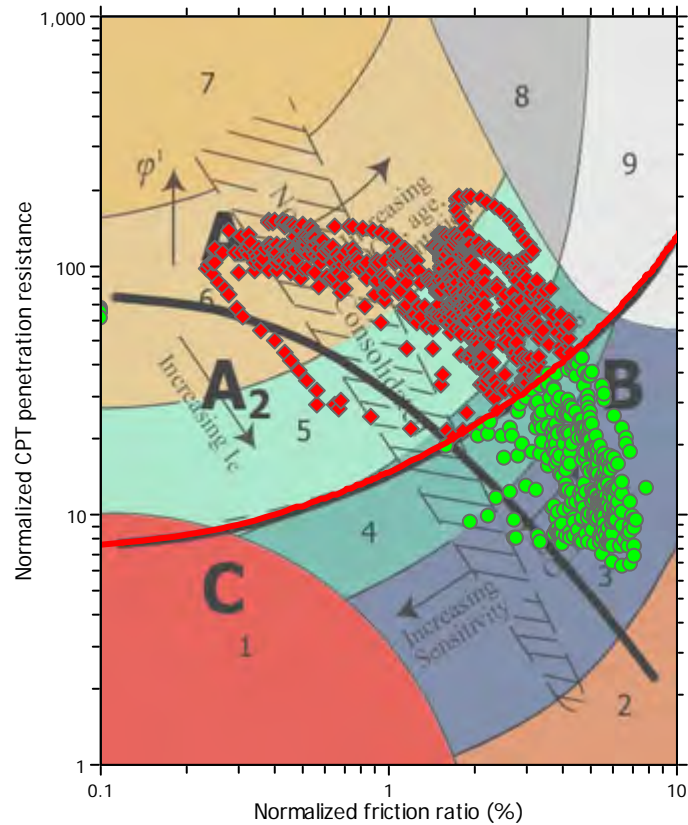
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

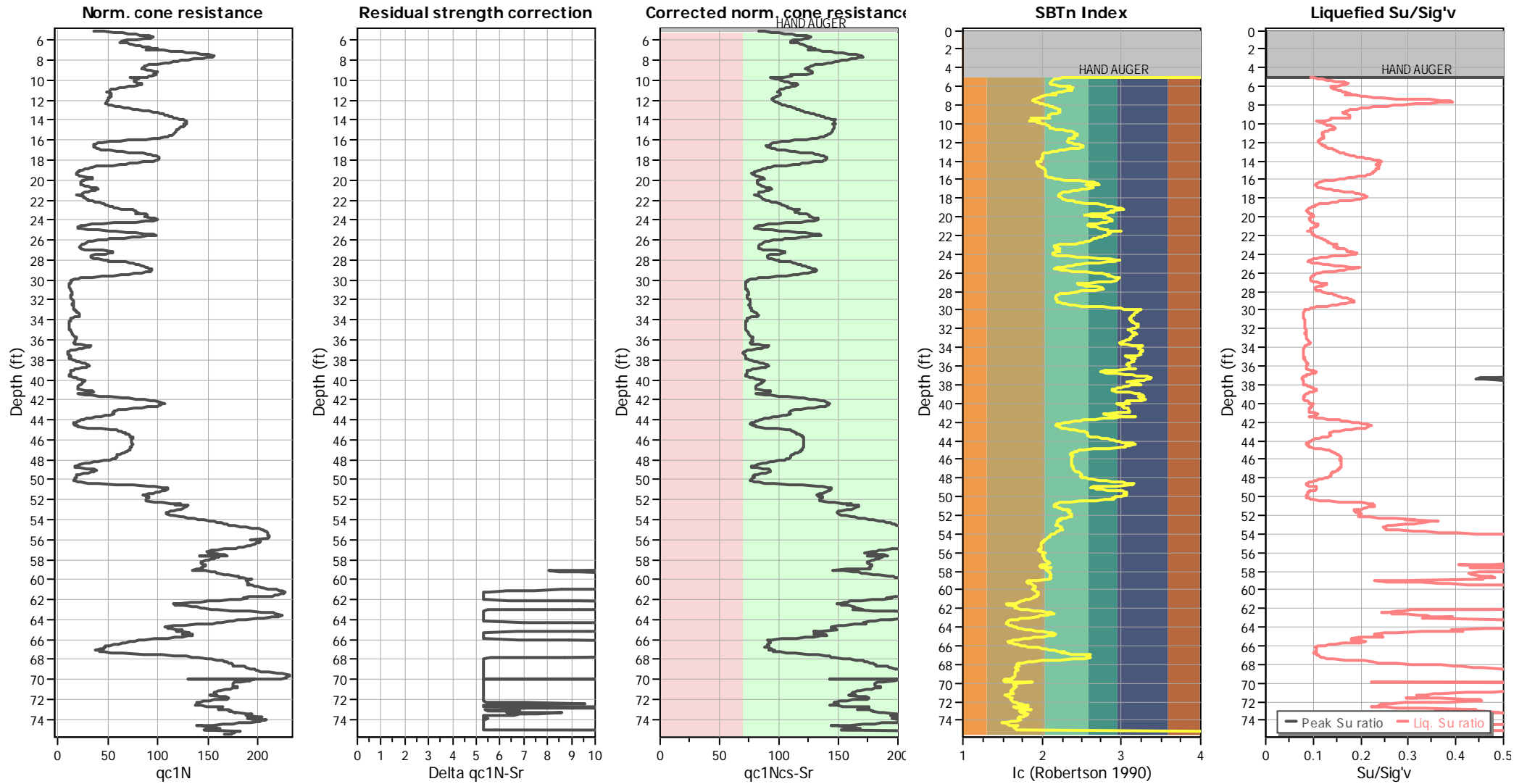
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.07	-9999.00	-9999.00	-9999.00	100.00	120.90
2	0.14	-9999.00	-9999.00	-9999.00	100.00	120.90
3	0.20	-9999.00	-9999.00	-9999.00	100.00	120.90
4	0.27	-9999.00	-9999.00	-9999.00	100.00	120.90
5	0.35	-9999.00	-9999.00	-9999.00	100.00	120.90
6	0.41	-9999.00	-9999.00	-9999.00	100.00	120.90
7	0.47	-9999.00	-9999.00	-9999.00	100.00	120.90
8	0.54	-9999.00	-9999.00	-9999.00	100.00	120.90
9	0.60	-9999.00	-9999.00	-9999.00	100.00	120.90
10	0.66	-9999.00	-9999.00	-9999.00	100.00	120.90
11	0.74	-9999.00	-9999.00	-9999.00	100.00	120.90
12	0.80	-9999.00	-9999.00	-9999.00	100.00	120.90
13	0.87	-9999.00	-9999.00	-9999.00	100.00	120.90
14	0.93	-9999.00	-9999.00	-9999.00	100.00	120.90
15	0.99	-9999.00	-9999.00	-9999.00	100.00	120.90
16	1.05	-9999.00	-9999.00	-9999.00	100.00	120.90
17	1.12	-9999.00	-9999.00	-9999.00	100.00	120.90
18	1.19	-9999.00	-9999.00	-9999.00	100.00	120.90
19	1.27	-9999.00	-9999.00	-9999.00	100.00	120.90
20	1.32	-9999.00	-9999.00	-9999.00	100.00	120.90
21	1.38	-9999.00	-9999.00	-9999.00	100.00	120.90
22	1.45	-9999.00	-9999.00	-9999.00	100.00	120.90
23	1.51	-9999.00	-9999.00	-9999.00	100.00	120.90
24	1.59	-9999.00	-9999.00	-9999.00	100.00	120.90
25	1.65	-9999.00	-9999.00	-9999.00	100.00	120.90
26	1.71	-9999.00	-9999.00	-9999.00	100.00	120.90
27	1.77	-9999.00	-9999.00	-9999.00	100.00	120.90
28	1.84	-9999.00	-9999.00	-9999.00	100.00	120.90
29	1.92	-9999.00	-9999.00	-9999.00	100.00	120.90
30	1.98	-9999.00	-9999.00	-9999.00	100.00	120.90
31	2.04	-9999.00	-9999.00	-9999.00	100.00	120.90
32	2.11	-9999.00	-9999.00	-9999.00	100.00	120.90
33	2.17	-9999.00	-9999.00	-9999.00	100.00	120.90
34	2.23	-9999.00	-9999.00	-9999.00	100.00	120.90
35	2.30	-9999.00	-9999.00	-9999.00	100.00	120.90
36	2.37	-9999.00	-9999.00	-9999.00	100.00	120.90
37	2.43	-9999.00	-9999.00	-9999.00	100.00	120.90
38	2.49	-9999.00	-9999.00	-9999.00	100.00	120.90
39	2.56	-9999.00	-9999.00	-9999.00	100.00	120.90
40	2.65	-9999.00	-9999.00	-9999.00	100.00	120.90
41	2.71	-9999.00	-9999.00	-9999.00	100.00	120.90
42	2.78	-9999.00	-9999.00	-9999.00	100.00	120.90
43	2.83	-9999.00	-9999.00	-9999.00	100.00	120.90
44	2.90	-9999.00	-9999.00	-9999.00	100.00	120.90
45	2.96	-9999.00	-9999.00	-9999.00	100.00	120.90
46	3.03	-9999.00	-9999.00	-9999.00	100.00	120.90
47	3.11	-9999.00	-9999.00	-9999.00	100.00	120.90
48	3.16	-9999.00	-9999.00	-9999.00	100.00	120.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.22	-9999.00	-9999.00	-9999.00	100.00	120.90
50	3.28	-9999.00	-9999.00	-9999.00	100.00	120.90
51	3.36	-9999.00	-9999.00	-9999.00	100.00	120.90
52	3.44	-9999.00	-9999.00	-9999.00	100.00	120.90
53	3.49	-9999.00	-9999.00	-9999.00	100.00	120.90
54	3.56	-9999.00	-9999.00	-9999.00	100.00	120.90
55	3.61	-9999.00	-9999.00	-9999.00	100.00	120.90
56	3.69	-9999.00	-9999.00	-9999.00	100.00	120.90
57	3.74	-9999.00	-9999.00	-9999.00	100.00	120.90
58	3.83	-9999.00	-9999.00	-9999.00	100.00	120.90
59	3.88	-9999.00	-9999.00	-9999.00	100.00	120.90
60	3.96	-9999.00	-9999.00	-9999.00	100.00	120.90
61	4.00	-9999.00	-9999.00	-9999.00	100.00	120.90
62	4.08	-9999.00	-9999.00	-9999.00	100.00	120.90
63	4.16	-9999.00	-9999.00	-9999.00	100.00	120.90
64	4.21	-9999.00	-9999.00	-9999.00	100.00	120.90
65	4.29	-9999.00	-9999.00	-9999.00	100.00	120.90
66	4.34	-9999.00	-9999.00	-9999.00	100.00	120.90
67	4.40	-9999.00	-9999.00	-9999.00	100.00	120.90
68	4.47	-9999.00	-9999.00	-9999.00	100.00	120.90
69	4.55	-9999.00	-9999.00	-9999.00	100.00	120.90
70	4.60	-9999.00	-9999.00	-9999.00	100.00	120.90
71	4.68	-9999.00	-9999.00	-9999.00	100.00	120.90
72	4.73	-9999.00	-9999.00	-9999.00	100.00	120.90
73	4.81	-9999.00	-9999.00	-9999.00	100.00	120.90
74	4.87	-9999.00	-9999.00	-9999.00	100.00	120.90
75	4.92	-9999.00	-9999.00	-9999.00	100.00	120.90
76	5.00	-9999.00	-9999.00	-9999.00	100.00	120.90
77	5.08	22.96	0.35	0.68	25.23	110.18
78	5.13	29.08	0.41	1.02	21.29	111.91
79	5.19	34.91	0.49	1.02	19.10	113.71
80	5.27	40.37	0.58	1.14	17.65	115.28
81	5.32	43.94	0.65	1.14	17.07	116.37
82	5.39	49.50	0.81	1.25	16.72	118.24
83	5.45	53.26	0.91	1.25	16.43	119.31
84	5.53	57.68	1.07	1.25	16.41	120.68
85	5.58	60.41	1.16	1.25	16.24	121.34
86	5.66	64.65	1.24	1.25	15.66	122.04
87	5.72	65.12	1.26	1.25	15.62	122.13
88	5.80	63.05	1.25	1.37	16.20	122.03
89	5.85	58.34	1.25	1.48	17.65	121.81
90	5.91	53.07	1.25	1.48	19.59	121.57
91	5.99	45.73	1.25	1.48	22.88	121.21
92	6.04	42.25	1.25	1.48	24.75	121.01
93	6.12	45.45	1.30	1.37	23.49	121.48
94	6.18	41.97	1.37	1.48	26.13	121.71
95	6.26	45.17	1.52	1.37	25.61	122.63
96	6.31	47.33	1.61	1.48	25.17	123.15

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.39	49.97	1.74	1.59	24.84	123.85
98	6.44	50.91	1.83	1.71	25.07	124.29
99	6.52	54.48	1.76	1.94	22.98	124.17
100	6.58	58.15	1.61	1.94	20.46	123.67
101	6.63	61.45	1.62	1.94	19.37	123.86
102	6.71	65.77	1.60	1.94	17.83	123.92
103	6.77	68.88	1.61	1.94	16.98	124.08
104	6.85	73.02	1.62	1.94	15.92	124.25
105	6.91	64.46	1.60	2.73	18.27	123.89
106	6.96	77.82	1.59	2.96	14.58	124.27
107	7.04	83.75	1.58	2.96	13.29	124.44
108	7.09	87.79	1.60	2.96	12.61	124.64
109	7.17	94.19	1.69	2.96	11.92	125.19
110	7.22	98.33	1.73	2.96	11.47	125.49
111	7.31	105.48	1.82	2.96	10.83	126.02
112	7.36	110.28	1.90	3.07	10.57	126.45
113	7.44	117.43	2.01	3.07	10.17	127.01
114	7.49	120.63	2.07	3.07	10.05	127.29
115	7.55	122.80	2.15	3.07	10.09	127.59
116	7.63	123.27	2.28	3.07	10.54	128.04
117	7.68	122.61	2.36	3.07	10.91	128.29
118	7.76	119.22	2.46	3.07	11.68	128.53
119	7.81	116.12	2.52	3.07	12.28	128.63
120	7.89	110.19	2.57	3.07	13.30	128.65
121	7.95	105.48	2.59	3.07	14.09	128.60
122	8.03	99.74	2.60	3.07	15.08	128.49
123	8.09	96.83	2.58	3.07	15.53	128.35
124	8.14	93.35	2.54	3.07	16.08	128.17
125	8.22	89.20	2.49	3.07	16.70	127.89
126	8.27	85.82	2.44	3.07	17.26	127.67
127	8.35	80.45	2.38	3.07	18.26	127.33
128	8.40	77.07	2.35	3.07	18.97	127.13
129	8.48	73.02	2.28	3.07	19.73	126.76
130	8.54	71.04	2.21	3.07	19.99	126.47
131	8.62	70.10	2.10	3.07	19.79	126.08
132	8.67	69.82	2.03	3.07	19.53	125.80
133	8.73	68.22	1.95	3.07	19.62	125.47
134	8.81	67.28	1.86	3.07	19.47	125.09
135	8.86	69.26	1.81	2.96	18.63	124.94
136	8.94	72.93	1.73	2.96	17.32	124.76
137	9.00	75.94	1.70	2.96	16.45	124.72
138	9.08	79.70	1.67	2.96	15.48	124.69
139	9.13	81.21	1.65	3.07	15.11	124.67
140	9.20	81.77	1.65	3.07	15.04	124.70
141	9.26	81.49	1.68	3.07	15.27	124.80
142	9.33	80.83	1.70	3.07	15.57	124.88
143	9.39	79.42	1.40	3.07	14.24	123.43
144	9.46	78.01	0.70	3.07	9.62	118.27

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.53	76.22	0.80	3.07	10.77	119.17
146	9.60	73.87	0.88	3.07	11.90	119.80
147	9.67	71.42	0.63	3.07	10.27	117.28
148	9.73	69.44	0.48	3.07	9.12	115.18
149	9.79	57.78	0.51	3.07	12.12	115.29
150	9.86	65.30	0.58	3.07	11.18	116.54
151	9.91	65.30	0.64	3.07	11.79	117.22
152	9.98	64.17	0.73	2.96	12.97	118.13
153	10.04	63.85	0.82	1.94	13.88	118.92
154	10.11	63.52	0.89	2.05	14.64	119.52
155	10.18	65.40	0.97	2.05	14.90	120.24
156	10.25	67.47	1.08	2.05	15.31	121.13
157	10.31	69.63	1.17	2.05	15.48	121.80
158	10.37	71.23	1.24	2.05	15.60	122.27
159	10.44	72.17	1.31	2.16	15.86	122.68
160	10.51	70.39	1.36	2.16	16.71	122.92
161	10.57	66.15	1.40	2.16	18.16	122.96
162	10.64	61.35	1.42	2.16	19.80	122.86
163	10.71	57.02	1.43	2.16	21.47	122.77
164	10.77	53.26	1.45	2.16	23.10	122.67
165	10.84	48.93	1.44	2.16	25.02	122.42
166	10.91	45.73	1.42	2.16	26.52	122.15
167	10.98	45.07	1.39	2.16	26.68	121.96
168	11.05	44.70	1.38	2.16	26.83	121.88
169	11.11	44.79	1.39	2.16	26.95	121.95
170	11.18	42.72	1.37	2.16	28.05	121.76
171	11.25	43.57	1.42	2.16	27.99	122.02
172	11.31	45.83	1.45	2.16	27.06	122.30
173	11.38	46.48	1.42	2.05	26.56	122.21
174	11.45	47.14	1.42	2.16	26.27	122.24
175	11.51	46.48	1.43	2.05	26.74	122.25
176	11.58	45.73	1.28	2.16	25.84	121.38
177	11.65	46.48	1.13	2.16	24.14	120.54
178	11.68	46.11	1.10	2.16	24.03	120.31
179	11.75	45.54	1.02	2.16	23.53	119.71
180	11.82	44.32	0.94	2.16	23.40	119.09
181	11.88	44.37	0.91	2.16	23.08	118.85
182	11.97	44.37	0.95	8.88	23.48	119.12
183	12.03	44.41	0.99	5.46	24.03	119.47
184	12.10	43.57	1.08	4.33	25.51	120.06
185	12.16	44.13	1.27	3.53	27.07	121.23
186	12.23	43.94	1.48	3.53	29.16	122.35
187	12.30	43.38	1.65	3.53	31.00	123.12
188	12.36	44.88	1.81	3.53	31.41	123.88
189	12.43	46.20	1.92	3.76	31.51	124.39
190	12.50	47.71	2.00	3.87	31.26	124.76
191	12.53	49.03	2.03	3.87	30.77	124.94
192	12.60	52.41	2.05	3.76	29.22	125.19

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.67	57.02	1.99	3.76	26.74	125.17
194	12.74	61.73	1.89	3.76	24.25	124.98
195	12.80	65.87	1.75	3.76	21.95	124.58
196	12.87	69.63	1.64	3.87	20.11	124.24
197	12.94	74.81	1.60	3.76	18.43	124.22
198	13.00	80.36	1.52	3.76	16.60	124.02
199	13.07	85.44	1.43	3.76	15.03	123.76
200	13.13	89.86	1.42	3.76	14.07	123.79
201	13.20	92.69	1.44	3.76	13.73	124.00
202	13.27	94.95	1.43	3.76	13.31	124.01
203	13.34	98.24	1.48	3.76	13.03	124.32
204	13.40	100.97	1.59	3.87	13.17	124.90
205	13.47	103.32	1.67	3.87	13.26	125.35
206	13.54	105.67	1.73	3.76	13.20	125.66
207	13.60	107.84	1.78	3.76	13.14	125.93
208	13.67	110.28	1.84	3.76	13.05	126.20
209	13.74	112.73	1.88	3.76	12.89	126.41
210	13.80	115.84	1.95	3.87	12.78	126.74
211	13.87	118.94	2.03	3.98	12.72	127.10
212	13.94	121.57	2.08	3.98	12.58	127.33
213	14.00	123.74	2.10	3.98	12.40	127.44
214	14.07	125.24	1.95	3.98	11.65	126.94
215	14.14	126.09	1.86	3.98	11.21	126.61
216	14.21	126.75	1.89	3.98	11.26	126.72
217	14.24	126.75	1.90	3.98	11.34	126.79
218	14.31	127.03	1.95	3.98	11.52	126.98
219	14.37	124.30	1.95	3.98	11.87	126.91
220	14.46	125.72	1.95	4.10	11.72	126.94
221	14.52	125.53	1.98	4.10	11.89	127.05
222	14.59	124.87	2.05	4.10	12.27	127.28
223	14.65	123.83	2.12	4.10	12.71	127.52
224	14.72	122.80	2.16	4.10	13.05	127.65
225	14.79	121.95	2.21	4.10	13.38	127.79
226	14.85	121.20	2.22	4.10	13.53	127.80
227	14.92	120.35	2.22	4.10	13.70	127.81
228	14.99	119.98	2.25	4.10	13.89	127.89
229	15.05	119.41	2.27	4.21	14.08	127.94
230	15.12	119.32	2.25	4.21	14.05	127.88
231	15.19	119.03	2.23	4.21	14.03	127.81
232	15.22	119.13	2.23	4.21	14.00	127.78
233	15.29	118.85	2.21	4.21	14.00	127.72
234	15.36	118.00	2.18	4.21	14.03	127.61
235	15.43	117.06	2.16	4.21	14.10	127.51
236	15.49	115.93	2.14	4.21	14.21	127.42
237	15.56	114.14	2.10	4.21	14.36	127.26
238	15.63	112.26	2.05	4.21	14.44	127.03
239	15.69	109.25	1.98	4.21	14.65	126.72
240	15.76	103.98	1.91	4.21	15.24	126.34

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.82	97.58	1.88	4.21	16.31	126.07
242	15.89	90.33	1.87	3.98	17.77	125.83
243	15.96	82.24	1.83	3.98	19.50	125.45
244	16.03	72.83	1.81	3.98	22.08	125.09
245	16.10	63.70	1.79	3.98	25.13	124.67
246	16.16	54.11	1.78	3.98	29.32	124.25
247	16.23	45.73	1.78	3.98	34.09	123.81
248	16.30	41.21	1.79	3.98	37.46	123.61
249	16.36	38.58	1.80	4.10	39.71	123.48
250	16.43	37.26	1.79	4.21	40.87	123.37
251	16.50	37.26	1.82	4.21	41.14	123.46
252	16.56	37.26	1.22	4.33	35.13	120.55
253	16.63	38.30	1.15	4.33	33.48	120.16
254	16.70	38.39	1.35	4.33	35.78	121.36
255	16.73	38.86	1.45	4.44	36.52	121.94
256	16.80	40.56	1.68	4.44	37.42	123.10
257	16.87	43.10	1.92	4.44	37.57	124.21
258	16.94	45.64	2.11	4.44	37.35	125.06
259	17.00	54.58	2.25	4.55	32.94	125.97
260	17.08	62.20	2.42	4.67	30.31	126.81
261	17.14	68.13	2.51	4.67	28.39	127.30
262	17.20	75.47	2.55	4.67	25.98	127.66
263	17.27	83.28	2.58	4.55	23.78	128.00
264	17.34	90.33	2.61	4.55	22.06	128.28
265	17.40	95.04	2.63	4.55	21.06	128.47
266	17.47	98.61	2.67	4.55	20.43	128.65
267	17.53	102.47	2.71	4.55	19.80	128.86
268	17.60	105.67	2.75	4.55	19.34	129.03
269	17.67	107.84	2.79	4.55	19.10	129.19
270	17.73	109.06	2.84	4.55	19.09	129.35
271	17.80	108.97	2.91	4.55	19.42	129.54
272	17.87	108.50	2.98	4.55	19.79	129.69
273	17.93	107.18	3.02	4.55	20.24	129.76
274	18.00	105.39	3.02	4.55	20.65	129.73
275	18.07	102.66	2.97	4.55	21.06	129.53
276	18.14	98.43	2.93	4.55	21.89	129.34
277	18.20	92.69	2.88	4.44	23.07	129.05
278	18.27	85.91	2.79	4.44	24.54	128.63
279	18.34	78.67	2.68	4.44	26.26	128.13
280	18.37	74.90	2.62	4.44	27.24	127.84
281	18.44	67.75	2.49	4.44	29.26	127.22
282	18.51	59.66	2.35	4.33	32.11	126.50
283	18.57	50.53	2.29	4.33	36.77	125.89
284	18.64	43.66	2.19	4.33	40.92	125.21
285	18.71	38.77	2.10	4.21	44.42	124.61
286	18.78	36.51	1.98	4.21	45.67	124.06
287	18.84	34.35	1.86	4.21	46.83	123.43
288	18.91	30.02	1.76	4.21	51.13	122.71

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.98	27.10	1.68	4.21	54.42	122.12
290	19.04	25.12	1.60	4.33	56.68	121.56
291	19.11	23.62	1.51	4.33	58.27	120.99
292	19.18	22.21	1.45	4.44	60.30	120.57
293	19.24	21.08	1.21	4.33	59.08	119.12
294	19.31	21.08	0.72	4.21	49.74	115.28
295	19.38	21.08	0.78	4.21	51.16	115.87
296	19.44	21.08	0.84	4.21	52.57	116.44
297	19.51	22.49	0.92	4.21	51.50	117.22
298	19.58	24.47	0.95	4.33	48.87	117.70
299	19.63	26.91	0.95	4.33	45.37	117.96
300	19.69	34.35	0.95	4.44	36.95	118.56
301	19.76	38.77	0.95	4.33	33.23	118.85
302	19.82	40.09	0.97	4.33	32.49	119.06
303	19.89	38.96	1.03	4.10	34.14	119.39
304	19.95	36.70	1.06	3.87	36.58	119.51
305	20.02	27.57	1.08	3.87	46.95	118.95
306	20.09	29.83	1.09	2.73	44.27	119.22
307	20.16	27.10	1.12	2.85	48.28	119.12
308	20.23	26.54	1.15	2.96	49.76	119.32
309	20.29	26.72	1.20	2.85	50.26	119.62
310	20.36	26.63	1.25	3.07	51.12	119.89
311	20.42	27.48	1.30	3.19	50.71	120.29
312	20.49	29.26	1.36	3.19	49.12	120.77
313	20.56	31.52	1.42	3.19	46.99	121.23
314	20.63	34.72	1.46	3.19	43.94	121.68
315	20.69	38.39	1.48	3.42	40.65	122.02
316	20.76	42.25	1.47	3.30	37.46	122.25
317	20.83	45.54	1.47	3.30	35.06	122.40
318	20.89	46.58	1.47	3.30	34.39	122.45
319	20.96	46.01	1.46	3.19	34.74	122.38
320	21.03	43.29	1.42	3.19	36.27	122.01
321	21.09	38.96	1.37	3.19	39.27	121.49
322	21.16	35.38	1.27	3.19	41.51	120.72
323	21.23	33.12	1.07	3.19	41.27	119.34
324	21.26	31.81	1.02	3.19	41.97	118.88
325	21.33	29.36	1.09	3.30	45.96	119.13
326	21.40	28.70	1.15	3.30	47.81	119.47
327	21.46	28.98	1.19	3.30	48.14	119.76
328	21.53	23.05	1.24	3.30	58.27	119.49
329	21.60	30.49	1.33	3.30	48.16	120.67
330	21.66	30.86	1.43	3.42	49.04	121.24
331	21.73	31.33	1.52	3.42	49.62	121.73
332	21.80	32.37	1.58	3.53	49.18	122.13
333	21.86	34.25	1.65	3.53	47.77	122.56
334	21.93	35.76	1.72	3.53	46.93	122.98
335	22.00	37.36	1.79	3.53	46.01	123.37
336	22.06	39.43	1.88	3.64	44.94	123.87

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.13	41.87	2.00	3.64	43.86	124.47
338	22.19	45.45	2.12	3.76	41.89	125.07
339	22.26	50.15	2.20	3.76	39.22	125.61
340	22.33	53.64	2.28	3.76	37.58	126.02
341	22.40	55.71	2.38	3.76	37.08	126.43
342	22.46	57.02	2.51	3.76	37.19	126.87
343	22.53	59.38	2.61	3.76	36.54	127.25
344	22.60	62.39	2.61	3.76	35.02	127.37
345	22.66	65.30	2.53	3.76	33.16	127.25
346	22.73	67.09	2.38	3.76	31.52	126.88
347	22.80	70.57	2.31	3.76	29.65	126.77
348	22.86	76.69	2.32	3.87	27.45	127.01
349	22.93	84.50	2.29	3.76	24.82	127.17
350	23.00	90.71	1.68	3.76	19.62	125.06
351	23.03	92.87	1.48	3.76	17.86	124.19
352	23.10	94.00	1.49	3.76	17.72	124.28
353	23.17	93.72	1.54	3.76	18.08	124.49
354	23.24	95.70	1.59	3.76	17.98	124.77
355	23.30	99.84	1.68	3.76	17.71	125.32
356	23.37	94.00	1.81	3.76	19.77	125.70
357	23.43	105.95	1.93	3.76	17.84	126.44
358	23.50	107.55	2.04	3.76	18.15	126.91
359	23.56	105.86	2.14	3.76	18.97	127.19
360	23.63	104.45	2.21	3.76	19.65	127.41
361	23.70	105.58	2.26	3.87	19.67	127.59
362	23.76	111.60	2.29	3.87	18.64	127.83
363	23.83	117.25	2.29	3.87	17.63	127.96
364	23.90	120.54	2.23	3.76	16.81	127.82
365	23.96	120.07	2.17	3.76	16.65	127.62
366	24.03	115.84	2.10	3.76	17.09	127.30
367	24.10	106.99	2.03	3.76	18.44	126.86
368	24.17	95.42	1.98	3.76	20.74	126.40
369	24.23	83.18	1.94	3.76	23.81	125.91
370	24.30	69.91	1.89	3.64	28.11	125.31
371	24.37	56.65	1.86	3.64	34.13	124.67
372	24.43	44.60	1.83	3.64	41.96	123.96
373	24.50	35.76	1.72	3.64	49.24	122.95
374	24.57	30.21	1.56	3.64	54.31	121.84
375	24.63	27.10	1.39	3.64	56.84	120.75
376	24.70	26.72	1.18	3.64	54.48	119.52
377	24.77	25.88	1.05	3.64	53.73	118.55
378	24.84	27.76	1.04	3.64	50.86	118.69
379	24.87	30.39	1.08	3.76	47.90	119.14
380	24.94	38.20	1.21	3.76	41.22	120.56
381	25.01	51.19	1.44	3.76	34.04	122.56
382	25.07	65.02	1.73	3.76	29.34	124.45
383	25.14	73.49	2.00	3.76	27.85	125.82
384	25.21	86.19	2.23	3.87	25.05	127.02

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.28	96.54	2.45	3.98	23.37	127.99
386	25.34	107.18	2.62	4.10	21.63	128.71
387	25.41	117.25	2.68	4.21	19.84	129.09
388	25.48	121.57	2.53	4.10	18.46	128.77
389	25.54	119.32	2.15	3.98	17.22	127.54
390	25.61	111.88	2.20	3.98	18.81	127.53
391	25.68	103.70	2.21	3.98	20.63	127.41
392	25.75	94.29	2.24	3.98	23.05	127.26
393	25.81	84.22	2.24	3.98	26.00	127.00
394	25.87	67.37	2.19	4.10	32.06	126.29
395	25.93	63.99	2.07	4.21	32.84	125.74
396	26.00	52.32	1.92	4.21	38.31	124.71
397	26.06	44.70	1.86	4.10	43.41	124.08
398	26.13	40.27	1.82	3.98	47.10	123.67
399	26.20	37.73	1.75	3.98	48.96	123.23
400	26.27	37.36	1.70	3.87	48.85	122.98
401	26.33	37.92	1.65	3.87	47.84	122.80
402	26.40	35.38	1.64	3.87	50.43	122.57
403	26.47	32.37	1.62	3.87	53.87	122.28
404	26.53	30.11	1.59	3.87	56.68	122.00
405	26.60	30.11	1.52	3.87	55.80	121.63
406	26.66	30.11	1.48	3.87	55.36	121.43
407	26.73	30.11	1.52	3.87	56.00	121.66
408	26.80	31.15	1.51	3.87	54.46	121.68
409	26.86	31.90	1.63	3.98	54.90	122.28
410	26.93	37.36	1.73	4.10	49.65	123.09
411	27.00	47.80	1.81	4.21	41.18	124.04
412	27.06	58.62	1.86	4.33	34.67	124.73
413	27.13	69.35	1.88	4.33	29.74	125.23
414	27.17	72.36	1.90	4.33	28.65	125.40
415	27.23	72.74	1.94	4.21	28.82	125.57
416	27.30	68.88	1.96	4.10	30.58	125.51
417	27.37	63.33	1.94	3.98	33.09	125.25
418	27.43	57.12	1.87	3.98	35.85	124.71
419	27.50	50.06	1.76	3.98	39.51	123.97
420	27.57	44.32	1.72	3.98	43.59	123.50
421	27.64	44.27	1.75	3.98	44.01	123.63
422	27.70	44.27	1.82	3.98	44.70	123.90
423	27.77	44.23	1.70	3.98	43.61	123.40
424	27.84	48.46	1.52	3.98	38.54	122.81
425	27.91	54.95	1.50	4.10	34.17	123.01
426	27.98	61.26	1.50	4.10	30.82	123.27
427	28.04	68.41	1.50	4.21	27.64	123.54
428	28.09	67.84	1.52	4.21	28.09	123.62
429	28.16	83.65	1.56	3.98	22.87	124.34
430	28.22	90.33	1.57	3.98	21.08	124.56
431	28.28	95.89	1.57	3.98	19.73	124.72
432	28.35	99.74	1.59	3.98	19.00	124.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.42	103.32	1.65	3.98	18.59	125.24
434	28.49	106.43	1.71	3.98	18.32	125.57
435	28.55	109.25	1.76	3.98	18.08	125.86
436	28.62	112.35	1.84	3.98	17.95	126.26
437	28.69	115.27	1.94	3.98	17.95	126.71
438	28.75	117.53	2.04	4.10	18.06	127.13
439	28.82	119.32	2.14	4.10	18.24	127.51
440	28.89	120.82	2.22	4.10	18.36	127.80
441	28.95	121.95	2.28	4.10	18.48	128.03
442	29.02	122.99	2.33	4.10	18.50	128.18
443	29.09	123.08	2.35	4.10	18.62	128.26
444	29.16	121.10	2.38	4.10	19.15	128.33
445	29.22	116.02	2.36	4.10	20.04	128.15
446	29.29	109.81	2.32	4.10	21.15	127.88
447	29.35	102.47	2.26	3.98	22.55	127.52
448	29.42	94.76	2.20	3.98	24.25	127.14
449	29.49	85.16	2.19	3.98	27.10	126.85
450	29.55	74.34	2.18	3.98	31.04	126.50
451	29.62	61.07	2.15	3.98	37.13	125.89
452	29.69	48.46	1.98	3.98	44.19	124.72
453	29.76	39.33	1.85	3.76	51.12	123.75
454	29.82	32.56	1.72	3.87	57.64	122.75
455	29.86	29.45	1.64	3.87	61.17	122.15
456	29.92	24.37	1.46	3.76	67.71	120.81
457	30.00	19.48	1.27	3.53	76.44	119.29
458	30.06	20.23	1.14	3.64	72.05	118.56
459	30.13	18.82	1.02	3.53	73.56	117.57
460	30.20	18.26	0.91	3.53	72.88	116.68
461	30.27	18.07	0.82	3.53	71.46	115.93
462	30.34	17.97	0.74	3.53	69.68	115.13
463	30.40	17.31	0.69	3.53	70.25	114.51
464	30.47	17.13	0.66	3.53	70.00	114.16
465	30.54	17.22	0.64	3.53	69.32	113.99
466	30.61	17.50	0.63	3.53	68.07	113.84
467	30.67	17.60	0.62	3.76	67.62	113.77
468	30.74	17.60	0.62	3.87	67.66	113.76
469	30.81	17.78	0.62	3.98	67.21	113.78
470	30.87	18.44	0.64	3.87	66.01	114.09
471	30.91	18.73	0.65	3.87	65.76	114.32
472	30.97	19.38	0.71	3.87	65.57	114.96
473	31.04	19.67	0.78	3.87	66.82	115.74
474	31.11	20.14	0.86	3.87	67.45	116.46
475	31.17	20.51	0.92	3.87	68.07	117.05
476	31.24	21.36	0.97	3.87	67.17	117.54
477	31.31	21.27	1.02	3.87	68.40	117.88
478	31.38	20.98	1.07	3.87	70.03	118.17
479	31.44	20.70	1.12	3.87	71.82	118.50
480	31.51	20.23	1.14	3.87	73.48	118.58

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.57	19.95	1.11	3.87	73.74	118.36
482	31.64	20.14	1.10	3.87	73.03	118.29
483	31.71	20.14	1.10	3.98	73.09	118.29
484	31.77	19.85	1.07	4.10	73.33	118.05
485	31.84	20.51	1.13	4.10	72.90	118.56
486	31.91	21.74	1.17	4.10	70.62	118.93
487	31.97	22.49	1.14	4.21	68.44	118.83
488	32.04	24.09	1.14	4.21	65.15	119.00
489	32.11	24.18	1.14	4.21	65.04	119.01
490	32.18	23.43	1.16	4.21	66.91	119.04
491	32.24	23.90	1.21	4.33	66.87	119.41
492	32.31	23.90	1.26	4.33	67.75	119.71
493	32.36	23.90	1.28	4.33	68.21	119.85
494	32.43	22.96	1.30	4.33	70.54	119.85
495	32.49	22.58	1.33	4.33	71.98	119.99
496	32.56	23.15	1.33	4.33	70.68	120.02
497	32.62	23.15	1.29	4.44	70.13	119.81
498	32.70	23.43	1.28	4.44	69.36	119.76
499	32.75	24.18	1.28	4.44	67.94	119.87
500	32.83	24.94	1.29	4.44	66.62	119.99
501	32.88	24.84	1.30	4.55	66.98	120.03
502	32.96	25.50	1.34	4.55	66.39	120.32
503	33.01	25.97	1.37	4.55	66.01	120.53
504	33.08	26.25	1.44	4.55	66.50	120.90
505	33.16	27.76	1.53	4.55	65.18	121.50
506	33.22	29.17	1.58	4.55	63.51	121.85
507	33.29	31.52	1.59	4.67	60.11	122.07
508	33.34	32.09	1.59	4.67	59.33	122.11
509	33.40	32.37	1.60	4.78	59.17	122.20
510	33.47	33.31	1.62	4.78	58.15	122.34
511	33.56	33.97	1.58	4.78	56.94	122.23
512	33.62	32.75	1.55	4.67	58.19	121.98
513	33.68	29.45	1.52	4.78	62.65	121.59
514	33.73	26.16	1.48	4.67	67.77	121.09
515	33.82	21.64	1.40	4.78	76.57	120.26
516	33.89	20.42	1.32	4.67	78.47	119.68
517	33.95	20.70	1.21	4.78	75.84	119.07
518	34.02	20.61	1.08	4.78	73.74	118.25
519	34.09	19.85	1.01	4.78	74.27	117.62
520	34.15	19.20	0.99	4.78	75.66	117.38
521	34.22	18.63	0.98	4.78	77.18	117.24
522	34.25	18.35	0.97	4.78	77.95	117.17
523	34.32	17.97	0.96	4.67	78.94	117.03
524	34.39	18.07	0.94	4.67	78.29	116.91
525	34.45	18.16	0.91	4.67	77.42	116.70
526	34.52	18.54	0.90	4.67	75.94	116.61
527	34.59	18.54	0.90	4.67	75.99	116.60
528	34.65	18.54	0.90	4.67	76.04	116.60

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.72	18.54	0.90	4.78	76.16	116.62
530	34.79	18.54	0.90	4.78	76.29	116.64
531	34.85	18.82	0.79	4.78	72.71	115.67
532	34.92	19.38	0.48	4.78	62.16	112.07
533	34.99	19.76	0.58	4.89	64.77	113.61
534	35.05	20.23	0.69	4.89	66.58	114.85
535	35.13	20.51	0.79	4.89	68.58	115.91
536	35.19	20.23	0.89	5.01	71.59	116.72
537	35.27	23.24	1.00	5.24	67.10	117.98
538	35.34	23.24	1.10	5.35	68.95	118.65
539	35.37	23.24	1.14	5.35	69.68	118.90
540	35.44	23.62	1.20	5.35	69.98	119.32
541	35.51	24.28	1.23	5.35	69.12	119.56
542	35.57	25.12	1.26	5.46	68.02	119.84
543	35.64	26.63	1.32	5.46	66.17	120.33
544	35.70	28.42	1.38	5.46	63.90	120.78
545	35.77	29.17	1.42	5.35	63.26	121.04
546	35.84	29.26	1.42	5.58	63.16	121.05
547	35.90	28.79	1.39	5.58	63.57	120.86
548	35.97	27.67	1.38	5.58	65.47	120.75
549	36.03	27.19	1.38	5.58	66.35	120.71
550	36.10	27.85	1.38	5.58	65.14	120.72
551	36.17	26.91	1.35	5.69	66.40	120.48
552	36.24	27.76	1.32	5.58	64.52	120.39
553	36.30	24.47	1.35	5.69	71.39	120.29
554	36.37	27.67	1.33	5.58	64.96	120.45
555	36.44	35.76	1.40	5.69	54.57	121.49
556	36.51	45.83	1.50	5.69	45.96	122.58
557	36.57	51.66	1.60	5.81	42.71	123.36
558	36.64	52.60	1.73	5.81	43.22	123.94
559	36.71	49.78	1.85	5.69	46.33	124.30
560	36.77	45.54	1.88	5.81	50.05	124.21
561	36.84	39.99	1.83	5.69	54.91	123.71
562	36.91	33.69	1.73	5.81	61.35	122.86
563	36.98	27.76	1.60	5.81	69.08	121.84
564	37.01	25.50	1.52	5.81	72.37	121.26
565	37.08	21.74	1.36	5.81	78.46	120.03
566	37.15	19.29	1.22	5.81	82.98	118.98
567	37.21	17.78	1.12	5.81	85.80	118.13
568	37.28	16.66	1.00	5.81	87.20	117.14
569	37.34	16.37	0.91	5.81	86.30	116.45
570	37.41	17.03	0.89	5.81	83.25	116.31
571	37.48	18.26	0.88	5.81	79.23	116.47
572	37.55	19.67	0.91	5.81	75.66	116.83
573	37.61	20.51	0.84	5.81	72.01	116.40
574	37.68	20.70	0.51	5.92	62.55	112.79
575	37.75	20.14	0.61	5.92	66.81	113.94
576	37.81	19.85	0.71	5.92	70.55	115.07

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.88	20.23	0.89	6.03	74.03	116.76
578	37.95	20.98	1.10	6.15	76.56	118.41
579	38.02	25.50	1.28	6.49	69.42	119.97
580	38.08	28.14	1.45	6.72	67.13	121.13
581	38.15	31.24	1.64	6.72	64.61	122.28
582	38.21	35.00	1.83	6.83	61.60	123.38
583	38.28	39.71	2.01	6.83	57.82	124.37
584	38.35	43.10	2.14	6.83	55.47	125.01
585	38.41	46.20	2.23	6.94	53.43	125.49
586	38.48	49.31	2.36	6.94	51.84	126.06
587	38.55	50.72	2.43	6.94	51.32	126.36
588	38.58	50.62	2.43	6.94	51.41	126.35
589	38.65	49.40	2.39	7.06	52.08	126.15
590	38.72	46.30	2.33	7.06	54.30	125.81
591	38.78	40.65	2.24	7.06	59.20	125.22
592	38.85	34.44	2.09	7.06	65.39	124.29
593	38.92	29.08	1.86	7.06	71.40	123.05
594	38.98	25.78	1.66	7.06	75.18	121.91
595	39.05	24.00	1.50	7.06	76.90	121.01
596	39.12	22.30	1.36	7.06	78.80	120.10
597	39.18	21.27	1.24	7.06	79.47	119.32
598	39.25	21.64	1.14	7.17	76.64	118.71
599	39.32	22.02	1.08	7.17	74.65	118.38
600	39.38	21.74	1.07	7.17	75.31	118.32
601	39.45	21.08	1.09	7.17	77.35	118.35
602	39.52	20.33	1.15	7.29	80.65	118.66
603	39.58	20.33	1.22	7.29	81.95	119.07
604	39.65	22.49	1.21	7.29	76.27	119.29
605	39.72	26.72	1.21	7.40	67.23	119.66
606	39.78	30.77	1.34	7.40	62.51	120.75
607	39.85	33.22	1.57	7.40	62.14	122.14
608	39.92	34.35	1.81	7.40	63.38	123.25
609	39.97	33.88	1.97	7.51	65.72	123.82
610	40.04	45.73	2.12	7.97	53.89	125.11
611	40.09	45.64	2.22	7.97	54.81	125.43
612	40.17	42.81	2.32	8.08	58.42	125.59
613	40.23	41.21	2.36	8.08	60.47	125.62
614	40.31	41.21	2.29	8.20	59.91	125.40
615	40.37	40.09	2.16	8.31	60.11	124.93
616	40.44	38.67	2.04	8.42	60.64	124.42
617	40.51	36.89	1.96	8.31	61.98	123.99
618	40.57	35.10	1.91	8.31	63.90	123.71
619	40.64	34.44	1.91	8.54	64.80	123.65
620	40.71	34.44	1.91	8.65	64.82	123.64
621	40.77	34.06	1.90	8.65	65.30	123.58
622	40.84	33.78	1.90	8.65	65.73	123.56
623	40.91	33.88	1.94	8.88	66.03	123.71
624	40.97	37.26	2.02	8.54	62.43	124.24

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.04	45.92	2.25	8.99	55.39	125.55
626	41.11	56.84	2.31	9.34	47.35	126.25
627	41.17	58.44	2.10	8.88	44.81	125.61
628	41.24	54.20	2.22	9.22	48.60	125.86
629	41.30	49.21	2.43	9.22	54.07	126.29
630	41.37	42.53	2.52	9.22	61.06	126.18
631	41.41	34.63	2.52	9.45	70.87	125.68
632	41.48	46.20	2.59	9.90	58.00	126.58
633	41.54	54.77	2.76	9.45	52.13	127.46
634	41.60	68.22	2.93	9.68	44.88	128.45
635	41.67	82.90	3.05	10.47	38.63	129.22
636	41.74	100.12	3.13	10.24	32.54	129.86
637	41.80	104.07	3.15	9.11	31.42	130.00
638	41.87	108.68	3.05	9.22	29.62	129.87
639	41.94	118.75	2.95	9.11	26.55	129.85
640	42.00	129.95	2.86	8.88	23.65	129.83
641	42.07	138.79	2.80	8.77	21.71	129.84
642	42.14	145.19	2.70	7.40	20.17	129.67
643	42.19	152.63	2.64	6.83	18.75	129.63
644	42.26	151.22	2.63	6.94	18.97	129.60
645	42.34	157.33	2.63	6.94	18.07	129.69
646	42.40	154.04	2.66	6.94	18.68	129.71
647	42.46	152.91	2.75	6.94	19.24	129.93
648	42.53	150.18	2.81	6.94	19.96	130.07
649	42.60	147.73	2.83	6.94	20.44	130.07
650	42.67	142.75	2.82	6.94	21.27	129.95
651	42.73	136.25	2.83	6.94	22.54	129.88
652	42.80	128.07	2.87	6.94	24.39	129.83
653	42.87	118.38	2.89	6.94	26.70	129.67
654	42.94	106.90	2.88	6.94	29.79	129.42
655	43.00	97.20	2.80	6.94	32.42	128.97
656	43.07	91.75	2.59	6.94	33.18	128.26
657	43.14	90.05	2.57	6.94	33.71	128.15
658	43.20	90.05	2.57	6.94	33.73	128.14
659	43.27	89.58	2.57	6.94	33.96	128.14
660	43.34	89.77	2.59	6.94	34.04	128.21
661	43.39	90.71	2.61	7.06	33.86	128.30
662	43.47	90.33	2.63	6.94	34.15	128.34
663	43.54	84.88	2.58	6.94	36.04	128.05
664	43.60	78.38	2.50	6.94	38.42	127.61
665	43.67	71.51	2.37	6.94	40.86	127.00
666	43.73	64.08	2.21	6.94	43.61	126.22
667	43.80	57.49	2.06	6.94	46.49	125.45
668	43.83	54.58	1.99	6.94	47.87	125.05
669	43.90	49.78	1.82	6.94	50.00	124.18
670	43.97	45.73	1.66	6.94	51.92	123.32
671	44.03	41.59	1.58	6.94	54.95	122.70
672	44.10	38.30	1.48	6.94	57.40	122.04

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.17	36.13	1.39	6.94	58.86	121.42
674	44.23	33.31	1.38	6.94	62.50	121.19
675	44.30	29.83	1.41	7.06	68.32	121.09
676	44.37	27.85	1.41	7.06	71.83	120.92
677	44.44	28.42	1.35	7.17	69.99	120.66
678	44.50	31.81	1.40	7.29	65.16	121.20
679	44.57	35.85	1.54	7.40	61.31	122.15
680	44.64	36.89	1.61	7.40	60.87	122.54
681	44.70	36.32	1.63	7.40	61.91	122.62
682	44.77	39.14	1.74	7.51	59.81	123.29
683	44.84	52.04	1.87	7.63	49.20	124.50
684	44.90	72.93	1.99	7.63	38.03	125.76
685	44.97	88.92	2.05	7.51	31.64	126.48
686	45.04	96.54	2.06	7.40	29.12	126.71
687	45.11	99.84	2.05	7.06	28.06	126.76
688	45.17	103.13	2.04	7.06	27.03	126.80
689	45.24	106.05	2.05	6.94	26.27	126.89
690	45.31	108.59	2.04	6.94	25.55	126.91
691	45.37	110.38	2.02	6.72	25.02	126.90
692	45.44	112.17	2.07	6.72	24.89	127.11
693	45.48	113.20	2.12	6.72	24.94	127.31
694	45.54	115.18	2.21	6.72	24.99	127.65
695	45.61	116.59	2.29	6.72	25.10	127.93
696	45.69	115.36	2.36	6.72	25.82	128.13
697	45.76	118.94	2.37	6.60	25.06	128.26
698	45.83	118.94	2.37	6.60	25.04	128.23
699	45.89	117.91	2.34	6.60	25.17	128.12
700	45.96	117.91	2.33	6.60	25.14	128.10
701	46.03	117.91	2.34	6.60	25.22	128.13
702	46.09	117.91	2.36	6.60	25.35	128.19
703	46.16	118.19	2.37	6.60	25.39	128.24
704	46.23	118.56	2.41	6.72	25.49	128.34
705	46.29	119.03	2.41	6.60	25.44	128.37
706	46.36	119.13	2.41	6.60	25.43	128.37
707	46.42	119.60	2.40	6.60	25.30	128.36
708	46.46	119.69	2.40	6.60	25.27	128.35
709	46.53	119.50	2.39	6.72	25.32	128.33
710	46.59	119.13	2.40	6.60	25.46	128.34
711	46.66	118.85	2.41	6.60	25.59	128.35
712	46.73	118.28	2.41	6.60	25.77	128.35
713	46.80	117.81	2.41	6.60	25.90	128.34
714	46.86	117.25	2.41	6.60	26.08	128.34
715	46.93	116.68	2.41	6.60	26.26	128.33
716	46.99	116.21	2.39	6.60	26.29	128.26
717	47.06	115.36	2.37	6.72	26.38	128.16
718	47.13	114.33	2.33	6.60	26.46	128.02
719	47.20	112.17	2.28	6.60	26.78	127.82
720	47.26	110.00	2.24	6.60	27.15	127.64

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.33	106.61	2.21	6.38	27.96	127.47
722	47.40	103.51	2.20	6.60	28.82	127.36
723	47.47	101.34	2.20	6.49	29.51	127.30
724	47.53	99.65	2.21	6.60	30.11	127.29
725	47.60	98.24	2.22	6.60	30.71	127.31
726	47.66	98.24	2.22	6.49	30.72	127.30
727	47.73	98.24	2.18	6.49	30.48	127.16
728	47.80	98.24	2.09	6.49	29.95	126.87
729	47.87	96.83	2.00	6.38	29.77	126.48
730	47.93	93.82	1.95	6.38	30.47	126.22
731	48.00	89.20	1.94	6.38	32.14	126.09
732	48.03	86.38	1.96	6.38	33.34	126.06
733	48.10	79.42	1.82	6.38	35.22	125.32
734	48.17	71.89	1.57	6.38	36.61	123.98
735	48.24	63.80	1.65	6.49	41.46	124.09
736	48.30	56.36	1.68	6.38	46.21	123.92
737	48.37	49.31	1.66	6.49	51.13	123.48
738	48.43	39.62	1.59	6.49	59.76	122.66
739	48.50	40.18	1.55	6.83	58.70	122.50
740	48.56	36.42	1.57	6.83	63.42	122.34
741	48.63	32.18	1.57	6.94	69.57	122.07
742	48.70	32.09	1.45	7.17	68.08	121.45
743	48.76	31.99	1.28	7.40	65.82	120.51
744	48.82	40.74	1.24	7.74	54.42	120.90
745	48.89	53.73	1.28	8.08	44.13	121.80
746	48.95	64.93	1.28	7.97	37.74	122.28
747	49.02	68.69	1.31	7.85	36.02	122.56
748	49.09	66.15	1.41	7.63	38.44	123.02
749	49.15	65.77	1.55	7.63	39.94	123.71
750	49.23	61.16	1.69	7.51	43.70	124.16
751	49.28	55.61	1.76	7.63	47.85	124.22
752	49.35	47.24	1.75	7.51	54.30	123.78
753	49.42	41.21	1.62	7.63	58.80	122.86
754	49.48	37.45	1.50	7.74	61.74	122.06
755	49.55	35.38	1.40	7.74	63.15	121.42
756	49.62	35.10	1.32	7.97	62.52	120.99
757	49.69	35.85	1.23	8.20	60.31	120.53
758	49.75	35.85	1.21	8.31	60.10	120.42
759	49.82	34.16	1.22	8.31	62.47	120.35
760	49.87	32.93	1.15	8.31	63.11	119.81
761	49.94	32.09	0.80	8.77	58.09	117.08
762	50.02	31.99	0.56	8.77	52.84	114.45
763	50.07	33.59	0.68	8.77	53.77	116.05
764	50.16	39.14	0.85	8.99	50.86	118.06
765	50.21	40.93	1.00	8.99	51.46	119.33
766	50.27	43.47	1.23	15.14	52.18	120.98
767	50.33	56.08	1.51	15.82	45.57	123.13
768	50.40	71.80	1.82	16.05	39.66	125.10

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.47	100.68	2.04	15.71	29.82	126.73
770	50.53	124.12	2.17	14.91	24.34	127.70
771	50.61	147.92	2.39	14.12	20.82	128.85
772	50.66	156.20	2.48	13.89	19.89	129.25
773	50.73	164.77	2.51	13.55	18.71	129.46
774	50.80	170.22	2.49	13.21	17.86	129.47
775	50.87	172.76	2.45	12.52	17.37	129.38
776	50.92	173.42	2.43	12.29	17.24	129.36
777	51.01	174.08	2.44	12.29	17.19	129.37
778	51.07	170.32	2.44	11.16	17.73	129.33
779	51.13	166.27	2.45	10.93	18.34	129.29
780	51.20	162.13	2.47	10.47	19.07	129.30
781	51.26	158.46	2.55	10.24	20.00	129.48
782	51.32	154.13	2.58	10.70	20.85	129.50
783	51.39	147.73	2.58	10.24	21.98	129.40
784	51.45	141.81	2.78	10.24	24.01	129.83
785	51.52	140.68	2.84	10.24	24.53	129.97
786	51.59	145.95	2.81	9.45	23.39	129.98
787	51.65	143.50	2.85	9.79	24.06	130.04
788	51.71	148.02	2.96	9.45	23.70	130.40
789	51.78	148.30	3.12	9.45	24.35	130.80
790	51.84	145.48	3.17	9.11	25.13	130.87
791	51.92	143.59	3.11	9.56	25.27	130.69
792	51.97	143.59	3.11	8.99	25.29	130.69
793	52.04	143.59	3.10	8.99	25.29	130.67
794	52.10	143.59	3.07	8.88	25.18	130.60
795	52.17	144.53	3.19	8.88	25.53	130.90
796	52.23	155.92	3.27	8.88	23.71	131.26
797	52.30	164.95	3.32	9.11	22.38	131.51
798	52.37	177.28	3.36	9.11	20.67	131.77
799	52.44	189.70	3.44	9.11	19.28	132.12
800	52.50	181.80	3.53	8.99	20.64	132.19
801	52.56	198.64	3.63	8.99	18.80	132.61
802	52.63	197.89	3.65	8.99	18.97	132.64
803	52.69	196.01	3.59	8.88	19.03	132.50
804	52.77	194.12	3.48	9.34	18.92	132.24
805	52.85	194.97	3.37	8.88	18.48	132.02
806	52.92	191.49	3.28	8.99	18.64	131.79
807	52.98	187.82	3.21	8.88	18.86	131.58
808	53.05	183.49	2.88	8.99	18.24	130.72
809	53.09	181.80	2.85	8.88	18.35	130.63
810	53.15	178.50	2.92	8.99	19.06	130.75
811	53.22	175.40	2.96	8.99	19.66	130.81
812	53.29	173.61	3.03	8.99	20.20	130.96
813	53.36	173.47	3.11	8.77	20.54	131.16
814	53.41	173.47	3.16	8.88	20.73	131.27
815	53.48	173.33	3.18	9.45	20.84	131.32
816	53.55	178.22	3.19	9.45	20.17	131.40

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.61	183.21	3.24	8.88	19.66	131.58
818	53.69	190.74	3.35	9.34	19.07	131.93
819	53.74	196.10	3.41	9.11	18.60	132.12
820	53.81	201.56	3.49	9.22	18.23	132.37
821	53.89	208.05	3.58	9.11	17.78	132.63
822	53.95	213.70	3.65	8.99	17.36	132.83
823	54.01	220.57	3.71	9.11	16.83	133.02
824	54.07	227.44	3.75	9.45	16.27	133.18
825	54.15	232.70	3.80	9.11	15.91	133.33
826	54.22	236.37	3.82	9.11	15.64	133.42
827	54.27	238.92	3.84	8.88	15.47	133.48
828	54.35	241.93	3.88	8.99	15.31	133.58
829	54.40	244.94	3.89	8.99	15.07	133.62
830	54.48	247.85	3.89	9.34	14.83	133.65
831	54.53	250.49	3.90	9.22	14.66	133.71
832	54.60	258.11	3.94	9.22	14.14	133.85
833	54.66	264.60	4.02	9.22	13.83	134.05
834	54.73	271.85	4.09	9.22	13.48	134.26
835	54.80	278.91	4.17	9.11	13.15	134.45
836	54.86	284.93	4.26	9.68	12.95	134.66
837	54.93	289.63	4.37	10.02	12.89	134.89
838	55.00	292.83	4.44	10.02	12.82	135.03
839	55.06	294.53	4.50	10.02	12.86	135.15
840	55.13	297.44	4.55	10.02	12.78	135.26
841	55.20	299.42	4.57	10.02	12.70	135.30
842	55.27	300.83	4.58	10.13	12.64	135.33
843	55.34	300.78	4.60	10.13	12.68	135.35
844	55.40	300.78	4.62	10.19	12.73	135.38
845	55.47	300.74	4.63	10.24	12.77	135.41
846	55.53	302.06	4.62	9.68	12.67	135.41
847	55.60	303.66	4.46	9.68	12.25	135.16
848	55.67	304.60	4.29	9.68	11.82	134.87
849	55.73	304.41	4.36	9.68	12.00	134.99
850	55.80	303.37	4.41	10.02	12.18	135.07
851	55.87	302.15	4.45	10.02	12.33	135.12
852	55.93	297.07	4.47	10.02	12.71	135.11
853	55.98	277.12	4.47	10.02	14.10	134.95
854	56.05	288.69	4.47	10.36	13.29	135.05
855	56.10	288.98	4.47	9.90	13.28	135.05
856	56.19	291.52	4.47	10.59	13.11	135.07
857	56.24	291.05	4.48	10.70	13.16	135.08
858	56.31	289.26	4.46	10.70	13.26	135.04
859	56.38	285.59	4.45	10.70	13.49	134.99
860	56.46	283.99	4.40	10.59	13.49	134.89
861	56.52	281.64	4.32	10.13	13.49	134.74
862	56.58	278.06	4.21	10.02	13.51	134.52
863	56.65	273.64	4.14	10.02	13.67	134.35
864	56.71	269.40	4.08	10.36	13.84	134.20

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.77	264.98	3.99	10.02	13.98	134.01
866	56.83	261.31	3.90	10.36	14.03	133.80
867	56.90	255.29	3.80	10.36	14.27	133.56
868	56.96	248.04	3.69	10.19	14.60	133.28
869	57.03	239.29	3.61	9.56	15.14	133.02
870	57.10	232.23	3.57	10.02	15.66	132.86
871	57.16	228.56	3.55	9.56	15.98	132.79
872	57.23	229.60	3.20	10.36	14.84	132.04
873	57.30	235.62	2.61	9.90	12.45	130.62
874	57.37	243.81	2.74	9.56	12.20	131.04
875	57.43	250.87	2.89	9.56	12.13	131.50
876	57.50	254.25	3.05	9.79	12.36	131.94
877	57.57	255.10	3.20	9.79	12.73	132.30
878	57.62	219.72	3.29	9.56	16.11	132.13
879	57.68	244.56	3.32	9.90	13.95	132.48
880	57.76	243.24	3.28	10.24	13.95	132.37
881	57.82	240.23	3.28	10.24	14.20	132.34
882	57.88	237.32	3.28	10.24	14.46	132.30
883	57.94	233.83	3.28	10.13	14.77	132.26
884	58.01	231.01	3.27	9.56	15.01	132.21
885	58.08	226.96	3.26	9.79	15.39	132.16
886	58.14	223.86	3.25	9.45	15.64	132.08
887	58.21	220.94	3.21	10.02	15.84	131.98
888	58.28	220.94	3.23	10.24	15.90	132.02
889	58.35	220.94	3.27	10.24	16.03	132.11
890	58.40	220.94	3.29	10.24	16.09	132.15
891	58.47	223.77	3.30	9.34	15.85	132.20
892	58.54	226.12	3.34	10.02	15.76	132.32
893	58.61	226.31	3.38	9.68	15.87	132.41
894	58.67	225.46	3.39	10.36	15.98	132.42
895	58.74	222.54	3.34	9.56	16.13	132.28
896	58.82	222.54	3.29	10.36	15.99	132.17
897	58.88	224.42	3.29	9.90	15.80	132.18
898	58.95	228.47	2.05	10.36	11.20	128.77
899	59.02	236.28	1.55	9.68	8.63	126.81
900	59.09	247.20	1.62	9.34	8.21	127.26
901	59.12	252.47	1.71	9.79	8.22	127.69
902	59.19	260.37	1.89	9.45	8.38	128.48
903	59.26	263.95	2.04	9.45	8.70	129.09
904	59.32	261.88	2.17	9.11	9.28	129.52
905	59.40	259.81	2.32	8.99	9.92	130.00
906	59.46	267.33	2.44	9.11	9.82	130.44
907	59.52	271.38	2.60	10.02	10.03	130.92
908	59.60	274.67	2.87	9.96	10.63	131.69
909	59.66	276.74	3.01	9.96	10.88	132.05
910	59.73	277.21	2.99	9.90	10.80	132.00
911	59.78	279.47	2.97	9.11	10.62	131.98
912	59.85	285.49	2.98	9.22	10.27	132.05

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.93	291.80	2.99	9.45	9.92	132.12
914	59.99	295.84	3.11	9.34	10.00	132.45
915	60.04	285.87	3.17	9.90	10.76	132.50
916	60.11	287.56	3.23	8.65	10.82	132.66
917	60.18	285.87	3.27	8.77	11.04	132.74
918	60.24	285.49	3.31	8.77	11.17	132.82
919	60.30	283.89	3.42	8.77	11.55	133.04
920	60.37	283.99	3.46	8.77	11.67	133.13
921	60.44	284.08	3.47	8.77	11.69	133.15
922	60.50	282.20	3.47	9.34	11.81	133.13
923	60.58	290.39	3.47	8.99	11.29	133.20
924	60.63	293.40	3.47	8.99	11.11	133.23
925	60.70	298.95	3.46	8.99	10.75	133.25
926	60.78	305.07	3.43	8.99	10.33	133.24
927	60.83	309.02	3.42	8.88	10.09	133.26
928	60.89	315.70	3.40	9.90	9.68	133.26
929	60.97	326.33	3.32	8.88	8.96	133.17
930	61.03	332.73	3.23	9.68	8.44	133.02
931	61.10	337.53	3.12	8.99	7.96	132.79
932	61.16	342.24	2.96	8.88	7.39	132.44
933	61.22	344.87	2.76	9.90	6.81	131.94
934	61.30	345.62	2.57	9.90	6.35	131.45
935	61.36	343.55	2.48	9.90	6.19	131.15
936	61.42	340.92	2.18	9.90	5.55	130.21
937	61.48	337.34	1.43	9.11	3.56	127.09
938	61.57	335.37	1.48	8.88	3.77	127.31
939	61.64	331.88	1.53	8.88	4.04	127.52
940	61.70	328.12	1.59	9.34	4.36	127.78
941	61.76	307.70	1.61	8.99	5.23	127.72
942	61.82	300.36	1.61	8.65	5.56	127.67
943	61.88	305.35	1.61	9.56	5.35	127.72
944	61.96	298.86	1.64	8.88	5.73	127.79
945	62.03	286.53	1.75	8.88	6.68	128.16
946	62.08	275.90	1.80	9.11	7.42	128.28
947	62.15	257.45	1.85	9.11	8.68	128.31
948	62.22	238.54	1.96	9.45	10.38	128.53
949	62.29	218.78	2.10	8.54	12.55	128.83
950	62.36	200.62	2.23	8.77	14.88	129.06
951	62.41	191.02	2.32	8.77	16.37	129.25
952	62.48	201.98	2.51	8.65	15.88	129.94
953	62.55	191.77	2.66	9.34	17.68	130.25
954	62.62	203.35	2.66	9.34	16.34	130.40
955	62.69	216.24	2.54	9.56	14.54	130.21
956	62.73	224.52	2.44	9.34	13.41	130.02
957	62.80	231.76	2.33	9.90	12.35	129.73
958	62.87	237.50	2.29	8.88	11.77	129.68
959	62.95	247.38	2.37	9.79	11.29	130.03
960	63.02	262.06	1.92	9.79	8.71	128.61

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	63.06	272.98	1.55	9.79	6.74	127.14
962	63.13	290.10	1.59	9.79	6.04	127.49
963	63.20	309.96	1.57	9.45	5.10	127.56
964	63.26	322.19	1.54	9.45	4.54	127.54
965	63.34	335.46	1.50	9.45	3.94	127.44
966	63.39	336.50	1.48	9.68	3.83	127.32
967	63.45	337.53	1.46	9.45	3.74	127.23
968	63.52	343.55	1.46	9.45	3.54	127.26
969	63.59	343.46	1.45	9.22	3.54	127.26
970	63.66	339.51	1.48	9.11	3.76	127.36
971	63.72	337.06	1.53	8.99	3.97	127.56
972	63.79	333.30	1.56	8.99	4.23	127.71
973	63.86	324.83	1.58	8.99	4.59	127.73
974	63.91	318.62	1.61	9.45	4.94	127.83
975	63.98	305.82	1.64	8.99	5.57	127.87
976	64.05	298.01	1.64	9.51	5.91	127.79
977	64.12	292.83	1.66	9.22	6.24	127.85
978	64.18	288.51	1.72	9.56	6.65	128.07
979	64.25	278.15	1.89	9.34	7.78	128.67
980	64.31	265.36	2.17	9.34	9.49	129.56
981	64.38	252.65	2.38	8.77	11.06	130.11
982	64.45	239.39	2.41	8.77	12.19	130.06
983	64.50	225.37	2.39	8.77	13.32	129.86
984	64.58	206.45	2.36	9.11	15.05	129.55
985	64.64	191.49	2.43	9.11	17.04	129.58
986	64.72	180.48	2.38	9.11	18.28	129.30
987	64.77	190.64	2.31	9.11	16.65	129.19
988	64.83	184.06	2.25	8.99	17.24	128.93
989	64.91	189.80	2.21	9.45	16.35	128.87
990	64.97	196.95	2.18	9.56	15.40	128.86
991	65.04	208.62	1.99	9.22	13.34	128.31
992	65.10	215.96	1.45	9.11	10.23	126.08
993	65.17	220.28	1.24	9.34	8.87	124.98
994	65.24	229.60	1.12	9.34	5.00	124.36
995	65.31	240.33	0.96	9.56	5.00	123.33
996	65.36	237.22	0.80	10.70	5.00	122.02
997	65.42	230.26	0.68	9.79	5.00	120.68
998	65.49	243.62	0.59	9.68	4.05	119.88
999	65.55	244.28	0.59	9.11	3.97	119.77
1000	65.62	239.10	0.56	9.11	4.04	119.32
1001	65.69	231.29	0.53	8.99	4.25	118.85
1002	65.76	221.88	0.53	8.99	4.77	118.80
1003	65.83	211.25	0.53	9.68	5.00	118.75
1004	65.89	203.91	0.54	8.77	5.00	118.71
1005	65.95	194.22	0.53	9.22	5.00	118.53
1006	66.03	178.41	0.52	8.77	5.00	118.11
1007	66.08	167.59	0.51	8.77	5.00	117.86
1008	66.16	152.53	0.53	8.65	5.00	117.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	66.22	142.84	0.55	8.77	5.00	118.06
1010	66.29	132.77	0.56	8.99	5.00	117.94
1011	66.36	125.72	0.55	8.77	5.00	117.74
1012	66.42	117.53	0.55	8.65	5.00	117.54
1013	66.49	109.53	0.55	8.42	17.32	117.35
1014	66.55	102.76	0.56	9.11	19.00	117.31
1015	66.62	97.58	0.64	8.31	21.49	118.18
1016	66.69	94.85	0.59	8.08	21.56	117.52
1017	66.75	93.25	0.50	8.08	20.62	116.26
1018	66.82	92.31	0.59	8.65	22.35	117.48
1019	66.89	89.49	0.74	8.20	25.44	119.06
1020	66.96	85.06	0.97	8.88	30.03	120.86
1021	67.00	74.43	1.11	8.88	36.04	121.56
1022	67.08	85.30	1.29	7.85	33.57	122.96
1023	67.14	81.96	1.30	8.88	34.90	122.93
1024	67.21	85.54	1.47	7.97	35.05	123.93
1025	67.28	89.96	1.81	8.88	36.06	125.58
1026	67.34	101.16	1.80	9.34	32.38	125.86
1027	67.41	121.10	1.77	8.88	26.23	126.15
1028	67.47	152.35	1.72	8.65	19.44	126.48
1029	67.54	180.01	1.66	8.88	15.14	126.63
1030	67.61	201.46	1.62	10.13	12.63	126.76
1031	67.67	227.44	1.58	9.22	10.15	126.85
1032	67.74	243.81	1.47	8.08	8.49	126.49
1033	67.80	254.54	1.26	7.74	6.91	125.45
1034	67.87	263.95	1.21	7.74	5.00	125.24
1035	67.94	270.81	1.29	7.74	5.00	125.78
1036	68.00	277.12	1.26	7.74	5.00	125.69
1037	68.07	281.17	1.33	7.74	5.00	126.09
1038	68.14	284.46	1.49	7.74	6.27	126.95
1039	68.20	286.53	1.41	7.85	5.89	126.60
1040	68.27	289.26	1.33	7.85	5.00	126.19
1041	68.34	291.05	1.38	7.85	5.00	126.47
1042	68.41	295.09	1.47	7.97	5.70	126.94
1043	68.44	296.69	1.51	7.97	5.79	127.17
1044	68.51	296.93	1.58	7.97	6.02	127.50
1045	68.58	297.16	1.59	7.85	6.06	127.55
1046	68.65	304.97	1.56	7.85	5.62	127.50
1047	68.73	308.17	1.56	7.85	5.47	127.50
1048	68.78	309.87	1.56	7.85	5.40	127.51
1049	68.83	310.52	1.56	7.85	5.39	127.54
1050	68.92	315.42	1.61	7.85	5.34	127.78
1051	68.97	319.46	1.65	7.85	5.30	127.99
1052	69.03	321.53	1.69	7.97	5.36	128.20
1053	69.09	323.23	1.70	7.97	5.33	128.26
1054	69.18	326.61	1.77	7.85	5.40	128.56
1055	69.24	331.23	1.81	7.97	5.35	128.77
1056	69.29	336.31	1.84	8.08	5.23	128.92

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	69.37	344.21	1.85	7.97	4.97	129.01
1058	69.43	348.63	1.85	7.97	4.80	129.04
1059	69.51	354.66	1.87	7.97	4.66	129.17
1060	69.57	356.54	1.77	8.65	4.33	128.80
1061	69.63	356.82	1.42	8.08	3.31	127.20
1062	69.69	354.84	1.34	8.08	3.12	126.75
1063	69.76	352.87	1.34	8.20	3.17	126.71
1064	69.82	354.09	1.37	8.88	3.25	126.91
1065	69.91	348.26	1.51	8.88	3.86	127.56
1066	69.95	234.02	1.54	7.97	9.67	126.73
1067	70.02	320.59	1.59	7.97	5.14	127.75
1068	70.08	315.32	1.59	7.63	5.35	127.69
1069	70.16	315.70	1.53	7.51	5.00	127.42
1070	70.22	305.25	1.51	7.74	5.52	127.23
1071	70.28	299.42	1.51	7.85	5.79	127.20
1072	70.35	297.82	1.47	7.85	5.72	126.98
1073	70.42	298.29	1.40	7.85	5.00	126.63
1074	70.48	297.82	1.35	7.85	5.00	126.35
1075	70.55	298.39	1.31	7.85	5.00	126.16
1076	70.61	299.14	1.29	7.85	5.01	126.02
1077	70.69	301.21	1.26	7.85	4.84	125.91
1078	70.75	303.00	1.22	7.85	4.60	125.65
1079	70.82	302.90	1.16	7.63	4.38	125.30
1080	70.88	299.04	1.13	7.63	4.40	125.04
1081	70.95	295.66	1.13	7.74	4.55	125.02
1082	71.02	290.58	1.15	7.29	4.88	125.13
1083	71.08	283.99	1.12	7.29	5.00	124.89
1084	71.15	281.73	0.99	6.94	4.59	123.96
1085	71.22	279.19	0.69	7.17	3.33	121.26
1086	71.28	276.74	0.67	7.06	3.37	121.10
1087	71.35	276.08	0.72	7.06	3.63	121.62
1088	71.42	276.37	0.80	7.06	3.96	122.31
1089	71.49	280.13	0.84	7.06	4.01	122.74
1090	71.54	276.23	0.89	7.06	4.40	123.11
1091	71.59	272.32	0.93	7.06	4.76	123.39
1092	71.67	283.89	0.96	7.17	4.41	123.78
1093	71.73	290.86	1.01	7.17	4.33	124.20
1094	71.79	293.87	1.08	7.29	4.47	124.67
1095	71.86	294.25	1.13	7.29	4.67	125.03
1096	71.92	292.36	1.15	7.29	4.85	125.14
1097	71.99	286.62	1.16	7.40	5.00	125.15
1098	72.06	277.12	1.15	7.40	5.00	124.99
1099	72.12	271.94	1.15	7.40	5.00	124.95
1100	72.19	265.17	1.15	7.40	5.00	124.88
1101	72.26	260.28	1.21	7.40	5.00	125.22
1102	72.31	256.32	1.40	7.40	7.78	126.28
1103	72.38	253.31	1.60	7.40	8.80	127.21
1104	72.46	252.09	1.56	7.40	8.74	127.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	72.52	253.88	1.14	7.40	5.00	124.74
1106	72.59	262.06	0.89	7.06	5.00	123.00
1107	72.65	268.37	1.07	7.29	5.00	124.43
1108	72.71	278.15	1.60	7.63	7.34	127.43
1109	72.78	282.48	2.14	8.20	8.99	129.59
1110	72.84	279.94	2.17	8.08	9.26	129.69
1111	72.90	282.77	1.79	7.51	7.80	128.31
1112	72.98	283.05	1.61	7.40	7.15	127.55
1113	73.03	295.28	1.60	7.85	6.49	127.60
1114	73.11	298.57	1.73	8.31	6.79	128.19
1115	73.17	295.56	1.95	9.11	7.68	129.05
1116	73.23	303.18	1.98	9.79	7.39	129.21
1117	73.30	301.30	2.07	9.45	7.76	129.50
1118	73.36	302.24	2.30	10.36	8.43	130.29
1119	73.44	314.85	2.38	9.56	8.03	130.66
1120	73.51	320.69	2.36	9.56	7.68	130.63
1121	73.56	314.90	2.22	10.02	7.57	130.14
1122	73.63	314.95	1.86	10.13	6.45	128.83
1123	73.70	327.37	1.85	10.02	5.90	128.90
1124	73.76	332.64	1.93	9.79	5.92	129.25
1125	73.83	330.85	1.88	10.81	5.86	129.06
1126	73.89	316.55	1.96	10.70	6.73	129.25
1127	73.95	323.89	2.03	12.29	6.60	129.55
1128	74.02	337.06	1.85	11.61	5.52	128.98
1129	74.09	336.50	1.57	10.24	4.70	127.78
1130	74.16	326.52	1.05	9.90	3.29	124.77
1131	74.24	330.47	0.90	9.90	2.62	123.69
1132	74.31	320.87	0.97	10.70	3.19	124.14
1133	74.38	307.23	1.00	9.90	3.77	124.22
1134	74.41	301.30	0.97	11.16	3.90	123.99
1135	74.48	290.86	0.92	10.47	4.10	123.51
1136	74.55	277.35	0.99	12.52	5.00	123.93
1137	74.62	257.64	0.97	11.95	5.00	123.62
1138	74.68	263.85	0.94	12.07	5.00	123.41
1139	74.75	271.19	0.95	12.07	5.00	123.54
1140	74.82	279.57	1.12	12.29	5.00	124.81
1141	74.89	285.87	1.15	12.18	5.00	125.07
1142	74.94	287.56	1.24	11.50	5.00	125.67
1143	75.01	286.15	1.33	11.04	5.00	126.17
1144	75.07	268.09	1.36	11.04	7.11	126.15
1145	75.14	273.45	0.00	11.04	100.00	87.36
1146	75.20	267.05	0.00	11.04	100.00	87.36
1147	75.27	264.79	0.00	11.16	100.00	87.36
1148	75.33	263.19	0.00	10.24	100.00	87.36
1149	75.41	262.53	0.00	10.36	100.00	87.36
1150	75.48	250.96	0.00	9.90	100.00	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.07	0.00	0.00	0.00	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
2	0.14	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
3	0.20	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
4	0.27	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
5	0.35	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
6	0.41	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
7	0.47	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
8	0.54	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
9	0.60	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
10	0.66	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
11	0.74	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
12	0.80	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
13	0.87	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
14	0.93	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
15	0.99	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
16	1.05	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
17	1.12	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
18	1.19	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
19	1.27	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
20	1.32	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
21	1.38	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
22	1.45	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
23	1.51	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
24	1.59	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
25	1.65	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
26	1.71	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
27	1.77	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
28	1.84	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
29	1.92	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
30	1.98	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
31	2.04	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
32	2.11	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
33	2.17	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
34	2.23	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
35	2.30	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
36	2.37	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
37	2.43	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
38	2.49	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
39	2.56	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
40	2.65	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
41	2.71	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
42	2.78	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
43	2.83	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
44	2.90	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
45	2.96	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
46	3.03	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
47	3.11	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
48	3.16	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	3.22	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
50	3.28	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
51	3.36	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
52	3.44	0.21	0.00	0.21	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
53	3.49	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
54	3.56	0.22	0.00	0.22	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
55	3.61	0.22	0.00	0.22	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
56	3.69	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
57	3.74	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
58	3.83	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
59	3.88	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
60	3.96	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
61	4.00	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
62	4.08	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
63	4.16	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
64	4.21	0.25	0.00	0.25	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
65	4.29	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
66	4.34	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
67	4.40	0.27	0.00	0.27	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
68	4.47	0.27	0.00	0.27	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
69	4.55	0.28	0.00	0.28	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
70	4.60	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
71	4.68	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
72	4.73	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
73	4.81	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
74	4.87	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
75	4.92	0.30	0.00	0.30	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
76	5.00	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
77	5.08	0.31	0.00	0.31	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
78	5.13	0.31	0.00	0.31	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
79	5.19	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
80	5.27	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
81	5.32	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
82	5.39	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
83	5.45	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
84	5.53	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
85	5.58	0.34	0.00	0.34	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
86	5.66	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
87	5.72	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
88	5.80	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
89	5.85	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
90	5.91	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
91	5.99	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
92	6.04	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
93	6.12	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
94	6.18	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
95	6.26	0.38	0.00	0.38	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
96	6.31	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	6.39	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
98	6.44	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
99	6.52	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
100	6.58	0.40	0.00	0.40	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
101	6.63	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
102	6.71	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
103	6.77	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
104	6.85	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
105	6.91	0.42	0.00	0.42	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
106	6.96	0.42	0.00	0.42	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
107	7.04	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
108	7.09	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
109	7.17	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
110	7.22	0.44	0.00	0.44	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
111	7.31	0.44	0.00	0.44	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
112	7.36	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
113	7.44	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
114	7.49	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
115	7.55	0.46	0.00	0.46	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
116	7.63	0.46	0.00	0.46	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
117	7.68	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
118	7.76	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
119	7.81	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
120	7.89	0.48	0.00	0.48	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
121	7.95	0.48	0.00	0.48	0.98	0.493	1.05	0.468	1.10	1.30	2.000	No
122	8.03	0.49	0.00	0.49	0.98	0.494	1.05	0.468	1.10	1.30	0.542	No
123	8.09	0.49	0.00	0.49	0.98	0.495	1.05	0.470	1.10	1.30	0.545	No
124	8.14	0.50	0.00	0.49	0.98	0.497	1.05	0.471	1.10	1.30	0.549	No
125	8.22	0.50	0.01	0.49	0.98	0.499	1.05	0.474	1.10	1.30	0.553	No
126	8.27	0.50	0.01	0.50	0.98	0.501	1.05	0.475	1.10	1.30	0.557	No
127	8.35	0.51	0.01	0.50	0.98	0.503	1.05	0.477	1.10	1.30	0.562	No
128	8.40	0.51	0.01	0.50	0.98	0.505	1.05	0.479	1.10	1.30	0.566	No
129	8.48	0.52	0.02	0.50	0.98	0.507	1.05	0.481	1.10	1.30	0.570	No
130	8.54	0.52	0.02	0.50	0.98	0.508	1.05	0.482	1.10	1.30	0.573	No
131	8.62	0.53	0.02	0.51	0.98	0.511	1.05	0.484	1.10	1.30	0.577	No
132	8.67	0.53	0.02	0.51	0.98	0.512	1.05	0.486	1.10	1.30	0.579	No
133	8.73	0.53	0.02	0.51	0.98	0.514	1.05	0.487	1.10	1.30	0.581	No
134	8.81	0.54	0.03	0.51	0.98	0.516	1.05	0.489	1.10	1.30	0.585	No
135	8.86	0.54	0.03	0.51	0.98	0.517	1.05	0.491	1.10	1.30	0.586	No
136	8.94	0.55	0.03	0.52	0.98	0.519	1.05	0.493	1.10	1.30	0.588	No
137	9.00	0.55	0.03	0.52	0.98	0.521	1.05	0.494	1.10	1.30	0.588	No
138	9.08	0.55	0.03	0.52	0.98	0.523	1.05	0.496	1.10	1.30	0.590	No
139	9.13	0.56	0.04	0.52	0.98	0.524	1.05	0.497	1.10	1.30	0.591	No
140	9.20	0.56	0.04	0.52	0.98	0.526	1.05	0.499	1.10	1.30	0.593	No
141	9.26	0.57	0.04	0.53	0.98	0.528	1.05	0.500	1.10	1.30	0.595	No
142	9.33	0.57	0.04	0.53	0.98	0.529	1.05	0.502	1.10	1.30	0.597	No
143	9.39	0.57	0.04	0.53	0.98	0.531	1.05	0.503	1.10	1.30	0.602	No
144	9.46	0.58	0.05	0.53	0.98	0.533	1.05	0.505	1.08	1.30	0.626	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	9.53	0.58	0.05	0.53	0.98	0.534	1.05	0.507	1.09	1.30	0.623	No
146	9.60	0.59	0.05	0.54	0.98	0.536	1.05	0.508	1.09	1.30	0.621	No
147	9.67	0.59	0.05	0.54	0.98	0.538	1.05	0.510	1.08	1.30	0.635	No
148	9.73	0.59	0.05	0.54	0.98	0.539	1.05	0.511	1.07	1.30	0.644	No
149	9.79	0.60	0.06	0.54	0.98	0.540	1.05	0.513	1.07	1.30	0.641	No
150	9.86	0.60	0.06	0.54	0.98	0.542	1.05	0.514	1.08	1.30	0.641	No
151	9.91	0.60	0.06	0.55	0.98	0.543	1.05	0.515	1.08	1.30	0.640	No
152	9.98	0.61	0.06	0.55	0.98	0.545	1.05	0.517	1.08	1.30	0.639	No
153	10.04	0.61	0.06	0.55	0.98	0.546	1.05	0.518	1.08	1.30	0.638	No
154	10.11	0.62	0.07	0.55	0.98	0.548	1.05	0.520	1.08	1.30	0.639	No
155	10.18	0.62	0.07	0.55	0.98	0.550	1.05	0.521	1.09	1.30	0.639	No
156	10.25	0.63	0.07	0.56	0.98	0.551	1.05	0.523	1.09	1.30	0.638	No
157	10.31	0.63	0.07	0.56	0.98	0.552	1.05	0.524	1.09	1.30	0.637	No
158	10.37	0.63	0.07	0.56	0.98	0.554	1.05	0.525	1.09	1.30	0.637	No
159	10.44	0.64	0.08	0.56	0.98	0.555	1.05	0.527	1.09	1.30	0.637	No
160	10.51	0.64	0.08	0.56	0.98	0.557	1.05	0.528	1.09	1.30	0.640	No
161	10.57	0.64	0.08	0.56	0.98	0.558	1.05	0.529	1.09	1.30	0.644	No
162	10.64	0.65	0.08	0.57	0.98	0.560	1.05	0.531	1.09	1.30	0.649	No
163	10.71	0.65	0.08	0.57	0.98	0.561	1.05	0.532	1.08	1.30	0.654	No
164	10.77	0.66	0.09	0.57	0.98	0.562	1.05	0.533	1.08	1.30	0.659	No
165	10.84	0.66	0.09	0.57	0.98	0.564	1.05	0.535	1.08	1.30	0.664	No
166	10.91	0.67	0.09	0.57	0.98	0.565	1.05	0.536	1.07	1.30	0.668	No
167	10.98	0.67	0.09	0.58	0.98	0.567	1.05	0.537	1.07	1.30	0.671	No
168	11.05	0.67	0.10	0.58	0.97	0.568	1.05	0.539	1.07	1.30	0.673	No
169	11.11	0.68	0.10	0.58	0.97	0.569	1.05	0.540	1.07	1.30	0.675	No
170	11.18	0.68	0.10	0.58	0.97	0.571	1.05	0.541	1.07	1.30	0.678	No
171	11.25	0.69	0.10	0.58	0.97	0.572	1.05	0.542	1.07	1.30	0.680	No
172	11.31	0.69	0.10	0.59	0.97	0.573	1.05	0.544	1.07	1.30	0.680	No
173	11.38	0.69	0.11	0.59	0.97	0.575	1.05	0.545	1.07	1.30	0.681	No
174	11.45	0.70	0.11	0.59	0.97	0.576	1.05	0.546	1.07	1.30	0.683	No
175	11.51	0.70	0.11	0.59	0.97	0.577	1.05	0.547	1.07	1.30	0.685	No
176	11.58	0.71	0.11	0.59	0.97	0.578	1.05	0.549	1.07	1.30	0.688	No
177	11.65	0.71	0.11	0.60	0.97	0.580	1.05	0.550	1.07	1.30	0.690	No
178	11.68	0.71	0.11	0.60	0.97	0.580	1.05	0.550	1.07	1.30	0.691	No
179	11.75	0.72	0.12	0.60	0.97	0.582	1.05	0.552	1.07	1.30	0.694	No
180	11.82	0.72	0.12	0.60	0.97	0.583	1.05	0.553	1.06	1.30	0.697	No
181	11.88	0.72	0.12	0.60	0.97	0.584	1.05	0.554	1.06	1.30	0.699	No
182	11.97	0.73	0.12	0.61	0.97	0.586	1.05	0.555	1.06	1.30	0.701	No
183	12.03	0.73	0.13	0.61	0.97	0.587	1.05	0.557	1.06	1.30	0.702	No
184	12.10	0.74	0.13	0.61	0.97	0.588	1.05	0.558	1.06	1.30	0.704	No
185	12.16	0.74	0.13	0.61	0.97	0.589	1.05	0.559	1.06	1.30	0.705	No
186	12.23	0.75	0.13	0.61	0.97	0.590	1.05	0.560	1.06	1.30	0.706	No
187	12.30	0.75	0.13	0.62	0.97	0.591	1.05	0.561	1.06	1.30	0.708	No
188	12.36	0.75	0.14	0.62	0.97	0.593	1.05	0.562	1.06	1.30	0.708	No
189	12.43	0.76	0.14	0.62	0.97	0.594	1.05	0.563	1.06	1.30	0.708	No
190	12.50	0.76	0.14	0.62	0.97	0.595	1.05	0.564	1.06	1.30	0.709	No
191	12.53	0.76	0.14	0.62	0.97	0.595	1.05	0.565	1.07	1.30	0.709	No
192	12.60	0.77	0.14	0.63	0.97	0.597	1.05	0.566	1.07	1.30	0.708	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	12.67	0.77	0.15	0.63	0.97	0.598	1.05	0.567	1.07	1.30	0.706	No
194	12.74	0.78	0.15	0.63	0.97	0.599	1.05	0.568	1.07	1.30	0.704	No
195	12.80	0.78	0.15	0.63	0.97	0.600	1.05	0.569	1.07	1.30	0.704	No
196	12.87	0.79	0.15	0.63	0.97	0.601	1.05	0.570	1.07	1.30	0.703	No
197	12.94	0.79	0.15	0.64	0.97	0.602	1.05	0.571	1.07	1.30	0.702	No
198	13.00	0.79	0.16	0.64	0.97	0.603	1.05	0.572	1.08	1.30	0.701	No
199	13.07	0.80	0.16	0.64	0.97	0.604	1.05	0.573	1.08	1.30	0.702	No
200	13.13	0.80	0.16	0.64	0.97	0.605	1.05	0.574	1.08	1.30	0.702	No
201	13.20	0.81	0.16	0.64	0.97	0.606	1.05	0.575	1.08	1.30	0.702	No
202	13.27	0.81	0.16	0.65	0.97	0.607	1.05	0.576	1.08	1.30	0.704	No
203	13.34	0.81	0.17	0.65	0.97	0.608	1.05	0.577	1.08	1.30	0.703	No
204	13.40	0.82	0.17	0.65	0.97	0.609	1.05	0.578	1.08	1.30	0.701	No
205	13.47	0.82	0.17	0.65	0.97	0.610	1.05	0.579	1.08	1.30	0.699	No
206	13.54	0.83	0.17	0.65	0.97	0.611	1.05	0.580	1.08	1.30	0.699	No
207	13.60	0.83	0.17	0.66	0.97	0.612	1.05	0.580	1.08	1.30	0.698	No
208	13.67	0.84	0.18	0.66	0.97	0.613	1.05	0.581	1.08	1.30	0.697	No
209	13.74	0.84	0.18	0.66	0.97	0.614	1.05	0.582	1.08	1.30	0.697	No
210	13.80	0.84	0.18	0.66	0.96	0.615	1.05	0.583	1.09	1.30	0.696	No
211	13.87	0.85	0.18	0.66	0.96	0.616	1.05	0.584	1.09	1.30	0.694	No
212	13.94	0.85	0.19	0.67	0.96	0.617	1.05	0.585	1.09	1.30	0.693	No
213	14.00	0.86	0.19	0.67	0.96	0.618	1.05	0.586	1.09	1.30	0.693	No
214	14.07	0.86	0.19	0.67	0.96	0.619	1.05	0.587	1.08	1.30	0.700	No
215	14.14	0.87	0.19	0.67	0.96	0.620	1.05	0.588	1.08	1.30	0.705	No
216	14.21	0.87	0.19	0.68	0.96	0.620	1.05	0.588	1.08	1.30	0.706	No
217	14.24	0.87	0.19	0.68	0.96	0.621	1.05	0.589	1.08	1.30	0.706	No
218	14.31	0.88	0.20	0.68	0.96	0.622	1.05	0.590	1.08	1.30	0.705	No
219	14.37	0.88	0.20	0.68	0.96	0.623	1.05	0.590	1.08	1.30	0.707	No
220	14.46	0.89	0.20	0.68	0.96	0.624	1.05	0.592	1.08	1.30	0.708	No
221	14.52	0.89	0.20	0.69	0.96	0.625	1.05	0.592	1.08	1.30	0.709	No
222	14.59	0.89	0.21	0.69	0.96	0.625	1.05	0.593	1.08	1.30	0.708	No
223	14.65	0.90	0.21	0.69	0.96	0.626	1.05	0.594	1.08	1.30	0.707	No
224	14.72	0.90	0.21	0.69	0.96	0.627	1.05	0.595	1.08	1.30	0.707	No
225	14.79	0.91	0.21	0.69	0.96	0.628	1.05	0.595	1.08	1.30	0.708	No
226	14.85	0.91	0.21	0.70	0.96	0.629	1.05	0.596	1.08	1.30	0.709	No
227	14.92	0.91	0.22	0.70	0.96	0.629	1.05	0.597	1.08	1.30	0.711	No
228	14.99	0.92	0.22	0.70	0.96	0.630	1.05	0.598	1.08	1.30	0.712	No
229	15.05	0.92	0.22	0.70	0.96	0.631	1.05	0.598	1.08	1.30	0.713	No
230	15.12	0.93	0.22	0.71	0.96	0.632	1.05	0.599	1.08	1.30	0.715	No
231	15.19	0.93	0.22	0.71	0.96	0.633	1.05	0.600	1.08	1.30	0.717	No
232	15.22	0.93	0.23	0.71	0.96	0.633	1.05	0.600	1.08	1.30	0.718	No
233	15.29	0.94	0.23	0.71	0.96	0.634	1.05	0.601	1.08	1.30	0.720	No
234	15.36	0.94	0.23	0.71	0.96	0.635	1.05	0.602	1.08	1.30	0.722	No
235	15.43	0.95	0.23	0.72	0.96	0.635	1.05	0.603	1.07	1.30	0.725	No
236	15.49	0.95	0.23	0.72	0.96	0.636	1.05	0.603	1.07	1.30	0.727	No
237	15.56	0.96	0.24	0.72	0.96	0.637	1.05	0.604	1.07	1.30	0.730	No
238	15.63	0.96	0.24	0.72	0.96	0.638	1.05	0.605	1.07	1.30	0.733	No
239	15.69	0.96	0.24	0.72	0.96	0.638	1.05	0.605	1.07	1.30	0.738	No
240	15.76	0.97	0.24	0.73	0.96	0.639	1.05	0.606	1.06	1.30	0.743	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
241	15.82	0.97	0.24	0.73	0.96	0.640	1.05	0.607	1.06	1.30	0.748	No
242	15.89	0.98	0.25	0.73	0.96	0.641	1.05	0.607	1.06	1.30	0.754	No
243	15.96	0.98	0.25	0.73	0.96	0.641	1.05	0.608	1.05	1.30	0.761	No
244	16.03	0.99	0.25	0.73	0.96	0.642	1.05	0.609	1.05	1.30	0.768	No
245	16.10	0.99	0.25	0.74	0.96	0.643	1.05	0.610	1.05	1.30	0.775	No
246	16.16	0.99	0.25	0.74	0.96	0.643	1.05	0.610	1.04	1.30	0.783	No
247	16.23	1.00	0.26	0.74	0.96	0.644	1.05	0.611	1.04	1.30	0.789	No
248	16.30	1.00	0.26	0.74	0.96	0.645	1.05	0.612	1.04	1.30	0.792	No
249	16.36	1.01	0.26	0.74	0.96	0.646	1.05	0.612	1.04	1.30	0.795	No
250	16.43	1.01	0.26	0.75	0.95	0.646	1.05	0.613	1.04	1.30	0.797	No
251	16.50	1.01	0.27	0.75	0.95	0.647	1.05	0.614	1.04	1.30	0.798	No
252	16.56	1.02	0.27	0.75	0.95	0.648	1.05	0.614	1.04	1.30	0.800	No
253	16.63	1.02	0.27	0.75	0.95	0.648	1.05	0.615	1.04	1.30	0.800	No
254	16.70	1.03	0.27	0.75	0.95	0.649	1.05	0.616	1.04	1.30	0.801	No
255	16.73	1.03	0.27	0.76	0.95	0.649	1.05	0.616	1.04	1.30	0.801	No
256	16.80	1.03	0.27	0.76	0.95	0.650	1.05	0.617	1.04	1.30	0.801	No
257	16.87	1.04	0.28	0.76	0.95	0.651	1.05	0.617	1.04	1.30	0.801	No
258	16.94	1.04	0.28	0.76	0.95	0.651	1.05	0.618	1.04	1.30	0.800	No
259	17.00	1.05	0.28	0.76	0.95	0.652	1.05	0.618	1.04	1.30	0.796	No
260	17.08	1.05	0.28	0.77	0.95	0.653	1.05	0.619	1.04	1.30	0.792	No
261	17.14	1.05	0.29	0.77	0.95	0.653	1.05	0.620	1.04	1.30	0.789	No
262	17.20	1.06	0.29	0.77	0.95	0.654	1.05	0.620	1.05	1.30	0.784	No
263	17.27	1.06	0.29	0.77	0.95	0.655	1.05	0.621	1.05	1.30	0.779	No
264	17.34	1.07	0.29	0.78	0.95	0.655	1.05	0.621	1.05	1.30	0.775	No
265	17.40	1.07	0.29	0.78	0.95	0.656	1.05	0.622	1.05	1.30	0.772	No
266	17.47	1.07	0.30	0.78	0.95	0.656	1.05	0.622	1.05	1.30	0.770	No
267	17.53	1.08	0.30	0.78	0.95	0.657	1.05	0.623	1.05	1.30	0.768	No
268	17.60	1.08	0.30	0.78	0.95	0.657	1.05	0.623	1.05	1.30	0.766	No
269	17.67	1.09	0.30	0.79	0.95	0.658	1.05	0.624	1.06	1.30	0.765	No
270	17.73	1.09	0.30	0.79	0.95	0.658	1.05	0.625	1.06	1.30	0.765	No
271	17.80	1.10	0.31	0.79	0.95	0.659	1.05	0.625	1.05	1.30	0.765	No
272	17.87	1.10	0.31	0.79	0.95	0.660	1.05	0.626	1.05	1.30	0.766	No
273	17.93	1.11	0.31	0.80	0.95	0.660	1.05	0.626	1.05	1.30	0.768	No
274	18.00	1.11	0.31	0.80	0.95	0.661	1.05	0.627	1.05	1.30	0.771	No
275	18.07	1.11	0.31	0.80	0.95	0.661	1.05	0.627	1.05	1.30	0.775	No
276	18.14	1.12	0.32	0.80	0.95	0.662	1.05	0.628	1.05	1.30	0.780	No
277	18.20	1.12	0.32	0.80	0.95	0.662	1.05	0.628	1.05	1.30	0.786	No
278	18.27	1.13	0.32	0.81	0.95	0.663	1.05	0.629	1.04	1.30	0.793	No
279	18.34	1.13	0.32	0.81	0.95	0.663	1.05	0.629	1.04	1.30	0.800	No
280	18.37	1.13	0.32	0.81	0.95	0.664	1.05	0.629	1.04	1.30	0.803	No
281	18.44	1.14	0.33	0.81	0.95	0.664	1.05	0.630	1.04	1.30	0.809	No
282	18.51	1.14	0.33	0.81	0.95	0.665	1.05	0.630	1.03	1.30	0.815	No
283	18.57	1.15	0.33	0.82	0.95	0.665	1.05	0.631	1.03	1.30	0.822	No
284	18.64	1.15	0.33	0.82	0.95	0.666	1.05	0.631	1.03	1.30	0.826	No
285	18.71	1.15	0.33	0.82	0.95	0.666	1.05	0.632	1.03	1.30	0.829	No
286	18.78	1.16	0.34	0.82	0.95	0.667	1.05	0.632	1.03	1.30	0.831	No
287	18.84	1.16	0.34	0.82	0.95	0.667	1.05	0.633	1.03	1.30	0.833	No
288	18.91	1.17	0.34	0.83	0.95	0.668	1.05	0.633	1.02	1.30	0.836	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	18.98	1.17	0.34	0.83	0.94	0.668	1.05	0.634	1.02	1.30	0.838	No
290	19.04	1.18	0.34	0.83	0.94	0.669	1.05	0.634	1.02	1.30	0.839	No
291	19.11	1.18	0.35	0.83	0.94	0.669	1.05	0.635	1.02	1.30	0.841	No
292	19.18	1.18	0.35	0.83	0.94	0.670	1.05	0.635	1.02	1.30	0.842	No
293	19.24	1.19	0.35	0.84	0.94	0.670	1.05	0.636	1.02	1.30	0.844	No
294	19.31	1.19	0.35	0.84	0.94	0.671	1.05	0.636	1.02	1.30	0.845	No
295	19.38	1.19	0.35	0.84	0.94	0.672	1.05	0.637	1.02	1.30	0.846	No
296	19.44	1.20	0.36	0.84	0.94	0.672	1.05	0.637	1.02	1.30	0.846	No
297	19.51	1.20	0.36	0.84	0.94	0.673	1.05	0.638	1.02	1.30	0.847	No
298	19.58	1.21	0.36	0.85	0.94	0.673	1.05	0.638	1.02	1.30	0.847	No
299	19.63	1.21	0.36	0.85	0.94	0.674	1.05	0.639	1.02	1.30	0.847	No
300	19.69	1.21	0.36	0.85	0.94	0.674	1.05	0.639	1.02	1.30	0.845	No
301	19.76	1.22	0.37	0.85	0.94	0.675	1.05	0.640	1.02	1.30	0.844	No
302	19.82	1.22	0.37	0.85	0.94	0.675	1.05	0.640	1.02	1.30	0.845	No
303	19.89	1.23	0.37	0.85	0.94	0.676	1.05	0.641	1.02	1.30	0.846	No
304	19.95	1.23	0.37	0.86	0.94	0.676	1.05	0.641	1.02	1.30	0.847	No
305	20.02	1.23	0.37	0.86	0.94	0.676	1.05	0.642	1.02	1.30	0.851	No
306	20.09	1.24	0.38	0.86	0.94	0.677	1.05	0.642	1.02	1.30	0.851	No
307	20.16	1.24	0.38	0.86	0.94	0.677	1.05	0.643	1.02	1.30	0.853	No
308	20.23	1.25	0.38	0.86	0.94	0.678	1.05	0.643	1.02	1.30	0.854	No
309	20.29	1.25	0.38	0.87	0.94	0.678	1.05	0.643	1.02	1.30	0.855	No
310	20.36	1.25	0.39	0.87	0.94	0.679	1.05	0.644	1.02	1.30	0.855	No
311	20.42	1.26	0.39	0.87	0.94	0.679	1.05	0.644	1.02	1.30	0.856	No
312	20.49	1.26	0.39	0.87	0.94	0.680	1.05	0.645	1.02	1.30	0.856	No
313	20.56	1.27	0.39	0.87	0.94	0.680	1.05	0.645	1.02	1.30	0.856	No
314	20.63	1.27	0.39	0.88	0.94	0.681	1.05	0.646	1.02	1.30	0.856	No
315	20.69	1.27	0.40	0.88	0.94	0.681	1.05	0.646	1.02	1.30	0.855	No
316	20.76	1.28	0.40	0.88	0.94	0.682	1.05	0.646	1.02	1.30	0.854	No
317	20.83	1.28	0.40	0.88	0.94	0.682	1.05	0.647	1.02	1.30	0.854	No
318	20.89	1.29	0.40	0.88	0.94	0.682	1.05	0.647	1.02	1.30	0.854	No
319	20.96	1.29	0.40	0.89	0.94	0.683	1.05	0.648	1.02	1.30	0.855	No
320	21.03	1.29	0.41	0.89	0.94	0.683	1.05	0.648	1.02	1.30	0.857	No
321	21.09	1.30	0.41	0.89	0.94	0.684	1.05	0.648	1.02	1.30	0.859	No
322	21.16	1.30	0.41	0.89	0.94	0.684	1.05	0.649	1.02	1.30	0.862	No
323	21.23	1.31	0.41	0.89	0.94	0.684	1.05	0.649	1.02	1.30	0.863	No
324	21.26	1.31	0.41	0.89	0.94	0.685	1.05	0.649	1.02	1.30	0.864	No
325	21.33	1.31	0.42	0.90	0.93	0.685	1.05	0.650	1.02	1.30	0.865	No
326	21.40	1.32	0.42	0.90	0.93	0.686	1.05	0.650	1.02	1.30	0.866	No
327	21.46	1.32	0.42	0.90	0.93	0.686	1.05	0.651	1.02	1.30	0.867	No
328	21.53	1.32	0.42	0.90	0.93	0.686	1.05	0.651	1.01	1.30	0.869	No
329	21.60	1.33	0.42	0.90	0.93	0.687	1.05	0.651	1.02	1.30	0.868	No
330	21.66	1.33	0.43	0.91	0.93	0.687	1.05	0.652	1.01	1.30	0.868	No
331	21.73	1.34	0.43	0.91	0.93	0.688	1.05	0.652	1.01	1.30	0.869	No
332	21.80	1.34	0.43	0.91	0.93	0.688	1.05	0.652	1.01	1.30	0.869	No
333	21.86	1.34	0.43	0.91	0.93	0.688	1.05	0.653	1.01	1.30	0.869	No
334	21.93	1.35	0.43	0.91	0.93	0.689	1.05	0.653	1.01	1.30	0.869	No
335	22.00	1.35	0.44	0.92	0.93	0.689	1.05	0.653	1.01	1.30	0.869	No
336	22.06	1.36	0.44	0.92	0.93	0.689	1.05	0.654	1.01	1.30	0.869	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	22.13	1.36	0.44	0.92	0.93	0.690	1.05	0.654	1.01	1.30	0.869	No
338	22.19	1.36	0.44	0.92	0.93	0.690	1.05	0.654	1.01	1.30	0.868	No
339	22.26	1.37	0.44	0.92	0.93	0.690	1.05	0.655	1.02	1.30	0.867	No
340	22.33	1.37	0.45	0.93	0.93	0.691	1.05	0.655	1.02	1.30	0.866	No
341	22.40	1.38	0.45	0.93	0.93	0.691	1.05	0.655	1.02	1.30	0.866	No
342	22.46	1.38	0.45	0.93	0.93	0.691	1.05	0.656	1.02	1.30	0.866	No
343	22.53	1.39	0.45	0.93	0.93	0.692	1.05	0.656	1.02	1.30	0.865	No
344	22.60	1.39	0.46	0.93	0.93	0.692	1.05	0.656	1.02	1.30	0.864	No
345	22.66	1.39	0.46	0.94	0.93	0.692	1.05	0.656	1.02	1.30	0.864	No
346	22.73	1.40	0.46	0.94	0.93	0.692	1.05	0.657	1.02	1.30	0.864	No
347	22.80	1.40	0.46	0.94	0.93	0.693	1.05	0.657	1.02	1.30	0.863	No
348	22.86	1.41	0.46	0.94	0.93	0.693	1.05	0.657	1.02	1.30	0.860	No
349	22.93	1.41	0.47	0.95	0.93	0.693	1.05	0.658	1.02	1.30	0.857	No
350	23.00	1.42	0.47	0.95	0.93	0.694	1.05	0.658	1.02	1.30	0.857	No
351	23.03	1.42	0.47	0.95	0.93	0.694	1.05	0.658	1.02	1.30	0.858	No
352	23.10	1.42	0.47	0.95	0.93	0.694	1.05	0.658	1.02	1.30	0.859	No
353	23.17	1.43	0.47	0.95	0.93	0.694	1.05	0.659	1.01	1.30	0.859	No
354	23.24	1.43	0.48	0.96	0.93	0.695	1.05	0.659	1.01	1.30	0.858	No
355	23.30	1.43	0.48	0.96	0.93	0.695	1.05	0.659	1.01	1.30	0.857	No
356	23.37	1.44	0.48	0.96	0.93	0.695	1.05	0.659	1.01	1.30	0.859	No
357	23.43	1.44	0.48	0.96	0.93	0.696	1.05	0.660	1.02	1.30	0.853	No
358	23.50	1.45	0.48	0.96	0.93	0.696	1.05	0.660	1.02	1.30	0.852	No
359	23.56	1.45	0.49	0.97	0.93	0.696	1.05	0.660	1.01	1.30	0.853	No
360	23.63	1.46	0.49	0.97	0.92	0.696	1.05	0.660	1.01	1.30	0.854	No
361	23.70	1.46	0.49	0.97	0.92	0.697	1.05	0.661	1.01	1.30	0.853	No
362	23.76	1.46	0.49	0.97	0.92	0.697	1.05	0.661	1.01	1.30	0.851	No
363	23.83	1.47	0.49	0.97	0.92	0.697	1.05	0.661	1.01	1.30	0.848	No
364	23.90	1.47	0.50	0.98	0.92	0.697	1.05	0.661	1.01	1.30	0.848	No
365	23.96	1.48	0.50	0.98	0.92	0.697	1.05	0.661	1.01	1.30	0.850	No
366	24.03	1.48	0.50	0.98	0.92	0.698	1.05	0.662	1.01	1.30	0.853	No
367	24.10	1.49	0.50	0.98	0.92	0.698	1.05	0.662	1.01	1.30	0.858	No
368	24.17	1.49	0.50	0.99	0.92	0.698	1.05	0.662	1.01	1.30	0.865	No
369	24.23	1.49	0.51	0.99	0.92	0.698	1.05	0.662	1.01	1.30	0.871	No
370	24.30	1.50	0.51	0.99	0.92	0.699	1.05	0.663	1.01	1.30	0.878	No
371	24.37	1.50	0.51	0.99	0.92	0.699	1.05	0.663	1.01	1.30	0.883	No
372	24.43	1.51	0.51	0.99	0.92	0.699	1.05	0.663	1.01	1.30	0.888	No
373	24.50	1.51	0.51	1.00	0.92	0.699	1.05	0.663	1.01	1.30	0.891	No
374	24.57	1.51	0.52	1.00	0.92	0.700	1.05	0.664	1.01	1.30	0.893	No
375	24.63	1.52	0.52	1.00	0.92	0.700	1.05	0.664	1.01	1.30	0.894	No
376	24.70	1.52	0.52	1.00	0.92	0.700	1.05	0.664	1.01	1.30	0.895	No
377	24.77	1.53	0.52	1.00	0.92	0.701	1.05	0.664	1.00	1.30	0.896	No
378	24.84	1.53	0.53	1.01	0.92	0.701	1.05	0.665	1.00	1.30	0.896	No
379	24.87	1.53	0.53	1.01	0.92	0.701	1.05	0.665	1.00	1.30	0.895	No
380	24.94	1.54	0.53	1.01	0.92	0.701	1.05	0.665	1.00	1.30	0.894	No
381	25.01	1.54	0.53	1.01	0.92	0.701	1.05	0.665	1.01	1.30	0.891	No
382	25.07	1.54	0.53	1.01	0.92	0.702	1.05	0.666	1.01	1.30	0.886	No
383	25.14	1.55	0.53	1.01	0.92	0.702	1.05	0.666	1.01	1.30	0.883	No
384	25.21	1.55	0.54	1.02	0.92	0.702	1.05	0.666	1.01	1.30	0.878	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	25.28	1.56	0.54	1.02	0.92	0.702	1.05	0.666	1.01	1.30	0.872	No
386	25.34	1.56	0.54	1.02	0.92	0.702	1.05	0.666	1.01	1.30	0.866	No
387	25.41	1.57	0.54	1.02	0.92	0.703	1.05	0.666	1.01	1.30	0.861	No
388	25.48	1.57	0.55	1.03	0.92	0.703	1.05	0.667	1.01	1.30	0.860	No
389	25.54	1.57	0.55	1.03	0.92	0.703	1.05	0.667	1.00	1.30	0.865	No
390	25.61	1.58	0.55	1.03	0.92	0.703	1.05	0.667	1.00	1.30	0.869	No
391	25.68	1.58	0.55	1.03	0.92	0.703	1.05	0.667	1.00	1.30	0.873	No
392	25.75	1.59	0.55	1.03	0.92	0.704	1.05	0.667	1.00	1.30	0.878	No
393	25.81	1.59	0.56	1.04	0.92	0.704	1.05	0.667	1.00	1.30	0.883	No
394	25.87	1.60	0.56	1.04	0.91	0.704	1.05	0.668	1.00	1.30	0.891	No
395	25.93	1.60	0.56	1.04	0.91	0.704	1.05	0.668	1.00	1.30	0.892	No
396	26.00	1.60	0.56	1.04	0.91	0.704	1.05	0.668	1.00	1.30	0.897	No
397	26.06	1.61	0.56	1.04	0.91	0.704	1.05	0.668	1.00	1.30	0.899	No
398	26.13	1.61	0.57	1.05	0.91	0.705	1.05	0.668	1.00	1.30	0.901	No
399	26.20	1.62	0.57	1.05	0.91	0.705	1.05	0.668	1.00	1.30	0.902	No
400	26.27	1.62	0.57	1.05	0.91	0.705	1.05	0.669	1.00	1.30	0.903	No
401	26.33	1.62	0.57	1.05	0.91	0.705	1.05	0.669	1.00	1.30	0.903	No
402	26.40	1.63	0.57	1.05	0.91	0.705	1.05	0.669	1.00	1.30	0.904	No
403	26.47	1.63	0.58	1.06	0.91	0.706	1.05	0.669	1.00	1.30	0.905	No
404	26.53	1.64	0.58	1.06	0.91	0.706	1.05	0.669	1.00	1.30	0.906	No
405	26.60	1.64	0.58	1.06	0.91	0.706	1.05	0.670	1.00	1.30	0.906	No
406	26.66	1.64	0.58	1.06	0.91	0.706	1.05	0.670	1.00	1.30	0.907	No
407	26.73	1.65	0.58	1.06	0.91	0.706	1.05	0.670	1.00	1.30	0.907	No
408	26.80	1.65	0.59	1.07	0.91	0.707	1.05	0.670	1.00	1.30	0.907	No
409	26.86	1.66	0.59	1.07	0.91	0.707	1.05	0.670	1.00	1.30	0.908	No
410	26.93	1.66	0.59	1.07	0.91	0.707	1.05	0.670	1.00	1.30	0.907	No
411	27.00	1.66	0.59	1.07	0.91	0.707	1.05	0.671	1.00	1.30	0.905	No
412	27.06	1.67	0.59	1.07	0.91	0.707	1.05	0.671	1.00	1.30	0.902	No
413	27.13	1.67	0.60	1.08	0.91	0.707	1.05	0.671	1.00	1.30	0.899	No
414	27.17	1.68	0.60	1.08	0.91	0.708	1.05	0.671	1.00	1.30	0.899	No
415	27.23	1.68	0.60	1.08	0.91	0.708	1.05	0.671	1.00	1.30	0.899	No
416	27.30	1.68	0.60	1.08	0.91	0.708	1.05	0.671	1.00	1.30	0.900	No
417	27.37	1.69	0.60	1.08	0.91	0.708	1.05	0.671	1.00	1.30	0.903	No
418	27.43	1.69	0.61	1.09	0.91	0.708	1.05	0.672	1.00	1.30	0.905	No
419	27.50	1.70	0.61	1.09	0.91	0.708	1.05	0.672	1.00	1.30	0.907	No
420	27.57	1.70	0.61	1.09	0.91	0.708	1.05	0.672	1.00	1.30	0.909	No
421	27.64	1.70	0.61	1.09	0.91	0.709	1.05	0.672	1.00	1.30	0.909	No
422	27.70	1.71	0.61	1.09	0.91	0.709	1.05	0.672	1.00	1.30	0.910	No
423	27.77	1.71	0.62	1.10	0.91	0.709	1.05	0.672	1.00	1.30	0.910	No
424	27.84	1.72	0.62	1.10	0.91	0.709	1.05	0.672	1.00	1.30	0.910	No
425	27.91	1.72	0.62	1.10	0.91	0.709	1.05	0.673	1.00	1.30	0.909	No
426	27.98	1.73	0.62	1.10	0.91	0.709	1.05	0.673	1.00	1.30	0.907	No
427	28.04	1.73	0.63	1.10	0.91	0.709	1.05	0.673	0.99	1.30	0.906	No
428	28.09	1.73	0.63	1.11	0.90	0.710	1.05	0.673	0.99	1.30	0.906	No
429	28.16	1.74	0.63	1.11	0.90	0.710	1.05	0.673	0.99	1.30	0.902	No
430	28.22	1.74	0.63	1.11	0.90	0.710	1.05	0.673	0.99	1.30	0.900	No
431	28.28	1.74	0.63	1.11	0.90	0.710	1.05	0.673	0.99	1.30	0.899	No
432	28.35	1.75	0.63	1.11	0.90	0.710	1.05	0.673	0.99	1.30	0.898	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	28.42	1.75	0.64	1.12	0.90	0.710	1.05	0.673	0.99	1.30	0.897	No
434	28.49	1.76	0.64	1.12	0.90	0.710	1.05	0.674	0.99	1.30	0.896	No
435	28.55	1.76	0.64	1.12	0.90	0.710	1.05	0.674	0.99	1.30	0.896	No
436	28.62	1.77	0.64	1.12	0.90	0.710	1.05	0.674	0.99	1.30	0.894	No
437	28.69	1.77	0.65	1.12	0.90	0.711	1.05	0.674	0.99	1.30	0.893	No
438	28.75	1.77	0.65	1.13	0.90	0.711	1.05	0.674	0.99	1.30	0.892	No
439	28.82	1.78	0.65	1.13	0.90	0.711	1.05	0.674	0.99	1.30	0.891	No
440	28.89	1.78	0.65	1.13	0.90	0.711	1.05	0.674	0.99	1.30	0.890	No
441	28.95	1.79	0.65	1.13	0.90	0.711	1.05	0.674	0.99	1.30	0.890	No
442	29.02	1.79	0.66	1.14	0.90	0.711	1.05	0.674	0.99	1.30	0.890	No
443	29.09	1.80	0.66	1.14	0.90	0.711	1.05	0.674	0.99	1.30	0.890	No
444	29.16	1.80	0.66	1.14	0.90	0.711	1.05	0.674	0.99	1.30	0.891	No
445	29.22	1.80	0.66	1.14	0.90	0.711	1.05	0.675	0.99	1.30	0.894	No
446	29.29	1.81	0.66	1.14	0.90	0.711	1.05	0.675	0.99	1.30	0.897	No
447	29.35	1.81	0.67	1.15	0.90	0.711	1.05	0.675	0.99	1.30	0.900	No
448	29.42	1.82	0.67	1.15	0.90	0.711	1.05	0.675	0.99	1.30	0.904	No
449	29.49	1.82	0.67	1.15	0.90	0.712	1.05	0.675	0.99	1.30	0.907	No
450	29.55	1.83	0.67	1.15	0.90	0.712	1.05	0.675	0.99	1.30	0.911	No
451	29.62	1.83	0.67	1.16	0.90	0.712	1.05	0.675	0.99	1.30	0.915	No
452	29.69	1.83	0.68	1.16	0.90	0.712	1.05	0.675	0.99	1.30	0.918	No
453	29.76	1.84	0.68	1.16	0.90	0.712	1.05	0.675	0.99	1.30	0.920	No
454	29.82	1.84	0.68	1.16	0.90	0.712	1.05	0.675	0.99	1.30	0.922	No
455	29.86	1.84	0.68	1.16	0.90	0.712	1.05	0.675	0.99	1.30	0.922	No
456	29.92	1.85	0.68	1.16	0.90	0.712	1.05	0.675	0.99	1.30	0.923	No
457	30.00	1.85	0.69	1.17	0.90	0.712	1.05	0.676	0.99	1.30	0.924	No
458	30.06	1.86	0.69	1.17	0.90	0.712	1.05	0.676	0.99	1.30	0.924	No
459	30.13	1.86	0.69	1.17	0.90	0.713	1.05	0.676	0.99	1.30	0.925	No
460	30.20	1.86	0.69	1.17	0.89	0.713	1.05	0.676	0.99	1.30	0.925	No
461	30.27	1.87	0.69	1.17	0.89	0.713	1.05	0.676	0.99	1.30	0.925	No
462	30.34	1.87	0.70	1.18	0.89	0.713	1.05	0.676	0.99	1.30	0.926	No
463	30.40	1.88	0.70	1.18	0.89	0.713	1.05	0.676	0.99	1.30	0.926	No
464	30.47	1.88	0.70	1.18	0.89	0.713	1.05	0.676	0.99	1.30	0.926	No
465	30.54	1.88	0.70	1.18	0.89	0.713	1.05	0.677	0.99	1.30	0.927	No
466	30.61	1.89	0.71	1.18	0.89	0.714	1.05	0.677	0.99	1.30	0.927	No
467	30.67	1.89	0.71	1.18	0.89	0.714	1.05	0.677	0.99	1.30	0.927	No
468	30.74	1.90	0.71	1.19	0.89	0.714	1.05	0.677	0.99	1.30	0.928	No
469	30.81	1.90	0.71	1.19	0.89	0.714	1.05	0.677	0.99	1.30	0.928	No
470	30.87	1.90	0.71	1.19	0.89	0.714	1.05	0.677	0.99	1.30	0.928	No
471	30.91	1.91	0.71	1.19	0.89	0.714	1.05	0.677	0.99	1.30	0.928	No
472	30.97	1.91	0.72	1.19	0.89	0.714	1.05	0.677	0.99	1.30	0.929	No
473	31.04	1.91	0.72	1.19	0.89	0.714	1.05	0.678	0.99	1.30	0.929	No
474	31.11	1.92	0.72	1.20	0.89	0.715	1.05	0.678	0.99	1.30	0.929	No
475	31.17	1.92	0.72	1.20	0.89	0.715	1.05	0.678	0.99	1.30	0.929	No
476	31.24	1.92	0.73	1.20	0.89	0.715	1.05	0.678	0.99	1.30	0.929	No
477	31.31	1.93	0.73	1.20	0.89	0.715	1.05	0.678	0.99	1.30	0.930	No
478	31.38	1.93	0.73	1.20	0.89	0.715	1.05	0.678	0.99	1.30	0.930	No
479	31.44	1.94	0.73	1.20	0.89	0.715	1.05	0.678	0.99	1.30	0.930	No
480	31.51	1.94	0.73	1.21	0.89	0.715	1.05	0.678	0.99	1.30	0.931	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	31.57	1.94	0.74	1.21	0.89	0.715	1.05	0.678	0.99	1.30	0.931	No
482	31.64	1.95	0.74	1.21	0.89	0.715	1.05	0.678	0.99	1.30	0.931	No
483	31.71	1.95	0.74	1.21	0.89	0.715	1.05	0.679	0.99	1.30	0.931	No
484	31.77	1.96	0.74	1.21	0.89	0.716	1.05	0.679	0.99	1.30	0.932	No
485	31.84	1.96	0.74	1.22	0.89	0.716	1.05	0.679	0.99	1.30	0.932	No
486	31.91	1.96	0.75	1.22	0.89	0.716	1.05	0.679	0.99	1.30	0.932	No
487	31.97	1.97	0.75	1.22	0.89	0.716	1.05	0.679	0.99	1.30	0.932	No
488	32.04	1.97	0.75	1.22	0.89	0.716	1.05	0.679	0.99	1.30	0.932	No
489	32.11	1.98	0.75	1.22	0.89	0.716	1.05	0.679	0.99	1.30	0.932	No
490	32.18	1.98	0.75	1.23	0.89	0.716	1.05	0.679	0.99	1.30	0.933	No
491	32.24	1.98	0.76	1.23	0.89	0.716	1.05	0.679	0.99	1.30	0.933	No
492	32.31	1.99	0.76	1.23	0.88	0.716	1.05	0.679	0.99	1.30	0.933	No
493	32.36	1.99	0.76	1.23	0.88	0.716	1.05	0.679	0.99	1.30	0.933	No
494	32.43	1.99	0.76	1.23	0.88	0.716	1.05	0.679	0.99	1.30	0.934	No
495	32.49	2.00	0.76	1.23	0.88	0.716	1.05	0.679	0.99	1.30	0.934	No
496	32.56	2.00	0.77	1.24	0.88	0.716	1.05	0.679	0.99	1.30	0.934	No
497	32.62	2.01	0.77	1.24	0.88	0.716	1.05	0.679	0.99	1.30	0.934	No
498	32.70	2.01	0.77	1.24	0.88	0.716	1.05	0.680	0.99	1.30	0.934	No
499	32.75	2.01	0.77	1.24	0.88	0.717	1.05	0.680	0.99	1.30	0.934	No
500	32.83	2.02	0.77	1.24	0.88	0.717	1.05	0.680	0.99	1.30	0.935	No
501	32.88	2.02	0.78	1.25	0.88	0.717	1.05	0.680	0.99	1.30	0.935	No
502	32.96	2.03	0.78	1.25	0.88	0.717	1.05	0.680	0.99	1.30	0.935	No
503	33.01	2.03	0.78	1.25	0.88	0.717	1.05	0.680	0.99	1.30	0.935	No
504	33.08	2.03	0.78	1.25	0.88	0.717	1.05	0.680	0.99	1.30	0.935	No
505	33.16	2.04	0.78	1.25	0.88	0.717	1.05	0.680	0.98	1.30	0.935	No
506	33.22	2.04	0.79	1.26	0.88	0.717	1.05	0.680	0.98	1.30	0.935	No
507	33.29	2.05	0.79	1.26	0.88	0.717	1.05	0.680	0.98	1.30	0.935	No
508	33.34	2.05	0.79	1.26	0.88	0.717	1.05	0.680	0.98	1.30	0.936	No
509	33.40	2.05	0.79	1.26	0.88	0.717	1.05	0.680	0.98	1.30	0.936	No
510	33.47	2.06	0.79	1.26	0.88	0.717	1.05	0.680	0.98	1.30	0.936	No
511	33.56	2.06	0.80	1.27	0.88	0.717	1.05	0.680	0.98	1.30	0.936	No
512	33.62	2.07	0.80	1.27	0.88	0.717	1.05	0.680	0.98	1.30	0.936	No
513	33.68	2.07	0.80	1.27	0.88	0.717	1.05	0.680	0.98	1.30	0.937	No
514	33.73	2.07	0.80	1.27	0.88	0.717	1.05	0.680	0.98	1.30	0.937	No
515	33.82	2.08	0.81	1.27	0.88	0.717	1.05	0.680	0.98	1.30	0.937	No
516	33.89	2.08	0.81	1.28	0.88	0.717	1.05	0.680	0.98	1.30	0.938	No
517	33.95	2.09	0.81	1.28	0.88	0.717	1.05	0.680	0.98	1.30	0.938	No
518	34.02	2.09	0.81	1.28	0.88	0.717	1.05	0.680	0.98	1.30	0.938	No
519	34.09	2.09	0.81	1.28	0.88	0.717	1.05	0.680	0.98	1.30	0.938	No
520	34.15	2.10	0.82	1.28	0.88	0.717	1.05	0.680	0.98	1.30	0.938	No
521	34.22	2.10	0.82	1.28	0.88	0.717	1.05	0.680	0.98	1.30	0.939	No
522	34.25	2.10	0.82	1.29	0.88	0.717	1.05	0.680	0.98	1.30	0.939	No
523	34.32	2.11	0.82	1.29	0.88	0.717	1.05	0.680	0.98	1.30	0.939	No
524	34.39	2.11	0.82	1.29	0.87	0.718	1.05	0.680	0.98	1.30	0.939	No
525	34.45	2.12	0.83	1.29	0.87	0.718	1.05	0.681	0.98	1.30	0.939	No
526	34.52	2.12	0.83	1.29	0.87	0.718	1.05	0.681	0.98	1.30	0.939	No
527	34.59	2.12	0.83	1.29	0.87	0.718	1.05	0.681	0.98	1.30	0.940	No
528	34.65	2.13	0.83	1.30	0.87	0.718	1.05	0.681	0.98	1.30	0.940	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
529	34.72	2.13	0.83	1.30	0.87	0.718	1.05	0.681	0.98	1.30	0.940	No
530	34.79	2.14	0.84	1.30	0.87	0.718	1.05	0.681	0.98	1.30	0.940	No
531	34.85	2.14	0.84	1.30	0.87	0.718	1.05	0.681	0.98	1.30	0.940	No
532	34.92	2.14	0.84	1.30	0.87	0.718	1.05	0.681	0.98	1.30	0.940	No
533	34.99	2.15	0.84	1.31	0.87	0.718	1.05	0.681	0.98	1.30	0.941	No
534	35.05	2.15	0.84	1.31	0.87	0.718	1.05	0.681	0.98	1.30	0.941	No
535	35.13	2.16	0.85	1.31	0.87	0.718	1.05	0.681	0.98	1.30	0.941	No
536	35.19	2.16	0.85	1.31	0.87	0.718	1.05	0.681	0.98	1.30	0.941	No
537	35.27	2.16	0.85	1.31	0.87	0.718	1.05	0.681	0.98	1.30	0.941	No
538	35.34	2.17	0.85	1.31	0.87	0.718	1.05	0.681	0.98	1.30	0.941	No
539	35.37	2.17	0.85	1.32	0.87	0.718	1.05	0.681	0.98	1.30	0.941	No
540	35.44	2.17	0.86	1.32	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
541	35.51	2.18	0.86	1.32	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
542	35.57	2.18	0.86	1.32	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
543	35.64	2.19	0.86	1.32	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
544	35.70	2.19	0.86	1.33	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
545	35.77	2.19	0.87	1.33	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
546	35.84	2.20	0.87	1.33	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
547	35.90	2.20	0.87	1.33	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
548	35.97	2.21	0.87	1.33	0.87	0.718	1.05	0.681	0.98	1.30	0.942	No
549	36.03	2.21	0.87	1.34	0.87	0.718	1.05	0.681	0.98	1.30	0.943	No
550	36.10	2.21	0.88	1.34	0.87	0.718	1.05	0.681	0.98	1.30	0.943	No
551	36.17	2.22	0.88	1.34	0.87	0.718	1.05	0.681	0.98	1.30	0.943	No
552	36.24	2.22	0.88	1.34	0.87	0.718	1.05	0.681	0.98	1.30	0.943	No
553	36.30	2.23	0.88	1.34	0.87	0.718	1.05	0.681	0.98	1.30	0.943	No
554	36.37	2.23	0.89	1.34	0.87	0.718	1.05	0.681	0.98	1.30	0.943	No
555	36.44	2.23	0.89	1.35	0.86	0.718	1.05	0.681	0.98	1.30	0.943	No
556	36.51	2.24	0.89	1.35	0.86	0.718	1.05	0.681	0.98	1.30	0.942	No
557	36.57	2.24	0.89	1.35	0.86	0.718	1.05	0.681	0.97	1.30	0.942	No
558	36.64	2.25	0.89	1.35	0.86	0.718	1.05	0.681	0.97	1.30	0.942	No
559	36.71	2.25	0.90	1.35	0.86	0.718	1.05	0.681	0.97	1.30	0.942	No
560	36.77	2.25	0.90	1.36	0.86	0.718	1.05	0.681	0.98	1.30	0.943	No
561	36.84	2.26	0.90	1.36	0.86	0.718	1.05	0.681	0.98	1.30	0.943	No
562	36.91	2.26	0.90	1.36	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
563	36.98	2.27	0.90	1.36	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
564	37.01	2.27	0.91	1.36	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
565	37.08	2.27	0.91	1.37	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
566	37.15	2.28	0.91	1.37	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
567	37.21	2.28	0.91	1.37	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
568	37.28	2.29	0.91	1.37	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
569	37.34	2.29	0.92	1.37	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
570	37.41	2.29	0.92	1.38	0.86	0.718	1.05	0.681	0.98	1.30	0.944	No
571	37.48	2.30	0.92	1.38	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
572	37.55	2.30	0.92	1.38	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
573	37.61	2.30	0.92	1.38	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
574	37.68	2.31	0.93	1.38	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
575	37.75	2.31	0.93	1.38	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
576	37.81	2.32	0.93	1.39	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
577	37.88	2.32	0.93	1.39	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
578	37.95	2.32	0.93	1.39	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
579	38.02	2.33	0.94	1.39	0.86	0.718	1.05	0.681	0.98	1.30	0.945	No
580	38.08	2.33	0.94	1.39	0.86	0.718	1.05	0.681	0.98	1.30	0.946	No
581	38.15	2.34	0.94	1.40	0.86	0.718	1.05	0.681	0.98	1.30	0.946	No
582	38.21	2.34	0.94	1.40	0.86	0.718	1.05	0.681	0.97	1.30	0.946	No
583	38.28	2.34	0.94	1.40	0.86	0.718	1.05	0.680	0.97	1.30	0.946	No
584	38.35	2.35	0.95	1.40	0.86	0.717	1.05	0.680	0.97	1.30	0.945	No
585	38.41	2.35	0.95	1.40	0.86	0.717	1.05	0.680	0.97	1.30	0.945	No
586	38.48	2.36	0.95	1.41	0.85	0.717	1.05	0.680	0.97	1.30	0.945	No
587	38.55	2.36	0.95	1.41	0.85	0.717	1.05	0.680	0.97	1.30	0.945	No
588	38.58	2.36	0.95	1.41	0.85	0.717	1.05	0.680	0.97	1.30	0.945	No
589	38.65	2.37	0.96	1.41	0.85	0.717	1.05	0.680	0.97	1.30	0.945	No
590	38.72	2.37	0.96	1.41	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
591	38.78	2.38	0.96	1.42	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
592	38.85	2.38	0.96	1.42	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
593	38.92	2.38	0.96	1.42	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
594	38.98	2.39	0.97	1.42	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
595	39.05	2.39	0.97	1.42	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
596	39.12	2.40	0.97	1.43	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
597	39.18	2.40	0.97	1.43	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
598	39.25	2.40	0.97	1.43	0.85	0.717	1.05	0.680	0.97	1.30	0.946	No
599	39.32	2.41	0.98	1.43	0.85	0.716	1.05	0.680	0.97	1.30	0.946	No
600	39.38	2.41	0.98	1.43	0.85	0.716	1.05	0.679	0.97	1.30	0.946	No
601	39.45	2.42	0.98	1.43	0.85	0.716	1.05	0.679	0.97	1.30	0.946	No
602	39.52	2.42	0.98	1.44	0.85	0.716	1.05	0.679	0.97	1.30	0.946	No
603	39.58	2.42	0.99	1.44	0.85	0.716	1.05	0.679	0.97	1.30	0.946	No
604	39.65	2.43	0.99	1.44	0.85	0.716	1.05	0.679	0.97	1.30	0.946	No
605	39.72	2.43	0.99	1.44	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
606	39.78	2.44	0.99	1.44	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
607	39.85	2.44	0.99	1.45	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
608	39.92	2.44	1.00	1.45	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
609	39.97	2.45	1.00	1.45	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
610	40.04	2.45	1.00	1.45	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
611	40.09	2.46	1.00	1.45	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
612	40.17	2.46	1.00	1.46	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
613	40.23	2.46	1.01	1.46	0.85	0.716	1.05	0.679	0.97	1.30	0.947	No
614	40.31	2.47	1.01	1.46	0.85	0.715	1.05	0.679	0.97	1.30	0.947	No
615	40.37	2.47	1.01	1.46	0.85	0.715	1.05	0.678	0.97	1.30	0.947	No
616	40.44	2.48	1.01	1.46	0.85	0.715	1.05	0.678	0.97	1.30	0.947	No
617	40.51	2.48	1.01	1.47	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No
618	40.57	2.49	1.02	1.47	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No
619	40.64	2.49	1.02	1.47	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No
620	40.71	2.49	1.02	1.47	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No
621	40.77	2.50	1.02	1.47	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No
622	40.84	2.50	1.02	1.48	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No
623	40.91	2.51	1.03	1.48	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No
624	40.97	2.51	1.03	1.48	0.84	0.715	1.05	0.678	0.97	1.30	0.947	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
625	41.04	2.51	1.03	1.48	0.84	0.714	1.05	0.678	0.97	1.30	0.947	No
626	41.11	2.52	1.03	1.49	0.84	0.714	1.05	0.678	0.96	1.30	0.947	No
627	41.17	2.52	1.04	1.49	0.84	0.714	1.05	0.677	0.96	1.30	0.947	No
628	41.24	2.53	1.04	1.49	0.84	0.714	1.05	0.677	0.96	1.30	0.947	No
629	41.30	2.53	1.04	1.49	0.84	0.714	1.05	0.677	0.97	1.30	0.947	No
630	41.37	2.53	1.04	1.49	0.84	0.714	1.05	0.677	0.97	1.30	0.947	No
631	41.41	2.54	1.04	1.50	0.84	0.714	1.05	0.677	0.97	1.30	0.947	No
632	41.48	2.54	1.04	1.50	0.84	0.714	1.05	0.677	0.97	1.30	0.947	No
633	41.54	2.55	1.05	1.50	0.84	0.714	1.05	0.677	0.96	1.30	0.947	No
634	41.60	2.55	1.05	1.50	0.84	0.714	1.05	0.677	0.96	1.30	0.946	No
635	41.67	2.55	1.05	1.50	0.84	0.713	1.05	0.677	0.96	1.30	0.945	No
636	41.74	2.56	1.05	1.51	0.84	0.713	1.05	0.676	0.95	1.30	0.943	No
637	41.80	2.56	1.05	1.51	0.84	0.713	1.05	0.676	0.95	1.30	0.943	No
638	41.87	2.57	1.06	1.51	0.84	0.713	1.05	0.676	0.95	1.30	0.942	No
639	41.94	2.57	1.06	1.51	0.84	0.713	1.05	0.676	0.94	1.30	0.941	No
640	42.00	2.58	1.06	1.51	0.84	0.713	1.05	0.676	0.94	1.30	0.939	No
641	42.07	2.58	1.06	1.52	0.84	0.713	1.05	0.676	0.94	1.30	0.938	No
642	42.14	2.58	1.07	1.52	0.84	0.712	1.05	0.676	0.93	1.30	0.937	No
643	42.19	2.59	1.07	1.52	0.84	0.712	1.05	0.676	0.93	1.30	0.936	No
644	42.26	2.59	1.07	1.52	0.84	0.712	1.05	0.675	0.93	1.30	0.937	No
645	42.34	2.60	1.07	1.53	0.84	0.712	1.05	0.675	0.93	1.30	0.936	No
646	42.40	2.60	1.07	1.53	0.84	0.712	1.05	0.675	0.93	1.30	0.936	No
647	42.46	2.61	1.08	1.53	0.84	0.712	1.05	0.675	0.93	1.30	0.936	No
648	42.53	2.61	1.08	1.53	0.83	0.712	1.05	0.675	0.93	1.30	0.937	No
649	42.60	2.61	1.08	1.53	0.83	0.711	1.05	0.675	0.93	1.30	0.937	No
650	42.67	2.62	1.08	1.54	0.83	0.711	1.05	0.675	0.93	1.30	0.938	No
651	42.73	2.62	1.08	1.54	0.83	0.711	1.05	0.674	0.94	1.30	0.939	No
652	42.80	2.63	1.09	1.54	0.83	0.711	1.05	0.674	0.94	1.30	0.940	No
653	42.87	2.63	1.09	1.54	0.83	0.711	1.05	0.674	0.94	1.30	0.941	No
654	42.94	2.64	1.09	1.55	0.83	0.711	1.05	0.674	0.95	1.30	0.943	No
655	43.00	2.64	1.09	1.55	0.83	0.710	1.05	0.674	0.95	1.30	0.944	No
656	43.07	2.64	1.09	1.55	0.83	0.710	1.05	0.674	0.95	1.30	0.944	No
657	43.14	2.65	1.10	1.55	0.83	0.710	1.05	0.674	0.95	1.30	0.945	No
658	43.20	2.65	1.10	1.56	0.83	0.710	1.05	0.673	0.95	1.30	0.945	No
659	43.27	2.66	1.10	1.56	0.83	0.710	1.05	0.673	0.95	1.30	0.945	No
660	43.34	2.66	1.10	1.56	0.83	0.710	1.05	0.673	0.95	1.30	0.945	No
661	43.39	2.67	1.10	1.56	0.83	0.710	1.05	0.673	0.95	1.30	0.944	No
662	43.47	2.67	1.11	1.56	0.83	0.710	1.05	0.673	0.95	1.30	0.944	No
663	43.54	2.67	1.11	1.57	0.83	0.709	1.05	0.673	0.95	1.30	0.945	No
664	43.60	2.68	1.11	1.57	0.83	0.709	1.05	0.673	0.95	1.30	0.945	No
665	43.67	2.68	1.11	1.57	0.83	0.709	1.05	0.673	0.96	1.30	0.945	No
666	43.73	2.69	1.11	1.57	0.83	0.709	1.05	0.672	0.96	1.30	0.945	No
667	43.80	2.69	1.12	1.57	0.83	0.709	1.05	0.672	0.96	1.30	0.945	No
668	43.83	2.69	1.12	1.58	0.83	0.709	1.05	0.672	0.96	1.30	0.945	No
669	43.90	2.70	1.12	1.58	0.83	0.709	1.05	0.672	0.96	1.30	0.945	No
670	43.97	2.70	1.12	1.58	0.83	0.709	1.05	0.672	0.96	1.30	0.945	No
671	44.03	2.71	1.12	1.58	0.83	0.708	1.05	0.672	0.96	1.30	0.945	No
672	44.10	2.71	1.13	1.58	0.83	0.708	1.05	0.672	0.96	1.30	0.945	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
673	44.17	2.71	1.13	1.59	0.83	0.708	1.05	0.672	0.96	1.30	0.944	No
674	44.23	2.72	1.13	1.59	0.83	0.708	1.05	0.672	0.96	1.30	0.944	No
675	44.30	2.72	1.13	1.59	0.83	0.708	1.05	0.671	0.96	1.30	0.944	No
676	44.37	2.73	1.13	1.59	0.83	0.708	1.05	0.671	0.96	1.30	0.944	No
677	44.44	2.73	1.14	1.59	0.83	0.708	1.05	0.671	0.96	1.30	0.944	No
678	44.50	2.73	1.14	1.60	0.82	0.708	1.05	0.671	0.96	1.30	0.944	No
679	44.57	2.74	1.14	1.60	0.82	0.708	1.05	0.671	0.96	1.30	0.944	No
680	44.64	2.74	1.14	1.60	0.82	0.707	1.05	0.671	0.96	1.30	0.944	No
681	44.70	2.75	1.15	1.60	0.82	0.707	1.05	0.671	0.96	1.30	0.944	No
682	44.77	2.75	1.15	1.60	0.82	0.707	1.05	0.671	0.96	1.30	0.944	No
683	44.84	2.75	1.15	1.61	0.82	0.707	1.05	0.671	0.96	1.30	0.945	No
684	44.90	2.76	1.15	1.61	0.82	0.707	1.05	0.670	0.95	1.30	0.945	No
685	44.97	2.76	1.15	1.61	0.82	0.707	1.05	0.670	0.95	1.30	0.945	No
686	45.04	2.77	1.16	1.61	0.82	0.707	1.05	0.670	0.95	1.30	0.944	No
687	45.11	2.77	1.16	1.61	0.82	0.706	1.05	0.670	0.94	1.30	0.944	No
688	45.17	2.78	1.16	1.62	0.82	0.706	1.05	0.670	0.94	1.30	0.944	No
689	45.24	2.78	1.16	1.62	0.82	0.706	1.05	0.670	0.94	1.30	0.944	No
690	45.31	2.78	1.16	1.62	0.82	0.706	1.05	0.670	0.94	1.30	0.944	No
691	45.37	2.79	1.17	1.62	0.82	0.706	1.05	0.669	0.94	1.30	0.944	No
692	45.44	2.79	1.17	1.62	0.82	0.706	1.05	0.669	0.94	1.30	0.944	No
693	45.48	2.80	1.17	1.63	0.82	0.706	1.05	0.669	0.94	1.30	0.943	No
694	45.54	2.80	1.17	1.63	0.82	0.705	1.05	0.669	0.94	1.30	0.943	No
695	45.61	2.80	1.17	1.63	0.82	0.705	1.05	0.669	0.94	1.30	0.943	No
696	45.69	2.81	1.18	1.63	0.82	0.705	1.05	0.669	0.94	1.30	0.943	No
697	45.76	2.81	1.18	1.64	0.82	0.705	1.05	0.669	0.94	1.30	0.943	No
698	45.83	2.82	1.18	1.64	0.82	0.705	1.05	0.668	0.94	1.30	0.943	No
699	45.89	2.82	1.18	1.64	0.82	0.705	1.05	0.668	0.94	1.30	0.943	No
700	45.96	2.83	1.18	1.64	0.82	0.704	1.05	0.668	0.94	1.30	0.943	No
701	46.03	2.83	1.19	1.64	0.82	0.704	1.05	0.668	0.94	1.30	0.943	No
702	46.09	2.83	1.19	1.65	0.82	0.704	1.05	0.668	0.93	1.30	0.943	No
703	46.16	2.84	1.19	1.65	0.82	0.704	1.05	0.668	0.93	1.30	0.943	No
704	46.23	2.84	1.19	1.65	0.82	0.704	1.05	0.668	0.93	1.30	0.943	No
705	46.29	2.85	1.19	1.65	0.82	0.704	1.05	0.667	0.93	1.30	0.943	No
706	46.36	2.85	1.20	1.66	0.82	0.704	1.05	0.667	0.93	1.30	0.943	No
707	46.42	2.86	1.20	1.66	0.82	0.703	1.05	0.667	0.93	1.30	0.943	No
708	46.46	2.86	1.20	1.66	0.82	0.703	1.05	0.667	0.93	1.30	0.943	No
709	46.53	2.86	1.20	1.66	0.81	0.703	1.05	0.667	0.93	1.30	0.943	No
710	46.59	2.87	1.20	1.66	0.81	0.703	1.05	0.667	0.93	1.30	0.943	No
711	46.66	2.87	1.21	1.67	0.81	0.703	1.05	0.667	0.93	1.30	0.943	No
712	46.73	2.88	1.21	1.67	0.81	0.703	1.05	0.666	0.93	1.30	0.943	No
713	46.80	2.88	1.21	1.67	0.81	0.702	1.05	0.666	0.93	1.30	0.943	No
714	46.86	2.88	1.21	1.67	0.81	0.702	1.05	0.666	0.93	1.30	0.943	No
715	46.93	2.89	1.21	1.67	0.81	0.702	1.05	0.666	0.93	1.30	0.943	No
716	46.99	2.89	1.22	1.68	0.81	0.702	1.05	0.666	0.93	1.30	0.943	No
717	47.06	2.90	1.22	1.68	0.81	0.702	1.05	0.666	0.93	1.30	0.943	No
718	47.13	2.90	1.22	1.68	0.81	0.702	1.05	0.665	0.93	1.30	0.943	No
719	47.20	2.91	1.22	1.68	0.81	0.701	1.05	0.665	0.93	1.30	0.943	No
720	47.26	2.91	1.22	1.68	0.81	0.701	1.05	0.665	0.94	1.30	0.943	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
721	47.33	2.91	1.23	1.69	0.81	0.701	1.05	0.665	0.94	1.30	0.943	No
722	47.40	2.92	1.23	1.69	0.81	0.701	1.05	0.665	0.94	1.30	0.943	No
723	47.47	2.92	1.23	1.69	0.81	0.701	1.05	0.665	0.94	1.30	0.943	No
724	47.53	2.93	1.23	1.69	0.81	0.701	1.05	0.664	0.94	1.30	0.943	No
725	47.60	2.93	1.24	1.70	0.81	0.700	1.05	0.664	0.94	1.30	0.943	No
726	47.66	2.94	1.24	1.70	0.81	0.700	1.05	0.664	0.94	1.30	0.943	No
727	47.73	2.94	1.24	1.70	0.81	0.700	1.05	0.664	0.94	1.30	0.943	No
728	47.80	2.94	1.24	1.70	0.81	0.700	1.05	0.664	0.94	1.30	0.943	No
729	47.87	2.95	1.24	1.70	0.81	0.700	1.05	0.664	0.94	1.30	0.942	No
730	47.93	2.95	1.25	1.71	0.81	0.700	1.05	0.664	0.94	1.30	0.942	No
731	48.00	2.96	1.25	1.71	0.81	0.699	1.05	0.663	0.94	1.30	0.942	No
732	48.03	2.96	1.25	1.71	0.81	0.699	1.05	0.663	0.94	1.30	0.942	No
733	48.10	2.96	1.25	1.71	0.81	0.699	1.05	0.663	0.94	1.30	0.942	No
734	48.17	2.97	1.25	1.71	0.81	0.699	1.05	0.663	0.95	1.30	0.941	No
735	48.24	2.97	1.26	1.72	0.81	0.699	1.05	0.663	0.95	1.30	0.941	No
736	48.30	2.98	1.26	1.72	0.81	0.699	1.05	0.663	0.95	1.30	0.941	No
737	48.37	2.98	1.26	1.72	0.81	0.699	1.05	0.663	0.95	1.30	0.940	No
738	48.43	2.98	1.26	1.72	0.81	0.698	1.05	0.662	0.96	1.30	0.939	No
739	48.50	2.99	1.26	1.72	0.81	0.698	1.05	0.662	0.95	1.30	0.939	No
740	48.56	2.99	1.27	1.73	0.80	0.698	1.05	0.662	0.96	1.30	0.939	No
741	48.63	3.00	1.27	1.73	0.80	0.698	1.05	0.662	0.96	1.30	0.938	No
742	48.70	3.00	1.27	1.73	0.80	0.698	1.05	0.662	0.96	1.30	0.938	No
743	48.76	3.00	1.27	1.73	0.80	0.698	1.05	0.662	0.96	1.30	0.938	No
744	48.82	3.01	1.27	1.73	0.80	0.698	1.05	0.662	0.95	1.30	0.939	No
745	48.89	3.01	1.28	1.74	0.80	0.698	1.05	0.662	0.95	1.30	0.940	No
746	48.95	3.02	1.28	1.74	0.80	0.697	1.05	0.661	0.95	1.30	0.940	No
747	49.02	3.02	1.28	1.74	0.80	0.697	1.05	0.661	0.95	1.30	0.940	No
748	49.09	3.02	1.28	1.74	0.80	0.697	1.05	0.661	0.95	1.30	0.940	No
749	49.15	3.03	1.28	1.74	0.80	0.697	1.05	0.661	0.95	1.30	0.940	No
750	49.23	3.03	1.29	1.75	0.80	0.697	1.05	0.661	0.95	1.30	0.940	No
751	49.28	3.04	1.29	1.75	0.80	0.697	1.05	0.661	0.95	1.30	0.939	No
752	49.35	3.04	1.29	1.75	0.80	0.696	1.05	0.661	0.95	1.30	0.938	No
753	49.42	3.04	1.29	1.75	0.80	0.696	1.05	0.660	0.95	1.30	0.938	No
754	49.48	3.05	1.29	1.75	0.80	0.696	1.05	0.660	0.95	1.30	0.937	No
755	49.55	3.05	1.30	1.76	0.80	0.696	1.05	0.660	0.95	1.30	0.937	No
756	49.62	3.06	1.30	1.76	0.80	0.696	1.05	0.660	0.95	1.30	0.937	No
757	49.69	3.06	1.30	1.76	0.80	0.696	1.05	0.660	0.95	1.30	0.937	No
758	49.75	3.06	1.30	1.76	0.80	0.696	1.05	0.660	0.95	1.30	0.937	No
759	49.82	3.07	1.30	1.76	0.80	0.695	1.05	0.660	0.95	1.30	0.936	No
760	49.87	3.07	1.31	1.76	0.80	0.695	1.05	0.660	0.95	1.30	0.936	No
761	49.94	3.08	1.31	1.77	0.80	0.695	1.05	0.659	0.95	1.30	0.936	No
762	50.02	3.08	1.31	1.77	0.80	0.695	1.05	0.659	0.95	1.30	2.000	No
763	50.07	3.08	1.31	1.77	0.80	0.695	1.05	0.659	0.95	1.30	2.000	No
764	50.16	3.09	1.32	1.77	0.80	0.695	1.05	0.659	0.95	1.30	2.000	No
765	50.21	3.09	1.32	1.77	0.80	0.695	1.05	0.659	0.95	1.30	2.000	No
766	50.27	3.09	1.32	1.78	0.80	0.695	1.05	0.659	0.95	1.30	2.000	No
767	50.33	3.10	1.32	1.78	0.80	0.694	1.05	0.659	0.95	1.30	2.000	No
768	50.40	3.10	1.32	1.78	0.80	0.694	1.05	0.659	0.94	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
769	50.47	3.11	1.33	1.78	0.80	0.694	1.05	0.658	0.93	1.30	2.000	No
770	50.53	3.11	1.33	1.78	0.80	0.694	1.05	0.658	0.92	1.30	2.000	No
771	50.61	3.12	1.33	1.79	0.79	0.694	1.05	0.658	0.91	1.30	2.000	No
772	50.66	3.12	1.33	1.79	0.79	0.694	1.05	0.658	0.90	1.30	2.000	No
773	50.73	3.12	1.33	1.79	0.79	0.693	1.05	0.658	0.90	1.30	2.000	No
774	50.80	3.13	1.34	1.79	0.79	0.693	1.05	0.657	0.90	1.30	2.000	No
775	50.87	3.13	1.34	1.80	0.79	0.693	1.05	0.657	0.90	1.30	2.000	No
776	50.92	3.14	1.34	1.80	0.79	0.693	1.05	0.657	0.90	1.30	2.000	No
777	51.01	3.14	1.34	1.80	0.79	0.693	1.05	0.657	0.89	1.30	2.000	No
778	51.07	3.15	1.34	1.80	0.79	0.692	1.05	0.657	0.90	1.30	2.000	No
779	51.13	3.15	1.35	1.80	0.79	0.692	1.05	0.657	0.90	1.30	2.000	No
780	51.20	3.15	1.35	1.81	0.79	0.692	1.05	0.656	0.90	1.30	2.000	No
781	51.26	3.16	1.35	1.81	0.79	0.692	1.05	0.656	0.90	1.30	2.000	No
782	51.32	3.16	1.35	1.81	0.79	0.692	1.05	0.656	0.90	1.30	2.000	No
783	51.39	3.17	1.35	1.81	0.79	0.691	1.05	0.656	0.91	1.30	2.000	No
784	51.45	3.17	1.36	1.82	0.79	0.691	1.05	0.656	0.91	1.30	2.000	No
785	51.52	3.18	1.36	1.82	0.79	0.691	1.05	0.655	0.91	1.30	2.000	No
786	51.59	3.18	1.36	1.82	0.79	0.691	1.05	0.655	0.91	1.30	2.000	No
787	51.65	3.18	1.36	1.82	0.79	0.691	1.05	0.655	0.91	1.30	2.000	No
788	51.71	3.19	1.36	1.82	0.79	0.691	1.05	0.655	0.90	1.30	2.000	No
789	51.78	3.19	1.37	1.83	0.79	0.690	1.05	0.655	0.90	1.30	2.000	No
790	51.84	3.20	1.37	1.83	0.79	0.690	1.05	0.655	0.90	1.30	2.000	No
791	51.92	3.20	1.37	1.83	0.79	0.690	1.05	0.654	0.91	1.30	2.000	No
792	51.97	3.20	1.37	1.83	0.79	0.690	1.05	0.654	0.91	1.30	2.000	No
793	52.04	3.21	1.37	1.84	0.79	0.689	1.05	0.654	0.90	1.30	2.000	No
794	52.10	3.21	1.38	1.84	0.79	0.689	1.05	0.654	0.90	1.30	2.000	No
795	52.17	3.22	1.38	1.84	0.79	0.689	1.05	0.654	0.90	1.30	2.000	No
796	52.23	3.22	1.38	1.84	0.79	0.689	1.05	0.653	0.90	1.30	2.000	No
797	52.30	3.23	1.38	1.84	0.79	0.689	1.05	0.653	0.89	1.30	2.000	No
798	52.37	3.23	1.38	1.85	0.79	0.688	1.05	0.653	0.88	1.30	2.000	No
799	52.44	3.24	1.39	1.85	0.79	0.688	1.05	0.653	0.86	1.30	2.000	No
800	52.50	3.24	1.39	1.85	0.79	0.688	1.05	0.653	0.87	1.30	2.000	No
801	52.56	3.24	1.39	1.85	0.79	0.688	1.05	0.652	0.85	1.30	2.000	No
802	52.63	3.25	1.39	1.86	0.78	0.688	1.05	0.652	0.85	1.30	2.000	No
803	52.69	3.25	1.39	1.86	0.78	0.687	1.05	0.652	0.85	1.30	2.000	No
804	52.77	3.26	1.40	1.86	0.78	0.687	1.05	0.652	0.86	1.30	2.000	No
805	52.85	3.26	1.40	1.86	0.78	0.687	1.05	0.651	0.86	1.30	2.000	No
806	52.92	3.27	1.40	1.87	0.78	0.687	1.05	0.651	0.86	1.30	2.000	No
807	52.98	3.27	1.40	1.87	0.78	0.687	1.05	0.651	0.87	1.30	2.000	No
808	53.05	3.28	1.41	1.87	0.78	0.686	1.05	0.651	0.87	1.30	2.000	No
809	53.09	3.28	1.41	1.87	0.78	0.686	1.05	0.651	0.88	1.30	2.000	No
810	53.15	3.28	1.41	1.87	0.78	0.686	1.05	0.651	0.88	1.30	2.000	No
811	53.22	3.29	1.41	1.88	0.78	0.686	1.05	0.650	0.88	1.30	2.000	No
812	53.29	3.29	1.41	1.88	0.78	0.686	1.05	0.650	0.88	1.30	2.000	No
813	53.36	3.30	1.42	1.88	0.78	0.685	1.05	0.650	0.88	1.30	2.000	No
814	53.41	3.30	1.42	1.88	0.78	0.685	1.05	0.650	0.88	1.30	2.000	No
815	53.48	3.30	1.42	1.88	0.78	0.685	1.05	0.650	0.88	1.30	2.000	No
816	53.55	3.31	1.42	1.89	0.78	0.685	1.05	0.649	0.87	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
817	53.61	3.31	1.42	1.89	0.78	0.685	1.05	0.649	0.87	1.30	2.000	No
818	53.69	3.32	1.43	1.89	0.78	0.684	1.05	0.649	0.86	1.30	2.000	No
819	53.74	3.32	1.43	1.89	0.78	0.684	1.05	0.649	0.85	1.30	2.000	No
820	53.81	3.33	1.43	1.90	0.78	0.684	1.05	0.649	0.84	1.30	2.000	No
821	53.89	3.33	1.43	1.90	0.78	0.684	1.05	0.648	0.83	1.30	2.000	No
822	53.95	3.33	1.43	1.90	0.78	0.683	1.05	0.648	0.82	1.30	2.000	No
823	54.01	3.34	1.44	1.90	0.78	0.683	1.05	0.648	0.82	1.30	2.000	No
824	54.07	3.34	1.44	1.91	0.78	0.683	1.05	0.648	0.82	1.30	2.000	No
825	54.15	3.35	1.44	1.91	0.78	0.683	1.05	0.648	0.82	1.30	2.000	No
826	54.22	3.35	1.44	1.91	0.78	0.683	1.05	0.647	0.82	1.30	2.000	No
827	54.27	3.36	1.44	1.91	0.78	0.682	1.05	0.647	0.82	1.30	2.000	No
828	54.35	3.36	1.45	1.92	0.78	0.682	1.05	0.647	0.82	1.30	2.000	No
829	54.40	3.36	1.45	1.92	0.78	0.682	1.05	0.647	0.82	1.30	2.000	No
830	54.48	3.37	1.45	1.92	0.78	0.682	1.05	0.647	0.82	1.30	2.000	No
831	54.53	3.37	1.45	1.92	0.78	0.681	1.05	0.646	0.82	1.30	2.000	No
832	54.60	3.38	1.45	1.92	0.78	0.681	1.05	0.646	0.82	1.30	2.000	No
833	54.66	3.38	1.46	1.93	0.78	0.681	1.05	0.646	0.82	1.30	2.000	No
834	54.73	3.39	1.46	1.93	0.77	0.681	1.05	0.646	0.82	1.30	2.000	No
835	54.80	3.39	1.46	1.93	0.77	0.681	1.05	0.645	0.82	1.30	2.000	No
836	54.86	3.40	1.46	1.93	0.77	0.680	1.05	0.645	0.82	1.30	2.000	No
837	54.93	3.40	1.46	1.94	0.77	0.680	1.05	0.645	0.82	1.30	2.000	No
838	55.00	3.40	1.47	1.94	0.77	0.680	1.05	0.645	0.82	1.30	2.000	No
839	55.06	3.41	1.47	1.94	0.77	0.680	1.05	0.645	0.82	1.30	2.000	No
840	55.13	3.41	1.47	1.94	0.77	0.679	1.05	0.644	0.82	1.30	2.000	No
841	55.20	3.42	1.47	1.95	0.77	0.679	1.05	0.644	0.82	1.30	2.000	No
842	55.27	3.42	1.47	1.95	0.77	0.679	1.05	0.644	0.82	1.30	2.000	No
843	55.34	3.43	1.48	1.95	0.77	0.679	1.05	0.644	0.82	1.30	2.000	No
844	55.40	3.43	1.48	1.95	0.77	0.678	1.05	0.643	0.82	1.30	2.000	No
845	55.47	3.44	1.48	1.96	0.77	0.678	1.05	0.643	0.82	1.30	2.000	No
846	55.53	3.44	1.48	1.96	0.77	0.678	1.05	0.643	0.82	1.30	2.000	No
847	55.60	3.45	1.49	1.96	0.77	0.678	1.05	0.643	0.81	1.30	2.000	No
848	55.67	3.45	1.49	1.96	0.77	0.678	1.05	0.643	0.81	1.30	2.000	No
849	55.73	3.45	1.49	1.97	0.77	0.677	1.05	0.642	0.81	1.30	2.000	No
850	55.80	3.46	1.49	1.97	0.77	0.677	1.05	0.642	0.81	1.30	2.000	No
851	55.87	3.46	1.49	1.97	0.77	0.677	1.05	0.642	0.81	1.30	2.000	No
852	55.93	3.47	1.50	1.97	0.77	0.677	1.05	0.642	0.81	1.30	2.000	No
853	55.98	3.47	1.50	1.97	0.77	0.676	1.05	0.642	0.81	1.30	2.000	No
854	56.05	3.48	1.50	1.98	0.77	0.676	1.05	0.641	0.81	1.30	2.000	No
855	56.10	3.48	1.50	1.98	0.77	0.676	1.05	0.641	0.81	1.30	2.000	No
856	56.19	3.49	1.50	1.98	0.77	0.676	1.05	0.641	0.81	1.30	2.000	No
857	56.24	3.49	1.50	1.98	0.77	0.676	1.05	0.641	0.81	1.30	2.000	No
858	56.31	3.49	1.51	1.99	0.77	0.675	1.05	0.640	0.81	1.30	2.000	No
859	56.38	3.50	1.51	1.99	0.77	0.675	1.05	0.640	0.81	1.30	2.000	No
860	56.46	3.50	1.51	1.99	0.77	0.675	1.05	0.640	0.81	1.30	2.000	No
861	56.52	3.51	1.51	1.99	0.77	0.675	1.05	0.640	0.81	1.30	2.000	No
862	56.58	3.51	1.52	2.00	0.77	0.674	1.05	0.640	0.81	1.30	2.000	No
863	56.65	3.52	1.52	2.00	0.77	0.674	1.05	0.639	0.81	1.30	2.000	No
864	56.71	3.52	1.52	2.00	0.77	0.674	1.05	0.639	0.81	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
865	56.77	3.52	1.52	2.00	0.76	0.674	1.05	0.639	0.81	1.30	2.000	No
866	56.83	3.53	1.52	2.01	0.76	0.673	1.05	0.639	0.81	1.30	2.000	No
867	56.90	3.53	1.53	2.01	0.76	0.673	1.05	0.639	0.81	1.30	2.000	No
868	56.96	3.54	1.53	2.01	0.76	0.673	1.05	0.638	0.81	1.30	2.000	No
869	57.03	3.54	1.53	2.01	0.76	0.673	1.05	0.638	0.81	1.30	2.000	No
870	57.10	3.55	1.53	2.01	0.76	0.673	1.05	0.638	0.81	1.30	2.000	No
871	57.16	3.55	1.53	2.02	0.76	0.672	1.05	0.638	0.81	1.30	2.000	No
872	57.23	3.56	1.54	2.02	0.76	0.672	1.05	0.637	0.81	1.30	2.000	No
873	57.30	3.56	1.54	2.02	0.76	0.672	1.05	0.637	0.83	1.30	2.000	No
874	57.37	3.56	1.54	2.02	0.76	0.672	1.05	0.637	0.82	1.30	2.000	No
875	57.43	3.57	1.54	2.03	0.76	0.671	1.05	0.637	0.81	1.30	2.000	No
876	57.50	3.57	1.54	2.03	0.76	0.671	1.05	0.637	0.80	1.30	2.000	No
877	57.57	3.58	1.55	2.03	0.76	0.671	1.05	0.636	0.80	1.30	2.000	No
878	57.62	3.58	1.55	2.03	0.76	0.671	1.05	0.636	0.81	1.30	2.000	No
879	57.68	3.58	1.55	2.03	0.76	0.671	1.05	0.636	0.80	1.30	2.000	No
880	57.76	3.59	1.55	2.04	0.76	0.670	1.05	0.636	0.80	1.30	2.000	No
881	57.82	3.59	1.55	2.04	0.76	0.670	1.05	0.636	0.80	1.30	2.000	No
882	57.88	3.60	1.56	2.04	0.76	0.670	1.05	0.635	0.80	1.30	2.000	No
883	57.94	3.60	1.56	2.04	0.76	0.670	1.05	0.635	0.80	1.30	2.000	No
884	58.01	3.61	1.56	2.05	0.76	0.670	1.05	0.635	0.80	1.30	2.000	No
885	58.08	3.61	1.56	2.05	0.76	0.669	1.05	0.635	0.80	1.30	2.000	No
886	58.14	3.62	1.56	2.05	0.76	0.669	1.05	0.635	0.80	1.30	2.000	No
887	58.21	3.62	1.57	2.05	0.76	0.669	1.05	0.634	0.81	1.30	2.000	No
888	58.28	3.62	1.57	2.06	0.76	0.669	1.05	0.634	0.81	1.30	2.000	No
889	58.35	3.63	1.57	2.06	0.76	0.668	1.05	0.634	0.80	1.30	2.000	No
890	58.40	3.63	1.57	2.06	0.76	0.668	1.05	0.634	0.80	1.30	2.000	No
891	58.47	3.64	1.57	2.06	0.76	0.668	1.05	0.634	0.80	1.30	2.000	No
892	58.54	3.64	1.58	2.06	0.76	0.668	1.05	0.633	0.80	1.30	2.000	No
893	58.61	3.65	1.58	2.07	0.76	0.668	1.05	0.633	0.80	1.30	2.000	No
894	58.67	3.65	1.58	2.07	0.76	0.667	1.05	0.633	0.80	1.30	2.000	No
895	58.74	3.65	1.58	2.07	0.76	0.667	1.05	0.633	0.80	1.30	2.000	No
896	58.82	3.66	1.59	2.07	0.76	0.667	1.05	0.632	0.80	1.30	2.000	No
897	58.88	3.66	1.59	2.08	0.75	0.667	1.05	0.632	0.80	1.30	2.000	No
898	58.95	3.67	1.59	2.08	0.75	0.666	1.05	0.632	0.86	1.30	2.000	No
899	59.02	3.67	1.59	2.08	0.75	0.666	1.05	0.632	0.90	1.30	2.000	No
900	59.09	3.68	1.59	2.08	0.75	0.666	1.05	0.632	0.90	1.30	2.000	No
901	59.12	3.68	1.59	2.08	0.75	0.666	1.05	0.632	0.89	1.30	2.000	No
902	59.19	3.68	1.60	2.09	0.75	0.666	1.05	0.631	0.88	1.30	2.000	No
903	59.26	3.69	1.60	2.09	0.75	0.666	1.05	0.631	0.88	1.30	2.000	No
904	59.32	3.69	1.60	2.09	0.75	0.665	1.05	0.631	0.87	1.30	2.000	No
905	59.40	3.70	1.60	2.09	0.75	0.665	1.05	0.631	0.85	1.30	2.000	No
906	59.46	3.70	1.61	2.10	0.75	0.665	1.05	0.631	0.84	1.30	2.000	No
907	59.52	3.71	1.61	2.10	0.75	0.665	1.05	0.630	0.83	1.30	2.000	No
908	59.60	3.71	1.61	2.10	0.75	0.664	1.05	0.630	0.80	1.30	2.000	No
909	59.66	3.71	1.61	2.10	0.75	0.664	1.05	0.630	0.79	1.30	2.000	No
910	59.73	3.72	1.61	2.11	0.75	0.664	1.05	0.630	0.79	1.30	2.000	No
911	59.78	3.72	1.62	2.11	0.75	0.664	1.05	0.630	0.79	1.30	2.000	No
912	59.85	3.73	1.62	2.11	0.75	0.664	1.05	0.629	0.79	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
913	59.93	3.73	1.62	2.11	0.75	0.663	1.05	0.629	0.79	1.30	2.000	No
914	59.99	3.74	1.62	2.11	0.75	0.663	1.05	0.629	0.79	1.30	2.000	No
915	60.04	3.74	1.62	2.12	0.75	0.663	1.05	0.629	0.79	1.30	2.000	No
916	60.11	3.74	1.63	2.12	0.75	0.663	1.05	0.629	0.79	1.30	2.000	No
917	60.18	3.75	1.63	2.12	0.75	0.663	1.05	0.628	0.79	1.30	2.000	No
918	60.24	3.75	1.63	2.12	0.75	0.662	1.05	0.628	0.79	1.30	2.000	No
919	60.30	3.76	1.63	2.13	0.75	0.662	1.05	0.628	0.79	1.30	2.000	No
920	60.37	3.76	1.63	2.13	0.75	0.662	1.05	0.628	0.79	1.30	2.000	No
921	60.44	3.77	1.64	2.13	0.75	0.662	1.05	0.627	0.79	1.30	2.000	No
922	60.50	3.77	1.64	2.13	0.75	0.661	1.05	0.627	0.79	1.30	2.000	No
923	60.58	3.78	1.64	2.14	0.75	0.661	1.05	0.627	0.79	1.30	2.000	No
924	60.63	3.78	1.64	2.14	0.75	0.661	1.05	0.627	0.79	1.30	2.000	No
925	60.70	3.78	1.64	2.14	0.75	0.661	1.05	0.627	0.79	1.30	2.000	No
926	60.78	3.79	1.65	2.14	0.75	0.660	1.05	0.626	0.79	1.30	2.000	No
927	60.83	3.79	1.65	2.14	0.75	0.660	1.05	0.626	0.79	1.30	2.000	No
928	60.89	3.80	1.65	2.15	0.75	0.660	1.05	0.626	0.79	1.30	2.000	No
929	60.97	3.80	1.65	2.15	0.75	0.660	1.05	0.626	0.79	1.30	2.000	No
930	61.03	3.81	1.65	2.15	0.74	0.660	1.05	0.626	0.79	1.30	2.000	No
931	61.10	3.81	1.66	2.15	0.74	0.659	1.05	0.625	0.79	1.30	2.000	No
932	61.16	3.81	1.66	2.16	0.74	0.659	1.05	0.625	0.79	1.30	2.000	No
933	61.22	3.82	1.66	2.16	0.74	0.659	1.05	0.625	0.79	1.30	2.000	No
934	61.30	3.82	1.66	2.16	0.74	0.659	1.05	0.625	0.79	1.30	2.000	No
935	61.36	3.83	1.66	2.16	0.74	0.659	1.05	0.625	0.79	1.30	2.000	No
936	61.42	3.83	1.67	2.16	0.74	0.658	1.05	0.624	0.79	1.30	2.000	No
937	61.48	3.84	1.67	2.17	0.74	0.658	1.05	0.624	0.78	1.30	2.000	No
938	61.57	3.84	1.67	2.17	0.74	0.658	1.05	0.624	0.78	1.30	2.000	No
939	61.64	3.85	1.67	2.17	0.74	0.658	1.05	0.624	0.78	1.30	2.000	No
940	61.70	3.85	1.68	2.17	0.74	0.657	1.05	0.624	0.78	1.30	2.000	No
941	61.76	3.85	1.68	2.18	0.74	0.657	1.05	0.623	0.83	1.30	2.000	No
942	61.82	3.86	1.68	2.18	0.74	0.657	1.05	0.623	0.84	1.30	2.000	No
943	61.88	3.86	1.68	2.18	0.74	0.657	1.05	0.623	0.83	1.30	2.000	No
944	61.96	3.87	1.68	2.18	0.74	0.657	1.05	0.623	0.84	1.30	2.000	No
945	62.03	3.87	1.69	2.18	0.74	0.657	1.05	0.623	0.86	1.30	2.000	No
946	62.08	3.87	1.69	2.19	0.74	0.656	1.05	0.622	0.87	1.30	2.000	No
947	62.15	3.88	1.69	2.19	0.74	0.656	1.05	0.622	0.88	1.30	2.000	No
948	62.22	3.88	1.69	2.19	0.74	0.656	1.05	0.622	0.86	1.30	2.000	No
949	62.29	3.89	1.69	2.19	0.74	0.656	1.05	0.622	0.85	1.30	2.000	No
950	62.36	3.89	1.70	2.20	0.74	0.655	1.05	0.622	0.85	1.30	2.000	No
951	62.41	3.89	1.70	2.20	0.74	0.655	1.05	0.622	0.85	1.30	2.000	No
952	62.48	3.90	1.70	2.20	0.74	0.655	1.05	0.621	0.83	1.30	2.000	No
953	62.55	3.90	1.70	2.20	0.74	0.655	1.05	0.621	0.84	1.30	2.000	No
954	62.62	3.91	1.70	2.20	0.74	0.655	1.05	0.621	0.83	1.30	2.000	No
955	62.69	3.91	1.71	2.21	0.74	0.654	1.05	0.621	0.82	1.30	2.000	No
956	62.73	3.92	1.71	2.21	0.74	0.654	1.05	0.621	0.82	1.30	2.000	No
957	62.80	3.92	1.71	2.21	0.74	0.654	1.05	0.620	0.83	1.30	2.000	No
958	62.87	3.92	1.71	2.21	0.74	0.654	1.05	0.620	0.83	1.30	2.000	No
959	62.95	3.93	1.71	2.22	0.74	0.654	1.05	0.620	0.82	1.30	2.000	No
960	63.02	3.93	1.72	2.22	0.74	0.653	1.05	0.620	0.87	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
961	63.06	3.94	1.72	2.22	0.74	0.653	1.05	0.620	0.87	1.30	2.000	No
962	63.13	3.94	1.72	2.22	0.74	0.653	1.05	0.619	0.85	1.30	2.000	No
963	63.20	3.95	1.72	2.22	0.74	0.653	1.05	0.619	0.82	1.30	2.000	No
964	63.26	3.95	1.72	2.23	0.73	0.653	1.05	0.619	0.80	1.30	2.000	No
965	63.34	3.95	1.73	2.23	0.73	0.652	1.05	0.619	0.78	1.30	2.000	No
966	63.39	3.96	1.73	2.23	0.73	0.652	1.05	0.619	0.78	1.30	2.000	No
967	63.45	3.96	1.73	2.23	0.73	0.652	1.05	0.618	0.78	1.30	2.000	No
968	63.52	3.97	1.73	2.23	0.73	0.652	1.05	0.618	0.78	1.30	2.000	No
969	63.59	3.97	1.73	2.24	0.73	0.652	1.05	0.618	0.78	1.30	2.000	No
970	63.66	3.98	1.74	2.24	0.73	0.651	1.05	0.618	0.78	1.30	2.000	No
971	63.72	3.98	1.74	2.24	0.73	0.651	1.05	0.618	0.77	1.30	2.000	No
972	63.79	3.98	1.74	2.24	0.73	0.651	1.05	0.617	0.77	1.30	2.000	No
973	63.86	3.99	1.74	2.24	0.73	0.651	1.05	0.617	0.79	1.30	2.000	No
974	63.91	3.99	1.74	2.25	0.73	0.651	1.05	0.617	0.80	1.30	2.000	No
975	63.98	4.00	1.75	2.25	0.73	0.650	1.05	0.617	0.83	1.30	2.000	No
976	64.05	4.00	1.75	2.25	0.73	0.650	1.05	0.617	0.84	1.30	2.000	No
977	64.12	4.00	1.75	2.25	0.73	0.650	1.05	0.617	0.85	1.30	2.000	No
978	64.18	4.01	1.75	2.26	0.73	0.650	1.05	0.616	0.85	1.30	2.000	No
979	64.25	4.01	1.75	2.26	0.73	0.650	1.05	0.616	0.86	1.30	2.000	No
980	64.31	4.02	1.76	2.26	0.73	0.649	1.05	0.616	0.85	1.30	2.000	No
981	64.38	4.02	1.76	2.26	0.73	0.649	1.05	0.616	0.82	1.30	2.000	No
982	64.45	4.03	1.76	2.26	0.73	0.649	1.05	0.616	0.81	1.30	2.000	No
983	64.50	4.03	1.76	2.27	0.73	0.649	1.05	0.615	0.82	1.30	2.000	No
984	64.58	4.03	1.77	2.27	0.73	0.649	1.05	0.615	0.83	1.30	2.000	No
985	64.64	4.04	1.77	2.27	0.73	0.648	1.05	0.615	0.84	1.30	2.000	No
986	64.72	4.04	1.77	2.27	0.73	0.648	1.05	0.615	0.85	1.30	2.000	No
987	64.77	4.05	1.77	2.28	0.73	0.648	1.05	0.615	0.84	1.30	2.000	No
988	64.83	4.05	1.77	2.28	0.73	0.648	1.05	0.614	0.85	1.30	2.000	No
989	64.91	4.06	1.78	2.28	0.73	0.648	1.05	0.614	0.84	1.30	2.000	No
990	64.97	4.06	1.78	2.28	0.73	0.647	1.05	0.614	0.84	1.30	2.000	No
991	65.04	4.06	1.78	2.28	0.73	0.647	1.05	0.614	0.84	1.30	2.000	No
992	65.10	4.07	1.78	2.29	0.73	0.647	1.05	0.614	0.88	1.30	2.000	No
993	65.17	4.07	1.78	2.29	0.73	0.647	1.05	0.613	0.90	1.30	2.000	No
994	65.24	4.08	1.79	2.29	0.73	0.647	1.05	0.613	0.90	1.30	2.000	No
995	65.31	4.08	1.79	2.29	0.73	0.646	1.05	0.613	0.89	1.30	2.000	No
996	65.36	4.08	1.79	2.29	0.73	0.646	1.05	0.613	0.90	1.30	2.000	No
997	65.42	4.09	1.79	2.30	0.73	0.646	1.05	0.613	0.90	1.30	2.000	No
998	65.49	4.09	1.79	2.30	0.72	0.646	1.05	0.613	0.89	1.30	2.000	No
999	65.55	4.10	1.80	2.30	0.72	0.646	1.05	0.612	0.89	1.30	2.000	No
1000	65.62	4.10	1.80	2.30	0.72	0.646	1.05	0.612	0.89	1.30	2.000	No
1001	65.69	4.10	1.80	2.30	0.72	0.645	1.05	0.612	0.90	1.30	2.000	No
1002	65.76	4.11	1.80	2.31	0.72	0.645	1.05	0.612	0.91	1.30	2.000	No
1003	65.83	4.11	1.80	2.31	0.72	0.645	1.05	0.612	0.91	1.30	2.000	No
1004	65.89	4.12	1.81	2.31	0.72	0.645	1.05	0.612	0.91	1.30	2.000	No
1005	65.95	4.12	1.81	2.31	0.72	0.645	1.05	0.612	0.92	1.30	2.000	No
1006	66.03	4.12	1.81	2.31	0.72	0.645	1.05	0.611	0.92	1.30	2.000	No
1007	66.08	4.13	1.81	2.31	0.72	0.644	1.05	0.611	0.93	1.30	2.000	No
1008	66.16	4.13	1.81	2.32	0.72	0.644	1.05	0.611	0.92	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1009	66.22	4.14	1.82	2.32	0.72	0.644	1.05	0.611	0.91	1.30	2.000	No
1010	66.29	4.14	1.82	2.32	0.72	0.644	1.05	0.611	0.91	1.30	2.000	No
1011	66.36	4.14	1.82	2.32	0.72	0.644	1.05	0.611	0.91	1.30	2.000	No
1012	66.42	4.15	1.82	2.32	0.72	0.644	1.05	0.610	0.91	1.30	2.000	No
1013	66.49	4.15	1.82	2.33	0.72	0.643	1.05	0.610	0.91	1.30	2.000	No
1014	66.55	4.15	1.83	2.33	0.72	0.643	1.05	0.610	0.91	1.30	2.000	No
1015	66.62	4.16	1.83	2.33	0.72	0.643	1.05	0.610	0.91	1.30	2.000	No
1016	66.69	4.16	1.83	2.33	0.72	0.643	1.05	0.610	0.91	1.30	2.000	No
1017	66.75	4.17	1.83	2.33	0.72	0.643	1.05	0.610	0.91	1.30	2.000	No
1018	66.82	4.17	1.84	2.33	0.72	0.643	1.05	0.610	0.91	1.30	2.000	No
1019	66.89	4.17	1.84	2.34	0.72	0.643	1.05	0.609	0.91	1.30	2.000	No
1020	66.96	4.18	1.84	2.34	0.72	0.642	1.05	0.609	0.91	1.30	2.000	No
1021	67.00	4.18	1.84	2.34	0.72	0.642	1.05	0.609	0.92	1.30	2.000	No
1022	67.08	4.19	1.84	2.34	0.72	0.642	1.05	0.609	0.91	1.30	2.000	No
1023	67.14	4.19	1.85	2.34	0.72	0.642	1.05	0.609	0.91	1.30	2.000	No
1024	67.21	4.19	1.85	2.35	0.72	0.642	1.05	0.609	0.91	1.30	2.000	No
1025	67.28	4.20	1.85	2.35	0.72	0.641	1.05	0.608	0.91	1.30	2.000	No
1026	67.34	4.20	1.85	2.35	0.72	0.641	1.05	0.608	0.90	1.30	2.000	No
1027	67.41	4.21	1.85	2.35	0.72	0.641	1.05	0.608	0.89	1.30	2.000	No
1028	67.47	4.21	1.86	2.35	0.72	0.641	1.05	0.608	0.87	1.30	2.000	No
1029	67.54	4.21	1.86	2.36	0.72	0.641	1.05	0.608	0.86	1.30	2.000	No
1030	67.61	4.22	1.86	2.36	0.72	0.640	1.05	0.607	0.86	1.30	2.000	No
1031	67.67	4.22	1.86	2.36	0.72	0.640	1.05	0.607	0.87	1.30	2.000	No
1032	67.74	4.23	1.86	2.36	0.72	0.640	1.05	0.607	0.88	1.30	2.000	No
1033	67.80	4.23	1.87	2.37	0.71	0.640	1.05	0.607	0.88	1.30	2.000	No
1034	67.87	4.24	1.87	2.37	0.71	0.640	1.05	0.607	0.87	1.30	2.000	No
1035	67.94	4.24	1.87	2.37	0.71	0.640	1.05	0.607	0.87	1.30	2.000	No
1036	68.00	4.24	1.87	2.37	0.71	0.639	1.05	0.606	0.86	1.30	2.000	No
1037	68.07	4.25	1.87	2.37	0.71	0.639	1.05	0.606	0.86	1.30	2.000	No
1038	68.14	4.25	1.88	2.38	0.71	0.639	1.05	0.606	0.85	1.30	2.000	No
1039	68.20	4.26	1.88	2.38	0.71	0.639	1.05	0.606	0.85	1.30	2.000	No
1040	68.27	4.26	1.88	2.38	0.71	0.639	1.05	0.606	0.85	1.30	2.000	No
1041	68.34	4.27	1.88	2.38	0.71	0.638	1.05	0.605	0.84	1.30	2.000	No
1042	68.41	4.27	1.88	2.38	0.71	0.638	1.05	0.605	0.84	1.30	2.000	No
1043	68.44	4.27	1.89	2.39	0.71	0.638	1.05	0.605	0.84	1.30	2.000	No
1044	68.51	4.28	1.89	2.39	0.71	0.638	1.05	0.605	0.83	1.30	2.000	No
1045	68.58	4.28	1.89	2.39	0.71	0.638	1.05	0.605	0.83	1.30	2.000	No
1046	68.65	4.28	1.89	2.39	0.71	0.637	1.05	0.605	0.82	1.30	2.000	No
1047	68.73	4.29	1.89	2.40	0.71	0.637	1.05	0.604	0.82	1.30	2.000	No
1048	68.78	4.29	1.90	2.40	0.71	0.637	1.05	0.604	0.81	1.30	2.000	No
1049	68.83	4.30	1.90	2.40	0.71	0.637	1.05	0.604	0.81	1.30	2.000	No
1050	68.92	4.30	1.90	2.40	0.71	0.637	1.05	0.604	0.80	1.30	2.000	No
1051	68.97	4.31	1.90	2.40	0.71	0.636	1.05	0.604	0.79	1.30	2.000	No
1052	69.03	4.31	1.90	2.41	0.71	0.636	1.05	0.603	0.79	1.30	2.000	No
1053	69.09	4.31	1.91	2.41	0.71	0.636	1.05	0.603	0.78	1.30	2.000	No
1054	69.18	4.32	1.91	2.41	0.71	0.636	1.05	0.603	0.78	1.30	2.000	No
1055	69.24	4.32	1.91	2.41	0.71	0.636	1.05	0.603	0.76	1.30	2.000	No
1056	69.29	4.33	1.91	2.41	0.71	0.635	1.05	0.603	0.75	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
1057	69.37	4.33	1.91	2.42	0.71	0.635	1.05	0.602	0.75	1.30	2.000	No
1058	69.43	4.33	1.92	2.42	0.71	0.635	1.05	0.602	0.75	1.30	2.000	No
1059	69.51	4.34	1.92	2.42	0.71	0.635	1.05	0.602	0.75	1.30	2.000	No
1060	69.57	4.34	1.92	2.42	0.71	0.635	1.05	0.602	0.75	1.30	2.000	No
1061	69.63	4.35	1.92	2.42	0.71	0.634	1.05	0.602	0.75	1.30	2.000	No
1062	69.69	4.35	1.92	2.43	0.71	0.634	1.05	0.602	0.75	1.30	2.000	No
1063	69.76	4.36	1.93	2.43	0.71	0.634	1.05	0.601	0.75	1.30	2.000	No
1064	69.82	4.36	1.93	2.43	0.71	0.634	1.05	0.601	0.75	1.30	2.000	No
1065	69.91	4.37	1.93	2.43	0.71	0.634	1.05	0.601	0.75	1.30	2.000	No
1066	69.95	4.37	1.93	2.44	0.71	0.633	1.05	0.601	0.87	1.30	2.000	No
1067	70.02	4.37	1.94	2.44	0.71	0.633	1.05	0.601	0.79	1.30	2.000	No
1068	70.08	4.38	1.94	2.44	0.71	0.633	1.05	0.600	0.80	1.30	2.000	No
1069	70.16	4.38	1.94	2.44	0.70	0.633	1.05	0.600	0.80	1.30	2.000	No
1070	70.22	4.39	1.94	2.44	0.70	0.633	1.05	0.600	0.82	1.30	2.000	No
1071	70.28	4.39	1.94	2.45	0.70	0.632	1.05	0.600	0.83	1.30	2.000	No
1072	70.35	4.39	1.95	2.45	0.70	0.632	1.05	0.600	0.83	1.30	2.000	No
1073	70.42	4.40	1.95	2.45	0.70	0.632	1.05	0.599	0.83	1.30	2.000	No
1074	70.48	4.40	1.95	2.45	0.70	0.632	1.05	0.599	0.83	1.30	2.000	No
1075	70.55	4.41	1.95	2.45	0.70	0.632	1.05	0.599	0.83	1.30	2.000	No
1076	70.61	4.41	1.95	2.46	0.70	0.632	1.05	0.599	0.83	1.30	2.000	No
1077	70.69	4.41	1.96	2.46	0.70	0.631	1.05	0.599	0.82	1.30	2.000	No
1078	70.75	4.42	1.96	2.46	0.70	0.631	1.05	0.599	0.82	1.30	2.000	No
1079	70.82	4.42	1.96	2.46	0.70	0.631	1.05	0.598	0.82	1.30	2.000	No
1080	70.88	4.43	1.96	2.47	0.70	0.631	1.05	0.598	0.83	1.30	2.000	No
1081	70.95	4.43	1.96	2.47	0.70	0.631	1.05	0.598	0.83	1.30	2.000	No
1082	71.02	4.44	1.97	2.47	0.70	0.630	1.05	0.598	0.84	1.30	2.000	No
1083	71.08	4.44	1.97	2.47	0.70	0.630	1.05	0.598	0.85	1.30	2.000	No
1084	71.15	4.44	1.97	2.47	0.70	0.630	1.05	0.598	0.85	1.30	2.000	No
1085	71.22	4.45	1.97	2.48	0.70	0.630	1.05	0.597	0.85	1.30	2.000	No
1086	71.28	4.45	1.97	2.48	0.70	0.630	1.05	0.597	0.86	1.30	2.000	No
1087	71.35	4.46	1.98	2.48	0.70	0.629	1.05	0.597	0.86	1.30	2.000	No
1088	71.42	4.46	1.98	2.48	0.70	0.629	1.05	0.597	0.86	1.30	2.000	No
1089	71.49	4.46	1.98	2.48	0.70	0.629	1.05	0.597	0.85	1.30	2.000	No
1090	71.54	4.47	1.98	2.49	0.70	0.629	1.05	0.597	0.86	1.30	2.000	No
1091	71.59	4.47	1.98	2.49	0.70	0.629	1.05	0.596	0.86	1.30	2.000	No
1092	71.67	4.48	1.99	2.49	0.70	0.629	1.05	0.596	0.85	1.30	2.000	No
1093	71.73	4.48	1.99	2.49	0.70	0.628	1.05	0.596	0.84	1.30	2.000	No
1094	71.79	4.48	1.99	2.49	0.70	0.628	1.05	0.596	0.83	1.30	2.000	No
1095	71.86	4.49	1.99	2.49	0.70	0.628	1.05	0.596	0.83	1.30	2.000	No
1096	71.92	4.49	1.99	2.50	0.70	0.628	1.05	0.596	0.84	1.30	2.000	No
1097	71.99	4.50	2.00	2.50	0.70	0.628	1.05	0.595	0.84	1.30	2.000	No
1098	72.06	4.50	2.00	2.50	0.70	0.628	1.05	0.595	0.85	1.30	2.000	No
1099	72.12	4.50	2.00	2.50	0.70	0.627	1.05	0.595	0.86	1.30	2.000	No
1100	72.19	4.51	2.00	2.51	0.70	0.627	1.05	0.595	0.87	1.30	2.000	No
1101	72.26	4.51	2.00	2.51	0.70	0.627	1.05	0.595	0.87	1.30	2.000	No
1102	72.31	4.52	2.01	2.51	0.70	0.627	1.05	0.594	0.87	1.30	2.000	No
1103	72.38	4.52	2.01	2.51	0.70	0.627	1.05	0.594	0.86	1.30	2.000	No
1104	72.46	4.53	2.01	2.51	0.70	0.626	1.05	0.594	0.87	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1105	72.52	4.53	2.01	2.52	0.70	0.626	1.05	0.594	0.88	1.30	2.000	No
1106	72.59	4.53	2.02	2.52	0.69	0.626	1.05	0.594	0.87	1.30	2.000	No
1107	72.65	4.54	2.02	2.52	0.69	0.626	1.05	0.594	0.86	1.30	2.000	No
1108	72.71	4.54	2.02	2.52	0.69	0.626	1.05	0.593	0.85	1.30	2.000	No
1109	72.78	4.55	2.02	2.52	0.69	0.625	1.05	0.593	0.82	1.30	2.000	No
1110	72.84	4.55	2.02	2.53	0.69	0.625	1.05	0.593	0.82	1.30	2.000	No
1111	72.90	4.55	2.02	2.53	0.69	0.625	1.05	0.593	0.85	1.30	2.000	No
1112	72.98	4.56	2.03	2.53	0.69	0.625	1.05	0.593	0.85	1.30	2.000	No
1113	73.03	4.56	2.03	2.53	0.69	0.625	1.05	0.592	0.83	1.30	2.000	No
1114	73.11	4.57	2.03	2.54	0.69	0.625	1.05	0.592	0.83	1.30	2.000	No
1115	73.17	4.57	2.03	2.54	0.69	0.624	1.05	0.592	0.83	1.30	2.000	No
1116	73.23	4.57	2.04	2.54	0.69	0.624	1.05	0.592	0.82	1.30	2.000	No
1117	73.30	4.58	2.04	2.54	0.69	0.624	1.05	0.592	0.82	1.30	2.000	No
1118	73.36	4.58	2.04	2.54	0.69	0.624	1.05	0.592	0.81	1.30	2.000	No
1119	73.44	4.59	2.04	2.55	0.69	0.624	1.05	0.591	0.79	1.30	2.000	No
1120	73.51	4.59	2.04	2.55	0.69	0.623	1.05	0.591	0.78	1.30	2.000	No
1121	73.56	4.60	2.05	2.55	0.69	0.623	1.05	0.591	0.80	1.30	2.000	No
1122	73.63	4.60	2.05	2.55	0.69	0.623	1.05	0.591	0.80	1.30	2.000	No
1123	73.70	4.60	2.05	2.55	0.69	0.623	1.05	0.591	0.77	1.30	2.000	No
1124	73.76	4.61	2.05	2.56	0.69	0.623	1.05	0.590	0.75	1.30	2.000	No
1125	73.83	4.61	2.05	2.56	0.69	0.622	1.05	0.590	0.76	1.30	2.000	No
1126	73.89	4.62	2.06	2.56	0.69	0.622	1.05	0.590	0.79	1.30	2.000	No
1127	73.95	4.62	2.06	2.56	0.69	0.622	1.05	0.590	0.78	1.30	2.000	No
1128	74.02	4.63	2.06	2.57	0.69	0.622	1.05	0.590	0.74	1.30	2.000	No
1129	74.09	4.63	2.06	2.57	0.69	0.622	1.05	0.589	0.74	1.30	2.000	No
1130	74.16	4.63	2.06	2.57	0.69	0.621	1.05	0.589	0.77	1.30	2.000	No
1131	74.24	4.64	2.07	2.57	0.69	0.621	1.05	0.589	0.76	1.30	2.000	No
1132	74.31	4.64	2.07	2.57	0.69	0.621	1.05	0.589	0.78	1.30	2.000	No
1133	74.38	4.65	2.07	2.58	0.69	0.621	1.05	0.589	0.81	1.30	2.000	No
1134	74.41	4.65	2.07	2.58	0.69	0.621	1.05	0.589	0.82	1.30	2.000	No
1135	74.48	4.65	2.07	2.58	0.69	0.621	1.05	0.589	0.84	1.30	2.000	No
1136	74.55	4.66	2.08	2.58	0.69	0.620	1.05	0.588	0.85	1.30	2.000	No
1137	74.62	4.66	2.08	2.58	0.69	0.620	1.05	0.588	0.87	1.30	2.000	No
1138	74.68	4.67	2.08	2.59	0.69	0.620	1.05	0.588	0.86	1.30	2.000	No
1139	74.75	4.67	2.08	2.59	0.69	0.620	1.05	0.588	0.86	1.30	2.000	No
1140	74.82	4.68	2.08	2.59	0.69	0.620	1.05	0.588	0.85	1.30	2.000	No
1141	74.89	4.68	2.09	2.59	0.69	0.619	1.05	0.587	0.84	1.30	2.000	No
1142	74.94	4.68	2.09	2.59	0.69	0.619	1.05	0.587	0.84	1.30	2.000	No
1143	75.01	4.69	2.09	2.60	0.69	0.619	1.05	0.587	0.84	1.30	2.000	No
1144	75.07	4.69	2.09	2.60	0.68	0.619	1.05	0.587	0.86	1.30	2.000	No
1145	75.14	4.69	2.09	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1146	75.20	4.70	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1147	75.27	4.70	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1148	75.33	4.70	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1149	75.41	4.71	2.10	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No
1150	75.48	4.71	2.11	2.60	0.68	0.619	1.05	0.587	0.73	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR_{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.07	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
2	0.14	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
3	0.20	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
4	0.27	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
5	0.35	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
6	0.41	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
7	0.47	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
8	0.54	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
9	0.60	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
10	0.66	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
11	0.74	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
12	0.80	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
13	0.87	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
14	0.93	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
15	0.99	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
16	1.05	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
17	1.12	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
18	1.19	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
19	1.27	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
20	1.32	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
21	1.38	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
22	1.45	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
23	1.51	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
24	1.59	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
25	1.65	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
26	1.71	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
27	1.77	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
28	1.84	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
29	1.92	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
30	1.98	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
31	2.04	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
32	2.11	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
33	2.17	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
34	2.23	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
35	2.30	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
36	2.37	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
37	2.43	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
38	2.49	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
39	2.56	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
40	2.65	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
41	2.71	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
42	2.78	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
43	2.83	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
44	2.90	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
45	2.96	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
46	3.03	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
47	3.11	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
48	3.16	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	3.22	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
50	3.28	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
51	3.36	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
52	3.44	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
53	3.49	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
54	3.56	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
55	3.61	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
56	3.69	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
57	3.74	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
58	3.83	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
59	3.88	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
60	3.96	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
61	4.00	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
62	4.08	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
63	4.16	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
64	4.21	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
65	4.29	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
66	4.34	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
67	4.40	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
68	4.47	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
69	4.55	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
70	4.60	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
71	4.68	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
72	4.73	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
73	4.81	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
74	4.87	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
75	4.92	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
76	5.00	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
77	5.08	22.97	52.65	2.37	0.51	1.70	36.89	56.77	93.66	4.000	No	No	2.00
78	5.13	29.09	44.29	2.27	0.49	1.70	46.72	55.71	102.43	4.000	No	No	2.00
79	5.19	34.92	39.25	2.20	0.47	1.70	56.09	54.94	111.03	4.000	No	No	2.00
80	5.27	40.38	35.73	2.16	0.46	1.70	64.86	54.24	119.10	4.000	No	No	2.00
81	5.32	43.95	34.26	2.14	0.45	1.70	70.60	54.19	124.79	4.000	No	No	2.00
82	5.39	49.52	33.36	2.13	0.43	1.67	78.05	54.94	132.99	4.000	No	No	2.00
83	5.45	53.28	32.63	2.12	0.43	1.65	82.81	55.19	138.00	4.000	No	No	2.00
84	5.53	57.70	32.56	2.12	0.41	1.61	87.85	56.19	144.04	4.000	No	No	2.00
85	5.58	60.43	32.13	2.11	0.41	1.59	91.04	56.38	147.42	4.000	No	No	2.00
86	5.66	64.67	30.59	2.09	0.40	1.57	96.08	55.54	151.62	4.000	No	No	2.00
87	5.72	65.14	30.50	2.09	0.40	1.57	96.36	55.48	151.84	4.000	No	No	2.00
88	5.80	63.07	32.02	2.11	0.40	1.56	93.12	56.69	149.81	4.000	No	No	2.00
89	5.85	58.36	35.73	2.16	0.41	1.57	86.50	59.17	145.67	4.000	No	No	2.00
90	5.91	53.09	40.40	2.22	0.42	1.58	79.16	61.32	140.48	4.000	No	No	2.00
91	5.99	45.75	47.76	2.31	0.43	1.59	68.92	63.19	132.11	4.000	No	No	2.00
92	6.04	42.27	51.69	2.36	0.44	1.60	63.98	63.68	127.67	4.000	No	No	2.00
93	6.12	45.47	49.06	2.33	0.43	1.58	67.92	63.56	131.48	4.000	No	No	2.00
94	6.18	41.99	54.45	2.39	0.44	1.59	62.97	64.50	127.47	4.000	No	No	2.00
95	6.26	45.19	53.41	2.38	0.43	1.56	66.80	65.14	131.94	4.000	No	No	2.00
96	6.31	47.35	52.54	2.37	0.43	1.55	69.36	65.48	134.84	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	6.39	49.99	51.86	2.36	0.42	1.53	72.37	66.00	138.37	4.000	No	No	2.00
98	6.44	50.93	52.34	2.37	0.42	1.52	73.29	66.45	139.74	4.000	No	No	2.00
99	6.52	54.50	47.99	2.31	0.41	1.51	77.57	65.56	143.13	4.000	No	No	2.00
100	6.58	58.17	42.41	2.24	0.41	1.49	82.16	63.46	145.62	4.000	No	No	2.00
101	6.63	61.47	39.88	2.21	0.40	1.48	86.09	62.61	148.69	4.000	No	No	2.00
102	6.71	65.79	36.17	2.16	0.40	1.47	91.20	60.66	151.86	4.000	No	No	2.00
103	6.77	68.90	34.05	2.14	0.40	1.46	94.85	59.35	154.20	4.000	No	No	2.00
104	6.85	73.04	31.30	2.10	0.39	1.44	99.67	57.19	156.86	4.000	No	No	2.00
105	6.91	64.49	37.25	2.18	0.40	1.46	88.65	61.05	149.70	4.000	No	No	2.00
106	6.96	77.86	27.66	2.06	0.39	1.43	105.28	53.14	158.43	4.000	No	No	2.00
107	7.04	83.79	24.01	2.01	0.39	1.42	112.48	47.87	160.35	4.000	No	No	2.00
108	7.09	87.83	21.99	1.99	0.38	1.41	117.34	44.26	161.60	4.000	No	No	2.00
109	7.17	94.23	19.89	1.96	0.38	1.40	124.76	40.06	164.82	4.000	No	No	2.00
110	7.22	98.37	18.47	1.94	0.38	1.39	129.60	36.66	166.26	4.000	No	No	2.00
111	7.31	105.52	16.45	1.92	0.37	1.38	137.87	31.22	169.09	4.000	No	No	2.00
112	7.36	110.32	15.58	1.91	0.37	1.37	143.20	28.74	171.94	4.000	No	No	2.00
113	7.44	117.47	14.25	1.89	0.36	1.36	151.13	24.57	175.70	4.000	No	No	2.00
114	7.49	120.67	13.86	1.89	0.36	1.35	154.44	23.36	177.80	4.000	No	No	2.00
115	7.55	122.84	14.00	1.89	0.36	1.35	156.31	24.02	180.33	4.000	No	No	2.00
116	7.63	123.31	15.48	1.91	0.35	1.33	155.44	29.47	184.91	4.000	No	No	2.00
117	7.68	122.65	16.70	1.92	0.35	1.33	153.77	33.67	187.44	4.000	No	No	2.00
118	7.76	119.26	19.14	1.95	0.34	1.32	148.60	41.03	189.63	4.000	No	No	2.00
119	7.81	116.16	21.00	1.97	0.34	1.32	144.32	45.76	190.07	4.000	No	No	2.00
120	7.89	110.23	24.04	2.01	0.34	1.31	136.67	51.97	188.64	4.000	No	No	2.00
121	7.95	105.52	26.30	2.04	0.35	1.31	130.84	55.55	186.39	4.000	No	No	2.00
122	8.03	99.78	29.05	2.08	0.35	1.31	123.76	58.93	182.69	0.812	No	No	1.50
123	8.09	96.87	30.26	2.09	0.36	1.31	120.18	60.03	180.21	0.733	No	No	1.34
124	8.14	93.39	31.70	2.11	0.36	1.31	115.98	61.13	177.11	0.649	No	No	1.18
125	8.22	89.24	33.33	2.13	0.37	1.32	110.92	62.07	172.98	0.558	No	No	1.01
126	8.27	85.86	34.75	2.15	0.37	1.32	106.85	62.76	169.61	0.498	No	No	0.89
127	8.35	80.49	37.22	2.18	0.38	1.32	100.41	63.76	164.17	0.419	No	No	0.75
128	8.40	77.11	38.93	2.20	0.39	1.32	96.33	64.30	160.64	0.378	No	No	0.67
129	8.48	73.06	40.75	2.22	0.39	1.32	91.41	64.55	155.96	0.334	No	No	0.59
130	8.54	71.08	41.34	2.23	0.40	1.33	88.97	64.39	153.36	0.313	No	No	0.55
131	8.62	70.14	40.88	2.22	0.40	1.32	87.66	63.73	151.39	0.298	No	No	0.52
132	8.67	69.86	40.26	2.22	0.40	1.32	87.18	63.16	150.34	0.291	No	No	0.50
133	8.73	68.26	40.49	2.22	0.41	1.32	85.19	62.85	148.04	0.276	No	No	0.48
134	8.81	67.32	40.12	2.21	0.41	1.32	83.87	62.25	146.12	0.265	No	No	0.45
135	8.86	69.30	38.13	2.19	0.41	1.31	86.01	61.19	147.20	0.271	No	No	0.46
136	8.94	72.97	34.89	2.15	0.40	1.31	90.03	59.15	149.18	0.284	No	No	0.48
137	9.00	75.98	32.68	2.12	0.40	1.30	93.35	57.50	150.86	0.295	No	No	0.50
138	9.08	79.74	30.11	2.09	0.40	1.29	97.44	55.18	152.62	0.307	No	No	0.52
139	9.13	81.25	29.12	2.08	0.40	1.29	98.99	54.13	153.11	0.311	No	No	0.53
140	9.20	81.81	28.94	2.07	0.40	1.29	99.37	53.93	153.30	0.312	No	No	0.53
141	9.26	81.53	29.55	2.08	0.40	1.28	98.73	54.67	153.41	0.313	No	No	0.53
142	9.33	80.87	30.35	2.09	0.40	1.28	97.67	55.55	153.22	0.312	No	No	0.52
143	9.39	79.46	26.73	2.05	0.41	1.28	96.36	49.97	146.33	0.266	No	No	0.44
144	9.46	78.05	12.37	1.87	0.47	1.33	98.01	14.67	112.68	0.157	No	No	0.25

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	9.53	76.26	16.23	1.92	0.46	1.31	94.55	26.23	120.78	0.173	No	No	0.28
146	9.60	73.91	19.82	1.96	0.45	1.30	90.81	35.34	126.14	0.186	No	No	0.30
147	9.67	71.46	14.58	1.89	0.48	1.32	89.14	20.90	110.03	0.152	No	No	0.24
148	9.73	69.48	10.63	1.85	0.51	1.34	87.84	9.05	96.89	0.134	No	No	0.21
149	9.79	57.82	20.50	1.97	0.48	1.32	72.02	34.30	106.33	0.146	No	No	0.23
150	9.86	65.34	17.56	1.93	0.48	1.31	80.84	28.45	109.29	0.151	No	No	0.24
151	9.91	65.34	19.47	1.96	0.47	1.30	80.27	33.12	113.39	0.158	No	No	0.25
152	9.98	64.21	23.07	2.00	0.46	1.29	78.19	40.41	118.60	0.168	No	No	0.26
153	10.04	63.87	25.71	2.03	0.45	1.28	77.29	44.86	122.14	0.176	No	No	0.28
154	10.11	63.55	27.84	2.06	0.45	1.27	76.49	47.91	124.40	0.182	No	No	0.28
155	10.18	65.43	28.54	2.07	0.44	1.27	78.27	49.24	127.51	0.190	No	No	0.30
156	10.25	67.50	29.67	2.08	0.44	1.26	80.21	51.12	131.33	0.202	No	No	0.32
157	10.31	69.66	30.11	2.09	0.43	1.25	82.34	52.11	134.45	0.212	No	No	0.33
158	10.37	71.26	30.44	2.09	0.43	1.25	83.85	52.83	136.67	0.221	No	No	0.35
159	10.44	72.20	31.12	2.10	0.42	1.24	84.58	53.82	138.40	0.228	No	No	0.36
160	10.51	70.42	33.34	2.13	0.42	1.24	82.29	55.83	138.12	0.227	No	No	0.35
161	10.57	66.18	36.98	2.17	0.43	1.24	77.29	58.18	135.47	0.216	No	No	0.34
162	10.64	61.38	40.90	2.22	0.44	1.24	71.73	59.87	131.60	0.203	No	No	0.31
163	10.71	57.05	44.71	2.27	0.44	1.24	66.71	61.00	127.71	0.191	No	No	0.29
164	10.77	53.29	48.25	2.32	0.45	1.24	62.34	61.71	124.05	0.181	No	No	0.27
165	10.84	48.96	52.22	2.37	0.46	1.24	57.34	62.12	119.46	0.170	No	No	0.26
166	10.91	45.76	55.21	2.40	0.47	1.24	53.62	62.22	115.84	0.163	No	No	0.24
167	10.98	45.10	55.52	2.41	0.47	1.24	52.74	62.08	114.82	0.161	No	No	0.24
168	11.05	44.73	55.82	2.41	0.47	1.24	52.18	62.03	114.21	0.160	No	No	0.24
169	11.11	44.82	56.05	2.41	0.47	1.23	52.14	62.10	114.24	0.160	No	No	0.24
170	11.18	42.75	58.16	2.44	0.47	1.23	49.70	62.10	111.80	0.155	No	No	0.23
171	11.25	43.60	58.04	2.44	0.47	1.23	50.50	62.29	112.79	0.157	No	No	0.23
172	11.31	45.86	56.25	2.42	0.47	1.22	52.86	62.37	115.23	0.162	No	No	0.24
173	11.38	46.51	55.29	2.40	0.47	1.22	53.44	62.20	115.64	0.162	No	No	0.24
174	11.45	47.17	54.72	2.40	0.46	1.21	54.03	62.16	116.19	0.163	No	No	0.24
175	11.51	46.51	55.65	2.41	0.47	1.21	53.17	62.25	115.41	0.162	No	No	0.24
176	11.58	45.76	53.87	2.39	0.47	1.21	52.25	61.37	113.61	0.158	No	No	0.23
177	11.65	46.51	50.43	2.34	0.47	1.21	52.98	60.22	113.20	0.158	No	No	0.23
178	11.68	46.14	50.20	2.34	0.47	1.21	52.51	60.00	112.51	0.157	No	No	0.23
179	11.75	45.57	49.15	2.33	0.47	1.20	51.78	59.36	111.13	0.154	No	No	0.22
180	11.82	44.35	48.87	2.32	0.48	1.20	50.33	58.85	109.19	0.151	No	No	0.22
181	11.88	44.40	48.20	2.31	0.48	1.20	50.27	58.54	108.81	0.150	No	No	0.21
182	11.97	44.48	49.05	2.33	0.48	1.19	50.10	58.87	108.97	0.150	No	No	0.21
183	12.03	44.48	50.20	2.34	0.48	1.19	50.01	59.33	109.34	0.151	No	No	0.22
184	12.10	43.62	53.21	2.38	0.48	1.19	48.94	60.23	109.17	0.151	No	No	0.21
185	12.16	44.17	56.29	2.42	0.48	1.18	49.39	61.42	110.81	0.154	No	No	0.22
186	12.23	43.98	60.22	2.47	0.47	1.18	49.02	62.52	111.54	0.155	No	No	0.22
187	12.30	43.42	63.57	2.51	0.47	1.18	48.27	63.21	111.48	0.155	No	No	0.22
188	12.36	44.92	64.29	2.52	0.47	1.17	49.74	63.81	113.55	0.158	No	No	0.22
189	12.43	46.25	64.47	2.52	0.47	1.17	51.01	64.22	115.22	0.162	No	No	0.23
190	12.50	47.76	64.02	2.51	0.46	1.16	52.48	64.52	117.00	0.165	No	No	0.23
191	12.53	49.08	63.15	2.50	0.46	1.16	53.81	64.68	118.48	0.168	No	No	0.24
192	12.60	52.46	60.33	2.47	0.45	1.16	57.24	64.86	122.11	0.176	No	No	0.25

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	12.67	57.07	55.65	2.41	0.44	1.15	61.96	64.66	126.62	0.188	No	No	0.27
194	12.74	61.78	50.65	2.35	0.44	1.14	66.76	63.98	130.74	0.200	No	No	0.28
195	12.80	65.92	45.75	2.28	0.43	1.14	70.96	62.67	133.63	0.210	No	No	0.30
196	12.87	69.68	41.61	2.23	0.43	1.14	74.76	61.09	135.85	0.218	No	No	0.31
197	12.94	74.86	37.64	2.18	0.42	1.13	79.99	59.37	139.36	0.232	No	No	0.33
198	13.00	80.41	33.07	2.13	0.42	1.13	85.63	56.27	141.90	0.243	No	No	0.35
199	13.07	85.49	28.90	2.07	0.42	1.12	90.80	52.19	142.98	0.249	No	No	0.35
200	13.13	89.91	26.25	2.04	0.41	1.12	95.24	48.98	144.22	0.255	No	No	0.36
201	13.20	92.74	25.27	2.03	0.41	1.12	97.97	47.78	145.75	0.263	No	No	0.37
202	13.27	95.00	24.05	2.01	0.41	1.12	100.12	45.89	146.01	0.265	No	No	0.38
203	13.34	98.29	23.24	2.00	0.41	1.11	103.28	44.79	148.07	0.277	No	No	0.39
204	13.40	101.02	23.66	2.01	0.40	1.11	105.76	46.04	151.81	0.301	No	No	0.43
205	13.47	103.37	23.90	2.01	0.40	1.10	107.88	46.88	154.76	0.324	No	No	0.46
206	13.54	105.72	23.74	2.01	0.39	1.10	110.02	46.91	156.93	0.342	No	No	0.49
207	13.60	107.89	23.57	2.01	0.39	1.10	111.97	46.89	158.86	0.360	No	No	0.52
208	13.67	110.33	23.31	2.00	0.39	1.10	114.19	46.69	160.88	0.381	No	No	0.55
209	13.74	112.78	22.83	2.00	0.38	1.09	116.43	46.02	162.45	0.398	No	No	0.57
210	13.80	115.89	22.49	1.99	0.38	1.09	119.31	45.71	165.02	0.430	No	No	0.62
211	13.87	118.99	22.31	1.99	0.38	1.09	122.15	45.73	167.88	0.470	No	No	0.68
212	13.94	121.62	21.90	1.99	0.37	1.08	124.55	45.14	169.68	0.499	No	No	0.72
213	14.00	123.79	21.35	1.98	0.37	1.08	126.50	44.09	170.59	0.514	No	No	0.74
214	14.07	125.29	19.06	1.95	0.38	1.08	127.97	38.18	166.15	0.445	No	No	0.64
215	14.14	126.14	17.66	1.93	0.38	1.08	128.73	34.11	162.84	0.403	No	No	0.57
216	14.21	126.80	17.81	1.94	0.38	1.08	129.12	34.61	163.73	0.414	No	No	0.59
217	14.24	126.80	18.07	1.94	0.38	1.08	128.97	35.39	164.36	0.422	No	No	0.60
218	14.31	127.08	18.65	1.95	0.38	1.07	128.95	37.12	166.06	0.444	No	No	0.63
219	14.37	124.35	19.74	1.96	0.38	1.07	125.97	39.80	165.77	0.440	No	No	0.62
220	14.46	125.77	19.26	1.95	0.38	1.07	127.12	38.63	165.75	0.440	No	No	0.62
221	14.52	125.58	19.79	1.96	0.38	1.07	126.67	40.04	166.71	0.453	No	No	0.64
222	14.59	124.92	20.95	1.97	0.37	1.07	125.71	42.96	168.68	0.482	No	No	0.68
223	14.65	123.88	22.29	1.99	0.37	1.06	124.40	46.04	170.44	0.511	No	No	0.72
224	14.72	122.85	23.30	2.00	0.37	1.06	123.13	48.12	171.25	0.526	No	No	0.74
225	14.79	122.00	24.26	2.02	0.37	1.06	122.04	49.98	172.02	0.540	No	No	0.76
226	14.85	121.25	24.69	2.02	0.37	1.06	121.08	50.70	171.78	0.535	No	No	0.75
227	14.92	120.40	25.20	2.03	0.37	1.06	120.03	51.52	171.55	0.531	No	No	0.75
228	14.99	120.03	25.73	2.03	0.37	1.05	119.45	52.42	171.87	0.537	No	No	0.75
229	15.05	119.46	26.26	2.04	0.37	1.05	118.67	53.27	171.94	0.538	No	No	0.76
230	15.12	119.37	26.17	2.04	0.37	1.05	118.39	53.05	171.44	0.529	No	No	0.74
231	15.19	119.08	26.12	2.04	0.37	1.05	117.91	52.87	170.79	0.518	No	No	0.72
232	15.22	119.18	26.04	2.04	0.37	1.05	117.92	52.72	170.64	0.515	No	No	0.72
233	15.29	118.90	26.04	2.04	0.37	1.05	117.45	52.64	170.08	0.505	No	No	0.70
234	15.36	118.05	26.12	2.04	0.37	1.04	116.44	52.61	169.04	0.488	No	No	0.68
235	15.43	117.11	26.32	2.04	0.37	1.04	115.33	52.77	168.10	0.474	No	No	0.65
236	15.49	115.98	26.64	2.05	0.38	1.04	114.04	53.09	167.13	0.459	No	No	0.63
237	15.56	114.19	27.07	2.05	0.38	1.04	112.12	53.47	165.59	0.438	No	No	0.60
238	15.63	112.31	27.29	2.05	0.38	1.04	110.12	53.46	163.58	0.412	No	No	0.56
239	15.69	109.30	27.87	2.06	0.39	1.04	107.03	53.81	160.85	0.381	No	No	0.52
240	15.76	104.03	29.48	2.08	0.39	1.04	101.76	55.19	156.95	0.342	No	No	0.46

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	15.82	97.63	32.31	2.12	0.40	1.03	95.38	57.52	152.90	0.309	No	No	0.41
242	15.89	90.38	36.02	2.16	0.41	1.03	88.20	59.82	148.02	0.276	No	No	0.37
243	15.96	82.29	40.19	2.21	0.42	1.03	80.22	61.42	141.65	0.242	No	No	0.32
244	16.03	72.88	46.04	2.29	0.43	1.03	70.98	62.83	133.81	0.210	No	No	0.27
245	16.10	63.75	52.44	2.37	0.45	1.03	62.03	63.47	125.50	0.185	No	No	0.24
246	16.16	54.16	60.53	2.47	0.46	1.03	52.66	63.63	116.29	0.164	No	No	0.21
247	16.23	45.78	68.89	2.57	0.48	1.03	44.46	63.34	107.80	0.149	No	No	0.19
248	16.30	41.26	74.38	2.64	0.49	1.03	40.01	0.00	40.01	4.000	No	Yes	2.00
249	16.36	38.63	77.88	2.69	0.50	1.03	37.39	0.00	37.39	4.000	No	Yes	2.00
250	16.43	37.31	79.62	2.71	0.50	1.02	36.04	0.00	36.04	4.000	No	Yes	2.00
251	16.50	37.31	80.03	2.71	0.50	1.02	35.97	0.00	35.97	4.000	No	Yes	2.00
252	16.56	37.31	70.63	2.60	0.50	1.02	35.90	61.20	97.10	0.134	No	No	0.17
253	16.63	38.35	67.88	2.56	0.50	1.02	36.83	60.92	97.75	0.135	No	No	0.17
254	16.70	38.44	71.68	2.61	0.50	1.02	36.84	0.00	36.84	4.000	No	Yes	2.00
255	16.73	38.91	72.88	2.62	0.50	1.01	37.25	0.00	37.25	4.000	No	Yes	2.00
256	16.80	40.61	74.31	2.64	0.49	1.01	38.80	0.00	38.80	4.000	No	Yes	2.00
257	16.87	43.15	74.56	2.64	0.49	1.01	41.14	0.00	41.14	4.000	No	Yes	2.00
258	16.94	45.69	74.20	2.64	0.48	1.01	43.47	0.00	43.47	4.000	No	Yes	2.00
259	17.00	54.64	66.95	2.55	0.46	1.01	51.88	65.06	116.94	0.165	No	No	0.21
260	17.08	62.26	62.33	2.49	0.45	1.00	58.98	65.92	124.91	0.183	No	No	0.23
261	17.14	68.19	58.79	2.45	0.44	1.00	64.50	66.42	130.92	0.200	No	No	0.25
262	17.20	75.53	54.15	2.39	0.42	1.00	71.33	66.66	137.99	0.226	No	No	0.29
263	17.27	83.34	49.67	2.33	0.41	1.00	78.58	66.66	145.24	0.260	No	No	0.33
264	17.34	90.39	46.00	2.29	0.40	1.00	85.10	66.43	151.53	0.299	No	No	0.39
265	17.40	95.10	43.78	2.26	0.39	1.00	89.41	66.17	155.58	0.330	No	No	0.43
266	17.47	98.67	42.35	2.24	0.39	0.99	92.63	66.01	158.64	0.358	No	No	0.47
267	17.53	102.53	40.90	2.22	0.38	0.99	96.11	65.81	161.93	0.392	No	No	0.51
268	17.60	105.73	39.81	2.21	0.38	0.99	98.97	65.65	164.63	0.425	No	No	0.55
269	17.67	107.90	39.24	2.20	0.38	0.99	100.86	65.64	166.50	0.450	No	No	0.59
270	17.73	109.12	39.23	2.20	0.38	0.99	101.86	65.87	167.73	0.468	No	No	0.61
271	17.80	109.03	40.01	2.21	0.37	0.99	101.62	66.45	168.07	0.473	No	No	0.62
272	17.87	108.56	40.88	2.22	0.37	0.99	101.03	66.99	168.03	0.472	No	No	0.62
273	17.93	107.24	41.91	2.24	0.38	0.98	99.65	67.44	167.09	0.459	No	No	0.60
274	18.00	105.45	42.85	2.25	0.38	0.98	97.83	67.65	165.48	0.436	No	No	0.57
275	18.07	102.72	43.78	2.26	0.38	0.98	95.13	67.60	162.74	0.402	No	No	0.52
276	18.14	98.49	45.63	2.28	0.39	0.98	91.04	67.74	158.78	0.359	No	No	0.46
277	18.20	92.74	48.18	2.31	0.40	0.98	85.56	67.75	153.31	0.312	No	No	0.40
278	18.27	85.96	51.24	2.35	0.41	0.97	79.13	67.54	146.67	0.268	No	No	0.34
279	18.34	78.72	54.70	2.40	0.42	0.97	72.29	67.13	139.42	0.232	No	No	0.29
280	18.37	74.95	56.62	2.42	0.43	0.97	68.74	66.86	135.60	0.217	No	No	0.27
281	18.44	67.80	60.42	2.47	0.44	0.97	62.02	66.23	128.24	0.192	No	No	0.24
282	18.51	59.71	65.52	2.53	0.46	0.97	54.46	65.46	119.92	0.171	No	No	0.21
283	18.57	50.58	73.28	2.63	0.48	0.96	45.97	0.00	45.97	4.000	No	Yes	2.00
284	18.64	43.71	79.70	2.71	0.49	0.96	39.60	0.00	39.60	4.000	No	Yes	2.00
285	18.71	38.82	84.79	2.77	0.50	0.96	35.07	0.00	35.07	4.000	No	Yes	2.00
286	18.78	36.56	86.55	2.79	0.51	0.95	32.95	0.00	32.95	4.000	No	Yes	2.00
287	18.84	34.40	88.16	2.81	0.51	0.95	30.93	0.00	30.93	4.000	No	Yes	2.00
288	18.91	30.07	93.88	2.89	0.52	0.95	26.95	0.00	26.95	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	18.98	27.15	98.06	2.94	0.53	0.95	24.27	0.00	24.27	4.000	No	Yes	2.00
290	19.04	25.17	100.00	2.97	0.54	0.95	22.44	0.00	22.44	4.000	No	Yes	2.00
291	19.11	23.67	100.00	3.00	0.54	0.94	21.05	0.00	21.05	4.000	No	Yes	2.00
292	19.18	22.26	100.00	3.03	0.55	0.94	19.75	0.00	19.75	4.000	No	Yes	2.00
293	19.24	21.13	100.00	3.01	0.55	0.94	18.70	0.00	18.70	4.000	No	Yes	2.00
294	19.31	21.13	92.07	2.86	0.55	0.94	18.66	0.00	18.66	4.000	No	Yes	2.00
295	19.38	21.13	93.92	2.89	0.55	0.94	18.63	0.00	18.63	4.000	No	Yes	2.00
296	19.44	21.13	95.73	2.91	0.55	0.93	18.60	0.00	18.60	4.000	No	Yes	2.00
297	19.51	22.54	94.36	2.89	0.55	0.93	19.82	0.00	19.82	4.000	No	Yes	2.00
298	19.58	24.52	90.91	2.85	0.54	0.93	21.53	0.00	21.53	4.000	No	Yes	2.00
299	19.63	26.96	86.13	2.79	0.54	0.93	23.67	0.00	23.67	4.000	No	Yes	2.00
300	19.69	34.40	73.58	2.63	0.52	0.93	30.23	0.00	30.23	4.000	No	Yes	2.00
301	19.76	38.82	67.44	2.56	0.51	0.93	34.11	60.04	94.15	0.130	No	No	0.15
302	19.82	40.14	66.18	2.54	0.51	0.93	35.23	60.09	95.32	0.132	No	No	0.16
303	19.89	39.01	68.99	2.57	0.51	0.93	34.17	60.37	94.54	0.131	No	No	0.15
304	19.95	36.75	72.98	2.62	0.51	0.93	32.11	0.00	32.11	4.000	No	Yes	2.00
305	20.02	27.62	88.32	2.82	0.54	0.92	24.01	0.00	24.01	4.000	No	Yes	2.00
306	20.09	29.86	84.59	2.77	0.53	0.92	25.95	0.00	25.95	4.000	No	Yes	2.00
307	20.16	27.13	90.13	2.84	0.54	0.92	23.51	0.00	23.51	4.000	No	Yes	2.00
308	20.23	26.58	92.09	2.86	0.54	0.92	22.98	0.00	22.98	4.000	No	Yes	2.00
309	20.29	26.75	92.75	2.87	0.54	0.91	23.10	0.00	23.10	4.000	No	Yes	2.00
310	20.36	26.67	93.88	2.89	0.54	0.91	22.98	0.00	22.98	4.000	No	Yes	2.00
311	20.42	27.52	93.34	2.88	0.54	0.91	23.69	0.00	23.69	4.000	No	Yes	2.00
312	20.49	29.30	91.25	2.85	0.53	0.91	25.20	0.00	25.20	4.000	No	Yes	2.00
313	20.56	31.56	88.38	2.82	0.53	0.91	27.12	0.00	27.12	4.000	No	Yes	2.00
314	20.63	34.76	84.12	2.76	0.52	0.91	29.86	0.00	29.86	4.000	No	Yes	2.00
315	20.69	38.43	79.29	2.70	0.51	0.91	33.02	0.00	33.02	4.000	No	Yes	2.00
316	20.76	42.29	74.39	2.64	0.50	0.91	36.33	0.00	36.33	4.000	No	Yes	2.00
317	20.83	45.58	70.51	2.59	0.50	0.91	39.14	62.12	101.26	0.139	No	No	0.16
318	20.89	46.62	69.40	2.58	0.49	0.91	39.99	62.15	102.13	0.140	No	No	0.16
319	20.96	46.05	69.99	2.59	0.49	0.91	39.43	62.10	101.53	0.139	No	No	0.16
320	21.03	43.33	72.48	2.62	0.50	0.90	36.99	0.00	36.99	4.000	No	Yes	2.00
321	21.09	39.00	77.19	2.68	0.51	0.90	33.18	0.00	33.18	4.000	No	Yes	2.00
322	21.16	35.42	80.57	2.72	0.52	0.90	30.03	0.00	30.03	4.000	No	Yes	2.00
323	21.23	33.16	80.22	2.72	0.52	0.90	28.03	0.00	28.03	4.000	No	Yes	2.00
324	21.26	31.85	81.25	2.73	0.53	0.89	26.88	0.00	26.88	4.000	No	Yes	2.00
325	21.33	29.40	86.96	2.80	0.53	0.89	24.74	0.00	24.74	4.000	No	Yes	2.00
326	21.40	28.74	89.48	2.83	0.53	0.89	24.14	0.00	24.14	4.000	No	Yes	2.00
327	21.46	29.02	89.93	2.84	0.53	0.89	24.34	0.00	24.34	4.000	No	Yes	2.00
328	21.53	23.09	100.00	3.00	0.55	0.88	19.27	0.00	19.27	4.000	No	Yes	2.00
329	21.60	30.53	89.96	2.84	0.53	0.89	25.55	0.00	25.55	4.000	No	Yes	2.00
330	21.66	30.90	91.13	2.85	0.53	0.89	25.82	0.00	25.82	4.000	No	Yes	2.00
331	21.73	31.37	91.91	2.86	0.53	0.88	26.18	0.00	26.18	4.000	No	Yes	2.00
332	21.80	32.41	91.33	2.85	0.52	0.88	27.03	0.00	27.03	4.000	No	Yes	2.00
333	21.86	34.29	89.43	2.83	0.52	0.88	28.58	0.00	28.58	4.000	No	Yes	2.00
334	21.93	35.80	88.29	2.82	0.52	0.88	29.82	0.00	29.82	4.000	No	Yes	2.00
335	22.00	37.40	87.02	2.80	0.51	0.88	31.13	0.00	31.13	4.000	No	Yes	2.00
336	22.06	39.47	85.53	2.78	0.51	0.88	32.85	0.00	32.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	22.13	41.91	83.99	2.76	0.50	0.88	34.87	0.00	34.87	4.000	No	Yes	2.00
338	22.19	45.50	81.14	2.73	0.50	0.88	37.87	0.00	37.87	4.000	No	Yes	2.00
339	22.26	50.20	77.12	2.68	0.49	0.88	41.83	0.00	41.83	4.000	No	Yes	2.00
340	22.33	53.69	74.57	2.64	0.48	0.88	44.75	0.00	44.75	4.000	No	Yes	2.00
341	22.40	55.76	73.78	2.63	0.47	0.88	46.46	0.00	46.46	4.000	No	Yes	2.00
342	22.46	57.07	73.95	2.64	0.47	0.88	47.52	0.00	47.52	4.000	No	Yes	2.00
343	22.53	59.43	72.91	2.62	0.47	0.88	49.48	0.00	49.48	4.000	No	Yes	2.00
344	22.60	62.44	70.44	2.59	0.46	0.88	51.99	65.86	117.85	0.167	No	No	0.19
345	22.66	65.35	67.32	2.55	0.46	0.88	54.41	65.88	120.29	0.172	No	No	0.20
346	22.73	67.14	64.48	2.52	0.45	0.88	55.86	65.61	121.47	0.175	No	No	0.20
347	22.80	70.62	61.13	2.48	0.45	0.88	58.77	65.52	124.29	0.182	No	No	0.21
348	22.86	76.74	57.01	2.43	0.44	0.88	63.96	65.68	129.64	0.197	No	No	0.23
349	22.93	84.55	51.82	2.36	0.43	0.88	70.61	65.51	136.13	0.219	No	No	0.26
350	23.00	90.76	40.47	2.22	0.43	0.88	75.71	60.54	136.25	0.219	No	No	0.26
351	23.03	92.92	36.23	2.17	0.43	0.88	77.42	57.55	134.97	0.214	No	No	0.25
352	23.10	94.05	35.89	2.16	0.43	0.88	78.29	57.45	135.74	0.217	No	No	0.25
353	23.17	93.77	36.80	2.17	0.43	0.88	77.97	58.18	136.15	0.219	No	No	0.25
354	23.24	95.75	36.55	2.17	0.42	0.88	79.59	58.34	137.93	0.226	No	No	0.26
355	23.30	99.89	35.88	2.16	0.42	0.88	83.10	58.53	141.63	0.242	No	No	0.28
356	23.37	94.05	40.83	2.22	0.42	0.88	78.05	61.36	139.40	0.232	No	No	0.27
357	23.43	106.00	36.20	2.16	0.41	0.88	88.28	60.01	148.29	0.278	No	No	0.33
358	23.50	107.60	36.96	2.17	0.40	0.88	89.61	61.01	150.62	0.293	No	No	0.34
359	23.56	105.91	38.95	2.20	0.40	0.88	88.09	62.35	150.45	0.292	No	No	0.34
360	23.63	104.50	40.56	2.22	0.40	0.88	86.80	63.29	150.09	0.289	No	No	0.34
361	23.70	105.63	40.61	2.22	0.40	0.88	87.69	63.54	151.23	0.297	No	No	0.35
362	23.76	111.65	38.14	2.19	0.39	0.88	92.79	62.79	155.59	0.331	No	No	0.39
363	23.83	117.30	35.67	2.16	0.39	0.88	97.56	61.62	159.18	0.363	No	No	0.43
364	23.90	120.59	33.60	2.13	0.39	0.88	100.24	60.04	160.29	0.375	No	No	0.44
365	23.96	120.12	33.19	2.13	0.39	0.88	99.68	59.46	159.14	0.363	No	No	0.43
366	24.03	115.89	34.33	2.14	0.39	0.88	95.89	59.87	155.76	0.332	No	No	0.39
367	24.10	107.04	37.66	2.18	0.40	0.87	88.15	61.29	149.44	0.285	No	No	0.33
368	24.17	95.47	43.05	2.25	0.42	0.87	78.15	62.88	141.03	0.239	No	No	0.28
369	24.23	83.23	49.74	2.33	0.44	0.86	67.65	63.81	131.46	0.202	No	No	0.23
370	24.30	69.95	58.27	2.44	0.46	0.85	56.38	63.99	120.38	0.172	No	No	0.20
371	24.37	56.69	68.97	2.57	0.48	0.85	45.27	63.59	108.86	0.150	No	No	0.17
372	24.43	44.64	81.24	2.73	0.50	0.84	35.30	0.00	35.30	4.000	No	Yes	2.00
373	24.50	35.80	91.41	2.86	0.52	0.83	28.07	0.00	28.07	4.000	No	Yes	2.00
374	24.57	30.25	97.92	2.94	0.53	0.83	23.57	0.00	23.57	4.000	No	Yes	2.00
375	24.63	27.14	100.00	2.98	0.54	0.82	21.06	0.00	21.06	4.000	No	Yes	2.00
376	24.70	26.76	98.14	2.94	0.54	0.82	20.72	0.00	20.72	4.000	No	Yes	2.00
377	24.77	25.92	97.19	2.93	0.55	0.82	20.02	0.00	20.02	4.000	No	Yes	2.00
378	24.84	27.80	93.54	2.88	0.54	0.82	21.48	0.00	21.48	4.000	No	Yes	2.00
379	24.87	30.44	89.61	2.83	0.54	0.82	23.55	0.00	23.55	4.000	No	Yes	2.00
380	24.94	38.25	80.15	2.71	0.52	0.82	29.74	0.00	29.74	4.000	No	Yes	2.00
381	25.01	51.24	68.81	2.57	0.49	0.83	40.19	62.08	102.28	0.140	No	No	0.16
382	25.07	65.07	60.57	2.47	0.47	0.84	51.49	63.31	114.81	0.161	No	No	0.18
383	25.14	73.54	57.79	2.43	0.45	0.84	58.47	64.42	122.90	0.178	No	No	0.20
384	25.21	86.24	52.29	2.37	0.43	0.85	69.05	65.29	134.34	0.212	No	No	0.24

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	25.28	96.59	48.82	2.32	0.41	0.85	77.74	66.02	143.76	0.253	No	No	0.29
386	25.34	107.23	45.06	2.28	0.40	0.86	86.72	66.29	153.01	0.310	No	No	0.36
387	25.41	117.30	41.00	2.22	0.39	0.86	95.23	65.67	160.90	0.381	No	No	0.44
388	25.48	121.62	37.72	2.18	0.38	0.86	98.73	63.82	162.55	0.400	No	No	0.46
389	25.54	119.37	34.63	2.15	0.39	0.86	96.46	60.32	156.78	0.341	No	No	0.39
390	25.61	111.93	38.56	2.19	0.40	0.85	90.11	62.51	152.62	0.307	No	No	0.35
391	25.68	103.75	42.81	2.25	0.41	0.85	83.12	63.96	147.08	0.271	No	No	0.31
392	25.75	94.34	48.14	2.31	0.42	0.84	75.14	65.01	140.14	0.235	No	No	0.27
393	25.81	84.27	54.19	2.39	0.43	0.84	66.65	65.40	132.05	0.204	No	No	0.23
394	25.87	67.42	65.44	2.53	0.46	0.83	52.68	64.93	117.61	0.166	No	No	0.19
395	25.93	64.04	66.77	2.55	0.47	0.82	49.84	64.43	114.27	0.160	No	No	0.18
396	26.00	52.37	75.71	2.66	0.49	0.82	40.32	0.00	40.32	4.000	No	Yes	2.00
397	26.06	44.75	83.35	2.75	0.50	0.81	34.20	0.00	34.20	4.000	No	Yes	2.00
398	26.13	40.32	88.53	2.82	0.51	0.81	30.65	0.00	30.65	4.000	No	Yes	2.00
399	26.20	37.78	91.03	2.85	0.52	0.80	28.61	0.00	28.61	4.000	No	Yes	2.00
400	26.27	37.41	90.88	2.85	0.52	0.80	28.28	0.00	28.28	4.000	No	Yes	2.00
401	26.33	37.97	89.53	2.83	0.52	0.80	28.68	0.00	28.68	4.000	No	Yes	2.00
402	26.40	35.43	92.97	2.87	0.53	0.80	26.66	0.00	26.66	4.000	No	Yes	2.00
403	26.47	32.42	97.37	2.93	0.53	0.79	24.29	0.00	24.29	4.000	No	Yes	2.00
404	26.53	30.16	100.00	2.97	0.54	0.79	22.51	0.00	22.51	4.000	No	Yes	2.00
405	26.60	30.16	99.77	2.96	0.54	0.79	22.48	0.00	22.48	4.000	No	Yes	2.00
406	26.66	30.16	99.22	2.95	0.54	0.79	22.45	0.00	22.45	4.000	No	Yes	2.00
407	26.73	30.16	100.00	2.96	0.54	0.79	22.42	0.00	22.42	4.000	No	Yes	2.00
408	26.80	31.20	98.11	2.94	0.54	0.79	23.19	0.00	23.19	4.000	No	Yes	2.00
409	26.86	31.95	98.65	2.95	0.53	0.79	23.73	0.00	23.73	4.000	No	Yes	2.00
410	26.93	37.41	91.95	2.86	0.52	0.79	27.91	0.00	27.91	4.000	No	Yes	2.00
411	27.00	47.85	80.09	2.71	0.50	0.80	36.00	0.00	36.00	4.000	No	Yes	2.00
412	27.06	58.67	69.87	2.59	0.48	0.80	44.50	63.55	108.05	0.149	No	No	0.17
413	27.13	69.40	61.30	2.48	0.46	0.81	53.01	63.95	116.96	0.165	No	No	0.18
414	27.17	72.41	59.29	2.45	0.46	0.81	55.41	64.04	119.44	0.170	No	No	0.19
415	27.23	72.79	59.60	2.46	0.46	0.81	55.65	64.20	119.85	0.171	No	No	0.19
416	27.30	68.93	62.82	2.50	0.46	0.81	52.49	64.21	116.70	0.164	No	No	0.18
417	27.37	63.38	67.20	2.55	0.47	0.80	47.99	64.00	111.99	0.156	No	No	0.17
418	27.43	57.17	71.80	2.61	0.48	0.80	43.01	0.00	43.01	4.000	No	Yes	2.00
419	27.50	50.11	77.56	2.68	0.50	0.79	37.40	0.00	37.40	4.000	No	Yes	2.00
420	27.57	44.37	83.61	2.76	0.51	0.79	32.91	0.00	32.91	4.000	No	Yes	2.00
421	27.64	44.32	84.21	2.77	0.51	0.78	32.83	0.00	32.83	4.000	No	Yes	2.00
422	27.70	44.32	85.19	2.78	0.51	0.78	32.79	0.00	32.79	4.000	No	Yes	2.00
423	27.77	44.28	83.64	2.76	0.51	0.78	32.71	0.00	32.71	4.000	No	Yes	2.00
424	27.84	48.51	76.07	2.66	0.50	0.78	35.91	0.00	35.91	4.000	No	Yes	2.00
425	27.91	55.00	69.04	2.58	0.49	0.79	40.88	62.33	103.21	0.142	No	No	0.16
426	27.98	61.31	63.25	2.50	0.48	0.79	45.77	62.42	108.18	0.149	No	No	0.16
427	28.04	68.46	57.38	2.43	0.47	0.79	51.33	62.31	113.64	0.159	No	No	0.18
428	28.09	67.89	58.23	2.44	0.47	0.79	50.84	62.44	113.28	0.158	No	No	0.17
429	28.16	83.70	47.75	2.31	0.45	0.80	63.34	61.73	125.07	0.184	No	No	0.20
430	28.22	90.38	43.83	2.26	0.44	0.80	68.60	60.97	129.57	0.196	No	No	0.22
431	28.28	95.94	40.74	2.22	0.43	0.81	72.98	60.06	133.05	0.208	No	No	0.23
432	28.35	99.79	39.01	2.20	0.43	0.81	76.00	59.52	135.53	0.216	No	No	0.24

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	28.42	103.37	38.02	2.19	0.42	0.81	78.84	59.41	138.24	0.227	No	No	0.25
434	28.49	106.48	37.37	2.18	0.42	0.81	81.30	59.44	140.75	0.238	No	No	0.27
435	28.55	109.30	36.78	2.17	0.42	0.81	83.54	59.45	142.99	0.249	No	No	0.28
436	28.62	112.40	36.47	2.17	0.41	0.81	86.03	59.74	145.77	0.263	No	No	0.29
437	28.69	115.32	36.46	2.17	0.41	0.81	88.39	60.28	148.67	0.280	No	No	0.31
438	28.75	117.58	36.74	2.17	0.40	0.81	90.23	60.96	151.19	0.297	No	No	0.33
439	28.82	119.37	37.19	2.18	0.40	0.81	91.68	61.70	153.38	0.313	No	No	0.35
440	28.89	120.87	37.48	2.18	0.40	0.81	92.88	62.24	155.11	0.327	No	No	0.37
441	28.95	122.00	37.75	2.18	0.39	0.81	93.76	62.69	156.45	0.338	No	No	0.38
442	29.02	123.04	37.81	2.19	0.39	0.81	94.55	62.92	157.47	0.347	No	No	0.39
443	29.09	123.13	38.10	2.19	0.39	0.81	94.55	63.17	157.72	0.349	No	No	0.39
444	29.16	121.15	39.37	2.20	0.39	0.81	92.86	63.83	156.69	0.340	No	No	0.38
445	29.22	116.07	41.45	2.23	0.40	0.81	88.61	64.38	152.99	0.310	No	No	0.35
446	29.29	109.86	43.98	2.26	0.41	0.80	83.44	64.79	148.23	0.278	No	No	0.31
447	29.35	102.52	47.06	2.30	0.42	0.80	77.38	65.03	142.41	0.246	No	No	0.27
448	29.42	94.81	50.66	2.35	0.43	0.79	71.08	65.13	136.21	0.219	No	No	0.24
449	29.49	85.21	56.35	2.42	0.44	0.79	63.35	65.29	128.63	0.194	No	No	0.21
450	29.55	74.39	63.64	2.51	0.46	0.78	54.75	65.07	119.82	0.171	No	No	0.19
451	29.62	61.12	73.87	2.64	0.48	0.77	44.38	0.00	44.38	4.000	No	Yes	2.00
452	29.69	48.51	84.46	2.77	0.50	0.76	34.73	0.00	34.73	4.000	No	Yes	2.00
453	29.76	39.38	93.87	2.89	0.52	0.75	27.87	0.00	27.87	4.000	No	Yes	2.00
454	29.82	32.61	100.00	2.99	0.54	0.74	22.86	0.00	22.86	4.000	No	Yes	2.00
455	29.86	29.50	100.00	3.04	0.54	0.74	20.57	0.00	20.57	4.000	No	Yes	2.00
456	29.92	24.42	100.00	3.13	0.56	0.73	16.88	0.00	16.88	4.000	No	Yes	2.00
457	30.00	19.52	100.00	3.24	0.57	0.73	13.38	0.00	13.38	4.000	No	Yes	2.00
458	30.06	20.27	100.00	3.19	0.57	0.73	13.90	0.00	13.90	4.000	No	Yes	2.00
459	30.13	18.86	100.00	3.21	0.57	0.72	12.88	0.00	12.88	4.000	No	Yes	2.00
460	30.20	18.30	100.00	3.20	0.57	0.72	12.47	0.00	12.47	4.000	No	Yes	2.00
461	30.27	18.11	100.00	3.18	0.57	0.72	12.33	0.00	12.33	4.000	No	Yes	2.00
462	30.34	18.01	100.00	3.16	0.57	0.72	12.24	0.00	12.24	4.000	No	Yes	2.00
463	30.40	17.35	100.00	3.16	0.58	0.72	11.77	0.00	11.77	4.000	No	Yes	2.00
464	30.47	17.17	100.00	3.16	0.58	0.72	11.63	0.00	11.63	4.000	No	Yes	2.00
465	30.54	17.26	100.00	3.15	0.58	0.72	11.67	0.00	11.67	4.000	No	Yes	2.00
466	30.61	17.54	100.00	3.14	0.58	0.72	11.85	0.00	11.85	4.000	No	Yes	2.00
467	30.67	17.65	100.00	3.13	0.57	0.72	11.91	0.00	11.91	4.000	No	Yes	2.00
468	30.74	17.65	100.00	3.13	0.57	0.72	11.90	0.00	11.90	4.000	No	Yes	2.00
469	30.81	17.83	100.00	3.12	0.57	0.71	12.01	0.00	12.01	4.000	No	Yes	2.00
470	30.87	18.49	100.00	3.11	0.57	0.71	12.45	0.00	12.45	4.000	No	Yes	2.00
471	30.91	18.78	100.00	3.10	0.57	0.71	12.64	0.00	12.64	4.000	No	Yes	2.00
472	30.97	19.43	100.00	3.10	0.57	0.71	13.08	0.00	13.08	4.000	No	Yes	2.00
473	31.04	19.72	100.00	3.12	0.57	0.71	13.27	0.00	13.27	4.000	No	Yes	2.00
474	31.11	20.19	100.00	3.13	0.57	0.71	13.58	0.00	13.58	4.000	No	Yes	2.00
475	31.17	20.56	100.00	3.14	0.57	0.71	13.82	0.00	13.82	4.000	No	Yes	2.00
476	31.24	21.41	100.00	3.12	0.57	0.71	14.39	0.00	14.39	4.000	No	Yes	2.00
477	31.31	21.32	100.00	3.14	0.57	0.71	14.31	0.00	14.31	4.000	No	Yes	2.00
478	31.38	21.03	100.00	3.16	0.57	0.71	14.09	0.00	14.09	4.000	No	Yes	2.00
479	31.44	20.75	100.00	3.18	0.57	0.71	13.88	0.00	13.88	4.000	No	Yes	2.00
480	31.51	20.28	100.00	3.21	0.57	0.71	13.54	0.00	13.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	31.57	20.00	100.00	3.21	0.57	0.71	13.33	0.00	13.33	4.000	No	Yes	2.00
482	31.64	20.19	100.00	3.20	0.57	0.71	13.45	0.00	13.45	4.000	No	Yes	2.00
483	31.71	20.19	100.00	3.20	0.57	0.71	13.43	0.00	13.43	4.000	No	Yes	2.00
484	31.77	19.90	100.00	3.20	0.57	0.70	13.22	0.00	13.22	4.000	No	Yes	2.00
485	31.84	20.56	100.00	3.20	0.57	0.70	13.65	0.00	13.65	4.000	No	Yes	2.00
486	31.91	21.79	100.00	3.17	0.57	0.70	14.48	0.00	14.48	4.000	No	Yes	2.00
487	31.97	22.54	100.00	3.14	0.56	0.70	14.98	0.00	14.98	4.000	No	Yes	2.00
488	32.04	24.14	100.00	3.10	0.56	0.71	16.07	0.00	16.07	4.000	No	Yes	2.00
489	32.11	24.23	100.00	3.09	0.56	0.71	16.11	0.00	16.11	4.000	No	Yes	2.00
490	32.18	23.48	100.00	3.12	0.56	0.70	15.58	0.00	15.58	4.000	No	Yes	2.00
491	32.24	23.95	100.00	3.12	0.56	0.70	15.88	0.00	15.88	4.000	No	Yes	2.00
492	32.31	23.95	100.00	3.13	0.56	0.70	15.87	0.00	15.87	4.000	No	Yes	2.00
493	32.36	23.95	100.00	3.14	0.56	0.70	15.85	0.00	15.85	4.000	No	Yes	2.00
494	32.43	23.01	100.00	3.17	0.56	0.70	15.19	0.00	15.19	4.000	No	Yes	2.00
495	32.49	22.63	100.00	3.19	0.56	0.70	14.91	0.00	14.91	4.000	No	Yes	2.00
496	32.56	23.20	100.00	3.17	0.56	0.70	15.28	0.00	15.28	4.000	No	Yes	2.00
497	32.62	23.20	100.00	3.16	0.56	0.70	15.27	0.00	15.27	4.000	No	Yes	2.00
498	32.70	23.48	100.00	3.15	0.56	0.70	15.44	0.00	15.44	4.000	No	Yes	2.00
499	32.75	24.23	100.00	3.13	0.56	0.70	15.93	0.00	15.93	4.000	No	Yes	2.00
500	32.83	24.99	100.00	3.12	0.56	0.70	16.43	0.00	16.43	4.000	No	Yes	2.00
501	32.88	24.90	100.00	3.12	0.56	0.70	16.35	0.00	16.35	4.000	No	Yes	2.00
502	32.96	25.56	100.00	3.11	0.56	0.70	16.78	0.00	16.78	4.000	No	Yes	2.00
503	33.01	26.03	100.00	3.11	0.56	0.70	17.09	0.00	17.09	4.000	No	Yes	2.00
504	33.08	26.31	100.00	3.11	0.56	0.70	17.26	0.00	17.26	4.000	No	Yes	2.00
505	33.16	27.82	100.00	3.10	0.55	0.70	18.27	0.00	18.27	4.000	No	Yes	2.00
506	33.22	29.23	100.00	3.07	0.55	0.70	19.22	0.00	19.22	4.000	No	Yes	2.00
507	33.29	31.58	100.00	3.02	0.54	0.70	20.82	0.00	20.82	4.000	No	Yes	2.00
508	33.34	32.15	100.00	3.01	0.54	0.70	21.19	0.00	21.19	4.000	No	Yes	2.00
509	33.40	32.43	100.00	3.01	0.54	0.70	21.37	0.00	21.37	4.000	No	Yes	2.00
510	33.47	33.37	100.00	3.00	0.54	0.70	22.00	0.00	22.00	4.000	No	Yes	2.00
511	33.56	34.03	100.00	2.98	0.54	0.70	22.42	0.00	22.42	4.000	No	Yes	2.00
512	33.62	32.81	100.00	3.00	0.54	0.70	21.55	0.00	21.55	4.000	No	Yes	2.00
513	33.68	29.51	100.00	3.06	0.55	0.69	19.26	0.00	19.26	4.000	No	Yes	2.00
514	33.73	26.22	100.00	3.13	0.56	0.69	17.00	0.00	17.00	4.000	No	Yes	2.00
515	33.82	21.70	100.00	3.25	0.57	0.68	13.94	0.00	13.94	4.000	No	Yes	2.00
516	33.89	20.48	100.00	3.27	0.57	0.68	13.11	0.00	13.11	4.000	No	Yes	2.00
517	33.95	20.76	100.00	3.24	0.57	0.68	13.29	0.00	13.29	4.000	No	Yes	2.00
518	34.02	20.67	100.00	3.21	0.57	0.68	13.21	0.00	13.21	4.000	No	Yes	2.00
519	34.09	19.91	100.00	3.22	0.57	0.68	12.69	0.00	12.69	4.000	No	Yes	2.00
520	34.15	19.26	100.00	3.23	0.57	0.68	12.25	0.00	12.25	4.000	No	Yes	2.00
521	34.22	18.69	100.00	3.25	0.58	0.67	11.86	0.00	11.86	4.000	No	Yes	2.00
522	34.25	18.41	100.00	3.26	0.58	0.67	11.67	0.00	11.67	4.000	No	Yes	2.00
523	34.32	18.03	100.00	3.27	0.58	0.67	11.41	0.00	11.41	4.000	No	Yes	2.00
524	34.39	18.13	100.00	3.27	0.58	0.67	11.46	0.00	11.46	4.000	No	Yes	2.00
525	34.45	18.22	100.00	3.26	0.58	0.67	11.51	0.00	11.51	4.000	No	Yes	2.00
526	34.52	18.60	100.00	3.24	0.58	0.67	11.74	0.00	11.74	4.000	No	Yes	2.00
527	34.59	18.60	100.00	3.24	0.58	0.67	11.73	0.00	11.73	4.000	No	Yes	2.00
528	34.65	18.60	100.00	3.24	0.58	0.67	11.72	0.00	11.72	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	34.72	18.60	100.00	3.24	0.58	0.67	11.71	0.00	11.71	4.000	No	Yes	2.00
530	34.79	18.60	100.00	3.24	0.58	0.67	11.69	0.00	11.69	4.000	No	Yes	2.00
531	34.85	18.88	100.00	3.20	0.58	0.67	11.86	0.00	11.86	4.000	No	Yes	2.00
532	34.92	19.44	100.00	3.05	0.57	0.67	12.22	0.00	12.22	4.000	No	Yes	2.00
533	34.99	19.82	100.00	3.09	0.57	0.67	12.45	0.00	12.45	4.000	No	Yes	2.00
534	35.05	20.29	100.00	3.12	0.57	0.67	12.74	0.00	12.74	4.000	No	Yes	2.00
535	35.13	20.57	100.00	3.14	0.57	0.67	12.91	0.00	12.91	4.000	No	Yes	2.00
536	35.19	20.29	100.00	3.18	0.57	0.67	12.72	0.00	12.72	4.000	No	Yes	2.00
537	35.27	23.30	100.00	3.12	0.56	0.67	14.67	0.00	14.67	4.000	No	Yes	2.00
538	35.34	23.31	100.00	3.15	0.56	0.67	14.65	0.00	14.65	4.000	No	Yes	2.00
539	35.37	23.31	100.00	3.16	0.56	0.67	14.64	0.00	14.64	4.000	No	Yes	2.00
540	35.44	23.69	100.00	3.16	0.56	0.67	14.88	0.00	14.88	4.000	No	Yes	2.00
541	35.51	24.35	100.00	3.15	0.56	0.67	15.29	0.00	15.29	4.000	No	Yes	2.00
542	35.57	25.19	100.00	3.13	0.56	0.67	15.83	0.00	15.83	4.000	No	Yes	2.00
543	35.64	26.70	100.00	3.11	0.56	0.67	16.80	0.00	16.80	4.000	No	Yes	2.00
544	35.70	28.49	100.00	3.08	0.55	0.67	17.97	0.00	17.97	4.000	No	Yes	2.00
545	35.77	29.24	100.00	3.07	0.55	0.67	18.45	0.00	18.45	4.000	No	Yes	2.00
546	35.84	29.33	100.00	3.07	0.55	0.67	18.49	0.00	18.49	4.000	No	Yes	2.00
547	35.90	28.86	100.00	3.07	0.55	0.67	18.16	0.00	18.16	4.000	No	Yes	2.00
548	35.97	27.74	100.00	3.10	0.55	0.67	17.40	0.00	17.40	4.000	No	Yes	2.00
549	36.03	27.26	100.00	3.11	0.56	0.66	17.06	0.00	17.06	4.000	No	Yes	2.00
550	36.10	27.92	100.00	3.10	0.55	0.66	17.48	0.00	17.48	4.000	No	Yes	2.00
551	36.17	26.98	100.00	3.11	0.56	0.66	16.84	0.00	16.84	4.000	No	Yes	2.00
552	36.24	27.83	100.00	3.09	0.55	0.66	17.38	0.00	17.38	4.000	No	Yes	2.00
553	36.30	24.54	100.00	3.18	0.56	0.66	15.22	0.00	15.22	4.000	No	Yes	2.00
554	36.37	27.74	100.00	3.09	0.56	0.66	17.29	0.00	17.29	4.000	No	Yes	2.00
555	36.44	35.83	98.25	2.94	0.54	0.67	22.62	0.00	22.62	4.000	No	Yes	2.00
556	36.51	45.90	86.95	2.80	0.52	0.68	29.37	0.00	29.37	4.000	No	Yes	2.00
557	36.57	51.73	82.33	2.74	0.51	0.68	33.35	0.00	33.35	4.000	No	Yes	2.00
558	36.64	52.67	83.08	2.75	0.51	0.68	33.98	0.00	33.98	4.000	No	Yes	2.00
559	36.71	49.85	87.46	2.81	0.51	0.68	32.02	0.00	32.02	4.000	No	Yes	2.00
560	36.77	45.61	92.47	2.87	0.52	0.68	29.09	0.00	29.09	4.000	No	Yes	2.00
561	36.84	40.06	98.67	2.95	0.53	0.67	25.32	0.00	25.32	4.000	No	Yes	2.00
562	36.91	33.76	100.00	3.04	0.54	0.66	21.09	0.00	21.09	4.000	No	Yes	2.00
563	36.98	27.83	100.00	3.15	0.56	0.65	17.18	0.00	17.18	4.000	No	Yes	2.00
564	37.01	25.57	100.00	3.19	0.56	0.65	15.71	0.00	15.71	4.000	No	Yes	2.00
565	37.08	21.81	100.00	3.27	0.57	0.65	13.29	0.00	13.29	4.000	No	Yes	2.00
566	37.15	19.36	100.00	3.32	0.58	0.64	11.73	0.00	11.73	4.000	No	Yes	2.00
567	37.21	17.85	100.00	3.36	0.58	0.64	10.77	0.00	10.77	4.000	No	Yes	2.00
568	37.28	16.73	100.00	3.37	0.58	0.64	10.06	0.00	10.06	4.000	No	Yes	2.00
569	37.34	16.44	100.00	3.36	0.58	0.64	9.87	0.00	9.87	4.000	No	Yes	2.00
570	37.41	17.10	100.00	3.33	0.58	0.64	10.27	0.00	10.27	4.000	No	Yes	2.00
571	37.48	18.33	100.00	3.28	0.58	0.64	11.02	0.00	11.02	4.000	No	Yes	2.00
572	37.55	19.74	100.00	3.23	0.57	0.64	11.89	0.00	11.89	4.000	No	Yes	2.00
573	37.61	20.58	100.00	3.19	0.57	0.64	12.41	0.00	12.41	4.000	No	Yes	2.00
574	37.68	20.77	100.00	3.06	0.57	0.64	12.52	0.00	12.52	4.000	No	Yes	2.00
575	37.75	20.21	100.00	3.12	0.57	0.64	12.15	0.00	12.15	4.000	No	Yes	2.00
576	37.81	19.92	100.00	3.17	0.57	0.64	11.96	0.00	11.96	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
577	37.88	20.30	100.00	3.21	0.57	0.64	12.18	0.00	12.18	4.000	No	Yes	2.00
578	37.95	21.06	100.00	3.25	0.57	0.64	12.64	0.00	12.64	4.000	No	Yes	2.00
579	38.02	25.58	100.00	3.15	0.56	0.64	15.48	0.00	15.48	4.000	No	Yes	2.00
580	38.08	28.22	100.00	3.12	0.56	0.64	17.14	0.00	17.14	4.000	No	Yes	2.00
581	38.15	31.32	100.00	3.09	0.55	0.65	19.12	0.00	19.12	4.000	No	Yes	2.00
582	38.21	35.08	100.00	3.05	0.54	0.65	21.54	0.00	21.54	4.000	No	Yes	2.00
583	38.28	39.79	100.00	2.99	0.53	0.66	24.61	0.00	24.61	4.000	No	Yes	2.00
584	38.35	43.18	99.36	2.95	0.52	0.66	26.84	0.00	26.84	4.000	No	Yes	2.00
585	38.41	46.28	96.82	2.92	0.52	0.66	28.87	0.00	28.87	4.000	No	Yes	2.00
586	38.48	49.39	94.80	2.90	0.51	0.66	30.93	0.00	30.93	4.000	No	Yes	2.00
587	38.55	50.80	94.13	2.89	0.51	0.66	31.87	0.00	31.87	4.000	No	Yes	2.00
588	38.58	50.70	94.25	2.89	0.51	0.66	31.79	0.00	31.79	4.000	No	Yes	2.00
589	38.65	49.49	95.11	2.90	0.51	0.66	30.92	0.00	30.92	4.000	No	Yes	2.00
590	38.72	46.39	97.91	2.94	0.52	0.66	28.82	0.00	28.82	4.000	No	Yes	2.00
591	38.78	40.74	100.00	3.01	0.53	0.65	25.04	0.00	25.04	4.000	No	Yes	2.00
592	38.85	34.53	100.00	3.10	0.54	0.64	20.97	0.00	20.97	4.000	No	Yes	2.00
593	38.92	29.17	100.00	3.18	0.55	0.64	17.52	0.00	17.52	4.000	No	Yes	2.00
594	38.98	25.87	100.00	3.23	0.56	0.63	15.42	0.00	15.42	4.000	No	Yes	2.00
595	39.05	24.09	100.00	3.25	0.57	0.63	14.30	0.00	14.30	4.000	No	Yes	2.00
596	39.12	22.39	100.00	3.27	0.57	0.63	13.23	0.00	13.23	4.000	No	Yes	2.00
597	39.18	21.36	100.00	3.28	0.57	0.63	12.58	0.00	12.58	4.000	No	Yes	2.00
598	39.25	21.73	100.00	3.25	0.57	0.63	12.79	0.00	12.79	4.000	No	Yes	2.00
599	39.32	22.11	100.00	3.22	0.57	0.63	13.02	0.00	13.02	4.000	No	Yes	2.00
600	39.38	21.83	100.00	3.23	0.57	0.62	12.83	0.00	12.83	4.000	No	Yes	2.00
601	39.45	21.17	100.00	3.25	0.57	0.62	12.41	0.00	12.41	4.000	No	Yes	2.00
602	39.52	20.42	100.00	3.29	0.57	0.62	11.94	0.00	11.94	4.000	No	Yes	2.00
603	39.58	20.42	100.00	3.31	0.57	0.62	11.93	0.00	11.93	4.000	No	Yes	2.00
604	39.65	22.58	100.00	3.24	0.57	0.62	13.24	0.00	13.24	4.000	No	Yes	2.00
605	39.72	26.81	100.00	3.12	0.56	0.63	15.84	0.00	15.84	4.000	No	Yes	2.00
606	39.78	30.86	100.00	3.06	0.55	0.63	18.36	0.00	18.36	4.000	No	Yes	2.00
607	39.85	33.31	100.00	3.05	0.55	0.63	19.89	0.00	19.89	4.000	No	Yes	2.00
608	39.92	34.44	100.00	3.07	0.54	0.63	20.59	0.00	20.59	4.000	No	Yes	2.00
609	39.97	33.97	100.00	3.10	0.54	0.63	20.28	0.00	20.28	4.000	No	Yes	2.00
610	40.04	45.83	97.40	2.93	0.52	0.65	27.91	0.00	27.91	4.000	No	Yes	2.00
611	40.09	45.74	98.55	2.94	0.52	0.65	27.83	0.00	27.83	4.000	No	Yes	2.00
612	40.17	42.91	100.00	3.00	0.53	0.64	25.96	0.00	25.96	4.000	No	Yes	2.00
613	40.23	41.31	100.00	3.03	0.53	0.64	24.90	0.00	24.90	4.000	No	Yes	2.00
614	40.31	41.31	100.00	3.02	0.53	0.64	24.87	0.00	24.87	4.000	No	Yes	2.00
615	40.37	40.19	100.00	3.02	0.53	0.64	24.12	0.00	24.12	4.000	No	Yes	2.00
616	40.44	38.77	100.00	3.03	0.53	0.63	23.19	0.00	23.19	4.000	No	Yes	2.00
617	40.51	36.99	100.00	3.05	0.54	0.63	22.03	0.00	22.03	4.000	No	Yes	2.00
618	40.57	35.20	100.00	3.08	0.54	0.63	20.87	0.00	20.87	4.000	No	Yes	2.00
619	40.64	34.54	100.00	3.09	0.54	0.63	20.43	0.00	20.43	4.000	No	Yes	2.00
620	40.71	34.55	100.00	3.09	0.54	0.63	20.41	0.00	20.41	4.000	No	Yes	2.00
621	40.77	34.17	100.00	3.10	0.55	0.63	20.16	0.00	20.16	4.000	No	Yes	2.00
622	40.84	33.89	100.00	3.10	0.55	0.63	19.96	0.00	19.96	4.000	No	Yes	2.00
623	40.91	33.99	100.00	3.11	0.55	0.62	20.00	0.00	20.00	4.000	No	Yes	2.00
624	40.97	37.36	100.00	3.06	0.54	0.63	22.12	0.00	22.12	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	41.04	46.03	99.26	2.95	0.52	0.64	27.65	0.00	27.65	4.000	No	Yes	2.00
626	41.11	56.95	88.86	2.82	0.50	0.65	34.77	0.00	34.77	4.000	No	Yes	2.00
627	41.17	58.55	85.34	2.78	0.50	0.65	35.77	0.00	35.77	4.000	No	Yes	2.00
628	41.24	54.31	90.56	2.84	0.51	0.64	32.97	0.00	32.97	4.000	No	Yes	2.00
629	41.30	49.32	97.63	2.93	0.51	0.64	29.68	0.00	29.68	4.000	No	Yes	2.00
630	41.37	42.64	100.00	3.04	0.53	0.63	25.34	0.00	25.34	4.000	No	Yes	2.00
631	41.41	34.75	100.00	3.17	0.54	0.62	20.33	0.00	20.33	4.000	No	Yes	2.00
632	41.48	46.32	100.00	2.99	0.52	0.63	27.67	0.00	27.67	4.000	No	Yes	2.00
633	41.54	54.89	95.17	2.90	0.50	0.64	33.24	0.00	33.24	4.000	No	Yes	2.00
634	41.60	68.34	85.44	2.78	0.48	0.65	42.20	0.00	42.20	4.000	No	Yes	2.00
635	41.67	83.03	76.22	2.67	0.46	0.67	52.31	0.00	52.31	4.000	No	Yes	2.00
636	41.74	100.25	66.27	2.54	0.43	0.68	64.54	68.54	133.08	0.208	No	No	0.22
637	41.80	104.18	64.31	2.52	0.43	0.68	67.36	68.85	136.21	0.219	No	No	0.23
638	41.87	108.79	61.08	2.48	0.42	0.69	70.64	68.85	139.50	0.232	No	No	0.25
639	41.94	118.86	55.27	2.40	0.41	0.70	78.09	68.94	147.03	0.270	No	No	0.29
640	42.00	130.06	49.40	2.33	0.40	0.70	86.38	68.59	154.97	0.325	No	No	0.35
641	42.07	138.90	45.23	2.28	0.39	0.71	92.98	67.99	160.97	0.382	No	No	0.41
642	42.14	145.28	41.76	2.23	0.38	0.71	97.67	66.84	164.51	0.423	No	No	0.45
643	42.19	152.71	38.41	2.19	0.37	0.72	103.21	65.49	168.69	0.483	No	No	0.52
644	42.26	151.30	38.95	2.20	0.38	0.71	102.05	65.68	167.73	0.468	No	No	0.50
645	42.34	157.41	36.76	2.17	0.37	0.72	106.62	64.77	171.39	0.528	No	No	0.56
646	42.40	154.12	38.24	2.19	0.37	0.71	104.09	65.54	169.63	0.498	No	No	0.53
647	42.46	152.99	39.57	2.21	0.37	0.71	103.29	66.50	169.78	0.500	No	No	0.53
648	42.53	150.26	41.27	2.23	0.37	0.71	101.20	67.34	168.54	0.480	No	No	0.51
649	42.60	147.81	42.38	2.24	0.38	0.71	99.28	67.68	166.96	0.457	No	No	0.49
650	42.67	142.83	44.25	2.27	0.38	0.71	95.40	67.98	163.38	0.409	No	No	0.44
651	42.73	136.33	47.04	2.30	0.39	0.70	90.41	68.39	158.81	0.360	No	No	0.38
652	42.80	128.15	50.95	2.35	0.40	0.70	84.22	68.76	152.98	0.310	No	No	0.33
653	42.87	118.46	55.56	2.41	0.41	0.69	76.95	68.74	145.69	0.263	No	No	0.28
654	42.94	106.98	61.39	2.48	0.43	0.68	68.41	68.32	136.73	0.221	No	No	0.23
655	43.00	97.28	66.06	2.54	0.44	0.67	61.39	67.59	128.98	0.195	No	No	0.21
656	43.07	91.83	67.35	2.55	0.45	0.66	57.45	66.76	124.21	0.181	No	No	0.19
657	43.14	90.13	68.26	2.57	0.45	0.66	56.21	66.61	122.82	0.178	No	No	0.19
658	43.20	90.13	68.29	2.57	0.45	0.66	56.16	66.60	122.76	0.178	No	No	0.19
659	43.27	89.66	68.69	2.57	0.45	0.66	55.79	66.58	122.37	0.177	No	No	0.19
660	43.34	89.85	68.82	2.57	0.45	0.66	55.88	66.64	122.52	0.177	No	No	0.19
661	43.39	90.80	68.51	2.57	0.45	0.66	56.51	66.75	123.26	0.179	No	No	0.19
662	43.47	90.41	69.00	2.57	0.45	0.66	56.19	66.77	122.96	0.178	No	No	0.19
663	43.54	84.96	72.11	2.61	0.46	0.65	52.37	0.00	52.37	4.000	No	Yes	2.00
664	43.60	78.46	75.88	2.66	0.47	0.65	47.88	0.00	47.88	4.000	No	Yes	2.00
665	43.67	71.59	79.60	2.71	0.48	0.64	43.20	0.00	43.20	4.000	No	Yes	2.00
666	43.73	64.16	83.64	2.76	0.49	0.63	38.22	0.00	38.22	4.000	No	Yes	2.00
667	43.80	57.57	87.69	2.81	0.50	0.62	33.93	0.00	33.93	4.000	No	Yes	2.00
668	43.83	54.66	89.57	2.83	0.51	0.62	32.06	0.00	32.06	4.000	No	Yes	2.00
669	43.90	49.86	92.40	2.87	0.52	0.62	28.96	0.00	28.96	4.000	No	Yes	2.00
670	43.97	45.81	94.90	2.90	0.53	0.61	26.40	0.00	26.40	4.000	No	Yes	2.00
671	44.03	41.67	98.72	2.95	0.53	0.61	23.83	0.00	23.83	4.000	No	Yes	2.00
672	44.10	38.38	100.00	2.98	0.54	0.60	21.79	0.00	21.79	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
673	44.17	36.21	100.00	3.01	0.54	0.60	20.45	0.00	20.45	4.000	No	Yes	2.00
674	44.23	33.39	100.00	3.06	0.55	0.60	18.74	0.00	18.74	4.000	No	Yes	2.00
675	44.30	29.92	100.00	3.14	0.56	0.59	16.65	0.00	16.65	4.000	No	Yes	2.00
676	44.37	27.94	100.00	3.18	0.56	0.59	15.47	0.00	15.47	4.000	No	Yes	2.00
677	44.44	28.51	100.00	3.16	0.56	0.59	15.79	0.00	15.79	4.000	No	Yes	2.00
678	44.50	31.90	100.00	3.10	0.55	0.59	17.78	0.00	17.78	4.000	No	Yes	2.00
679	44.57	35.94	100.00	3.04	0.55	0.60	20.18	0.00	20.18	4.000	No	Yes	2.00
680	44.64	36.98	100.00	3.03	0.54	0.60	20.79	0.00	20.79	4.000	No	Yes	2.00
681	44.70	36.41	100.00	3.05	0.54	0.60	20.43	0.00	20.43	4.000	No	Yes	2.00
682	44.77	39.23	100.00	3.02	0.54	0.60	22.11	0.00	22.11	4.000	No	Yes	2.00
683	44.84	52.13	91.35	2.85	0.52	0.61	30.04	0.00	30.04	4.000	No	Yes	2.00
684	44.90	73.02	75.28	2.65	0.48	0.63	43.44	0.00	43.44	4.000	No	Yes	2.00
685	44.97	89.01	64.69	2.52	0.46	0.64	54.10	65.15	119.25	0.170	No	No	0.18
686	45.04	96.63	60.16	2.46	0.45	0.65	59.27	65.38	124.65	0.183	No	No	0.19
687	45.11	99.93	58.17	2.44	0.44	0.65	61.49	65.38	126.87	0.188	No	No	0.20
688	45.17	103.22	56.20	2.41	0.44	0.65	63.71	65.33	129.05	0.195	No	No	0.21
689	45.24	106.13	54.73	2.40	0.44	0.66	65.70	65.35	131.04	0.201	No	No	0.21
690	45.31	108.67	53.29	2.38	0.43	0.66	67.41	65.26	132.67	0.206	No	No	0.22
691	45.37	110.46	52.23	2.37	0.43	0.66	68.60	65.15	133.75	0.210	No	No	0.22
692	45.44	112.25	51.96	2.36	0.43	0.66	69.84	65.37	135.21	0.215	No	No	0.23
693	45.48	113.28	52.07	2.36	0.43	0.66	70.57	65.61	136.18	0.219	No	No	0.23
694	45.54	115.26	52.16	2.36	0.43	0.66	71.98	66.02	138.00	0.226	No	No	0.24
695	45.61	116.67	52.39	2.37	0.42	0.66	73.09	66.42	139.51	0.232	No	No	0.25
696	45.69	115.44	53.82	2.39	0.42	0.66	72.19	66.76	138.96	0.230	No	No	0.24
697	45.76	119.02	52.32	2.37	0.42	0.66	74.71	66.82	141.53	0.242	No	No	0.26
698	45.83	119.02	52.27	2.37	0.42	0.66	74.65	66.79	141.44	0.241	No	No	0.26
699	45.89	117.99	52.52	2.37	0.42	0.66	73.84	66.68	140.52	0.237	No	No	0.25
700	45.96	117.99	52.48	2.37	0.42	0.66	73.78	66.64	140.42	0.237	No	No	0.25
701	46.03	117.99	52.64	2.37	0.42	0.66	73.74	66.70	140.43	0.237	No	No	0.25
702	46.09	117.99	52.90	2.37	0.42	0.66	73.70	66.80	140.49	0.237	No	No	0.25
703	46.16	118.27	52.96	2.37	0.42	0.66	73.85	66.87	140.72	0.238	No	No	0.25
704	46.23	118.64	53.18	2.38	0.42	0.66	74.09	67.02	141.11	0.240	No	No	0.25
705	46.29	119.11	53.07	2.38	0.42	0.66	74.37	67.05	141.42	0.241	No	No	0.26
706	46.36	119.21	53.05	2.38	0.42	0.66	74.39	67.05	141.44	0.241	No	No	0.26
707	46.42	119.68	52.80	2.37	0.42	0.66	74.67	67.02	141.69	0.242	No	No	0.26
708	46.46	119.77	52.73	2.37	0.42	0.66	74.71	67.00	141.71	0.242	No	No	0.26
709	46.53	119.58	52.82	2.37	0.42	0.66	74.51	66.99	141.50	0.241	No	No	0.26
710	46.59	119.21	53.12	2.38	0.42	0.66	74.20	67.02	141.23	0.240	No	No	0.25
711	46.66	118.93	53.37	2.38	0.42	0.66	73.95	67.06	141.01	0.239	No	No	0.25
712	46.73	118.36	53.74	2.38	0.42	0.66	73.50	67.08	140.58	0.237	No	No	0.25
713	46.80	117.89	54.00	2.39	0.42	0.66	73.11	67.08	140.19	0.235	No	No	0.25
714	46.86	117.33	54.36	2.39	0.42	0.66	72.66	67.10	139.77	0.234	No	No	0.25
715	46.93	116.76	54.70	2.40	0.42	0.65	72.21	67.11	139.32	0.232	No	No	0.25
716	46.99	116.29	54.76	2.40	0.42	0.65	71.81	67.03	138.84	0.230	No	No	0.24
717	47.06	115.44	54.93	2.40	0.42	0.65	71.15	66.91	138.06	0.226	No	No	0.24
718	47.13	114.41	55.09	2.40	0.43	0.65	70.24	66.72	136.96	0.222	No	No	0.24
719	47.20	112.25	55.73	2.41	0.43	0.65	68.66	66.52	135.18	0.215	No	No	0.23
720	47.26	110.08	56.44	2.42	0.43	0.65	67.08	66.34	133.43	0.209	No	No	0.22

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	47.33	106.69	57.99	2.44	0.44	0.64	64.68	66.21	130.89	0.200	No	No	0.21
722	47.40	103.59	59.60	2.46	0.44	0.64	62.50	66.11	128.62	0.193	No	No	0.21
723	47.47	101.42	60.87	2.47	0.44	0.64	60.97	66.07	127.04	0.189	No	No	0.20
724	47.53	99.73	61.98	2.49	0.45	0.63	59.79	66.05	125.84	0.186	No	No	0.20
725	47.60	98.32	63.04	2.50	0.45	0.63	58.79	66.06	124.86	0.183	No	No	0.19
726	47.66	98.32	63.07	2.50	0.45	0.63	58.75	66.06	124.81	0.183	No	No	0.19
727	47.73	98.32	62.63	2.50	0.45	0.63	58.69	65.92	124.61	0.182	No	No	0.19
728	47.80	98.32	61.67	2.48	0.45	0.63	58.61	65.63	124.25	0.182	No	No	0.19
729	47.87	96.91	61.36	2.48	0.45	0.63	57.58	65.25	122.83	0.178	No	No	0.19
730	47.93	93.90	62.62	2.50	0.46	0.63	55.51	65.02	120.52	0.173	No	No	0.18
731	48.00	89.28	65.58	2.53	0.46	0.62	52.40	64.89	117.29	0.166	No	No	0.18
732	48.03	86.46	67.64	2.56	0.47	0.62	50.54	64.83	115.36	0.162	No	No	0.17
733	48.10	79.50	70.77	2.60	0.48	0.61	45.93	64.15	110.09	0.152	No	No	0.16
734	48.17	71.97	73.03	2.63	0.49	0.60	40.98	0.00	40.98	4.000	No	Yes	2.00
735	48.24	63.88	80.51	2.72	0.50	0.60	35.95	0.00	35.95	4.000	No	Yes	2.00
736	48.30	56.44	87.30	2.80	0.51	0.59	31.36	0.00	31.36	4.000	No	Yes	2.00
737	48.37	49.39	93.89	2.89	0.52	0.58	27.10	0.00	27.10	4.000	No	Yes	2.00
738	48.43	39.70	100.00	3.02	0.54	0.57	21.37	0.00	21.37	4.000	No	Yes	2.00
739	48.50	40.26	100.00	3.00	0.54	0.57	21.68	0.00	21.68	4.000	No	Yes	2.00
740	48.56	36.50	100.00	3.07	0.55	0.57	19.49	0.00	19.49	4.000	No	Yes	2.00
741	48.63	32.26	100.00	3.16	0.56	0.56	17.05	0.00	17.05	4.000	No	Yes	2.00
742	48.70	32.18	100.00	3.14	0.56	0.56	16.99	0.00	16.99	4.000	No	Yes	2.00
743	48.76	32.08	100.00	3.10	0.56	0.56	16.92	0.00	16.92	4.000	No	Yes	2.00
744	48.82	40.83	98.06	2.94	0.54	0.57	21.91	0.00	21.91	4.000	No	Yes	2.00
745	48.89	53.83	84.37	2.77	0.52	0.58	29.52	0.00	29.52	4.000	No	Yes	2.00
746	48.95	65.03	74.82	2.65	0.50	0.59	36.29	0.00	36.29	4.000	No	Yes	2.00
747	49.02	68.79	72.07	2.61	0.50	0.59	38.56	0.00	38.56	4.000	No	Yes	2.00
748	49.09	66.24	75.91	2.66	0.50	0.59	37.01	0.00	37.01	4.000	No	Yes	2.00
749	49.15	65.86	78.22	2.69	0.50	0.59	36.78	0.00	36.78	4.000	No	Yes	2.00
750	49.23	61.25	83.76	2.76	0.51	0.59	33.96	0.00	33.96	4.000	No	Yes	2.00
751	49.28	55.70	89.54	2.83	0.51	0.58	30.57	0.00	30.57	4.000	No	Yes	2.00
752	49.35	47.33	97.91	2.94	0.53	0.57	25.58	0.00	25.58	4.000	No	Yes	2.00
753	49.42	41.30	100.00	3.00	0.54	0.57	22.04	0.00	22.04	4.000	No	Yes	2.00
754	49.48	37.54	100.00	3.05	0.55	0.56	19.86	0.00	19.86	4.000	No	Yes	2.00
755	49.55	35.47	100.00	3.07	0.55	0.56	18.67	0.00	18.67	4.000	No	Yes	2.00
756	49.62	35.20	100.00	3.06	0.55	0.56	18.50	0.00	18.50	4.000	No	Yes	2.00
757	49.69	35.95	100.00	3.03	0.55	0.56	18.91	0.00	18.91	4.000	No	Yes	2.00
758	49.75	35.95	100.00	3.02	0.55	0.56	18.89	0.00	18.89	4.000	No	Yes	2.00
759	49.82	34.26	100.00	3.06	0.55	0.56	17.92	0.00	17.92	4.000	No	Yes	2.00
760	49.87	33.03	100.00	3.07	0.56	0.55	17.22	0.00	17.22	4.000	No	Yes	2.00
761	49.94	32.20	100.00	2.99	0.56	0.55	16.74	0.00	16.74	4.000	No	Yes	2.00
762	50.02	32.10	96.07	2.91	0.56	0.55	16.65	0.00	16.65	4.000	No	Yes	2.00
763	50.07	33.70	97.25	2.93	0.55	0.55	17.54	0.00	17.54	4.000	No	Yes	2.00
764	50.16	39.25	93.53	2.88	0.54	0.56	20.64	0.00	20.64	4.000	No	Yes	2.00
765	50.21	41.04	94.31	2.89	0.54	0.56	21.65	0.00	21.65	4.000	No	Yes	2.00
766	50.27	43.66	95.24	2.90	0.54	0.56	23.10	0.00	23.10	4.000	No	Yes	2.00
767	50.33	56.27	86.42	2.79	0.52	0.57	30.47	0.00	30.47	4.000	No	Yes	2.00
768	50.40	72.00	77.79	2.68	0.49	0.59	40.00	0.00	40.00	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
769	50.47	100.87	61.44	2.48	0.45	0.62	58.61	65.57	124.18	4.000	No	No	2.00
770	50.53	124.30	50.84	2.35	0.42	0.64	74.65	66.16	140.81	4.000	No	No	2.00
771	50.61	148.09	43.25	2.25	0.39	0.66	91.64	66.38	158.02	4.000	No	No	2.00
772	50.66	156.37	41.10	2.23	0.38	0.66	97.71	66.36	164.07	4.000	No	No	2.00
773	50.73	164.94	38.33	2.19	0.37	0.67	103.93	65.59	169.51	4.000	No	No	2.00
774	50.80	170.38	36.25	2.17	0.37	0.67	107.79	64.53	172.32	4.000	No	No	2.00
775	50.87	172.91	35.01	2.15	0.37	0.67	109.47	63.64	173.11	4.000	No	No	2.00
776	50.92	173.57	34.70	2.15	0.37	0.67	109.88	63.39	173.26	4.000	No	No	2.00
777	51.01	174.23	34.56	2.14	0.37	0.67	110.28	63.33	173.61	4.000	No	No	2.00
778	51.07	170.46	35.92	2.16	0.37	0.67	107.52	64.14	171.65	4.000	No	No	2.00
779	51.13	166.40	37.42	2.18	0.37	0.67	104.54	64.90	169.44	4.000	No	No	2.00
780	51.20	162.26	39.18	2.20	0.38	0.66	101.53	65.74	167.27	4.000	No	No	2.00
781	51.26	158.59	41.37	2.23	0.38	0.66	98.95	66.86	165.81	4.000	No	No	2.00
782	51.32	154.26	43.31	2.25	0.38	0.66	95.79	67.46	163.24	4.000	No	No	2.00
783	51.39	147.86	45.83	2.29	0.39	0.65	91.10	67.87	158.97	4.000	No	No	2.00
784	51.45	141.94	50.15	2.34	0.39	0.65	86.97	69.11	156.09	4.000	No	No	2.00
785	51.52	140.81	51.23	2.35	0.39	0.65	86.15	69.41	155.57	4.000	No	No	2.00
786	51.59	146.07	48.86	2.32	0.39	0.65	89.88	69.23	159.12	4.000	No	No	2.00
787	51.65	143.62	50.25	2.34	0.39	0.65	88.10	69.46	157.56	4.000	No	No	2.00
788	51.71	148.14	49.52	2.33	0.39	0.65	91.43	69.98	161.41	4.000	No	No	2.00
789	51.78	148.42	50.87	2.35	0.38	0.65	91.71	70.72	162.42	4.000	No	No	2.00
790	51.84	145.59	52.45	2.37	0.39	0.65	89.63	70.90	160.53	4.000	No	No	2.00
791	51.92	143.71	52.74	2.37	0.39	0.65	88.15	70.63	158.77	4.000	No	No	2.00
792	51.97	143.70	52.78	2.37	0.39	0.65	88.10	70.63	158.74	4.000	No	No	2.00
793	52.04	143.70	52.77	2.37	0.39	0.65	88.04	70.61	158.65	4.000	No	No	2.00
794	52.10	143.70	52.54	2.37	0.39	0.65	87.97	70.49	158.46	4.000	No	No	2.00
795	52.17	144.64	53.25	2.38	0.39	0.65	88.68	70.99	159.68	4.000	No	No	2.00
796	52.23	156.03	49.52	2.33	0.37	0.66	97.07	71.47	168.54	4.000	No	No	2.00
797	52.30	165.06	46.70	2.30	0.36	0.67	103.81	71.65	175.46	4.000	No	No	2.00
798	52.37	177.39	42.90	2.25	0.35	0.68	113.13	71.50	184.64	4.000	No	No	2.00
799	52.44	189.81	39.69	2.21	0.34	0.68	122.73	71.27	194.00	4.000	No	No	2.00
800	52.50	181.91	42.84	2.25	0.35	0.68	116.70	72.35	189.05	4.000	No	No	2.00
801	52.56	198.75	38.54	2.19	0.33	0.69	129.89	71.92	201.81	4.000	No	No	2.00
802	52.63	198.00	38.95	2.20	0.33	0.69	129.27	72.16	201.43	4.000	No	No	2.00
803	52.69	196.12	39.08	2.20	0.33	0.69	127.63	71.89	199.52	4.000	No	No	2.00
804	52.77	194.23	38.82	2.20	0.33	0.69	125.89	71.24	197.12	4.000	No	No	2.00
805	52.85	195.08	37.77	2.18	0.34	0.69	126.26	70.32	196.59	4.000	No	No	2.00
806	52.92	191.60	38.15	2.19	0.34	0.68	123.37	70.01	193.37	4.000	No	No	2.00
807	52.98	187.93	38.69	2.20	0.34	0.68	120.39	69.81	190.20	4.000	No	No	2.00
808	53.05	183.60	37.17	2.18	0.35	0.67	116.43	67.43	183.87	4.000	No	No	2.00
809	53.09	181.91	37.45	2.18	0.35	0.67	115.10	67.40	182.49	4.000	No	No	2.00
810	53.15	178.61	39.15	2.20	0.36	0.67	112.74	68.39	181.13	4.000	No	No	2.00
811	53.22	175.51	40.57	2.22	0.36	0.67	110.47	69.05	179.52	4.000	No	No	2.00
812	53.29	173.72	41.82	2.24	0.36	0.67	109.21	69.72	178.93	4.000	No	No	2.00
813	53.36	173.58	42.61	2.25	0.36	0.67	109.20	70.31	179.50	4.000	No	No	2.00
814	53.41	173.58	43.04	2.25	0.36	0.67	109.24	70.63	179.86	4.000	No	No	2.00
815	53.48	173.45	43.30	2.25	0.36	0.67	109.13	70.79	179.92	4.000	No	No	2.00
816	53.55	178.34	41.75	2.23	0.35	0.67	112.79	70.55	183.35	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	53.61	183.32	40.58	2.22	0.35	0.67	116.62	70.55	187.17	4.000	No	No	2.00
818	53.69	190.85	39.19	2.20	0.34	0.68	122.53	70.77	193.30	4.000	No	No	2.00
819	53.74	196.21	38.05	2.19	0.33	0.68	126.73	70.70	197.44	4.000	No	No	2.00
820	53.81	201.67	37.15	2.18	0.33	0.69	131.10	70.83	201.93	4.000	No	No	2.00
821	53.89	208.16	36.04	2.16	0.32	0.69	136.32	70.84	207.16	4.000	No	No	2.00
822	53.95	213.81	35.00	2.15	0.32	0.70	140.87	70.68	211.55	4.000	No	No	2.00
823	54.01	220.68	33.65	2.13	0.31	0.70	146.41	70.22	216.63	4.000	No	No	2.00
824	54.07	227.56	32.21	2.12	0.30	0.71	151.93	69.45	221.38	4.000	No	No	2.00
825	54.15	232.81	31.27	2.10	0.30	0.71	156.21	68.97	225.18	4.000	No	No	2.00
826	54.22	236.48	30.56	2.09	0.29	0.71	159.64	68.56	228.21	4.000	No	No	2.00
827	54.27	239.03	30.11	2.09	0.29	0.72	161.73	68.26	229.99	4.000	No	No	2.00
828	54.35	242.04	29.67	2.08	0.29	0.72	164.23	68.03	232.26	4.000	No	No	2.00
829	54.40	245.05	29.01	2.08	0.29	0.72	166.63	67.35	233.99	4.000	No	No	2.00
830	54.48	247.96	28.36	2.07	0.29	0.72	168.92	66.60	235.52	4.000	No	No	2.00
831	54.53	250.60	27.88	2.06	0.28	0.72	171.06	66.10	237.16	4.000	No	No	2.00
832	54.60	258.22	26.45	2.04	0.28	0.73	177.27	64.35	241.62	4.000	No	No	2.00
833	54.66	264.71	25.56	2.03	0.27	0.73	182.75	63.35	246.10	4.000	No	No	2.00
834	54.73	271.96	24.56	2.02	0.27	0.74	188.89	62.03	250.92	4.000	No	No	2.00
835	54.80	279.02	23.59	2.01	0.26	0.74	194.72	60.52	255.24	4.000	No	No	2.00
836	54.86	285.05	23.01	2.00	0.26	0.74	198.88	59.59	258.48	4.000	No	No	2.00
837	54.93	289.75	22.81	2.00	0.26	0.74	202.13	59.56	261.69	4.000	No	No	2.00
838	55.00	292.95	22.62	2.00	0.26	0.74	204.32	59.35	263.67	4.000	No	No	2.00
839	55.06	294.65	22.74	2.00	0.26	0.74	205.47	59.88	265.35	4.000	No	No	2.00
840	55.13	297.56	22.51	1.99	0.26	0.74	207.46	59.52	266.98	4.000	No	No	2.00
841	55.20	299.54	22.27	1.99	0.26	0.74	208.80	59.00	267.80	4.000	No	No	2.00
842	55.27	300.95	22.08	1.99	0.26	0.74	209.74	58.57	268.31	4.000	No	No	2.00
843	55.34	300.90	22.20	1.99	0.26	0.74	209.66	58.94	268.61	4.000	No	No	2.00
844	55.40	300.90	22.34	1.99	0.26	0.74	209.62	59.34	268.96	4.000	No	No	2.00
845	55.47	300.87	22.47	1.99	0.26	0.74	209.56	59.71	269.27	4.000	No	No	2.00
846	55.53	302.18	22.19	1.99	0.26	0.74	210.44	59.00	269.44	4.000	No	No	2.00
847	55.60	303.78	20.90	1.97	0.26	0.74	211.51	55.10	266.61	4.000	No	No	2.00
848	55.67	304.72	19.59	1.96	0.26	0.74	212.12	50.73	262.85	4.000	No	No	2.00
849	55.73	304.53	20.13	1.96	0.26	0.74	211.95	52.58	264.53	4.000	No	No	2.00
850	55.80	303.49	20.68	1.97	0.26	0.74	211.19	54.35	265.53	4.000	No	No	2.00
851	55.87	302.27	21.15	1.98	0.26	0.74	210.30	55.74	266.04	4.000	No	No	2.00
852	55.93	297.19	22.28	1.99	0.26	0.74	206.72	58.71	265.44	4.000	No	No	2.00
853	55.98	277.24	26.33	2.04	0.26	0.74	192.82	66.94	259.76	4.000	No	No	2.00
854	56.05	288.82	24.00	2.01	0.26	0.74	200.83	62.62	263.45	4.000	No	No	2.00
855	56.10	289.10	23.96	2.01	0.26	0.74	201.00	62.54	263.53	4.000	No	No	2.00
856	56.19	291.65	23.46	2.01	0.26	0.74	202.71	61.48	264.19	4.000	No	No	2.00
857	56.24	291.18	23.63	2.01	0.26	0.74	202.36	61.88	264.24	4.000	No	No	2.00
858	56.31	289.39	23.91	2.01	0.26	0.74	201.08	62.41	263.49	4.000	No	No	2.00
859	56.38	285.72	24.57	2.02	0.26	0.74	198.49	63.71	262.20	4.000	No	No	2.00
860	56.46	284.12	24.59	2.02	0.26	0.74	197.33	63.55	260.88	4.000	No	No	2.00
861	56.52	281.76	24.58	2.02	0.26	0.74	195.66	63.25	258.91	4.000	No	No	2.00
862	56.58	278.18	24.65	2.02	0.26	0.73	193.14	62.98	256.12	4.000	No	No	2.00
863	56.65	273.76	25.09	2.03	0.27	0.73	189.59	63.47	253.06	4.000	No	No	2.00
864	56.71	269.53	25.58	2.03	0.27	0.73	185.83	63.95	249.78	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	56.77	265.10	25.99	2.04	0.27	0.73	181.85	64.17	246.01	4.000	No	No	2.00
866	56.83	261.44	26.13	2.04	0.28	0.72	178.40	63.86	242.26	4.000	No	No	2.00
867	56.90	255.42	26.80	2.05	0.28	0.72	173.14	64.32	237.45	4.000	No	No	2.00
868	56.96	248.16	27.72	2.06	0.29	0.71	166.92	65.00	231.91	4.000	No	No	2.00
869	57.03	239.41	29.19	2.08	0.30	0.71	159.66	66.29	225.95	4.000	No	No	2.00
870	57.10	232.35	30.61	2.10	0.31	0.70	153.44	67.38	220.82	4.000	No	No	2.00
871	57.16	228.68	31.45	2.11	0.31	0.70	150.50	68.05	218.55	4.000	No	No	2.00
872	57.23	229.73	28.38	2.07	0.32	0.69	149.90	62.94	212.83	4.000	No	No	2.00
873	57.30	235.74	21.51	1.98	0.33	0.68	150.48	48.03	198.51	4.000	No	No	2.00
874	57.37	243.93	20.76	1.97	0.33	0.68	156.93	46.90	203.83	4.000	No	No	2.00
875	57.43	250.99	20.53	1.97	0.32	0.69	162.93	47.08	210.01	4.000	No	No	2.00
876	57.50	254.37	21.25	1.98	0.31	0.70	167.19	49.76	216.95	4.000	No	No	2.00
877	57.57	255.22	22.36	1.99	0.30	0.70	168.96	53.09	222.06	4.000	No	No	2.00
878	57.62	219.84	31.80	2.11	0.32	0.69	142.57	66.88	209.46	4.000	No	No	2.00
879	57.68	244.68	25.89	2.04	0.30	0.70	162.02	60.37	222.39	4.000	No	No	2.00
880	57.76	243.37	25.89	2.04	0.30	0.70	160.76	60.16	220.92	4.000	No	No	2.00
881	57.82	240.36	26.62	2.05	0.30	0.70	158.47	61.24	219.71	4.000	No	No	2.00
882	57.88	237.45	27.33	2.05	0.31	0.70	156.24	62.23	218.46	4.000	No	No	2.00
883	57.94	233.95	28.18	2.06	0.31	0.69	153.07	63.21	216.27	4.000	No	No	2.00
884	58.01	231.13	28.85	2.07	0.31	0.69	150.88	63.95	214.82	4.000	No	No	2.00
885	58.08	227.08	29.88	2.09	0.32	0.69	147.77	65.05	212.82	4.000	No	No	2.00
886	58.14	223.98	30.54	2.09	0.32	0.69	145.32	65.59	210.90	4.000	No	No	2.00
887	58.21	221.06	31.07	2.10	0.32	0.68	142.96	65.91	208.86	4.000	No	No	2.00
888	58.28	221.07	31.25	2.10	0.32	0.68	142.99	66.18	209.17	4.000	No	No	2.00
889	58.35	221.07	31.58	2.11	0.32	0.69	143.08	66.67	209.75	4.000	No	No	2.00
890	58.40	221.07	31.74	2.11	0.32	0.69	143.12	66.91	210.03	4.000	No	No	2.00
891	58.47	223.88	31.10	2.10	0.32	0.69	145.28	66.44	211.71	4.000	No	No	2.00
892	58.54	226.24	30.86	2.10	0.31	0.69	147.19	66.47	213.66	4.000	No	No	2.00
893	58.61	226.43	31.16	2.10	0.31	0.69	147.44	66.98	214.42	4.000	No	No	2.00
894	58.67	225.59	31.46	2.11	0.31	0.69	146.79	67.28	214.07	4.000	No	No	2.00
895	58.74	222.66	31.85	2.11	0.32	0.69	144.35	67.33	211.68	4.000	No	No	2.00
896	58.82	222.67	31.49	2.11	0.32	0.69	144.14	66.77	210.91	4.000	No	No	2.00
897	58.88	224.54	30.96	2.10	0.32	0.69	145.52	66.28	211.80	4.000	No	No	2.00
898	58.95	228.60	17.64	1.93	0.37	0.65	139.56	35.28	174.84	4.000	No	No	2.00
899	59.02	236.40	8.88	1.82	0.42	0.61	135.43	5.51	140.95	4.000	No	No	2.00
900	59.09	247.31	7.34	1.80	0.41	0.61	142.84	2.33	145.17	4.000	No	No	2.00
901	59.12	252.59	7.37	1.80	0.41	0.62	147.10	2.41	149.51	4.000	No	No	2.00
902	59.19	260.49	7.97	1.81	0.39	0.63	154.01	3.62	157.63	4.000	No	No	2.00
903	59.26	264.07	9.14	1.83	0.38	0.63	158.15	6.67	164.81	4.000	No	No	2.00
904	59.32	261.99	11.20	1.85	0.37	0.64	159.06	13.54	172.60	4.000	No	No	2.00
905	59.40	259.92	13.41	1.88	0.36	0.65	160.47	22.07	182.53	4.000	No	No	2.00
906	59.46	267.44	13.06	1.88	0.35	0.66	166.42	21.07	187.49	4.000	No	No	2.00
907	59.52	271.50	13.78	1.88	0.34	0.67	171.04	24.24	195.28	4.000	No	No	2.00
908	59.60	274.79	15.78	1.91	0.32	0.68	177.62	32.66	210.28	4.000	No	No	2.00
909	59.66	276.86	16.60	1.92	0.31	0.69	180.68	36.06	216.74	4.000	No	No	2.00
910	59.73	277.33	16.34	1.92	0.31	0.69	180.69	35.09	215.78	4.000	No	No	2.00
911	59.78	279.58	15.75	1.91	0.31	0.69	181.85	32.91	214.75	4.000	No	No	2.00
912	59.85	285.60	14.58	1.89	0.31	0.69	185.52	28.53	214.05	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
913	59.93	291.92	13.40	1.88	0.31	0.69	189.33	23.91	213.24	4.000	No	No	2.00
914	59.99	295.95	13.68	1.88	0.31	0.69	193.55	25.36	218.91	4.000	No	No	2.00
915	60.04	285.99	16.21	1.92	0.30	0.70	188.32	35.32	223.64	4.000	No	No	2.00
916	60.11	287.67	16.41	1.92	0.30	0.70	190.19	36.31	226.50	4.000	No	No	2.00
917	60.18	285.98	17.13	1.93	0.29	0.70	189.61	39.00	228.62	4.000	No	No	2.00
918	60.24	285.60	17.52	1.93	0.29	0.70	189.79	40.51	230.29	4.000	No	No	2.00
919	60.30	284.00	18.74	1.95	0.29	0.71	189.91	44.90	234.81	4.000	No	No	2.00
920	60.37	284.10	19.10	1.95	0.28	0.71	190.43	46.21	236.64	4.000	No	No	2.00
921	60.44	284.19	19.18	1.95	0.28	0.71	190.57	46.51	237.08	4.000	No	No	2.00
922	60.50	282.31	19.56	1.96	0.28	0.71	189.21	47.62	236.83	4.000	No	No	2.00
923	60.58	290.50	17.91	1.94	0.28	0.71	194.77	42.51	237.28	4.000	No	No	2.00
924	60.63	293.51	17.33	1.93	0.28	0.71	196.75	40.53	237.28	4.000	No	No	2.00
925	60.70	299.06	16.17	1.91	0.29	0.71	200.21	36.31	236.52	4.000	No	No	2.00
926	60.78	305.18	14.80	1.90	0.29	0.71	203.71	30.95	234.66	4.000	No	No	2.00
927	60.83	309.13	14.00	1.89	0.29	0.71	206.02	27.66	233.68	4.000	No	No	2.00
928	60.89	315.82	12.58	1.87	0.29	0.70	209.72	21.62	231.35	4.000	No	No	2.00
929	60.97	326.44	10.06	1.84	0.30	0.70	215.13	11.16	226.30	4.000	No	No	2.00
930	61.03	332.85	8.19	1.81	0.30	0.69	218.32	4.93	223.25	4.000	No	No	2.00
931	61.10	337.64	6.39	1.79	0.30	0.69	221.16	1.30	222.46	4.000	No	No	2.00
932	61.16	342.35	4.20	1.76	0.30	0.70	225.07	0.05	225.12	4.000	No	No	2.00
933	61.22	344.99	1.87	1.74	0.30	0.70	227.57	0.00	227.57	4.000	No	No	2.00
934	61.30	345.74	0.00	1.71	0.30	0.70	228.23	0.00	228.23	4.000	No	No	2.00
935	61.36	343.67	0.00	1.70	0.30	0.70	226.14	0.00	226.14	4.000	No	No	2.00
936	61.42	341.04	0.00	1.67	0.30	0.69	223.50	0.00	223.50	4.000	No	No	2.00
937	61.48	337.45	0.00	1.55	0.31	0.69	219.96	0.00	219.96	4.000	No	No	2.00
938	61.57	335.48	0.00	1.56	0.31	0.69	217.97	0.00	217.97	4.000	No	No	2.00
939	61.64	331.99	0.00	1.58	0.31	0.68	214.55	0.00	214.55	4.000	No	No	2.00
940	61.70	328.23	0.00	1.60	0.32	0.68	210.90	0.00	210.90	4.000	No	No	2.00
941	61.76	307.81	0.00	1.65	0.34	0.66	191.81	0.00	191.81	4.000	No	No	2.00
942	61.82	300.47	0.00	1.67	0.35	0.65	185.10	0.00	185.10	4.000	No	No	2.00
943	61.88	305.47	0.00	1.66	0.34	0.66	189.56	0.00	189.56	4.000	No	No	2.00
944	61.96	298.97	0.00	1.68	0.36	0.65	182.93	0.00	182.93	4.000	No	No	2.00
945	62.03	286.64	1.37	1.73	0.37	0.64	172.10	0.00	172.10	4.000	No	No	2.00
946	62.08	276.01	4.31	1.77	0.38	0.63	163.01	0.05	163.06	4.000	No	No	2.00
947	62.15	257.56	9.06	1.83	0.39	0.62	150.25	6.28	156.53	4.000	No	No	2.00
948	62.22	238.66	14.97	1.90	0.38	0.63	142.49	26.51	169.01	4.000	No	No	2.00
949	62.29	218.88	21.82	1.99	0.36	0.64	133.13	46.24	179.37	4.000	No	No	2.00
950	62.36	200.73	28.49	2.07	0.36	0.64	122.21	57.74	179.95	4.000	No	No	2.00
951	62.41	191.13	32.48	2.12	0.36	0.64	115.99	62.13	178.13	4.000	No	No	2.00
952	62.48	202.09	31.17	2.10	0.35	0.65	124.40	62.19	186.59	4.000	No	No	2.00
953	62.55	191.88	35.81	2.16	0.35	0.65	117.56	66.31	183.87	4.000	No	No	2.00
954	62.62	203.46	32.39	2.12	0.34	0.66	125.92	64.14	190.06	4.000	No	No	2.00
955	62.69	216.36	27.56	2.06	0.34	0.66	134.50	58.53	193.03	4.000	No	No	2.00
956	62.73	224.63	24.36	2.02	0.34	0.66	139.53	53.15	192.68	4.000	No	No	2.00
957	62.80	231.88	21.22	1.98	0.35	0.65	143.18	46.17	189.35	4.000	No	No	2.00
958	62.87	237.61	19.42	1.96	0.35	0.65	146.31	41.57	187.89	4.000	No	No	2.00
959	62.95	247.50	17.93	1.94	0.34	0.65	153.09	37.75	190.85	4.000	No	No	2.00
960	63.02	262.18	9.15	1.83	0.39	0.62	153.48	6.61	160.09	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	63.06	273.10	1.59	1.73	0.39	0.62	159.71	0.00	159.71	4.000	No	No	2.00
962	63.13	290.22	0.00	1.70	0.37	0.64	174.23	0.00	174.23	4.000	No	No	2.00
963	63.20	310.08	0.00	1.64	0.34	0.66	192.57	0.00	192.57	4.000	No	No	2.00
964	63.26	322.31	0.00	1.61	0.33	0.67	203.86	0.00	203.86	4.000	No	No	2.00
965	63.34	335.58	0.00	1.57	0.31	0.68	216.40	0.00	216.40	4.000	No	No	2.00
966	63.39	336.62	0.00	1.57	0.31	0.68	217.36	0.00	217.36	4.000	No	No	2.00
967	63.45	337.65	0.00	1.56	0.31	0.68	218.30	0.00	218.30	4.000	No	No	2.00
968	63.52	343.67	0.00	1.55	0.30	0.69	224.10	0.00	224.10	4.000	No	No	2.00
969	63.59	343.57	0.00	1.55	0.30	0.69	223.95	0.00	223.95	4.000	No	No	2.00
970	63.66	339.62	0.00	1.56	0.31	0.69	220.03	0.00	220.03	4.000	No	No	2.00
971	63.72	337.17	0.00	1.58	0.31	0.68	217.61	0.00	217.61	4.000	No	No	2.00
972	63.79	333.41	0.00	1.59	0.31	0.68	213.92	0.00	213.92	4.000	No	No	2.00
973	63.86	324.94	0.00	1.61	0.32	0.67	205.80	0.00	205.80	4.000	No	No	2.00
974	63.91	318.74	0.00	1.63	0.33	0.66	199.94	0.00	199.94	4.000	No	No	2.00
975	63.98	305.93	0.00	1.67	0.35	0.65	188.13	0.00	188.13	4.000	No	No	2.00
976	64.05	298.13	0.00	1.69	0.36	0.64	180.34	0.00	180.34	4.000	No	No	2.00
977	64.12	292.94	0.00	1.71	0.37	0.64	175.76	0.00	175.76	4.000	No	No	2.00
978	64.18	288.63	1.23	1.73	0.37	0.63	171.97	0.00	171.97	4.000	No	No	2.00
979	64.25	278.26	5.71	1.78	0.38	0.62	163.31	0.53	163.84	4.000	No	No	2.00
980	64.31	265.47	11.93	1.86	0.37	0.63	159.14	16.28	175.42	4.000	No	No	2.00
981	64.38	252.76	17.19	1.93	0.34	0.65	155.76	35.58	191.34	4.000	No	No	2.00
982	64.45	239.50	20.71	1.97	0.34	0.65	148.18	45.51	193.69	4.000	No	No	2.00
983	64.50	225.48	24.08	2.01	0.34	0.65	138.99	52.47	191.46	4.000	No	No	2.00
984	64.58	206.56	28.96	2.07	0.35	0.65	125.99	59.23	185.22	4.000	No	No	2.00
985	64.64	191.60	34.19	2.14	0.36	0.64	115.79	64.14	179.93	4.000	No	No	2.00
986	64.72	180.59	37.27	2.18	0.37	0.63	107.85	65.53	173.38	4.000	No	No	2.00
987	64.77	190.75	33.19	2.13	0.36	0.64	114.72	62.73	177.45	4.000	No	No	2.00
988	64.83	184.17	34.70	2.15	0.37	0.63	109.93	63.40	173.33	4.000	No	No	2.00
989	64.91	189.92	32.42	2.12	0.37	0.63	113.72	61.57	175.28	4.000	No	No	2.00
990	64.97	197.07	29.89	2.09	0.36	0.64	118.46	59.14	177.60	4.000	No	No	2.00
991	65.04	208.73	24.15	2.01	0.37	0.63	124.85	50.22	175.08	4.000	No	No	2.00
992	65.10	216.07	14.47	1.89	0.41	0.60	121.89	23.11	145.00	4.000	No	No	2.00
993	65.17	220.39	9.73	1.83	0.44	0.57	119.51	7.48	126.99	4.000	No	No	2.00
994	65.24	229.71	5.14	1.78	0.45	0.57	123.62	0.21	123.83	4.000	No	No	2.00
995	65.31	240.45	0.00	1.70	0.44	0.58	131.69	0.00	131.69	4.000	No	No	2.00
996	65.36	237.35	0.00	1.67	0.44	0.58	129.25	0.00	129.25	4.000	No	No	2.00
997	65.42	230.38	0.00	1.65	0.45	0.57	123.92	0.00	123.92	4.000	No	No	2.00
998	65.49	243.74	0.00	1.58	0.43	0.58	134.12	0.00	134.12	4.000	No	No	2.00
999	65.55	244.39	0.00	1.58	0.43	0.58	134.60	0.00	134.60	4.000	No	No	2.00
1000	65.62	239.21	0.00	1.58	0.44	0.58	130.54	0.00	130.54	4.000	No	No	2.00
1001	65.69	231.40	0.00	1.59	0.45	0.57	124.53	0.00	124.53	4.000	No	No	2.00
1002	65.76	221.99	0.00	1.62	0.46	0.56	117.11	0.00	117.11	4.000	No	No	2.00
1003	65.83	211.37	0.00	1.66	0.48	0.55	109.47	0.00	109.47	4.000	No	No	2.00
1004	65.89	204.02	0.00	1.69	0.49	0.54	103.99	0.00	103.99	4.000	No	No	2.00
1005	65.95	194.33	0.81	1.72	0.50	0.53	97.68	0.00	97.68	4.000	No	No	2.00
1006	66.03	178.52	5.24	1.78	0.53	0.52	87.08	0.22	87.30	4.000	No	No	2.00
1007	66.08	167.70	8.63	1.82	0.53	0.51	81.31	4.04	85.35	4.000	No	No	2.00
1008	66.16	152.64	14.75	1.90	0.50	0.53	76.50	20.38	96.88	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1009	66.22	142.95	19.36	1.95	0.49	0.54	73.13	31.93	105.06	4.000	No	No	2.00
1010	66.29	132.88	23.79	2.01	0.48	0.55	68.61	40.15	108.76	4.000	No	No	2.00
1011	66.36	125.83	26.87	2.05	0.48	0.55	65.07	44.38	109.45	4.000	No	No	2.00
1012	66.42	117.64	30.75	2.10	0.48	0.55	60.79	48.45	109.24	4.000	No	No	2.00
1013	66.49	109.63	34.90	2.15	0.48	0.55	56.48	51.63	108.10	4.000	No	No	2.00
1014	66.55	102.87	39.00	2.20	0.48	0.54	52.80	53.98	106.78	4.000	No	No	2.00
1015	66.62	97.68	44.74	2.27	0.48	0.54	50.15	56.81	106.96	4.000	No	No	2.00
1016	66.69	94.95	44.89	2.27	0.49	0.54	48.48	56.47	104.95	4.000	No	No	2.00
1017	66.75	93.35	42.80	2.25	0.49	0.54	47.27	55.03	102.29	4.000	No	No	2.00
1018	66.82	92.42	46.64	2.30	0.49	0.54	46.96	56.95	103.90	4.000	No	No	2.00
1019	66.89	89.59	53.07	2.38	0.49	0.54	45.71	59.30	105.02	4.000	No	No	2.00
1020	66.96	85.17	61.83	2.49	0.49	0.54	43.42	61.38	104.80	4.000	No	No	2.00
1021	67.00	74.54	72.12	2.61	0.50	0.53	37.43	0.00	37.43	4.000	No	Yes	2.00
1022	67.08	85.40	68.03	2.56	0.48	0.54	43.74	62.95	106.68	4.000	No	No	2.00
1023	67.14	82.07	70.24	2.59	0.49	0.54	41.79	62.84	104.62	4.000	No	No	2.00
1024	67.21	85.64	70.49	2.59	0.48	0.54	43.92	63.51	107.43	4.000	No	No	2.00
1025	67.28	90.07	72.14	2.61	0.47	0.55	46.63	0.00	46.63	4.000	No	Yes	2.00
1026	67.34	101.27	65.99	2.54	0.46	0.56	53.39	65.27	118.66	4.000	No	No	2.00
1027	67.41	121.21	54.64	2.40	0.44	0.57	65.74	65.32	131.06	4.000	No	No	2.00
1028	67.47	152.46	40.05	2.21	0.41	0.60	86.09	62.74	148.82	4.000	No	No	2.00
1029	67.54	180.12	29.21	2.08	0.39	0.61	103.77	55.20	158.97	4.000	No	No	2.00
1030	67.61	201.58	22.06	1.99	0.39	0.61	116.48	44.29	160.78	4.000	No	No	2.00
1031	67.67	227.55	14.18	1.89	0.40	0.60	129.08	22.67	151.75	4.000	No	No	2.00
1032	67.74	243.91	8.37	1.82	0.42	0.58	134.61	4.27	138.88	4.000	No	No	2.00
1033	67.80	254.63	2.29	1.74	0.42	0.59	141.18	0.00	141.18	4.000	No	No	2.00
1034	67.87	264.04	0.00	1.70	0.41	0.60	148.68	0.00	148.68	4.000	No	No	2.00
1035	67.94	270.90	0.00	1.70	0.40	0.60	154.23	0.00	154.23	4.000	No	No	2.00
1036	68.00	277.21	0.00	1.68	0.39	0.61	159.40	0.00	159.40	4.000	No	No	2.00
1037	68.07	281.26	0.00	1.68	0.39	0.61	162.74	0.00	162.74	4.000	No	No	2.00
1038	68.14	284.55	0.00	1.71	0.38	0.62	165.46	0.00	165.46	4.000	No	No	2.00
1039	68.20	286.63	0.00	1.69	0.38	0.62	167.17	0.00	167.17	4.000	No	No	2.00
1040	68.27	289.36	0.00	1.66	0.38	0.62	169.44	0.00	169.44	4.000	No	No	2.00
1041	68.34	291.15	0.00	1.67	0.37	0.62	170.92	0.00	170.92	4.000	No	No	2.00
1042	68.41	295.19	0.00	1.68	0.37	0.63	174.34	0.00	174.34	4.000	No	No	2.00
1043	68.44	296.79	0.00	1.68	0.37	0.63	175.70	0.00	175.70	4.000	No	No	2.00
1044	68.51	297.03	0.00	1.70	0.37	0.63	175.85	0.00	175.85	4.000	No	No	2.00
1045	68.58	297.26	0.00	1.70	0.37	0.63	175.99	0.00	175.99	4.000	No	No	2.00
1046	68.65	305.07	0.00	1.67	0.35	0.64	183.60	0.00	183.60	4.000	No	No	2.00
1047	68.73	308.27	0.00	1.66	0.35	0.64	186.41	0.00	186.41	4.000	No	No	2.00
1048	68.78	309.97	0.00	1.66	0.35	0.64	187.91	0.00	187.91	4.000	No	No	2.00
1049	68.83	310.62	0.00	1.66	0.35	0.64	188.45	0.00	188.45	4.000	No	No	2.00
1050	68.92	315.52	0.00	1.66	0.34	0.65	192.85	0.00	192.85	4.000	No	No	2.00
1051	68.97	319.56	0.00	1.66	0.34	0.65	196.52	0.00	196.52	4.000	No	No	2.00
1052	69.03	321.63	0.00	1.66	0.33	0.65	198.38	0.00	198.38	4.000	No	No	2.00
1053	69.09	323.33	0.00	1.66	0.33	0.65	199.91	0.00	199.91	4.000	No	No	2.00
1054	69.18	326.71	0.00	1.66	0.33	0.66	203.00	0.00	203.00	4.000	No	No	2.00
1055	69.24	331.33	0.00	1.66	0.32	0.66	207.30	0.00	207.30	4.000	No	No	2.00
1056	69.29	336.41	0.00	1.65	0.32	0.67	212.10	0.00	212.10	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1057	69.37	344.31	0.00	1.64	0.31	0.68	219.66	0.00	219.66	4.000	No	No	2.00
1058	69.43	348.73	0.00	1.63	0.30	0.68	223.93	0.00	223.93	4.000	No	No	2.00
1059	69.51	354.76	0.00	1.62	0.29	0.69	229.82	0.00	229.82	4.000	No	No	2.00
1060	69.57	356.65	0.00	1.60	0.29	0.69	231.64	0.00	231.64	4.000	No	No	2.00
1061	69.63	356.92	0.00	1.53	0.29	0.69	231.87	0.00	231.87	4.000	No	No	2.00
1062	69.69	354.94	0.00	1.52	0.29	0.69	229.84	0.00	229.84	4.000	No	No	2.00
1063	69.76	352.97	0.00	1.52	0.30	0.68	227.81	0.00	227.81	4.000	No	No	2.00
1064	69.82	354.20	0.00	1.53	0.29	0.68	228.98	0.00	228.98	4.000	No	No	2.00
1065	69.91	348.37	0.00	1.57	0.30	0.68	223.13	0.00	223.13	4.000	No	No	2.00
1066	69.95	234.12	12.57	1.87	0.41	0.59	130.67	17.11	147.78	4.000	No	No	2.00
1067	70.02	320.69	0.00	1.65	0.34	0.65	196.66	0.00	196.66	4.000	No	No	2.00
1068	70.08	315.41	0.00	1.66	0.34	0.64	191.76	0.00	191.76	4.000	No	No	2.00
1069	70.16	315.79	0.00	1.65	0.34	0.64	192.04	0.00	192.04	4.000	No	No	2.00
1070	70.22	305.34	0.00	1.67	0.35	0.63	182.53	0.00	182.53	4.000	No	No	2.00
1071	70.28	299.52	0.00	1.68	0.36	0.63	177.31	0.00	177.31	4.000	No	No	2.00
1072	70.35	297.92	0.00	1.68	0.37	0.62	175.10	0.00	175.10	4.000	No	No	2.00
1073	70.42	298.39	0.00	1.66	0.37	0.62	175.46	0.00	175.46	4.000	No	No	2.00
1074	70.48	297.92	0.00	1.65	0.37	0.62	174.99	0.00	174.99	4.000	No	No	2.00
1075	70.55	298.49	0.00	1.65	0.37	0.62	175.43	0.00	175.43	4.000	No	No	2.00
1076	70.61	299.24	0.00	1.64	0.37	0.62	176.03	0.00	176.03	4.000	No	No	2.00
1077	70.69	301.31	0.00	1.63	0.36	0.63	178.56	0.00	178.56	4.000	No	No	2.00
1078	70.75	303.10	0.00	1.61	0.36	0.63	180.10	0.00	180.10	4.000	No	No	2.00
1079	70.82	302.99	0.00	1.60	0.36	0.63	179.96	0.00	179.96	4.000	No	No	2.00
1080	70.88	299.13	0.00	1.60	0.37	0.62	175.73	0.00	175.73	4.000	No	No	2.00
1081	70.95	295.75	0.00	1.61	0.37	0.62	172.76	0.00	172.76	4.000	No	No	2.00
1082	71.02	290.67	0.00	1.63	0.38	0.61	168.35	0.00	168.35	4.000	No	No	2.00
1083	71.08	284.08	0.00	1.64	0.39	0.61	162.73	0.00	162.73	4.000	No	No	2.00
1084	71.15	281.81	0.00	1.61	0.39	0.60	160.79	0.00	160.79	4.000	No	No	2.00
1085	71.22	279.28	0.00	1.53	0.39	0.60	158.63	0.00	158.63	4.000	No	No	2.00
1086	71.28	276.83	0.00	1.54	0.40	0.60	156.55	0.00	156.55	4.000	No	No	2.00
1087	71.35	276.17	0.00	1.55	0.40	0.60	155.96	0.00	155.96	4.000	No	No	2.00
1088	71.42	276.46	0.00	1.58	0.40	0.60	156.15	0.00	156.15	4.000	No	No	2.00
1089	71.49	280.22	0.00	1.58	0.39	0.60	159.22	0.00	159.22	4.000	No	No	2.00
1090	71.54	276.32	0.00	1.60	0.40	0.60	155.95	0.00	155.95	4.000	No	No	2.00
1091	71.59	272.41	0.00	1.62	0.40	0.59	152.71	0.00	152.71	4.000	No	No	2.00
1092	71.67	283.98	0.00	1.60	0.39	0.60	162.23	0.00	162.23	4.000	No	No	2.00
1093	71.73	290.95	0.00	1.60	0.38	0.61	168.06	0.00	168.06	4.000	No	No	2.00
1094	71.79	293.96	0.00	1.61	0.37	0.61	170.59	0.00	170.59	4.000	No	No	2.00
1095	71.86	294.34	0.00	1.62	0.37	0.61	170.86	0.00	170.86	4.000	No	No	2.00
1096	71.92	292.45	0.00	1.63	0.38	0.61	169.20	0.00	169.20	4.000	No	No	2.00
1097	71.99	286.71	0.00	1.65	0.38	0.61	164.27	0.00	164.27	4.000	No	No	2.00
1098	72.06	277.21	0.00	1.67	0.40	0.60	156.30	0.00	156.30	4.000	No	No	2.00
1099	72.12	272.03	0.00	1.68	0.40	0.59	152.02	0.00	152.02	4.000	No	No	2.00
1100	72.19	265.26	0.00	1.70	0.41	0.58	146.49	0.00	146.49	4.000	No	No	2.00
1101	72.26	260.37	1.42	1.73	0.42	0.58	142.54	0.00	142.54	4.000	No	No	2.00
1102	72.31	256.41	5.69	1.78	0.42	0.58	139.59	0.48	140.07	4.000	No	No	2.00
1103	72.38	253.40	9.50	1.83	0.41	0.59	140.17	7.31	147.48	4.000	No	No	2.00
1104	72.46	252.18	9.27	1.83	0.41	0.58	138.86	6.63	145.49	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1105	72.52	253.97	1.71	1.73	0.43	0.57	137.31	0.00	137.31	4.000	No	No	2.00
1106	72.59	262.15	0.00	1.65	0.42	0.58	143.72	0.00	143.72	4.000	No	No	2.00
1107	72.65	268.46	0.00	1.68	0.41	0.59	148.74	0.00	148.74	4.000	No	No	2.00
1108	72.71	278.24	3.99	1.76	0.39	0.60	156.68	0.02	156.70	4.000	No	No	2.00
1109	72.78	282.58	10.16	1.84	0.37	0.62	164.88	10.08	174.96	4.000	No	No	2.00
1110	72.84	280.04	11.14	1.85	0.36	0.62	164.25	13.55	177.80	4.000	No	No	2.00
1111	72.90	282.86	5.79	1.78	0.39	0.60	160.63	0.58	161.21	4.000	No	No	2.00
1112	72.98	283.14	3.25	1.75	0.39	0.60	160.53	0.00	160.53	4.000	No	No	2.00
1113	73.03	295.38	0.58	1.72	0.37	0.61	170.82	0.00	170.82	4.000	No	No	2.00
1114	73.11	298.67	1.78	1.73	0.37	0.62	173.58	0.00	173.58	4.000	No	No	2.00
1115	73.17	295.67	5.33	1.78	0.37	0.61	171.11	0.33	171.44	4.000	No	No	2.00
1116	73.23	303.30	4.18	1.76	0.36	0.62	178.32	0.04	178.36	4.000	No	No	2.00
1117	73.30	301.42	5.61	1.78	0.36	0.62	176.84	0.49	177.32	4.000	No	No	2.00
1118	73.36	302.37	8.14	1.81	0.35	0.63	179.53	4.32	183.85	4.000	No	No	2.00
1119	73.44	314.97	6.67	1.80	0.34	0.64	189.40	1.56	190.95	4.000	No	No	2.00
1120	73.51	320.81	5.33	1.78	0.34	0.64	194.05	0.35	194.40	4.000	No	No	2.00
1121	73.56	315.02	4.89	1.77	0.35	0.63	188.62	0.17	188.79	4.000	No	No	2.00
1122	73.63	315.07	0.41	1.72	0.35	0.63	188.51	0.00	188.51	4.000	No	No	2.00
1123	73.70	327.49	0.00	1.69	0.33	0.65	199.89	0.00	199.89	4.000	No	No	2.00
1124	73.76	332.76	0.00	1.69	0.32	0.65	204.78	0.00	204.78	4.000	No	No	2.00
1125	73.83	330.98	0.00	1.69	0.33	0.65	203.04	0.00	203.04	4.000	No	No	2.00
1126	73.89	316.68	1.57	1.73	0.34	0.63	189.75	0.00	189.75	4.000	No	No	2.00
1127	73.95	324.04	1.04	1.73	0.34	0.64	196.43	0.00	196.43	4.000	No	No	2.00
1128	74.02	337.20	0.00	1.67	0.32	0.66	208.75	0.00	208.75	4.000	No	No	2.00
1129	74.09	336.63	0.00	1.62	0.32	0.65	208.15	0.00	208.15	4.000	No	No	2.00
1130	74.16	326.64	0.00	1.53	0.33	0.64	198.70	0.00	198.70	4.000	No	No	2.00
1131	74.24	330.59	0.00	1.48	0.33	0.65	202.33	0.00	202.33	4.000	No	No	2.00
1132	74.31	321.00	0.00	1.52	0.34	0.64	193.36	0.00	193.36	4.000	No	No	2.00
1133	74.38	307.35	0.00	1.56	0.36	0.62	180.96	0.00	180.96	4.000	No	No	2.00
1134	74.41	301.44	0.00	1.57	0.36	0.62	175.69	0.00	175.69	4.000	No	No	2.00
1135	74.48	290.99	0.00	1.58	0.38	0.60	165.91	0.00	165.91	4.000	No	No	2.00
1136	74.55	277.50	0.00	1.64	0.40	0.59	154.62	0.00	154.62	4.000	No	No	2.00
1137	74.62	257.79	0.00	1.69	0.42	0.57	138.77	0.00	138.77	4.000	No	No	2.00
1138	74.68	264.00	0.00	1.66	0.42	0.58	143.63	0.00	143.63	4.000	No	No	2.00
1139	74.75	271.34	0.00	1.64	0.41	0.58	149.46	0.00	149.46	4.000	No	No	2.00
1140	74.82	279.72	0.00	1.66	0.40	0.59	156.24	0.00	156.24	4.000	No	No	2.00
1141	74.89	286.02	0.00	1.66	0.39	0.60	161.42	0.00	161.42	4.000	No	No	2.00
1142	74.94	287.70	0.00	1.67	0.39	0.60	162.79	0.00	162.79	4.000	No	No	2.00
1143	75.01	286.29	0.00	1.70	0.39	0.60	161.56	0.00	161.56	4.000	No	No	2.00
1144	75.07	268.23	3.08	1.75	0.41	0.58	146.74	0.00	146.74	4.000	No	No	2.00
1145	75.14	273.59	100.00	4.06	0.26	0.70	181.92	0.00	181.92	4.000	No	Yes	2.00
1146	75.20	267.19	100.00	4.06	0.26	0.70	177.65	0.00	177.65	4.000	No	Yes	2.00
1147	75.27	264.93	100.00	4.06	0.26	0.70	176.14	0.00	176.14	4.000	No	Yes	2.00
1148	75.33	263.32	100.00	4.06	0.26	0.70	175.07	0.00	175.07	4.000	No	Yes	2.00
1149	75.41	262.66	100.00	4.06	0.26	0.70	174.62	0.00	174.62	4.000	No	Yes	2.00
1150	75.48	251.08	100.00	4.06	0.26	0.70	166.91	0.00	166.91	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
$CRR_{7.5}$:	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.07	2.00	0.00	0.00	0.00	0.00	0.14	2.00	0.00	0.00	0.00	0.00
0.20	2.00	0.00	0.00	0.00	0.00	0.27	2.00	0.00	0.00	0.00	0.00
0.35	2.00	0.00	0.00	0.00	0.00	0.41	2.00	0.00	0.00	0.00	0.00
0.47	2.00	0.00	0.00	0.00	0.00	0.54	2.00	0.00	0.00	0.00	0.00
0.60	2.00	0.00	0.00	0.00	0.00	0.66	2.00	0.00	0.00	0.00	0.00
0.74	2.00	0.00	0.00	0.00	0.00	0.80	2.00	0.00	0.00	0.00	0.00
0.87	2.00	0.00	0.00	0.00	0.00	0.93	2.00	0.00	0.00	0.00	0.00
0.99	2.00	0.00	0.00	0.00	0.00	1.05	2.00	0.00	0.00	0.00	0.00
1.12	2.00	0.00	0.00	0.00	0.00	1.19	2.00	0.00	0.00	0.00	0.00
1.27	2.00	0.00	0.00	0.00	0.00	1.32	2.00	0.00	0.00	0.00	0.00
1.38	2.00	0.00	0.00	0.00	0.00	1.45	2.00	0.00	0.00	0.00	0.00
1.51	2.00	0.00	0.00	0.00	0.00	1.59	2.00	0.00	0.00	0.00	0.00
1.65	2.00	0.00	0.00	0.00	0.00	1.71	2.00	0.00	0.00	0.00	0.00
1.77	2.00	0.00	0.00	0.00	0.00	1.84	2.00	0.00	0.00	0.00	0.00
1.92	2.00	0.00	0.00	0.00	0.00	1.98	2.00	0.00	0.00	0.00	0.00
2.04	2.00	0.00	0.00	0.00	0.00	2.11	2.00	0.00	0.00	0.00	0.00
2.17	2.00	0.00	0.00	0.00	0.00	2.23	2.00	0.00	0.00	0.00	0.00
2.30	2.00	0.00	0.00	0.00	0.00	2.37	2.00	0.00	0.00	0.00	0.00
2.43	2.00	0.00	0.00	0.00	0.00	2.49	2.00	0.00	0.00	0.00	0.00
2.56	2.00	0.00	0.00	0.00	0.00	2.65	2.00	0.00	0.00	0.00	0.00
2.71	2.00	0.00	0.00	0.00	0.00	2.78	2.00	0.00	0.00	0.00	0.00
2.83	2.00	0.00	0.00	0.00	0.00	2.90	2.00	0.00	0.00	0.00	0.00
2.96	2.00	0.00	0.00	0.00	0.00	3.03	2.00	0.00	0.00	0.00	0.00
3.11	2.00	0.00	0.00	0.00	0.00	3.16	2.00	0.00	0.00	0.00	0.00
3.22	2.00	0.00	0.00	0.00	0.00	3.28	2.00	0.00	0.00	0.00	0.00
3.36	2.00	0.00	0.00	0.00	0.00	3.44	2.00	0.00	0.00	0.00	0.00
3.49	2.00	0.00	0.00	0.00	0.00	3.56	2.00	0.00	0.00	0.00	0.00
3.61	2.00	0.00	0.00	0.00	0.00	3.69	2.00	0.00	0.00	0.00	0.00
3.74	2.00	0.00	0.00	0.00	0.00	3.83	2.00	0.00	0.00	0.00	0.00
3.88	2.00	0.00	0.00	0.00	0.00	3.96	2.00	0.00	0.00	0.00	0.00
4.00	2.00	0.00	0.00	0.00	0.00	4.08	2.00	0.00	0.00	0.00	0.00
4.16	2.00	0.00	0.00	0.00	0.00	4.21	2.00	0.00	0.00	0.00	0.00
4.29	2.00	0.00	0.00	0.00	0.00	4.34	2.00	0.00	0.00	0.00	0.00
4.40	2.00	0.00	0.00	0.00	0.00	4.47	2.00	0.00	0.00	0.00	0.00
4.55	2.00	0.00	0.00	0.00	0.00	4.60	2.00	0.00	0.00	0.00	0.00
4.68	2.00	0.00	0.00	0.00	0.00	4.73	2.00	0.00	0.00	0.00	0.00
4.81	2.00	0.00	0.00	0.00	0.00	4.87	2.00	0.00	0.00	0.00	0.00
4.92	2.00	0.00	0.00	0.00	0.00	5.00	2.00	0.00	0.00	0.00	0.00
5.08	2.00	0.00	0.00	0.08	0.00	5.13	2.00	0.00	0.00	0.05	0.00
5.19	2.00	0.00	0.00	0.07	0.00	5.27	2.00	0.00	0.00	0.08	0.00
5.32	2.00	0.00	0.00	0.05	0.00	5.39	2.00	0.00	0.00	0.08	0.00
5.45	2.00	0.00	0.00	0.05	0.00	5.53	2.00	0.00	0.00	0.08	0.00
5.58	2.00	0.00	0.00	0.05	0.00	5.66	2.00	0.00	0.00	0.08	0.00
5.72	2.00	0.00	0.00	0.05	0.00	5.80	2.00	0.00	0.00	0.08	0.00
5.85	2.00	0.00	0.00	0.05	0.00	5.91	2.00	0.00	0.00	0.05	0.00
5.99	2.00	0.00	0.00	0.08	0.00	6.04	2.00	0.00	0.00	0.05	0.00
6.12	2.00	0.00	0.00	0.08	0.00	6.18	2.00	0.00	0.00	0.05	0.00
6.26	2.00	0.00	0.00	0.08	0.00	6.31	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
6.39	2.00	0.00	0.00	0.08	0.00	6.44	2.00	0.00	0.00	0.05	0.00
6.52	2.00	0.00	0.00	0.08	0.00	6.58	2.00	0.00	0.00	0.05	0.00
6.63	2.00	0.00	0.00	0.05	0.00	6.71	2.00	0.00	0.00	0.08	0.00
6.77	2.00	0.00	0.00	0.05	0.00	6.85	2.00	0.00	0.00	0.08	0.00
6.91	2.00	0.00	0.00	0.06	0.00	6.96	2.00	0.00	0.00	0.05	0.00
7.04	2.00	0.00	0.00	0.08	0.00	7.09	2.00	0.00	0.00	0.05	0.00
7.17	2.00	0.00	0.00	0.08	0.00	7.22	2.00	0.00	0.00	0.05	0.00
7.31	2.00	0.00	0.00	0.08	0.00	7.36	2.00	0.00	0.00	0.05	0.00
7.44	2.00	0.00	0.00	0.08	0.00	7.49	2.00	0.00	0.00	0.05	0.00
7.55	2.00	0.00	0.00	0.06	0.00	7.63	2.00	0.00	0.00	0.08	0.00
7.68	2.00	0.00	0.00	0.05	0.00	7.76	2.00	0.00	0.00	0.08	0.00
7.81	2.00	0.00	0.00	0.05	0.00	7.89	2.00	0.00	0.00	0.08	0.00
7.95	2.00	0.00	0.00	0.05	0.00	8.03	1.50	0.00	0.00	0.08	0.00
8.09	1.34	0.00	0.00	0.05	0.00	8.14	1.18	0.00	0.00	0.05	0.00
8.22	1.01	0.00	0.00	0.08	0.00	8.27	0.89	0.00	0.00	0.05	0.02
8.35	0.75	0.25	1.16	0.08	0.05	8.40	0.67	0.33	0.81	0.05	0.05
8.48	0.59	0.41	0.60	0.08	0.09	8.54	0.55	0.45	0.54	0.05	0.07
8.62	0.52	0.48	0.50	0.08	0.10	8.67	0.50	0.50	0.48	0.05	0.07
8.73	0.48	0.52	0.45	0.05	0.07	8.81	0.45	0.55	0.43	0.08	0.12
8.86	0.46	0.54	0.44	0.05	0.07	8.94	0.48	0.52	0.46	0.08	0.11
9.00	0.50	0.50	0.48	0.05	0.07	9.08	0.52	0.48	0.50	0.08	0.10
9.13	0.53	0.47	0.51	0.06	0.07	9.20	0.53	0.47	0.51	0.06	0.08
9.26	0.53	0.47	0.51	0.07	0.08	9.33	0.52	0.48	0.51	0.07	0.08
9.39	0.44	0.56	0.42	0.07	0.10	9.46	0.25	0.75	0.30	0.07	0.13
9.53	0.28	0.72	0.31	0.07	0.13	9.60	0.30	0.70	0.32	0.07	0.12
9.67	0.24	0.76	0.29	0.07	0.13	9.73	0.21	0.79	0.28	0.07	0.14
9.79	0.23	0.77	0.29	0.05	0.10	9.86	0.24	0.76	0.29	0.07	0.15
9.91	0.25	0.75	0.30	0.05	0.10	9.98	0.26	0.74	0.30	0.07	0.13
10.04	0.28	0.72	0.31	0.06	0.12	10.11	0.28	0.72	0.31	0.07	0.12
10.18	0.30	0.70	0.32	0.07	0.13	10.25	0.32	0.68	0.33	0.07	0.12
10.31	0.33	0.67	0.34	0.06	0.10	10.37	0.35	0.65	0.35	0.06	0.10
10.44	0.36	0.64	0.36	0.07	0.12	10.51	0.35	0.65	0.35	0.07	0.11
10.57	0.34	0.66	0.34	0.07	0.12	10.64	0.31	0.69	0.33	0.07	0.12
10.71	0.29	0.71	0.32	0.07	0.12	10.77	0.27	0.73	0.31	0.07	0.12
10.84	0.26	0.74	0.30	0.07	0.13	10.91	0.24	0.76	0.30	0.07	0.13
10.98	0.24	0.76	0.29	0.07	0.14	11.05	0.24	0.76	0.29	0.07	0.13
11.11	0.24	0.76	0.29	0.07	0.13	11.18	0.23	0.77	0.29	0.07	0.13
11.25	0.23	0.77	0.29	0.07	0.13	11.31	0.24	0.76	0.29	0.07	0.13
11.38	0.24	0.76	0.29	0.07	0.13	11.45	0.24	0.76	0.29	0.07	0.13
11.51	0.24	0.76	0.29	0.07	0.12	11.58	0.23	0.77	0.29	0.07	0.13
11.65	0.23	0.77	0.29	0.07	0.13	11.68	0.23	0.77	0.29	0.03	0.07
11.75	0.22	0.78	0.29	0.07	0.13	11.82	0.22	0.78	0.28	0.07	0.13
11.88	0.21	0.79	0.28	0.07	0.13	11.97	0.21	0.79	0.28	0.08	0.16
12.03	0.22	0.78	0.28	0.06	0.13	12.10	0.21	0.79	0.28	0.07	0.13
12.16	0.22	0.78	0.28	0.06	0.13	12.23	0.22	0.78	0.28	0.07	0.13
12.30	0.22	0.78	0.28	0.07	0.13	12.36	0.22	0.78	0.29	0.07	0.13
12.43	0.23	0.77	0.29	0.07	0.13	12.50	0.23	0.77	0.29	0.07	0.13
12.53	0.24	0.76	0.29	0.03	0.06	12.60	0.25	0.75	0.30	0.07	0.13

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
12.67	0.27	0.73	0.31	0.07	0.12	12.74	0.28	0.72	0.31	0.07	0.12
12.80	0.30	0.70	0.32	0.07	0.11	12.87	0.31	0.69	0.33	0.07	0.11
12.94	0.33	0.67	0.34	0.07	0.11	13.00	0.35	0.65	0.35	0.07	0.11
13.07	0.35	0.65	0.35	0.07	0.10	13.13	0.36	0.64	0.36	0.07	0.10
13.20	0.37	0.63	0.37	0.06	0.10	13.27	0.38	0.62	0.37	0.07	0.10
13.34	0.39	0.61	0.38	0.07	0.10	13.40	0.43	0.57	0.41	0.07	0.09
13.47	0.46	0.54	0.44	0.07	0.09	13.54	0.49	0.51	0.47	0.07	0.08
13.60	0.52	0.48	0.50	0.07	0.08	13.67	0.55	0.45	0.54	0.07	0.08
13.74	0.57	0.43	0.58	0.07	0.07	13.80	0.62	0.38	0.67	0.06	0.06
13.87	0.68	0.32	0.84	0.07	0.05	13.94	0.72	0.28	1.01	0.07	0.05
14.00	0.74	0.26	1.13	0.07	0.04	14.07	0.64	0.36	0.71	0.07	0.06
14.14	0.57	0.43	0.58	0.07	0.07	14.21	0.59	0.41	0.60	0.07	0.07
14.24	0.60	0.40	0.63	0.04	0.03	14.31	0.63	0.37	0.70	0.07	0.06
14.37	0.62	0.38	0.68	0.06	0.06	14.46	0.62	0.38	0.67	0.08	0.07
14.52	0.64	0.36	0.72	0.07	0.06	14.59	0.68	0.32	0.85	0.07	0.05
14.65	0.72	0.28	1.03	0.06	0.04	14.72	0.74	0.26	1.14	0.06	0.04
14.79	0.76	0.00	0.00	0.07	0.04	14.85	0.75	0.00	0.00	0.07	0.04
14.92	0.75	0.25	1.17	0.07	0.04	14.99	0.75	0.00	0.00	0.07	0.04
15.05	0.76	0.00	0.00	0.07	0.04	15.12	0.74	0.26	1.12	0.07	0.04
15.19	0.72	0.28	1.02	0.07	0.04	15.22	0.72	0.28	1.00	0.03	0.02
15.29	0.70	0.30	0.93	0.07	0.05	15.36	0.68	0.32	0.83	0.07	0.05
15.43	0.65	0.35	0.76	0.07	0.05	15.49	0.63	0.37	0.70	0.07	0.06
15.56	0.60	0.40	0.63	0.07	0.06	15.63	0.56	0.44	0.56	0.07	0.07
15.69	0.52	0.48	0.50	0.07	0.07	15.76	0.46	0.54	0.44	0.07	0.08
15.82	0.41	0.59	0.40	0.07	0.09	15.89	0.37	0.63	0.36	0.07	0.10
15.96	0.32	0.68	0.33	0.07	0.11	16.03	0.27	0.73	0.31	0.07	0.11
16.10	0.24	0.76	0.29	0.07	0.12	16.16	0.21	0.79	0.28	0.07	0.12
16.23	0.19	0.81	0.27	0.07	0.12	16.30	2.00	0.00	0.00	0.07	0.00
16.36	2.00	0.00	0.00	0.07	0.00	16.43	2.00	0.00	0.00	0.07	0.00
16.50	2.00	0.00	0.00	0.07	0.00	16.56	0.17	0.83	0.26	0.07	0.13
16.63	0.17	0.83	0.27	0.07	0.13	16.70	2.00	0.00	0.00	0.07	0.00
16.73	2.00	0.00	0.00	0.04	0.00	16.80	2.00	0.00	0.00	0.07	0.00
16.87	2.00	0.00	0.00	0.07	0.00	16.94	2.00	0.00	0.00	0.07	0.00
17.00	0.21	0.79	0.28	0.06	0.12	17.08	0.23	0.77	0.29	0.08	0.14
17.14	0.25	0.75	0.30	0.06	0.10	17.20	0.29	0.71	0.32	0.06	0.10
17.27	0.33	0.67	0.34	0.07	0.10	17.34	0.39	0.61	0.38	0.06	0.09
17.40	0.43	0.57	0.41	0.06	0.08	17.47	0.47	0.53	0.44	0.07	0.08
17.53	0.51	0.49	0.49	0.07	0.07	17.60	0.55	0.45	0.55	0.07	0.07
17.67	0.59	0.41	0.61	0.07	0.06	17.73	0.61	0.39	0.66	0.07	0.06
17.80	0.62	0.38	0.67	0.07	0.06	17.87	0.62	0.38	0.67	0.07	0.06
17.93	0.60	0.40	0.62	0.07	0.06	18.00	0.57	0.43	0.57	0.07	0.06
18.07	0.52	0.48	0.50	0.07	0.07	18.14	0.46	0.54	0.44	0.07	0.08
18.20	0.40	0.60	0.38	0.07	0.09	18.27	0.34	0.66	0.34	0.07	0.10
18.34	0.29	0.71	0.32	0.07	0.11	18.37	0.27	0.73	0.31	0.03	0.05
18.44	0.24	0.76	0.29	0.07	0.11	18.51	0.21	0.79	0.28	0.07	0.12
18.57	2.00	0.00	0.00	0.07	0.00	18.64	2.00	0.00	0.00	0.07	0.00
18.71	2.00	0.00	0.00	0.07	0.00	18.78	2.00	0.00	0.00	0.07	0.00
18.84	2.00	0.00	0.00	0.07	0.00	18.91	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
18.98	2.00	0.00	0.00	0.07	0.00	19.04	2.00	0.00	0.00	0.07	0.00
19.11	2.00	0.00	0.00	0.07	0.00	19.18	2.00	0.00	0.00	0.07	0.00
19.24	2.00	0.00	0.00	0.07	0.00	19.31	2.00	0.00	0.00	0.07	0.00
19.38	2.00	0.00	0.00	0.07	0.00	19.44	2.00	0.00	0.00	0.07	0.00
19.51	2.00	0.00	0.00	0.07	0.00	19.58	2.00	0.00	0.00	0.07	0.00
19.63	2.00	0.00	0.00	0.05	0.00	19.69	2.00	0.00	0.00	0.06	0.00
19.76	0.15	0.85	0.26	0.06	0.12	19.82	0.16	0.84	0.26	0.07	0.12
19.89	0.15	0.85	0.26	0.07	0.12	19.95	2.00	0.00	0.00	0.06	0.00
20.02	2.00	0.00	0.00	0.06	0.00	20.09	2.00	0.00	0.00	0.07	0.00
20.16	2.00	0.00	0.00	0.07	0.00	20.23	2.00	0.00	0.00	0.07	0.00
20.29	2.00	0.00	0.00	0.07	0.00	20.36	2.00	0.00	0.00	0.07	0.00
20.42	2.00	0.00	0.00	0.07	0.00	20.49	2.00	0.00	0.00	0.07	0.00
20.56	2.00	0.00	0.00	0.07	0.00	20.63	2.00	0.00	0.00	0.07	0.00
20.69	2.00	0.00	0.00	0.07	0.00	20.76	2.00	0.00	0.00	0.07	0.00
20.83	0.16	0.84	0.26	0.07	0.12	20.89	0.16	0.84	0.26	0.07	0.12
20.96	0.16	0.84	0.26	0.07	0.12	21.03	2.00	0.00	0.00	0.07	0.00
21.09	2.00	0.00	0.00	0.07	0.00	21.16	2.00	0.00	0.00	0.07	0.00
21.23	2.00	0.00	0.00	0.07	0.00	21.26	2.00	0.00	0.00	0.03	0.00
21.33	2.00	0.00	0.00	0.07	0.00	21.40	2.00	0.00	0.00	0.07	0.00
21.46	2.00	0.00	0.00	0.07	0.00	21.53	2.00	0.00	0.00	0.07	0.00
21.60	2.00	0.00	0.00	0.07	0.00	21.66	2.00	0.00	0.00	0.06	0.00
21.73	2.00	0.00	0.00	0.07	0.00	21.80	2.00	0.00	0.00	0.07	0.00
21.86	2.00	0.00	0.00	0.07	0.00	21.93	2.00	0.00	0.00	0.07	0.00
22.00	2.00	0.00	0.00	0.07	0.00	22.06	2.00	0.00	0.00	0.07	0.00
22.13	2.00	0.00	0.00	0.07	0.00	22.19	2.00	0.00	0.00	0.07	0.00
22.26	2.00	0.00	0.00	0.07	0.00	22.33	2.00	0.00	0.00	0.07	0.00
22.40	2.00	0.00	0.00	0.07	0.00	22.46	2.00	0.00	0.00	0.07	0.00
22.53	2.00	0.00	0.00	0.07	0.00	22.60	0.19	0.81	0.27	0.07	0.11
22.66	0.20	0.80	0.28	0.07	0.11	22.73	0.20	0.80	0.28	0.06	0.10
22.80	0.21	0.79	0.28	0.07	0.11	22.86	0.23	0.77	0.29	0.07	0.10
22.93	0.26	0.74	0.30	0.07	0.10	23.00	0.26	0.74	0.30	0.07	0.10
23.03	0.25	0.75	0.30	0.03	0.05	23.10	0.25	0.75	0.30	0.07	0.10
23.17	0.25	0.75	0.30	0.07	0.10	23.24	0.26	0.74	0.30	0.07	0.10
23.30	0.28	0.72	0.31	0.07	0.09	23.37	0.27	0.73	0.31	0.07	0.09
23.43	0.33	0.67	0.34	0.07	0.09	23.50	0.34	0.66	0.35	0.07	0.08
23.56	0.34	0.66	0.35	0.06	0.08	23.63	0.34	0.66	0.34	0.07	0.09
23.70	0.35	0.65	0.35	0.07	0.09	23.76	0.39	0.61	0.38	0.07	0.08
23.83	0.43	0.57	0.41	0.07	0.07	23.90	0.44	0.56	0.42	0.07	0.07
23.96	0.43	0.57	0.41	0.07	0.07	24.03	0.39	0.61	0.38	0.07	0.08
24.10	0.33	0.67	0.34	0.07	0.09	24.17	0.28	0.72	0.31	0.07	0.09
24.23	0.23	0.77	0.29	0.07	0.10	24.30	0.20	0.80	0.28	0.07	0.10
24.37	0.17	0.83	0.27	0.07	0.10	24.43	2.00	0.00	0.00	0.07	0.00
24.50	2.00	0.00	0.00	0.07	0.00	24.57	2.00	0.00	0.00	0.07	0.00
24.63	2.00	0.00	0.00	0.07	0.00	24.70	2.00	0.00	0.00	0.07	0.00
24.77	2.00	0.00	0.00	0.07	0.00	24.84	2.00	0.00	0.00	0.07	0.00
24.87	2.00	0.00	0.00	0.04	0.00	24.94	2.00	0.00	0.00	0.07	0.00
25.01	0.16	0.84	0.26	0.07	0.10	25.07	0.18	0.82	0.27	0.07	0.11
25.14	0.20	0.80	0.28	0.07	0.10	25.21	0.24	0.76	0.29	0.07	0.09

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
25.28	0.29	0.71	0.32	0.07	0.09	25.34	0.36	0.64	0.36	0.07	0.08
25.41	0.44	0.56	0.42	0.07	0.07	25.48	0.46	0.54	0.44	0.07	0.06
25.54	0.39	0.61	0.38	0.07	0.08	25.61	0.35	0.65	0.35	0.07	0.08
25.68	0.31	0.69	0.33	0.07	0.09	25.75	0.27	0.73	0.31	0.07	0.09
25.81	0.23	0.77	0.29	0.07	0.10	25.87	0.19	0.81	0.27	0.05	0.08
25.93	0.18	0.82	0.27	0.06	0.09	26.00	2.00	0.00	0.00	0.07	0.00
26.06	2.00	0.00	0.00	0.07	0.00	26.13	2.00	0.00	0.00	0.07	0.00
26.20	2.00	0.00	0.00	0.07	0.00	26.27	2.00	0.00	0.00	0.07	0.00
26.33	2.00	0.00	0.00	0.07	0.00	26.40	2.00	0.00	0.00	0.07	0.00
26.47	2.00	0.00	0.00	0.07	0.00	26.53	2.00	0.00	0.00	0.07	0.00
26.60	2.00	0.00	0.00	0.07	0.00	26.66	2.00	0.00	0.00	0.07	0.00
26.73	2.00	0.00	0.00	0.07	0.00	26.80	2.00	0.00	0.00	0.07	0.00
26.86	2.00	0.00	0.00	0.07	0.00	26.93	2.00	0.00	0.00	0.07	0.00
27.00	2.00	0.00	0.00	0.07	0.00	27.06	0.17	0.83	0.26	0.07	0.10
27.13	0.18	0.82	0.27	0.07	0.10	27.17	0.19	0.81	0.27	0.03	0.05
27.23	0.19	0.81	0.27	0.07	0.10	27.30	0.18	0.82	0.27	0.07	0.10
27.37	0.17	0.83	0.27	0.07	0.10	27.43	2.00	0.00	0.00	0.07	0.00
27.50	2.00	0.00	0.00	0.07	0.00	27.57	2.00	0.00	0.00	0.07	0.00
27.64	2.00	0.00	0.00	0.07	0.00	27.70	2.00	0.00	0.00	0.07	0.00
27.77	2.00	0.00	0.00	0.07	0.00	27.84	2.00	0.00	0.00	0.07	0.00
27.91	0.16	0.84	0.26	0.07	0.10	27.98	0.16	0.84	0.26	0.07	0.10
28.04	0.18	0.82	0.27	0.07	0.10	28.09	0.17	0.83	0.27	0.05	0.07
28.16	0.20	0.80	0.28	0.07	0.09	28.22	0.22	0.78	0.28	0.07	0.09
28.28	0.23	0.77	0.29	0.06	0.08	28.35	0.24	0.76	0.29	0.07	0.09
28.42	0.25	0.75	0.30	0.07	0.09	28.49	0.27	0.73	0.31	0.07	0.08
28.55	0.28	0.72	0.31	0.06	0.08	28.62	0.29	0.71	0.32	0.07	0.08
28.69	0.31	0.69	0.33	0.07	0.08	28.75	0.33	0.67	0.34	0.07	0.08
28.82	0.35	0.65	0.35	0.07	0.07	28.89	0.37	0.63	0.36	0.07	0.07
28.95	0.38	0.62	0.37	0.07	0.07	29.02	0.39	0.61	0.38	0.07	0.07
29.09	0.39	0.61	0.38	0.07	0.07	29.16	0.38	0.62	0.37	0.07	0.07
29.22	0.35	0.65	0.35	0.07	0.07	29.29	0.31	0.69	0.33	0.07	0.08
29.35	0.27	0.73	0.31	0.07	0.08	29.42	0.24	0.76	0.29	0.07	0.09
29.49	0.21	0.79	0.28	0.07	0.09	29.55	0.19	0.81	0.27	0.07	0.09
29.62	2.00	0.00	0.00	0.07	0.00	29.69	2.00	0.00	0.00	0.07	0.00
29.76	2.00	0.00	0.00	0.07	0.00	29.82	2.00	0.00	0.00	0.07	0.00
29.86	2.00	0.00	0.00	0.03	0.00	29.92	2.00	0.00	0.00	0.07	0.00
30.00	2.00	0.00	0.00	0.07	0.00	30.06	2.00	0.00	0.00	0.06	0.00
30.13	2.00	0.00	0.00	0.07	0.00	30.20	2.00	0.00	0.00	0.07	0.00
30.27	2.00	0.00	0.00	0.06	0.00	30.34	2.00	0.00	0.00	0.07	0.00
30.40	2.00	0.00	0.00	0.07	0.00	30.47	2.00	0.00	0.00	0.07	0.00
30.54	2.00	0.00	0.00	0.07	0.00	30.61	2.00	0.00	0.00	0.07	0.00
30.67	2.00	0.00	0.00	0.07	0.00	30.74	2.00	0.00	0.00	0.07	0.00
30.81	2.00	0.00	0.00	0.07	0.00	30.87	2.00	0.00	0.00	0.07	0.00
30.91	2.00	0.00	0.00	0.03	0.00	30.97	2.00	0.00	0.00	0.07	0.00
31.04	2.00	0.00	0.00	0.07	0.00	31.11	2.00	0.00	0.00	0.07	0.00
31.17	2.00	0.00	0.00	0.07	0.00	31.24	2.00	0.00	0.00	0.07	0.00
31.31	2.00	0.00	0.00	0.07	0.00	31.38	2.00	0.00	0.00	0.07	0.00
31.44	2.00	0.00	0.00	0.07	0.00	31.51	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
31.57	2.00	0.00	0.00	0.07	0.00	31.64	2.00	0.00	0.00	0.07	0.00
31.71	2.00	0.00	0.00	0.07	0.00	31.77	2.00	0.00	0.00	0.07	0.00
31.84	2.00	0.00	0.00	0.07	0.00	31.91	2.00	0.00	0.00	0.07	0.00
31.97	2.00	0.00	0.00	0.07	0.00	32.04	2.00	0.00	0.00	0.07	0.00
32.11	2.00	0.00	0.00	0.07	0.00	32.18	2.00	0.00	0.00	0.07	0.00
32.24	2.00	0.00	0.00	0.07	0.00	32.31	2.00	0.00	0.00	0.06	0.00
32.36	2.00	0.00	0.00	0.06	0.00	32.43	2.00	0.00	0.00	0.06	0.00
32.49	2.00	0.00	0.00	0.07	0.00	32.56	2.00	0.00	0.00	0.06	0.00
32.62	2.00	0.00	0.00	0.06	0.00	32.70	2.00	0.00	0.00	0.07	0.00
32.75	2.00	0.00	0.00	0.06	0.00	32.83	2.00	0.00	0.00	0.08	0.00
32.88	2.00	0.00	0.00	0.05	0.00	32.96	2.00	0.00	0.00	0.08	0.00
33.01	2.00	0.00	0.00	0.05	0.00	33.08	2.00	0.00	0.00	0.07	0.00
33.16	2.00	0.00	0.00	0.08	0.00	33.22	2.00	0.00	0.00	0.06	0.00
33.29	2.00	0.00	0.00	0.08	0.00	33.34	2.00	0.00	0.00	0.05	0.00
33.40	2.00	0.00	0.00	0.06	0.00	33.47	2.00	0.00	0.00	0.06	0.00
33.56	2.00	0.00	0.00	0.09	0.00	33.62	2.00	0.00	0.00	0.06	0.00
33.68	2.00	0.00	0.00	0.06	0.00	33.73	2.00	0.00	0.00	0.06	0.00
33.82	2.00	0.00	0.00	0.09	0.00	33.89	2.00	0.00	0.00	0.06	0.00
33.95	2.00	0.00	0.00	0.07	0.00	34.02	2.00	0.00	0.00	0.07	0.00
34.09	2.00	0.00	0.00	0.07	0.00	34.15	2.00	0.00	0.00	0.07	0.00
34.22	2.00	0.00	0.00	0.07	0.00	34.25	2.00	0.00	0.00	0.03	0.00
34.32	2.00	0.00	0.00	0.07	0.00	34.39	2.00	0.00	0.00	0.07	0.00
34.45	2.00	0.00	0.00	0.07	0.00	34.52	2.00	0.00	0.00	0.07	0.00
34.59	2.00	0.00	0.00	0.07	0.00	34.65	2.00	0.00	0.00	0.07	0.00
34.72	2.00	0.00	0.00	0.07	0.00	34.79	2.00	0.00	0.00	0.07	0.00
34.85	2.00	0.00	0.00	0.07	0.00	34.92	2.00	0.00	0.00	0.07	0.00
34.99	2.00	0.00	0.00	0.07	0.00	35.05	2.00	0.00	0.00	0.07	0.00
35.13	2.00	0.00	0.00	0.07	0.00	35.19	2.00	0.00	0.00	0.06	0.00
35.27	2.00	0.00	0.00	0.08	0.00	35.34	2.00	0.00	0.00	0.07	0.00
35.37	2.00	0.00	0.00	0.03	0.00	35.44	2.00	0.00	0.00	0.07	0.00
35.51	2.00	0.00	0.00	0.07	0.00	35.57	2.00	0.00	0.00	0.07	0.00
35.64	2.00	0.00	0.00	0.07	0.00	35.70	2.00	0.00	0.00	0.06	0.00
35.77	2.00	0.00	0.00	0.07	0.00	35.84	2.00	0.00	0.00	0.07	0.00
35.90	2.00	0.00	0.00	0.07	0.00	35.97	2.00	0.00	0.00	0.07	0.00
36.03	2.00	0.00	0.00	0.07	0.00	36.10	2.00	0.00	0.00	0.07	0.00
36.17	2.00	0.00	0.00	0.07	0.00	36.24	2.00	0.00	0.00	0.07	0.00
36.30	2.00	0.00	0.00	0.07	0.00	36.37	2.00	0.00	0.00	0.07	0.00
36.44	2.00	0.00	0.00	0.06	0.00	36.51	2.00	0.00	0.00	0.07	0.00
36.57	2.00	0.00	0.00	0.07	0.00	36.64	2.00	0.00	0.00	0.07	0.00
36.71	2.00	0.00	0.00	0.07	0.00	36.77	2.00	0.00	0.00	0.07	0.00
36.84	2.00	0.00	0.00	0.07	0.00	36.91	2.00	0.00	0.00	0.07	0.00
36.98	2.00	0.00	0.00	0.07	0.00	37.01	2.00	0.00	0.00	0.04	0.00
37.08	2.00	0.00	0.00	0.07	0.00	37.15	2.00	0.00	0.00	0.07	0.00
37.21	2.00	0.00	0.00	0.07	0.00	37.28	2.00	0.00	0.00	0.07	0.00
37.34	2.00	0.00	0.00	0.07	0.00	37.41	2.00	0.00	0.00	0.07	0.00
37.48	2.00	0.00	0.00	0.07	0.00	37.55	2.00	0.00	0.00	0.07	0.00
37.61	2.00	0.00	0.00	0.07	0.00	37.68	2.00	0.00	0.00	0.07	0.00
37.75	2.00	0.00	0.00	0.07	0.00	37.81	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
37.88	2.00	0.00	0.00	0.07	0.00	37.95	2.00	0.00	0.00	0.07	0.00
38.02	2.00	0.00	0.00	0.06	0.00	38.08	2.00	0.00	0.00	0.06	0.00
38.15	2.00	0.00	0.00	0.07	0.00	38.21	2.00	0.00	0.00	0.07	0.00
38.28	2.00	0.00	0.00	0.07	0.00	38.35	2.00	0.00	0.00	0.07	0.00
38.41	2.00	0.00	0.00	0.07	0.00	38.48	2.00	0.00	0.00	0.07	0.00
38.55	2.00	0.00	0.00	0.07	0.00	38.58	2.00	0.00	0.00	0.03	0.00
38.65	2.00	0.00	0.00	0.07	0.00	38.72	2.00	0.00	0.00	0.07	0.00
38.78	2.00	0.00	0.00	0.07	0.00	38.85	2.00	0.00	0.00	0.07	0.00
38.92	2.00	0.00	0.00	0.07	0.00	38.98	2.00	0.00	0.00	0.07	0.00
39.05	2.00	0.00	0.00	0.07	0.00	39.12	2.00	0.00	0.00	0.07	0.00
39.18	2.00	0.00	0.00	0.07	0.00	39.25	2.00	0.00	0.00	0.07	0.00
39.32	2.00	0.00	0.00	0.07	0.00	39.38	2.00	0.00	0.00	0.07	0.00
39.45	2.00	0.00	0.00	0.07	0.00	39.52	2.00	0.00	0.00	0.07	0.00
39.58	2.00	0.00	0.00	0.07	0.00	39.65	2.00	0.00	0.00	0.07	0.00
39.72	2.00	0.00	0.00	0.07	0.00	39.78	2.00	0.00	0.00	0.07	0.00
39.85	2.00	0.00	0.00	0.07	0.00	39.92	2.00	0.00	0.00	0.07	0.00
39.97	2.00	0.00	0.00	0.05	0.00	40.04	2.00	0.00	0.00	0.07	0.00
40.09	2.00	0.00	0.00	0.05	0.00	40.17	2.00	0.00	0.00	0.08	0.00
40.23	2.00	0.00	0.00	0.05	0.00	40.31	2.00	0.00	0.00	0.08	0.00
40.37	2.00	0.00	0.00	0.06	0.00	40.44	2.00	0.00	0.00	0.07	0.00
40.51	2.00	0.00	0.00	0.07	0.00	40.57	2.00	0.00	0.00	0.07	0.00
40.64	2.00	0.00	0.00	0.07	0.00	40.71	2.00	0.00	0.00	0.07	0.00
40.77	2.00	0.00	0.00	0.07	0.00	40.84	2.00	0.00	0.00	0.07	0.00
40.91	2.00	0.00	0.00	0.07	0.00	40.97	2.00	0.00	0.00	0.06	0.00
41.04	2.00	0.00	0.00	0.07	0.00	41.11	2.00	0.00	0.00	0.07	0.00
41.17	2.00	0.00	0.00	0.07	0.00	41.24	2.00	0.00	0.00	0.06	0.00
41.30	2.00	0.00	0.00	0.06	0.00	41.37	2.00	0.00	0.00	0.07	0.00
41.41	2.00	0.00	0.00	0.04	0.00	41.48	2.00	0.00	0.00	0.07	0.00
41.54	2.00	0.00	0.00	0.06	0.00	41.60	2.00	0.00	0.00	0.06	0.00
41.67	2.00	0.00	0.00	0.07	0.00	41.74	0.22	0.78	0.29	0.07	0.06
41.80	0.23	0.77	0.29	0.06	0.05	41.87	0.25	0.75	0.30	0.07	0.06
41.94	0.29	0.71	0.32	0.07	0.05	42.00	0.35	0.65	0.35	0.07	0.05
42.07	0.41	0.59	0.39	0.06	0.04	42.14	0.45	0.55	0.43	0.07	0.04
42.19	0.52	0.48	0.50	0.05	0.03	42.26	0.50	0.50	0.48	0.07	0.04
42.34	0.56	0.44	0.57	0.07	0.04	42.40	0.53	0.47	0.52	0.06	0.03
42.46	0.53	0.47	0.52	0.06	0.03	42.53	0.51	0.49	0.49	0.07	0.04
42.60	0.49	0.51	0.46	0.07	0.04	42.67	0.44	0.56	0.42	0.07	0.04
42.73	0.38	0.62	0.37	0.07	0.04	42.80	0.33	0.67	0.34	0.07	0.05
42.87	0.28	0.72	0.31	0.07	0.05	42.94	0.23	0.77	0.29	0.07	0.05
43.00	0.21	0.79	0.28	0.07	0.06	43.07	0.19	0.81	0.27	0.07	0.06
43.14	0.19	0.81	0.27	0.07	0.06	43.20	0.19	0.81	0.27	0.07	0.06
43.27	0.19	0.81	0.27	0.07	0.06	43.34	0.19	0.81	0.27	0.07	0.06
43.39	0.19	0.81	0.27	0.05	0.04	43.47	0.19	0.81	0.27	0.08	0.07
43.54	2.00	0.00	0.00	0.07	0.00	43.60	2.00	0.00	0.00	0.06	0.00
43.67	2.00	0.00	0.00	0.07	0.00	43.73	2.00	0.00	0.00	0.07	0.00
43.80	2.00	0.00	0.00	0.07	0.00	43.83	2.00	0.00	0.00	0.03	0.00
43.90	2.00	0.00	0.00	0.07	0.00	43.97	2.00	0.00	0.00	0.07	0.00
44.03	2.00	0.00	0.00	0.07	0.00	44.10	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
44.17	2.00	0.00	0.00	0.07	0.00	44.23	2.00	0.00	0.00	0.07	0.00
44.30	2.00	0.00	0.00	0.07	0.00	44.37	2.00	0.00	0.00	0.07	0.00
44.44	2.00	0.00	0.00	0.07	0.00	44.50	2.00	0.00	0.00	0.07	0.00
44.57	2.00	0.00	0.00	0.07	0.00	44.64	2.00	0.00	0.00	0.07	0.00
44.70	2.00	0.00	0.00	0.07	0.00	44.77	2.00	0.00	0.00	0.07	0.00
44.84	2.00	0.00	0.00	0.06	0.00	44.90	2.00	0.00	0.00	0.07	0.00
44.97	0.18	0.82	0.27	0.07	0.05	45.04	0.19	0.81	0.27	0.07	0.05
45.11	0.20	0.80	0.28	0.07	0.05	45.17	0.21	0.79	0.28	0.07	0.05
45.24	0.21	0.79	0.28	0.06	0.05	45.31	0.22	0.78	0.28	0.07	0.05
45.37	0.22	0.78	0.29	0.07	0.05	45.44	0.23	0.77	0.29	0.07	0.05
45.48	0.23	0.77	0.29	0.03	0.02	45.54	0.24	0.76	0.29	0.07	0.05
45.61	0.25	0.75	0.30	0.07	0.05	45.69	0.24	0.76	0.30	0.09	0.06
45.76	0.26	0.74	0.30	0.06	0.04	45.83	0.26	0.74	0.30	0.07	0.05
45.89	0.25	0.75	0.30	0.07	0.05	45.96	0.25	0.75	0.30	0.07	0.05
46.03	0.25	0.75	0.30	0.07	0.04	46.09	0.25	0.75	0.30	0.07	0.05
46.16	0.25	0.75	0.30	0.06	0.04	46.23	0.25	0.75	0.30	0.07	0.04
46.29	0.26	0.74	0.30	0.07	0.04	46.36	0.26	0.74	0.30	0.07	0.04
46.42	0.26	0.74	0.30	0.06	0.04	46.46	0.26	0.74	0.30	0.03	0.02
46.53	0.26	0.74	0.30	0.07	0.04	46.59	0.25	0.75	0.30	0.07	0.04
46.66	0.25	0.75	0.30	0.07	0.04	46.73	0.25	0.75	0.30	0.07	0.05
46.80	0.25	0.75	0.30	0.07	0.04	46.86	0.25	0.75	0.30	0.07	0.04
46.93	0.25	0.75	0.30	0.06	0.04	46.99	0.24	0.76	0.30	0.07	0.04
47.06	0.24	0.76	0.29	0.07	0.04	47.13	0.24	0.76	0.29	0.07	0.04
47.20	0.23	0.77	0.29	0.07	0.04	47.26	0.22	0.78	0.29	0.07	0.04
47.33	0.21	0.79	0.28	0.07	0.05	47.40	0.21	0.79	0.28	0.07	0.05
47.47	0.20	0.80	0.28	0.07	0.05	47.53	0.20	0.80	0.28	0.07	0.04
47.60	0.19	0.81	0.27	0.07	0.04	47.66	0.19	0.81	0.27	0.07	0.04
47.73	0.19	0.81	0.27	0.07	0.04	47.80	0.19	0.81	0.27	0.07	0.04
47.87	0.19	0.81	0.27	0.07	0.04	47.93	0.18	0.82	0.27	0.07	0.04
48.00	0.18	0.82	0.27	0.07	0.05	48.03	0.17	0.83	0.27	0.03	0.02
48.10	0.16	0.84	0.26	0.07	0.05	48.17	2.00	0.00	0.00	0.07	0.00
48.24	2.00	0.00	0.00	0.07	0.00	48.30	2.00	0.00	0.00	0.07	0.00
48.37	2.00	0.00	0.00	0.07	0.00	48.43	2.00	0.00	0.00	0.06	0.00
48.50	2.00	0.00	0.00	0.07	0.00	48.56	2.00	0.00	0.00	0.06	0.00
48.63	2.00	0.00	0.00	0.07	0.00	48.70	2.00	0.00	0.00	0.07	0.00
48.76	2.00	0.00	0.00	0.06	0.00	48.82	2.00	0.00	0.00	0.06	0.00
48.89	2.00	0.00	0.00	0.06	0.00	48.95	2.00	0.00	0.00	0.07	0.00
49.02	2.00	0.00	0.00	0.06	0.00	49.09	2.00	0.00	0.00	0.07	0.00
49.15	2.00	0.00	0.00	0.06	0.00	49.23	2.00	0.00	0.00	0.08	0.00
49.28	2.00	0.00	0.00	0.05	0.00	49.35	2.00	0.00	0.00	0.07	0.00
49.42	2.00	0.00	0.00	0.07	0.00	49.48	2.00	0.00	0.00	0.06	0.00
49.55	2.00	0.00	0.00	0.07	0.00	49.62	2.00	0.00	0.00	0.07	0.00
49.69	2.00	0.00	0.00	0.07	0.00	49.75	2.00	0.00	0.00	0.07	0.00
49.82	2.00	0.00	0.00	0.07	0.00	49.87	2.00	0.00	0.00	0.05	0.00
49.94	2.00	0.00	0.00	0.07	0.00	50.02	2.00	0.00	0.00	0.07	0.00
50.07	2.00	0.00	0.00	0.05	0.00	50.16	2.00	0.00	0.00	0.09	0.00
50.21	2.00	0.00	0.00	0.05	0.00	50.27	2.00	0.00	0.00	0.06	0.00
50.33	2.00	0.00	0.00	0.06	0.00	50.40	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
50.47	2.00	0.00	0.00	0.07	0.00	50.53	2.00	0.00	0.00	0.06	0.00
50.61	2.00	0.00	0.00	0.08	0.00	50.66	2.00	0.00	0.00	0.05	0.00
50.73	2.00	0.00	0.00	0.07	0.00	50.80	2.00	0.00	0.00	0.07	0.00
50.87	2.00	0.00	0.00	0.07	0.00	50.92	2.00	0.00	0.00	0.05	0.00
51.01	2.00	0.00	0.00	0.09	0.00	51.07	2.00	0.00	0.00	0.06	0.00
51.13	2.00	0.00	0.00	0.06	0.00	51.20	2.00	0.00	0.00	0.07	0.00
51.26	2.00	0.00	0.00	0.06	0.00	51.32	2.00	0.00	0.00	0.06	0.00
51.39	2.00	0.00	0.00	0.07	0.00	51.45	2.00	0.00	0.00	0.07	0.00
51.52	2.00	0.00	0.00	0.07	0.00	51.59	2.00	0.00	0.00	0.07	0.00
51.65	2.00	0.00	0.00	0.06	0.00	51.71	2.00	0.00	0.00	0.06	0.00
51.78	2.00	0.00	0.00	0.08	0.00	51.84	2.00	0.00	0.00	0.06	0.00
51.92	2.00	0.00	0.00	0.07	0.00	51.97	2.00	0.00	0.00	0.06	0.00
52.04	2.00	0.00	0.00	0.07	0.00	52.10	2.00	0.00	0.00	0.06	0.00
52.17	2.00	0.00	0.00	0.07	0.00	52.23	2.00	0.00	0.00	0.06	0.00
52.30	2.00	0.00	0.00	0.06	0.00	52.37	2.00	0.00	0.00	0.07	0.00
52.44	2.00	0.00	0.00	0.07	0.00	52.50	2.00	0.00	0.00	0.06	0.00
52.56	2.00	0.00	0.00	0.06	0.00	52.63	2.00	0.00	0.00	0.07	0.00
52.69	2.00	0.00	0.00	0.06	0.00	52.77	2.00	0.00	0.00	0.08	0.00
52.85	2.00	0.00	0.00	0.08	0.00	52.92	2.00	0.00	0.00	0.06	0.00
52.98	2.00	0.00	0.00	0.07	0.00	53.05	2.00	0.00	0.00	0.07	0.00
53.09	2.00	0.00	0.00	0.03	0.00	53.15	2.00	0.00	0.00	0.07	0.00
53.22	2.00	0.00	0.00	0.07	0.00	53.29	2.00	0.00	0.00	0.07	0.00
53.36	2.00	0.00	0.00	0.07	0.00	53.41	2.00	0.00	0.00	0.06	0.00
53.48	2.00	0.00	0.00	0.07	0.00	53.55	2.00	0.00	0.00	0.06	0.00
53.61	2.00	0.00	0.00	0.06	0.00	53.69	2.00	0.00	0.00	0.08	0.00
53.74	2.00	0.00	0.00	0.05	0.00	53.81	2.00	0.00	0.00	0.06	0.00
53.89	2.00	0.00	0.00	0.08	0.00	53.95	2.00	0.00	0.00	0.06	0.00
54.01	2.00	0.00	0.00	0.06	0.00	54.07	2.00	0.00	0.00	0.06	0.00
54.15	2.00	0.00	0.00	0.07	0.00	54.22	2.00	0.00	0.00	0.07	0.00
54.27	2.00	0.00	0.00	0.05	0.00	54.35	2.00	0.00	0.00	0.08	0.00
54.40	2.00	0.00	0.00	0.06	0.00	54.48	2.00	0.00	0.00	0.08	0.00
54.53	2.00	0.00	0.00	0.06	0.00	54.60	2.00	0.00	0.00	0.06	0.00
54.66	2.00	0.00	0.00	0.07	0.00	54.73	2.00	0.00	0.00	0.07	0.00
54.80	2.00	0.00	0.00	0.07	0.00	54.86	2.00	0.00	0.00	0.07	0.00
54.93	2.00	0.00	0.00	0.07	0.00	55.00	2.00	0.00	0.00	0.07	0.00
55.06	2.00	0.00	0.00	0.07	0.00	55.13	2.00	0.00	0.00	0.07	0.00
55.20	2.00	0.00	0.00	0.07	0.00	55.27	2.00	0.00	0.00	0.07	0.00
55.34	2.00	0.00	0.00	0.07	0.00	55.40	2.00	0.00	0.00	0.07	0.00
55.47	2.00	0.00	0.00	0.07	0.00	55.53	2.00	0.00	0.00	0.06	0.00
55.60	2.00	0.00	0.00	0.07	0.00	55.67	2.00	0.00	0.00	0.07	0.00
55.73	2.00	0.00	0.00	0.07	0.00	55.80	2.00	0.00	0.00	0.07	0.00
55.87	2.00	0.00	0.00	0.07	0.00	55.93	2.00	0.00	0.00	0.06	0.00
55.98	2.00	0.00	0.00	0.05	0.00	56.05	2.00	0.00	0.00	0.07	0.00
56.10	2.00	0.00	0.00	0.06	0.00	56.19	2.00	0.00	0.00	0.09	0.00
56.24	2.00	0.00	0.00	0.05	0.00	56.31	2.00	0.00	0.00	0.07	0.00
56.38	2.00	0.00	0.00	0.07	0.00	56.46	2.00	0.00	0.00	0.08	0.00
56.52	2.00	0.00	0.00	0.06	0.00	56.58	2.00	0.00	0.00	0.07	0.00
56.65	2.00	0.00	0.00	0.06	0.00	56.71	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
56.77	2.00	0.00	0.00	0.06	0.00	56.83	2.00	0.00	0.00	0.06	0.00
56.90	2.00	0.00	0.00	0.06	0.00	56.96	2.00	0.00	0.00	0.07	0.00
57.03	2.00	0.00	0.00	0.07	0.00	57.10	2.00	0.00	0.00	0.07	0.00
57.16	2.00	0.00	0.00	0.07	0.00	57.23	2.00	0.00	0.00	0.07	0.00
57.30	2.00	0.00	0.00	0.07	0.00	57.37	2.00	0.00	0.00	0.07	0.00
57.43	2.00	0.00	0.00	0.07	0.00	57.50	2.00	0.00	0.00	0.07	0.00
57.57	2.00	0.00	0.00	0.07	0.00	57.62	2.00	0.00	0.00	0.05	0.00
57.68	2.00	0.00	0.00	0.06	0.00	57.76	2.00	0.00	0.00	0.08	0.00
57.82	2.00	0.00	0.00	0.06	0.00	57.88	2.00	0.00	0.00	0.06	0.00
57.94	2.00	0.00	0.00	0.06	0.00	58.01	2.00	0.00	0.00	0.06	0.00
58.08	2.00	0.00	0.00	0.08	0.00	58.14	2.00	0.00	0.00	0.06	0.00
58.21	2.00	0.00	0.00	0.07	0.00	58.28	2.00	0.00	0.00	0.07	0.00
58.35	2.00	0.00	0.00	0.07	0.00	58.40	2.00	0.00	0.00	0.05	0.00
58.47	2.00	0.00	0.00	0.07	0.00	58.54	2.00	0.00	0.00	0.07	0.00
58.61	2.00	0.00	0.00	0.07	0.00	58.67	2.00	0.00	0.00	0.05	0.00
58.74	2.00	0.00	0.00	0.07	0.00	58.82	2.00	0.00	0.00	0.09	0.00
58.88	2.00	0.00	0.00	0.06	0.00	58.95	2.00	0.00	0.00	0.07	0.00
59.02	2.00	0.00	0.00	0.07	0.00	59.09	2.00	0.00	0.00	0.07	0.00
59.12	2.00	0.00	0.00	0.04	0.00	59.19	2.00	0.00	0.00	0.07	0.00
59.26	2.00	0.00	0.00	0.07	0.00	59.32	2.00	0.00	0.00	0.06	0.00
59.40	2.00	0.00	0.00	0.07	0.00	59.46	2.00	0.00	0.00	0.06	0.00
59.52	2.00	0.00	0.00	0.06	0.00	59.60	2.00	0.00	0.00	0.09	0.00
59.66	2.00	0.00	0.00	0.06	0.00	59.73	2.00	0.00	0.00	0.06	0.00
59.78	2.00	0.00	0.00	0.06	0.00	59.85	2.00	0.00	0.00	0.07	0.00
59.93	2.00	0.00	0.00	0.08	0.00	59.99	2.00	0.00	0.00	0.07	0.00
60.04	2.00	0.00	0.00	0.05	0.00	60.11	2.00	0.00	0.00	0.07	0.00
60.18	2.00	0.00	0.00	0.07	0.00	60.24	2.00	0.00	0.00	0.06	0.00
60.30	2.00	0.00	0.00	0.07	0.00	60.37	2.00	0.00	0.00	0.07	0.00
60.44	2.00	0.00	0.00	0.07	0.00	60.50	2.00	0.00	0.00	0.06	0.00
60.58	2.00	0.00	0.00	0.08	0.00	60.63	2.00	0.00	0.00	0.05	0.00
60.70	2.00	0.00	0.00	0.07	0.00	60.78	2.00	0.00	0.00	0.07	0.00
60.83	2.00	0.00	0.00	0.05	0.00	60.89	2.00	0.00	0.00	0.06	0.00
60.97	2.00	0.00	0.00	0.08	0.00	61.03	2.00	0.00	0.00	0.06	0.00
61.10	2.00	0.00	0.00	0.06	0.00	61.16	2.00	0.00	0.00	0.06	0.00
61.22	2.00	0.00	0.00	0.06	0.00	61.30	2.00	0.00	0.00	0.08	0.00
61.36	2.00	0.00	0.00	0.05	0.00	61.42	2.00	0.00	0.00	0.06	0.00
61.48	2.00	0.00	0.00	0.07	0.00	61.57	2.00	0.00	0.00	0.09	0.00
61.64	2.00	0.00	0.00	0.07	0.00	61.70	2.00	0.00	0.00	0.07	0.00
61.76	2.00	0.00	0.00	0.05	0.00	61.82	2.00	0.00	0.00	0.06	0.00
61.88	2.00	0.00	0.00	0.06	0.00	61.96	2.00	0.00	0.00	0.07	0.00
62.03	2.00	0.00	0.00	0.07	0.00	62.08	2.00	0.00	0.00	0.05	0.00
62.15	2.00	0.00	0.00	0.07	0.00	62.22	2.00	0.00	0.00	0.07	0.00
62.29	2.00	0.00	0.00	0.07	0.00	62.36	2.00	0.00	0.00	0.07	0.00
62.41	2.00	0.00	0.00	0.05	0.00	62.48	2.00	0.00	0.00	0.07	0.00
62.55	2.00	0.00	0.00	0.07	0.00	62.62	2.00	0.00	0.00	0.07	0.00
62.69	2.00	0.00	0.00	0.07	0.00	62.73	2.00	0.00	0.00	0.05	0.00
62.80	2.00	0.00	0.00	0.07	0.00	62.87	2.00	0.00	0.00	0.07	0.00
62.95	2.00	0.00	0.00	0.07	0.00	63.02	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
63.06	2.00	0.00	0.00	0.05	0.00	63.13	2.00	0.00	0.00	0.07	0.00
63.20	2.00	0.00	0.00	0.07	0.00	63.26	2.00	0.00	0.00	0.05	0.00
63.34	2.00	0.00	0.00	0.08	0.00	63.39	2.00	0.00	0.00	0.05	0.00
63.45	2.00	0.00	0.00	0.06	0.00	63.52	2.00	0.00	0.00	0.07	0.00
63.59	2.00	0.00	0.00	0.07	0.00	63.66	2.00	0.00	0.00	0.07	0.00
63.72	2.00	0.00	0.00	0.05	0.00	63.79	2.00	0.00	0.00	0.07	0.00
63.86	2.00	0.00	0.00	0.07	0.00	63.91	2.00	0.00	0.00	0.05	0.00
63.98	2.00	0.00	0.00	0.07	0.00	64.05	2.00	0.00	0.00	0.07	0.00
64.12	2.00	0.00	0.00	0.06	0.00	64.18	2.00	0.00	0.00	0.06	0.00
64.25	2.00	0.00	0.00	0.07	0.00	64.31	2.00	0.00	0.00	0.07	0.00
64.38	2.00	0.00	0.00	0.07	0.00	64.45	2.00	0.00	0.00	0.06	0.00
64.50	2.00	0.00	0.00	0.06	0.00	64.58	2.00	0.00	0.00	0.08	0.00
64.64	2.00	0.00	0.00	0.06	0.00	64.72	2.00	0.00	0.00	0.07	0.00
64.77	2.00	0.00	0.00	0.05	0.00	64.83	2.00	0.00	0.00	0.06	0.00
64.91	2.00	0.00	0.00	0.08	0.00	64.97	2.00	0.00	0.00	0.06	0.00
65.04	2.00	0.00	0.00	0.07	0.00	65.10	2.00	0.00	0.00	0.07	0.00
65.17	2.00	0.00	0.00	0.07	0.00	65.24	2.00	0.00	0.00	0.07	0.00
65.31	2.00	0.00	0.00	0.07	0.00	65.36	2.00	0.00	0.00	0.06	0.00
65.42	2.00	0.00	0.00	0.06	0.00	65.49	2.00	0.00	0.00	0.07	0.00
65.55	2.00	0.00	0.00	0.07	0.00	65.62	2.00	0.00	0.00	0.07	0.00
65.69	2.00	0.00	0.00	0.07	0.00	65.76	2.00	0.00	0.00	0.07	0.00
65.83	2.00	0.00	0.00	0.07	0.00	65.89	2.00	0.00	0.00	0.06	0.00
65.95	2.00	0.00	0.00	0.06	0.00	66.03	2.00	0.00	0.00	0.08	0.00
66.08	2.00	0.00	0.00	0.06	0.00	66.16	2.00	0.00	0.00	0.08	0.00
66.22	2.00	0.00	0.00	0.06	0.00	66.29	2.00	0.00	0.00	0.07	0.00
66.36	2.00	0.00	0.00	0.07	0.00	66.42	2.00	0.00	0.00	0.06	0.00
66.49	2.00	0.00	0.00	0.06	0.00	66.55	2.00	0.00	0.00	0.07	0.00
66.62	2.00	0.00	0.00	0.07	0.00	66.69	2.00	0.00	0.00	0.07	0.00
66.75	2.00	0.00	0.00	0.07	0.00	66.82	2.00	0.00	0.00	0.07	0.00
66.89	2.00	0.00	0.00	0.07	0.00	66.96	2.00	0.00	0.00	0.07	0.00
67.00	2.00	0.00	0.00	0.04	0.00	67.08	2.00	0.00	0.00	0.08	0.00
67.14	2.00	0.00	0.00	0.06	0.00	67.21	2.00	0.00	0.00	0.07	0.00
67.28	2.00	0.00	0.00	0.07	0.00	67.34	2.00	0.00	0.00	0.07	0.00
67.41	2.00	0.00	0.00	0.07	0.00	67.47	2.00	0.00	0.00	0.06	0.00
67.54	2.00	0.00	0.00	0.07	0.00	67.61	2.00	0.00	0.00	0.07	0.00
67.67	2.00	0.00	0.00	0.07	0.00	67.74	2.00	0.00	0.00	0.07	0.00
67.80	2.00	0.00	0.00	0.07	0.00	67.87	2.00	0.00	0.00	0.07	0.00
67.94	2.00	0.00	0.00	0.07	0.00	68.00	2.00	0.00	0.00	0.07	0.00
68.07	2.00	0.00	0.00	0.06	0.00	68.14	2.00	0.00	0.00	0.07	0.00
68.20	2.00	0.00	0.00	0.07	0.00	68.27	2.00	0.00	0.00	0.07	0.00
68.34	2.00	0.00	0.00	0.07	0.00	68.41	2.00	0.00	0.00	0.07	0.00
68.44	2.00	0.00	0.00	0.03	0.00	68.51	2.00	0.00	0.00	0.07	0.00
68.58	2.00	0.00	0.00	0.08	0.00	68.65	2.00	0.00	0.00	0.06	0.00
68.73	2.00	0.00	0.00	0.08	0.00	68.78	2.00	0.00	0.00	0.05	0.00
68.83	2.00	0.00	0.00	0.05	0.00	68.92	2.00	0.00	0.00	0.08	0.00
68.97	2.00	0.00	0.00	0.06	0.00	69.03	2.00	0.00	0.00	0.06	0.00
69.09	2.00	0.00	0.00	0.06	0.00	69.18	2.00	0.00	0.00	0.09	0.00
69.24	2.00	0.00	0.00	0.06	0.00	69.29	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
69.37	2.00	0.00	0.00	0.08	0.00	69.43	2.00	0.00	0.00	0.06	0.00
69.51	2.00	0.00	0.00	0.08	0.00	69.57	2.00	0.00	0.00	0.06	0.00
69.63	2.00	0.00	0.00	0.06	0.00	69.69	2.00	0.00	0.00	0.06	0.00
69.76	2.00	0.00	0.00	0.08	0.00	69.82	2.00	0.00	0.00	0.06	0.00
69.91	2.00	0.00	0.00	0.09	0.00	69.95	2.00	0.00	0.00	0.04	0.00
70.02	2.00	0.00	0.00	0.07	0.00	70.08	2.00	0.00	0.00	0.06	0.00
70.16	2.00	0.00	0.00	0.07	0.00	70.22	2.00	0.00	0.00	0.07	0.00
70.28	2.00	0.00	0.00	0.06	0.00	70.35	2.00	0.00	0.00	0.07	0.00
70.42	2.00	0.00	0.00	0.06	0.00	70.48	2.00	0.00	0.00	0.07	0.00
70.55	2.00	0.00	0.00	0.07	0.00	70.61	2.00	0.00	0.00	0.07	0.00
70.69	2.00	0.00	0.00	0.07	0.00	70.75	2.00	0.00	0.00	0.06	0.00
70.82	2.00	0.00	0.00	0.07	0.00	70.88	2.00	0.00	0.00	0.07	0.00
70.95	2.00	0.00	0.00	0.07	0.00	71.02	2.00	0.00	0.00	0.07	0.00
71.08	2.00	0.00	0.00	0.06	0.00	71.15	2.00	0.00	0.00	0.07	0.00
71.22	2.00	0.00	0.00	0.07	0.00	71.28	2.00	0.00	0.00	0.07	0.00
71.35	2.00	0.00	0.00	0.07	0.00	71.42	2.00	0.00	0.00	0.07	0.00
71.49	2.00	0.00	0.00	0.07	0.00	71.54	2.00	0.00	0.00	0.05	0.00
71.59	2.00	0.00	0.00	0.05	0.00	71.67	2.00	0.00	0.00	0.07	0.00
71.73	2.00	0.00	0.00	0.06	0.00	71.79	2.00	0.00	0.00	0.06	0.00
71.86	2.00	0.00	0.00	0.06	0.00	71.92	2.00	0.00	0.00	0.07	0.00
71.99	2.00	0.00	0.00	0.07	0.00	72.06	2.00	0.00	0.00	0.07	0.00
72.12	2.00	0.00	0.00	0.05	0.00	72.19	2.00	0.00	0.00	0.07	0.00
72.26	2.00	0.00	0.00	0.07	0.00	72.31	2.00	0.00	0.00	0.05	0.00
72.38	2.00	0.00	0.00	0.06	0.00	72.46	2.00	0.00	0.00	0.08	0.00
72.52	2.00	0.00	0.00	0.06	0.00	72.59	2.00	0.00	0.00	0.07	0.00
72.65	2.00	0.00	0.00	0.06	0.00	72.71	2.00	0.00	0.00	0.07	0.00
72.78	2.00	0.00	0.00	0.07	0.00	72.84	2.00	0.00	0.00	0.06	0.00
72.90	2.00	0.00	0.00	0.06	0.00	72.98	2.00	0.00	0.00	0.08	0.00
73.03	2.00	0.00	0.00	0.06	0.00	73.11	2.00	0.00	0.00	0.08	0.00
73.17	2.00	0.00	0.00	0.06	0.00	73.23	2.00	0.00	0.00	0.07	0.00
73.30	2.00	0.00	0.00	0.06	0.00	73.36	2.00	0.00	0.00	0.07	0.00
73.44	2.00	0.00	0.00	0.08	0.00	73.51	2.00	0.00	0.00	0.07	0.00
73.56	2.00	0.00	0.00	0.05	0.00	73.63	2.00	0.00	0.00	0.07	0.00
73.70	2.00	0.00	0.00	0.07	0.00	73.76	2.00	0.00	0.00	0.06	0.00
73.83	2.00	0.00	0.00	0.07	0.00	73.89	2.00	0.00	0.00	0.06	0.00
73.95	2.00	0.00	0.00	0.06	0.00	74.02	2.00	0.00	0.00	0.07	0.00
74.09	2.00	0.00	0.00	0.07	0.00	74.16	2.00	0.00	0.00	0.07	0.00
74.24	2.00	0.00	0.00	0.08	0.00	74.31	2.00	0.00	0.00	0.07	0.00
74.38	2.00	0.00	0.00	0.07	0.00	74.41	2.00	0.00	0.00	0.03	0.00
74.48	2.00	0.00	0.00	0.07	0.00	74.55	2.00	0.00	0.00	0.07	0.00
74.62	2.00	0.00	0.00	0.07	0.00	74.68	2.00	0.00	0.00	0.06	0.00
74.75	2.00	0.00	0.00	0.07	0.00	74.82	2.00	0.00	0.00	0.07	0.00
74.89	2.00	0.00	0.00	0.07	0.00	74.94	2.00	0.00	0.00	0.05	0.00
75.01	2.00	0.00	0.00	0.07	0.00	75.07	2.00	0.00	0.00	0.06	0.00
75.14	2.00	0.00	0.00	0.07	0.00	75.20	2.00	0.00	0.00	0.06	0.00
75.27	2.00	0.00	0.00	0.08	0.00	75.33	2.00	0.00	0.00	0.06	0.00
75.41	2.00	0.00	0.00	0.08	0.00	75.48	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}	Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}

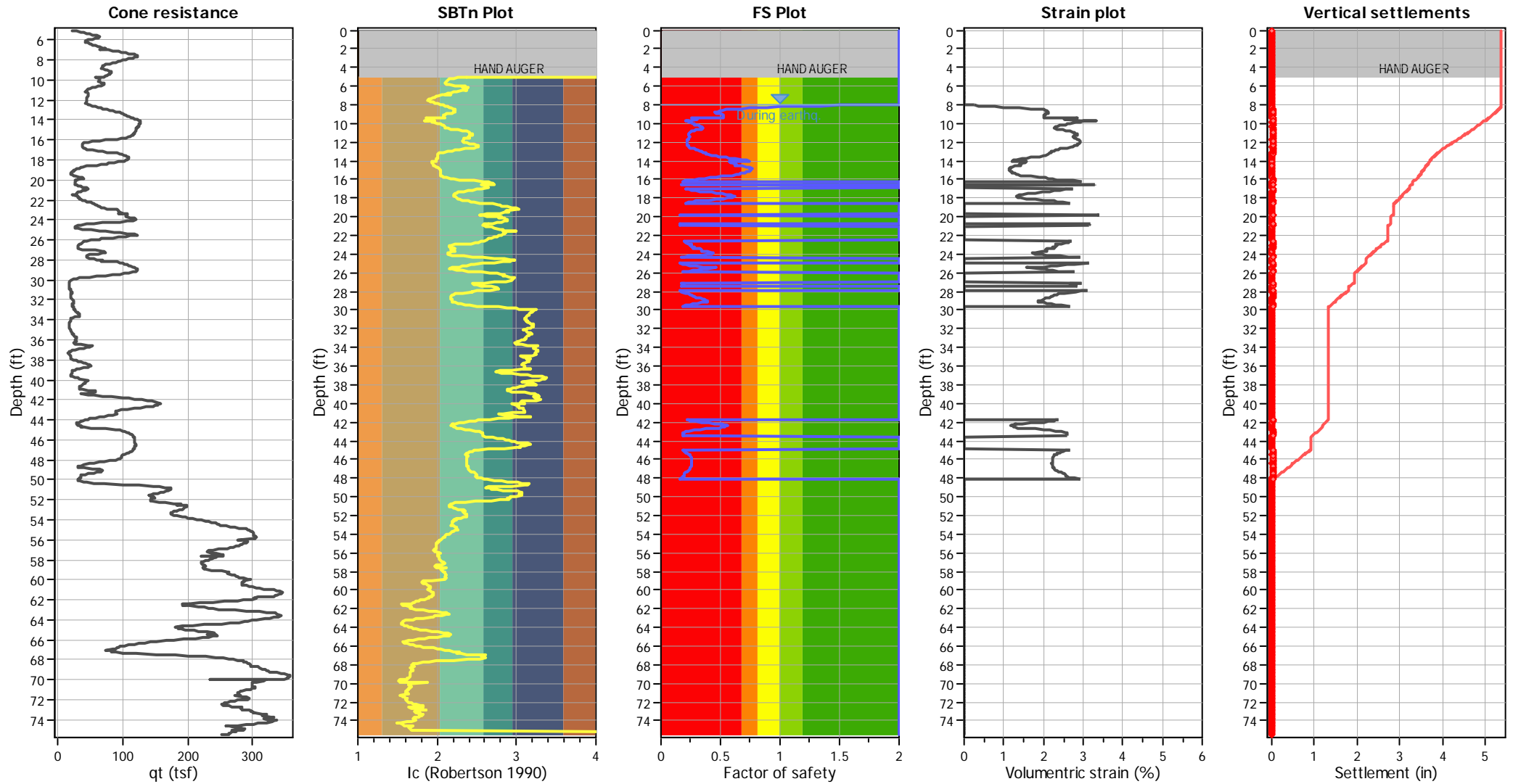
Overall liquefaction potential: 24.53

$LPI_{ISH} > 5.0$ - Liquefaction manifestation is expected

Abbreviations

- FS: Calculated factor of safety for test point
- d_z : Layer thickness (ft)
- LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- qt: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement due to soil liquefaction ::											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.03	182.69	1.50	0.26	1.00	0.00	8.09	180.21	1.34	0.37	1.00	0.00
8.14	177.11	1.18	0.52	1.00	0.00	8.22	172.98	1.01	0.76	1.00	0.01
8.27	169.61	0.89	0.97	1.00	0.01	8.35	164.17	0.75	1.41	1.00	0.01
8.40	160.64	0.67	1.69	1.00	0.01	8.48	155.96	0.59	1.98	1.00	0.02
8.54	153.36	0.55	2.02	1.00	0.01	8.62	151.39	0.52	2.05	1.00	0.02
8.67	150.34	0.50	2.07	1.00	0.01	8.73	148.04	0.48	2.11	1.00	0.01
8.81	146.12	0.45	2.14	1.00	0.02	8.86	147.20	0.46	2.12	1.00	0.01
8.94	149.18	0.48	2.09	1.00	0.02	9.00	150.86	0.50	2.06	1.00	0.01
9.08	152.62	0.52	2.03	1.00	0.02	9.13	153.11	0.53	2.03	1.00	0.01
9.20	153.30	0.53	2.02	1.00	0.02	9.26	153.41	0.53	2.02	1.00	0.02
9.33	153.22	0.52	2.03	1.00	0.02	9.39	146.33	0.44	2.13	1.00	0.02
9.46	112.68	0.25	2.84	1.00	0.02	9.53	120.78	0.28	2.64	1.00	0.02
9.60	126.14	0.30	2.52	1.00	0.02	9.67	110.03	0.24	2.91	1.00	0.02
9.73	96.89	0.21	3.32	1.00	0.03	9.79	106.33	0.23	3.02	1.00	0.02
9.86	109.29	0.24	2.93	1.00	0.03	9.91	113.39	0.25	2.82	1.00	0.02
9.98	118.60	0.26	2.69	1.00	0.02	10.04	122.14	0.28	2.61	1.00	0.02
10.11	124.40	0.28	2.55	1.00	0.02	10.18	127.51	0.30	2.49	1.00	0.02
10.25	131.33	0.32	2.41	1.00	0.02	10.31	134.45	0.33	2.35	1.00	0.02
10.37	136.67	0.35	2.30	1.00	0.02	10.44	138.40	0.36	2.27	1.00	0.02
10.51	138.12	0.35	2.28	1.00	0.02	10.57	135.47	0.34	2.33	1.00	0.02
10.64	131.60	0.31	2.40	1.00	0.02	10.71	127.71	0.29	2.48	1.00	0.02
10.77	124.05	0.27	2.56	1.00	0.02	10.84	119.46	0.26	2.67	1.00	0.02
10.91	115.84	0.24	2.76	1.00	0.02	10.98	114.82	0.24	2.78	1.00	0.02
11.05	114.21	0.24	2.80	1.00	0.02	11.11	114.24	0.24	2.80	1.00	0.02
11.18	111.80	0.23	2.86	1.00	0.02	11.25	112.79	0.23	2.84	1.00	0.02
11.31	115.23	0.24	2.77	1.00	0.02	11.38	115.64	0.24	2.76	1.00	0.02
11.45	116.19	0.24	2.75	1.00	0.02	11.51	115.41	0.24	2.77	1.00	0.02
11.58	113.61	0.23	2.81	1.00	0.02	11.65	113.20	0.23	2.83	1.00	0.02
11.68	112.51	0.23	2.84	1.00	0.01	11.75	111.13	0.22	2.88	1.00	0.02
11.82	109.19	0.22	2.93	1.00	0.02	11.88	108.81	0.21	2.94	1.00	0.02
11.97	108.97	0.21	2.94	1.00	0.03	12.03	109.34	0.22	2.93	1.00	0.02
12.10	109.17	0.21	2.93	1.00	0.02	12.16	110.81	0.22	2.89	1.00	0.02
12.23	111.54	0.22	2.87	1.00	0.02	12.30	111.48	0.22	2.87	1.00	0.02
12.36	113.55	0.22	2.82	1.00	0.02	12.43	115.22	0.23	2.77	1.00	0.02
12.50	117.00	0.23	2.73	1.00	0.02	12.53	118.48	0.24	2.69	1.00	0.01
12.60	122.11	0.25	2.61	1.00	0.02	12.67	126.62	0.27	2.51	1.00	0.02
12.74	130.74	0.28	2.42	1.00	0.02	12.80	133.63	0.30	2.36	1.00	0.02
12.87	135.85	0.31	2.32	1.00	0.02	12.94	139.36	0.33	2.25	1.00	0.02
13.00	141.90	0.35	2.21	1.00	0.02	13.07	142.98	0.35	2.19	1.00	0.02
13.13	144.22	0.36	2.17	1.00	0.02	13.20	145.75	0.37	2.14	1.00	0.02
13.27	146.01	0.38	2.14	1.00	0.02	13.34	148.07	0.39	2.11	1.00	0.02
13.40	151.81	0.43	2.05	1.00	0.02	13.47	154.76	0.46	2.00	1.00	0.02
13.54	156.93	0.49	1.92	1.00	0.02	13.60	158.86	0.52	1.79	1.00	0.01
13.67	160.88	0.55	1.68	1.00	0.01	13.74	162.45	0.57	1.59	1.00	0.01
13.80	165.02	0.62	1.45	1.00	0.01	13.87	167.88	0.68	1.32	1.00	0.01
13.94	169.68	0.72	1.24	1.00	0.01	14.00	170.59	0.74	1.20	1.00	0.01
14.07	166.15	0.64	1.40	1.00	0.01	14.14	162.84	0.57	1.57	1.00	0.01
14.21	163.73	0.59	1.52	1.00	0.01	14.24	164.36	0.60	1.49	1.00	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
14.31	166.06	0.63	1.40	1.00	0.01	14.37	165.77	0.62	1.42	1.00	0.01
14.46	165.75	0.62	1.42	1.00	0.01	14.52	166.71	0.64	1.37	1.00	0.01
14.59	168.68	0.68	1.28	1.00	0.01	14.65	170.44	0.72	1.20	1.00	0.01
14.72	171.25	0.74	1.17	1.00	0.01	14.79	172.02	0.76	1.14	1.00	0.01
14.85	171.78	0.75	1.15	1.00	0.01	14.92	171.55	0.75	1.16	1.00	0.01
14.99	171.87	0.75	1.15	1.00	0.01	15.05	171.94	0.76	1.14	1.00	0.01
15.12	171.44	0.74	1.16	1.00	0.01	15.19	170.79	0.72	1.19	1.00	0.01
15.22	170.64	0.72	1.20	1.00	0.00	15.29	170.08	0.70	1.22	1.00	0.01
15.36	169.04	0.68	1.26	1.00	0.01	15.43	168.10	0.65	1.31	1.00	0.01
15.49	167.13	0.63	1.35	1.00	0.01	15.56	165.59	0.60	1.43	1.00	0.01
15.63	163.58	0.56	1.53	1.00	0.01	15.69	160.85	0.52	1.68	1.00	0.01
15.76	156.95	0.46	1.91	1.00	0.02	15.82	152.90	0.41	2.03	1.00	0.02
15.89	148.02	0.37	2.11	1.00	0.02	15.96	141.65	0.32	2.21	1.00	0.02
16.03	133.81	0.27	2.36	1.00	0.02	16.10	125.50	0.24	2.53	1.00	0.02
16.16	116.29	0.21	2.75	1.00	0.02	16.23	107.80	0.19	2.97	1.00	0.02
16.30	40.01	2.00	0.00	1.00	0.00	16.36	37.39	2.00	0.00	1.00	0.00
16.43	36.04	2.00	0.00	1.00	0.00	16.50	35.97	2.00	0.00	1.00	0.00
16.56	97.10	0.17	3.31	1.00	0.03	16.63	97.75	0.17	3.29	1.00	0.03
16.70	36.84	2.00	0.00	1.00	0.00	16.73	37.25	2.00	0.00	1.00	0.00
16.80	38.80	2.00	0.00	1.00	0.00	16.87	41.14	2.00	0.00	1.00	0.00
16.94	43.47	2.00	0.00	1.00	0.00	17.00	116.94	0.21	2.73	1.00	0.02
17.08	124.91	0.23	2.54	1.00	0.02	17.14	130.92	0.25	2.42	1.00	0.02
17.20	137.99	0.29	2.28	1.00	0.02	17.27	145.24	0.33	2.15	1.00	0.02
17.34	151.53	0.39	2.05	1.00	0.02	17.40	155.58	0.43	1.99	1.00	0.02
17.47	158.64	0.47	1.81	1.00	0.01	17.53	161.93	0.51	1.62	1.00	0.01
17.60	164.63	0.55	1.47	1.00	0.01	17.67	166.50	0.59	1.38	1.00	0.01
17.73	167.73	0.61	1.32	1.00	0.01	17.80	168.07	0.62	1.31	1.00	0.01
17.87	168.03	0.62	1.31	1.00	0.01	17.93	167.09	0.60	1.35	1.00	0.01
18.00	165.48	0.57	1.43	1.00	0.01	18.07	162.74	0.52	1.57	1.00	0.01
18.14	158.78	0.46	1.80	1.00	0.01	18.20	153.31	0.40	2.02	1.00	0.02
18.27	146.67	0.34	2.13	1.00	0.02	18.34	139.42	0.29	2.25	1.00	0.02
18.37	135.60	0.27	2.32	1.00	0.01	18.44	128.24	0.24	2.47	1.00	0.02
18.51	119.92	0.21	2.66	1.00	0.02	18.57	45.97	2.00	0.00	1.00	0.00
18.64	39.60	2.00	0.00	1.00	0.00	18.71	35.07	2.00	0.00	1.00	0.00
18.78	32.95	2.00	0.00	1.00	0.00	18.84	30.93	2.00	0.00	1.00	0.00
18.91	26.95	2.00	0.00	1.00	0.00	18.98	24.27	2.00	0.00	1.00	0.00
19.04	22.44	2.00	0.00	1.00	0.00	19.11	21.05	2.00	0.00	1.00	0.00
19.18	19.75	2.00	0.00	1.00	0.00	19.24	18.70	2.00	0.00	1.00	0.00
19.31	18.66	2.00	0.00	1.00	0.00	19.38	18.63	2.00	0.00	1.00	0.00
19.44	18.60	2.00	0.00	1.00	0.00	19.51	19.82	2.00	0.00	1.00	0.00
19.58	21.53	2.00	0.00	1.00	0.00	19.63	23.67	2.00	0.00	1.00	0.00
19.69	30.23	2.00	0.00	1.00	0.00	19.76	94.15	0.15	3.42	1.00	0.03
19.82	95.32	0.16	3.37	1.00	0.03	19.89	94.54	0.15	3.40	1.00	0.03
19.95	32.11	2.00	0.00	1.00	0.00	20.02	24.01	2.00	0.00	1.00	0.00
20.09	25.95	2.00	0.00	1.00	0.00	20.16	23.51	2.00	0.00	1.00	0.00
20.23	22.98	2.00	0.00	1.00	0.00	20.29	23.10	2.00	0.00	1.00	0.00
20.36	22.98	2.00	0.00	1.00	0.00	20.42	23.69	2.00	0.00	1.00	0.00
20.49	25.20	2.00	0.00	1.00	0.00	20.56	27.12	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
20.63	29.86	2.00	0.00	1.00	0.00	20.69	33.02	2.00	0.00	1.00	0.00
20.76	36.33	2.00	0.00	1.00	0.00	20.83	101.26	0.16	3.17	1.00	0.03
20.89	102.13	0.16	3.14	1.00	0.03	20.96	101.53	0.16	3.16	1.00	0.03
21.03	36.99	2.00	0.00	1.00	0.00	21.09	33.18	2.00	0.00	1.00	0.00
21.16	30.03	2.00	0.00	1.00	0.00	21.23	28.03	2.00	0.00	1.00	0.00
21.26	26.88	2.00	0.00	1.00	0.00	21.33	24.74	2.00	0.00	1.00	0.00
21.40	24.14	2.00	0.00	1.00	0.00	21.46	24.34	2.00	0.00	1.00	0.00
21.53	19.27	2.00	0.00	1.00	0.00	21.60	25.55	2.00	0.00	1.00	0.00
21.66	25.82	2.00	0.00	1.00	0.00	21.73	26.18	2.00	0.00	1.00	0.00
21.80	27.03	2.00	0.00	1.00	0.00	21.86	28.58	2.00	0.00	1.00	0.00
21.93	29.82	2.00	0.00	1.00	0.00	22.00	31.13	2.00	0.00	1.00	0.00
22.06	32.85	2.00	0.00	1.00	0.00	22.13	34.87	2.00	0.00	1.00	0.00
22.19	37.87	2.00	0.00	1.00	0.00	22.26	41.83	2.00	0.00	1.00	0.00
22.33	44.75	2.00	0.00	1.00	0.00	22.40	46.46	2.00	0.00	1.00	0.00
22.46	47.52	2.00	0.00	1.00	0.00	22.53	49.48	2.00	0.00	1.00	0.00
22.60	117.85	0.19	2.71	1.00	0.02	22.66	120.29	0.20	2.65	1.00	0.02
22.73	121.47	0.20	2.62	1.00	0.02	22.80	124.29	0.21	2.56	1.00	0.02
22.86	129.64	0.23	2.44	1.00	0.02	22.93	136.13	0.26	2.31	1.00	0.02
23.00	136.25	0.26	2.31	1.00	0.02	23.03	134.97	0.25	2.34	1.00	0.01
23.10	135.74	0.25	2.32	1.00	0.02	23.17	136.15	0.25	2.31	1.00	0.02
23.24	137.93	0.26	2.28	1.00	0.02	23.30	141.63	0.28	2.21	1.00	0.02
23.37	139.40	0.27	2.25	1.00	0.02	23.43	148.29	0.33	2.10	1.00	0.02
23.50	150.62	0.34	2.07	1.00	0.02	23.56	150.45	0.34	2.07	1.00	0.02
23.63	150.09	0.34	2.07	1.00	0.02	23.70	151.23	0.35	2.06	1.00	0.02
23.76	155.59	0.39	1.99	1.00	0.02	23.83	159.18	0.43	1.77	1.00	0.01
23.90	160.29	0.44	1.71	1.00	0.01	23.96	159.14	0.43	1.78	1.00	0.01
24.03	155.76	0.39	1.99	1.00	0.02	24.10	149.44	0.33	2.08	1.00	0.02
24.17	141.03	0.28	2.22	1.00	0.02	24.23	131.46	0.23	2.40	1.00	0.02
24.30	120.38	0.20	2.65	1.00	0.02	24.37	108.86	0.17	2.94	1.00	0.02
24.43	35.30	2.00	0.00	1.00	0.00	24.50	28.07	2.00	0.00	1.00	0.00
24.57	23.57	2.00	0.00	1.00	0.00	24.63	21.06	2.00	0.00	1.00	0.00
24.70	20.72	2.00	0.00	1.00	0.00	24.77	20.02	2.00	0.00	1.00	0.00
24.84	21.48	2.00	0.00	1.00	0.00	24.87	23.55	2.00	0.00	1.00	0.00
24.94	29.74	2.00	0.00	1.00	0.00	25.01	102.28	0.16	3.14	1.00	0.02
25.07	114.81	0.18	2.78	1.00	0.02	25.14	122.90	0.20	2.59	1.00	0.02
25.21	134.34	0.24	2.35	1.00	0.02	25.28	143.76	0.29	2.18	1.00	0.02
25.34	153.01	0.36	2.03	1.00	0.02	25.41	160.90	0.44	1.67	1.00	0.01
25.48	162.55	0.46	1.58	1.00	0.01	25.54	156.78	0.39	1.92	1.00	0.02
25.61	152.62	0.35	2.03	1.00	0.02	25.68	147.08	0.31	2.12	1.00	0.02
25.75	140.14	0.27	2.24	1.00	0.02	25.81	132.05	0.23	2.39	1.00	0.02
25.87	117.61	0.19	2.71	1.00	0.02	25.93	114.27	0.18	2.80	1.00	0.02
26.00	40.32	2.00	0.00	1.00	0.00	26.06	34.20	2.00	0.00	1.00	0.00
26.13	30.65	2.00	0.00	1.00	0.00	26.20	28.61	2.00	0.00	1.00	0.00
26.27	28.28	2.00	0.00	1.00	0.00	26.33	28.68	2.00	0.00	1.00	0.00
26.40	26.66	2.00	0.00	1.00	0.00	26.47	24.29	2.00	0.00	1.00	0.00
26.53	22.51	2.00	0.00	1.00	0.00	26.60	22.48	2.00	0.00	1.00	0.00
26.66	22.45	2.00	0.00	1.00	0.00	26.73	22.42	2.00	0.00	1.00	0.00
26.80	23.19	2.00	0.00	1.00	0.00	26.86	23.73	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
26.93	27.91	2.00	0.00	1.00	0.00	27.00	36.00	2.00	0.00	1.00	0.00
27.06	108.05	0.17	2.97	1.00	0.02	27.13	116.96	0.18	2.73	1.00	0.02
27.17	119.44	0.19	2.67	1.00	0.01	27.23	119.85	0.19	2.66	1.00	0.02
27.30	116.70	0.18	2.74	1.00	0.02	27.37	111.99	0.17	2.86	1.00	0.02
27.43	43.01	2.00	0.00	1.00	0.00	27.50	37.40	2.00	0.00	1.00	0.00
27.57	32.91	2.00	0.00	1.00	0.00	27.64	32.83	2.00	0.00	1.00	0.00
27.70	32.79	2.00	0.00	1.00	0.00	27.77	32.71	2.00	0.00	1.00	0.00
27.84	35.91	2.00	0.00	1.00	0.00	27.91	103.21	0.16	3.11	1.00	0.03
27.98	108.18	0.16	2.96	1.00	0.02	28.04	113.64	0.18	2.81	1.00	0.02
28.09	113.28	0.17	2.82	1.00	0.02	28.16	125.07	0.20	2.54	1.00	0.02
28.22	129.57	0.22	2.44	1.00	0.02	28.28	133.05	0.23	2.37	1.00	0.02
28.35	135.53	0.24	2.33	1.00	0.02	28.42	138.24	0.25	2.27	1.00	0.02
28.49	140.75	0.27	2.23	1.00	0.02	28.55	142.99	0.28	2.19	1.00	0.02
28.62	145.77	0.29	2.14	1.00	0.02	28.69	148.67	0.31	2.10	1.00	0.02
28.75	151.19	0.33	2.06	1.00	0.02	28.82	153.38	0.35	2.02	1.00	0.02
28.89	155.11	0.37	2.00	1.00	0.02	28.95	156.45	0.38	1.95	1.00	0.02
29.02	157.47	0.39	1.88	1.00	0.01	29.09	157.72	0.39	1.86	1.00	0.02
29.16	156.69	0.38	1.93	1.00	0.02	29.22	152.99	0.35	2.03	1.00	0.02
29.29	148.23	0.31	2.10	1.00	0.02	29.35	142.41	0.27	2.20	1.00	0.02
29.42	136.21	0.24	2.31	1.00	0.02	29.49	128.63	0.21	2.46	1.00	0.02
29.55	119.82	0.19	2.66	1.00	0.02	29.62	44.38	2.00	0.00	1.00	0.00
29.69	34.73	2.00	0.00	1.00	0.00	29.76	27.87	2.00	0.00	1.00	0.00
29.82	22.86	2.00	0.00	1.00	0.00	29.86	20.57	2.00	0.00	1.00	0.00
29.92	16.88	2.00	0.00	1.00	0.00	30.00	13.38	2.00	0.00	1.00	0.00
30.06	13.90	2.00	0.00	1.00	0.00	30.13	12.88	2.00	0.00	1.00	0.00
30.20	12.47	2.00	0.00	1.00	0.00	30.27	12.33	2.00	0.00	1.00	0.00
30.34	12.24	2.00	0.00	1.00	0.00	30.40	11.77	2.00	0.00	1.00	0.00
30.47	11.63	2.00	0.00	1.00	0.00	30.54	11.67	2.00	0.00	1.00	0.00
30.61	11.85	2.00	0.00	1.00	0.00	30.67	11.91	2.00	0.00	1.00	0.00
30.74	11.90	2.00	0.00	1.00	0.00	30.81	12.01	2.00	0.00	1.00	0.00
30.87	12.45	2.00	0.00	1.00	0.00	30.91	12.64	2.00	0.00	1.00	0.00
30.97	13.08	2.00	0.00	1.00	0.00	31.04	13.27	2.00	0.00	1.00	0.00
31.11	13.58	2.00	0.00	1.00	0.00	31.17	13.82	2.00	0.00	1.00	0.00
31.24	14.39	2.00	0.00	1.00	0.00	31.31	14.31	2.00	0.00	1.00	0.00
31.38	14.09	2.00	0.00	1.00	0.00	31.44	13.88	2.00	0.00	1.00	0.00
31.51	13.54	2.00	0.00	1.00	0.00	31.57	13.33	2.00	0.00	1.00	0.00
31.64	13.45	2.00	0.00	1.00	0.00	31.71	13.43	2.00	0.00	1.00	0.00
31.77	13.22	2.00	0.00	1.00	0.00	31.84	13.65	2.00	0.00	1.00	0.00
31.91	14.48	2.00	0.00	1.00	0.00	31.97	14.98	2.00	0.00	1.00	0.00
32.04	16.07	2.00	0.00	1.00	0.00	32.11	16.11	2.00	0.00	1.00	0.00
32.18	15.58	2.00	0.00	1.00	0.00	32.24	15.88	2.00	0.00	1.00	0.00
32.31	15.87	2.00	0.00	1.00	0.00	32.36	15.85	2.00	0.00	1.00	0.00
32.43	15.19	2.00	0.00	1.00	0.00	32.49	14.91	2.00	0.00	1.00	0.00
32.56	15.28	2.00	0.00	1.00	0.00	32.62	15.27	2.00	0.00	1.00	0.00
32.70	15.44	2.00	0.00	1.00	0.00	32.75	15.93	2.00	0.00	1.00	0.00
32.83	16.43	2.00	0.00	1.00	0.00	32.88	16.35	2.00	0.00	1.00	0.00
32.96	16.78	2.00	0.00	1.00	0.00	33.01	17.09	2.00	0.00	1.00	0.00
33.08	17.26	2.00	0.00	1.00	0.00	33.16	18.27	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
33.22	19.22	2.00	0.00	1.00	0.00	33.29	20.82	2.00	0.00	1.00	0.00
33.34	21.19	2.00	0.00	1.00	0.00	33.40	21.37	2.00	0.00	1.00	0.00
33.47	22.00	2.00	0.00	1.00	0.00	33.56	22.42	2.00	0.00	1.00	0.00
33.62	21.55	2.00	0.00	1.00	0.00	33.68	19.26	2.00	0.00	1.00	0.00
33.73	17.00	2.00	0.00	1.00	0.00	33.82	13.94	2.00	0.00	1.00	0.00
33.89	13.11	2.00	0.00	1.00	0.00	33.95	13.29	2.00	0.00	1.00	0.00
34.02	13.21	2.00	0.00	1.00	0.00	34.09	12.69	2.00	0.00	1.00	0.00
34.15	12.25	2.00	0.00	1.00	0.00	34.22	11.86	2.00	0.00	1.00	0.00
34.25	11.67	2.00	0.00	1.00	0.00	34.32	11.41	2.00	0.00	1.00	0.00
34.39	11.46	2.00	0.00	1.00	0.00	34.45	11.51	2.00	0.00	1.00	0.00
34.52	11.74	2.00	0.00	1.00	0.00	34.59	11.73	2.00	0.00	1.00	0.00
34.65	11.72	2.00	0.00	1.00	0.00	34.72	11.71	2.00	0.00	1.00	0.00
34.79	11.69	2.00	0.00	1.00	0.00	34.85	11.86	2.00	0.00	1.00	0.00
34.92	12.22	2.00	0.00	1.00	0.00	34.99	12.45	2.00	0.00	1.00	0.00
35.05	12.74	2.00	0.00	1.00	0.00	35.13	12.91	2.00	0.00	1.00	0.00
35.19	12.72	2.00	0.00	1.00	0.00	35.27	14.67	2.00	0.00	1.00	0.00
35.34	14.65	2.00	0.00	1.00	0.00	35.37	14.64	2.00	0.00	1.00	0.00
35.44	14.88	2.00	0.00	1.00	0.00	35.51	15.29	2.00	0.00	1.00	0.00
35.57	15.83	2.00	0.00	1.00	0.00	35.64	16.80	2.00	0.00	1.00	0.00
35.70	17.97	2.00	0.00	1.00	0.00	35.77	18.45	2.00	0.00	1.00	0.00
35.84	18.49	2.00	0.00	1.00	0.00	35.90	18.16	2.00	0.00	1.00	0.00
35.97	17.40	2.00	0.00	1.00	0.00	36.03	17.06	2.00	0.00	1.00	0.00
36.10	17.48	2.00	0.00	1.00	0.00	36.17	16.84	2.00	0.00	1.00	0.00
36.24	17.38	2.00	0.00	1.00	0.00	36.30	15.22	2.00	0.00	1.00	0.00
36.37	17.29	2.00	0.00	1.00	0.00	36.44	22.62	2.00	0.00	1.00	0.00
36.51	29.37	2.00	0.00	1.00	0.00	36.57	33.35	2.00	0.00	1.00	0.00
36.64	33.98	2.00	0.00	1.00	0.00	36.71	32.02	2.00	0.00	1.00	0.00
36.77	29.09	2.00	0.00	1.00	0.00	36.84	25.32	2.00	0.00	1.00	0.00
36.91	21.09	2.00	0.00	1.00	0.00	36.98	17.18	2.00	0.00	1.00	0.00
37.01	15.71	2.00	0.00	1.00	0.00	37.08	13.29	2.00	0.00	1.00	0.00
37.15	11.73	2.00	0.00	1.00	0.00	37.21	10.77	2.00	0.00	1.00	0.00
37.28	10.06	2.00	0.00	1.00	0.00	37.34	9.87	2.00	0.00	1.00	0.00
37.41	10.27	2.00	0.00	1.00	0.00	37.48	11.02	2.00	0.00	1.00	0.00
37.55	11.89	2.00	0.00	1.00	0.00	37.61	12.41	2.00	0.00	1.00	0.00
37.68	12.52	2.00	0.00	1.00	0.00	37.75	12.15	2.00	0.00	1.00	0.00
37.81	11.96	2.00	0.00	1.00	0.00	37.88	12.18	2.00	0.00	1.00	0.00
37.95	12.64	2.00	0.00	1.00	0.00	38.02	15.48	2.00	0.00	1.00	0.00
38.08	17.14	2.00	0.00	1.00	0.00	38.15	19.12	2.00	0.00	1.00	0.00
38.21	21.54	2.00	0.00	1.00	0.00	38.28	24.61	2.00	0.00	1.00	0.00
38.35	26.84	2.00	0.00	1.00	0.00	38.41	28.87	2.00	0.00	1.00	0.00
38.48	30.93	2.00	0.00	1.00	0.00	38.55	31.87	2.00	0.00	1.00	0.00
38.58	31.79	2.00	0.00	1.00	0.00	38.65	30.92	2.00	0.00	1.00	0.00
38.72	28.82	2.00	0.00	1.00	0.00	38.78	25.04	2.00	0.00	1.00	0.00
38.85	20.97	2.00	0.00	1.00	0.00	38.92	17.52	2.00	0.00	1.00	0.00
38.98	15.42	2.00	0.00	1.00	0.00	39.05	14.30	2.00	0.00	1.00	0.00
39.12	13.23	2.00	0.00	1.00	0.00	39.18	12.58	2.00	0.00	1.00	0.00
39.25	12.79	2.00	0.00	1.00	0.00	39.32	13.02	2.00	0.00	1.00	0.00
39.38	12.83	2.00	0.00	1.00	0.00	39.45	12.41	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
39.52	11.94	2.00	0.00	1.00	0.00	39.58	11.93	2.00	0.00	1.00	0.00
39.65	13.24	2.00	0.00	1.00	0.00	39.72	15.84	2.00	0.00	1.00	0.00
39.78	18.36	2.00	0.00	1.00	0.00	39.85	19.89	2.00	0.00	1.00	0.00
39.92	20.59	2.00	0.00	1.00	0.00	39.97	20.28	2.00	0.00	1.00	0.00
40.04	27.91	2.00	0.00	1.00	0.00	40.09	27.83	2.00	0.00	1.00	0.00
40.17	25.96	2.00	0.00	1.00	0.00	40.23	24.90	2.00	0.00	1.00	0.00
40.31	24.87	2.00	0.00	1.00	0.00	40.37	24.12	2.00	0.00	1.00	0.00
40.44	23.19	2.00	0.00	1.00	0.00	40.51	22.03	2.00	0.00	1.00	0.00
40.57	20.87	2.00	0.00	1.00	0.00	40.64	20.43	2.00	0.00	1.00	0.00
40.71	20.41	2.00	0.00	1.00	0.00	40.77	20.16	2.00	0.00	1.00	0.00
40.84	19.96	2.00	0.00	1.00	0.00	40.91	20.00	2.00	0.00	1.00	0.00
40.97	22.12	2.00	0.00	1.00	0.00	41.04	27.65	2.00	0.00	1.00	0.00
41.11	34.77	2.00	0.00	1.00	0.00	41.17	35.77	2.00	0.00	1.00	0.00
41.24	32.97	2.00	0.00	1.00	0.00	41.30	29.68	2.00	0.00	1.00	0.00
41.37	25.34	2.00	0.00	1.00	0.00	41.41	20.33	2.00	0.00	1.00	0.00
41.48	27.67	2.00	0.00	1.00	0.00	41.54	33.24	2.00	0.00	1.00	0.00
41.60	42.20	2.00	0.00	1.00	0.00	41.67	52.31	2.00	0.00	1.00	0.00
41.74	133.08	0.22	2.37	1.00	0.02	41.80	136.21	0.23	2.31	1.00	0.02
41.87	139.50	0.25	2.25	1.00	0.02	41.94	147.03	0.29	2.12	1.00	0.02
42.00	154.97	0.35	2.00	1.00	0.02	42.07	160.97	0.41	1.67	1.00	0.01
42.14	164.51	0.45	1.48	1.00	0.01	42.19	168.69	0.52	1.28	1.00	0.01
42.26	167.73	0.50	1.32	1.00	0.01	42.34	171.39	0.56	1.17	1.00	0.01
42.40	169.63	0.53	1.24	1.00	0.01	42.46	169.78	0.53	1.23	1.00	0.01
42.53	168.54	0.51	1.29	1.00	0.01	42.60	166.96	0.49	1.36	1.00	0.01
42.67	163.38	0.44	1.54	1.00	0.01	42.73	158.81	0.38	1.80	1.00	0.01
42.80	152.98	0.33	2.03	1.00	0.02	42.87	145.69	0.28	2.14	1.00	0.02
42.94	136.73	0.23	2.30	1.00	0.02	43.00	128.98	0.21	2.46	1.00	0.02
43.07	124.21	0.19	2.56	1.00	0.02	43.14	122.82	0.19	2.59	1.00	0.02
43.20	122.76	0.19	2.59	1.00	0.02	43.27	122.37	0.19	2.60	1.00	0.02
43.34	122.52	0.19	2.60	1.00	0.02	43.39	123.26	0.19	2.58	1.00	0.02
43.47	122.96	0.19	2.59	1.00	0.02	43.54	52.37	2.00	0.00	1.00	0.00
43.60	47.88	2.00	0.00	1.00	0.00	43.67	43.20	2.00	0.00	1.00	0.00
43.73	38.22	2.00	0.00	1.00	0.00	43.80	33.93	2.00	0.00	1.00	0.00
43.83	32.06	2.00	0.00	1.00	0.00	43.90	28.96	2.00	0.00	1.00	0.00
43.97	26.40	2.00	0.00	1.00	0.00	44.03	23.83	2.00	0.00	1.00	0.00
44.10	21.79	2.00	0.00	1.00	0.00	44.17	20.45	2.00	0.00	1.00	0.00
44.23	18.74	2.00	0.00	1.00	0.00	44.30	16.65	2.00	0.00	1.00	0.00
44.37	15.47	2.00	0.00	1.00	0.00	44.44	15.79	2.00	0.00	1.00	0.00
44.50	17.78	2.00	0.00	1.00	0.00	44.57	20.18	2.00	0.00	1.00	0.00
44.64	20.79	2.00	0.00	1.00	0.00	44.70	20.43	2.00	0.00	1.00	0.00
44.77	22.11	2.00	0.00	1.00	0.00	44.84	30.04	2.00	0.00	1.00	0.00
44.90	43.44	2.00	0.00	1.00	0.00	44.97	119.25	0.18	2.67	1.00	0.02
45.04	124.65	0.19	2.55	1.00	0.02	45.11	126.87	0.20	2.50	1.00	0.02
45.17	129.05	0.21	2.45	1.00	0.02	45.24	131.04	0.21	2.41	1.00	0.02
45.31	132.67	0.22	2.38	1.00	0.02	45.37	133.75	0.22	2.36	1.00	0.02
45.44	135.21	0.23	2.33	1.00	0.02	45.48	136.18	0.23	2.31	1.00	0.01
45.54	138.00	0.24	2.28	1.00	0.02	45.61	139.51	0.25	2.25	1.00	0.02
45.69	138.96	0.24	2.26	1.00	0.02	45.76	141.53	0.26	2.22	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
45.83	141.44	0.26	2.22	1.00	0.02	45.89	140.52	0.25	2.23	1.00	0.02
45.96	140.42	0.25	2.24	1.00	0.02	46.03	140.43	0.25	2.24	1.00	0.02
46.09	140.49	0.25	2.23	1.00	0.02	46.16	140.72	0.25	2.23	1.00	0.02
46.23	141.11	0.25	2.22	1.00	0.02	46.29	141.42	0.26	2.22	1.00	0.02
46.36	141.44	0.26	2.22	1.00	0.02	46.42	141.69	0.26	2.21	1.00	0.02
46.46	141.71	0.26	2.21	1.00	0.01	46.53	141.50	0.26	2.22	1.00	0.02
46.59	141.23	0.25	2.22	1.00	0.02	46.66	141.01	0.25	2.23	1.00	0.02
46.73	140.58	0.25	2.23	1.00	0.02	46.80	140.19	0.25	2.24	1.00	0.02
46.86	139.77	0.25	2.25	1.00	0.02	46.93	139.32	0.25	2.26	1.00	0.02
46.99	138.84	0.24	2.26	1.00	0.02	47.06	138.06	0.24	2.28	1.00	0.02
47.13	136.96	0.24	2.30	1.00	0.02	47.20	135.18	0.23	2.33	1.00	0.02
47.26	133.43	0.22	2.37	1.00	0.02	47.33	130.89	0.21	2.42	1.00	0.02
47.40	128.62	0.21	2.46	1.00	0.02	47.47	127.04	0.20	2.50	1.00	0.02
47.53	125.84	0.20	2.52	1.00	0.02	47.60	124.86	0.19	2.54	1.00	0.02
47.66	124.81	0.19	2.54	1.00	0.02	47.73	124.61	0.19	2.55	1.00	0.02
47.80	124.25	0.19	2.56	1.00	0.02	47.87	122.83	0.19	2.59	1.00	0.02
47.93	120.52	0.18	2.64	1.00	0.02	48.00	117.29	0.18	2.72	1.00	0.02
48.03	115.36	0.17	2.77	1.00	0.01	48.10	110.09	0.16	2.91	1.00	0.02
48.17	40.98	2.00	0.00	1.00	0.00	48.24	35.95	2.00	0.00	1.00	0.00
48.30	31.36	2.00	0.00	1.00	0.00	48.37	27.10	2.00	0.00	1.00	0.00
48.43	21.37	2.00	0.00	1.00	0.00	48.50	21.68	2.00	0.00	1.00	0.00
48.56	19.49	2.00	0.00	1.00	0.00	48.63	17.05	2.00	0.00	1.00	0.00
48.70	16.99	2.00	0.00	1.00	0.00	48.76	16.92	2.00	0.00	1.00	0.00
48.82	21.91	2.00	0.00	1.00	0.00	48.89	29.52	2.00	0.00	1.00	0.00
48.95	36.29	2.00	0.00	1.00	0.00	49.02	38.56	2.00	0.00	1.00	0.00
49.09	37.01	2.00	0.00	1.00	0.00	49.15	36.78	2.00	0.00	1.00	0.00
49.23	33.96	2.00	0.00	1.00	0.00	49.28	30.57	2.00	0.00	1.00	0.00
49.35	25.58	2.00	0.00	1.00	0.00	49.42	22.04	2.00	0.00	1.00	0.00
49.48	19.86	2.00	0.00	1.00	0.00	49.55	18.67	2.00	0.00	1.00	0.00
49.62	18.50	2.00	0.00	1.00	0.00	49.69	18.91	2.00	0.00	1.00	0.00
49.75	18.89	2.00	0.00	1.00	0.00	49.82	17.92	2.00	0.00	1.00	0.00
49.87	17.22	2.00	0.00	1.00	0.00	49.94	16.74	2.00	0.00	1.00	0.00
50.02	16.65	2.00	0.00	1.00	0.00	50.07	17.54	2.00	0.00	1.00	0.00
50.16	20.64	2.00	0.00	1.00	0.00	50.21	21.65	2.00	0.00	1.00	0.00
50.27	23.10	2.00	0.00	1.00	0.00	50.33	30.47	2.00	0.00	1.00	0.00
50.40	40.00	2.00	0.00	1.00	0.00	50.47	124.18	2.00	0.00	1.00	0.00
50.53	140.81	2.00	0.00	1.00	0.00	50.61	158.02	2.00	0.00	1.00	0.00
50.66	164.07	2.00	0.00	1.00	0.00	50.73	169.51	2.00	0.00	1.00	0.00
50.80	172.32	2.00	0.00	1.00	0.00	50.87	173.11	2.00	0.00	1.00	0.00
50.92	173.26	2.00	0.00	1.00	0.00	51.01	173.61	2.00	0.00	1.00	0.00
51.07	171.65	2.00	0.00	1.00	0.00	51.13	169.44	2.00	0.00	1.00	0.00
51.20	167.27	2.00	0.00	1.00	0.00	51.26	165.81	2.00	0.00	1.00	0.00
51.32	163.24	2.00	0.00	1.00	0.00	51.39	158.97	2.00	0.00	1.00	0.00
51.45	156.09	2.00	0.00	1.00	0.00	51.52	155.57	2.00	0.00	1.00	0.00
51.59	159.12	2.00	0.00	1.00	0.00	51.65	157.56	2.00	0.00	1.00	0.00
51.71	161.41	2.00	0.00	1.00	0.00	51.78	162.42	2.00	0.00	1.00	0.00
51.84	160.53	2.00	0.00	1.00	0.00	51.92	158.77	2.00	0.00	1.00	0.00
51.97	158.74	2.00	0.00	1.00	0.00	52.04	158.65	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
52.10	158.46	2.00	0.00	1.00	0.00	52.17	159.68	2.00	0.00	1.00	0.00
52.23	168.54	2.00	0.00	1.00	0.00	52.30	175.46	2.00	0.00	1.00	0.00
52.37	184.64	2.00	0.00	1.00	0.00	52.44	194.00	2.00	0.00	1.00	0.00
52.50	189.05	2.00	0.00	1.00	0.00	52.56	201.81	2.00	0.00	1.00	0.00
52.63	201.43	2.00	0.00	1.00	0.00	52.69	199.52	2.00	0.00	1.00	0.00
52.77	197.12	2.00	0.00	1.00	0.00	52.85	196.59	2.00	0.00	1.00	0.00
52.92	193.37	2.00	0.00	1.00	0.00	52.98	190.20	2.00	0.00	1.00	0.00
53.05	183.87	2.00	0.00	1.00	0.00	53.09	182.49	2.00	0.00	1.00	0.00
53.15	181.13	2.00	0.00	1.00	0.00	53.22	179.52	2.00	0.00	1.00	0.00
53.29	178.93	2.00	0.00	1.00	0.00	53.36	179.50	2.00	0.00	1.00	0.00
53.41	179.86	2.00	0.00	1.00	0.00	53.48	179.92	2.00	0.00	1.00	0.00
53.55	183.35	2.00	0.00	1.00	0.00	53.61	187.17	2.00	0.00	1.00	0.00
53.69	193.30	2.00	0.00	1.00	0.00	53.74	197.44	2.00	0.00	1.00	0.00
53.81	201.93	2.00	0.00	1.00	0.00	53.89	207.16	2.00	0.00	1.00	0.00
53.95	211.55	2.00	0.00	1.00	0.00	54.01	216.63	2.00	0.00	1.00	0.00
54.07	221.38	2.00	0.00	1.00	0.00	54.15	225.18	2.00	0.00	1.00	0.00
54.22	228.21	2.00	0.00	1.00	0.00	54.27	229.99	2.00	0.00	1.00	0.00
54.35	232.26	2.00	0.00	1.00	0.00	54.40	233.99	2.00	0.00	1.00	0.00
54.48	235.52	2.00	0.00	1.00	0.00	54.53	237.16	2.00	0.00	1.00	0.00
54.60	241.62	2.00	0.00	1.00	0.00	54.66	246.10	2.00	0.00	1.00	0.00
54.73	250.92	2.00	0.00	1.00	0.00	54.80	255.24	2.00	0.00	1.00	0.00
54.86	258.48	2.00	0.00	1.00	0.00	54.93	261.69	2.00	0.00	1.00	0.00
55.00	263.67	2.00	0.00	1.00	0.00	55.06	265.35	2.00	0.00	1.00	0.00
55.13	266.98	2.00	0.00	1.00	0.00	55.20	267.80	2.00	0.00	1.00	0.00
55.27	268.31	2.00	0.00	1.00	0.00	55.34	268.61	2.00	0.00	1.00	0.00
55.40	268.96	2.00	0.00	1.00	0.00	55.47	269.27	2.00	0.00	1.00	0.00
55.53	269.44	2.00	0.00	1.00	0.00	55.60	266.61	2.00	0.00	1.00	0.00
55.67	262.85	2.00	0.00	1.00	0.00	55.73	264.53	2.00	0.00	1.00	0.00
55.80	265.53	2.00	0.00	1.00	0.00	55.87	266.04	2.00	0.00	1.00	0.00
55.93	265.44	2.00	0.00	1.00	0.00	55.98	259.76	2.00	0.00	1.00	0.00
56.05	263.45	2.00	0.00	1.00	0.00	56.10	263.53	2.00	0.00	1.00	0.00
56.19	264.19	2.00	0.00	1.00	0.00	56.24	264.24	2.00	0.00	1.00	0.00
56.31	263.49	2.00	0.00	1.00	0.00	56.38	262.20	2.00	0.00	1.00	0.00
56.46	260.88	2.00	0.00	1.00	0.00	56.52	258.91	2.00	0.00	1.00	0.00
56.58	256.12	2.00	0.00	1.00	0.00	56.65	253.06	2.00	0.00	1.00	0.00
56.71	249.78	2.00	0.00	1.00	0.00	56.77	246.01	2.00	0.00	1.00	0.00
56.83	242.26	2.00	0.00	1.00	0.00	56.90	237.45	2.00	0.00	1.00	0.00
56.96	231.91	2.00	0.00	1.00	0.00	57.03	225.95	2.00	0.00	1.00	0.00
57.10	220.82	2.00	0.00	1.00	0.00	57.16	218.55	2.00	0.00	1.00	0.00
57.23	212.83	2.00	0.00	1.00	0.00	57.30	198.51	2.00	0.00	1.00	0.00
57.37	203.83	2.00	0.00	1.00	0.00	57.43	210.01	2.00	0.00	1.00	0.00
57.50	216.95	2.00	0.00	1.00	0.00	57.57	222.06	2.00	0.00	1.00	0.00
57.62	209.46	2.00	0.00	1.00	0.00	57.68	222.39	2.00	0.00	1.00	0.00
57.76	220.92	2.00	0.00	1.00	0.00	57.82	219.71	2.00	0.00	1.00	0.00
57.88	218.46	2.00	0.00	1.00	0.00	57.94	216.27	2.00	0.00	1.00	0.00
58.01	214.82	2.00	0.00	1.00	0.00	58.08	212.82	2.00	0.00	1.00	0.00
58.14	210.90	2.00	0.00	1.00	0.00	58.21	208.86	2.00	0.00	1.00	0.00
58.28	209.17	2.00	0.00	1.00	0.00	58.35	209.75	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
58.40	210.03	2.00	0.00	1.00	0.00	58.47	211.71	2.00	0.00	1.00	0.00
58.54	213.66	2.00	0.00	1.00	0.00	58.61	214.42	2.00	0.00	1.00	0.00
58.67	214.07	2.00	0.00	1.00	0.00	58.74	211.68	2.00	0.00	1.00	0.00
58.82	210.91	2.00	0.00	1.00	0.00	58.88	211.80	2.00	0.00	1.00	0.00
58.95	174.84	2.00	0.00	1.00	0.00	59.02	140.95	2.00	0.00	1.00	0.00
59.09	145.17	2.00	0.00	1.00	0.00	59.12	149.51	2.00	0.00	1.00	0.00
59.19	157.63	2.00	0.00	1.00	0.00	59.26	164.81	2.00	0.00	1.00	0.00
59.32	172.60	2.00	0.00	1.00	0.00	59.40	182.53	2.00	0.00	1.00	0.00
59.46	187.49	2.00	0.00	1.00	0.00	59.52	195.28	2.00	0.00	1.00	0.00
59.60	210.28	2.00	0.00	1.00	0.00	59.66	216.74	2.00	0.00	1.00	0.00
59.73	215.78	2.00	0.00	1.00	0.00	59.78	214.75	2.00	0.00	1.00	0.00
59.85	214.05	2.00	0.00	1.00	0.00	59.93	213.24	2.00	0.00	1.00	0.00
59.99	218.91	2.00	0.00	1.00	0.00	60.04	223.64	2.00	0.00	1.00	0.00
60.11	226.50	2.00	0.00	1.00	0.00	60.18	228.62	2.00	0.00	1.00	0.00
60.24	230.29	2.00	0.00	1.00	0.00	60.30	234.81	2.00	0.00	1.00	0.00
60.37	236.64	2.00	0.00	1.00	0.00	60.44	237.08	2.00	0.00	1.00	0.00
60.50	236.83	2.00	0.00	1.00	0.00	60.58	237.28	2.00	0.00	1.00	0.00
60.63	237.28	2.00	0.00	1.00	0.00	60.70	236.52	2.00	0.00	1.00	0.00
60.78	234.66	2.00	0.00	1.00	0.00	60.83	233.68	2.00	0.00	1.00	0.00
60.89	231.35	2.00	0.00	1.00	0.00	60.97	226.30	2.00	0.00	1.00	0.00
61.03	223.25	2.00	0.00	1.00	0.00	61.10	222.46	2.00	0.00	1.00	0.00
61.16	225.12	2.00	0.00	1.00	0.00	61.22	227.57	2.00	0.00	1.00	0.00
61.30	228.23	2.00	0.00	1.00	0.00	61.36	226.14	2.00	0.00	1.00	0.00
61.42	223.50	2.00	0.00	1.00	0.00	61.48	219.96	2.00	0.00	1.00	0.00
61.57	217.97	2.00	0.00	1.00	0.00	61.64	214.55	2.00	0.00	1.00	0.00
61.70	210.90	2.00	0.00	1.00	0.00	61.76	191.81	2.00	0.00	1.00	0.00
61.82	185.10	2.00	0.00	1.00	0.00	61.88	189.56	2.00	0.00	1.00	0.00
61.96	182.93	2.00	0.00	1.00	0.00	62.03	172.10	2.00	0.00	1.00	0.00
62.08	163.06	2.00	0.00	1.00	0.00	62.15	156.53	2.00	0.00	1.00	0.00
62.22	169.01	2.00	0.00	1.00	0.00	62.29	179.37	2.00	0.00	1.00	0.00
62.36	179.95	2.00	0.00	1.00	0.00	62.41	178.13	2.00	0.00	1.00	0.00
62.48	186.59	2.00	0.00	1.00	0.00	62.55	183.87	2.00	0.00	1.00	0.00
62.62	190.06	2.00	0.00	1.00	0.00	62.69	193.03	2.00	0.00	1.00	0.00
62.73	192.68	2.00	0.00	1.00	0.00	62.80	189.35	2.00	0.00	1.00	0.00
62.87	187.89	2.00	0.00	1.00	0.00	62.95	190.85	2.00	0.00	1.00	0.00
63.02	160.09	2.00	0.00	1.00	0.00	63.06	159.71	2.00	0.00	1.00	0.00
63.13	174.23	2.00	0.00	1.00	0.00	63.20	192.57	2.00	0.00	1.00	0.00
63.26	203.86	2.00	0.00	1.00	0.00	63.34	216.40	2.00	0.00	1.00	0.00
63.39	217.36	2.00	0.00	1.00	0.00	63.45	218.30	2.00	0.00	1.00	0.00
63.52	224.10	2.00	0.00	1.00	0.00	63.59	223.95	2.00	0.00	1.00	0.00
63.66	220.03	2.00	0.00	1.00	0.00	63.72	217.61	2.00	0.00	1.00	0.00
63.79	213.92	2.00	0.00	1.00	0.00	63.86	205.80	2.00	0.00	1.00	0.00
63.91	199.94	2.00	0.00	1.00	0.00	63.98	188.13	2.00	0.00	1.00	0.00
64.05	180.34	2.00	0.00	1.00	0.00	64.12	175.76	2.00	0.00	1.00	0.00
64.18	171.97	2.00	0.00	1.00	0.00	64.25	163.84	2.00	0.00	1.00	0.00
64.31	175.42	2.00	0.00	1.00	0.00	64.38	191.34	2.00	0.00	1.00	0.00
64.45	193.69	2.00	0.00	1.00	0.00	64.50	191.46	2.00	0.00	1.00	0.00
64.58	185.22	2.00	0.00	1.00	0.00	64.64	179.93	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
64.72	173.38	2.00	0.00	1.00	0.00	64.77	177.45	2.00	0.00	1.00	0.00
64.83	173.33	2.00	0.00	1.00	0.00	64.91	175.28	2.00	0.00	1.00	0.00
64.97	177.60	2.00	0.00	1.00	0.00	65.04	175.08	2.00	0.00	1.00	0.00
65.10	145.00	2.00	0.00	1.00	0.00	65.17	126.99	2.00	0.00	1.00	0.00
65.24	123.83	2.00	0.00	1.00	0.00	65.31	131.69	2.00	0.00	1.00	0.00
65.36	129.25	2.00	0.00	1.00	0.00	65.42	123.92	2.00	0.00	1.00	0.00
65.49	134.12	2.00	0.00	1.00	0.00	65.55	134.60	2.00	0.00	1.00	0.00
65.62	130.54	2.00	0.00	1.00	0.00	65.69	124.53	2.00	0.00	1.00	0.00
65.76	117.11	2.00	0.00	1.00	0.00	65.83	109.47	2.00	0.00	1.00	0.00
65.89	103.99	2.00	0.00	1.00	0.00	65.95	97.68	2.00	0.00	1.00	0.00
66.03	87.30	2.00	0.00	1.00	0.00	66.08	85.35	2.00	0.00	1.00	0.00
66.16	96.88	2.00	0.00	1.00	0.00	66.22	105.06	2.00	0.00	1.00	0.00
66.29	108.76	2.00	0.00	1.00	0.00	66.36	109.45	2.00	0.00	1.00	0.00
66.42	109.24	2.00	0.00	1.00	0.00	66.49	108.10	2.00	0.00	1.00	0.00
66.55	106.78	2.00	0.00	1.00	0.00	66.62	106.96	2.00	0.00	1.00	0.00
66.69	104.95	2.00	0.00	1.00	0.00	66.75	102.29	2.00	0.00	1.00	0.00
66.82	103.90	2.00	0.00	1.00	0.00	66.89	105.02	2.00	0.00	1.00	0.00
66.96	104.80	2.00	0.00	1.00	0.00	67.00	37.43	2.00	0.00	1.00	0.00
67.08	106.68	2.00	0.00	1.00	0.00	67.14	104.62	2.00	0.00	1.00	0.00
67.21	107.43	2.00	0.00	1.00	0.00	67.28	46.63	2.00	0.00	1.00	0.00
67.34	118.66	2.00	0.00	1.00	0.00	67.41	131.06	2.00	0.00	1.00	0.00
67.47	148.82	2.00	0.00	1.00	0.00	67.54	158.97	2.00	0.00	1.00	0.00
67.61	160.78	2.00	0.00	1.00	0.00	67.67	151.75	2.00	0.00	1.00	0.00
67.74	138.88	2.00	0.00	1.00	0.00	67.80	141.18	2.00	0.00	1.00	0.00
67.87	148.68	2.00	0.00	1.00	0.00	67.94	154.23	2.00	0.00	1.00	0.00
68.00	159.40	2.00	0.00	1.00	0.00	68.07	162.74	2.00	0.00	1.00	0.00
68.14	165.46	2.00	0.00	1.00	0.00	68.20	167.17	2.00	0.00	1.00	0.00
68.27	169.44	2.00	0.00	1.00	0.00	68.34	170.92	2.00	0.00	1.00	0.00
68.41	174.34	2.00	0.00	1.00	0.00	68.44	175.70	2.00	0.00	1.00	0.00
68.51	175.85	2.00	0.00	1.00	0.00	68.58	175.99	2.00	0.00	1.00	0.00
68.65	183.60	2.00	0.00	1.00	0.00	68.73	186.41	2.00	0.00	1.00	0.00
68.78	187.91	2.00	0.00	1.00	0.00	68.83	188.45	2.00	0.00	1.00	0.00
68.92	192.85	2.00	0.00	1.00	0.00	68.97	196.52	2.00	0.00	1.00	0.00
69.03	198.38	2.00	0.00	1.00	0.00	69.09	199.91	2.00	0.00	1.00	0.00
69.18	203.00	2.00	0.00	1.00	0.00	69.24	207.30	2.00	0.00	1.00	0.00
69.29	212.10	2.00	0.00	1.00	0.00	69.37	219.66	2.00	0.00	1.00	0.00
69.43	223.93	2.00	0.00	1.00	0.00	69.51	229.82	2.00	0.00	1.00	0.00
69.57	231.64	2.00	0.00	1.00	0.00	69.63	231.87	2.00	0.00	1.00	0.00
69.69	229.84	2.00	0.00	1.00	0.00	69.76	227.81	2.00	0.00	1.00	0.00
69.82	228.98	2.00	0.00	1.00	0.00	69.91	223.13	2.00	0.00	1.00	0.00
69.95	147.78	2.00	0.00	1.00	0.00	70.02	196.66	2.00	0.00	1.00	0.00
70.08	191.76	2.00	0.00	1.00	0.00	70.16	192.04	2.00	0.00	1.00	0.00
70.22	182.53	2.00	0.00	1.00	0.00	70.28	177.31	2.00	0.00	1.00	0.00
70.35	175.10	2.00	0.00	1.00	0.00	70.42	175.46	2.00	0.00	1.00	0.00
70.48	174.99	2.00	0.00	1.00	0.00	70.55	175.43	2.00	0.00	1.00	0.00
70.61	176.03	2.00	0.00	1.00	0.00	70.69	178.56	2.00	0.00	1.00	0.00
70.75	180.10	2.00	0.00	1.00	0.00	70.82	179.96	2.00	0.00	1.00	0.00
70.88	175.73	2.00	0.00	1.00	0.00	70.95	172.76	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
71.02	168.35	2.00	0.00	1.00	0.00	71.08	162.73	2.00	0.00	1.00	0.00
71.15	160.79	2.00	0.00	1.00	0.00	71.22	158.63	2.00	0.00	1.00	0.00
71.28	156.55	2.00	0.00	1.00	0.00	71.35	155.96	2.00	0.00	1.00	0.00
71.42	156.15	2.00	0.00	1.00	0.00	71.49	159.22	2.00	0.00	1.00	0.00
71.54	155.95	2.00	0.00	1.00	0.00	71.59	152.71	2.00	0.00	1.00	0.00
71.67	162.23	2.00	0.00	1.00	0.00	71.73	168.06	2.00	0.00	1.00	0.00
71.79	170.59	2.00	0.00	1.00	0.00	71.86	170.86	2.00	0.00	1.00	0.00
71.92	169.20	2.00	0.00	1.00	0.00	71.99	164.27	2.00	0.00	1.00	0.00
72.06	156.30	2.00	0.00	1.00	0.00	72.12	152.02	2.00	0.00	1.00	0.00
72.19	146.49	2.00	0.00	1.00	0.00	72.26	142.54	2.00	0.00	1.00	0.00
72.31	140.07	2.00	0.00	1.00	0.00	72.38	147.48	2.00	0.00	1.00	0.00
72.46	145.49	2.00	0.00	1.00	0.00	72.52	137.31	2.00	0.00	1.00	0.00
72.59	143.72	2.00	0.00	1.00	0.00	72.65	148.74	2.00	0.00	1.00	0.00
72.71	156.70	2.00	0.00	1.00	0.00	72.78	174.96	2.00	0.00	1.00	0.00
72.84	177.80	2.00	0.00	1.00	0.00	72.90	161.21	2.00	0.00	1.00	0.00
72.98	160.53	2.00	0.00	1.00	0.00	73.03	170.82	2.00	0.00	1.00	0.00
73.11	173.58	2.00	0.00	1.00	0.00	73.17	171.44	2.00	0.00	1.00	0.00
73.23	178.36	2.00	0.00	1.00	0.00	73.30	177.32	2.00	0.00	1.00	0.00
73.36	183.85	2.00	0.00	1.00	0.00	73.44	190.95	2.00	0.00	1.00	0.00
73.51	194.40	2.00	0.00	1.00	0.00	73.56	188.79	2.00	0.00	1.00	0.00
73.63	188.51	2.00	0.00	1.00	0.00	73.70	199.89	2.00	0.00	1.00	0.00
73.76	204.78	2.00	0.00	1.00	0.00	73.83	203.04	2.00	0.00	1.00	0.00
73.89	189.75	2.00	0.00	1.00	0.00	73.95	196.43	2.00	0.00	1.00	0.00
74.02	208.75	2.00	0.00	1.00	0.00	74.09	208.15	2.00	0.00	1.00	0.00
74.16	198.70	2.00	0.00	1.00	0.00	74.24	202.33	2.00	0.00	1.00	0.00
74.31	193.36	2.00	0.00	1.00	0.00	74.38	180.96	2.00	0.00	1.00	0.00
74.41	175.69	2.00	0.00	1.00	0.00	74.48	165.91	2.00	0.00	1.00	0.00
74.55	154.62	2.00	0.00	1.00	0.00	74.62	138.77	2.00	0.00	1.00	0.00
74.68	143.63	2.00	0.00	1.00	0.00	74.75	149.46	2.00	0.00	1.00	0.00
74.82	156.24	2.00	0.00	1.00	0.00	74.89	161.42	2.00	0.00	1.00	0.00
74.94	162.79	2.00	0.00	1.00	0.00	75.01	161.56	2.00	0.00	1.00	0.00
75.07	146.74	2.00	0.00	1.00	0.00	75.14	181.92	2.00	0.00	1.00	0.00
75.20	177.65	2.00	0.00	1.00	0.00	75.27	176.14	2.00	0.00	1.00	0.00
75.33	175.07	2.00	0.00	1.00	0.00	75.41	174.62	2.00	0.00	1.00	0.00
75.48	166.91	2.00	0.00	1.00	0.00						

Total estimated settlement: 5.37

Abbreviations

Q_{tn,cs}: Equivalent clean sand normalized cone resistance
 FS: Factor of safety against liquefaction
 e_v (%): Post-liquefaction volumetric strain
 DF: e_v depth weighting factor
 Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::							
Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.07	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.14	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.20	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.27	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.35	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.41	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.47	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.54	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.60	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.66	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.74	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.80	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.87	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.93	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.99	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.05	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.12	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.19	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.27	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.32	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.38	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.45	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.51	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.59	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.65	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.71	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.77	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.84	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.92	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.98	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.04	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.11	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.17	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.23	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.30	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.37	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.43	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.49	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.56	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.65	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.71	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.78	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.83	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.90	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.96	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.03	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.11	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.16	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
3.22	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.28	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.36	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.44	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.49	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.56	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.61	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.69	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.74	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.83	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.88	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.96	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.00	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.08	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.16	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.21	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.29	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.34	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.40	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.47	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.55	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.60	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.68	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.73	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.81	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.87	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.92	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
5.00	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
5.08	22.97	36.41	2.23	81.05	2.37	0.09	0.74
5.13	29.09	46.24	1.80	83.47	2.27	0.10	0.75
5.19	34.92	55.60	1.62	90.19	2.20	0.11	0.77
5.27	40.38	64.37	1.52	97.97	2.16	0.12	0.78
5.32	43.95	70.10	1.49	104.19	2.14	0.13	0.79
5.39	49.52	79.03	1.47	115.88	2.13	0.14	0.80
5.45	53.28	85.07	1.45	123.41	2.12	0.15	0.81
5.53	57.70	92.16	1.45	133.56	2.12	0.16	0.82
5.58	60.43	96.54	1.44	139.07	2.11	0.16	0.82
5.66	64.67	103.35	1.41	145.86	2.09	0.17	0.83
5.72	65.14	104.10	1.41	146.75	2.09	0.17	0.83
5.80	63.07	100.76	1.44	144.92	2.11	0.17	0.83
5.85	58.36	93.19	1.52	141.83	2.16	0.16	0.82
5.91	53.09	84.72	1.66	140.58	2.22	0.15	0.81
5.99	45.75	72.92	1.96	143.00	2.31	0.14	0.80
6.04	42.27	67.32	2.17	146.07	2.36	0.14	0.79
6.12	45.47	72.46	2.03	146.80	2.33	0.14	0.80
6.18	41.99	66.86	2.34	156.34	2.39	0.14	0.79
6.26	45.19	71.99	2.27	163.63	2.38	0.14	0.80
6.31	47.35	75.46	2.22	167.48	2.37	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
6.39	49.99	79.70	2.18	173.71	2.36	0.15	0.81
6.44	50.93	81.20	2.21	179.27	2.37	0.16	0.81
6.52	54.50	86.94	1.97	171.44	2.31	0.16	0.82
6.58	58.17	92.83	1.73	160.67	2.24	0.16	0.82
6.63	61.47	98.12	1.64	161.14	2.21	0.17	0.83
6.71	65.79	105.06	1.53	161.09	2.16	0.17	0.83
6.77	68.90	110.05	1.48	163.02	2.14	0.18	0.83
6.85	73.04	116.69	1.42	166.21	2.10	0.18	0.84
6.91	64.49	102.95	1.56	160.83	2.18	0.17	0.83
6.96	77.86	124.41	1.36	169.72	2.06	0.19	0.84
7.04	83.79	133.93	1.32	176.53	2.01	0.20	0.84
7.09	87.83	140.42	1.30	182.13	1.99	0.21	0.84
7.17	94.23	150.69	1.28	192.54	1.96	0.23	0.85
7.22	98.37	157.34	1.27	199.12	1.94	0.24	0.85
7.31	105.52	167.80	1.25	209.57	1.92	0.27	0.85
7.36	110.32	174.08	1.24	216.16	1.91	0.30	0.85
7.44	117.47	183.22	1.23	225.47	1.89	0.34	0.86
7.49	120.67	187.17	1.23	229.71	1.89	0.37	0.86
7.55	122.84	189.82	1.23	233.18	1.89	0.39	0.86
7.63	123.31	190.42	1.24	236.28	1.91	0.39	0.87
7.68	122.65	189.47	1.25	237.01	1.92	0.39	0.87
7.76	119.26	184.76	1.27	234.87	1.95	0.36	0.88
7.81	116.16	180.42	1.29	232.31	1.97	0.35	0.88
7.89	110.23	171.99	1.32	226.74	2.01	0.31	0.87
7.95	105.52	165.24	1.35	222.34	2.04	0.29	0.87
8.03	99.78	156.70	1.39	217.09	2.08	0.27	0.87
8.09	96.87	152.08	1.41	213.76	2.09	0.25	0.86
8.14	93.39	146.68	1.43	210.05	2.11	0.24	0.86
8.22	89.24	139.97	1.47	205.12	2.13	0.23	0.86
8.27	85.86	134.71	1.50	201.74	2.15	0.22	0.85
8.35	80.49	126.47	1.56	197.50	2.18	0.20	0.85
8.40	77.11	121.28	1.61	195.50	2.20	0.19	0.84
8.48	73.06	114.78	1.67	191.82	2.22	0.18	0.83
8.54	71.08	111.35	1.69	188.38	2.23	0.18	0.83
8.62	70.14	108.96	1.68	182.57	2.22	0.17	0.83
8.67	69.86	107.81	1.65	178.39	2.22	0.17	0.83
8.73	68.26	104.92	1.66	174.42	2.22	0.17	0.82
8.81	67.32	102.64	1.65	169.35	2.21	0.16	0.82
8.86	69.30	104.56	1.59	166.02	2.19	0.16	0.82
8.94	72.97	108.33	1.50	162.62	2.15	0.17	0.83
9.00	75.98	111.60	1.45	161.99	2.12	0.17	0.83
9.08	79.74	115.48	1.40	162.01	2.09	0.17	0.83
9.13	81.25	116.84	1.39	162.00	2.08	0.18	0.83
9.20	81.81	117.04	1.38	161.92	2.07	0.18	0.83
9.26	81.53	116.30	1.39	162.05	2.08	0.18	0.83
9.33	80.87	115.07	1.41	161.92	2.09	0.18	0.83
9.39	79.46	111.33	1.35	150.43	2.05	0.16	0.82
9.46	78.05	104.44	1.21	126.79	1.87	0.14	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
9.53	76.26	102.74	1.25	128.12	1.92	0.14	0.78
9.60	73.91	100.14	1.28	127.89	1.96	0.14	0.79
9.67	71.46	95.00	1.23	117.18	1.89	0.12	0.77
9.73	69.48	90.99	1.20	108.90	1.85	0.12	0.74
9.79	57.82	77.42	1.28	99.34	1.97	0.11	0.76
9.86	65.34	86.52	1.26	108.84	1.93	0.12	0.76
9.91	65.34	86.71	1.27	110.47	1.96	0.12	0.77
9.98	64.21	85.64	1.31	112.02	2.00	0.12	0.78
10.04	63.87	85.44	1.34	114.33	2.03	0.12	0.79
10.11	63.55	85.11	1.37	116.33	2.06	0.13	0.79
10.18	65.43	87.42	1.38	120.41	2.07	0.13	0.79
10.25	67.50	90.06	1.40	125.68	2.08	0.14	0.80
10.31	69.66	92.72	1.40	130.09	2.09	0.14	0.81
10.37	71.26	94.57	1.41	133.22	2.09	0.14	0.81
10.44	72.20	95.56	1.42	135.80	2.10	0.15	0.81
10.51	70.42	93.28	1.47	136.71	2.13	0.15	0.81
10.57	66.18	87.97	1.55	136.79	2.17	0.14	0.81
10.64	61.38	81.91	1.68	137.31	2.22	0.14	0.80
10.71	57.05	76.39	1.82	139.19	2.27	0.13	0.79
10.77	53.29	71.54	1.98	142.00	2.32	0.13	0.79
10.84	48.96	65.92	2.20	145.06	2.37	0.13	0.78
10.91	45.76	61.66	2.39	147.21	2.40	0.12	0.78
10.98	45.10	60.49	2.41	145.66	2.41	0.12	0.77
11.05	44.73	59.73	2.43	145.02	2.41	0.12	0.77
11.11	44.82	59.60	2.44	145.66	2.41	0.12	0.77
11.18	42.75	56.78	2.59	147.25	2.44	0.12	0.77
11.25	43.60	57.64	2.58	148.98	2.44	0.12	0.77
11.31	45.86	60.16	2.46	147.86	2.42	0.12	0.77
11.38	46.51	60.61	2.39	145.03	2.40	0.12	0.78
11.45	47.17	61.13	2.36	143.97	2.40	0.12	0.78
11.51	46.51	60.11	2.42	145.28	2.41	0.12	0.78
11.58	45.76	58.64	2.30	134.94	2.39	0.12	0.77
11.65	46.51	58.96	2.10	123.77	2.34	0.12	0.77
11.68	46.14	58.33	2.09	121.71	2.34	0.12	0.77
11.75	45.57	57.23	2.03	116.22	2.33	0.11	0.77
11.82	44.35	55.40	2.02	111.72	2.32	0.11	0.76
11.88	44.40	55.16	1.98	109.36	2.31	0.11	0.76
11.97	44.48	55.05	2.03	111.52	2.33	0.11	0.76
12.03	44.48	54.94	2.09	114.62	2.34	0.11	0.76
12.10	43.62	53.93	2.26	121.88	2.38	0.11	0.76
12.16	44.17	54.67	2.46	134.51	2.42	0.12	0.77
12.23	43.98	54.55	2.75	150.01	2.47	0.12	0.77
12.30	43.42	53.89	3.03	163.16	2.51	0.12	0.77
12.36	44.92	55.59	3.09	171.87	2.52	0.12	0.77
12.43	46.25	57.00	3.11	177.14	2.52	0.12	0.77
12.50	47.76	58.57	3.07	179.67	2.51	0.13	0.78
12.53	49.08	59.99	2.99	179.45	2.50	0.13	0.78
12.60	52.46	63.61	2.76	175.50	2.47	0.13	0.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
12.67	57.07	68.49	2.42	165.54	2.41	0.14	0.79
12.74	61.78	73.36	2.11	154.86	2.35	0.14	0.80
12.80	65.92	77.47	1.87	144.68	2.28	0.14	0.80
12.87	69.68	81.14	1.70	138.05	2.23	0.14	0.81
12.94	74.86	86.42	1.57	135.98	2.18	0.15	0.81
13.00	80.41	91.95	1.46	134.24	2.13	0.15	0.82
13.07	85.49	96.93	1.38	134.04	2.07	0.16	0.82
13.13	89.91	101.28	1.34	136.21	2.04	0.16	0.82
13.20	92.74	104.02	1.33	138.62	2.03	0.16	0.82
13.27	95.00	106.04	1.32	139.81	2.01	0.17	0.82
13.34	98.29	109.26	1.31	143.11	2.00	0.17	0.82
13.40	101.02	112.00	1.31	147.20	2.01	0.18	0.83
13.47	103.37	114.29	1.32	150.50	2.01	0.19	0.83
13.54	105.72	116.50	1.32	153.21	2.01	0.19	0.84
13.60	107.89	118.51	1.31	155.63	2.01	0.20	0.84
13.67	110.33	120.76	1.31	158.25	2.00	0.20	0.84
13.74	112.78	123.00	1.31	160.57	2.00	0.21	0.84
13.80	115.89	125.97	1.30	164.01	1.99	0.22	0.85
13.87	118.99	128.92	1.30	167.61	1.99	0.23	0.85
13.94	121.62	131.30	1.30	170.19	1.99	0.24	0.85
14.00	123.79	133.17	1.29	171.91	1.98	0.24	0.85
14.07	125.29	134.05	1.27	170.32	1.95	0.24	0.85
14.14	126.14	134.36	1.26	169.13	1.93	0.24	0.84
14.21	126.80	134.66	1.26	169.68	1.94	0.24	0.84
14.24	126.80	134.48	1.26	169.74	1.94	0.24	0.85
14.31	127.08	134.43	1.27	170.33	1.95	0.24	0.85
14.37	124.35	131.26	1.28	167.54	1.96	0.23	0.85
14.46	125.77	132.22	1.27	168.21	1.95	0.24	0.85
14.52	125.58	131.68	1.28	168.13	1.96	0.24	0.85
14.59	124.92	130.71	1.29	168.25	1.97	0.24	0.85
14.65	123.88	129.36	1.30	168.17	1.99	0.24	0.85
14.72	122.85	127.99	1.31	167.71	2.00	0.24	0.85
14.79	122.00	126.79	1.32	167.46	2.02	0.24	0.86
14.85	121.25	125.65	1.33	166.58	2.02	0.23	0.85
14.92	120.40	124.42	1.33	165.69	2.03	0.23	0.85
14.99	120.03	123.69	1.34	165.53	2.03	0.23	0.85
15.05	119.46	122.76	1.35	165.12	2.04	0.23	0.85
15.12	119.37	122.27	1.34	164.32	2.04	0.23	0.85
15.19	119.08	121.59	1.34	163.32	2.04	0.23	0.85
15.22	119.18	121.50	1.34	163.07	2.04	0.23	0.85
15.29	118.90	120.83	1.34	162.18	2.04	0.23	0.85
15.36	118.05	119.61	1.34	160.66	2.04	0.22	0.85
15.43	117.11	118.29	1.35	159.20	2.04	0.22	0.85
15.49	115.98	116.81	1.35	157.70	2.05	0.21	0.85
15.56	114.19	114.67	1.36	155.47	2.05	0.21	0.85
15.63	112.31	112.44	1.36	152.79	2.05	0.20	0.84
15.69	109.30	109.10	1.37	149.17	2.06	0.20	0.84
15.76	104.03	103.56	1.39	144.19	2.08	0.18	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
15.82	97.63	96.94	1.44	140.00	2.12	0.17	0.83
15.89	90.38	89.52	1.53	136.89	2.16	0.16	0.82
15.96	82.29	81.28	1.65	134.30	2.21	0.15	0.82
16.03	72.88	71.78	1.88	134.99	2.29	0.14	0.80
16.10	63.75	62.58	2.21	138.54	2.37	0.13	0.79
16.16	54.16	52.97	2.77	146.96	2.47	0.12	0.78
16.23	45.78	44.57	3.53	157.38	2.57	0.12	0.76
16.30	41.26	39.98	4.13	165.21	2.64	0.11	0.62
16.36	38.63	37.25	4.56	169.94	2.69	0.11	0.62
16.43	37.31	35.83	4.79	171.55	2.71	0.11	0.62
16.50	37.31	35.69	4.84	172.83	2.71	0.11	0.62
16.56	37.31	35.49	3.71	131.79	2.60	0.10	0.74
16.63	38.35	36.36	3.43	124.71	2.56	0.10	0.74
16.70	38.44	36.34	3.83	139.06	2.61	0.11	0.62
16.73	38.91	36.73	3.96	145.46	2.62	0.11	0.62
16.80	40.61	38.24	4.12	157.75	2.64	0.11	0.62
16.87	43.15	40.55	4.15	168.42	2.64	0.11	0.62
16.94	45.69	42.83	4.11	176.12	2.64	0.12	0.62
17.00	54.64	51.20	3.34	170.94	2.55	0.13	0.78
17.08	62.26	58.22	2.92	170.07	2.49	0.14	0.79
17.14	68.19	63.66	2.64	168.04	2.45	0.14	0.80
17.20	75.53	70.38	2.32	163.22	2.39	0.15	0.81
17.27	83.34	77.52	2.06	159.52	2.33	0.16	0.82
17.34	90.39	83.91	1.88	157.62	2.29	0.18	0.83
17.40	95.10	88.08	1.78	157.13	2.26	0.18	0.83
17.47	98.67	91.15	1.73	157.56	2.24	0.19	0.84
17.53	102.53	94.47	1.68	158.37	2.22	0.20	0.84
17.60	105.73	97.17	1.64	159.34	2.21	0.20	0.85
17.67	107.90	98.90	1.62	160.38	2.20	0.21	0.85
17.73	109.12	99.73	1.62	161.69	2.20	0.21	0.85
17.80	109.03	99.34	1.65	163.52	2.21	0.21	0.85
17.87	108.56	98.59	1.68	165.19	2.22	0.21	0.85
17.93	107.24	97.07	1.71	166.22	2.24	0.21	0.85
18.00	105.45	95.12	1.75	166.22	2.25	0.21	0.85
18.07	102.72	92.33	1.78	164.70	2.26	0.20	0.84
18.14	98.49	88.17	1.86	164.20	2.28	0.19	0.84
18.20	92.74	82.66	1.98	163.82	2.31	0.18	0.83
18.27	85.96	76.24	2.14	163.48	2.35	0.17	0.82
18.34	78.72	69.44	2.35	163.46	2.40	0.16	0.81
18.37	74.95	65.92	2.48	163.68	2.42	0.15	0.81
18.44	67.80	59.27	2.77	163.92	2.47	0.14	0.80
18.51	59.71	51.81	3.20	165.97	2.53	0.13	0.78
18.57	50.58	43.46	4.01	174.07	2.63	0.12	0.62
18.64	43.71	37.19	4.80	178.47	2.71	0.11	0.62
18.71	38.82	32.73	5.52	180.54	2.77	0.11	0.62
18.78	36.56	30.64	5.78	177.19	2.79	0.11	0.62
18.84	34.40	28.64	6.04	172.89	2.81	0.10	0.62
18.91	30.07	24.77	7.00	173.45	2.89	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
18.98	27.15	22.19	7.78	172.66	2.94	0.10	0.62
19.04	25.17	20.42	8.33	170.21	2.97	0.09	0.62
19.11	23.67	19.08	8.73	166.53	3.00	0.09	0.62
19.18	22.26	17.82	9.25	164.76	3.03	0.09	1.27
19.24	21.13	16.80	8.94	150.16	3.01	0.09	1.20
19.31	21.13	16.75	6.68	111.96	2.86	0.09	0.62
19.38	21.13	16.69	7.01	116.97	2.89	0.09	0.62
19.44	21.13	16.63	7.34	122.05	2.91	0.09	0.62
19.51	22.54	17.74	7.09	125.79	2.89	0.09	0.62
19.58	24.52	19.34	6.49	125.47	2.85	0.09	0.62
19.63	26.96	21.37	5.72	122.23	2.79	0.09	0.62
19.69	34.40	27.69	4.04	111.87	2.63	0.10	0.62
19.76	38.82	31.41	3.39	106.37	2.56	0.10	0.74
19.82	40.14	32.45	3.27	105.96	2.54	0.10	0.74
19.89	39.01	31.35	3.54	111.02	2.57	0.10	0.74
19.95	36.75	29.30	3.97	116.35	2.62	0.10	0.62
20.02	27.62	21.47	6.06	130.11	2.82	0.09	0.62
20.09	29.86	23.27	5.49	127.66	2.77	0.09	0.62
20.16	27.13	20.89	6.36	132.81	2.84	0.09	0.62
20.23	26.58	20.35	6.69	136.08	2.86	0.09	0.62
20.29	26.75	20.42	6.80	138.91	2.87	0.09	0.62
20.36	26.67	20.28	7.00	142.03	2.89	0.09	0.62
20.42	27.52	20.90	6.91	144.33	2.88	0.09	0.62
20.49	29.30	22.25	6.54	145.59	2.85	0.10	0.62
20.56	31.56	24.02	6.07	145.79	2.82	0.10	0.62
20.63	34.76	26.57	5.42	143.89	2.76	0.10	0.62
20.69	38.43	29.51	4.74	140.01	2.70	0.10	0.62
20.76	42.29	32.61	4.13	134.81	2.64	0.11	0.62
20.83	45.58	35.25	3.70	130.40	2.59	0.11	0.75
20.89	46.62	36.00	3.58	129.01	2.58	0.11	0.75
20.96	46.05	35.42	3.64	129.10	2.59	0.11	0.75
21.03	43.33	33.09	3.92	129.57	2.62	0.11	0.62
21.09	39.00	29.46	4.47	131.83	2.68	0.10	0.62
21.16	35.42	26.49	4.92	130.25	2.72	0.10	0.62
21.23	33.16	24.67	4.87	120.12	2.72	0.10	0.62
21.26	31.85	23.60	5.01	118.20	2.73	0.09	0.62
21.33	29.40	21.51	5.85	125.74	2.80	0.09	0.62
21.40	28.74	20.88	6.25	130.49	2.83	0.09	0.62
21.46	29.02	21.02	6.32	132.89	2.84	0.09	0.62
21.53	23.09	16.44	8.73	143.54	3.00	0.09	0.62
21.60	30.53	22.02	6.33	139.34	2.84	0.10	0.62
21.66	30.90	22.20	6.52	144.87	2.85	0.10	0.62
21.73	31.37	22.48	6.66	149.67	2.86	0.10	0.62
21.80	32.41	23.19	6.56	152.05	2.85	0.10	0.62
21.86	34.29	24.56	6.24	153.27	2.83	0.10	0.62
21.93	35.80	25.64	6.06	155.27	2.82	0.10	0.62
22.00	37.40	26.79	5.86	156.84	2.80	0.10	0.62
22.06	39.47	28.29	5.63	159.16	2.78	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
22.13	41.91	30.06	5.40	162.26	2.76	0.11	0.62
22.19	45.50	32.72	4.99	163.42	2.73	0.11	0.62
22.26	50.20	36.28	4.47	161.99	2.68	0.12	0.62
22.33	53.69	38.87	4.15	161.50	2.64	0.12	0.62
22.40	55.76	40.33	4.06	163.87	2.63	0.12	0.62
22.46	57.07	41.17	4.08	168.12	2.64	0.12	0.62
22.53	59.43	42.85	3.96	169.82	2.62	0.13	0.62
22.60	62.44	45.08	3.69	166.49	2.59	0.13	0.78
22.66	65.35	47.29	3.37	159.59	2.55	0.13	0.78
22.73	67.14	48.66	3.11	151.28	2.52	0.13	0.79
22.80	70.62	51.32	2.82	144.88	2.48	0.13	0.79
22.86	76.74	56.02	2.51	140.63	2.43	0.14	0.80
22.93	84.55	62.10	2.18	135.23	2.36	0.15	0.81
23.00	90.76	67.63	1.66	112.39	2.22	0.15	0.81
23.03	92.92	69.59	1.53	106.82	2.17	0.14	0.81
23.10	94.05	70.32	1.53	107.32	2.16	0.14	0.81
23.17	93.77	69.86	1.55	108.28	2.17	0.14	0.81
23.24	95.75	71.22	1.54	109.91	2.17	0.15	0.81
23.30	99.89	74.25	1.53	113.28	2.16	0.15	0.82
23.37	94.05	69.18	1.67	115.80	2.22	0.15	0.81
23.43	106.00	78.47	1.53	120.37	2.16	0.17	0.82
23.50	107.60	79.40	1.55	123.42	2.17	0.17	0.83
23.56	105.91	77.73	1.61	125.33	2.20	0.17	0.83
23.63	104.50	76.32	1.66	127.04	2.22	0.17	0.83
23.70	105.63	76.97	1.67	128.25	2.22	0.17	0.83
23.76	111.65	81.54	1.59	129.48	2.19	0.18	0.83
23.83	117.30	85.85	1.52	130.53	2.16	0.19	0.84
23.90	120.59	88.39	1.47	130.05	2.13	0.19	0.84
23.96	120.12	87.90	1.46	128.55	2.13	0.19	0.84
24.03	115.89	84.42	1.49	125.60	2.14	0.18	0.83
24.10	107.04	77.29	1.57	121.65	2.18	0.17	0.83
24.17	95.47	68.06	1.76	119.47	2.25	0.15	0.81
24.23	83.23	58.42	2.06	120.44	2.33	0.14	0.80
24.30	69.95	48.13	2.60	125.20	2.44	0.13	0.78
24.37	56.69	38.03	3.54	134.61	2.57	0.12	0.76
24.43	44.64	29.04	5.01	145.41	2.73	0.11	0.62
24.50	35.80	22.71	6.57	149.22	2.86	0.10	0.62
24.57	30.25	18.98	7.75	147.17	2.94	0.09	0.62
24.63	27.14	16.88	8.37	141.30	2.98	0.09	0.62
24.70	26.76	16.58	7.80	129.28	2.94	0.09	0.62
24.77	25.92	15.98	7.61	121.72	2.93	0.09	0.62
24.84	27.80	17.17	6.94	119.17	2.88	0.09	0.62
24.87	30.44	18.86	6.27	118.28	2.83	0.09	0.62
24.94	38.25	24.28	4.86	117.96	2.71	0.10	0.62
25.01	51.24	33.45	3.52	117.86	2.57	0.11	0.75
25.07	65.07	43.28	2.78	120.21	2.47	0.12	0.77
25.14	73.54	49.18	2.57	126.19	2.43	0.13	0.79
25.21	86.24	58.30	2.20	128.54	2.37	0.15	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
25.28	96.59	65.68	2.01	132.26	2.32	0.16	0.82
25.34	107.23	73.37	1.84	134.82	2.28	0.18	0.83
25.41	117.30	80.80	1.68	135.71	2.22	0.19	0.84
25.48	121.62	84.16	1.58	132.61	2.18	0.20	0.84
25.54	119.37	82.88	1.50	123.91	2.15	0.18	0.84
25.61	111.93	76.90	1.60	123.09	2.19	0.17	0.83
25.68	103.75	70.47	1.75	123.03	2.25	0.16	0.82
25.75	94.34	63.17	1.98	125.06	2.31	0.15	0.81
25.81	84.27	55.52	2.32	128.88	2.39	0.14	0.80
25.87	67.42	43.17	3.20	137.95	2.53	0.13	0.78
25.93	64.04	40.75	3.32	135.36	2.55	0.12	0.77
26.00	52.37	32.47	4.29	139.36	2.66	0.11	0.62
26.06	44.75	27.11	5.31	143.84	2.75	0.11	0.62
26.13	40.32	24.01	6.09	146.34	2.82	0.10	0.62
26.20	37.78	22.38	6.51	145.63	2.85	0.10	0.62
26.27	37.41	22.09	6.48	143.17	2.85	0.10	0.62
26.33	37.97	22.38	6.26	139.99	2.83	0.10	0.62
26.40	35.43	20.76	6.84	141.99	2.87	0.10	0.62
26.47	32.42	18.86	7.65	144.24	2.93	0.10	0.62
26.53	30.16	17.43	8.33	145.25	2.97	0.09	0.62
26.60	30.16	17.38	8.12	141.10	2.96	0.09	0.62
26.66	30.16	17.34	8.01	138.86	2.95	0.09	0.62
26.73	30.16	17.29	8.16	141.18	2.96	0.09	0.62
26.80	31.20	17.88	7.79	139.27	2.94	0.09	0.62
26.86	31.95	18.29	7.90	144.39	2.95	0.10	0.62
26.93	37.41	21.53	6.66	143.45	2.86	0.10	0.62
27.00	47.85	28.22	4.85	136.89	2.71	0.11	0.62
27.06	58.67	35.51	3.63	129.00	2.59	0.12	0.76
27.13	69.40	42.88	2.84	121.63	2.48	0.13	0.78
27.17	72.41	44.93	2.68	120.33	2.45	0.13	0.78
27.23	72.79	45.04	2.70	121.68	2.46	0.13	0.78
27.30	68.93	42.19	2.96	125.04	2.50	0.13	0.78
27.37	63.38	38.25	3.36	128.63	2.55	0.12	0.77
27.43	57.17	33.96	3.84	130.42	2.61	0.11	0.62
27.50	50.11	29.19	4.52	131.97	2.68	0.11	0.62
27.57	44.37	25.32	5.34	135.27	2.76	0.10	0.62
27.64	44.32	25.19	5.43	136.79	2.77	0.10	0.62
27.70	44.32	25.07	5.58	139.77	2.78	0.10	0.62
27.77	44.28	25.07	5.35	134.04	2.76	0.10	0.62
27.84	48.51	27.97	4.34	121.26	2.66	0.11	0.62
27.91	55.00	32.29	3.55	114.50	2.58	0.11	0.75
27.98	61.31	36.51	3.00	109.55	2.50	0.11	0.76
28.04	68.46	41.37	2.54	104.94	2.43	0.12	0.77
28.09	67.89	40.87	2.60	106.18	2.44	0.12	0.77
28.16	83.70	51.80	1.96	101.54	2.31	0.13	0.79
28.22	90.38	56.42	1.79	100.78	2.26	0.14	0.80
28.28	95.94	60.29	1.67	100.75	2.22	0.14	0.80
28.35	99.79	62.89	1.61	101.54	2.20	0.14	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
28.42	103.37	65.21	1.58	103.33	2.19	0.15	0.81
28.49	106.48	67.18	1.57	105.19	2.18	0.15	0.81
28.55	109.30	68.96	1.55	106.85	2.17	0.16	0.82
28.62	112.40	70.86	1.54	109.20	2.17	0.16	0.82
28.69	115.32	72.59	1.54	111.84	2.17	0.17	0.83
28.75	117.58	73.83	1.55	114.33	2.17	0.17	0.83
28.82	119.37	74.75	1.56	116.66	2.18	0.18	0.83
28.89	120.87	75.50	1.57	118.44	2.18	0.18	0.83
28.95	122.00	76.01	1.58	119.85	2.18	0.18	0.84
29.02	123.04	76.51	1.58	120.75	2.19	0.18	0.84
29.09	123.13	76.35	1.59	121.16	2.19	0.19	0.84
29.16	121.15	74.72	1.63	121.46	2.20	0.18	0.84
29.22	116.07	71.02	1.70	120.42	2.23	0.18	0.83
29.29	109.86	66.60	1.79	119.34	2.26	0.17	0.82
29.35	102.52	61.46	1.93	118.45	2.30	0.16	0.82
29.42	94.81	56.11	2.11	118.49	2.35	0.15	0.81
29.49	85.21	49.47	2.46	121.91	2.42	0.14	0.80
29.55	74.39	42.15	3.03	127.89	2.51	0.13	0.78
29.62	61.12	33.46	4.07	136.30	2.64	0.12	0.62
29.69	48.51	25.56	5.47	139.75	2.77	0.11	0.62
29.76	39.38	20.42	7.00	142.96	2.89	0.10	0.62
29.82	32.61	16.70	8.57	143.15	2.99	0.09	0.62
29.86	29.50	14.99	9.47	141.98	3.04	0.09	1.07
29.92	24.42	12.21	11.23	137.06	3.13	0.09	0.87
30.00	19.52	9.54	13.76	131.18	3.24	0.08	0.68
30.06	20.27	9.92	12.46	123.59	3.19	0.08	0.71
30.13	18.86	9.14	12.90	117.85	3.21	0.08	0.65
30.20	18.30	8.81	12.70	111.94	3.20	0.08	0.63
30.27	18.11	8.69	12.29	106.81	3.18	0.08	0.62
30.34	18.01	8.62	11.78	101.54	3.16	0.08	0.62
30.40	17.35	8.25	11.94	98.49	3.16	0.08	0.59
30.47	17.17	8.13	11.87	96.54	3.16	0.08	0.58
30.54	17.26	8.16	11.68	95.32	3.15	0.08	0.58
30.61	17.54	8.29	11.33	93.93	3.14	0.08	0.59
30.67	17.65	8.33	11.20	93.30	3.13	0.08	0.59
30.74	17.65	8.31	11.21	93.17	3.13	0.08	0.59
30.81	17.83	8.39	11.09	92.99	3.12	0.08	0.60
30.87	18.49	8.71	10.76	93.77	3.11	0.08	0.62
30.91	18.78	8.86	10.69	94.69	3.10	0.08	0.63
30.97	19.43	9.18	10.64	97.65	3.10	0.08	0.66
31.04	19.72	9.31	10.98	102.22	3.12	0.08	0.66
31.11	20.19	9.53	11.15	106.33	3.13	0.08	0.68
31.17	20.56	9.70	11.33	109.92	3.14	0.08	0.69
31.24	21.41	10.12	11.08	112.14	3.12	0.08	0.72
31.31	21.32	10.05	11.42	114.80	3.14	0.08	0.72
31.38	21.03	9.88	11.88	117.37	3.16	0.08	0.71
31.44	20.75	9.71	12.39	120.36	3.18	0.08	0.69
31.51	20.28	9.45	12.87	121.67	3.21	0.08	0.68

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
31.57	20.00	9.29	12.95	120.26	3.21	0.08	0.66
31.64	20.19	9.36	12.74	119.30	3.20	0.08	0.67
31.71	20.19	9.34	12.76	119.20	3.20	0.08	0.67
31.77	19.90	9.17	12.83	117.71	3.20	0.08	0.66
31.84	20.56	9.49	12.70	120.55	3.20	0.08	0.68
31.91	21.79	10.10	12.05	121.61	3.17	0.08	0.72
31.97	22.54	10.46	11.43	119.49	3.14	0.08	0.75
32.04	24.14	11.24	10.53	118.34	3.10	0.08	0.80
32.11	24.23	11.26	10.49	118.21	3.09	0.09	0.80
32.18	23.48	10.86	11.01	119.51	3.12	0.08	0.78
32.24	23.95	11.07	10.99	121.74	3.12	0.08	0.79
32.31	23.95	11.05	11.24	124.17	3.13	0.08	0.79
32.36	23.95	11.03	11.36	125.35	3.14	0.08	0.79
32.43	23.01	10.54	12.02	126.68	3.17	0.08	0.75
32.49	22.63	10.32	12.44	128.37	3.19	0.08	0.74
32.56	23.20	10.59	12.06	127.68	3.17	0.08	0.76
32.62	23.20	10.56	11.91	125.78	3.16	0.08	0.75
32.70	23.48	10.68	11.69	124.80	3.15	0.08	0.76
32.75	24.23	11.03	11.29	124.54	3.13	0.08	0.79
32.83	24.99	11.38	10.93	124.32	3.12	0.09	0.81
32.88	24.90	11.31	11.02	124.70	3.12	0.09	0.81
32.96	25.56	11.61	10.86	126.10	3.11	0.09	0.83
33.01	26.03	11.82	10.76	127.20	3.11	0.09	0.84
33.08	26.31	11.93	10.89	129.97	3.11	0.09	0.85
33.16	27.82	12.64	10.53	133.15	3.10	0.09	0.90
33.22	29.23	13.31	10.08	134.23	3.07	0.09	0.95
33.29	31.58	14.43	9.20	132.68	3.02	0.09	1.03
33.34	32.15	14.68	9.00	132.09	3.01	0.09	1.05
33.40	32.43	14.79	8.96	132.46	3.01	0.09	1.06
33.47	33.37	15.22	8.70	132.39	3.00	0.09	0.62
33.56	34.03	15.49	8.40	130.11	2.98	0.09	0.62
33.62	32.81	14.87	8.71	129.53	3.00	0.09	0.62
33.68	29.51	13.25	9.86	130.64	3.06	0.09	0.95
33.73	26.22	11.64	11.24	130.88	3.13	0.09	0.83
33.82	21.70	9.44	13.80	130.17	3.25	0.08	0.67
33.89	20.48	8.83	14.38	126.94	3.27	0.08	0.63
33.95	20.76	8.95	13.57	121.44	3.24	0.08	0.64
34.02	20.67	8.88	12.95	115.07	3.21	0.08	0.63
34.09	19.91	8.50	13.11	111.45	3.22	0.08	0.61
34.15	19.26	8.18	13.52	110.54	3.23	0.08	0.58
34.22	18.69	7.89	13.98	110.27	3.25	0.08	0.56
34.25	18.41	7.75	14.22	110.12	3.26	0.08	0.55
34.32	18.03	7.55	14.52	109.61	3.27	0.08	0.54
34.39	18.13	7.58	14.32	108.57	3.27	0.08	0.54
34.45	18.22	7.61	14.05	106.91	3.26	0.08	0.54
34.52	18.60	7.77	13.61	105.72	3.24	0.08	0.56
34.59	18.60	7.75	13.62	105.61	3.24	0.08	0.55
34.65	18.60	7.74	13.64	105.52	3.24	0.08	0.55

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
34.72	18.60	7.72	13.67	105.60	3.24	0.08	0.55
34.79	18.60	7.71	13.71	105.67	3.24	0.08	0.55
34.85	18.88	7.82	12.65	98.95	3.20	0.08	0.56
34.92	19.44	8.07	9.73	78.50	3.05	0.08	0.58
34.99	19.82	8.23	10.42	85.78	3.09	0.08	0.59
35.05	20.29	8.43	10.91	92.03	3.12	0.08	0.60
35.13	20.57	8.54	11.47	97.99	3.14	0.08	0.61
35.19	20.29	8.40	12.33	103.51	3.18	0.08	0.60
35.27	23.30	9.77	11.06	108.04	3.12	0.08	0.70
35.34	23.31	9.75	11.57	112.85	3.15	0.08	0.70
35.37	23.31	9.74	11.78	114.74	3.16	0.08	0.70
35.44	23.69	9.90	11.86	117.40	3.16	0.08	0.71
35.51	24.35	10.18	11.62	118.30	3.15	0.08	0.73
35.57	25.19	10.54	11.31	119.29	3.13	0.08	0.75
35.64	26.70	11.21	10.80	121.15	3.11	0.09	0.80
35.70	28.49	12.01	10.19	122.37	3.08	0.09	0.86
35.77	29.24	12.33	10.02	123.50	3.07	0.09	0.88
35.84	29.33	12.34	9.99	123.36	3.07	0.09	0.88
35.90	28.86	12.11	10.10	122.29	3.07	0.09	0.86
35.97	27.74	11.58	10.61	122.84	3.10	0.09	0.83
36.03	27.26	11.34	10.85	123.02	3.11	0.09	0.81
36.10	27.92	11.61	10.52	122.19	3.10	0.09	0.83
36.17	26.98	11.16	10.87	121.32	3.11	0.09	0.80
36.24	27.83	11.52	10.36	119.34	3.09	0.09	0.82
36.30	24.54	10.02	12.27	122.96	3.18	0.08	0.72
36.37	27.74	11.44	10.47	119.81	3.09	0.09	0.82
36.44	35.83	15.04	7.82	117.58	2.94	0.09	0.62
36.51	45.90	19.51	5.85	114.03	2.80	0.10	0.62
36.57	51.73	22.07	5.16	113.88	2.74	0.10	0.62
36.64	52.67	22.45	5.27	118.21	2.75	0.11	0.62
36.71	49.85	21.15	5.93	125.32	2.81	0.10	0.62
36.77	45.61	19.23	6.75	129.87	2.87	0.10	0.62
36.84	40.06	16.73	7.90	132.20	2.95	0.10	0.62
36.91	33.76	13.92	9.52	132.46	3.04	0.09	0.99
36.98	27.83	11.28	11.61	130.91	3.15	0.09	0.81
37.01	25.57	10.27	12.55	128.86	3.19	0.08	0.73
37.08	21.81	8.59	14.37	123.50	3.27	0.08	0.61
37.15	19.36	7.50	15.80	118.50	3.32	0.08	0.54
37.21	17.85	6.83	16.72	114.10	3.36	0.08	0.49
37.28	16.73	6.32	17.18	108.63	3.37	0.08	0.45
37.34	16.44	6.18	16.88	104.38	3.36	0.08	0.44
37.41	17.10	6.46	15.88	102.57	3.33	0.08	0.46
37.48	18.33	6.98	14.61	101.98	3.28	0.08	0.50
37.55	19.74	7.58	13.52	102.50	3.23	0.08	0.54
37.61	20.58	7.93	12.45	98.70	3.19	0.08	0.57
37.68	20.77	8.00	9.83	78.65	3.06	0.08	0.57
37.75	20.21	7.74	10.98	85.00	3.12	0.08	0.55
37.81	19.92	7.60	12.03	91.42	3.17	0.08	0.54

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
37.88	20.30	7.75	13.04	101.05	3.21	0.08	0.55
37.95	21.06	8.06	13.79	111.15	3.25	0.08	0.58
38.02	25.58	9.99	11.71	116.92	3.15	0.08	0.71
38.08	28.22	11.10	11.07	122.85	3.12	0.09	0.79
38.15	31.32	12.41	10.38	128.79	3.09	0.09	0.89
38.21	35.08	13.99	9.58	134.09	3.05	0.09	1.00
38.28	39.79	15.97	8.62	137.65	2.99	0.10	0.62
38.35	43.18	17.39	8.04	139.75	2.95	0.10	0.62
38.41	46.28	18.67	7.54	140.88	2.92	0.10	0.62
38.48	49.39	19.96	7.17	143.09	2.90	0.10	0.62
38.55	50.80	20.52	7.05	144.59	2.89	0.11	0.62
38.58	50.70	20.45	7.07	144.60	2.89	0.11	0.62
38.65	49.49	19.90	7.22	143.79	2.90	0.10	0.62
38.72	46.39	18.56	7.75	143.87	2.94	0.10	0.62
38.78	40.74	16.14	8.97	144.75	3.01	0.10	1.15
38.85	34.53	13.51	10.59	143.04	3.10	0.09	0.96
38.92	29.17	11.23	12.27	137.81	3.18	0.09	0.80
38.98	25.87	9.83	13.38	131.51	3.23	0.08	0.70
39.05	24.09	9.07	13.89	126.00	3.25	0.08	0.65
39.12	22.39	8.34	14.48	120.77	3.27	0.08	0.60
39.18	21.36	7.90	14.69	115.98	3.28	0.08	0.56
39.25	21.73	8.04	13.82	111.04	3.25	0.08	0.57
39.32	22.11	8.18	13.22	108.13	3.22	0.08	0.58
39.38	21.83	8.05	13.42	108.00	3.23	0.08	0.57
39.45	21.17	7.76	14.03	108.92	3.25	0.08	0.55
39.52	20.42	7.44	15.05	111.96	3.29	0.08	0.53
39.58	20.42	7.42	15.47	114.82	3.31	0.08	0.53
39.65	22.58	8.30	13.70	113.74	3.24	0.08	0.59
39.72	26.81	10.02	11.09	111.21	3.12	0.08	0.72
39.78	30.86	11.67	9.82	114.59	3.06	0.09	0.83
39.85	33.31	12.65	9.72	123.03	3.05	0.09	0.90
39.92	34.44	13.09	10.05	131.57	3.07	0.09	0.94
39.97	33.97	12.88	10.68	137.58	3.10	0.09	0.92
40.04	45.83	17.69	7.65	135.42	2.93	0.10	0.62
40.09	45.74	17.63	7.88	138.85	2.94	0.10	0.62
40.17	42.91	16.44	8.77	144.16	3.00	0.10	0.62
40.23	41.31	15.77	9.29	146.47	3.03	0.10	1.13
40.31	41.31	15.73	9.15	143.92	3.02	0.10	1.12
40.37	40.19	15.26	9.20	140.30	3.02	0.10	1.09
40.44	38.77	14.65	9.33	136.77	3.03	0.09	1.05
40.51	36.99	13.91	9.68	134.69	3.05	0.09	0.99
40.57	35.20	13.17	10.19	134.15	3.08	0.09	0.94
40.64	34.54	12.88	10.43	134.32	3.09	0.09	0.92
40.71	34.55	12.86	10.44	134.17	3.09	0.09	0.92
40.77	34.17	12.68	10.57	133.98	3.10	0.09	0.91
40.84	33.89	12.55	10.68	134.04	3.10	0.09	0.90
40.91	33.99	12.56	10.76	135.25	3.11	0.09	0.90
40.97	37.36	13.89	9.80	136.09	3.06	0.09	0.99

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
41.04	46.03	17.31	8.02	138.74	2.95	0.10	0.62
41.11	56.95	21.62	6.15	132.91	2.82	0.11	0.62
41.17	58.55	22.21	5.60	124.34	2.78	0.11	0.62
41.24	54.31	20.50	6.43	131.74	2.84	0.11	0.62
41.30	49.32	18.49	7.70	142.34	2.93	0.10	0.62
41.37	42.64	15.82	9.44	149.39	3.04	0.10	1.13
41.41	34.75	12.69	12.12	153.80	3.17	0.09	0.91
41.48	46.32	17.22	8.66	149.16	2.99	0.10	0.62
41.54	54.89	20.56	7.24	148.81	2.90	0.11	0.62
41.60	68.34	25.80	5.61	144.86	2.78	0.12	0.62
41.67	83.03	31.89	4.35	138.85	2.67	0.13	0.63
41.74	100.25	40.27	3.27	131.83	2.54	0.15	0.80
41.80	104.18	42.17	3.09	130.45	2.52	0.15	0.81
41.87	108.79	44.60	2.82	125.69	2.48	0.16	0.81
41.94	118.86	49.98	2.39	119.54	2.40	0.17	0.82
42.00	130.06	56.08	2.04	114.62	2.33	0.18	0.83
42.07	138.90	60.94	1.84	112.41	2.28	0.20	0.84
42.14	145.28	64.63	1.71	110.32	2.23	0.20	0.85
42.19	152.71	68.88	1.60	109.95	2.19	0.21	0.85
42.26	151.30	67.97	1.61	109.59	2.20	0.21	0.85
42.34	157.41	71.30	1.55	110.45	2.17	0.22	0.85
42.40	154.12	69.25	1.59	110.17	2.19	0.22	0.85
42.46	152.99	68.24	1.63	111.38	2.21	0.22	0.85
42.53	150.26	66.40	1.69	112.16	2.23	0.21	0.85
42.60	147.81	64.88	1.73	112.23	2.24	0.21	0.85
42.67	142.83	62.06	1.80	111.90	2.27	0.20	0.84
42.73	136.33	58.38	1.93	112.47	2.30	0.19	0.84
42.80	128.15	53.80	2.13	114.47	2.35	0.18	0.83
42.87	118.46	48.58	2.41	117.12	2.41	0.17	0.82
42.94	106.98	42.57	2.84	121.04	2.48	0.15	0.81
43.00	97.28	37.78	3.25	122.94	2.54	0.14	0.80
43.07	91.83	35.34	3.38	119.39	2.55	0.14	0.79
43.14	90.13	34.47	3.47	119.55	2.57	0.14	0.79
43.20	90.13	34.41	3.47	119.41	2.57	0.13	0.79
43.27	89.66	34.10	3.51	119.71	2.57	0.13	0.79
43.34	89.85	34.09	3.52	120.14	2.57	0.13	0.79
43.39	90.80	34.46	3.49	120.35	2.57	0.14	0.79
43.47	90.41	34.17	3.54	121.04	2.57	0.14	0.79
43.54	84.96	31.56	3.87	122.24	2.61	0.13	0.63
43.60	78.46	28.52	4.31	122.97	2.66	0.12	0.62
43.67	71.59	25.68	4.79	122.92	2.71	0.12	0.62
43.73	64.16	22.88	5.35	122.33	2.76	0.11	0.62
43.80	57.57	20.39	5.96	121.54	2.81	0.11	0.62
43.83	54.66	19.29	6.26	120.87	2.83	0.10	0.62
43.90	49.86	17.48	6.74	117.88	2.87	0.10	0.62
43.97	45.81	15.96	7.19	114.68	2.90	0.10	0.62
44.03	41.67	14.40	7.91	113.91	2.95	0.10	0.62
44.10	38.38	13.16	8.51	112.06	2.98	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
44.17	36.21	12.34	8.88	109.58	3.01	0.09	0.88
44.23	33.39	11.29	9.82	110.82	3.06	0.09	0.81
44.30	29.92	9.99	11.40	113.85	3.14	0.09	0.71
44.37	27.94	9.25	12.39	114.61	3.18	0.08	0.66
44.44	28.51	9.44	11.87	112.03	3.16	0.08	0.67
44.50	31.90	10.67	10.53	112.29	3.10	0.09	0.76
44.57	35.94	12.13	9.51	115.27	3.04	0.09	0.87
44.64	36.98	12.48	9.39	117.28	3.03	0.09	0.89
44.70	36.41	12.26	9.66	118.46	3.05	0.09	0.88
44.77	39.23	13.26	9.12	120.95	3.02	0.09	0.95
44.84	52.13	17.93	6.56	117.61	2.85	0.10	0.62
44.90	73.02	25.66	4.24	108.78	2.65	0.12	0.62
44.97	89.01	33.00	3.13	103.22	2.52	0.13	0.78
45.04	96.63	36.60	2.74	100.46	2.46	0.14	0.79
45.11	99.93	38.16	2.59	98.98	2.44	0.14	0.79
45.17	103.22	39.79	2.45	97.64	2.41	0.14	0.80
45.24	106.13	41.16	2.36	96.96	2.40	0.14	0.80
45.31	108.67	42.38	2.27	96.00	2.38	0.14	0.80
45.37	110.46	43.24	2.20	95.18	2.37	0.15	0.80
45.44	112.25	43.94	2.19	96.03	2.36	0.15	0.81
45.48	113.28	44.30	2.19	97.09	2.36	0.15	0.81
45.54	115.26	45.00	2.20	98.87	2.36	0.15	0.81
45.61	116.67	45.44	2.21	100.47	2.37	0.16	0.81
45.69	115.44	44.56	2.30	102.42	2.39	0.15	0.81
45.76	119.02	46.23	2.21	102.00	2.37	0.16	0.82
45.83	119.02	46.17	2.20	101.73	2.37	0.16	0.82
45.89	117.99	45.63	2.22	101.24	2.37	0.16	0.81
45.96	117.99	45.57	2.22	100.98	2.37	0.16	0.81
46.03	117.99	45.46	2.23	101.18	2.37	0.16	0.81
46.09	117.99	45.34	2.24	101.61	2.37	0.16	0.81
46.16	118.27	45.36	2.25	101.85	2.37	0.16	0.81
46.23	118.64	45.39	2.26	102.51	2.38	0.16	0.81
46.29	119.11	45.53	2.25	102.51	2.38	0.16	0.82
46.36	119.21	45.50	2.25	102.38	2.38	0.16	0.82
46.42	119.68	45.67	2.24	102.07	2.37	0.16	0.82
46.46	119.77	45.68	2.23	101.92	2.37	0.16	0.82
46.53	119.58	45.51	2.24	101.80	2.37	0.16	0.82
46.59	119.21	45.23	2.25	101.99	2.38	0.16	0.81
46.66	118.93	45.00	2.27	102.15	2.38	0.16	0.81
46.73	118.36	44.63	2.29	102.32	2.38	0.16	0.81
46.80	117.89	44.32	2.31	102.35	2.39	0.16	0.81
46.86	117.33	43.96	2.33	102.52	2.39	0.16	0.81
46.93	116.76	43.61	2.35	102.65	2.40	0.16	0.81
46.99	116.29	43.34	2.36	102.21	2.40	0.16	0.81
47.06	115.44	42.92	2.37	101.68	2.40	0.15	0.81
47.13	114.41	42.42	2.38	100.95	2.40	0.15	0.81
47.20	112.25	41.41	2.42	100.30	2.41	0.15	0.81
47.26	110.08	40.39	2.47	99.78	2.42	0.15	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
47.33	106.69	38.71	2.58	99.90	2.44	0.14	0.80
47.40	103.59	37.21	2.70	100.52	2.46	0.14	0.80
47.47	101.42	36.13	2.80	101.22	2.47	0.14	0.79
47.53	99.73	35.27	2.89	101.99	2.49	0.14	0.79
47.60	98.32	34.52	2.98	102.95	2.50	0.14	0.79
47.66	98.32	34.46	2.98	102.85	2.50	0.14	0.79
47.73	98.32	34.48	2.95	101.61	2.50	0.14	0.79
47.80	98.32	34.58	2.87	99.13	2.48	0.14	0.79
47.87	96.91	34.07	2.84	96.78	2.48	0.13	0.79
47.93	93.90	32.72	2.95	96.41	2.50	0.13	0.78
48.00	89.28	30.57	3.21	98.10	2.53	0.13	0.78
48.03	86.46	29.26	3.41	99.64	2.56	0.12	0.78
48.10	79.50	26.37	3.73	98.30	2.60	0.12	0.77
48.17	71.97	23.46	3.98	93.29	2.63	0.11	0.62
48.24	63.88	20.50	4.91	100.59	2.72	0.11	0.62
48.30	56.44	17.97	5.90	106.00	2.80	0.10	0.62
48.37	49.39	15.57	7.00	109.09	2.89	0.10	0.62
48.43	39.70	12.31	9.11	112.09	3.02	0.09	0.88
48.50	40.26	12.48	8.84	110.29	3.00	0.09	0.89
48.56	36.50	11.20	10.06	112.72	3.07	0.09	0.80
48.63	32.26	9.77	11.75	114.79	3.16	0.09	0.70
48.70	32.18	9.73	11.33	110.22	3.14	0.09	0.69
48.76	32.08	9.68	10.71	103.65	3.10	0.09	0.69
48.82	40.83	12.58	7.78	97.87	2.94	0.09	0.62
48.89	53.83	16.88	5.45	92.05	2.77	0.10	0.62
48.95	65.03	20.57	4.18	86.07	2.65	0.11	0.62
49.02	68.79	22.05	3.87	85.31	2.61	0.11	0.62
49.09	66.24	20.91	4.32	90.25	2.66	0.11	0.62
49.15	65.86	20.76	4.60	95.58	2.69	0.11	0.62
49.23	61.25	19.20	5.36	103.01	2.76	0.11	0.62
49.28	55.70	17.35	6.26	108.61	2.83	0.10	0.62
49.35	47.33	14.57	7.75	112.94	2.94	0.10	0.62
49.42	41.30	12.57	8.86	111.40	3.00	0.09	0.90
49.48	37.54	11.32	9.62	108.89	3.05	0.09	0.81
49.55	35.47	10.62	9.99	106.13	3.07	0.09	0.76
49.62	35.20	10.52	9.82	103.33	3.06	0.09	0.75
49.69	35.95	10.75	9.25	99.41	3.03	0.09	0.77
49.75	35.95	10.73	9.19	98.68	3.02	0.09	0.77
49.82	34.26	10.17	9.81	99.75	3.06	0.09	0.73
49.87	33.03	9.76	9.98	97.36	3.07	0.09	0.70
49.94	32.20	9.47	8.69	82.24	2.99	0.09	0.62
50.02	32.10	9.42	7.40	69.76	2.91	0.08	0.62
50.07	33.70	9.93	7.62	75.72	2.93	0.09	0.62
50.16	39.25	11.71	6.94	81.27	2.88	0.09	0.62
50.21	41.04	12.28	7.08	86.93	2.89	0.09	0.62
50.27	43.66	13.11	7.25	95.00	2.90	0.09	0.62
50.33	56.27	17.16	5.76	98.89	2.79	0.10	0.62
50.40	72.00	22.20	4.55	101.04	2.68	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
50.47	100.87	33.46	2.85	95.28	2.48	0.13	0.79
50.53	124.30	43.78	2.12	92.89	2.35	0.16	0.81
50.61	148.09	54.35	1.76	95.81	2.25	0.19	0.84
50.66	156.37	58.03	1.68	97.69	2.23	0.20	0.85
50.73	164.94	62.06	1.59	98.90	2.19	0.22	0.85
50.80	170.38	64.74	1.54	99.40	2.17	0.22	0.86
50.87	172.91	66.05	1.50	99.34	2.15	0.23	0.86
50.92	173.57	66.35	1.50	99.29	2.15	0.23	0.86
51.01	174.23	66.53	1.49	99.34	2.14	0.23	0.86
51.07	170.46	64.53	1.53	98.51	2.16	0.22	0.85
51.13	166.40	62.40	1.57	97.79	2.18	0.22	0.85
51.20	162.26	60.18	1.62	97.46	2.20	0.21	0.85
51.26	158.59	58.05	1.69	98.27	2.23	0.21	0.85
51.32	154.26	55.79	1.77	98.49	2.25	0.20	0.84
51.39	147.86	52.65	1.87	98.52	2.29	0.19	0.84
51.45	141.94	49.30	2.08	102.74	2.34	0.19	0.84
51.52	140.81	48.55	2.14	104.09	2.35	0.19	0.83
51.59	146.07	50.96	2.02	102.74	2.32	0.19	0.84
51.65	143.62	49.66	2.09	103.76	2.34	0.19	0.84
51.71	148.14	51.39	2.05	105.35	2.33	0.20	0.84
51.78	148.42	51.04	2.12	108.36	2.35	0.20	0.84
51.84	145.59	49.57	2.21	109.75	2.37	0.20	0.84
51.92	143.71	48.76	2.23	108.80	2.37	0.19	0.84
51.97	143.70	48.68	2.23	108.76	2.37	0.19	0.84
52.04	143.70	48.61	2.23	108.56	2.37	0.19	0.84
52.10	143.70	48.60	2.22	107.89	2.37	0.19	0.84
52.17	144.64	48.67	2.26	110.11	2.38	0.20	0.84
52.23	156.03	53.56	2.05	109.81	2.33	0.22	0.85
52.30	165.06	57.50	1.91	109.85	2.30	0.24	0.86
52.37	177.39	63.04	1.75	110.29	2.25	0.27	0.87
52.44	189.81	68.60	1.64	112.22	2.21	0.32	0.88
52.50	181.91	64.52	1.75	112.73	2.25	0.29	0.87
52.56	198.75	72.14	1.60	115.42	2.19	0.36	0.89
52.63	198.00	71.61	1.61	115.46	2.20	0.36	0.89
52.69	196.12	70.77	1.62	114.40	2.20	0.35	0.89
52.77	194.23	70.06	1.61	112.70	2.20	0.33	0.88
52.85	195.08	70.65	1.58	111.43	2.18	0.33	0.88
52.92	191.60	69.14	1.59	109.82	2.19	0.31	0.88
52.98	187.93	67.55	1.60	108.38	2.20	0.30	0.88
53.05	183.60	66.45	1.56	103.68	2.18	0.27	0.87
53.09	181.91	65.71	1.57	103.03	2.18	0.26	0.87
53.15	178.61	63.86	1.62	103.37	2.20	0.26	0.87
53.22	175.51	62.21	1.67	103.58	2.22	0.25	0.86
53.29	173.72	61.10	1.71	104.42	2.24	0.25	0.86
53.36	173.58	60.75	1.74	105.59	2.25	0.25	0.86
53.41	173.58	60.57	1.75	106.28	2.25	0.25	0.86
53.48	173.45	60.39	1.76	106.58	2.25	0.25	0.86
53.55	178.34	62.60	1.71	106.83	2.23	0.27	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
53.61	183.32	64.75	1.67	107.82	2.22	0.28	0.87
53.69	190.85	67.90	1.62	110.00	2.20	0.31	0.88
53.74	196.21	70.23	1.59	111.35	2.19	0.33	0.88
53.81	201.67	72.52	1.56	113.11	2.18	0.36	0.89
53.89	208.16	75.28	1.53	115.16	2.16	0.40	0.89
53.95	213.81	77.73	1.50	116.90	2.15	0.44	0.90
54.01	220.68	80.81	1.47	118.98	2.13	0.50	0.90
54.07	227.56	83.96	1.44	121.07	2.12	0.56	0.91
54.15	232.81	86.30	1.42	122.87	2.10	0.62	0.91
54.22	236.48	87.95	1.41	124.08	2.09	0.68	0.92
54.27	239.03	89.08	1.40	124.96	2.09	0.72	0.92
54.35	242.04	90.35	1.40	126.09	2.08	0.77	0.92
54.40	245.05	91.77	1.38	127.07	2.08	0.82	0.92
54.48	247.96	93.13	1.37	128.01	2.07	0.82	0.92
54.53	250.60	94.32	1.37	128.97	2.06	0.82	0.92
54.60	258.22	97.92	1.35	131.95	2.04	0.82	0.93
54.66	264.71	100.83	1.34	134.72	2.03	0.83	0.93
54.73	271.96	104.12	1.32	137.88	2.02	0.83	0.94
54.80	279.02	107.35	1.31	141.00	2.01	0.84	0.94
54.86	285.05	109.97	1.31	143.76	2.00	0.84	0.94
54.93	289.75	111.85	1.31	145.99	2.00	0.84	0.95
55.00	292.95	113.13	1.30	147.45	2.00	0.84	0.95
55.06	294.65	113.64	1.30	148.25	2.00	0.85	0.95
55.13	297.56	114.84	1.30	149.55	1.99	0.85	0.95
55.20	299.54	115.69	1.30	150.37	1.99	0.85	0.95
55.27	300.95	116.28	1.30	150.92	1.99	0.85	0.95
55.34	300.90	116.09	1.30	150.82	1.99	0.85	0.95
55.40	300.90	115.93	1.30	150.76	1.99	0.85	0.95
55.47	300.87	115.75	1.30	150.68	1.99	0.85	0.95
55.53	302.18	116.36	1.30	151.14	1.99	0.85	0.95
55.60	303.78	117.73	1.29	151.48	1.97	0.85	0.95
55.67	304.72	118.86	1.28	151.56	1.96	0.85	0.95
55.73	304.53	118.35	1.28	151.47	1.96	0.85	0.95
55.80	303.49	117.51	1.28	150.97	1.97	0.85	0.95
55.87	302.27	116.65	1.29	150.36	1.98	0.85	0.95
55.93	297.19	113.88	1.30	148.03	1.99	0.85	0.95
55.98	277.24	103.74	1.35	139.64	2.04	0.83	0.94
56.05	288.82	109.45	1.32	144.25	2.01	0.84	0.95
56.10	289.10	109.52	1.32	144.29	2.01	0.84	0.95
56.19	291.65	110.70	1.31	145.24	2.01	0.84	0.95
56.24	291.18	110.36	1.31	145.00	2.01	0.84	0.95
56.31	289.39	109.43	1.32	144.10	2.01	0.84	0.95
56.38	285.72	107.55	1.32	142.43	2.02	0.84	0.95
56.46	284.12	106.84	1.32	141.51	2.02	0.84	0.95
56.52	281.76	105.87	1.32	140.23	2.02	0.84	0.94
56.58	278.18	104.40	1.33	138.35	2.02	0.83	0.94
56.65	273.76	102.40	1.33	136.24	2.03	0.83	0.94
56.71	269.53	100.45	1.34	134.25	2.03	0.83	0.94

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
56.77	265.10	98.50	1.34	132.13	2.04	0.83	0.93
56.83	261.44	96.98	1.34	130.27	2.04	0.82	0.93
56.90	255.42	94.30	1.35	127.50	2.05	0.82	0.92
56.96	248.16	91.05	1.37	124.29	2.06	0.79	0.92
57.03	239.41	87.01	1.39	120.74	2.08	0.65	0.91
57.10	232.35	83.69	1.41	118.15	2.10	0.56	0.91
57.16	228.68	81.90	1.43	116.89	2.11	0.53	0.91
57.23	229.73	83.64	1.37	114.99	2.07	0.48	0.90
57.30	235.74	89.15	1.29	115.22	1.98	0.41	0.89
57.37	243.93	92.62	1.29	119.06	1.97	0.47	0.89
57.43	250.99	95.40	1.28	122.44	1.97	0.55	0.90
57.50	254.37	96.26	1.29	124.17	1.98	0.64	0.90
57.57	255.22	95.92	1.30	124.76	1.99	0.70	0.91
57.62	219.84	78.16	1.43	112.07	2.11	0.43	0.90
57.68	244.68	90.01	1.34	120.63	2.04	0.64	0.91
57.76	243.37	89.44	1.34	119.88	2.04	0.61	0.91
57.82	240.36	87.91	1.35	118.65	2.05	0.58	0.91
57.88	237.45	86.42	1.36	117.50	2.05	0.56	0.91
57.94	233.95	84.67	1.37	116.16	2.06	0.52	0.90
58.01	231.13	83.27	1.38	115.08	2.07	0.50	0.90
58.08	227.08	81.25	1.40	113.67	2.09	0.47	0.90
58.14	223.98	79.78	1.41	112.52	2.09	0.45	0.90
58.21	221.06	78.43	1.42	111.38	2.10	0.43	0.90
58.28	221.07	78.30	1.42	111.45	2.10	0.43	0.90
58.35	221.07	78.09	1.43	111.65	2.11	0.43	0.90
58.40	221.07	77.98	1.43	111.73	2.11	0.44	0.90
58.47	223.88	79.22	1.42	112.55	2.10	0.45	0.90
58.54	226.24	80.12	1.42	113.47	2.10	0.48	0.90
58.61	226.43	79.99	1.42	113.73	2.10	0.48	0.90
58.67	225.59	79.51	1.43	113.49	2.11	0.48	0.90
58.74	222.66	78.23	1.43	112.25	2.11	0.45	0.90
58.82	222.67	78.32	1.43	111.84	2.11	0.45	0.90
58.88	224.54	79.17	1.42	112.28	2.10	0.46	0.90
58.95	228.60	86.86	1.26	109.33	1.93	0.29	0.86
59.02	236.40	94.37	1.18	111.11	1.82	0.23	0.81
59.09	247.31	99.60	1.16	115.31	1.80	0.26	0.82
59.12	252.59	101.72	1.16	117.80	1.80	0.28	0.83
59.19	260.49	104.53	1.17	121.88	1.81	0.33	0.84
59.26	264.07	105.23	1.18	124.21	1.83	0.36	0.85
59.32	261.99	103.12	1.20	124.01	1.85	0.39	0.86
59.40	259.92	100.95	1.22	123.50	1.88	0.42	0.87
59.46	267.44	104.07	1.22	126.98	1.88	0.49	0.87
59.52	271.50	105.18	1.23	129.01	1.88	0.57	0.88
59.60	274.79	105.19	1.24	130.79	1.91	0.75	0.90
59.66	276.86	105.44	1.25	131.81	1.92	0.83	0.90
59.73	277.33	105.71	1.25	131.93	1.92	0.84	0.90
59.78	279.58	106.88	1.24	132.87	1.91	0.84	0.90
59.85	285.60	109.87	1.23	135.52	1.89	0.84	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
59.93	291.92	113.01	1.22	138.23	1.88	0.84	0.90
59.99	295.95	114.34	1.23	140.14	1.88	0.85	0.91
60.04	285.99	108.81	1.25	135.67	1.92	0.84	0.91
60.11	287.67	109.25	1.25	136.41	1.92	0.84	0.91
60.18	285.98	108.09	1.25	135.60	1.93	0.84	0.92
60.24	285.60	107.64	1.26	135.38	1.93	0.84	0.92
60.30	284.00	106.22	1.27	134.66	1.95	0.84	0.92
60.37	284.10	105.97	1.27	134.67	1.95	0.84	0.92
60.44	284.19	105.88	1.27	134.63	1.95	0.84	0.92
60.50	282.31	104.88	1.27	133.70	1.96	0.83	0.92
60.58	290.50	108.90	1.26	137.32	1.94	0.84	0.92
60.63	293.51	110.36	1.26	138.62	1.93	0.84	0.92
60.70	299.06	113.14	1.25	141.04	1.91	0.84	0.92
60.78	305.18	116.31	1.24	143.68	1.90	0.85	0.92
60.83	309.13	118.32	1.23	145.36	1.89	0.85	0.92
60.89	315.82	121.83	1.22	148.13	1.87	0.86	0.92
60.97	326.44	127.72	1.19	152.09	1.84	0.86	0.91
61.03	332.85	131.59	1.17	153.81	1.81	0.87	0.91
61.10	337.64	134.82	1.14	154.23	1.79	0.87	0.91
61.16	342.35	138.37	1.11	153.28	1.76	0.87	0.91
61.22	344.99	141.24	1.06	149.73	1.74	0.88	0.91
61.30	345.74	143.01	1.01	144.81	1.71	0.88	0.92
61.36	343.67	142.61	1.00	142.61	1.70	0.88	0.91
61.42	341.04	143.71	1.00	143.71	1.67	0.88	0.91
61.48	337.45	150.16	1.00	150.16	1.55	0.89	0.91
61.57	335.48	148.23	1.00	148.23	1.56	0.88	0.91
61.64	331.99	145.43	1.00	145.43	1.58	0.88	0.90
61.70	328.23	142.38	1.00	142.38	1.60	0.88	0.90
61.76	307.81	130.25	1.00	130.25	1.65	0.86	0.88
61.82	300.47	125.96	1.00	125.96	1.67	0.69	0.87
61.88	305.47	128.69	1.00	128.69	1.66	0.80	0.88
61.96	298.97	124.65	1.00	124.65	1.68	0.64	0.87
62.03	286.64	116.60	1.05	122.24	1.73	0.47	0.86
62.08	276.01	110.28	1.11	122.40	1.77	0.38	0.84
62.15	257.56	99.96	1.18	117.90	1.83	0.31	0.84
62.22	238.66	89.34	1.24	110.48	1.90	0.29	0.85
62.29	218.88	78.58	1.30	101.79	1.99	0.28	0.86
62.36	200.73	69.16	1.38	95.21	2.07	0.26	0.86
62.41	191.13	64.25	1.45	93.01	2.12	0.24	0.86
62.48	202.09	68.49	1.42	97.39	2.10	0.28	0.87
62.55	191.88	63.19	1.52	96.30	2.16	0.27	0.87
62.62	203.46	68.38	1.45	98.86	2.12	0.30	0.88
62.69	216.36	74.82	1.36	101.96	2.06	0.32	0.88
62.73	224.63	79.16	1.32	104.64	2.02	0.34	0.88
62.80	231.88	83.21	1.29	107.32	1.98	0.34	0.88
62.87	237.61	86.14	1.27	109.71	1.96	0.35	0.87
62.95	247.50	90.51	1.26	114.14	1.94	0.39	0.88
63.02	262.18	100.94	1.18	119.17	1.83	0.33	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
63.06	273.10	109.90	1.05	115.78	1.73	0.35	0.84
63.13	290.22	118.82	1.00	118.82	1.70	0.50	0.86
63.20	310.08	130.11	1.00	130.11	1.64	0.86	0.88
63.26	322.31	137.36	1.00	137.36	1.61	0.87	0.89
63.34	335.58	145.48	1.00	145.48	1.57	0.88	0.90
63.39	336.62	146.38	1.00	146.38	1.57	0.88	0.90
63.45	337.65	147.17	1.00	147.17	1.56	0.88	0.91
63.52	343.67	150.66	1.00	150.66	1.55	0.89	0.91
63.59	343.57	150.52	1.00	150.52	1.55	0.89	0.91
63.66	339.62	147.72	1.00	147.72	1.56	0.88	0.91
63.72	337.17	145.63	1.00	145.63	1.58	0.88	0.91
63.79	333.41	142.84	1.00	142.84	1.59	0.88	0.90
63.86	324.94	137.64	1.00	137.64	1.61	0.87	0.89
63.91	318.74	133.65	1.00	133.65	1.63	0.87	0.89
63.98	305.93	125.99	1.00	125.99	1.67	0.76	0.87
64.05	298.13	121.60	1.00	121.60	1.69	0.59	0.86
64.12	292.94	118.42	1.00	118.42	1.71	0.52	0.86
64.18	288.63	115.42	1.05	120.61	1.73	0.47	0.85
64.25	278.26	108.27	1.13	122.73	1.78	0.39	0.84
64.31	265.47	99.45	1.21	120.32	1.86	0.40	0.86
64.38	252.76	91.68	1.25	115.05	1.93	0.41	0.88
64.45	239.50	84.96	1.28	109.17	1.97	0.38	0.88
64.50	225.48	78.28	1.32	103.24	2.01	0.33	0.88
64.58	206.56	69.51	1.38	96.20	2.07	0.28	0.87
64.64	191.60	62.38	1.48	92.62	2.14	0.25	0.86
64.72	180.59	57.62	1.56	90.05	2.18	0.23	0.86
64.77	190.75	62.39	1.46	91.24	2.13	0.24	0.86
64.83	184.17	59.61	1.50	89.22	2.15	0.23	0.86
64.91	189.92	62.30	1.45	90.11	2.12	0.23	0.86
64.97	197.07	65.64	1.40	91.84	2.09	0.25	0.86
65.04	208.73	71.97	1.32	94.96	2.01	0.25	0.86
65.10	216.07	78.89	1.23	97.22	1.89	0.20	0.82
65.17	220.39	82.73	1.19	98.21	1.83	0.18	0.79
65.24	229.71	88.62	1.00	88.62	1.78	0.18	0.79
65.31	240.45	96.11	1.00	96.11	1.70	0.20	0.80
65.36	237.35	96.35	1.00	96.35	1.67	0.19	0.80
65.42	230.38	94.46	1.00	94.46	1.65	0.18	0.79
65.49	243.74	103.29	1.00	103.29	1.58	0.21	0.80
65.55	244.39	103.77	1.00	103.77	1.58	0.21	0.81
65.62	239.21	101.27	1.00	101.27	1.58	0.20	0.80
65.69	231.40	97.24	1.00	97.24	1.59	0.18	0.79
65.76	221.99	91.80	1.00	91.80	1.62	0.16	0.78
65.83	211.37	85.75	1.00	85.75	1.66	0.15	0.77
65.89	204.02	81.43	1.00	81.43	1.69	0.14	0.76
65.95	194.33	76.24	1.00	76.24	1.72	0.12	0.74
66.03	178.52	68.04	1.00	68.04	1.78	0.11	0.72
66.08	167.70	62.52	1.00	62.52	1.82	0.10	0.72
66.16	152.64	54.70	1.00	54.70	1.90	0.11	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
66.22	142.95	49.73	1.00	49.73	1.95	0.11	0.76
66.29	132.88	44.90	1.00	44.90	2.01	0.11	0.76
66.36	125.83	41.65	1.00	41.65	2.05	0.11	0.77
66.42	117.64	37.93	1.00	37.93	2.10	0.11	0.76
66.49	109.63	34.38	1.50	51.61	2.15	0.11	0.76
66.55	102.87	31.38	1.61	50.65	2.20	0.10	0.76
66.62	97.68	28.71	1.82	52.36	2.27	0.11	0.76
66.69	94.95	27.83	1.83	50.94	2.27	0.10	0.76
66.75	93.35	27.67	1.75	48.29	2.25	0.10	0.75
66.82	92.42	26.74	1.91	51.01	2.30	0.10	0.76
66.89	89.59	24.89	2.25	56.05	2.38	0.11	0.76
66.96	85.17	22.37	2.88	64.42	2.49	0.11	0.76
67.00	74.54	18.81	3.87	72.87	2.61	0.11	0.62
67.08	85.40	21.69	3.44	74.73	2.56	0.11	0.76
67.14	82.07	20.79	3.67	76.35	2.59	0.11	0.76
67.21	85.64	21.73	3.70	80.36	2.59	0.12	0.76
67.28	90.07	22.90	3.88	88.80	2.61	0.12	0.62
67.34	101.27	26.04	3.25	84.58	2.54	0.13	0.78
67.41	121.21	33.57	2.35	78.88	2.40	0.14	0.80
67.47	152.46	46.47	1.65	76.56	2.21	0.17	0.83
67.54	180.12	58.81	1.39	81.62	2.08	0.19	0.84
67.61	201.58	68.84	1.30	89.34	1.99	0.21	0.84
67.67	227.55	81.63	1.23	100.41	1.89	0.22	0.83
67.74	243.91	90.67	1.17	106.19	1.82	0.22	0.81
67.80	254.63	98.20	1.07	105.03	1.74	0.24	0.81
67.87	264.04	103.71	1.00	103.71	1.70	0.27	0.83
67.94	270.90	106.43	1.00	106.43	1.70	0.31	0.83
68.00	277.21	110.06	1.00	110.06	1.68	0.34	0.84
68.07	281.26	111.46	1.00	111.46	1.68	0.37	0.84
68.14	284.55	111.43	1.00	111.78	1.71	0.40	0.85
68.20	286.63	113.26	1.00	113.26	1.69	0.41	0.85
68.27	289.36	115.59	1.00	115.59	1.66	0.44	0.85
68.34	291.15	115.92	1.00	115.92	1.67	0.45	0.85
68.41	295.19	117.10	1.00	117.10	1.68	0.50	0.86
68.44	296.79	117.44	1.00	117.44	1.68	0.52	0.86
68.51	297.03	116.76	1.00	116.76	1.70	0.52	0.86
68.58	297.26	116.67	1.00	116.67	1.70	0.52	0.86
68.65	305.07	121.10	1.00	121.10	1.67	0.66	0.87
68.73	308.27	122.82	1.00	122.82	1.66	0.72	0.87
68.78	309.97	123.70	1.00	123.70	1.66	0.75	0.87
68.83	310.62	123.94	1.00	123.94	1.66	0.77	0.87
68.92	315.52	126.02	1.00	126.02	1.66	0.86	0.88
68.97	319.56	127.73	1.00	127.73	1.66	0.86	0.88
69.03	321.63	128.29	1.00	128.29	1.66	0.86	0.89
69.09	323.33	129.03	1.00	129.03	1.66	0.86	0.89
69.18	326.71	130.06	1.00	130.06	1.66	0.86	0.89
69.24	331.33	132.06	1.00	132.06	1.66	0.87	0.89
69.29	336.41	134.48	1.00	134.48	1.65	0.87	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
69.37	344.31	138.62	1.00	138.62	1.64	0.87	0.91
69.43	348.73	141.01	1.00	141.01	1.63	0.88	0.91
69.51	354.76	143.99	1.00	143.99	1.62	0.88	0.92
69.57	356.65	146.09	1.00	146.09	1.60	0.88	0.92
69.63	356.92	151.16	1.00	151.16	1.53	0.89	0.92
69.69	354.94	151.17	1.00	151.17	1.52	0.89	0.92
69.76	352.97	149.99	1.00	149.99	1.52	0.89	0.92
69.82	354.20	150.08	1.00	150.08	1.53	0.89	0.92
69.91	348.37	144.32	1.00	144.32	1.57	0.88	0.91
69.95	234.12	83.20	1.22	101.15	1.87	0.22	0.82
70.02	320.69	127.69	1.00	127.69	1.65	0.86	0.88
70.08	315.41	124.77	1.00	124.77	1.66	0.86	0.88
70.16	315.79	125.57	1.00	125.57	1.65	0.86	0.88
70.22	305.34	120.04	1.00	120.04	1.67	0.63	0.87
70.28	299.52	116.80	1.00	116.80	1.68	0.54	0.86
70.35	297.92	116.33	1.00	116.33	1.68	0.51	0.86
70.42	298.39	117.31	1.00	117.31	1.66	0.51	0.86
70.48	297.92	117.59	1.00	117.59	1.65	0.51	0.86
70.55	298.49	118.24	1.00	118.24	1.65	0.51	0.86
70.61	299.24	118.90	1.00	118.90	1.64	0.52	0.86
70.69	301.31	120.26	1.00	120.26	1.63	0.56	0.86
70.75	303.10	121.76	1.00	121.76	1.61	0.59	0.86
70.82	302.99	122.70	1.00	122.70	1.60	0.59	0.86
70.88	299.13	120.98	1.00	120.98	1.60	0.52	0.86
70.95	295.75	119.02	1.00	119.02	1.61	0.48	0.86
71.02	290.67	115.54	1.00	115.54	1.63	0.42	0.85
71.08	284.08	112.23	1.00	112.23	1.64	0.37	0.84
71.15	281.81	113.00	1.00	113.00	1.61	0.35	0.84
71.22	279.28	116.41	1.00	116.41	1.53	0.34	0.84
71.28	276.83	115.19	1.00	115.19	1.54	0.32	0.84
71.35	276.17	113.85	1.00	113.85	1.55	0.32	0.83
71.42	276.46	112.74	1.00	112.74	1.58	0.32	0.84
71.49	280.22	114.07	1.00	114.07	1.58	0.34	0.84
71.54	276.32	111.09	1.00	111.09	1.60	0.32	0.83
71.59	272.41	108.30	1.00	108.30	1.62	0.30	0.83
71.67	283.98	114.07	1.00	114.07	1.60	0.37	0.84
71.73	290.95	117.15	1.00	117.15	1.60	0.42	0.85
71.79	293.96	117.84	1.00	117.84	1.61	0.45	0.85
71.86	294.34	117.22	1.00	117.22	1.62	0.45	0.85
71.92	292.45	115.57	1.00	115.57	1.63	0.43	0.85
71.99	286.71	112.26	1.00	112.26	1.65	0.38	0.85
72.06	277.21	107.24	1.00	107.24	1.67	0.32	0.84
72.12	272.03	104.40	1.00	104.40	1.68	0.29	0.83
72.19	265.26	100.78	1.00	100.78	1.70	0.26	0.82
72.26	260.37	97.45	1.00	97.45	1.73	0.24	0.82
72.31	256.41	93.41	1.13	105.86	1.78	0.24	0.81
72.38	253.40	90.10	1.18	106.73	1.83	0.25	0.82
72.46	252.18	89.72	1.18	106.04	1.83	0.25	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
72.52	253.97	94.64	1.00	94.64	1.73	0.22	0.81
72.59	262.15	102.28	1.00	102.28	1.65	0.25	0.82
72.65	268.46	102.90	1.00	102.90	1.68	0.27	0.83
72.71	278.24	102.26	1.10	112.88	1.76	0.33	0.84
72.78	282.58	99.93	1.19	119.11	1.84	0.44	0.86
72.84	280.04	98.37	1.20	118.25	1.85	0.44	0.86
72.90	282.86	102.68	1.13	116.52	1.78	0.37	0.84
72.98	283.14	104.34	1.09	113.70	1.75	0.36	0.84
73.03	295.38	110.70	1.03	113.89	1.72	0.45	0.85
73.11	298.67	111.05	1.06	117.50	1.73	0.49	0.86
73.17	295.67	107.47	1.13	121.18	1.78	0.48	0.85
73.23	303.30	111.02	1.11	122.96	1.76	0.57	0.86
73.30	301.42	109.29	1.13	123.72	1.78	0.56	0.86
73.36	302.37	107.87	1.17	126.02	1.81	0.64	0.87
73.44	314.97	113.40	1.15	130.20	1.80	0.85	0.88
73.51	320.81	116.43	1.13	131.27	1.78	0.85	0.88
73.56	315.02	114.56	1.12	128.32	1.77	0.81	0.87
73.63	315.07	117.75	1.02	120.63	1.72	0.77	0.87
73.70	327.49	124.20	1.00	124.20	1.69	0.86	0.89
73.76	332.76	126.09	1.00	126.09	1.69	0.86	0.89
73.83	330.98	125.54	1.00	125.54	1.69	0.86	0.89
73.89	316.68	117.26	1.05	123.50	1.73	0.81	0.88
73.95	324.04	120.37	1.04	125.22	1.73	0.85	0.88
74.02	337.20	128.93	1.00	128.93	1.67	0.86	0.90
74.09	336.63	131.71	1.00	131.71	1.62	0.87	0.90
74.16	326.64	133.77	1.00	133.77	1.53	0.87	0.89
74.24	330.59	138.53	1.00	138.53	1.48	0.87	0.89
74.31	321.00	131.76	1.00	131.76	1.52	0.87	0.88
74.38	307.35	123.58	1.00	123.58	1.56	0.60	0.87
74.41	301.44	120.63	1.00	120.63	1.57	0.52	0.86
74.48	290.99	115.58	1.00	115.58	1.58	0.40	0.85
74.55	277.50	107.14	1.00	107.14	1.64	0.31	0.83
74.62	257.79	96.61	1.00	96.61	1.69	0.23	0.81
74.68	264.00	100.53	1.00	100.53	1.66	0.25	0.82
74.75	271.34	104.26	1.00	104.26	1.64	0.28	0.83
74.82	279.72	106.14	1.00	106.14	1.66	0.32	0.84
74.89	286.02	109.00	1.00	109.00	1.66	0.36	0.84
74.94	287.70	108.65	1.00	108.65	1.67	0.37	0.84
75.01	286.29	106.79	1.00	106.79	1.70	0.36	0.84
75.07	268.23	97.20	1.09	105.58	1.75	0.27	0.82
75.14	273.59	67.22	54.25	3646.84	4.06	0.77	4.80
75.20	267.19	65.61	54.25	3559.37	4.06	0.77	4.69
75.27	264.93	65.03	54.25	3527.87	4.06	0.77	4.65
75.33	263.32	64.62	54.25	3505.36	4.06	0.77	4.62
75.41	262.66	64.44	54.25	3495.57	4.06	0.77	4.60
75.48	251.08	61.53	54.25	3337.93	4.06	0.76	4.39

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
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Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

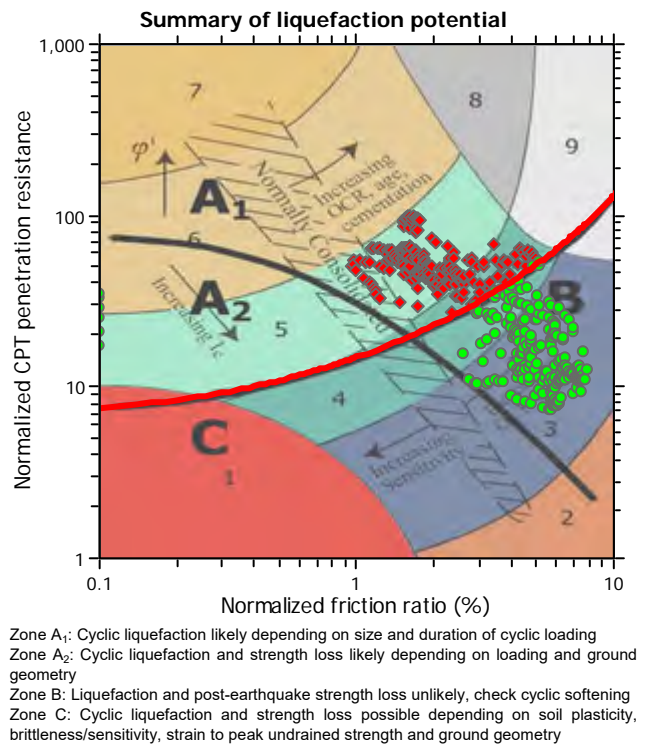
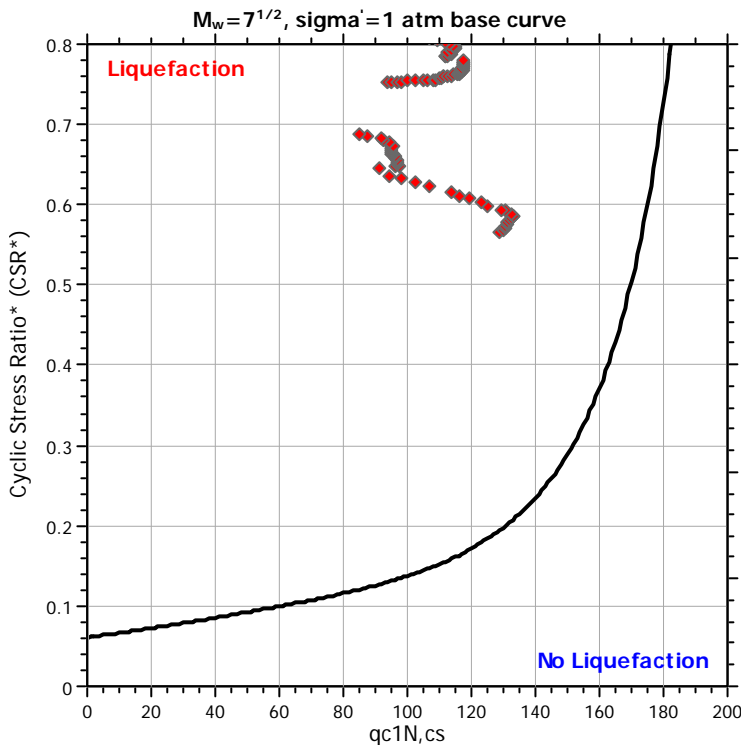
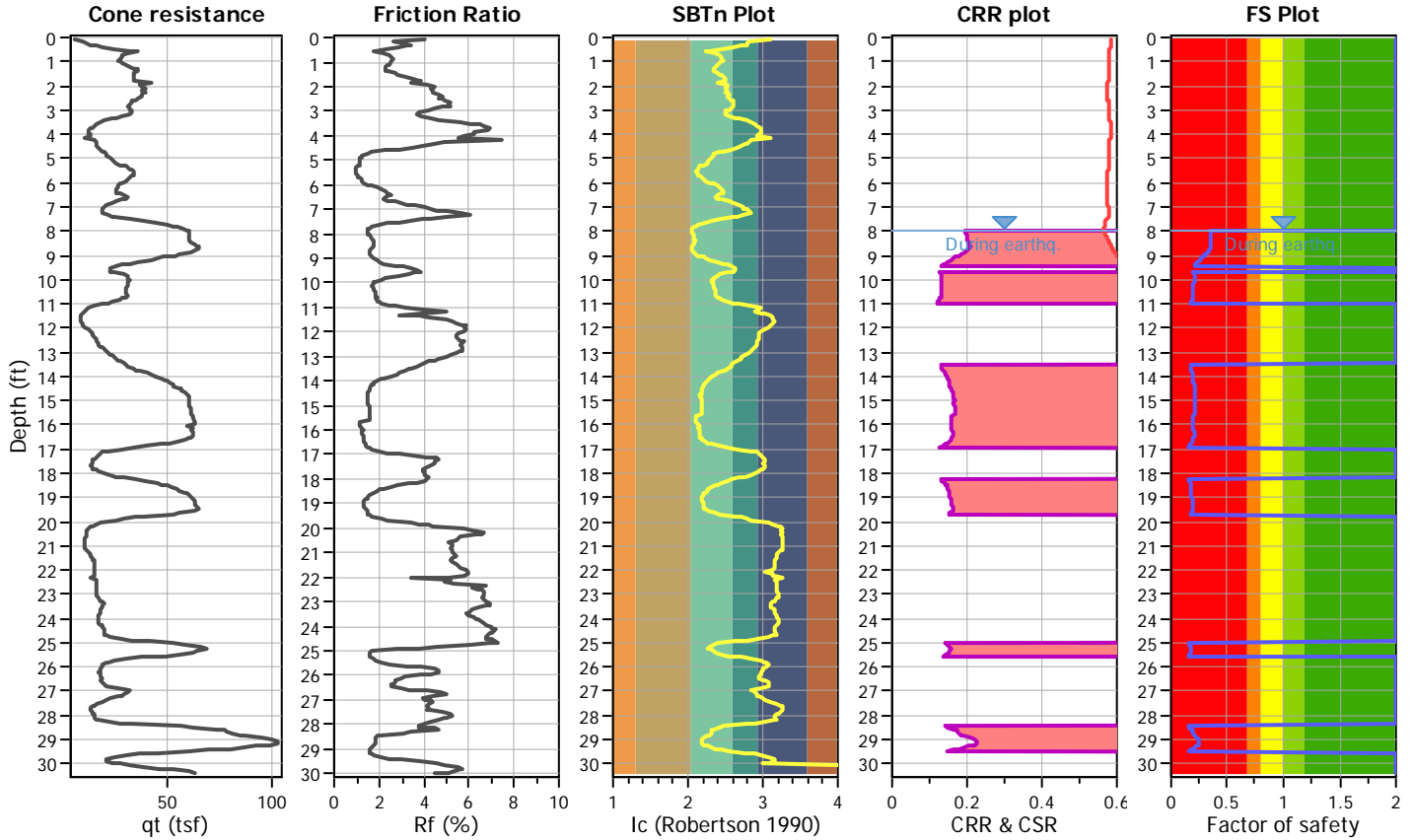
LIQUEFACTION ANALYSIS REPORT

Project title : Universal Engineering Services / Compton
CPT file : CPT-3

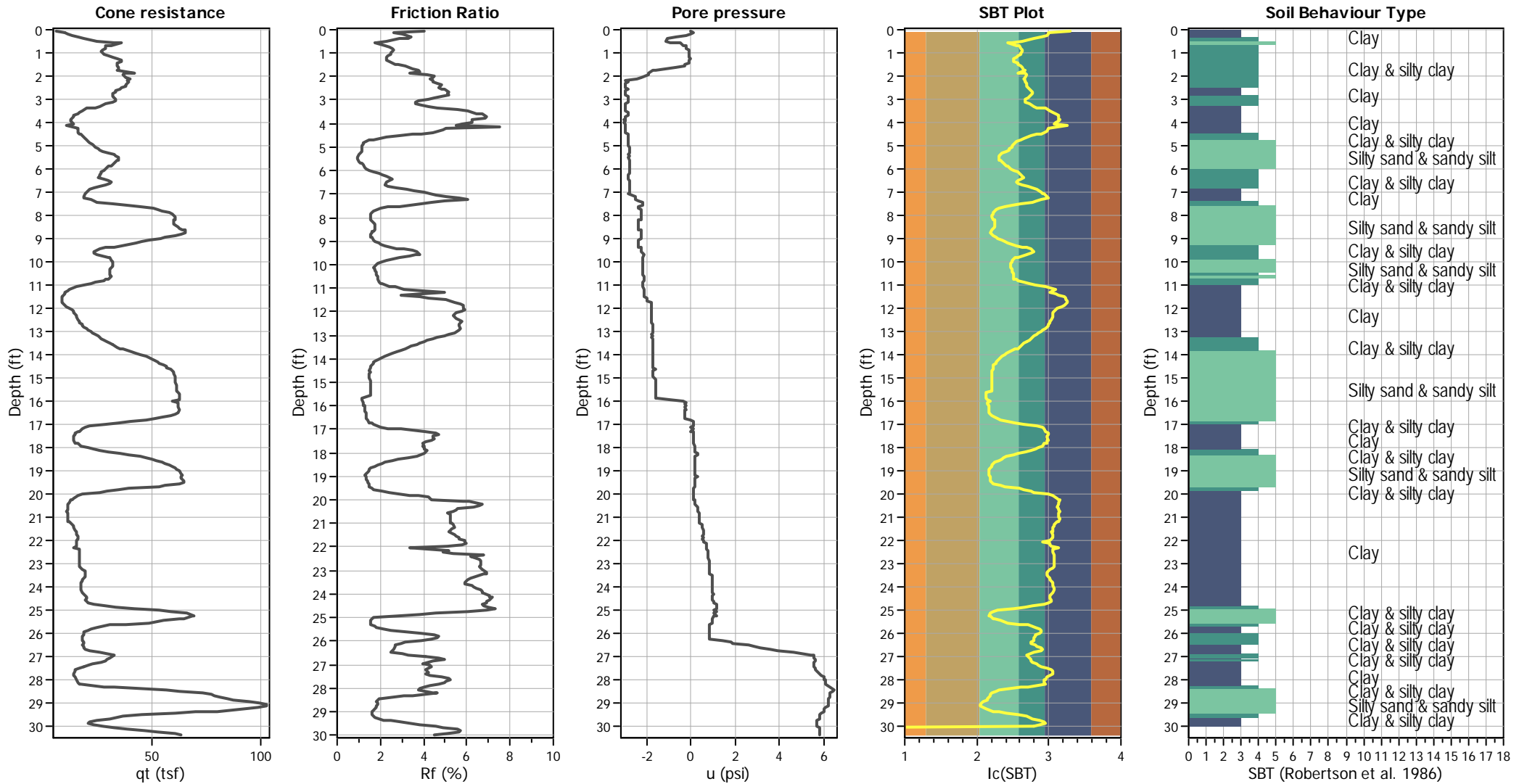
Location : 1111 E. Artesia Blvd, Compton, CA

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	52.90 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	1	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w :	7.30	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method
Peak ground acceleration:	0.77	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



CPT basic interpretation plots



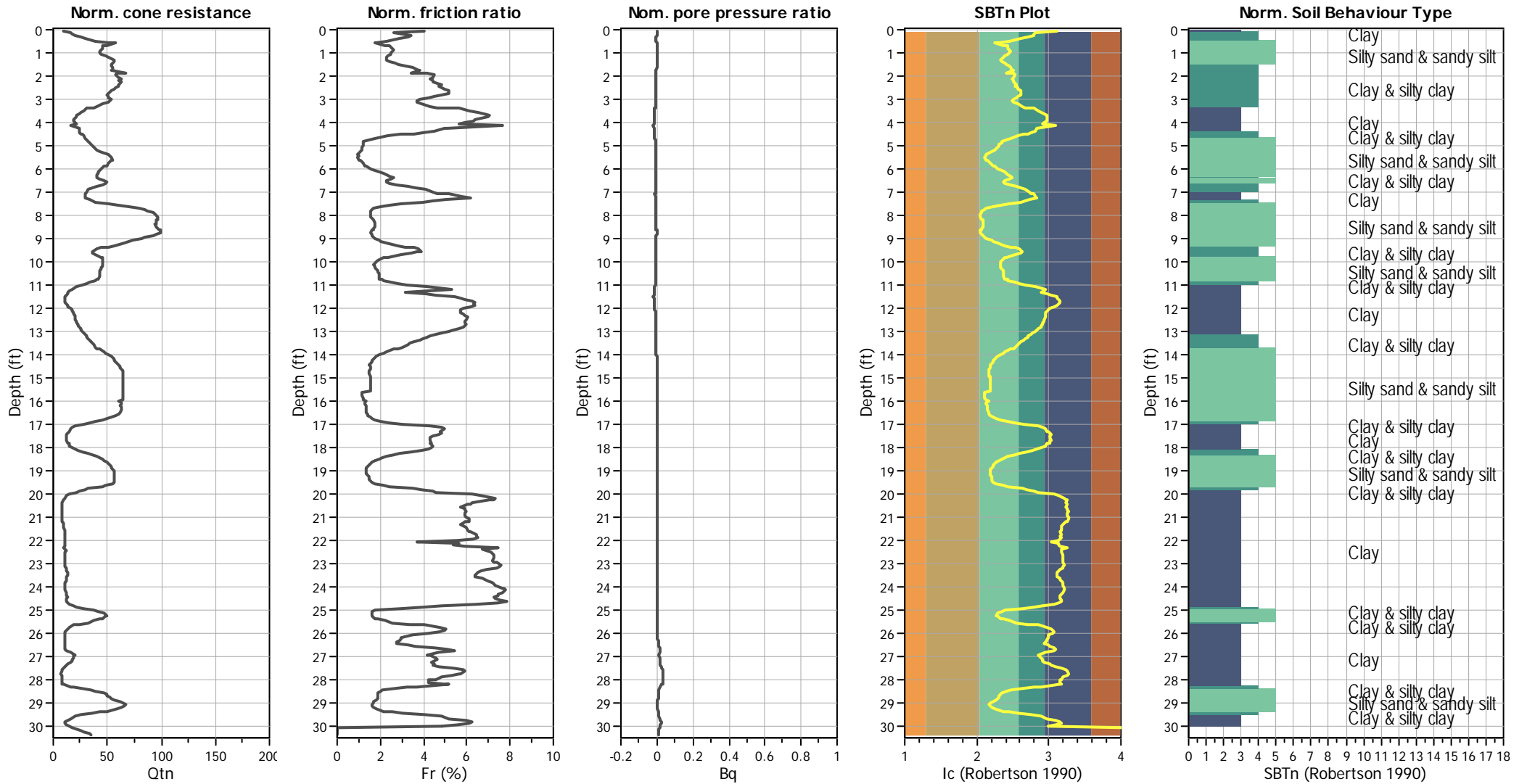
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



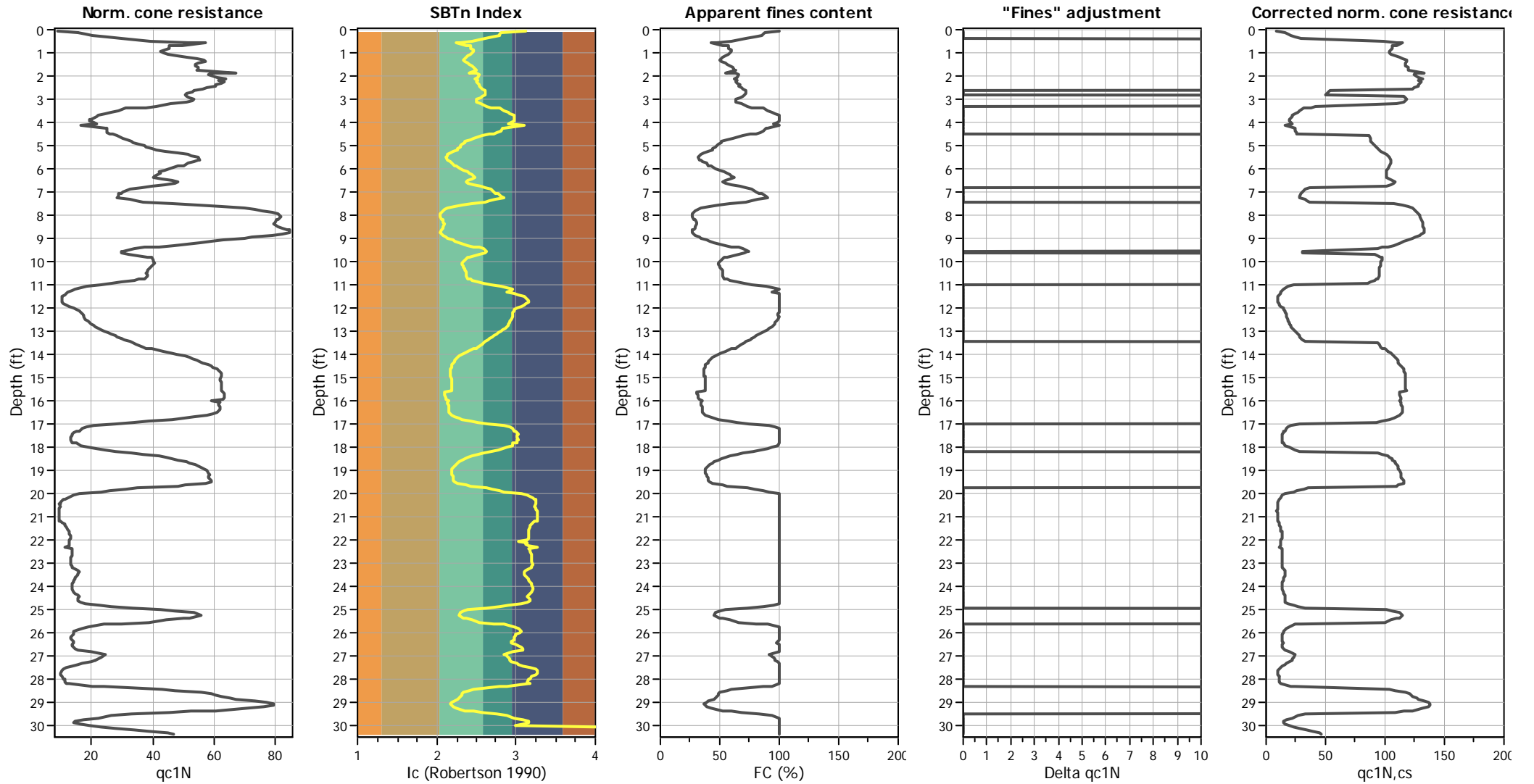
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

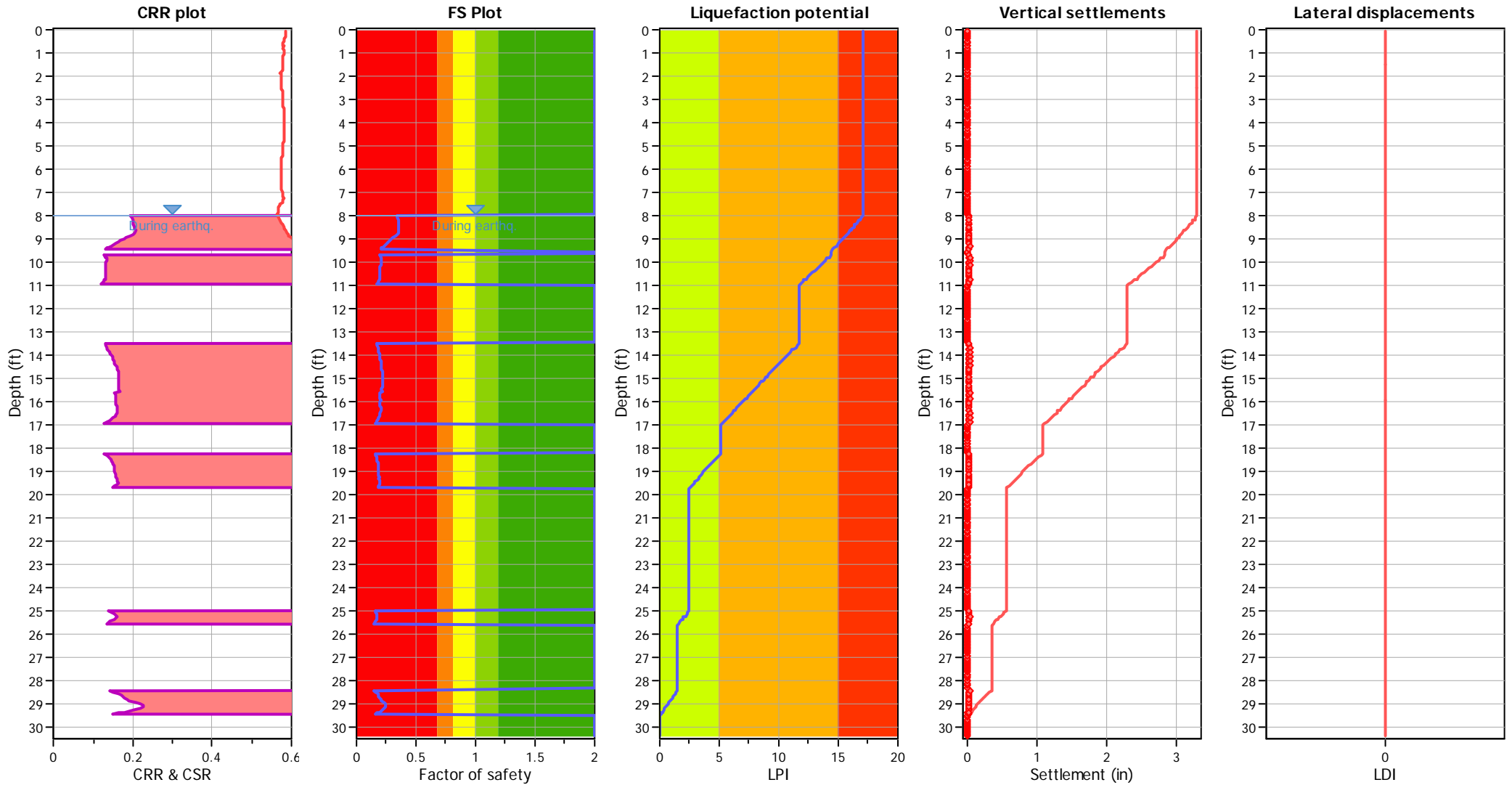
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

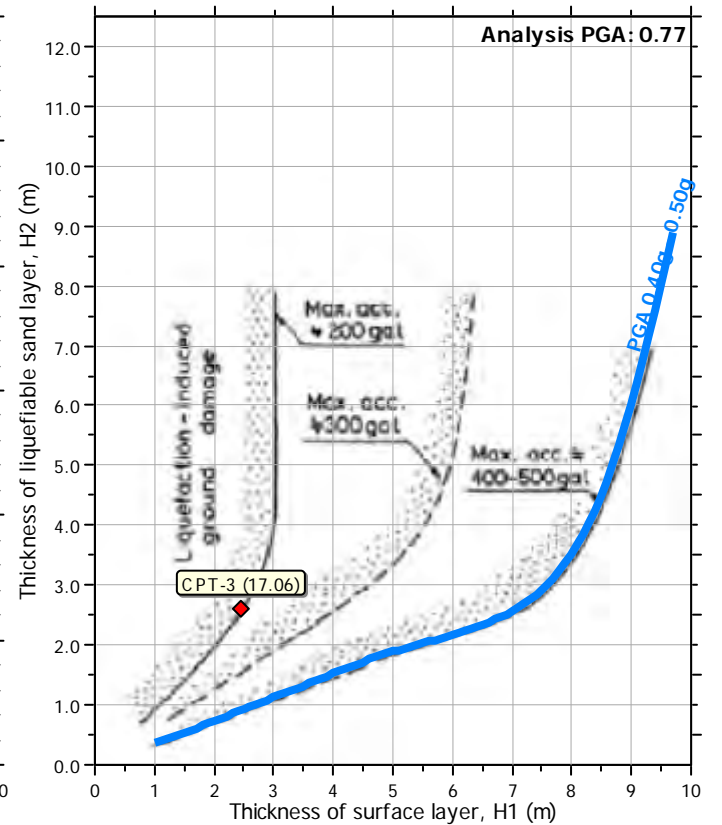
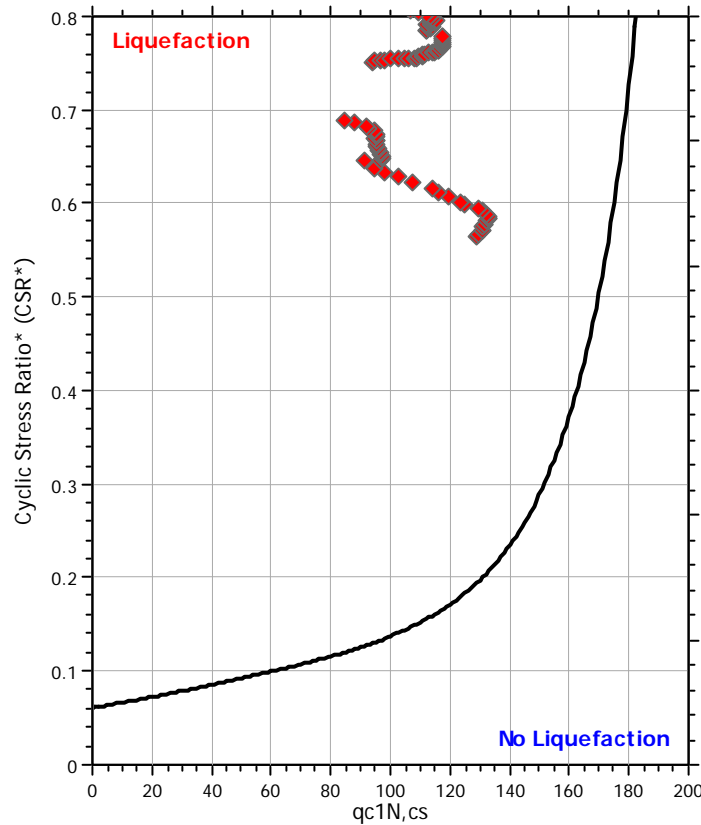
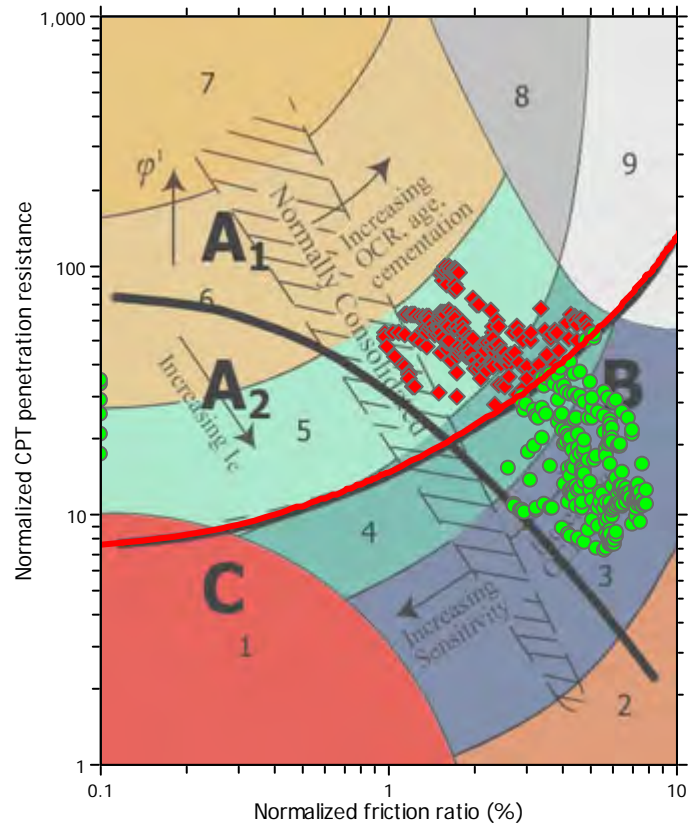
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

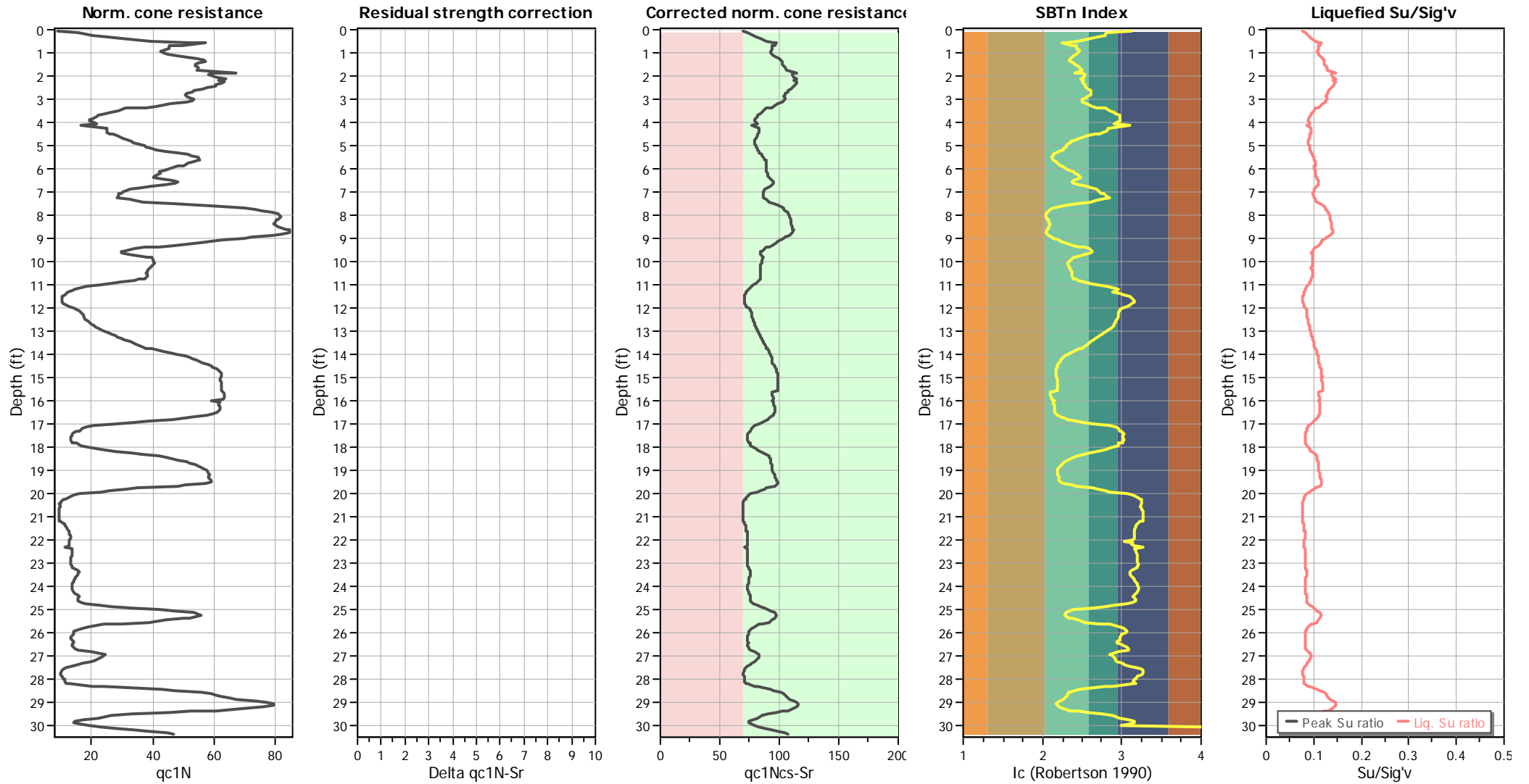
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_G applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.07	5.53	0.22	0.00	66.42	103.45
2	0.14	9.65	0.25	0.10	46.37	105.71
3	0.20	11.06	0.34	0.00	45.91	108.16
4	0.29	12.67	0.44	-0.19	45.21	110.40
5	0.35	15.49	0.51	-0.67	40.69	111.96
6	0.41	18.50	0.54	-1.05	36.00	112.85
7	0.49	24.54	0.57	-1.14	28.66	113.90
8	0.54	32.08	0.59	-0.95	22.55	114.84
9	0.59	35.60	0.61	-0.48	20.66	115.40
10	0.67	30.87	0.68	-0.38	24.95	115.76
11	0.72	28.16	0.69	-0.19	27.41	115.65
12	0.80	28.26	0.72	-0.19	27.86	115.98
13	0.86	27.25	0.72	-0.10	28.80	115.89
14	0.94	26.45	0.68	-0.10	28.97	115.45
15	0.99	27.15	0.68	-0.10	28.27	115.50
16	1.09	27.86	0.69	-0.10	27.76	115.65
17	1.12	29.77	0.70	-0.10	26.19	115.89
18	1.20	31.78	0.73	-0.10	25.15	116.40
19	1.27	33.89	0.77	0.00	24.27	116.99
20	1.33	35.40	0.81	-0.10	23.80	117.45
21	1.38	35.50	0.85	-0.10	24.26	117.80
22	1.48	33.99	0.91	-0.10	26.10	118.18
23	1.51	33.69	0.94	-0.29	26.79	118.43
24	1.58	33.59	1.05	-0.29	28.20	119.19
25	1.66	34.19	1.19	-0.67	29.40	120.16
26	1.73	34.09	1.28	-1.62	30.44	120.66
27	1.77	33.79	1.30	-1.72	30.95	120.77
28	1.85	41.94	1.42	-1.91	26.43	121.93
29	1.91	36.81	1.53	-1.91	30.93	122.19
30	1.97	36.31	1.64	-1.91	32.27	122.63
31	2.06	37.91	1.68	-2.29	31.42	122.91
32	2.12	39.83	1.70	-2.48	30.26	123.13
33	2.17	38.12	1.68	-2.96	31.33	122.95
34	2.25	39.32	1.73	-2.86	30.89	123.24
35	2.31	38.72	1.79	-2.96	31.81	123.44
36	2.36	37.81	1.82	-2.96	32.72	123.50
37	2.47	37.61	1.76	-2.96	32.36	123.24
38	2.52	36.00	1.74	-2.96	33.47	123.05
39	2.56	35.00	1.73	-2.86	34.22	122.95
40	2.63	33.39	1.73	-2.96	35.59	122.82
41	2.71	32.99	1.69	-2.96	35.60	122.62
42	2.77	31.78	1.63	-2.96	36.25	122.30
43	2.83	31.48	1.52	-2.96	35.40	121.75
44	2.90	31.68	1.42	-2.86	34.19	121.27
45	2.97	32.28	1.35	-2.86	32.90	120.95
46	3.03	33.29	1.26	-2.86	31.00	120.50
47	3.09	32.99	1.20	-2.86	30.63	120.15
48	3.16	31.88	1.16	-2.86	31.08	119.81

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.22	28.66	1.11	-2.96	33.52	119.24
50	3.30	25.65	1.09	-2.96	36.55	118.81
51	3.36	23.53	1.08	-2.96	39.21	118.56
52	3.41	19.41	1.08	-2.96	45.75	118.09
53	3.49	17.80	1.07	-2.96	48.75	117.81
54	3.57	16.39	1.06	-2.86	51.58	117.49
55	3.62	15.39	1.03	-2.86	53.53	117.13
56	3.70	13.78	0.95	-2.86	56.52	116.30
57	3.74	13.38	0.92	-2.96	56.99	115.95
58	3.85	12.17	0.76	-2.96	57.21	114.34
59	3.88	12.07	0.75	-3.05	57.35	114.24
60	3.95	12.07	0.75	-2.96	57.28	114.21
61	4.01	12.87	0.74	-3.05	54.53	114.31
62	4.09	13.58	0.75	-2.96	52.56	114.51
63	4.13	10.16	0.76	-2.96	65.15	113.90
64	4.23	15.39	0.77	-2.97	48.27	115.01
65	4.27	15.49	0.75	-2.97	47.67	114.87
66	4.37	15.49	0.69	-2.96	46.12	114.20
67	4.43	15.69	0.61	-2.96	43.80	113.40
68	4.48	16.09	0.56	-2.86	41.47	112.77
69	4.54	16.69	0.49	-2.86	38.24	111.85
70	4.60	17.50	0.40	-2.86	34.17	110.54
71	4.68	18.91	0.32	-2.86	29.38	109.14
72	4.73	19.61	0.29	-2.86	27.16	108.36
73	4.82	20.62	0.25	-2.86	24.58	107.48
74	4.86	20.82	0.25	-2.86	24.37	107.52
75	4.93	22.13	0.26	-2.86	23.22	107.89
76	5.02	23.13	0.27	-2.86	22.62	108.32
77	5.05	23.63	0.27	-2.76	22.28	108.49
78	5.13	24.74	0.28	-2.76	21.38	108.70
79	5.19	25.44	0.28	-2.76	20.92	108.89
80	5.25	27.25	0.28	-2.76	19.55	109.13
81	5.32	29.87	0.29	-2.76	17.87	109.52
82	5.41	32.18	0.31	-2.86	16.85	110.10
83	5.46	32.79	0.32	-2.76	16.72	110.37
84	5.51	34.09	0.33	-2.86	16.25	110.71
85	5.61	34.29	0.35	-2.76	16.65	111.20
86	5.66	33.99	0.36	-2.76	17.11	111.46
87	5.71	33.29	0.37	-2.76	17.74	111.60
88	5.78	32.08	0.39	-2.76	18.82	111.79
89	5.86	31.08	0.39	-2.76	19.62	111.83
90	5.91	29.97	0.40	-2.76	20.56	111.88
91	6.00	28.36	0.42	-2.76	22.31	112.15
92	6.06	27.36	0.46	-2.76	24.01	112.68
93	6.11	26.25	0.51	-2.76	26.00	113.25
94	6.20	26.35	0.56	-2.76	26.97	113.95
95	6.25	25.85	0.58	-2.86	28.05	114.26
96	6.31	25.44	0.61	-2.86	29.02	114.55

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.39	25.34	0.65	-2.86	29.90	114.99
98	6.45	27.36	0.66	-2.86	28.06	115.31
99	6.50	29.57	0.67	-2.76	26.18	115.57
100	6.59	31.28	0.69	-2.76	25.24	116.00
101	6.65	30.57	0.73	-2.76	26.33	116.27
102	6.70	28.56	0.78	-2.76	28.92	116.59
103	6.79	25.65	0.83	-2.76	32.86	116.84
104	6.85	23.33	0.83	-2.76	35.74	116.63
105	6.90	20.82	0.83	-2.76	39.31	116.33
106	6.99	19.31	0.83	-2.76	41.79	116.12
107	7.05	19.01	0.86	-2.76	42.94	116.36
108	7.10	18.71	0.94	-2.86	44.97	116.96
109	7.17	18.61	1.05	-2.54	47.12	117.76
110	7.23	18.50	1.12	-2.54	48.45	118.19
111	7.32	21.62	1.07	-2.54	42.13	118.26
112	7.38	23.13	1.00	-2.37	38.83	117.95
113	7.43	24.64	0.96	-2.19	36.19	117.80
114	7.51	31.88	0.92	-2.19	28.22	118.13
115	7.57	38.32	0.90	-2.19	23.36	118.41
116	7.62	44.15	0.88	-2.38	19.93	118.58
117	7.71	50.18	0.85	-2.38	16.95	118.62
118	7.77	52.70	0.84	-2.29	15.88	118.63
119	7.82	54.81	0.83	-2.29	15.09	118.67
120	7.91	57.73	0.87	-2.29	14.58	119.16
121	7.97	59.24	0.90	-2.29	14.38	119.44
122	8.01	60.04	0.92	-2.29	14.32	119.63
123	8.07	60.74	0.94	-2.29	14.34	119.85
124	8.17	60.34	0.99	-2.29	14.86	120.17
125	8.21	59.94	1.00	-2.38	15.15	120.28
126	8.30	59.94	1.03	-2.38	15.40	120.45
127	8.36	59.94	1.04	-2.38	15.54	120.54
128	8.41	59.94	1.05	-2.38	15.62	120.59
129	8.50	61.55	1.05	-2.38	15.29	120.70
130	8.56	62.86	1.05	-2.38	14.96	120.73
131	8.61	63.96	1.05	-2.38	14.69	120.76
132	8.66	64.97	1.04	-2.29	14.42	120.75
133	8.73	65.17	1.02	-2.29	14.21	120.58
134	8.81	63.26	1.00	-2.29	14.58	120.35
135	8.86	60.84	0.98	-2.29	15.15	120.16
136	8.96	55.82	0.94	-2.29	16.33	119.62
137	9.01	53.91	0.92	-2.29	16.83	119.41
138	9.06	48.47	0.93	-2.38	18.94	119.23
139	9.13	45.36	0.92	-2.38	20.11	118.92
140	9.20	42.54	0.95	-2.38	21.82	119.02
141	9.30	36.00	0.99	-2.38	26.13	118.96
142	9.35	32.08	0.98	-2.38	28.99	118.62
143	9.40	28.26	0.98	-2.29	32.42	118.24
144	9.46	25.75	0.95	-2.29	34.81	117.83

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.55	22.93	0.88	-2.29	37.19	116.93
146	9.60	22.73	0.82	-2.29	36.57	116.47
147	9.66	22.73	0.76	-2.19	35.45	115.91
148	9.71	24.64	0.72	-2.10	32.26	115.66
149	9.80	29.47	0.68	-2.19	27.08	115.65
150	9.85	30.67	0.65	-2.19	25.72	115.43
151	9.93	31.28	0.58	-2.19	24.26	114.71
152	9.98	31.48	0.56	-2.19	23.82	114.46
153	10.04	31.68	0.54	-2.19	23.43	114.25
154	10.12	31.48	0.53	-2.19	23.35	114.01
155	10.19	31.38	0.54	-2.19	23.67	114.15
156	10.25	30.98	0.54	-2.19	23.94	114.07
157	10.31	30.57	0.55	-2.19	24.54	114.21
158	10.39	30.47	0.56	-2.19	24.83	114.31
159	10.45	30.57	0.56	-2.19	24.94	114.41
160	10.52	30.27	0.57	-2.19	25.36	114.48
161	10.58	30.57	0.58	-2.19	25.31	114.59
162	10.64	30.87	0.58	-2.10	25.21	114.67
163	10.74	29.97	0.58	-2.10	25.97	114.57
164	10.79	28.46	0.58	-2.10	27.23	114.43
165	10.83	27.56	0.58	-2.10	28.05	114.34
166	10.90	23.83	0.58	-2.19	31.90	113.98
167	10.96	21.32	0.58	-2.19	35.05	113.70
168	11.03	18.50	0.58	-2.19	39.38	113.35
169	11.10	14.78	0.58	-2.19	47.13	112.88
170	11.18	11.87	0.59	-2.10	55.87	112.47
171	11.24	10.76	0.43	-2.10	54.18	109.81
172	11.29	9.86	0.29	-2.10	51.46	106.72
173	11.36	9.45	0.36	-2.10	56.94	108.24
174	11.42	8.95	0.38	-2.10	60.42	108.48
175	11.51	8.25	0.41	-2.10	66.12	108.92
176	11.57	8.25	0.43	-1.97	67.17	109.25
177	11.62	8.25	0.45	-1.97	67.94	109.49
178	11.70	8.25	0.47	-1.97	69.32	109.91
179	11.75	8.35	0.49	-1.81	69.57	110.20
180	11.83	8.95	0.52	-1.81	67.56	110.81
181	11.90	9.55	0.56	-1.81	66.16	111.54
182	11.95	10.36	0.60	-1.81	63.73	112.21
183	12.03	11.77	0.65	-1.81	59.67	113.11
184	12.10	12.77	0.69	-1.81	57.41	113.76
185	12.15	13.38	0.72	-1.81	56.36	114.21
186	12.21	13.88	0.75	-1.81	55.66	114.58
187	12.28	14.38	0.79	-1.81	55.35	115.07
188	12.34	14.68	0.82	-1.81	55.29	115.39
189	12.40	14.88	0.85	-1.81	55.55	115.70
190	12.48	15.49	0.88	-1.81	54.61	116.03
191	12.55	16.09	0.91	-1.81	53.76	116.35
192	12.60	16.59	0.94	-1.81	53.22	116.65

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.70	17.30	0.99	-1.72	52.67	117.13
194	12.75	17.90	1.01	-1.72	51.90	117.41
195	12.80	18.50	1.04	-1.72	51.19	117.68
196	12.89	19.51	1.05	-1.72	49.55	117.90
197	12.94	20.42	1.06	-1.72	48.04	118.04
198	13.00	21.32	1.06	-1.72	46.53	118.13
199	13.09	22.53	1.05	-1.72	44.59	118.21
200	13.14	23.43	1.04	-1.81	43.20	118.25
201	13.19	24.74	1.03	-1.72	41.34	118.33
202	13.28	25.34	1.02	-1.81	40.53	118.33
203	13.34	26.65	1.02	-1.72	38.91	118.41
204	13.39	27.56	1.02	-1.72	37.88	118.47
205	13.47	29.27	1.01	-1.72	36.02	118.57
206	13.53	30.37	1.00	-1.72	34.88	118.60
207	13.59	31.38	1.00	-1.72	33.94	118.66
208	13.67	33.49	0.98	-1.72	31.91	118.67
209	13.73	34.80	0.96	-1.72	30.69	118.64
210	13.79	36.71	0.94	-1.72	29.00	118.58
211	13.88	40.23	0.90	-1.72	26.25	118.49
212	13.93	42.54	0.88	-1.72	24.77	118.51
213	13.99	44.55	0.85	-1.72	23.38	118.38
214	14.07	47.07	0.84	-1.72	22.04	118.39
215	14.13	48.68	0.83	-1.72	21.25	118.41
216	14.18	49.78	0.83	-1.72	20.77	118.43
217	14.28	51.19	0.82	-1.72	20.11	118.40
218	14.33	52.30	0.81	-1.72	19.64	118.41
219	14.38	53.00	0.81	-1.72	19.40	118.44
220	14.48	55.21	0.81	-1.72	18.62	118.54
221	14.53	56.32	0.85	-1.72	18.60	118.87
222	14.58	56.82	0.87	-1.72	18.69	119.09
223	14.65	58.43	0.87	-1.62	18.25	119.21
224	14.72	59.03	0.88	-1.72	18.11	119.26
225	14.78	59.54	0.88	-1.72	18.02	119.32
226	14.83	60.14	0.89	-1.72	17.94	119.42
227	14.92	60.24	0.91	-1.72	18.16	119.59
228	14.98	60.44	0.93	-1.72	18.27	119.72
229	15.05	60.24	0.93	-1.62	18.37	119.70
230	15.12	60.24	0.93	-1.62	18.40	119.70
231	15.16	60.34	0.93	-1.62	18.42	119.73
232	15.22	60.74	0.94	-1.62	18.39	119.80
233	15.32	60.94	0.94	-1.62	18.42	119.84
234	15.37	60.94	0.94	-1.62	18.41	119.81
235	15.46	61.05	0.94	-1.62	18.43	119.82
236	15.52	61.25	0.94	-1.62	18.43	119.86
237	15.56	61.45	0.95	-1.62	18.44	119.92
238	15.66	62.05	0.70	-1.62	15.74	117.71
239	15.71	62.35	0.70	-1.62	15.74	117.79
240	15.75	62.45	0.72	-1.62	15.85	117.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.86	62.86	0.74	-1.62	16.08	118.19
242	15.91	62.86	0.75	-1.52	16.23	118.31
243	15.96	62.76	0.76	-0.94	16.38	118.39
244	16.02	59.13	0.77	-0.38	17.63	118.32
245	16.10	61.95	0.77	-0.19	16.79	118.46
246	16.16	61.75	0.78	-0.29	16.91	118.47
247	16.21	61.65	0.80	-0.19	17.23	118.69
248	16.29	62.05	0.83	-0.29	17.41	118.95
249	16.36	62.35	0.84	-0.19	17.48	119.06
250	16.41	62.45	0.84	-0.29	17.48	119.08
251	16.51	61.65	0.83	-0.29	17.66	118.94
252	16.56	60.24	0.82	-0.29	18.09	118.84
253	16.61	58.43	0.81	-0.29	18.64	118.69
254	16.71	54.31	0.81	-0.29	20.18	118.48
255	16.76	50.99	0.81	-0.29	21.54	118.29
256	16.81	47.07	0.79	0.00	23.23	117.98
257	16.89	39.72	0.79	0.10	27.40	117.53
258	16.95	34.29	0.80	0.10	31.62	117.29
259	17.00	28.46	0.83	0.10	37.79	117.11
260	17.10	21.22	0.87	0.10	48.84	116.70
261	17.14	18.81	0.86	0.00	53.38	116.29
262	17.20	17.50	0.82	0.10	55.66	115.79
263	17.29	16.49	0.73	0.00	56.33	114.84
264	17.33	15.69	0.70	0.10	57.61	114.36
265	17.39	14.58	0.65	0.10	59.65	113.67
266	17.46	13.98	0.61	0.10	60.29	113.03
267	17.52	13.88	0.57	0.10	59.52	112.54
268	17.59	13.78	0.54	0.10	59.17	112.22
269	17.70	13.48	0.54	0.10	60.13	112.09
270	17.72	13.68	0.55	0.10	59.74	112.22
271	17.80	14.38	0.58	0.10	58.85	112.84
272	17.85	15.89	0.64	0.10	56.22	113.76
273	17.92	17.10	0.72	0.19	55.18	114.75
274	17.99	20.01	0.82	0.19	51.24	116.14
275	18.05	22.83	0.92	0.19	48.08	117.28
276	18.14	25.75	0.96	0.19	44.38	117.87
277	18.18	29.47	0.97	0.19	39.97	118.31
278	18.25	35.20	1.00	0.29	34.71	118.93
279	18.32	39.32	1.00	0.29	31.60	119.25
280	18.39	44.75	0.99	0.19	27.95	119.49
281	18.45	47.27	0.97	0.19	26.27	119.44
282	18.50	49.68	0.94	0.19	24.75	119.36
283	18.57	51.79	0.89	0.19	23.19	119.05
284	18.64	54.51	0.86	0.19	21.65	118.88
285	18.73	56.02	0.84	0.19	20.95	118.85
286	18.78	58.13	0.85	0.19	20.24	119.00
287	18.85	59.24	0.84	0.19	19.71	118.92
288	18.91	60.24	0.80	0.19	19.02	118.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.97	61.25	0.79	0.19	18.59	118.62
290	19.03	62.25	0.82	0.19	18.53	118.86
291	19.11	63.16	0.85	0.19	18.65	119.21
292	19.17	63.56	0.88	0.19	18.84	119.46
293	19.23	63.36	0.90	0.29	19.19	119.66
294	19.31	63.16	0.92	0.19	19.46	119.78
295	19.39	64.16	0.94	0.19	19.39	119.99
296	19.43	64.57	0.96	0.19	19.43	120.13
297	19.49	64.57	1.03	0.19	20.14	120.65
298	19.57	62.76	1.07	0.19	21.21	120.88
299	19.65	55.82	1.17	0.19	24.98	121.24
300	19.69	52.90	1.26	0.19	27.27	121.67
301	19.79	38.72	1.31	0.10	36.90	121.16
302	19.83	34.60	1.29	0.10	40.48	120.80
303	19.89	29.06	1.23	0.10	45.99	120.03
304	19.97	25.65	1.12	0.10	49.17	119.01
305	20.03	17.70	1.03	0.10	63.49	117.51
306	20.08	15.69	0.96	0.10	67.88	116.70
307	20.17	13.78	0.92	0.10	73.68	116.07
308	20.23	12.77	0.84	0.10	75.85	115.24
309	20.28	11.97	0.76	0.19	77.09	114.31
310	20.37	11.26	0.63	0.19	76.41	112.77
311	20.42	10.96	0.60	0.19	77.04	112.39
312	20.47	10.86	0.59	0.19	77.09	112.18
313	20.55	11.16	0.57	0.29	75.14	112.06
314	20.63	10.76	0.57	0.29	77.04	111.89
315	20.67	10.66	0.56	0.29	77.44	111.80
316	20.77	10.46	0.55	0.29	78.29	111.63
317	20.82	10.56	0.55	0.38	77.82	111.66
318	20.88	10.56	0.55	0.38	77.97	111.67
319	20.96	10.56	0.55	0.38	78.15	111.69
320	21.01	10.56	0.56	0.38	78.51	111.79
321	21.06	10.66	0.57	0.38	78.59	111.99
322	21.17	11.06	0.60	0.38	77.72	112.42
323	21.21	11.57	0.61	0.38	75.72	112.68
324	21.26	12.07	0.63	0.38	74.22	113.02
325	21.33	12.87	0.67	0.48	71.96	113.54
326	21.40	13.28	0.70	0.48	71.52	114.00
327	21.46	13.68	0.74	0.48	71.25	114.48
328	21.55	14.28	0.79	0.57	70.33	114.99
329	21.61	14.58	0.82	0.57	70.20	115.34
330	21.66	15.09	0.85	0.57	69.44	115.74
331	21.75	15.09	0.89	0.57	70.50	116.07
332	21.81	15.29	0.91	0.48	70.24	116.21
333	21.86	15.29	0.91	0.57	70.44	116.25
334	21.94	15.29	0.88	0.48	69.86	116.02
335	22.00	14.98	0.77	0.57	68.01	114.92
336	22.06	14.98	0.51	0.57	60.29	111.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.14	14.98	0.77	0.67	68.35	114.98
338	22.20	14.98	0.73	0.67	67.44	114.62
339	22.25	15.09	0.81	0.67	69.14	115.36
340	22.34	13.38	0.90	0.67	77.93	115.86
341	22.40	15.99	0.98	0.67	70.47	116.91
342	22.47	16.29	1.04	0.76	70.82	117.37
343	22.52	16.19	1.06	0.76	71.68	117.51
344	22.61	16.09	1.07	0.76	72.19	117.52
345	22.67	16.09	1.07	0.76	72.29	117.53
346	22.72	16.09	1.07	0.76	72.37	117.54
347	22.78	16.09	1.07	0.76	72.41	117.53
348	22.86	16.09	1.06	0.86	72.42	117.49
349	22.92	16.09	1.07	0.86	72.58	117.52
350	22.97	16.09	1.09	0.86	73.03	117.65
351	23.06	16.09	1.12	0.86	73.79	117.86
352	23.12	16.39	1.13	0.86	73.19	118.00
353	23.17	16.80	1.14	0.86	72.16	118.12
354	23.26	17.90	1.15	0.86	69.18	118.31
355	23.31	18.61	1.15	0.86	67.35	118.42
356	23.41	19.21	1.16	0.86	66.12	118.56
357	23.46	19.11	1.14	0.86	66.08	118.42
358	23.51	19.01	1.12	0.95	66.09	118.31
359	23.56	18.71	1.11	0.95	66.69	118.18
360	23.65	18.00	1.12	0.95	68.91	118.16
361	23.71	17.70	1.12	0.95	69.79	118.12
362	23.75	17.60	1.13	0.95	70.31	118.16
363	23.85	17.20	1.14	0.95	71.82	118.18
364	23.91	17.10	1.14	0.95	72.22	118.17
365	23.95	17.00	1.15	0.95	72.66	118.19
366	24.04	16.69	1.17	0.95	74.22	118.30
367	24.10	16.80	1.19	0.95	74.23	118.41
368	24.15	16.90	1.21	0.95	74.42	118.57
369	24.25	17.70	1.24	0.95	72.75	118.88
370	24.30	18.40	1.27	1.05	71.24	119.11
371	24.36	19.11	1.32	0.95	70.20	119.48
372	24.45	19.71	1.33	0.95	68.94	119.61
373	24.50	19.51	1.32	0.95	69.47	119.57
374	24.55	19.21	1.34	0.95	70.61	119.64
375	24.64	19.41	1.41	1.05	71.35	120.05
376	24.69	20.52	1.42	1.05	68.70	120.21
377	24.75	22.63	1.37	1.14	63.36	120.20
378	24.84	28.36	1.29	1.14	52.52	120.32
379	24.89	33.09	1.26	1.14	46.09	120.51
380	24.95	41.54	1.17	1.14	36.81	120.51
381	25.02	52.80	0.89	1.05	26.19	119.07
382	25.07	58.53	0.93	1.14	24.12	119.70
383	25.14	65.87	1.02	1.05	22.20	120.65
384	25.23	68.99	1.07	1.14	21.59	121.08

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.29	68.79	1.08	1.05	21.80	121.16
386	25.36	64.47	1.12	0.95	23.76	121.23
387	25.41	62.25	1.15	0.95	24.98	121.35
388	25.48	55.21	1.17	0.95	28.50	121.22
389	25.55	48.47	1.19	0.95	32.61	121.04
390	25.61	37.51	1.20	0.86	41.27	120.47
391	25.66	30.47	1.18	0.86	48.80	119.80
392	25.75	24.34	1.09	0.86	56.72	118.70
393	25.80	21.72	1.02	0.86	60.51	117.92
394	25.86	20.32	0.94	0.86	62.06	117.16
395	25.94	18.50	0.80	0.86	63.54	115.79
396	25.99	18.50	0.72	0.86	61.50	114.96
397	26.06	18.20	0.58	0.86	58.51	113.36
398	26.12	17.50	0.52	0.86	58.42	112.44
399	26.19	17.30	0.47	0.86	57.39	111.71
400	26.25	17.40	0.47	0.86	57.07	111.66
401	26.34	17.60	0.46	1.43	56.53	111.64
402	26.38	18.20	0.46	1.81	54.98	111.66
403	26.45	18.50	0.46	1.91	54.51	111.78
404	26.54	17.90	0.54	2.57	58.39	112.76
405	26.59	18.00	0.60	2.86	60.04	113.57
406	26.65	18.30	0.76	3.15	63.57	115.32
407	26.71	19.21	0.91	3.62	64.80	116.76
408	26.78	20.72	1.04	3.91	63.94	117.94
409	26.84	25.85	1.15	4.67	55.96	119.21
410	26.94	32.18	1.28	5.43	49.09	120.55
411	26.98	32.08	1.30	5.53	49.56	120.68
412	27.04	30.57	1.32	5.53	51.70	120.64
413	27.11	28.96	1.27	5.62	53.35	120.26
414	27.18	28.16	1.19	5.62	53.40	119.71
415	27.23	26.25	1.08	5.53	54.62	118.82
416	27.32	22.43	0.94	5.53	59.03	117.45
417	27.38	20.52	0.84	5.53	61.01	116.40
418	27.43	18.40	0.79	5.53	65.00	115.69
419	27.52	15.89	0.77	5.62	71.73	115.08
420	27.58	14.48	0.76	5.62	76.48	114.76
421	27.63	13.98	0.74	5.72	77.90	114.47
422	27.73	13.48	0.68	5.81	78.33	113.80
423	27.78	13.28	0.66	5.81	78.59	113.55
424	27.83	13.58	0.64	5.91	76.75	113.38
425	27.91	14.28	0.61	6.00	73.22	113.18
426	27.98	14.78	0.60	6.00	71.08	113.11
427	28.03	15.09	0.58	6.10	69.30	112.87
428	28.11	15.19	0.57	6.10	68.94	112.85
429	28.18	15.89	0.71	6.10	70.96	114.55
430	28.22	17.10	0.80	6.10	69.58	115.57
431	28.32	27.46	0.95	6.29	51.50	118.00
432	28.35	32.38	1.00	6.29	45.85	118.73

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.43	56.42	1.14	6.48	29.04	121.05
434	28.48	62.15	1.21	6.39	27.11	121.75
435	28.56	73.01	1.34	6.29	24.05	122.88
436	28.63	77.04	1.43	6.29	23.45	123.48
437	28.68	78.54	1.46	6.29	23.20	123.67
438	28.74	81.06	1.50	6.29	22.75	123.95
439	28.82	84.58	1.53	6.20	22.02	124.23
440	28.88	87.09	1.55	6.20	21.44	124.37
441	28.95	94.94	1.58	6.20	19.70	124.74
442	29.02	99.66	1.62	6.20	18.85	125.02
443	29.08	102.68	1.62	6.20	18.24	125.10
444	29.15	102.58	1.63	6.20	18.34	125.14
445	29.21	98.86	1.64	6.10	19.21	125.08
446	29.27	92.52	1.64	6.00	20.81	124.95
447	29.37	79.85	1.70	6.00	24.90	124.85
448	29.40	69.79	1.73	6.00	28.80	124.63
449	29.46	60.34	1.78	5.91	33.65	124.50
450	29.54	44.95	1.74	5.81	43.49	123.59
451	29.60	36.21	1.66	5.81	51.10	122.75
452	29.67	30.47	1.49	5.81	56.27	121.53
453	29.73	24.44	1.36	5.72	64.46	120.34
454	29.81	20.72	1.19	5.72	69.75	118.93
455	29.86	20.11	1.13	5.72	70.30	118.51
456	29.96	22.93	1.18	5.72	64.81	119.13
457	29.99	27.15	1.23	5.72	57.90	119.83
458	30.06	32.28	0.00	5.81	100.00	87.36
459	30.14	38.62	0.00	5.81	100.00	87.36
460	30.20	46.26	0.00	5.81	100.00	87.36
461	30.26	52.40	0.00	5.81	100.00	87.36
462	30.33	60.34	0.00	5.81	100.00	87.36
463	30.38	62.86	0.00	5.81	100.00	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q _c :	Measured cone resistance (tsf)
f _s :	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.07	0.00	0.00	0.00	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
2	0.14	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
3	0.20	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
4	0.29	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
5	0.35	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
6	0.41	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
7	0.49	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
8	0.54	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
9	0.59	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
10	0.67	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
11	0.72	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
12	0.80	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
13	0.86	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
14	0.94	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
15	0.99	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
16	1.09	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
17	1.12	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
18	1.20	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
19	1.27	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
20	1.33	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
21	1.38	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
22	1.48	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
23	1.51	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
24	1.58	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
25	1.66	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
26	1.73	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
27	1.77	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
28	1.85	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
29	1.91	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
30	1.97	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
31	2.06	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
32	2.12	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
33	2.17	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
34	2.25	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
35	2.31	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
36	2.36	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
37	2.47	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
38	2.52	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
39	2.56	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
40	2.63	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
41	2.71	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
42	2.77	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
43	2.83	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
44	2.90	0.17	0.00	0.17	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
45	2.97	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
46	3.03	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
47	3.09	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
48	3.16	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	3.22	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
50	3.30	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
51	3.36	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
52	3.41	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
53	3.49	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
54	3.57	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
55	3.62	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
56	3.70	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
57	3.74	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
58	3.85	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
59	3.88	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
60	3.95	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
61	4.01	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
62	4.09	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
63	4.13	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
64	4.23	0.25	0.00	0.25	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
65	4.27	0.25	0.00	0.25	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
66	4.37	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
67	4.43	0.26	0.00	0.26	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
68	4.48	0.26	0.00	0.26	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
69	4.54	0.27	0.00	0.27	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
70	4.60	0.27	0.00	0.27	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
71	4.68	0.27	0.00	0.27	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
72	4.73	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
73	4.82	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
74	4.86	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
75	4.93	0.29	0.00	0.29	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
76	5.02	0.29	0.00	0.29	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
77	5.05	0.29	0.00	0.29	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
78	5.13	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
79	5.19	0.30	0.00	0.30	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
80	5.25	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
81	5.32	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
82	5.41	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
83	5.46	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
84	5.51	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
85	5.61	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
86	5.66	0.33	0.00	0.33	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
87	5.71	0.33	0.00	0.33	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
88	5.78	0.33	0.00	0.33	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
89	5.86	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
90	5.91	0.34	0.00	0.34	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
91	6.00	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
92	6.06	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
93	6.11	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
94	6.20	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
95	6.25	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
96	6.31	0.36	0.00	0.36	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
97	6.39	0.37	0.00	0.37	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
98	6.45	0.37	0.00	0.37	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
99	6.50	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
100	6.59	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
101	6.65	0.38	0.00	0.38	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
102	6.70	0.39	0.00	0.39	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
103	6.79	0.39	0.00	0.39	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
104	6.85	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
105	6.90	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
106	6.99	0.40	0.00	0.40	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
107	7.05	0.41	0.00	0.41	0.99	0.494	1.05	0.469	1.09	1.30	2.000	No
108	7.10	0.41	0.00	0.41	0.99	0.494	1.05	0.469	1.09	1.30	2.000	No
109	7.17	0.41	0.00	0.41	0.99	0.494	1.05	0.469	1.09	1.30	2.000	No
110	7.23	0.42	0.00	0.42	0.99	0.494	1.05	0.469	1.09	1.30	2.000	No
111	7.32	0.42	0.00	0.42	0.99	0.494	1.05	0.468	1.09	1.30	2.000	No
112	7.38	0.43	0.00	0.43	0.99	0.494	1.05	0.468	1.09	1.30	2.000	No
113	7.43	0.43	0.00	0.43	0.99	0.494	1.05	0.468	1.09	1.30	2.000	No
114	7.51	0.43	0.00	0.43	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
115	7.57	0.44	0.00	0.44	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
116	7.62	0.44	0.00	0.44	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
117	7.71	0.45	0.00	0.45	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
118	7.77	0.45	0.00	0.45	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
119	7.82	0.45	0.00	0.45	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
120	7.91	0.46	0.00	0.46	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
121	7.97	0.46	0.00	0.46	0.98	0.493	1.05	0.468	1.10	1.30	2.000	No
122	8.01	0.46	0.00	0.46	0.98	0.493	1.05	0.468	1.10	1.30	0.565	No
123	8.07	0.47	0.00	0.47	0.98	0.495	1.05	0.470	1.10	1.30	0.567	No
124	8.17	0.47	0.01	0.47	0.98	0.498	1.05	0.472	1.10	1.30	0.570	No
125	8.21	0.48	0.01	0.47	0.98	0.500	1.05	0.474	1.10	1.30	0.572	No
126	8.30	0.48	0.01	0.47	0.98	0.502	1.05	0.476	1.10	1.30	0.575	No
127	8.36	0.49	0.01	0.47	0.98	0.504	1.05	0.478	1.10	1.30	0.577	No
128	8.41	0.49	0.01	0.48	0.98	0.505	1.05	0.479	1.10	1.30	0.578	No
129	8.50	0.49	0.02	0.48	0.98	0.508	1.05	0.482	1.10	1.30	0.581	No
130	8.56	0.50	0.02	0.48	0.98	0.510	1.05	0.484	1.10	1.30	0.583	No
131	8.61	0.50	0.02	0.48	0.98	0.511	1.05	0.485	1.10	1.30	0.585	No
132	8.66	0.50	0.02	0.48	0.98	0.513	1.05	0.486	1.10	1.30	0.586	No
133	8.73	0.51	0.02	0.48	0.98	0.515	1.05	0.488	1.10	1.30	0.589	No
134	8.81	0.51	0.03	0.49	0.98	0.517	1.05	0.490	1.10	1.30	0.592	No
135	8.86	0.52	0.03	0.49	0.98	0.518	1.05	0.492	1.10	1.30	0.594	No
136	8.96	0.52	0.03	0.49	0.98	0.521	1.05	0.494	1.10	1.30	0.599	No
137	9.01	0.52	0.03	0.49	0.98	0.523	1.05	0.496	1.10	1.30	0.602	No
138	9.06	0.53	0.03	0.49	0.98	0.524	1.05	0.497	1.09	1.30	0.607	No
139	9.13	0.53	0.04	0.50	0.98	0.526	1.05	0.499	1.09	1.30	0.611	No
140	9.20	0.54	0.04	0.50	0.98	0.528	1.05	0.501	1.09	1.30	0.616	No
141	9.30	0.54	0.04	0.50	0.98	0.531	1.05	0.503	1.08	1.30	0.623	No
142	9.35	0.54	0.04	0.50	0.98	0.532	1.05	0.505	1.08	1.30	0.628	No
143	9.40	0.55	0.04	0.50	0.98	0.533	1.05	0.506	1.08	1.30	0.633	No
144	9.46	0.55	0.05	0.51	0.98	0.535	1.05	0.507	1.08	1.30	0.637	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	9.55	0.56	0.05	0.51	0.98	0.537	1.05	0.509	1.07	1.30	0.642	No
146	9.60	0.56	0.05	0.51	0.98	0.538	1.05	0.511	1.07	1.30	0.644	No
147	9.66	0.56	0.05	0.51	0.98	0.540	1.05	0.512	1.07	1.30	0.646	No
148	9.71	0.57	0.05	0.51	0.98	0.541	1.05	0.513	1.07	1.30	0.647	No
149	9.80	0.57	0.06	0.51	0.98	0.543	1.05	0.515	1.07	1.30	0.647	No
150	9.85	0.57	0.06	0.52	0.98	0.545	1.05	0.517	1.07	1.30	0.648	No
151	9.93	0.58	0.06	0.52	0.98	0.547	1.05	0.518	1.07	1.30	0.651	No
152	9.98	0.58	0.06	0.52	0.98	0.548	1.05	0.520	1.07	1.30	0.653	No
153	10.04	0.58	0.06	0.52	0.98	0.549	1.05	0.521	1.07	1.30	0.654	No
154	10.12	0.59	0.07	0.52	0.98	0.551	1.05	0.523	1.07	1.30	0.657	No
155	10.19	0.59	0.07	0.52	0.98	0.553	1.05	0.525	1.07	1.30	0.660	No
156	10.25	0.60	0.07	0.53	0.98	0.554	1.05	0.526	1.07	1.30	0.662	No
157	10.31	0.60	0.07	0.53	0.98	0.556	1.05	0.527	1.07	1.30	0.664	No
158	10.39	0.60	0.07	0.53	0.98	0.558	1.05	0.529	1.07	1.30	0.666	No
159	10.45	0.61	0.08	0.53	0.98	0.559	1.05	0.530	1.07	1.30	0.668	No
160	10.52	0.61	0.08	0.53	0.98	0.561	1.05	0.532	1.07	1.30	0.671	No
161	10.58	0.62	0.08	0.53	0.98	0.562	1.05	0.533	1.07	1.30	0.672	No
162	10.64	0.62	0.08	0.54	0.98	0.564	1.05	0.535	1.07	1.30	0.674	No
163	10.74	0.62	0.09	0.54	0.98	0.566	1.05	0.537	1.07	1.30	0.677	No
164	10.79	0.63	0.09	0.54	0.98	0.567	1.05	0.538	1.07	1.30	0.680	No
165	10.83	0.63	0.09	0.54	0.98	0.568	1.05	0.539	1.07	1.30	0.682	No
166	10.90	0.63	0.09	0.54	0.98	0.569	1.05	0.540	1.06	1.30	0.686	No
167	10.96	0.64	0.09	0.54	0.98	0.571	1.05	0.541	1.06	1.30	0.689	No
168	11.03	0.64	0.09	0.55	0.97	0.572	1.05	0.543	1.06	1.30	0.693	No
169	11.10	0.65	0.10	0.55	0.97	0.574	1.05	0.544	1.06	1.30	0.697	No
170	11.18	0.65	0.10	0.55	0.97	0.576	1.05	0.546	1.06	1.30	0.701	No
171	11.24	0.65	0.10	0.55	0.97	0.577	1.05	0.547	1.06	1.30	0.703	No
172	11.29	0.66	0.10	0.55	0.97	0.578	1.05	0.548	1.05	1.30	0.706	No
173	11.36	0.66	0.10	0.55	0.97	0.580	1.05	0.550	1.05	1.30	0.708	No
174	11.42	0.66	0.11	0.56	0.97	0.581	1.05	0.551	1.05	1.30	0.710	No
175	11.51	0.67	0.11	0.56	0.97	0.583	1.05	0.553	1.05	1.30	0.713	No
176	11.57	0.67	0.11	0.56	0.97	0.584	1.05	0.554	1.05	1.30	0.715	No
177	11.62	0.67	0.11	0.56	0.97	0.585	1.05	0.555	1.05	1.30	0.716	No
178	11.70	0.68	0.12	0.56	0.97	0.587	1.05	0.556	1.05	1.30	0.718	No
179	11.75	0.68	0.12	0.56	0.97	0.588	1.05	0.557	1.05	1.30	0.720	No
180	11.83	0.69	0.12	0.57	0.97	0.589	1.05	0.559	1.05	1.30	0.721	No
181	11.90	0.69	0.12	0.57	0.97	0.591	1.05	0.560	1.05	1.30	0.723	No
182	11.95	0.69	0.12	0.57	0.97	0.592	1.05	0.561	1.05	1.30	0.724	No
183	12.03	0.70	0.13	0.57	0.97	0.593	1.05	0.563	1.05	1.30	0.725	No
184	12.10	0.70	0.13	0.57	0.97	0.595	1.05	0.564	1.05	1.30	0.726	No
185	12.15	0.70	0.13	0.57	0.97	0.596	1.05	0.565	1.05	1.30	0.727	No
186	12.21	0.71	0.13	0.58	0.97	0.597	1.05	0.566	1.05	1.30	0.728	No
187	12.28	0.71	0.13	0.58	0.97	0.598	1.05	0.567	1.05	1.30	0.730	No
188	12.34	0.71	0.14	0.58	0.97	0.599	1.05	0.568	1.05	1.30	0.731	No
189	12.40	0.72	0.14	0.58	0.97	0.600	1.05	0.569	1.05	1.30	0.733	No
190	12.48	0.72	0.14	0.58	0.97	0.602	1.05	0.571	1.05	1.30	0.734	No
191	12.55	0.73	0.14	0.58	0.97	0.603	1.05	0.572	1.05	1.30	0.736	No
192	12.60	0.73	0.14	0.59	0.97	0.604	1.05	0.573	1.05	1.30	0.737	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	12.70	0.73	0.15	0.59	0.97	0.606	1.05	0.575	1.05	1.30	0.739	No
194	12.75	0.74	0.15	0.59	0.97	0.607	1.05	0.575	1.05	1.30	0.740	No
195	12.80	0.74	0.15	0.59	0.97	0.608	1.05	0.576	1.05	1.30	0.741	No
196	12.89	0.75	0.15	0.59	0.97	0.609	1.05	0.578	1.05	1.30	0.742	No
197	12.94	0.75	0.15	0.60	0.97	0.610	1.05	0.579	1.05	1.30	0.743	No
198	13.00	0.75	0.16	0.60	0.97	0.611	1.05	0.580	1.05	1.30	0.744	No
199	13.09	0.76	0.16	0.60	0.97	0.613	1.05	0.581	1.05	1.30	0.746	No
200	13.14	0.76	0.16	0.60	0.97	0.614	1.05	0.582	1.05	1.30	0.746	No
201	13.19	0.76	0.16	0.60	0.97	0.614	1.05	0.583	1.05	1.30	0.747	No
202	13.28	0.77	0.16	0.60	0.97	0.616	1.05	0.584	1.05	1.30	0.749	No
203	13.34	0.77	0.17	0.61	0.97	0.617	1.05	0.585	1.05	1.30	0.749	No
204	13.39	0.78	0.17	0.61	0.97	0.618	1.05	0.586	1.05	1.30	0.750	No
205	13.47	0.78	0.17	0.61	0.97	0.619	1.05	0.587	1.06	1.30	0.751	No
206	13.53	0.78	0.17	0.61	0.97	0.620	1.05	0.588	1.06	1.30	0.752	No
207	13.59	0.79	0.17	0.61	0.97	0.621	1.05	0.589	1.06	1.30	0.752	No
208	13.67	0.79	0.18	0.62	0.97	0.622	1.05	0.590	1.06	1.30	0.753	No
209	13.73	0.80	0.18	0.62	0.97	0.623	1.05	0.591	1.06	1.30	0.754	No
210	13.79	0.80	0.18	0.62	0.97	0.624	1.05	0.592	1.06	1.30	0.754	No
211	13.88	0.80	0.18	0.62	0.96	0.625	1.05	0.593	1.06	1.30	0.754	No
212	13.93	0.81	0.18	0.62	0.96	0.626	1.05	0.594	1.06	1.30	0.754	No
213	13.99	0.81	0.19	0.62	0.96	0.627	1.05	0.595	1.06	1.30	0.755	No
214	14.07	0.82	0.19	0.63	0.96	0.628	1.05	0.596	1.06	1.30	0.756	No
215	14.13	0.82	0.19	0.63	0.96	0.629	1.05	0.597	1.06	1.30	0.756	No
216	14.18	0.82	0.19	0.63	0.96	0.630	1.05	0.597	1.06	1.30	0.757	No
217	14.28	0.83	0.20	0.63	0.96	0.631	1.05	0.599	1.06	1.30	0.758	No
218	14.33	0.83	0.20	0.63	0.96	0.632	1.05	0.600	1.06	1.30	0.759	No
219	14.38	0.83	0.20	0.64	0.96	0.633	1.05	0.600	1.06	1.30	0.760	No
220	14.48	0.84	0.20	0.64	0.96	0.634	1.05	0.602	1.06	1.30	0.761	No
221	14.53	0.84	0.20	0.64	0.96	0.635	1.05	0.602	1.06	1.30	0.761	No
222	14.58	0.85	0.21	0.64	0.96	0.636	1.05	0.603	1.06	1.30	0.762	No
223	14.65	0.85	0.21	0.64	0.96	0.637	1.05	0.604	1.06	1.30	0.763	No
224	14.72	0.85	0.21	0.65	0.96	0.638	1.05	0.605	1.06	1.30	0.764	No
225	14.78	0.86	0.21	0.65	0.96	0.638	1.05	0.606	1.06	1.30	0.765	No
226	14.83	0.86	0.21	0.65	0.96	0.639	1.05	0.606	1.06	1.30	0.765	No
227	14.92	0.87	0.22	0.65	0.96	0.640	1.05	0.607	1.06	1.30	0.767	No
228	14.98	0.87	0.22	0.65	0.96	0.641	1.05	0.608	1.06	1.30	0.768	No
229	15.05	0.87	0.22	0.65	0.96	0.642	1.05	0.609	1.06	1.30	0.770	No
230	15.12	0.88	0.22	0.66	0.96	0.643	1.05	0.610	1.06	1.30	0.771	No
231	15.16	0.88	0.22	0.66	0.96	0.644	1.05	0.610	1.06	1.30	0.772	No
232	15.22	0.88	0.23	0.66	0.96	0.644	1.05	0.611	1.06	1.30	0.773	No
233	15.32	0.89	0.23	0.66	0.96	0.646	1.05	0.612	1.06	1.30	0.774	No
234	15.37	0.89	0.23	0.66	0.96	0.646	1.05	0.613	1.06	1.30	0.776	No
235	15.46	0.90	0.23	0.67	0.96	0.647	1.05	0.614	1.06	1.30	0.777	No
236	15.52	0.90	0.23	0.67	0.96	0.648	1.05	0.615	1.06	1.30	0.778	No
237	15.56	0.90	0.24	0.67	0.96	0.649	1.05	0.615	1.06	1.30	0.779	No
238	15.66	0.91	0.24	0.67	0.96	0.650	1.05	0.617	1.05	1.30	0.785	No
239	15.71	0.91	0.24	0.67	0.96	0.651	1.05	0.617	1.05	1.30	0.786	No
240	15.75	0.92	0.24	0.67	0.96	0.651	1.05	0.618	1.05	1.30	0.786	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	15.86	0.92	0.25	0.68	0.96	0.653	1.05	0.619	1.05	1.30	0.788	No
242	15.91	0.93	0.25	0.68	0.96	0.653	1.05	0.619	1.05	1.30	0.788	No
243	15.96	0.93	0.25	0.68	0.96	0.654	1.05	0.620	1.05	1.30	0.789	No
244	16.02	0.93	0.25	0.68	0.96	0.654	1.05	0.621	1.05	1.30	0.791	No
245	16.10	0.94	0.25	0.68	0.96	0.655	1.05	0.622	1.05	1.30	0.792	No
246	16.16	0.94	0.25	0.69	0.96	0.656	1.05	0.622	1.05	1.30	0.793	No
247	16.21	0.94	0.26	0.69	0.96	0.657	1.05	0.623	1.05	1.30	0.794	No
248	16.29	0.95	0.26	0.69	0.96	0.658	1.05	0.624	1.05	1.30	0.794	No
249	16.36	0.95	0.26	0.69	0.96	0.659	1.05	0.625	1.05	1.30	0.796	No
250	16.41	0.96	0.26	0.69	0.96	0.659	1.05	0.625	1.05	1.30	0.796	No
251	16.51	0.96	0.27	0.70	0.95	0.660	1.05	0.626	1.05	1.30	0.799	No
252	16.56	0.96	0.27	0.70	0.95	0.661	1.05	0.627	1.05	1.30	0.800	No
253	16.61	0.97	0.27	0.70	0.95	0.661	1.05	0.627	1.05	1.30	0.802	No
254	16.71	0.97	0.27	0.70	0.95	0.662	1.05	0.628	1.05	1.30	0.805	No
255	16.76	0.98	0.27	0.70	0.95	0.663	1.05	0.629	1.05	1.30	0.807	No
256	16.81	0.98	0.27	0.70	0.95	0.664	1.05	0.629	1.04	1.30	0.810	No
257	16.89	0.98	0.28	0.71	0.95	0.664	1.05	0.630	1.04	1.30	0.815	No
258	16.95	0.99	0.28	0.71	0.95	0.665	1.05	0.631	1.04	1.30	0.818	No
259	17.00	0.99	0.28	0.71	0.95	0.666	1.05	0.631	1.04	1.30	0.822	No
260	17.10	1.00	0.28	0.71	0.95	0.667	1.05	0.632	1.04	1.30	0.827	No
261	17.14	1.00	0.29	0.71	0.95	0.667	1.05	0.633	1.04	1.30	0.828	No
262	17.20	1.00	0.29	0.71	0.95	0.668	1.05	0.633	1.03	1.30	0.830	No
263	17.29	1.01	0.29	0.72	0.95	0.669	1.05	0.634	1.03	1.30	0.832	No
264	17.33	1.01	0.29	0.72	0.95	0.669	1.05	0.635	1.03	1.30	0.833	No
265	17.39	1.01	0.29	0.72	0.95	0.670	1.05	0.635	1.03	1.30	0.834	No
266	17.46	1.02	0.30	0.72	0.95	0.671	1.05	0.636	1.03	1.30	0.836	No
267	17.52	1.02	0.30	0.72	0.95	0.671	1.05	0.637	1.03	1.30	0.837	No
268	17.59	1.02	0.30	0.72	0.95	0.672	1.05	0.637	1.03	1.30	0.838	No
269	17.70	1.03	0.30	0.73	0.95	0.673	1.05	0.639	1.03	1.30	0.840	No
270	17.72	1.03	0.30	0.73	0.95	0.673	1.05	0.639	1.03	1.30	0.840	No
271	17.80	1.04	0.31	0.73	0.95	0.674	1.05	0.640	1.03	1.30	0.841	No
272	17.85	1.04	0.31	0.73	0.95	0.675	1.05	0.640	1.03	1.30	0.841	No
273	17.92	1.04	0.31	0.73	0.95	0.676	1.05	0.641	1.03	1.30	0.842	No
274	17.99	1.05	0.31	0.73	0.95	0.676	1.05	0.641	1.03	1.30	0.841	No
275	18.05	1.05	0.31	0.74	0.95	0.677	1.05	0.642	1.03	1.30	0.841	No
276	18.14	1.06	0.32	0.74	0.95	0.678	1.05	0.643	1.03	1.30	0.841	No
277	18.18	1.06	0.32	0.74	0.95	0.678	1.05	0.643	1.03	1.30	0.840	No
278	18.25	1.06	0.32	0.74	0.95	0.679	1.05	0.644	1.04	1.30	0.839	No
279	18.32	1.07	0.32	0.74	0.95	0.679	1.05	0.644	1.04	1.30	0.838	No
280	18.39	1.07	0.32	0.75	0.95	0.680	1.05	0.645	1.04	1.30	0.836	No
281	18.45	1.07	0.33	0.75	0.95	0.681	1.05	0.645	1.04	1.30	0.836	No
282	18.50	1.08	0.33	0.75	0.95	0.681	1.05	0.646	1.04	1.30	0.836	No
283	18.57	1.08	0.33	0.75	0.95	0.682	1.05	0.647	1.04	1.30	0.837	No
284	18.64	1.09	0.33	0.75	0.95	0.682	1.05	0.647	1.04	1.30	0.837	No
285	18.73	1.09	0.33	0.76	0.95	0.683	1.05	0.648	1.04	1.30	0.837	No
286	18.78	1.09	0.34	0.76	0.95	0.684	1.05	0.648	1.04	1.30	0.837	No
287	18.85	1.10	0.34	0.76	0.95	0.684	1.05	0.649	1.04	1.30	0.838	No
288	18.91	1.10	0.34	0.76	0.95	0.685	1.05	0.649	1.04	1.30	0.839	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	18.97	1.10	0.34	0.76	0.94	0.685	1.05	0.650	1.04	1.30	0.840	No
290	19.03	1.11	0.34	0.76	0.94	0.686	1.05	0.650	1.04	1.30	0.840	No
291	19.11	1.11	0.35	0.77	0.94	0.686	1.05	0.651	1.04	1.30	0.840	No
292	19.17	1.12	0.35	0.77	0.94	0.687	1.05	0.651	1.04	1.30	0.841	No
293	19.23	1.12	0.35	0.77	0.94	0.687	1.05	0.652	1.04	1.30	0.841	No
294	19.31	1.12	0.35	0.77	0.94	0.688	1.05	0.652	1.04	1.30	0.842	No
295	19.39	1.13	0.36	0.77	0.94	0.689	1.05	0.653	1.04	1.30	0.843	No
296	19.43	1.13	0.36	0.78	0.94	0.689	1.05	0.653	1.04	1.30	0.843	No
297	19.49	1.14	0.36	0.78	0.94	0.689	1.05	0.654	1.04	1.30	0.843	No
298	19.57	1.14	0.36	0.78	0.94	0.690	1.05	0.654	1.04	1.30	0.845	No
299	19.65	1.15	0.36	0.78	0.94	0.691	1.05	0.655	1.04	1.30	0.849	No
300	19.69	1.15	0.36	0.78	0.94	0.691	1.05	0.655	1.03	1.30	0.850	No
301	19.79	1.15	0.37	0.79	0.94	0.692	1.05	0.656	1.03	1.30	0.858	No
302	19.83	1.16	0.37	0.79	0.94	0.692	1.05	0.656	1.03	1.30	0.860	No
303	19.89	1.16	0.37	0.79	0.94	0.692	1.05	0.657	1.03	1.30	0.864	No
304	19.97	1.17	0.37	0.79	0.94	0.693	1.05	0.657	1.03	1.30	0.866	No
305	20.03	1.17	0.38	0.79	0.94	0.693	1.05	0.658	1.03	1.30	0.870	No
306	20.08	1.17	0.38	0.79	0.94	0.694	1.05	0.658	1.02	1.30	0.871	No
307	20.17	1.18	0.38	0.80	0.94	0.695	1.05	0.659	1.02	1.30	0.873	No
308	20.23	1.18	0.38	0.80	0.94	0.695	1.05	0.659	1.02	1.30	0.874	No
309	20.28	1.18	0.38	0.80	0.94	0.695	1.05	0.660	1.02	1.30	0.875	No
310	20.37	1.19	0.39	0.80	0.94	0.696	1.05	0.660	1.02	1.30	0.877	No
311	20.42	1.19	0.39	0.80	0.94	0.697	1.05	0.661	1.02	1.30	0.877	No
312	20.47	1.19	0.39	0.80	0.94	0.697	1.05	0.661	1.02	1.30	0.878	No
313	20.55	1.20	0.39	0.81	0.94	0.698	1.05	0.662	1.02	1.30	0.879	No
314	20.63	1.20	0.39	0.81	0.94	0.698	1.05	0.662	1.02	1.30	0.880	No
315	20.67	1.20	0.40	0.81	0.94	0.699	1.05	0.663	1.02	1.30	0.880	No
316	20.77	1.21	0.40	0.81	0.94	0.699	1.05	0.663	1.02	1.30	0.882	No
317	20.82	1.21	0.40	0.81	0.94	0.700	1.05	0.664	1.02	1.30	0.882	No
318	20.88	1.22	0.40	0.81	0.94	0.700	1.05	0.664	1.02	1.30	0.883	No
319	20.96	1.22	0.40	0.82	0.94	0.701	1.05	0.665	1.02	1.30	0.884	No
320	21.01	1.22	0.41	0.82	0.94	0.701	1.05	0.665	1.02	1.30	0.885	No
321	21.06	1.23	0.41	0.82	0.94	0.702	1.05	0.665	1.02	1.30	0.885	No
322	21.17	1.23	0.41	0.82	0.94	0.702	1.05	0.666	1.02	1.30	0.886	No
323	21.21	1.23	0.41	0.82	0.94	0.703	1.05	0.666	1.02	1.30	0.887	No
324	21.26	1.24	0.41	0.82	0.94	0.703	1.05	0.667	1.02	1.30	0.887	No
325	21.33	1.24	0.42	0.83	0.93	0.704	1.05	0.667	1.02	1.30	0.888	No
326	21.40	1.25	0.42	0.83	0.93	0.704	1.05	0.668	1.02	1.30	0.888	No
327	21.46	1.25	0.42	0.83	0.93	0.705	1.05	0.668	1.02	1.30	0.889	No
328	21.55	1.25	0.42	0.83	0.93	0.705	1.05	0.669	1.02	1.30	0.889	No
329	21.61	1.26	0.42	0.83	0.93	0.705	1.05	0.669	1.02	1.30	0.890	No
330	21.66	1.26	0.43	0.83	0.93	0.706	1.05	0.669	1.02	1.30	0.890	No
331	21.75	1.27	0.43	0.84	0.93	0.706	1.05	0.670	1.02	1.30	0.891	No
332	21.81	1.27	0.43	0.84	0.93	0.707	1.05	0.670	1.02	1.30	0.892	No
333	21.86	1.27	0.43	0.84	0.93	0.707	1.05	0.671	1.02	1.30	0.892	No
334	21.94	1.28	0.43	0.84	0.93	0.708	1.05	0.671	1.02	1.30	0.893	No
335	22.00	1.28	0.44	0.84	0.93	0.708	1.05	0.672	1.02	1.30	0.894	No
336	22.06	1.28	0.44	0.85	0.93	0.708	1.05	0.672	1.02	1.30	0.895	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	22.14	1.29	0.44	0.85	0.93	0.709	1.05	0.672	1.02	1.30	0.896	No
338	22.20	1.29	0.44	0.85	0.93	0.709	1.05	0.673	1.02	1.30	0.896	No
339	22.25	1.29	0.44	0.85	0.93	0.710	1.05	0.673	1.02	1.30	0.897	No
340	22.34	1.30	0.45	0.85	0.93	0.710	1.05	0.674	1.02	1.30	0.898	No
341	22.40	1.30	0.45	0.85	0.93	0.711	1.05	0.674	1.02	1.30	0.898	No
342	22.47	1.31	0.45	0.86	0.93	0.711	1.05	0.674	1.02	1.30	0.899	No
343	22.52	1.31	0.45	0.86	0.93	0.711	1.05	0.675	1.02	1.30	0.899	No
344	22.61	1.32	0.46	0.86	0.93	0.712	1.05	0.675	1.02	1.30	0.900	No
345	22.67	1.32	0.46	0.86	0.93	0.712	1.05	0.675	1.02	1.30	0.901	No
346	22.72	1.32	0.46	0.86	0.93	0.712	1.05	0.676	1.02	1.30	0.901	No
347	22.78	1.33	0.46	0.86	0.93	0.713	1.05	0.676	1.02	1.30	0.902	No
348	22.86	1.33	0.46	0.87	0.93	0.713	1.05	0.676	1.02	1.30	0.902	No
349	22.92	1.33	0.47	0.87	0.93	0.713	1.05	0.677	1.02	1.30	0.903	No
350	22.97	1.34	0.47	0.87	0.93	0.714	1.05	0.677	1.02	1.30	0.903	No
351	23.06	1.34	0.47	0.87	0.93	0.714	1.05	0.677	1.02	1.30	0.904	No
352	23.12	1.35	0.47	0.87	0.93	0.715	1.05	0.678	1.02	1.30	0.905	No
353	23.17	1.35	0.47	0.88	0.93	0.715	1.05	0.678	1.02	1.30	0.905	No
354	23.26	1.35	0.48	0.88	0.93	0.715	1.05	0.678	1.02	1.30	0.906	No
355	23.31	1.36	0.48	0.88	0.93	0.716	1.05	0.679	1.02	1.30	0.906	No
356	23.41	1.36	0.48	0.88	0.93	0.716	1.05	0.679	1.02	1.30	0.906	No
357	23.46	1.37	0.48	0.88	0.93	0.716	1.05	0.679	1.02	1.30	0.907	No
358	23.51	1.37	0.48	0.88	0.93	0.717	1.05	0.680	1.02	1.30	0.907	No
359	23.56	1.37	0.49	0.89	0.93	0.717	1.05	0.680	1.02	1.30	0.908	No
360	23.65	1.38	0.49	0.89	0.92	0.717	1.05	0.680	1.02	1.30	0.909	No
361	23.71	1.38	0.49	0.89	0.92	0.717	1.05	0.680	1.01	1.30	0.909	No
362	23.75	1.38	0.49	0.89	0.92	0.718	1.05	0.681	1.01	1.30	0.910	No
363	23.85	1.39	0.49	0.89	0.92	0.718	1.05	0.681	1.01	1.30	0.911	No
364	23.91	1.39	0.50	0.90	0.92	0.718	1.05	0.681	1.01	1.30	0.911	No
365	23.95	1.40	0.50	0.90	0.92	0.719	1.05	0.682	1.01	1.30	0.912	No
366	24.04	1.40	0.50	0.90	0.92	0.719	1.05	0.682	1.01	1.30	0.913	No
367	24.10	1.40	0.50	0.90	0.92	0.719	1.05	0.682	1.01	1.30	0.913	No
368	24.15	1.41	0.50	0.90	0.92	0.720	1.05	0.682	1.01	1.30	0.913	No
369	24.25	1.41	0.51	0.91	0.92	0.720	1.05	0.683	1.01	1.30	0.914	No
370	24.30	1.42	0.51	0.91	0.92	0.720	1.05	0.683	1.01	1.30	0.914	No
371	24.36	1.42	0.51	0.91	0.92	0.720	1.05	0.683	1.01	1.30	0.914	No
372	24.45	1.42	0.51	0.91	0.92	0.721	1.05	0.684	1.01	1.30	0.915	No
373	24.50	1.43	0.51	0.91	0.92	0.721	1.05	0.684	1.01	1.30	0.916	No
374	24.55	1.43	0.52	0.91	0.92	0.721	1.05	0.684	1.01	1.30	0.916	No
375	24.64	1.44	0.52	0.92	0.92	0.722	1.05	0.684	1.01	1.30	0.917	No
376	24.69	1.44	0.52	0.92	0.92	0.722	1.05	0.685	1.01	1.30	0.917	No
377	24.75	1.44	0.52	0.92	0.92	0.722	1.05	0.685	1.01	1.30	0.917	No
378	24.84	1.45	0.53	0.92	0.92	0.722	1.05	0.685	1.01	1.30	0.916	No
379	24.89	1.45	0.53	0.92	0.92	0.723	1.05	0.685	1.01	1.30	0.915	No
380	24.95	1.45	0.53	0.93	0.92	0.723	1.05	0.686	1.01	1.30	0.913	No
381	25.02	1.46	0.53	0.93	0.92	0.723	1.05	0.686	1.01	1.30	0.910	No
382	25.07	1.46	0.53	0.93	0.92	0.723	1.05	0.686	1.01	1.30	0.909	No
383	25.14	1.47	0.53	0.93	0.92	0.724	1.05	0.686	1.01	1.30	0.906	No
384	25.23	1.47	0.54	0.93	0.92	0.724	1.05	0.687	1.01	1.30	0.906	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	25.29	1.47	0.54	0.94	0.92	0.724	1.05	0.687	1.01	1.30	0.906	No
386	25.36	1.48	0.54	0.94	0.92	0.724	1.05	0.687	1.01	1.30	0.908	No
387	25.41	1.48	0.54	0.94	0.92	0.724	1.05	0.687	1.01	1.30	0.909	No
388	25.48	1.49	0.55	0.94	0.92	0.725	1.05	0.687	1.01	1.30	0.912	No
389	25.55	1.49	0.55	0.94	0.92	0.725	1.05	0.688	1.01	1.30	0.915	No
390	25.61	1.49	0.55	0.94	0.92	0.725	1.05	0.688	1.01	1.30	0.919	No
391	25.66	1.50	0.55	0.95	0.92	0.725	1.05	0.688	1.01	1.30	0.921	No
392	25.75	1.50	0.55	0.95	0.92	0.726	1.05	0.688	1.01	1.30	0.923	No
393	25.80	1.51	0.56	0.95	0.92	0.726	1.05	0.688	1.01	1.30	0.924	No
394	25.86	1.51	0.56	0.95	0.92	0.726	1.05	0.689	1.01	1.30	0.925	No
395	25.94	1.51	0.56	0.95	0.91	0.726	1.05	0.689	1.01	1.30	0.926	No
396	25.99	1.52	0.56	0.96	0.91	0.727	1.05	0.689	1.01	1.30	0.927	No
397	26.06	1.52	0.56	0.96	0.91	0.727	1.05	0.689	1.01	1.30	0.927	No
398	26.12	1.52	0.57	0.96	0.91	0.727	1.05	0.690	1.01	1.30	0.928	No
399	26.19	1.53	0.57	0.96	0.91	0.727	1.05	0.690	1.01	1.30	0.928	No
400	26.25	1.53	0.57	0.96	0.91	0.728	1.05	0.690	1.01	1.30	0.929	No
401	26.34	1.54	0.57	0.96	0.91	0.728	1.05	0.691	1.01	1.30	0.929	No
402	26.38	1.54	0.57	0.97	0.91	0.728	1.05	0.691	1.01	1.30	0.930	No
403	26.45	1.54	0.58	0.97	0.91	0.728	1.05	0.691	1.01	1.30	0.930	No
404	26.54	1.55	0.58	0.97	0.91	0.729	1.05	0.691	1.01	1.30	0.931	No
405	26.59	1.55	0.58	0.97	0.91	0.729	1.05	0.691	1.01	1.30	0.931	No
406	26.65	1.55	0.58	0.97	0.91	0.729	1.05	0.692	1.01	1.30	0.931	No
407	26.71	1.56	0.58	0.97	0.91	0.729	1.05	0.692	1.01	1.30	0.932	No
408	26.78	1.56	0.59	0.98	0.91	0.730	1.05	0.692	1.01	1.30	0.932	No
409	26.84	1.57	0.59	0.98	0.91	0.730	1.05	0.692	1.01	1.30	0.931	No
410	26.94	1.57	0.59	0.98	0.91	0.730	1.05	0.692	1.01	1.30	0.930	No
411	26.98	1.57	0.59	0.98	0.91	0.730	1.05	0.693	1.01	1.30	0.930	No
412	27.04	1.58	0.59	0.98	0.91	0.730	1.05	0.693	1.01	1.30	0.931	No
413	27.11	1.58	0.60	0.99	0.91	0.731	1.05	0.693	1.01	1.30	0.932	No
414	27.18	1.59	0.60	0.99	0.91	0.731	1.05	0.693	1.01	1.30	0.932	No
415	27.23	1.59	0.60	0.99	0.91	0.731	1.05	0.693	1.01	1.30	0.933	No
416	27.32	1.59	0.60	0.99	0.91	0.731	1.05	0.693	1.01	1.30	0.935	No
417	27.38	1.60	0.60	0.99	0.91	0.731	1.05	0.694	1.01	1.30	0.935	No
418	27.43	1.60	0.61	0.99	0.91	0.732	1.05	0.694	1.01	1.30	0.936	No
419	27.52	1.61	0.61	1.00	0.91	0.732	1.05	0.694	1.01	1.30	0.937	No
420	27.58	1.61	0.61	1.00	0.91	0.732	1.05	0.694	1.00	1.30	0.938	No
421	27.63	1.61	0.61	1.00	0.91	0.732	1.05	0.694	1.00	1.30	0.938	No
422	27.73	1.62	0.62	1.00	0.91	0.733	1.05	0.695	1.00	1.30	0.939	No
423	27.78	1.62	0.62	1.00	0.91	0.733	1.05	0.695	1.00	1.30	0.939	No
424	27.83	1.62	0.62	1.00	0.91	0.733	1.05	0.695	1.00	1.30	0.940	No
425	27.91	1.63	0.62	1.01	0.91	0.733	1.05	0.695	1.00	1.30	0.940	No
426	27.98	1.63	0.62	1.01	0.91	0.733	1.05	0.695	1.00	1.30	0.940	No
427	28.03	1.63	0.62	1.01	0.91	0.733	1.05	0.696	1.00	1.30	0.941	No
428	28.11	1.64	0.63	1.01	0.90	0.734	1.05	0.696	1.00	1.30	0.941	No
429	28.18	1.64	0.63	1.01	0.90	0.734	1.05	0.696	1.00	1.30	0.941	No
430	28.22	1.65	0.63	1.01	0.90	0.734	1.05	0.696	1.00	1.30	0.941	No
431	28.32	1.65	0.63	1.02	0.90	0.734	1.05	0.696	1.00	1.30	0.940	No
432	28.35	1.65	0.63	1.02	0.90	0.734	1.05	0.696	1.00	1.30	0.939	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
433	28.43	1.66	0.64	1.02	0.90	0.735	1.05	0.697	1.00	1.30	0.933	No
434	28.48	1.66	0.64	1.02	0.90	0.735	1.05	0.697	1.00	1.30	0.932	No
435	28.56	1.67	0.64	1.02	0.90	0.735	1.05	0.697	1.00	1.30	0.928	No
436	28.63	1.67	0.64	1.03	0.90	0.735	1.05	0.697	1.00	1.30	0.927	No
437	28.68	1.67	0.65	1.03	0.90	0.735	1.05	0.697	1.00	1.30	0.927	No
438	28.74	1.68	0.65	1.03	0.90	0.735	1.05	0.697	1.00	1.30	0.926	No
439	28.82	1.68	0.65	1.03	0.90	0.735	1.05	0.697	1.00	1.30	0.925	No
440	28.88	1.69	0.65	1.03	0.90	0.735	1.05	0.697	1.00	1.30	0.925	No
441	28.95	1.69	0.65	1.04	0.90	0.735	1.05	0.697	1.00	1.30	0.922	No
442	29.02	1.69	0.66	1.04	0.90	0.735	1.05	0.697	1.00	1.30	0.920	No
443	29.08	1.70	0.66	1.04	0.90	0.735	1.05	0.697	1.00	1.30	0.920	No
444	29.15	1.70	0.66	1.04	0.90	0.736	1.05	0.698	1.00	1.30	0.920	No
445	29.21	1.71	0.66	1.04	0.90	0.736	1.05	0.698	1.00	1.30	0.922	No
446	29.27	1.71	0.66	1.05	0.90	0.736	1.05	0.698	1.00	1.30	0.924	No
447	29.37	1.72	0.67	1.05	0.90	0.736	1.05	0.698	1.00	1.30	0.929	No
448	29.40	1.72	0.67	1.05	0.90	0.736	1.05	0.698	1.00	1.30	0.933	No
449	29.46	1.72	0.67	1.05	0.90	0.736	1.05	0.698	1.00	1.30	0.936	No
450	29.54	1.73	0.67	1.05	0.90	0.736	1.05	0.698	1.00	1.30	0.941	No
451	29.60	1.73	0.67	1.06	0.90	0.736	1.05	0.698	1.00	1.30	0.943	No
452	29.67	1.73	0.68	1.06	0.90	0.736	1.05	0.698	1.00	1.30	0.945	No
453	29.73	1.74	0.68	1.06	0.90	0.736	1.05	0.698	1.00	1.30	0.946	No
454	29.81	1.74	0.68	1.06	0.90	0.736	1.05	0.698	1.00	1.30	0.947	No
455	29.86	1.75	0.68	1.06	0.90	0.736	1.05	0.698	1.00	1.30	0.948	No
456	29.96	1.75	0.69	1.07	0.90	0.737	1.05	0.699	1.00	1.30	0.948	No
457	29.99	1.75	0.69	1.07	0.90	0.737	1.05	0.699	1.00	1.30	0.947	No
458	30.06	1.76	0.69	1.07	0.90	0.737	1.05	0.699	1.00	1.30	0.947	No
459	30.14	1.76	0.69	1.07	0.90	0.738	1.05	0.699	1.00	1.30	0.946	No
460	30.20	1.76	0.69	1.07	0.89	0.738	1.05	0.700	1.00	1.30	0.944	No
461	30.26	1.77	0.69	1.07	0.89	0.738	1.05	0.700	1.00	1.30	0.943	No
462	30.33	1.77	0.70	1.07	0.89	0.739	1.05	0.700	1.00	1.30	0.940	No
463	30.38	1.77	0.70	1.07	0.89	0.739	1.05	0.701	1.00	1.30	0.940	No

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR _{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.07	5.53	100.00	3.11	0.59	1.70	8.88	0.00	8.88	4.000	No	Yes	2.00
2	0.14	9.65	87.52	2.81	0.56	1.70	15.50	0.00	15.50	4.000	No	Yes	2.00
3	0.20	11.06	86.89	2.80	0.56	1.70	17.77	0.00	17.77	4.000	No	Yes	2.00
4	0.29	12.67	85.90	2.79	0.55	1.70	20.36	0.00	20.36	4.000	No	Yes	2.00
5	0.35	15.48	79.35	2.70	0.54	1.70	24.89	0.00	24.89	4.000	No	Yes	2.00
6	0.41	18.49	72.04	2.61	0.52	1.70	29.72	0.00	29.72	4.000	No	Yes	2.00
7	0.49	24.53	59.30	2.45	0.50	1.70	39.43	59.58	99.00	4.000	No	No	2.00
8	0.54	32.07	47.05	2.30	0.48	1.70	51.54	58.33	109.87	4.000	No	No	2.00
9	0.59	35.59	42.89	2.25	0.47	1.70	57.20	57.55	114.75	4.000	No	No	2.00
10	0.67	30.87	52.08	2.36	0.48	1.70	49.60	59.98	109.58	4.000	No	No	2.00
11	0.72	28.16	56.94	2.42	0.49	1.70	45.24	60.49	105.73	4.000	No	No	2.00
12	0.80	28.26	57.79	2.43	0.48	1.70	45.40	60.80	106.20	4.000	No	No	2.00
13	0.86	27.25	59.57	2.46	0.49	1.70	43.78	60.87	104.65	4.000	No	No	2.00
14	0.94	26.45	59.89	2.46	0.49	1.70	42.50	60.60	103.09	4.000	No	No	2.00
15	0.99	27.15	58.58	2.44	0.49	1.70	43.62	60.54	104.16	4.000	No	No	2.00
16	1.09	27.86	57.60	2.43	0.49	1.70	44.76	60.56	105.32	4.000	No	No	2.00
17	1.12	29.77	54.57	2.39	0.48	1.70	47.83	60.41	108.24	4.000	No	No	2.00
18	1.20	31.78	52.49	2.37	0.47	1.70	51.06	60.53	111.59	4.000	No	No	2.00
19	1.27	33.89	50.69	2.35	0.47	1.70	54.45	60.72	115.17	4.000	No	No	2.00
20	1.33	35.40	49.71	2.33	0.46	1.70	56.88	60.95	117.82	4.000	No	No	2.00
21	1.38	35.50	50.68	2.35	0.46	1.70	57.04	61.40	118.44	4.000	No	No	2.00
22	1.48	33.99	54.39	2.39	0.46	1.70	54.61	62.20	116.81	4.000	No	No	2.00
23	1.51	33.69	55.74	2.41	0.46	1.70	54.13	62.54	116.67	4.000	No	No	2.00
24	1.58	33.59	58.43	2.44	0.46	1.70	53.97	63.37	117.34	4.000	No	No	2.00
25	1.66	34.18	60.68	2.47	0.46	1.70	54.93	64.31	119.25	4.000	No	No	2.00
26	1.73	34.07	62.57	2.49	0.46	1.70	54.77	64.79	119.57	4.000	No	No	2.00
27	1.77	33.77	63.48	2.51	0.46	1.70	54.29	64.90	119.19	4.000	No	No	2.00
28	1.85	41.92	55.03	2.40	0.43	1.70	67.38	65.92	133.30	4.000	No	No	2.00
29	1.91	36.79	63.45	2.51	0.45	1.70	59.14	66.27	125.41	4.000	No	No	2.00
30	1.97	36.29	65.80	2.54	0.45	1.70	58.34	66.64	124.98	4.000	No	No	2.00
31	2.06	37.88	64.32	2.52	0.44	1.70	60.91	67.00	127.91	4.000	No	No	2.00
32	2.12	39.80	62.24	2.49	0.44	1.70	63.99	67.32	131.31	4.000	No	No	2.00
33	2.17	38.08	64.15	2.51	0.44	1.70	61.25	67.06	128.30	4.000	No	No	2.00
34	2.25	39.29	63.37	2.50	0.44	1.70	63.17	67.40	130.57	4.000	No	No	2.00
35	2.31	38.68	64.99	2.52	0.44	1.70	62.21	67.55	129.76	4.000	No	No	2.00
36	2.36	37.77	66.58	2.54	0.44	1.70	60.75	67.53	128.27	4.000	No	No	2.00
37	2.47	37.57	65.96	2.54	0.44	1.70	60.43	67.28	127.71	4.000	No	No	2.00
38	2.52	35.96	67.85	2.56	0.45	1.70	57.84	66.99	124.83	4.000	No	No	2.00
39	2.56	34.97	69.12	2.58	0.45	1.70	56.23	66.81	123.04	4.000	No	No	2.00
40	2.63	33.35	71.39	2.60	0.46	1.70	53.65	0.00	53.65	4.000	No	Yes	2.00
41	2.71	32.95	71.40	2.61	0.46	1.70	53.00	0.00	53.00	4.000	No	Yes	2.00
42	2.77	31.74	72.45	2.62	0.46	1.70	51.06	0.00	51.06	4.000	No	Yes	2.00
43	2.83	31.44	71.06	2.60	0.46	1.70	50.58	0.00	50.58	4.000	No	Yes	2.00
44	2.90	31.65	69.06	2.58	0.46	1.70	50.90	65.25	116.14	4.000	No	No	2.00
45	2.97	32.25	66.88	2.55	0.46	1.70	51.86	65.04	116.90	4.000	No	No	2.00
46	3.03	33.26	63.57	2.51	0.46	1.70	53.49	64.69	118.18	4.000	No	No	2.00
47	3.09	32.96	62.90	2.50	0.46	1.70	53.00	64.38	117.38	4.000	No	No	2.00
48	3.16	31.85	63.72	2.51	0.47	1.70	51.22	64.09	115.31	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	3.22	28.62	67.95	2.56	0.48	1.70	46.05	63.60	109.64	4.000	No	No	2.00
50	3.30	25.61	72.94	2.62	0.49	1.70	41.21	0.00	41.21	4.000	No	Yes	2.00
51	3.36	23.49	77.10	2.68	0.50	1.70	37.80	0.00	37.80	4.000	No	Yes	2.00
52	3.41	19.37	86.66	2.80	0.51	1.70	31.18	0.00	31.18	4.000	No	Yes	2.00
53	3.49	17.76	90.76	2.85	0.52	1.70	28.60	0.00	28.60	4.000	No	Yes	2.00
54	3.57	16.36	94.47	2.89	0.53	1.70	26.33	0.00	26.33	4.000	No	Yes	2.00
55	3.62	15.36	96.95	2.92	0.53	1.70	24.73	0.00	24.73	4.000	No	Yes	2.00
56	3.70	13.75	100.00	2.97	0.54	1.70	22.14	0.00	22.14	4.000	No	Yes	2.00
57	3.74	13.34	100.00	2.98	0.54	1.70	21.50	0.00	21.50	4.000	No	Yes	2.00
58	3.85	12.13	100.00	2.98	0.55	1.70	19.55	0.00	19.55	4.000	No	Yes	2.00
59	3.88	12.03	100.00	2.98	0.55	1.70	19.39	0.00	19.39	4.000	No	Yes	2.00
60	3.95	12.03	100.00	2.98	0.55	1.70	19.39	0.00	19.39	4.000	No	Yes	2.00
61	4.01	12.83	98.19	2.94	0.54	1.70	20.68	0.00	20.68	4.000	No	Yes	2.00
62	4.09	13.54	95.72	2.91	0.54	1.70	21.82	0.00	21.82	4.000	No	Yes	2.00
63	4.13	10.12	100.00	3.10	0.56	1.70	16.32	0.00	16.32	4.000	No	Yes	2.00
64	4.23	15.35	90.11	2.84	0.53	1.70	24.73	0.00	24.73	4.000	No	Yes	2.00
65	4.27	15.45	89.30	2.83	0.53	1.70	24.89	0.00	24.89	4.000	No	Yes	2.00
66	4.37	15.45	87.17	2.80	0.53	1.70	24.89	0.00	24.89	4.000	No	Yes	2.00
67	4.43	15.65	83.91	2.76	0.53	1.70	25.21	0.00	25.21	4.000	No	Yes	2.00
68	4.48	16.06	80.52	2.72	0.53	1.70	25.85	0.00	25.85	4.000	No	Yes	2.00
69	4.54	16.66	75.60	2.66	0.53	1.70	26.81	0.00	26.81	4.000	No	Yes	2.00
70	4.60	17.47	69.03	2.58	0.53	1.70	28.12	58.62	86.74	4.000	No	No	2.00
71	4.68	18.88	60.64	2.47	0.53	1.70	30.38	57.40	87.78	4.000	No	No	2.00
72	4.73	19.58	56.45	2.42	0.53	1.70	31.51	56.55	88.05	4.000	No	No	2.00
73	4.82	20.59	51.32	2.35	0.53	1.70	33.13	55.28	88.41	4.000	No	No	2.00
74	4.86	20.79	50.90	2.35	0.52	1.70	33.45	55.21	88.66	4.000	No	No	2.00
75	4.93	22.10	48.50	2.32	0.52	1.70	35.55	54.82	90.37	4.000	No	No	2.00
76	5.02	23.10	47.21	2.30	0.52	1.70	37.16	54.68	91.84	4.000	No	No	2.00
77	5.05	23.60	46.48	2.29	0.52	1.70	37.96	54.55	92.52	4.000	No	No	2.00
78	5.13	24.71	44.50	2.27	0.51	1.70	39.75	54.05	93.80	4.000	No	No	2.00
79	5.19	25.41	43.47	2.26	0.51	1.70	40.87	53.80	94.67	4.000	No	No	2.00
80	5.25	27.22	40.30	2.22	0.51	1.70	43.78	52.68	96.46	4.000	No	No	2.00
81	5.32	29.84	36.27	2.17	0.50	1.70	47.99	50.84	98.83	4.000	No	No	2.00
82	5.41	32.15	33.69	2.13	0.50	1.70	51.70	49.49	101.19	4.000	No	No	2.00
83	5.46	32.76	33.38	2.13	0.49	1.70	52.68	49.42	102.10	4.000	No	No	2.00
84	5.51	34.06	32.15	2.11	0.49	1.70	54.77	48.68	103.45	4.000	No	No	2.00
85	5.61	34.26	33.19	2.13	0.49	1.70	55.09	49.76	104.85	4.000	No	No	2.00
86	5.66	33.96	34.38	2.14	0.49	1.70	54.61	50.75	105.36	4.000	No	No	2.00
87	5.71	33.26	35.96	2.16	0.49	1.70	53.49	51.85	105.33	4.000	No	No	2.00
88	5.78	32.05	38.57	2.19	0.49	1.70	51.54	53.39	104.93	4.000	No	No	2.00
89	5.86	31.05	40.47	2.22	0.49	1.70	49.93	54.28	104.21	4.000	No	No	2.00
90	5.91	29.94	42.64	2.25	0.49	1.70	48.15	55.16	103.31	4.000	No	No	2.00
91	6.00	28.33	46.54	2.29	0.49	1.70	45.56	56.54	102.11	4.000	No	No	2.00
92	6.06	27.33	50.15	2.34	0.49	1.70	43.96	57.71	101.67	4.000	No	No	2.00
93	6.11	26.22	54.19	2.39	0.50	1.70	42.17	58.74	100.92	4.000	No	No	2.00
94	6.20	26.32	56.09	2.41	0.49	1.70	42.33	59.42	101.75	4.000	No	No	2.00
95	6.25	25.82	58.15	2.44	0.50	1.70	41.53	59.83	101.36	4.000	No	No	2.00
96	6.31	25.41	59.96	2.46	0.50	1.70	40.80	60.14	100.95	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	6.39	25.31	61.59	2.48	0.50	1.69	40.37	60.46	100.83	4.000	No	No	2.00
98	6.45	27.33	58.19	2.44	0.49	1.67	43.16	60.29	103.45	4.000	No	No	2.00
99	6.50	29.54	54.55	2.39	0.49	1.65	46.20	59.96	106.16	4.000	No	No	2.00
100	6.59	31.25	52.66	2.37	0.48	1.64	48.34	59.86	108.20	4.000	No	No	2.00
101	6.65	30.54	54.84	2.40	0.48	1.63	47.11	60.31	107.42	4.000	No	No	2.00
102	6.70	28.53	59.79	2.46	0.49	1.63	44.06	61.01	105.07	4.000	No	No	2.00
103	6.79	25.62	66.82	2.55	0.50	1.63	39.63	61.50	101.13	4.000	No	No	2.00
104	6.85	23.30	71.62	2.61	0.50	1.64	36.19	0.00	36.19	4.000	No	Yes	2.00
105	6.90	20.79	77.26	2.68	0.51	1.65	32.45	0.00	32.45	4.000	No	Yes	2.00
106	6.99	19.28	80.99	2.72	0.52	1.65	30.05	0.00	30.05	4.000	No	Yes	2.00
107	7.05	18.98	82.68	2.75	0.52	1.64	29.50	0.00	29.50	4.000	No	Yes	2.00
108	7.10	18.68	85.57	2.78	0.52	1.64	28.95	0.00	28.95	4.000	No	Yes	2.00
109	7.17	18.58	88.55	2.82	0.52	1.63	28.64	0.00	28.64	4.000	No	Yes	2.00
110	7.23	18.47	90.35	2.84	0.52	1.62	28.36	0.00	28.36	4.000	No	Yes	2.00
111	7.32	21.59	81.49	2.73	0.51	1.60	32.61	0.00	32.61	4.000	No	Yes	2.00
112	7.38	23.10	76.52	2.67	0.51	1.58	34.64	0.00	34.64	4.000	No	Yes	2.00
113	7.43	24.61	72.35	2.62	0.50	1.57	36.61	0.00	36.61	4.000	No	Yes	2.00
114	7.51	31.85	58.48	2.44	0.48	1.54	46.28	61.25	107.52	4.000	No	No	2.00
115	7.57	38.29	48.80	2.32	0.47	1.51	54.72	59.97	114.70	4.000	No	No	2.00
116	7.62	44.12	41.19	2.23	0.46	1.49	62.26	57.75	120.01	4.000	No	No	2.00
117	7.71	50.15	33.96	2.14	0.45	1.48	69.96	53.76	123.72	4.000	No	No	2.00
118	7.77	52.67	31.18	2.10	0.45	1.47	73.12	51.50	124.62	4.000	No	No	2.00
119	7.82	54.78	29.08	2.08	0.45	1.46	75.76	49.46	125.22	4.000	No	No	2.00
120	7.91	57.70	27.68	2.06	0.44	1.45	79.12	48.18	127.30	4.000	No	No	2.00
121	7.97	59.21	27.11	2.05	0.44	1.44	80.69	47.65	128.34	4.000	No	No	2.00
122	8.01	60.01	26.94	2.05	0.44	1.44	81.50	47.54	129.04	0.195	No	No	0.34
123	8.07	60.71	27.01	2.05	0.44	1.43	82.07	47.76	129.83	0.197	No	No	0.35
124	8.17	60.31	28.45	2.07	0.44	1.42	81.00	49.64	130.64	0.200	No	No	0.35
125	8.21	59.91	29.22	2.08	0.44	1.42	80.24	50.54	130.77	0.200	No	No	0.35
126	8.30	59.91	29.90	2.09	0.44	1.41	79.80	51.33	131.13	0.201	No	No	0.35
127	8.36	59.91	30.28	2.09	0.44	1.40	79.53	51.74	131.28	0.202	No	No	0.35
128	8.41	59.91	30.49	2.09	0.44	1.40	79.43	51.99	131.42	0.202	No	No	0.35
129	8.50	61.52	29.60	2.08	0.43	1.39	80.98	51.18	132.16	0.205	No	No	0.35
130	8.56	62.83	28.71	2.07	0.43	1.39	82.37	50.27	132.64	0.206	No	No	0.35
131	8.61	63.93	27.96	2.06	0.43	1.38	83.55	49.45	133.00	0.207	No	No	0.35
132	8.66	64.94	27.21	2.05	0.43	1.38	84.63	48.54	133.17	0.208	No	No	0.35
133	8.73	65.14	26.63	2.05	0.43	1.37	84.68	47.66	132.35	0.205	No	No	0.35
134	8.81	63.23	27.67	2.06	0.44	1.37	82.11	48.74	130.85	0.200	No	No	0.34
135	8.86	60.81	29.24	2.08	0.44	1.37	78.94	50.30	129.23	0.195	No	No	0.33
136	8.96	55.79	32.37	2.12	0.45	1.37	72.44	52.67	125.12	0.184	No	No	0.31
137	9.01	53.88	33.66	2.13	0.45	1.37	69.94	53.47	123.41	0.179	No	No	0.30
138	9.06	48.44	38.88	2.20	0.46	1.38	63.03	56.33	119.36	0.170	No	No	0.28
139	9.13	45.33	41.63	2.23	0.46	1.38	59.03	57.24	116.27	0.164	No	No	0.27
140	9.20	42.51	45.47	2.28	0.47	1.38	55.32	58.51	113.84	0.159	No	No	0.26
141	9.30	35.97	54.45	2.39	0.48	1.38	47.01	60.15	107.16	0.148	No	No	0.24
142	9.35	32.05	59.92	2.46	0.49	1.39	42.03	60.48	102.51	0.141	No	No	0.22
143	9.40	28.23	66.05	2.54	0.50	1.39	37.21	60.63	97.84	0.135	No	No	0.21
144	9.46	25.72	70.11	2.59	0.51	1.40	33.95	60.53	94.48	0.131	No	No	0.21

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	9.55	22.90	73.96	2.64	0.52	1.40	30.28	0.00	30.28	4.000	No	Yes	2.00
146	9.60	22.70	72.97	2.62	0.52	1.39	29.96	0.00	29.96	4.000	No	Yes	2.00
147	9.66	22.70	71.16	2.60	0.52	1.39	29.89	0.00	29.89	4.000	No	Yes	2.00
148	9.71	24.61	65.77	2.53	0.52	1.38	32.20	59.13	91.34	0.127	No	No	0.20
149	9.80	29.44	56.30	2.42	0.51	1.37	38.08	58.31	96.39	0.133	No	No	0.21
150	9.85	30.64	53.63	2.38	0.50	1.36	39.48	57.82	97.29	0.134	No	No	0.21
151	9.93	31.25	50.68	2.35	0.51	1.36	40.12	56.90	97.02	0.134	No	No	0.21
152	9.98	31.45	49.76	2.33	0.51	1.35	40.27	56.58	96.85	0.133	No	No	0.20
153	10.04	31.65	48.94	2.32	0.51	1.35	40.43	56.28	96.70	0.133	No	No	0.20
154	10.12	31.45	48.77	2.32	0.51	1.35	40.04	56.11	96.15	0.133	No	No	0.20
155	10.19	31.35	49.45	2.33	0.51	1.34	39.77	56.32	96.10	0.133	No	No	0.20
156	10.25	30.95	50.02	2.34	0.51	1.34	39.20	56.40	95.59	0.132	No	No	0.20
157	10.31	30.54	51.24	2.35	0.51	1.33	38.57	56.70	95.27	0.132	No	No	0.20
158	10.39	30.44	51.83	2.36	0.51	1.33	38.31	56.86	95.16	0.131	No	No	0.20
159	10.45	30.54	52.07	2.36	0.51	1.33	38.32	56.95	95.27	0.132	No	No	0.20
160	10.52	30.24	52.91	2.37	0.51	1.32	37.82	57.12	94.94	0.131	No	No	0.20
161	10.58	30.54	52.81	2.37	0.51	1.32	38.08	57.15	95.23	0.132	No	No	0.20
162	10.64	30.84	52.62	2.37	0.51	1.31	38.33	57.15	95.48	0.132	No	No	0.20
163	10.74	29.94	54.12	2.39	0.51	1.31	37.08	57.33	94.42	0.131	No	No	0.19
164	10.79	28.43	56.59	2.42	0.51	1.31	35.20	57.61	92.81	0.129	No	No	0.19
165	10.83	27.53	58.16	2.44	0.52	1.31	34.05	57.75	91.81	0.128	No	No	0.19
166	10.90	23.80	65.14	2.53	0.53	1.31	29.50	58.22	87.72	0.123	No	No	0.18
167	10.96	21.29	70.49	2.59	0.53	1.31	26.42	58.40	84.82	0.120	No	No	0.17
168	11.03	18.47	77.38	2.68	0.54	1.31	22.95	0.00	22.95	4.000	No	Yes	2.00
169	11.10	14.75	88.56	2.82	0.55	1.32	18.38	0.00	18.38	4.000	No	Yes	2.00
170	11.18	11.84	99.85	2.96	0.56	1.32	14.78	0.00	14.78	4.000	No	Yes	2.00
171	11.24	10.73	97.76	2.93	0.57	1.32	13.39	0.00	13.39	4.000	No	Yes	2.00
172	11.29	9.83	94.31	2.89	0.57	1.32	12.27	0.00	12.27	4.000	No	Yes	2.00
173	11.36	9.42	100.00	2.98	0.58	1.31	11.72	0.00	11.72	4.000	No	Yes	2.00
174	11.42	8.92	100.00	3.03	0.58	1.31	11.09	0.00	11.09	4.000	No	Yes	2.00
175	11.51	8.22	100.00	3.11	0.58	1.31	10.19	0.00	10.19	4.000	No	Yes	2.00
176	11.57	8.23	100.00	3.12	0.58	1.30	10.16	0.00	10.16	4.000	No	Yes	2.00
177	11.62	8.23	100.00	3.13	0.58	1.30	10.14	0.00	10.14	4.000	No	Yes	2.00
178	11.70	8.23	100.00	3.15	0.58	1.30	10.10	0.00	10.10	4.000	No	Yes	2.00
179	11.75	8.33	100.00	3.16	0.58	1.29	10.20	0.00	10.20	4.000	No	Yes	2.00
180	11.83	8.93	100.00	3.13	0.58	1.29	10.88	0.00	10.88	4.000	No	Yes	2.00
181	11.90	9.53	100.00	3.11	0.58	1.28	11.56	0.00	11.56	4.000	No	Yes	2.00
182	11.95	10.34	100.00	3.08	0.57	1.28	12.49	0.00	12.49	4.000	No	Yes	2.00
183	12.03	11.75	100.00	3.02	0.57	1.27	14.10	0.00	14.10	4.000	No	Yes	2.00
184	12.10	12.75	100.00	2.98	0.56	1.26	15.23	0.00	15.23	4.000	No	Yes	2.00
185	12.15	13.36	100.00	2.97	0.56	1.26	15.90	0.00	15.90	4.000	No	Yes	2.00
186	12.21	13.86	99.59	2.96	0.56	1.25	16.44	0.00	16.44	4.000	No	Yes	2.00
187	12.28	14.36	99.21	2.95	0.56	1.25	16.96	0.00	16.96	4.000	No	Yes	2.00
188	12.34	14.66	99.14	2.95	0.56	1.24	17.26	0.00	17.26	4.000	No	Yes	2.00
189	12.40	14.86	99.46	2.96	0.55	1.24	17.44	0.00	17.44	4.000	No	Yes	2.00
190	12.48	15.47	98.30	2.94	0.55	1.24	18.08	0.00	18.08	4.000	No	Yes	2.00
191	12.55	16.07	97.23	2.93	0.55	1.23	18.71	0.00	18.71	4.000	No	Yes	2.00
192	12.60	16.57	96.55	2.92	0.55	1.23	19.23	0.00	19.23	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	12.70	17.28	95.86	2.91	0.55	1.22	19.96	0.00	19.96	4.000	No	Yes	2.00
194	12.75	17.88	94.88	2.90	0.54	1.22	20.59	0.00	20.59	4.000	No	Yes	2.00
195	12.80	18.48	93.96	2.89	0.54	1.21	21.22	0.00	21.22	4.000	No	Yes	2.00
196	12.89	19.49	91.82	2.86	0.54	1.21	22.27	0.00	22.27	4.000	No	Yes	2.00
197	12.94	20.40	89.79	2.83	0.54	1.20	23.23	0.00	23.23	4.000	No	Yes	2.00
198	13.00	21.30	87.75	2.81	0.53	1.20	24.18	0.00	24.18	4.000	No	Yes	2.00
199	13.09	22.51	85.04	2.78	0.53	1.19	25.42	0.00	25.42	4.000	No	Yes	2.00
200	13.14	23.41	83.05	2.75	0.53	1.19	26.36	0.00	26.36	4.000	No	Yes	2.00
201	13.19	24.72	80.33	2.72	0.53	1.19	27.75	0.00	27.75	4.000	No	Yes	2.00
202	13.28	25.32	79.12	2.70	0.52	1.18	28.30	0.00	28.30	4.000	No	Yes	2.00
203	13.34	26.63	76.65	2.67	0.52	1.18	29.66	0.00	29.66	4.000	No	Yes	2.00
204	13.39	27.54	75.04	2.65	0.52	1.17	30.59	0.00	30.59	4.000	No	Yes	2.00
205	13.47	29.25	72.08	2.61	0.51	1.17	32.35	0.00	32.35	4.000	No	Yes	2.00
206	13.53	30.35	70.21	2.59	0.51	1.17	33.46	60.40	93.87	0.130	No	No	0.17
207	13.59	31.36	68.65	2.57	0.51	1.16	34.47	60.39	94.87	0.131	No	No	0.17
208	13.67	33.47	65.17	2.53	0.51	1.16	36.63	60.27	96.90	0.134	No	No	0.18
209	13.73	34.78	63.02	2.50	0.50	1.15	37.95	60.13	98.08	0.135	No	No	0.18
210	13.79	36.69	59.93	2.46	0.50	1.15	39.90	59.88	99.79	0.137	No	No	0.18
211	13.88	40.21	54.68	2.40	0.49	1.14	43.50	59.27	102.78	0.141	No	No	0.19
212	13.93	42.52	51.72	2.36	0.49	1.14	45.87	58.84	104.71	0.144	No	No	0.19
213	13.99	44.53	48.84	2.32	0.48	1.14	47.90	58.20	106.10	0.146	No	No	0.19
214	14.07	47.05	45.95	2.29	0.48	1.13	50.40	57.50	107.90	0.149	No	No	0.20
215	14.13	48.66	44.22	2.27	0.48	1.13	51.99	57.00	108.98	0.150	No	No	0.20
216	14.18	49.76	43.12	2.25	0.48	1.13	53.06	56.66	109.71	0.152	No	No	0.20
217	14.28	51.17	41.62	2.23	0.48	1.12	54.36	56.09	110.44	0.153	No	No	0.20
218	14.33	52.28	40.52	2.22	0.47	1.12	55.42	55.64	111.06	0.154	No	No	0.20
219	14.38	52.98	39.95	2.21	0.47	1.12	56.06	55.42	111.48	0.155	No	No	0.20
220	14.48	55.19	38.11	2.19	0.47	1.11	58.17	54.61	112.78	0.157	No	No	0.21
221	14.53	56.30	38.06	2.19	0.47	1.11	59.20	54.82	114.02	0.159	No	No	0.21
222	14.58	56.80	38.27	2.19	0.47	1.11	59.61	55.07	114.69	0.161	No	No	0.21
223	14.65	58.41	37.19	2.18	0.47	1.11	61.12	54.60	115.72	0.162	No	No	0.21
224	14.72	59.01	36.86	2.17	0.46	1.10	61.60	54.44	116.05	0.163	No	No	0.21
225	14.78	59.52	36.64	2.17	0.46	1.10	62.01	54.36	116.37	0.164	No	No	0.21
226	14.83	60.12	36.45	2.17	0.46	1.10	62.52	54.32	116.84	0.165	No	No	0.22
227	14.92	60.22	36.97	2.17	0.46	1.10	62.44	54.73	117.17	0.165	No	No	0.22
228	14.98	60.42	37.25	2.18	0.46	1.09	62.52	54.97	117.50	0.166	No	No	0.22
229	15.05	60.22	37.49	2.18	0.46	1.09	62.17	55.08	117.25	0.166	No	No	0.22
230	15.12	60.22	37.58	2.18	0.46	1.09	62.04	55.11	117.16	0.165	No	No	0.21
231	15.16	60.32	37.62	2.18	0.46	1.09	62.06	55.15	117.21	0.165	No	No	0.21
232	15.22	60.72	37.55	2.18	0.46	1.09	62.35	55.17	117.51	0.166	No	No	0.21
233	15.32	60.92	37.61	2.18	0.46	1.08	62.37	55.22	117.59	0.166	No	No	0.21
234	15.37	60.92	37.59	2.18	0.46	1.08	62.27	55.18	117.45	0.166	No	No	0.21
235	15.46	61.03	37.63	2.18	0.46	1.08	62.21	55.20	117.41	0.166	No	No	0.21
236	15.52	61.23	37.63	2.18	0.46	1.08	62.30	55.22	117.52	0.166	No	No	0.21
237	15.56	61.43	37.67	2.18	0.46	1.07	62.42	55.28	117.70	0.166	No	No	0.21
238	15.66	62.03	30.80	2.10	0.47	1.07	62.95	48.96	111.90	0.155	No	No	0.20
239	15.71	62.33	30.83	2.10	0.47	1.07	63.15	49.03	112.18	0.156	No	No	0.20
240	15.75	62.43	31.12	2.10	0.47	1.07	63.17	49.35	112.52	0.157	No	No	0.20

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	15.86	62.84	31.70	2.11	0.47	1.07	63.35	50.03	113.38	0.158	No	No	0.20
242	15.91	62.84	32.10	2.11	0.47	1.06	63.26	50.43	113.69	0.159	No	No	0.20
243	15.96	62.75	32.49	2.12	0.47	1.06	63.06	50.79	113.85	0.159	No	No	0.20
244	16.02	59.13	35.66	2.16	0.47	1.06	59.34	52.93	112.27	0.156	No	No	0.20
245	16.10	61.95	33.56	2.13	0.47	1.06	61.99	51.62	113.61	0.158	No	No	0.20
246	16.16	61.75	33.86	2.14	0.47	1.06	61.68	51.84	113.51	0.158	No	No	0.20
247	16.21	61.65	34.66	2.15	0.47	1.06	61.48	52.54	114.01	0.159	No	No	0.20
248	16.29	62.05	35.13	2.15	0.47	1.05	61.73	53.01	114.75	0.161	No	No	0.20
249	16.36	62.35	35.29	2.15	0.47	1.05	61.89	53.19	115.08	0.161	No	No	0.20
250	16.41	62.45	35.31	2.15	0.47	1.05	61.90	53.21	115.12	0.161	No	No	0.20
251	16.51	61.65	35.74	2.16	0.47	1.05	60.94	53.37	114.31	0.160	No	No	0.20
252	16.56	60.24	36.80	2.17	0.47	1.04	59.48	53.91	113.39	0.158	No	No	0.20
253	16.61	58.43	38.16	2.19	0.47	1.04	57.62	54.52	112.14	0.156	No	No	0.19
254	16.71	54.31	41.77	2.23	0.48	1.04	53.43	55.95	109.38	0.151	No	No	0.19
255	16.76	50.99	44.85	2.27	0.48	1.04	50.11	56.86	106.98	0.147	No	No	0.18
256	16.81	47.07	48.52	2.32	0.49	1.04	46.22	57.62	103.83	0.143	No	No	0.18
257	16.89	39.72	56.92	2.42	0.50	1.04	38.94	58.74	97.68	0.135	No	No	0.17
258	16.95	34.29	64.67	2.52	0.51	1.04	33.58	59.28	92.86	0.129	No	No	0.16
259	17.00	28.46	74.90	2.65	0.53	1.04	27.86	0.00	27.86	4.000	No	Yes	2.00
260	17.10	21.22	90.88	2.85	0.55	1.03	20.73	0.00	20.73	4.000	No	Yes	2.00
261	17.14	18.81	96.75	2.92	0.55	1.03	18.36	0.00	18.36	4.000	No	Yes	2.00
262	17.20	17.50	99.59	2.96	0.56	1.03	17.05	0.00	17.05	4.000	No	Yes	2.00
263	17.29	16.49	100.00	2.97	0.56	1.03	16.02	0.00	16.02	4.000	No	Yes	2.00
264	17.33	15.69	100.00	2.99	0.56	1.03	15.23	0.00	15.23	4.000	No	Yes	2.00
265	17.39	14.58	100.00	3.02	0.57	1.03	14.13	0.00	14.13	4.000	No	Yes	2.00
266	17.46	13.98	100.00	3.03	0.57	1.02	13.51	0.00	13.51	4.000	No	Yes	2.00
267	17.52	13.88	100.00	3.02	0.57	1.02	13.39	0.00	13.39	4.000	No	Yes	2.00
268	17.59	13.78	100.00	3.01	0.57	1.02	13.27	0.00	13.27	4.000	No	Yes	2.00
269	17.70	13.48	100.00	3.02	0.57	1.02	12.94	0.00	12.94	4.000	No	Yes	2.00
270	17.72	13.68	100.00	3.02	0.57	1.01	13.12	0.00	13.12	4.000	No	Yes	2.00
271	17.80	14.38	100.00	3.01	0.57	1.01	13.76	0.00	13.76	4.000	No	Yes	2.00
272	17.85	15.89	100.00	2.97	0.56	1.01	15.18	0.00	15.18	4.000	No	Yes	2.00
273	17.92	17.10	99.00	2.95	0.56	1.01	16.30	0.00	16.30	4.000	No	Yes	2.00
274	17.99	20.01	94.03	2.89	0.55	1.01	19.02	0.00	19.02	4.000	No	Yes	2.00
275	18.05	22.83	89.86	2.84	0.54	1.00	21.67	0.00	21.67	4.000	No	Yes	2.00
276	18.14	25.75	84.74	2.77	0.54	1.00	24.37	0.00	24.37	4.000	No	Yes	2.00
277	18.18	29.47	78.28	2.69	0.53	1.00	27.86	0.00	27.86	4.000	No	Yes	2.00
278	18.25	35.20	69.93	2.59	0.51	1.00	33.20	60.28	93.48	0.130	No	No	0.15
279	18.32	39.32	64.62	2.52	0.50	1.00	37.02	60.25	97.27	0.134	No	No	0.16
280	18.39	44.75	57.97	2.44	0.49	0.99	42.06	59.92	101.98	0.140	No	No	0.17
281	18.45	47.27	54.72	2.40	0.49	0.99	44.36	59.52	103.87	0.143	No	No	0.17
282	18.50	49.68	51.68	2.36	0.49	0.99	46.55	59.01	105.55	0.145	No	No	0.17
283	18.57	51.79	48.44	2.32	0.48	0.99	48.44	58.16	106.60	0.147	No	No	0.18
284	18.64	54.51	45.09	2.28	0.48	0.99	50.89	57.19	108.08	0.149	No	No	0.18
285	18.73	56.02	43.53	2.26	0.48	0.99	52.19	56.67	108.86	0.150	No	No	0.18
286	18.78	58.13	41.91	2.24	0.48	0.98	54.08	56.19	110.27	0.153	No	No	0.18
287	18.85	59.24	40.69	2.22	0.48	0.98	55.02	55.65	110.68	0.153	No	No	0.18
288	18.91	60.24	39.06	2.20	0.48	0.98	55.87	54.76	110.62	0.153	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	18.97	61.25	38.02	2.19	0.47	0.98	56.71	54.21	110.92	0.154	No	No	0.18
290	19.03	62.25	37.88	2.19	0.47	0.98	57.55	54.30	111.85	0.155	No	No	0.18
291	19.11	63.16	38.17	2.19	0.47	0.98	58.29	54.69	112.98	0.157	No	No	0.19
292	19.17	63.56	38.64	2.20	0.47	0.97	58.56	55.10	113.66	0.159	No	No	0.19
293	19.23	63.36	39.47	2.21	0.47	0.97	58.30	55.62	113.92	0.159	No	No	0.19
294	19.31	63.16	40.09	2.21	0.47	0.97	58.01	55.98	113.99	0.159	No	No	0.19
295	19.39	64.16	39.93	2.21	0.47	0.97	58.81	56.07	114.88	0.161	No	No	0.19
296	19.43	64.57	40.03	2.21	0.47	0.97	59.12	56.21	115.33	0.162	No	No	0.19
297	19.49	64.57	41.69	2.23	0.46	0.97	59.05	57.28	116.33	0.164	No	No	0.19
298	19.57	62.76	44.12	2.26	0.47	0.97	57.27	58.28	115.55	0.162	No	No	0.19
299	19.65	55.82	52.15	2.36	0.47	0.96	50.81	60.33	111.14	0.154	No	No	0.18
300	19.69	52.90	56.68	2.42	0.48	0.96	48.09	61.19	109.28	0.151	No	No	0.18
301	19.79	38.72	73.50	2.63	0.51	0.96	35.02	0.00	35.02	4.000	No	Yes	2.00
302	19.83	34.60	79.03	2.70	0.52	0.96	31.24	0.00	31.24	4.000	No	Yes	2.00
303	19.89	29.06	87.00	2.80	0.53	0.95	26.16	0.00	26.16	4.000	No	Yes	2.00
304	19.97	25.65	91.32	2.85	0.54	0.95	23.02	0.00	23.02	4.000	No	Yes	2.00
305	20.03	17.70	100.00	3.07	0.56	0.95	15.82	0.00	15.82	4.000	No	Yes	2.00
306	20.08	15.69	100.00	3.13	0.57	0.94	14.00	0.00	14.00	4.000	No	Yes	2.00
307	20.17	13.78	100.00	3.21	0.57	0.94	12.26	0.00	12.26	4.000	No	Yes	2.00
308	20.23	12.77	100.00	3.24	0.58	0.94	11.33	0.00	11.33	4.000	No	Yes	2.00
309	20.28	11.97	100.00	3.25	0.58	0.94	10.61	0.00	10.61	4.000	No	Yes	2.00
310	20.37	11.26	100.00	3.24	0.58	0.93	9.95	0.00	9.95	4.000	No	Yes	2.00
311	20.42	10.96	100.00	3.25	0.58	0.93	9.67	0.00	9.67	4.000	No	Yes	2.00
312	20.47	10.86	100.00	3.25	0.58	0.93	9.57	0.00	9.57	4.000	No	Yes	2.00
313	20.55	11.16	100.00	3.23	0.58	0.93	9.81	0.00	9.81	4.000	No	Yes	2.00
314	20.63	10.76	100.00	3.25	0.58	0.93	9.44	0.00	9.44	4.000	No	Yes	2.00
315	20.67	10.66	100.00	3.26	0.58	0.93	9.34	0.00	9.34	4.000	No	Yes	2.00
316	20.77	10.46	100.00	3.27	0.59	0.92	9.14	0.00	9.14	4.000	No	Yes	2.00
317	20.82	10.56	100.00	3.26	0.59	0.92	9.21	0.00	9.21	4.000	No	Yes	2.00
318	20.88	10.56	100.00	3.26	0.59	0.92	9.20	0.00	9.20	4.000	No	Yes	2.00
319	20.96	10.56	100.00	3.26	0.59	0.92	9.18	0.00	9.18	4.000	No	Yes	2.00
320	21.01	10.56	100.00	3.27	0.59	0.92	9.17	0.00	9.17	4.000	No	Yes	2.00
321	21.06	10.66	100.00	3.27	0.59	0.92	9.24	0.00	9.24	4.000	No	Yes	2.00
322	21.17	11.06	100.00	3.26	0.58	0.91	9.56	0.00	9.56	4.000	No	Yes	2.00
323	21.21	11.57	100.00	3.23	0.58	0.91	9.99	0.00	9.99	4.000	No	Yes	2.00
324	21.26	12.07	100.00	3.22	0.58	0.91	10.41	0.00	10.41	4.000	No	Yes	2.00
325	21.33	12.88	100.00	3.19	0.58	0.91	11.09	0.00	11.09	4.000	No	Yes	2.00
326	21.40	13.29	100.00	3.18	0.58	0.91	11.42	0.00	11.42	4.000	No	Yes	2.00
327	21.46	13.69	100.00	3.18	0.58	0.91	11.75	0.00	11.75	4.000	No	Yes	2.00
328	21.55	14.29	100.00	3.17	0.57	0.91	12.24	0.00	12.24	4.000	No	Yes	2.00
329	21.61	14.59	100.00	3.16	0.57	0.91	12.48	0.00	12.48	4.000	No	Yes	2.00
330	21.66	15.10	100.00	3.15	0.57	0.90	12.90	0.00	12.90	4.000	No	Yes	2.00
331	21.75	15.10	100.00	3.17	0.57	0.90	12.87	0.00	12.87	4.000	No	Yes	2.00
332	21.81	15.30	100.00	3.16	0.57	0.90	13.03	0.00	13.03	4.000	No	Yes	2.00
333	21.86	15.30	100.00	3.17	0.57	0.90	13.01	0.00	13.01	4.000	No	Yes	2.00
334	21.94	15.30	100.00	3.16	0.57	0.90	12.98	0.00	12.98	4.000	No	Yes	2.00
335	22.00	14.99	100.00	3.13	0.57	0.90	12.70	0.00	12.70	4.000	No	Yes	2.00
336	22.06	14.99	100.00	3.03	0.57	0.90	12.68	0.00	12.68	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	22.14	14.99	100.00	3.14	0.57	0.89	12.65	0.00	12.65	4.000	No	Yes	2.00
338	22.20	14.99	100.00	3.13	0.57	0.89	12.63	0.00	12.63	4.000	No	Yes	2.00
339	22.25	15.10	100.00	3.15	0.57	0.89	12.71	0.00	12.71	4.000	No	Yes	2.00
340	22.34	13.39	100.00	3.26	0.58	0.89	11.23	0.00	11.23	4.000	No	Yes	2.00
341	22.40	16.00	100.00	3.17	0.57	0.89	13.42	0.00	13.42	4.000	No	Yes	2.00
342	22.47	16.30	100.00	3.17	0.57	0.89	13.65	0.00	13.65	4.000	No	Yes	2.00
343	22.52	16.20	100.00	3.18	0.57	0.89	13.55	0.00	13.55	4.000	No	Yes	2.00
344	22.61	16.10	100.00	3.19	0.57	0.88	13.43	0.00	13.43	4.000	No	Yes	2.00
345	22.67	16.10	100.00	3.19	0.57	0.88	13.41	0.00	13.41	4.000	No	Yes	2.00
346	22.72	16.10	100.00	3.19	0.57	0.88	13.39	0.00	13.39	4.000	No	Yes	2.00
347	22.78	16.10	100.00	3.19	0.57	0.88	13.38	0.00	13.38	4.000	No	Yes	2.00
348	22.86	16.10	100.00	3.19	0.57	0.88	13.35	0.00	13.35	4.000	No	Yes	2.00
349	22.92	16.10	100.00	3.19	0.57	0.88	13.33	0.00	13.33	4.000	No	Yes	2.00
350	22.97	16.10	100.00	3.20	0.57	0.88	13.31	0.00	13.31	4.000	No	Yes	2.00
351	23.06	16.10	100.00	3.21	0.57	0.87	13.28	0.00	13.28	4.000	No	Yes	2.00
352	23.12	16.40	100.00	3.20	0.57	0.87	13.51	0.00	13.51	4.000	No	Yes	2.00
353	23.17	16.81	100.00	3.19	0.57	0.87	13.83	0.00	13.83	4.000	No	Yes	2.00
354	23.26	17.91	100.00	3.15	0.56	0.87	14.72	0.00	14.72	4.000	No	Yes	2.00
355	23.31	18.62	100.00	3.13	0.56	0.87	15.29	0.00	15.29	4.000	No	Yes	2.00
356	23.41	19.22	100.00	3.11	0.56	0.87	15.75	0.00	15.75	4.000	No	Yes	2.00
357	23.46	19.12	100.00	3.11	0.56	0.87	15.65	0.00	15.65	4.000	No	Yes	2.00
358	23.51	19.02	100.00	3.11	0.56	0.87	15.55	0.00	15.55	4.000	No	Yes	2.00
359	23.56	18.72	100.00	3.12	0.56	0.86	15.28	0.00	15.28	4.000	No	Yes	2.00
360	23.65	18.01	100.00	3.15	0.56	0.86	14.66	0.00	14.66	4.000	No	Yes	2.00
361	23.71	17.71	100.00	3.16	0.57	0.86	14.39	0.00	14.39	4.000	No	Yes	2.00
362	23.75	17.61	100.00	3.17	0.57	0.86	14.29	0.00	14.29	4.000	No	Yes	2.00
363	23.85	17.21	100.00	3.18	0.57	0.86	13.93	0.00	13.93	4.000	No	Yes	2.00
364	23.91	17.11	100.00	3.19	0.57	0.86	13.83	0.00	13.83	4.000	No	Yes	2.00
365	23.95	17.01	100.00	3.20	0.57	0.85	13.73	0.00	13.73	4.000	No	Yes	2.00
366	24.04	16.70	100.00	3.22	0.57	0.85	13.45	0.00	13.45	4.000	No	Yes	2.00
367	24.10	16.81	100.00	3.22	0.57	0.85	13.52	0.00	13.52	4.000	No	Yes	2.00
368	24.15	16.91	100.00	3.22	0.57	0.85	13.58	0.00	13.58	4.000	No	Yes	2.00
369	24.25	17.71	100.00	3.20	0.57	0.85	14.20	0.00	14.20	4.000	No	Yes	2.00
370	24.30	18.41	100.00	3.18	0.56	0.85	14.76	0.00	14.76	4.000	No	Yes	2.00
371	24.36	19.12	100.00	3.16	0.56	0.85	15.31	0.00	15.31	4.000	No	Yes	2.00
372	24.45	19.72	100.00	3.15	0.56	0.85	15.77	0.00	15.77	4.000	No	Yes	2.00
373	24.50	19.52	100.00	3.15	0.56	0.85	15.59	0.00	15.59	4.000	No	Yes	2.00
374	24.55	19.22	100.00	3.17	0.56	0.84	15.32	0.00	15.32	4.000	No	Yes	2.00
375	24.64	19.42	100.00	3.18	0.56	0.84	15.45	0.00	15.45	4.000	No	Yes	2.00
376	24.69	20.53	100.00	3.14	0.56	0.84	16.33	0.00	16.33	4.000	No	Yes	2.00
377	24.75	22.64	100.00	3.07	0.55	0.84	18.02	0.00	18.02	4.000	No	Yes	2.00
378	24.84	28.37	95.67	2.91	0.54	0.84	22.64	0.00	22.64	4.000	No	Yes	2.00
379	24.89	33.10	87.14	2.80	0.53	0.85	26.47	0.00	26.47	4.000	No	Yes	2.00
380	24.95	41.55	73.36	2.63	0.51	0.85	33.37	0.00	33.37	4.000	No	Yes	2.00
381	25.02	52.81	54.56	2.39	0.49	0.85	42.57	58.98	101.54	0.139	No	No	0.15
382	25.07	58.54	50.38	2.34	0.49	0.85	47.29	58.69	105.98	0.146	No	No	0.16
383	25.14	65.88	46.31	2.29	0.47	0.86	53.36	58.44	111.79	0.155	No	No	0.17
384	25.23	69.00	44.97	2.27	0.47	0.86	55.87	58.39	114.26	0.160	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	25.29	68.80	45.43	2.28	0.47	0.86	55.65	58.58	114.23	0.160	No	No	0.18
386	25.36	64.48	49.63	2.33	0.47	0.85	51.99	59.62	111.61	0.155	No	No	0.17
387	25.41	62.26	52.14	2.36	0.48	0.85	50.10	60.14	110.24	0.153	No	No	0.17
388	25.48	55.22	59.01	2.45	0.49	0.85	44.22	60.83	105.04	0.144	No	No	0.16
389	25.55	48.48	66.38	2.54	0.50	0.84	38.61	61.11	99.72	0.137	No	No	0.15
390	25.61	37.52	80.22	2.72	0.52	0.84	29.63	0.00	29.63	4.000	No	Yes	2.00
391	25.66	30.48	90.82	2.85	0.53	0.83	23.91	0.00	23.91	4.000	No	Yes	2.00
392	25.75	24.35	100.00	2.97	0.55	0.82	18.97	0.00	18.97	4.000	No	Yes	2.00
393	25.80	21.73	100.00	3.03	0.56	0.82	16.87	0.00	16.87	4.000	No	Yes	2.00
394	25.86	20.33	100.00	3.05	0.56	0.82	15.74	0.00	15.74	4.000	No	Yes	2.00
395	25.94	18.51	100.00	3.07	0.57	0.82	14.28	0.00	14.28	4.000	No	Yes	2.00
396	25.99	18.51	100.00	3.04	0.57	0.82	14.26	0.00	14.26	4.000	No	Yes	2.00
397	26.06	18.21	100.00	3.00	0.57	0.81	14.00	0.00	14.00	4.000	No	Yes	2.00
398	26.12	17.51	100.00	3.00	0.57	0.81	13.44	0.00	13.44	4.000	No	Yes	2.00
399	26.19	17.31	100.00	2.98	0.57	0.81	13.26	0.00	13.26	4.000	No	Yes	2.00
400	26.25	17.41	100.00	2.98	0.57	0.81	13.32	0.00	13.32	4.000	No	Yes	2.00
401	26.34	17.62	100.00	2.97	0.57	0.81	13.45	0.00	13.45	4.000	No	Yes	2.00
402	26.38	18.22	98.75	2.95	0.57	0.81	13.91	0.00	13.91	4.000	No	Yes	2.00
403	26.45	18.52	98.17	2.94	0.57	0.81	14.12	0.00	14.12	4.000	No	Yes	2.00
404	26.54	17.93	100.00	3.00	0.57	0.81	13.63	0.00	13.63	4.000	No	Yes	2.00
405	26.59	18.04	100.00	3.02	0.57	0.80	13.69	0.00	13.69	4.000	No	Yes	2.00
406	26.65	18.34	100.00	3.07	0.57	0.80	13.91	0.00	13.91	4.000	No	Yes	2.00
407	26.71	19.25	100.00	3.09	0.56	0.80	14.59	0.00	14.59	4.000	No	Yes	2.00
408	26.78	20.77	100.00	3.08	0.56	0.80	15.74	0.00	15.74	4.000	No	Yes	2.00
409	26.84	25.91	99.96	2.96	0.55	0.81	19.72	0.00	19.72	4.000	No	Yes	2.00
410	26.94	32.25	91.21	2.85	0.53	0.81	24.64	0.00	24.64	4.000	No	Yes	2.00
411	26.98	32.15	91.83	2.86	0.53	0.81	24.55	0.00	24.55	4.000	No	Yes	2.00
412	27.04	30.64	94.62	2.90	0.54	0.81	23.33	0.00	23.33	4.000	No	Yes	2.00
413	27.11	29.03	96.72	2.92	0.54	0.81	22.03	0.00	22.03	4.000	No	Yes	2.00
414	27.18	28.23	96.78	2.92	0.54	0.80	21.38	0.00	21.38	4.000	No	Yes	2.00
415	27.23	26.32	98.31	2.94	0.55	0.80	19.87	0.00	19.87	4.000	No	Yes	2.00
416	27.32	22.50	100.00	3.01	0.56	0.80	16.88	0.00	16.88	4.000	No	Yes	2.00
417	27.38	20.59	100.00	3.04	0.56	0.79	15.39	0.00	15.39	4.000	No	Yes	2.00
418	27.43	18.47	100.00	3.09	0.57	0.79	13.75	0.00	13.75	4.000	No	Yes	2.00
419	27.52	15.96	100.00	3.18	0.58	0.79	11.82	0.00	11.82	4.000	No	Yes	2.00
420	27.58	14.55	100.00	3.24	0.58	0.78	10.74	0.00	10.74	4.000	No	Yes	2.00
421	27.63	14.05	100.00	3.26	0.58	0.78	10.35	0.00	10.35	4.000	No	Yes	2.00
422	27.73	13.55	100.00	3.27	0.58	0.78	9.95	0.00	9.95	4.000	No	Yes	2.00
423	27.78	13.35	100.00	3.27	0.58	0.78	9.79	0.00	9.79	4.000	No	Yes	2.00
424	27.83	13.65	100.00	3.25	0.58	0.78	10.00	0.00	10.00	4.000	No	Yes	2.00
425	27.91	14.35	100.00	3.20	0.58	0.78	10.51	0.00	10.51	4.000	No	Yes	2.00
426	27.98	14.85	100.00	3.18	0.58	0.78	10.87	0.00	10.87	4.000	No	Yes	2.00
427	28.03	15.16	100.00	3.15	0.58	0.78	11.09	0.00	11.09	4.000	No	Yes	2.00
428	28.11	15.26	100.00	3.15	0.58	0.78	11.15	0.00	11.15	4.000	No	Yes	2.00
429	28.18	15.96	100.00	3.17	0.58	0.78	11.66	0.00	11.66	4.000	No	Yes	2.00
430	28.22	17.17	100.00	3.16	0.57	0.78	12.55	0.00	12.55	4.000	No	Yes	2.00
431	28.32	27.54	94.36	2.89	0.55	0.78	20.36	0.00	20.36	4.000	No	Yes	2.00
432	28.35	32.46	86.80	2.80	0.54	0.79	24.10	0.00	24.10	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	28.43	56.50	60.00	2.46	0.49	0.80	42.77	60.71	103.48	0.142	No	No	0.15
434	28.48	62.23	56.36	2.42	0.48	0.81	47.30	60.87	108.17	0.149	No	No	0.16
435	28.56	73.09	50.25	2.34	0.46	0.81	55.93	60.93	116.85	0.165	No	No	0.18
436	28.63	77.12	48.98	2.32	0.46	0.81	59.13	61.21	120.33	0.172	No	No	0.19
437	28.68	78.62	48.46	2.32	0.45	0.81	60.29	61.28	121.57	0.175	No	No	0.19
438	28.74	81.14	47.50	2.31	0.45	0.81	62.27	61.33	123.60	0.180	No	No	0.19
439	28.82	84.66	45.90	2.29	0.45	0.81	65.04	61.23	126.27	0.187	No	No	0.20
440	28.88	87.17	44.64	2.27	0.44	0.81	67.01	61.04	128.05	0.192	No	No	0.21
441	28.95	95.02	40.67	2.22	0.43	0.82	73.29	60.08	133.37	0.209	No	No	0.23
442	29.02	99.74	38.66	2.20	0.43	0.82	77.05	59.50	136.56	0.220	No	No	0.24
443	29.08	102.76	37.19	2.18	0.42	0.82	79.43	58.85	138.27	0.227	No	No	0.25
444	29.15	102.66	37.43	2.18	0.42	0.82	79.26	59.02	138.28	0.227	No	No	0.25
445	29.21	98.93	39.52	2.21	0.43	0.82	76.18	59.95	136.14	0.219	No	No	0.24
446	29.27	92.59	43.22	2.25	0.43	0.81	70.99	61.20	132.18	0.205	No	No	0.22
447	29.37	79.92	51.98	2.36	0.45	0.80	60.71	62.92	123.63	0.180	No	No	0.19
448	29.40	69.86	59.56	2.46	0.46	0.80	52.66	63.35	116.01	0.163	No	No	0.17
449	29.46	60.41	68.16	2.56	0.48	0.79	45.14	63.38	108.52	0.150	No	No	0.16
450	29.54	45.02	83.47	2.76	0.51	0.78	33.13	0.00	33.13	4.000	No	Yes	2.00
451	29.60	36.28	93.85	2.89	0.53	0.77	26.42	0.00	26.42	4.000	No	Yes	2.00
452	29.67	30.54	100.00	2.97	0.54	0.77	22.06	0.00	22.06	4.000	No	Yes	2.00
453	29.73	24.51	100.00	3.09	0.55	0.76	17.54	0.00	17.54	4.000	No	Yes	2.00
454	29.81	20.79	100.00	3.16	0.56	0.75	14.78	0.00	14.78	4.000	No	Yes	2.00
455	29.86	20.18	100.00	3.16	0.57	0.75	14.32	0.00	14.32	4.000	No	Yes	2.00
456	29.96	23.00	100.00	3.09	0.56	0.75	16.35	0.00	16.35	4.000	No	Yes	2.00
457	29.99	27.22	100.00	2.99	0.55	0.76	19.46	0.00	19.46	4.000	No	Yes	2.00
458	30.06	32.35	100.00	4.06	0.53	0.76	23.26	0.00	23.26	4.000	No	Yes	2.00
459	30.14	38.69	100.00	4.06	0.52	0.77	28.02	0.00	28.02	4.000	No	Yes	2.00
460	30.20	46.33	100.00	4.06	0.50	0.77	33.84	0.00	33.84	4.000	No	Yes	2.00
461	30.26	52.47	100.00	4.06	0.49	0.78	38.57	0.00	38.57	4.000	No	Yes	2.00
462	30.33	60.41	100.00	4.06	0.47	0.78	44.76	0.00	44.76	4.000	No	Yes	2.00
463	30.38	62.93	100.00	4.06	0.47	0.79	46.72	0.00	46.72	4.000	No	Yes	2.00

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
CRR _{7.5} :	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.07	2.00	0.00	0.00	0.07	0.00	0.14	2.00	0.00	0.00	0.07	0.00
0.20	2.00	0.00	0.00	0.06	0.00	0.29	2.00	0.00	0.00	0.09	0.00
0.35	2.00	0.00	0.00	0.06	0.00	0.41	2.00	0.00	0.00	0.06	0.00
0.49	2.00	0.00	0.00	0.09	0.00	0.54	2.00	0.00	0.00	0.05	0.00
0.59	2.00	0.00	0.00	0.05	0.00	0.67	2.00	0.00	0.00	0.08	0.00
0.72	2.00	0.00	0.00	0.06	0.00	0.80	2.00	0.00	0.00	0.07	0.00
0.86	2.00	0.00	0.00	0.06	0.00	0.94	2.00	0.00	0.00	0.08	0.00
0.99	2.00	0.00	0.00	0.04	0.00	1.09	2.00	0.00	0.00	0.10	0.00
1.12	2.00	0.00	0.00	0.04	0.00	1.20	2.00	0.00	0.00	0.08	0.00
1.27	2.00	0.00	0.00	0.07	0.00	1.33	2.00	0.00	0.00	0.06	0.00
1.38	2.00	0.00	0.00	0.05	0.00	1.48	2.00	0.00	0.00	0.09	0.00
1.51	2.00	0.00	0.00	0.04	0.00	1.58	2.00	0.00	0.00	0.07	0.00
1.66	2.00	0.00	0.00	0.08	0.00	1.73	2.00	0.00	0.00	0.07	0.00
1.77	2.00	0.00	0.00	0.04	0.00	1.85	2.00	0.00	0.00	0.08	0.00
1.91	2.00	0.00	0.00	0.06	0.00	1.97	2.00	0.00	0.00	0.06	0.00
2.06	2.00	0.00	0.00	0.08	0.00	2.12	2.00	0.00	0.00	0.06	0.00
2.17	2.00	0.00	0.00	0.06	0.00	2.25	2.00	0.00	0.00	0.07	0.00
2.31	2.00	0.00	0.00	0.06	0.00	2.36	2.00	0.00	0.00	0.05	0.00
2.47	2.00	0.00	0.00	0.10	0.00	2.52	2.00	0.00	0.00	0.06	0.00
2.56	2.00	0.00	0.00	0.04	0.00	2.63	2.00	0.00	0.00	0.07	0.00
2.71	2.00	0.00	0.00	0.08	0.00	2.77	2.00	0.00	0.00	0.06	0.00
2.83	2.00	0.00	0.00	0.07	0.00	2.90	2.00	0.00	0.00	0.06	0.00
2.97	2.00	0.00	0.00	0.08	0.00	3.03	2.00	0.00	0.00	0.06	0.00
3.09	2.00	0.00	0.00	0.06	0.00	3.16	2.00	0.00	0.00	0.07	0.00
3.22	2.00	0.00	0.00	0.06	0.00	3.30	2.00	0.00	0.00	0.08	0.00
3.36	2.00	0.00	0.00	0.06	0.00	3.41	2.00	0.00	0.00	0.05	0.00
3.49	2.00	0.00	0.00	0.08	0.00	3.57	2.00	0.00	0.00	0.07	0.00
3.62	2.00	0.00	0.00	0.05	0.00	3.70	2.00	0.00	0.00	0.09	0.00
3.74	2.00	0.00	0.00	0.04	0.00	3.85	2.00	0.00	0.00	0.11	0.00
3.88	2.00	0.00	0.00	0.02	0.00	3.95	2.00	0.00	0.00	0.07	0.00
4.01	2.00	0.00	0.00	0.06	0.00	4.09	2.00	0.00	0.00	0.08	0.00
4.13	2.00	0.00	0.00	0.04	0.00	4.23	2.00	0.00	0.00	0.10	0.00
4.27	2.00	0.00	0.00	0.04	0.00	4.37	2.00	0.00	0.00	0.09	0.00
4.43	2.00	0.00	0.00	0.06	0.00	4.48	2.00	0.00	0.00	0.05	0.00
4.54	2.00	0.00	0.00	0.06	0.00	4.60	2.00	0.00	0.00	0.06	0.00
4.68	2.00	0.00	0.00	0.08	0.00	4.73	2.00	0.00	0.00	0.05	0.00
4.82	2.00	0.00	0.00	0.09	0.00	4.86	2.00	0.00	0.00	0.04	0.00
4.93	2.00	0.00	0.00	0.07	0.00	5.02	2.00	0.00	0.00	0.09	0.00
5.05	2.00	0.00	0.00	0.04	0.00	5.13	2.00	0.00	0.00	0.08	0.00
5.19	2.00	0.00	0.00	0.06	0.00	5.25	2.00	0.00	0.00	0.06	0.00
5.32	2.00	0.00	0.00	0.07	0.00	5.41	2.00	0.00	0.00	0.10	0.00
5.46	2.00	0.00	0.00	0.05	0.00	5.51	2.00	0.00	0.00	0.05	0.00
5.61	2.00	0.00	0.00	0.09	0.00	5.66	2.00	0.00	0.00	0.06	0.00
5.71	2.00	0.00	0.00	0.05	0.00	5.78	2.00	0.00	0.00	0.07	0.00
5.86	2.00	0.00	0.00	0.08	0.00	5.91	2.00	0.00	0.00	0.05	0.00
6.00	2.00	0.00	0.00	0.09	0.00	6.06	2.00	0.00	0.00	0.06	0.00
6.11	2.00	0.00	0.00	0.05	0.00	6.20	2.00	0.00	0.00	0.09	0.00
6.25	2.00	0.00	0.00	0.05	0.00	6.31	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
6.39	2.00	0.00	0.00	0.09	0.00	6.45	2.00	0.00	0.00	0.06	0.00
6.50	2.00	0.00	0.00	0.05	0.00	6.59	2.00	0.00	0.00	0.09	0.00
6.65	2.00	0.00	0.00	0.06	0.00	6.70	2.00	0.00	0.00	0.05	0.00
6.79	2.00	0.00	0.00	0.09	0.00	6.85	2.00	0.00	0.00	0.06	0.00
6.90	2.00	0.00	0.00	0.05	0.00	6.99	2.00	0.00	0.00	0.10	0.00
7.05	2.00	0.00	0.00	0.05	0.00	7.10	2.00	0.00	0.00	0.05	0.00
7.17	2.00	0.00	0.00	0.08	0.00	7.23	2.00	0.00	0.00	0.06	0.00
7.32	2.00	0.00	0.00	0.09	0.00	7.38	2.00	0.00	0.00	0.06	0.00
7.43	2.00	0.00	0.00	0.05	0.00	7.51	2.00	0.00	0.00	0.08	0.00
7.57	2.00	0.00	0.00	0.05	0.00	7.62	2.00	0.00	0.00	0.06	0.00
7.71	2.00	0.00	0.00	0.09	0.00	7.77	2.00	0.00	0.00	0.06	0.00
7.82	2.00	0.00	0.00	0.05	0.00	7.91	2.00	0.00	0.00	0.09	0.00
7.97	2.00	0.00	0.00	0.06	0.00	8.01	0.34	0.66	0.35	0.04	0.07
8.07	0.35	0.65	0.35	0.06	0.11	8.17	0.35	0.65	0.35	0.10	0.16
8.21	0.35	0.65	0.35	0.05	0.08	8.30	0.35	0.65	0.35	0.09	0.15
8.36	0.35	0.65	0.35	0.06	0.10	8.41	0.35	0.65	0.35	0.04	0.07
8.50	0.35	0.65	0.35	0.09	0.16	8.56	0.35	0.65	0.35	0.06	0.11
8.61	0.35	0.65	0.35	0.05	0.09	8.66	0.35	0.65	0.35	0.05	0.09
8.73	0.35	0.65	0.35	0.07	0.12	8.81	0.34	0.66	0.34	0.08	0.14
8.86	0.33	0.67	0.34	0.05	0.08	8.96	0.31	0.69	0.33	0.10	0.18
9.01	0.30	0.70	0.32	0.05	0.09	9.06	0.28	0.72	0.31	0.06	0.11
9.13	0.27	0.73	0.31	0.06	0.12	9.20	0.26	0.74	0.30	0.08	0.15
9.30	0.24	0.76	0.29	0.10	0.19	9.35	0.22	0.78	0.29	0.05	0.11
9.40	0.21	0.79	0.28	0.05	0.10	9.46	0.21	0.79	0.28	0.06	0.13
9.55	2.00	0.00	0.00	0.09	0.00	9.60	2.00	0.00	0.00	0.05	0.00
9.66	2.00	0.00	0.00	0.06	0.00	9.71	0.20	0.80	0.28	0.06	0.12
9.80	0.21	0.79	0.28	0.08	0.18	9.85	0.21	0.79	0.28	0.05	0.10
9.93	0.21	0.79	0.28	0.08	0.16	9.98	0.20	0.80	0.28	0.06	0.12
10.04	0.20	0.80	0.28	0.05	0.11	10.12	0.20	0.80	0.28	0.08	0.17
10.19	0.20	0.80	0.28	0.07	0.15	10.25	0.20	0.80	0.28	0.05	0.11
10.31	0.20	0.80	0.28	0.07	0.14	10.39	0.20	0.80	0.28	0.07	0.15
10.45	0.20	0.80	0.28	0.06	0.12	10.52	0.20	0.80	0.28	0.07	0.15
10.58	0.20	0.80	0.28	0.06	0.13	10.64	0.20	0.80	0.28	0.06	0.12
10.74	0.19	0.81	0.27	0.10	0.20	10.79	0.19	0.81	0.27	0.05	0.10
10.83	0.19	0.81	0.27	0.05	0.10	10.90	0.18	0.82	0.27	0.07	0.14
10.96	0.17	0.83	0.27	0.06	0.12	11.03	2.00	0.00	0.00	0.07	0.00
11.10	2.00	0.00	0.00	0.07	0.00	11.18	2.00	0.00	0.00	0.08	0.00
11.24	2.00	0.00	0.00	0.06	0.00	11.29	2.00	0.00	0.00	0.05	0.00
11.36	2.00	0.00	0.00	0.07	0.00	11.42	2.00	0.00	0.00	0.06	0.00
11.51	2.00	0.00	0.00	0.09	0.00	11.57	2.00	0.00	0.00	0.06	0.00
11.62	2.00	0.00	0.00	0.04	0.00	11.70	2.00	0.00	0.00	0.08	0.00
11.75	2.00	0.00	0.00	0.06	0.00	11.83	2.00	0.00	0.00	0.08	0.00
11.90	2.00	0.00	0.00	0.07	0.00	11.95	2.00	0.00	0.00	0.05	0.00
12.03	2.00	0.00	0.00	0.08	0.00	12.10	2.00	0.00	0.00	0.06	0.00
12.15	2.00	0.00	0.00	0.05	0.00	12.21	2.00	0.00	0.00	0.06	0.00
12.28	2.00	0.00	0.00	0.07	0.00	12.34	2.00	0.00	0.00	0.06	0.00
12.40	2.00	0.00	0.00	0.06	0.00	12.48	2.00	0.00	0.00	0.07	0.00
12.55	2.00	0.00	0.00	0.07	0.00	12.60	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
12.70	2.00	0.00	0.00	0.09	0.00	12.75	2.00	0.00	0.00	0.05	0.00
12.80	2.00	0.00	0.00	0.05	0.00	12.89	2.00	0.00	0.00	0.09	0.00
12.94	2.00	0.00	0.00	0.06	0.00	13.00	2.00	0.00	0.00	0.05	0.00
13.09	2.00	0.00	0.00	0.09	0.00	13.14	2.00	0.00	0.00	0.05	0.00
13.19	2.00	0.00	0.00	0.05	0.00	13.28	2.00	0.00	0.00	0.09	0.00
13.34	2.00	0.00	0.00	0.06	0.00	13.39	2.00	0.00	0.00	0.05	0.00
13.47	2.00	0.00	0.00	0.07	0.00	13.53	0.17	0.83	0.27	0.06	0.13
13.59	0.17	0.83	0.27	0.06	0.11	13.67	0.18	0.82	0.27	0.08	0.16
13.73	0.18	0.82	0.27	0.06	0.12	13.79	0.18	0.82	0.27	0.06	0.11
13.88	0.19	0.81	0.27	0.09	0.17	13.93	0.19	0.81	0.27	0.05	0.10
13.99	0.19	0.81	0.27	0.06	0.12	14.07	0.20	0.80	0.28	0.09	0.17
14.13	0.20	0.80	0.28	0.06	0.11	14.18	0.20	0.80	0.28	0.04	0.09
14.28	0.20	0.80	0.28	0.10	0.19	14.33	0.20	0.80	0.28	0.05	0.10
14.38	0.20	0.80	0.28	0.05	0.09	14.48	0.21	0.79	0.28	0.10	0.19
14.53	0.21	0.79	0.28	0.05	0.10	14.58	0.21	0.79	0.28	0.05	0.09
14.65	0.21	0.79	0.28	0.08	0.14	14.72	0.21	0.79	0.28	0.07	0.13
14.78	0.21	0.79	0.28	0.06	0.10	14.83	0.22	0.78	0.28	0.05	0.10
14.92	0.22	0.78	0.28	0.08	0.16	14.98	0.22	0.78	0.28	0.06	0.11
15.05	0.22	0.78	0.28	0.08	0.14	15.12	0.21	0.79	0.28	0.07	0.12
15.16	0.21	0.79	0.28	0.04	0.08	15.22	0.21	0.79	0.28	0.06	0.11
15.32	0.21	0.79	0.28	0.09	0.17	15.37	0.21	0.79	0.28	0.05	0.10
15.46	0.21	0.79	0.28	0.09	0.16	15.52	0.21	0.79	0.28	0.06	0.11
15.56	0.21	0.79	0.28	0.04	0.07	15.66	0.20	0.80	0.28	0.10	0.20
15.71	0.20	0.80	0.28	0.05	0.09	15.75	0.20	0.80	0.28	0.04	0.08
15.86	0.20	0.80	0.28	0.11	0.20	15.91	0.20	0.80	0.28	0.05	0.09
15.96	0.20	0.80	0.28	0.05	0.09	16.02	0.20	0.80	0.28	0.06	0.11
16.10	0.20	0.80	0.28	0.08	0.15	16.16	0.20	0.80	0.28	0.06	0.12
16.21	0.20	0.80	0.28	0.05	0.09	16.29	0.20	0.80	0.28	0.07	0.14
16.36	0.20	0.80	0.28	0.08	0.14	16.41	0.20	0.80	0.28	0.05	0.08
16.51	0.20	0.80	0.28	0.10	0.18	16.56	0.20	0.80	0.28	0.05	0.09
16.61	0.19	0.81	0.27	0.05	0.10	16.71	0.19	0.81	0.27	0.10	0.18
16.76	0.18	0.82	0.27	0.05	0.09	16.81	0.18	0.82	0.27	0.05	0.10
16.89	0.17	0.83	0.26	0.09	0.16	16.95	0.16	0.84	0.26	0.06	0.11
17.00	2.00	0.00	0.00	0.05	0.00	17.10	2.00	0.00	0.00	0.10	0.00
17.14	2.00	0.00	0.00	0.04	0.00	17.20	2.00	0.00	0.00	0.06	0.00
17.29	2.00	0.00	0.00	0.10	0.00	17.33	2.00	0.00	0.00	0.04	0.00
17.39	2.00	0.00	0.00	0.06	0.00	17.46	2.00	0.00	0.00	0.08	0.00
17.52	2.00	0.00	0.00	0.06	0.00	17.59	2.00	0.00	0.00	0.07	0.00
17.70	2.00	0.00	0.00	0.11	0.00	17.72	2.00	0.00	0.00	0.02	0.00
17.80	2.00	0.00	0.00	0.08	0.00	17.85	2.00	0.00	0.00	0.05	0.00
17.92	2.00	0.00	0.00	0.07	0.00	17.99	2.00	0.00	0.00	0.07	0.00
18.05	2.00	0.00	0.00	0.06	0.00	18.14	2.00	0.00	0.00	0.09	0.00
18.18	2.00	0.00	0.00	0.04	0.00	18.25	0.15	0.85	0.26	0.07	0.14
18.32	0.16	0.84	0.26	0.07	0.13	18.39	0.17	0.83	0.26	0.06	0.12
18.45	0.17	0.83	0.27	0.06	0.11	18.50	0.17	0.83	0.27	0.06	0.10
18.57	0.18	0.82	0.27	0.07	0.13	18.64	0.18	0.82	0.27	0.07	0.12
18.73	0.18	0.82	0.27	0.08	0.15	18.78	0.18	0.82	0.27	0.06	0.10
18.85	0.18	0.82	0.27	0.07	0.12	18.91	0.18	0.82	0.27	0.06	0.10

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
18.97	0.18	0.82	0.27	0.07	0.12	19.03	0.18	0.82	0.27	0.06	0.11
19.11	0.19	0.81	0.27	0.08	0.13	19.17	0.19	0.81	0.27	0.07	0.12
19.23	0.19	0.81	0.27	0.06	0.10	19.31	0.19	0.81	0.27	0.08	0.13
19.39	0.19	0.81	0.27	0.08	0.14	19.43	0.19	0.81	0.27	0.05	0.08
19.49	0.19	0.81	0.27	0.06	0.10	19.57	0.19	0.81	0.27	0.08	0.14
19.65	0.18	0.82	0.27	0.08	0.13	19.69	0.18	0.82	0.27	0.04	0.06
19.79	2.00	0.00	0.00	0.10	0.00	19.83	2.00	0.00	0.00	0.04	0.00
19.89	2.00	0.00	0.00	0.06	0.00	19.97	2.00	0.00	0.00	0.09	0.00
20.03	2.00	0.00	0.00	0.06	0.00	20.08	2.00	0.00	0.00	0.05	0.00
20.17	2.00	0.00	0.00	0.08	0.00	20.23	2.00	0.00	0.00	0.06	0.00
20.28	2.00	0.00	0.00	0.05	0.00	20.37	2.00	0.00	0.00	0.10	0.00
20.42	2.00	0.00	0.00	0.05	0.00	20.47	2.00	0.00	0.00	0.05	0.00
20.55	2.00	0.00	0.00	0.07	0.00	20.63	2.00	0.00	0.00	0.08	0.00
20.67	2.00	0.00	0.00	0.05	0.00	20.77	2.00	0.00	0.00	0.10	0.00
20.82	2.00	0.00	0.00	0.04	0.00	20.88	2.00	0.00	0.00	0.07	0.00
20.96	2.00	0.00	0.00	0.07	0.00	21.01	2.00	0.00	0.00	0.05	0.00
21.06	2.00	0.00	0.00	0.05	0.00	21.17	2.00	0.00	0.00	0.11	0.00
21.21	2.00	0.00	0.00	0.04	0.00	21.26	2.00	0.00	0.00	0.05	0.00
21.33	2.00	0.00	0.00	0.07	0.00	21.40	2.00	0.00	0.00	0.07	0.00
21.46	2.00	0.00	0.00	0.06	0.00	21.55	2.00	0.00	0.00	0.08	0.00
21.61	2.00	0.00	0.00	0.06	0.00	21.66	2.00	0.00	0.00	0.06	0.00
21.75	2.00	0.00	0.00	0.08	0.00	21.81	2.00	0.00	0.00	0.06	0.00
21.86	2.00	0.00	0.00	0.05	0.00	21.94	2.00	0.00	0.00	0.08	0.00
22.00	2.00	0.00	0.00	0.06	0.00	22.06	2.00	0.00	0.00	0.06	0.00
22.14	2.00	0.00	0.00	0.08	0.00	22.20	2.00	0.00	0.00	0.06	0.00
22.25	2.00	0.00	0.00	0.05	0.00	22.34	2.00	0.00	0.00	0.08	0.00
22.40	2.00	0.00	0.00	0.06	0.00	22.47	2.00	0.00	0.00	0.07	0.00
22.52	2.00	0.00	0.00	0.05	0.00	22.61	2.00	0.00	0.00	0.09	0.00
22.67	2.00	0.00	0.00	0.06	0.00	22.72	2.00	0.00	0.00	0.05	0.00
22.78	2.00	0.00	0.00	0.06	0.00	22.86	2.00	0.00	0.00	0.09	0.00
22.92	2.00	0.00	0.00	0.05	0.00	22.97	2.00	0.00	0.00	0.05	0.00
23.06	2.00	0.00	0.00	0.09	0.00	23.12	2.00	0.00	0.00	0.06	0.00
23.17	2.00	0.00	0.00	0.05	0.00	23.26	2.00	0.00	0.00	0.10	0.00
23.31	2.00	0.00	0.00	0.05	0.00	23.41	2.00	0.00	0.00	0.10	0.00
23.46	2.00	0.00	0.00	0.05	0.00	23.51	2.00	0.00	0.00	0.05	0.00
23.56	2.00	0.00	0.00	0.05	0.00	23.65	2.00	0.00	0.00	0.09	0.00
23.71	2.00	0.00	0.00	0.05	0.00	23.75	2.00	0.00	0.00	0.05	0.00
23.85	2.00	0.00	0.00	0.10	0.00	23.91	2.00	0.00	0.00	0.06	0.00
23.95	2.00	0.00	0.00	0.05	0.00	24.04	2.00	0.00	0.00	0.09	0.00
24.10	2.00	0.00	0.00	0.06	0.00	24.15	2.00	0.00	0.00	0.05	0.00
24.25	2.00	0.00	0.00	0.09	0.00	24.30	2.00	0.00	0.00	0.05	0.00
24.36	2.00	0.00	0.00	0.05	0.00	24.45	2.00	0.00	0.00	0.09	0.00
24.50	2.00	0.00	0.00	0.05	0.00	24.55	2.00	0.00	0.00	0.05	0.00
24.64	2.00	0.00	0.00	0.09	0.00	24.69	2.00	0.00	0.00	0.05	0.00
24.75	2.00	0.00	0.00	0.05	0.00	24.84	2.00	0.00	0.00	0.09	0.00
24.89	2.00	0.00	0.00	0.05	0.00	24.95	2.00	0.00	0.00	0.06	0.00
25.02	0.15	0.85	0.26	0.07	0.12	25.07	0.16	0.84	0.26	0.04	0.07
25.14	0.17	0.83	0.27	0.07	0.11	25.23	0.18	0.82	0.27	0.10	0.15

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
25.29	0.18	0.82	0.27	0.05	0.08	25.36	0.17	0.83	0.27	0.07	0.11
25.41	0.17	0.83	0.26	0.05	0.08	25.48	0.16	0.84	0.26	0.07	0.10
25.55	0.15	0.85	0.26	0.07	0.11	25.61	2.00	0.00	0.00	0.06	0.00
25.66	2.00	0.00	0.00	0.05	0.00	25.75	2.00	0.00	0.00	0.09	0.00
25.80	2.00	0.00	0.00	0.05	0.00	25.86	2.00	0.00	0.00	0.05	0.00
25.94	2.00	0.00	0.00	0.08	0.00	25.99	2.00	0.00	0.00	0.05	0.00
26.06	2.00	0.00	0.00	0.07	0.00	26.12	2.00	0.00	0.00	0.06	0.00
26.19	2.00	0.00	0.00	0.07	0.00	26.25	2.00	0.00	0.00	0.06	0.00
26.34	2.00	0.00	0.00	0.09	0.00	26.38	2.00	0.00	0.00	0.04	0.00
26.45	2.00	0.00	0.00	0.06	0.00	26.54	2.00	0.00	0.00	0.09	0.00
26.59	2.00	0.00	0.00	0.05	0.00	26.65	2.00	0.00	0.00	0.06	0.00
26.71	2.00	0.00	0.00	0.07	0.00	26.78	2.00	0.00	0.00	0.07	0.00
26.84	2.00	0.00	0.00	0.06	0.00	26.94	2.00	0.00	0.00	0.10	0.00
26.98	2.00	0.00	0.00	0.03	0.00	27.04	2.00	0.00	0.00	0.07	0.00
27.11	2.00	0.00	0.00	0.07	0.00	27.18	2.00	0.00	0.00	0.07	0.00
27.23	2.00	0.00	0.00	0.06	0.00	27.32	2.00	0.00	0.00	0.08	0.00
27.38	2.00	0.00	0.00	0.06	0.00	27.43	2.00	0.00	0.00	0.05	0.00
27.52	2.00	0.00	0.00	0.08	0.00	27.58	2.00	0.00	0.00	0.06	0.00
27.63	2.00	0.00	0.00	0.05	0.00	27.73	2.00	0.00	0.00	0.10	0.00
27.78	2.00	0.00	0.00	0.04	0.00	27.83	2.00	0.00	0.00	0.05	0.00
27.91	2.00	0.00	0.00	0.07	0.00	27.98	2.00	0.00	0.00	0.07	0.00
28.03	2.00	0.00	0.00	0.05	0.00	28.11	2.00	0.00	0.00	0.07	0.00
28.18	2.00	0.00	0.00	0.07	0.00	28.22	2.00	0.00	0.00	0.05	0.00
28.32	2.00	0.00	0.00	0.10	0.00	28.35	2.00	0.00	0.00	0.03	0.00
28.43	0.15	0.85	0.26	0.08	0.12	28.48	0.16	0.84	0.26	0.05	0.07
28.56	0.18	0.82	0.27	0.08	0.11	28.63	0.19	0.81	0.27	0.07	0.10
28.68	0.19	0.81	0.27	0.05	0.07	28.74	0.19	0.81	0.27	0.06	0.09
28.82	0.20	0.80	0.28	0.08	0.11	28.88	0.21	0.79	0.28	0.05	0.07
28.95	0.23	0.77	0.29	0.08	0.10	29.02	0.24	0.76	0.29	0.07	0.08
29.08	0.25	0.75	0.30	0.06	0.08	29.15	0.25	0.75	0.30	0.07	0.09
29.21	0.24	0.76	0.29	0.06	0.07	29.27	0.22	0.78	0.29	0.07	0.09
29.37	0.19	0.81	0.27	0.10	0.13	29.40	0.17	0.83	0.27	0.03	0.04
29.46	0.16	0.84	0.26	0.07	0.09	29.54	2.00	0.00	0.00	0.07	0.00
29.60	2.00	0.00	0.00	0.06	0.00	29.67	2.00	0.00	0.00	0.07	0.00
29.73	2.00	0.00	0.00	0.06	0.00	29.81	2.00	0.00	0.00	0.08	0.00
29.86	2.00	0.00	0.00	0.05	0.00	29.96	2.00	0.00	0.00	0.10	0.00
29.99	2.00	0.00	0.00	0.03	0.00	30.06	2.00	0.00	0.00	0.07	0.00
30.14	2.00	0.00	0.00	0.08	0.00	30.20	2.00	0.00	0.00	0.05	0.00
30.26	2.00	0.00	0.00	0.06	0.00	30.33	2.00	0.00	0.00	0.07	0.00
30.38	2.00	0.00	0.00	0.05	0.00						

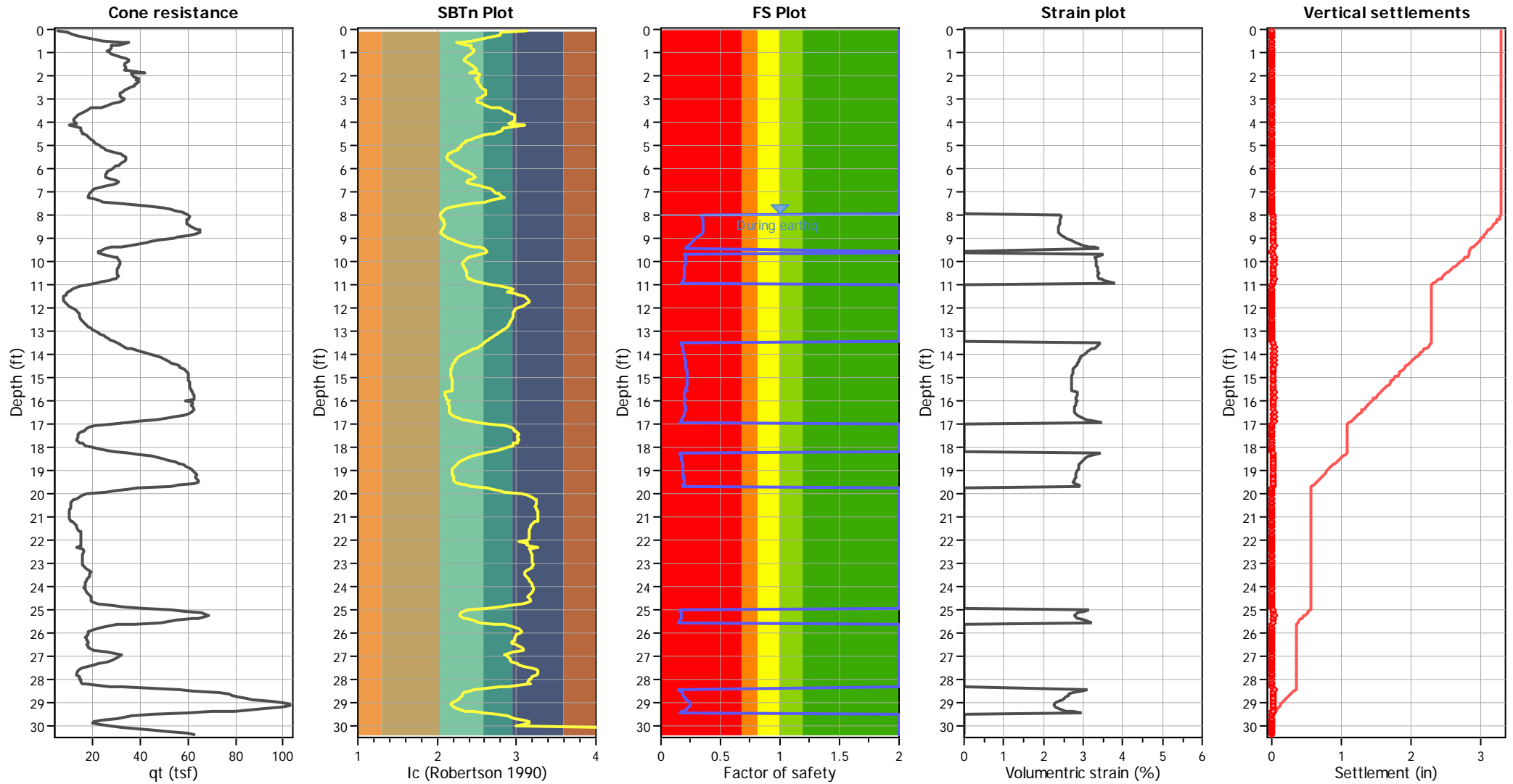
Overall liquefaction potential: 17.06

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

- FS: Calculated factor of safety for test point
- d_z: Layer thickness (ft)
- LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- qt: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement due to soil liquefaction ::											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.01	129.04	0.34	2.45	1.00	0.01	8.07	129.83	0.35	2.44	1.00	0.02
8.17	130.64	0.35	2.42	1.00	0.03	8.21	130.77	0.35	2.42	1.00	0.01
8.30	131.13	0.35	2.41	1.00	0.03	8.36	131.28	0.35	2.41	1.00	0.02
8.41	131.42	0.35	2.41	1.00	0.01	8.50	132.16	0.35	2.39	1.00	0.03
8.56	132.64	0.35	2.38	1.00	0.02	8.61	133.00	0.35	2.37	1.00	0.01
8.66	133.17	0.35	2.37	1.00	0.01	8.73	132.35	0.35	2.39	1.00	0.02
8.81	130.85	0.34	2.42	1.00	0.02	8.86	129.23	0.33	2.45	1.00	0.01
8.96	125.12	0.31	2.54	1.00	0.03	9.01	123.41	0.30	2.58	1.00	0.02
9.06	119.36	0.28	2.67	1.00	0.02	9.13	116.27	0.27	2.75	1.00	0.02
9.20	113.84	0.26	2.81	1.00	0.03	9.30	107.16	0.24	2.99	1.00	0.03
9.35	102.51	0.22	3.13	1.00	0.02	9.40	97.84	0.21	3.29	1.00	0.02
9.46	94.48	0.21	3.40	1.00	0.03	9.55	30.28	2.00	0.00	1.00	0.00
9.60	29.96	2.00	0.00	1.00	0.00	9.66	29.89	2.00	0.00	1.00	0.00
9.71	91.34	0.20	3.52	1.00	0.02	9.80	96.39	0.21	3.34	1.00	0.03
9.85	97.29	0.21	3.30	1.00	0.02	9.93	97.02	0.21	3.31	1.00	0.03
9.98	96.85	0.20	3.32	1.00	0.02	10.04	96.70	0.20	3.32	1.00	0.02
10.12	96.15	0.20	3.34	1.00	0.03	10.19	96.10	0.20	3.35	1.00	0.03
10.25	95.59	0.20	3.36	1.00	0.02	10.31	95.27	0.20	3.37	1.00	0.03
10.39	95.16	0.20	3.38	1.00	0.03	10.45	95.27	0.20	3.38	1.00	0.02
10.52	94.94	0.20	3.39	1.00	0.03	10.58	95.23	0.20	3.38	1.00	0.03
10.64	95.48	0.20	3.37	1.00	0.02	10.74	94.42	0.19	3.41	1.00	0.04
10.79	92.81	0.19	3.46	1.00	0.02	10.83	91.81	0.19	3.50	1.00	0.02
10.90	87.72	0.18	3.66	1.00	0.03	10.96	84.82	0.17	3.79	1.00	0.03
11.03	22.95	2.00	0.00	1.00	0.00	11.10	18.38	2.00	0.00	1.00	0.00
11.18	14.78	2.00	0.00	1.00	0.00	11.24	13.39	2.00	0.00	1.00	0.00
11.29	12.27	2.00	0.00	1.00	0.00	11.36	11.72	2.00	0.00	1.00	0.00
11.42	11.09	2.00	0.00	1.00	0.00	11.51	10.19	2.00	0.00	1.00	0.00
11.57	10.16	2.00	0.00	1.00	0.00	11.62	10.14	2.00	0.00	1.00	0.00
11.70	10.10	2.00	0.00	1.00	0.00	11.75	10.20	2.00	0.00	1.00	0.00
11.83	10.88	2.00	0.00	1.00	0.00	11.90	11.56	2.00	0.00	1.00	0.00
11.95	12.49	2.00	0.00	1.00	0.00	12.03	14.10	2.00	0.00	1.00	0.00
12.10	15.23	2.00	0.00	1.00	0.00	12.15	15.90	2.00	0.00	1.00	0.00
12.21	16.44	2.00	0.00	1.00	0.00	12.28	16.96	2.00	0.00	1.00	0.00
12.34	17.26	2.00	0.00	1.00	0.00	12.40	17.44	2.00	0.00	1.00	0.00
12.48	18.08	2.00	0.00	1.00	0.00	12.55	18.71	2.00	0.00	1.00	0.00
12.60	19.23	2.00	0.00	1.00	0.00	12.70	19.96	2.00	0.00	1.00	0.00
12.75	20.59	2.00	0.00	1.00	0.00	12.80	21.22	2.00	0.00	1.00	0.00
12.89	22.27	2.00	0.00	1.00	0.00	12.94	23.23	2.00	0.00	1.00	0.00
13.00	24.18	2.00	0.00	1.00	0.00	13.09	25.42	2.00	0.00	1.00	0.00
13.14	26.36	2.00	0.00	1.00	0.00	13.19	27.75	2.00	0.00	1.00	0.00
13.28	28.30	2.00	0.00	1.00	0.00	13.34	29.66	2.00	0.00	1.00	0.00
13.39	30.59	2.00	0.00	1.00	0.00	13.47	32.35	2.00	0.00	1.00	0.00
13.53	93.87	0.17	3.43	1.00	0.03	13.59	94.87	0.17	3.39	1.00	0.02
13.67	96.90	0.18	3.32	1.00	0.03	13.73	98.08	0.18	3.28	1.00	0.02
13.79	99.79	0.18	3.22	1.00	0.02	13.88	102.78	0.19	3.12	1.00	0.03
13.93	104.71	0.19	3.06	1.00	0.02	13.99	106.10	0.19	3.02	1.00	0.02
14.07	107.90	0.20	2.97	1.00	0.03	14.13	108.98	0.20	2.94	1.00	0.02
14.18	109.71	0.20	2.92	1.00	0.02	14.28	110.44	0.20	2.90	1.00	0.03

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
14.33	111.06	0.20	2.88	1.00	0.02	14.38	111.48	0.20	2.87	1.00	0.02
14.48	112.78	0.21	2.84	1.00	0.03	14.53	114.02	0.21	2.80	1.00	0.02
14.58	114.69	0.21	2.79	1.00	0.02	14.65	115.72	0.21	2.76	1.00	0.03
14.72	116.05	0.21	2.75	1.00	0.02	14.78	116.37	0.21	2.74	1.00	0.02
14.83	116.84	0.22	2.73	1.00	0.02	14.92	117.17	0.22	2.72	1.00	0.03
14.98	117.50	0.22	2.72	1.00	0.02	15.05	117.25	0.22	2.72	1.00	0.03
15.12	117.16	0.21	2.72	1.00	0.02	15.16	117.21	0.21	2.72	1.00	0.01
15.22	117.51	0.21	2.72	1.00	0.02	15.32	117.59	0.21	2.71	1.00	0.03
15.37	117.45	0.21	2.72	1.00	0.02	15.46	117.41	0.21	2.72	1.00	0.03
15.52	117.52	0.21	2.72	1.00	0.02	15.56	117.70	0.21	2.71	1.00	0.01
15.66	111.90	0.20	2.86	1.00	0.04	15.71	112.18	0.20	2.85	1.00	0.02
15.75	112.52	0.20	2.84	1.00	0.01	15.86	113.38	0.20	2.82	1.00	0.04
15.91	113.69	0.20	2.81	1.00	0.02	15.96	113.85	0.20	2.81	1.00	0.02
16.02	112.27	0.20	2.85	1.00	0.02	16.10	113.61	0.20	2.81	1.00	0.03
16.16	113.51	0.20	2.82	1.00	0.02	16.21	114.01	0.20	2.80	1.00	0.02
16.29	114.75	0.20	2.78	1.00	0.02	16.36	115.08	0.20	2.78	1.00	0.03
16.41	115.12	0.20	2.78	1.00	0.02	16.51	114.31	0.20	2.80	1.00	0.03
16.56	113.39	0.20	2.82	1.00	0.02	16.61	112.14	0.19	2.85	1.00	0.02
16.71	109.38	0.19	2.93	1.00	0.03	16.76	106.98	0.18	3.00	1.00	0.02
16.81	103.83	0.18	3.09	1.00	0.02	16.89	97.68	0.17	3.29	1.00	0.03
16.95	92.86	0.16	3.46	1.00	0.02	17.00	27.86	2.00	0.00	1.00	0.00
17.10	20.73	2.00	0.00	1.00	0.00	17.14	18.36	2.00	0.00	1.00	0.00
17.20	17.05	2.00	0.00	1.00	0.00	17.29	16.02	2.00	0.00	1.00	0.00
17.33	15.23	2.00	0.00	1.00	0.00	17.39	14.13	2.00	0.00	1.00	0.00
17.46	13.51	2.00	0.00	1.00	0.00	17.52	13.39	2.00	0.00	1.00	0.00
17.59	13.27	2.00	0.00	1.00	0.00	17.70	12.94	2.00	0.00	1.00	0.00
17.72	13.12	2.00	0.00	1.00	0.00	17.80	13.76	2.00	0.00	1.00	0.00
17.85	15.18	2.00	0.00	1.00	0.00	17.92	16.30	2.00	0.00	1.00	0.00
17.99	19.02	2.00	0.00	1.00	0.00	18.05	21.67	2.00	0.00	1.00	0.00
18.14	24.37	2.00	0.00	1.00	0.00	18.18	27.86	2.00	0.00	1.00	0.00
18.25	93.48	0.15	3.44	1.00	0.03	18.32	97.27	0.16	3.30	1.00	0.03
18.39	101.98	0.17	3.15	1.00	0.02	18.45	103.87	0.17	3.09	1.00	0.02
18.50	105.55	0.17	3.04	1.00	0.02	18.57	106.60	0.18	3.01	1.00	0.03
18.64	108.08	0.18	2.97	1.00	0.02	18.73	108.86	0.18	2.94	1.00	0.03
18.78	110.27	0.18	2.90	1.00	0.02	18.85	110.68	0.18	2.89	1.00	0.02
18.91	110.62	0.18	2.89	1.00	0.02	18.97	110.92	0.18	2.89	1.00	0.02
19.03	111.85	0.18	2.86	1.00	0.02	19.11	112.98	0.19	2.83	1.00	0.03
19.17	113.66	0.19	2.81	1.00	0.02	19.23	113.92	0.19	2.81	1.00	0.02
19.31	113.99	0.19	2.80	1.00	0.03	19.39	114.88	0.19	2.78	1.00	0.03
19.43	115.33	0.19	2.77	1.00	0.02	19.49	116.33	0.19	2.74	1.00	0.02
19.57	115.55	0.19	2.76	1.00	0.03	19.65	111.14	0.18	2.88	1.00	0.03
19.69	109.28	0.18	2.93	1.00	0.01	19.79	35.02	2.00	0.00	1.00	0.00
19.83	31.24	2.00	0.00	1.00	0.00	19.89	26.16	2.00	0.00	1.00	0.00
19.97	23.02	2.00	0.00	1.00	0.00	20.03	15.82	2.00	0.00	1.00	0.00
20.08	14.00	2.00	0.00	1.00	0.00	20.17	12.26	2.00	0.00	1.00	0.00
20.23	11.33	2.00	0.00	1.00	0.00	20.28	10.61	2.00	0.00	1.00	0.00
20.37	9.95	2.00	0.00	1.00	0.00	20.42	9.67	2.00	0.00	1.00	0.00
20.47	9.57	2.00	0.00	1.00	0.00	20.55	9.81	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
20.63	9.44	2.00	0.00	1.00	0.00	20.67	9.34	2.00	0.00	1.00	0.00
20.77	9.14	2.00	0.00	1.00	0.00	20.82	9.21	2.00	0.00	1.00	0.00
20.88	9.20	2.00	0.00	1.00	0.00	20.96	9.18	2.00	0.00	1.00	0.00
21.01	9.17	2.00	0.00	1.00	0.00	21.06	9.24	2.00	0.00	1.00	0.00
21.17	9.56	2.00	0.00	1.00	0.00	21.21	9.99	2.00	0.00	1.00	0.00
21.26	10.41	2.00	0.00	1.00	0.00	21.33	11.09	2.00	0.00	1.00	0.00
21.40	11.42	2.00	0.00	1.00	0.00	21.46	11.75	2.00	0.00	1.00	0.00
21.55	12.24	2.00	0.00	1.00	0.00	21.61	12.48	2.00	0.00	1.00	0.00
21.66	12.90	2.00	0.00	1.00	0.00	21.75	12.87	2.00	0.00	1.00	0.00
21.81	13.03	2.00	0.00	1.00	0.00	21.86	13.01	2.00	0.00	1.00	0.00
21.94	12.98	2.00	0.00	1.00	0.00	22.00	12.70	2.00	0.00	1.00	0.00
22.06	12.68	2.00	0.00	1.00	0.00	22.14	12.65	2.00	0.00	1.00	0.00
22.20	12.63	2.00	0.00	1.00	0.00	22.25	12.71	2.00	0.00	1.00	0.00
22.34	11.23	2.00	0.00	1.00	0.00	22.40	13.42	2.00	0.00	1.00	0.00
22.47	13.65	2.00	0.00	1.00	0.00	22.52	13.55	2.00	0.00	1.00	0.00
22.61	13.43	2.00	0.00	1.00	0.00	22.67	13.41	2.00	0.00	1.00	0.00
22.72	13.39	2.00	0.00	1.00	0.00	22.78	13.38	2.00	0.00	1.00	0.00
22.86	13.35	2.00	0.00	1.00	0.00	22.92	13.33	2.00	0.00	1.00	0.00
22.97	13.31	2.00	0.00	1.00	0.00	23.06	13.28	2.00	0.00	1.00	0.00
23.12	13.51	2.00	0.00	1.00	0.00	23.17	13.83	2.00	0.00	1.00	0.00
23.26	14.72	2.00	0.00	1.00	0.00	23.31	15.29	2.00	0.00	1.00	0.00
23.41	15.75	2.00	0.00	1.00	0.00	23.46	15.65	2.00	0.00	1.00	0.00
23.51	15.55	2.00	0.00	1.00	0.00	23.56	15.28	2.00	0.00	1.00	0.00
23.65	14.66	2.00	0.00	1.00	0.00	23.71	14.39	2.00	0.00	1.00	0.00
23.75	14.29	2.00	0.00	1.00	0.00	23.85	13.93	2.00	0.00	1.00	0.00
23.91	13.83	2.00	0.00	1.00	0.00	23.95	13.73	2.00	0.00	1.00	0.00
24.04	13.45	2.00	0.00	1.00	0.00	24.10	13.52	2.00	0.00	1.00	0.00
24.15	13.58	2.00	0.00	1.00	0.00	24.25	14.20	2.00	0.00	1.00	0.00
24.30	14.76	2.00	0.00	1.00	0.00	24.36	15.31	2.00	0.00	1.00	0.00
24.45	15.77	2.00	0.00	1.00	0.00	24.50	15.59	2.00	0.00	1.00	0.00
24.55	15.32	2.00	0.00	1.00	0.00	24.64	15.45	2.00	0.00	1.00	0.00
24.69	16.33	2.00	0.00	1.00	0.00	24.75	18.02	2.00	0.00	1.00	0.00
24.84	22.64	2.00	0.00	1.00	0.00	24.89	26.47	2.00	0.00	1.00	0.00
24.95	33.37	2.00	0.00	1.00	0.00	25.02	101.54	0.15	3.16	1.00	0.03
25.07	105.98	0.16	3.03	1.00	0.02	25.14	111.79	0.17	2.86	1.00	0.03
25.23	114.26	0.18	2.80	1.00	0.03	25.29	114.23	0.18	2.80	1.00	0.02
25.36	111.61	0.17	2.87	1.00	0.03	25.41	110.24	0.17	2.90	1.00	0.02
25.48	105.04	0.16	3.05	1.00	0.02	25.55	99.72	0.15	3.22	1.00	0.03
25.61	29.63	2.00	0.00	1.00	0.00	25.66	23.91	2.00	0.00	1.00	0.00
25.75	18.97	2.00	0.00	1.00	0.00	25.80	16.87	2.00	0.00	1.00	0.00
25.86	15.74	2.00	0.00	1.00	0.00	25.94	14.28	2.00	0.00	1.00	0.00
25.99	14.26	2.00	0.00	1.00	0.00	26.06	14.00	2.00	0.00	1.00	0.00
26.12	13.44	2.00	0.00	1.00	0.00	26.19	13.26	2.00	0.00	1.00	0.00
26.25	13.32	2.00	0.00	1.00	0.00	26.34	13.45	2.00	0.00	1.00	0.00
26.38	13.91	2.00	0.00	1.00	0.00	26.45	14.12	2.00	0.00	1.00	0.00
26.54	13.63	2.00	0.00	1.00	0.00	26.59	13.69	2.00	0.00	1.00	0.00
26.65	13.91	2.00	0.00	1.00	0.00	26.71	14.59	2.00	0.00	1.00	0.00
26.78	15.74	2.00	0.00	1.00	0.00	26.84	19.72	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
26.94	24.64	2.00	0.00	1.00	0.00	26.98	24.55	2.00	0.00	1.00	0.00
27.04	23.33	2.00	0.00	1.00	0.00	27.11	22.03	2.00	0.00	1.00	0.00
27.18	21.38	2.00	0.00	1.00	0.00	27.23	19.87	2.00	0.00	1.00	0.00
27.32	16.88	2.00	0.00	1.00	0.00	27.38	15.39	2.00	0.00	1.00	0.00
27.43	13.75	2.00	0.00	1.00	0.00	27.52	11.82	2.00	0.00	1.00	0.00
27.58	10.74	2.00	0.00	1.00	0.00	27.63	10.35	2.00	0.00	1.00	0.00
27.73	9.95	2.00	0.00	1.00	0.00	27.78	9.79	2.00	0.00	1.00	0.00
27.83	10.00	2.00	0.00	1.00	0.00	27.91	10.51	2.00	0.00	1.00	0.00
27.98	10.87	2.00	0.00	1.00	0.00	28.03	11.09	2.00	0.00	1.00	0.00
28.11	11.15	2.00	0.00	1.00	0.00	28.18	11.66	2.00	0.00	1.00	0.00
28.22	12.55	2.00	0.00	1.00	0.00	28.32	20.36	2.00	0.00	1.00	0.00
28.35	24.10	2.00	0.00	1.00	0.00	28.43	103.48	0.15	3.10	1.00	0.03
28.48	108.17	0.16	2.96	1.00	0.02	28.56	116.85	0.18	2.73	1.00	0.03
28.63	120.33	0.19	2.65	1.00	0.02	28.68	121.57	0.19	2.62	1.00	0.02
28.74	123.60	0.19	2.57	1.00	0.02	28.82	126.27	0.20	2.51	1.00	0.02
28.88	128.05	0.21	2.48	1.00	0.02	28.95	133.37	0.23	2.37	1.00	0.02
29.02	136.56	0.24	2.31	1.00	0.02	29.08	138.27	0.25	2.27	1.00	0.02
29.15	138.28	0.25	2.27	1.00	0.02	29.21	136.14	0.24	2.31	1.00	0.02
29.27	132.18	0.22	2.39	1.00	0.02	29.37	123.63	0.19	2.57	1.00	0.03
29.40	116.01	0.17	2.75	1.00	0.01	29.46	108.52	0.16	2.95	1.00	0.02
29.54	33.13	2.00	0.00	1.00	0.00	29.60	26.42	2.00	0.00	1.00	0.00
29.67	22.06	2.00	0.00	1.00	0.00	29.73	17.54	2.00	0.00	1.00	0.00
29.81	14.78	2.00	0.00	1.00	0.00	29.86	14.32	2.00	0.00	1.00	0.00
29.96	16.35	2.00	0.00	1.00	0.00	29.99	19.46	2.00	0.00	1.00	0.00
30.06	23.26	2.00	0.00	1.00	0.00	30.14	28.02	2.00	0.00	1.00	0.00
30.20	33.84	2.00	0.00	1.00	0.00	30.26	38.57	2.00	0.00	1.00	0.00
30.33	44.76	2.00	0.00	1.00	0.00	30.38	46.72	2.00	0.00	1.00	0.00

Total estimated settlement: 3.30

Abbreviations

- Q_{tn,cs}: Equivalent clean sand normalized cone resistance
- FS: Factor of safety against liquefaction
- e_v (%): Post-liquefaction volumetric strain
- DF: e_v depth weighting factor
- Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
0.07	5.53	8.88	10.87	96.52	3.11	0.08	107.48
0.14	9.65	15.49	5.93	91.94	2.81	0.08	0.62
0.20	11.06	17.75	5.84	103.60	2.80	0.08	0.62
0.29	12.67	20.33	5.68	115.54	2.79	0.09	0.62
0.35	15.48	24.84	4.75	118.07	2.70	0.09	0.62
0.41	18.49	29.67	3.87	114.70	2.61	0.10	0.62
0.49	24.53	39.36	2.68	105.45	2.45	0.10	0.75
0.54	32.07	51.47	1.93	99.19	2.30	0.11	0.77
0.59	35.59	57.13	1.75	99.92	2.25	0.12	0.77
0.67	30.87	49.53	2.19	108.59	2.36	0.11	0.77
0.72	28.16	45.17	2.51	113.20	2.42	0.11	0.76
0.80	28.26	45.33	2.57	116.32	2.43	0.11	0.76
0.86	27.25	43.70	2.70	117.96	2.46	0.11	0.76
0.94	26.45	42.41	2.72	115.51	2.46	0.11	0.75
0.99	27.15	43.53	2.62	114.23	2.44	0.11	0.76
1.09	27.86	44.66	2.55	114.00	2.43	0.11	0.76
1.12	29.77	47.73	2.35	111.96	2.39	0.11	0.76
1.20	31.78	50.95	2.22	112.95	2.37	0.12	0.77
1.27	33.89	54.33	2.11	114.83	2.35	0.12	0.77
1.33	35.40	56.75	2.06	116.93	2.33	0.12	0.78
1.38	35.50	56.91	2.11	120.22	2.35	0.12	0.78
1.48	33.99	54.47	2.33	127.16	2.39	0.12	0.78
1.51	33.69	53.98	2.42	130.80	2.41	0.12	0.78
1.58	33.59	53.82	2.61	140.65	2.44	0.12	0.78
1.66	34.18	54.77	2.79	152.60	2.47	0.13	0.78
1.73	34.07	54.58	2.94	160.58	2.49	0.13	0.78
1.77	33.77	54.09	3.02	163.36	2.51	0.13	0.78
1.85	41.92	67.17	2.38	159.58	2.40	0.15	0.80
1.91	36.79	58.93	3.02	177.79	2.51	0.14	0.79
1.97	36.29	58.12	3.23	187.71	2.54	0.14	0.79
2.06	37.88	60.67	3.09	187.71	2.52	0.14	0.80
2.12	39.80	63.75	2.91	185.74	2.49	0.15	0.80
2.17	38.08	60.98	3.08	187.79	2.51	0.14	0.80
2.25	39.29	62.91	3.01	189.40	2.50	0.14	0.80
2.31	38.68	61.93	3.15	195.38	2.52	0.14	0.80
2.36	37.77	60.47	3.30	199.73	2.54	0.14	0.80
2.47	37.57	60.14	3.24	195.09	2.54	0.14	0.79
2.52	35.96	57.54	3.43	197.19	2.56	0.14	0.79
2.56	34.97	55.93	3.55	198.82	2.58	0.14	0.79
2.63	33.35	53.34	3.79	202.39	2.60	0.13	0.64
2.71	32.95	52.69	3.80	200.01	2.61	0.13	0.64
2.77	31.74	50.74	3.91	198.46	2.62	0.13	0.63
2.83	31.44	50.25	3.76	188.91	2.60	0.13	0.63
2.90	31.65	50.57	3.55	179.47	2.58	0.13	0.78
2.97	32.25	51.52	3.33	171.70	2.55	0.13	0.78
3.03	33.26	53.14	3.03	160.90	2.51	0.13	0.78
3.09	32.96	52.65	2.97	156.36	2.50	0.13	0.78
3.16	31.85	50.86	3.04	154.66	2.51	0.12	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
3.22	28.62	45.68	3.44	156.99	2.56	0.12	0.77
3.30	25.61	40.84	3.97	161.98	2.62	0.11	0.62
3.36	23.49	37.43	4.46	167.05	2.68	0.11	0.62
3.41	19.37	30.80	5.80	178.67	2.80	0.10	0.62
3.49	17.76	28.21	6.46	182.25	2.85	0.10	0.62
3.57	16.36	25.94	7.11	184.38	2.89	0.10	0.62
3.62	15.36	24.33	7.57	184.12	2.92	0.10	0.62
3.70	13.75	21.73	8.29	180.24	2.97	0.09	0.62
3.74	13.34	21.08	8.41	177.31	2.98	0.09	0.62
3.85	12.13	19.13	8.46	161.90	2.98	0.09	0.62
3.88	12.03	18.96	8.50	161.18	2.98	0.09	0.62
3.95	12.03	18.96	8.48	160.83	2.98	0.09	0.62
4.01	12.83	20.24	7.81	157.99	2.94	0.09	0.62
4.09	13.54	21.37	7.34	156.82	2.91	0.09	0.62
4.13	10.12	15.87	10.53	167.10	3.10	0.09	2.90
4.23	15.35	24.27	6.35	154.17	2.84	0.09	0.62
4.27	15.45	24.42	6.22	151.92	2.83	0.09	0.62
4.37	15.45	24.42	5.88	143.55	2.80	0.09	0.62
4.43	15.65	24.73	5.39	133.23	2.76	0.09	0.62
4.48	16.06	25.37	4.91	124.55	2.72	0.09	0.62
4.54	16.66	26.33	4.28	112.66	2.66	0.09	0.62
4.60	17.47	27.63	3.55	97.95	2.58	0.09	0.72
4.68	18.88	29.88	2.78	83.17	2.47	0.09	0.72
4.73	19.58	31.01	2.47	76.63	2.42	0.09	0.72
4.82	20.59	32.62	2.15	70.09	2.35	0.09	0.73
4.86	20.79	32.94	2.13	69.99	2.35	0.09	0.73
4.93	22.10	35.04	2.00	69.99	2.32	0.09	0.73
5.02	23.10	36.64	1.93	70.86	2.30	0.09	0.73
5.05	23.60	37.44	1.90	71.14	2.29	0.09	0.73
5.13	24.71	39.21	1.81	71.11	2.27	0.09	0.74
5.19	25.41	40.33	1.77	71.46	2.26	0.09	0.74
5.25	27.22	43.24	1.66	71.60	2.22	0.09	0.74
5.32	29.84	47.44	1.54	72.86	2.17	0.09	0.75
5.41	32.15	51.14	1.47	75.35	2.13	0.10	0.75
5.46	32.76	52.12	1.47	76.44	2.13	0.10	0.75
5.51	34.06	54.20	1.44	78.10	2.11	0.10	0.75
5.61	34.26	54.52	1.46	79.72	2.13	0.10	0.76
5.66	33.96	54.03	1.49	80.45	2.14	0.10	0.76
5.71	33.26	52.90	1.53	80.82	2.16	0.10	0.76
5.78	32.05	50.95	1.60	81.57	2.19	0.10	0.76
5.86	31.05	49.34	1.66	81.98	2.22	0.10	0.76
5.91	29.94	47.55	1.74	82.71	2.25	0.10	0.75
6.00	28.33	44.95	1.90	85.55	2.29	0.10	0.75
6.06	27.33	43.34	2.08	90.31	2.34	0.10	0.75
6.11	26.22	41.55	2.32	96.46	2.39	0.10	0.75
6.20	26.32	41.71	2.45	102.05	2.41	0.10	0.75
6.25	25.82	40.90	2.59	106.03	2.44	0.11	0.75
6.31	25.41	40.23	2.73	109.83	2.46	0.11	0.75

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
6.39	25.31	40.06	2.86	114.58	2.48	0.11	0.75
6.45	27.33	43.30	2.60	112.37	2.44	0.11	0.75
6.50	29.54	46.85	2.34	109.84	2.39	0.11	0.76
6.59	31.25	49.59	2.23	110.44	2.37	0.11	0.76
6.65	30.54	48.44	2.36	114.47	2.40	0.11	0.76
6.70	28.53	45.21	2.72	122.80	2.46	0.11	0.76
6.79	25.62	40.53	3.33	134.79	2.55	0.11	0.75
6.85	23.30	36.79	3.82	140.55	2.61	0.10	0.62
6.90	20.79	32.76	4.48	146.86	2.68	0.10	0.62
6.99	19.28	30.32	4.97	150.78	2.72	0.10	0.62
7.05	18.98	29.83	5.21	155.39	2.75	0.10	0.62
7.10	18.68	29.35	5.63	165.32	2.78	0.10	0.62
7.17	18.58	29.18	6.10	177.97	2.82	0.10	0.62
7.23	18.47	29.00	6.39	185.40	2.84	0.10	0.62
7.32	21.59	34.01	5.04	171.44	2.73	0.10	0.62
7.38	23.10	36.43	4.39	159.95	2.67	0.10	0.62
7.43	24.61	38.85	3.90	151.53	2.62	0.11	0.62
7.51	31.85	50.48	2.62	132.11	2.44	0.11	0.76
7.57	38.29	60.82	2.01	122.41	2.32	0.12	0.77
7.62	44.12	70.18	1.69	118.36	2.23	0.12	0.78
7.71	50.15	79.86	1.48	118.14	2.14	0.13	0.79
7.77	52.67	83.90	1.42	119.32	2.10	0.13	0.79
7.82	54.78	87.29	1.39	120.96	2.08	0.13	0.79
7.91	57.70	91.97	1.36	125.49	2.06	0.13	0.79
7.97	59.21	94.39	1.36	128.03	2.05	0.13	0.80
8.01	60.01	95.67	1.35	129.55	2.05	0.13	0.80
8.07	60.71	96.79	1.36	131.16	2.05	0.13	0.80
8.17	60.31	96.14	1.38	132.27	2.07	0.14	0.80
8.21	59.91	95.42	1.39	132.45	2.08	0.14	0.80
8.30	59.91	94.97	1.40	132.89	2.09	0.14	0.80
8.36	59.91	94.64	1.41	133.05	2.09	0.14	0.80
8.41	59.91	94.39	1.41	133.06	2.09	0.14	0.80
8.50	61.52	95.92	1.39	133.74	2.08	0.14	0.80
8.56	62.83	97.18	1.38	134.09	2.07	0.14	0.80
8.61	63.93	98.24	1.37	134.46	2.06	0.14	0.80
8.66	64.94	99.16	1.36	134.64	2.05	0.14	0.80
8.73	65.14	98.75	1.35	133.30	2.05	0.14	0.80
8.81	63.23	95.59	1.36	130.41	2.06	0.14	0.80
8.86	60.81	92.06	1.39	127.81	2.08	0.13	0.80
8.96	55.79	84.66	1.45	122.35	2.12	0.13	0.79
9.01	53.88	81.78	1.47	120.45	2.13	0.12	0.79
9.06	48.44	74.38	1.61	119.77	2.20	0.12	0.78
9.13	45.33	69.82	1.70	118.83	2.23	0.12	0.78
9.20	42.51	65.84	1.86	122.14	2.28	0.12	0.77
9.30	35.97	56.74	2.34	132.65	2.39	0.11	0.76
9.35	32.05	50.62	2.73	138.01	2.46	0.11	0.75
9.40	28.23	44.48	3.25	144.70	2.54	0.10	0.74
9.46	25.72	40.44	3.66	147.90	2.59	0.10	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
9.55	22.90	35.90	4.08	146.61	2.64	0.10	0.62
9.60	22.70	35.58	3.97	141.24	2.62	0.10	0.62
9.66	22.70	35.57	3.77	134.09	2.60	0.10	0.62
9.71	24.61	38.51	3.23	124.28	2.53	0.10	0.73
9.80	29.44	44.66	2.46	109.92	2.42	0.10	0.74
9.85	30.64	45.97	2.29	105.10	2.38	0.10	0.74
9.93	31.25	46.22	2.11	97.65	2.35	0.10	0.74
9.98	31.45	46.20	2.06	95.31	2.33	0.10	0.74
10.04	31.65	46.18	2.02	93.28	2.32	0.10	0.74
10.12	31.45	45.59	2.01	91.68	2.32	0.10	0.74
10.19	31.35	45.28	2.05	92.67	2.33	0.10	0.74
10.25	30.95	44.59	2.08	92.59	2.34	0.10	0.74
10.31	30.54	43.91	2.14	94.15	2.35	0.10	0.74
10.39	30.44	43.59	2.18	94.95	2.36	0.10	0.74
10.45	30.54	43.58	2.19	95.52	2.36	0.10	0.74
10.52	30.24	43.01	2.24	96.43	2.37	0.10	0.74
10.58	30.54	43.24	2.24	96.67	2.37	0.10	0.74
10.64	30.84	43.46	2.22	96.67	2.37	0.10	0.74
10.74	29.94	42.03	2.32	97.39	2.39	0.10	0.74
10.79	28.43	39.97	2.48	99.17	2.42	0.10	0.73
10.83	27.53	38.68	2.59	100.31	2.44	0.09	0.73
10.90	23.80	33.72	3.17	106.86	2.53	0.09	0.72
10.96	21.29	30.34	3.70	112.20	2.59	0.09	0.72
11.03	18.47	26.49	4.50	119.15	2.68	0.09	0.62
11.10	14.75	21.39	6.10	130.47	2.82	0.09	0.62
11.18	11.84	17.24	8.13	140.21	2.96	0.08	0.62
11.24	10.73	15.43	7.72	119.17	2.93	0.08	0.62
11.29	9.83	13.89	7.08	98.31	2.89	0.08	0.62
11.36	9.42	13.29	8.40	111.60	2.98	0.08	0.62
11.42	8.92	12.47	9.28	115.64	3.03	0.08	0.89
11.51	8.22	11.32	10.79	122.14	3.11	0.08	0.81
11.57	8.23	11.26	11.08	124.75	3.12	0.08	0.80
11.62	8.23	11.22	11.29	126.65	3.13	0.08	0.80
11.70	8.23	11.14	11.68	130.07	3.15	0.08	0.80
11.75	8.33	11.23	11.75	131.96	3.16	0.08	0.80
11.83	8.93	12.03	11.19	134.57	3.13	0.08	0.86
11.90	9.53	12.83	10.80	138.56	3.11	0.08	0.92
11.95	10.34	13.94	10.15	141.42	3.08	0.08	1.00
12.03	11.75	15.87	9.08	144.14	3.02	0.08	1.13
12.10	12.75	17.21	8.51	146.53	2.98	0.08	0.62
12.15	13.36	18.00	8.25	148.56	2.97	0.08	0.62
12.21	13.86	18.62	8.08	150.44	2.96	0.09	0.62
12.28	14.36	19.20	8.01	153.75	2.95	0.09	0.62
12.34	14.66	19.53	7.99	156.11	2.95	0.09	0.62
12.40	14.86	19.70	8.06	158.71	2.96	0.09	0.62
12.48	15.47	20.42	7.83	159.87	2.94	0.09	0.62
12.55	16.07	21.13	7.62	161.03	2.93	0.09	0.62
12.60	16.57	21.69	7.49	162.53	2.92	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
12.70	17.28	22.46	7.36	165.39	2.91	0.09	0.62
12.75	17.88	23.14	7.18	166.26	2.90	0.09	0.62
12.80	18.48	23.81	7.02	167.11	2.89	0.09	0.62
12.89	19.49	24.91	6.64	165.43	2.86	0.09	0.62
12.94	20.40	25.91	6.30	163.27	2.83	0.09	0.62
13.00	21.30	26.89	5.97	160.55	2.81	0.09	0.62
13.09	22.51	28.16	5.55	156.35	2.78	0.09	0.62
13.14	23.41	29.11	5.26	153.20	2.75	0.09	0.62
13.19	24.72	30.56	4.88	149.21	2.72	0.10	0.62
13.28	25.32	31.06	4.72	146.66	2.70	0.10	0.62
13.34	26.63	32.46	4.41	143.06	2.67	0.10	0.62
13.39	27.54	33.40	4.21	140.65	2.65	0.10	0.62
13.47	29.25	35.20	3.87	136.23	2.61	0.10	0.62
13.53	30.35	36.30	3.67	133.17	2.59	0.10	0.74
13.59	31.36	37.32	3.51	130.89	2.57	0.10	0.74
13.67	33.47	39.49	3.17	125.22	2.53	0.10	0.74
13.73	34.78	40.80	2.98	121.58	2.50	0.10	0.74
13.79	36.69	42.76	2.73	116.62	2.46	0.10	0.75
13.88	40.21	46.38	2.35	109.14	2.40	0.11	0.75
13.93	42.52	48.77	2.17	105.92	2.36	0.11	0.76
13.99	44.53	50.75	2.01	102.26	2.32	0.11	0.76
14.07	47.05	53.22	1.88	99.86	2.29	0.11	0.76
14.13	48.66	54.78	1.80	98.70	2.27	0.11	0.76
14.18	49.76	55.82	1.76	98.14	2.25	0.11	0.77
14.28	51.17	57.03	1.70	97.05	2.23	0.11	0.77
14.33	52.28	58.05	1.66	96.55	2.22	0.11	0.77
14.38	52.98	58.65	1.64	96.45	2.21	0.11	0.77
14.48	55.19	60.70	1.59	96.34	2.19	0.11	0.77
14.53	56.30	61.77	1.59	97.93	2.19	0.11	0.77
14.58	56.80	62.18	1.59	98.99	2.19	0.11	0.77
14.65	58.41	63.65	1.56	99.35	2.18	0.12	0.78
14.72	59.01	64.07	1.55	99.41	2.17	0.12	0.78
14.78	59.52	64.44	1.55	99.59	2.17	0.12	0.78
14.83	60.12	64.91	1.54	99.99	2.17	0.12	0.78
14.92	60.22	64.77	1.55	100.70	2.17	0.12	0.78
14.98	60.42	64.81	1.56	101.27	2.18	0.12	0.78
15.05	60.22	64.36	1.57	100.99	2.18	0.12	0.78
15.12	60.22	64.15	1.57	100.82	2.18	0.12	0.78
15.16	60.32	64.13	1.57	100.86	2.18	0.12	0.78
15.22	60.72	64.36	1.57	101.11	2.18	0.12	0.78
15.32	60.92	64.28	1.57	101.10	2.18	0.12	0.78
15.37	60.92	64.12	1.57	100.79	2.18	0.12	0.78
15.46	61.03	63.96	1.57	100.62	2.18	0.12	0.78
15.52	61.23	63.98	1.57	100.66	2.18	0.12	0.78
15.56	61.43	64.07	1.57	100.88	2.18	0.12	0.78
15.66	62.03	64.07	1.42	90.68	2.10	0.11	0.77
15.71	62.33	64.25	1.42	90.95	2.10	0.11	0.77
15.75	62.43	64.24	1.42	91.29	2.10	0.11	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
15.86	62.84	64.38	1.43	92.19	2.11	0.11	0.77
15.91	62.84	64.25	1.44	92.52	2.11	0.11	0.77
15.96	62.75	64.03	1.45	92.69	2.12	0.11	0.77
16.02	59.13	60.24	1.52	91.57	2.16	0.11	0.77
16.10	61.95	62.84	1.47	92.40	2.13	0.11	0.77
16.16	61.75	62.47	1.48	92.27	2.14	0.11	0.77
16.21	61.65	62.25	1.50	93.10	2.15	0.11	0.77
16.29	62.05	62.46	1.51	94.13	2.15	0.11	0.77
16.36	62.35	62.56	1.51	94.52	2.15	0.11	0.77
16.41	62.45	62.53	1.51	94.51	2.15	0.11	0.77
16.51	61.65	61.45	1.52	93.54	2.16	0.11	0.77
16.56	60.24	59.92	1.55	92.89	2.17	0.11	0.77
16.61	58.43	57.99	1.59	92.13	2.19	0.11	0.77
16.71	54.31	53.67	1.71	91.63	2.23	0.11	0.77
16.76	50.99	50.28	1.83	91.92	2.27	0.11	0.76
16.81	47.07	46.29	2.00	92.52	2.32	0.10	0.76
16.89	39.72	38.86	2.50	97.30	2.42	0.10	0.74
16.95	34.29	33.40	3.13	104.39	2.52	0.10	0.73
17.00	28.46	27.57	4.19	115.66	2.65	0.09	0.62
17.10	21.22	20.29	6.48	131.48	2.85	0.09	0.62
17.14	18.81	17.84	7.53	134.38	2.92	0.09	0.62
17.20	17.50	16.47	8.08	133.14	2.96	0.09	0.62
17.29	16.49	15.37	8.25	126.78	2.97	0.08	0.62
17.33	15.69	14.55	8.56	124.60	2.99	0.08	0.62
17.39	14.58	13.40	9.08	121.69	3.02	0.08	0.96
17.46	13.98	12.75	9.24	117.87	3.03	0.08	0.91
17.52	13.88	12.61	9.05	114.04	3.02	0.08	0.90
17.59	13.78	12.46	8.96	111.62	3.01	0.08	0.89
17.70	13.48	12.09	9.20	111.28	3.02	0.08	0.86
17.72	13.68	12.27	9.10	111.66	3.02	0.08	0.88
17.80	14.38	12.88	8.88	114.37	3.01	0.08	0.92
17.85	15.89	14.30	8.22	117.56	2.97	0.08	0.62
17.92	17.10	15.41	7.96	122.70	2.95	0.09	0.62
17.99	20.01	18.12	7.03	127.38	2.89	0.09	0.62
18.05	22.83	20.74	6.31	130.90	2.84	0.09	0.62
18.14	25.75	23.40	5.51	128.92	2.77	0.09	0.62
18.18	29.47	26.87	4.61	123.91	2.69	0.10	0.62
18.25	35.20	32.16	3.64	117.04	2.59	0.10	0.74
18.32	39.32	35.92	3.12	112.12	2.52	0.10	0.74
18.39	44.75	40.90	2.58	105.50	2.44	0.11	0.75
18.45	47.27	43.15	2.36	101.62	2.40	0.11	0.76
18.50	49.68	45.29	2.17	98.23	2.36	0.11	0.76
18.57	51.79	47.12	1.99	93.98	2.32	0.11	0.76
18.64	54.51	49.52	1.84	91.05	2.28	0.11	0.76
18.73	56.02	50.75	1.77	90.03	2.26	0.11	0.76
18.78	58.13	52.58	1.71	90.04	2.24	0.11	0.77
18.85	59.24	53.47	1.67	89.24	2.22	0.11	0.77
18.91	60.24	54.27	1.62	87.70	2.20	0.11	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
18.97	61.25	55.07	1.58	87.26	2.19	0.11	0.77
19.03	62.25	55.85	1.58	88.26	2.19	0.11	0.77
19.11	63.16	56.50	1.59	89.78	2.19	0.11	0.77
19.17	63.56	56.70	1.60	90.90	2.20	0.11	0.77
19.23	63.36	56.38	1.63	91.83	2.21	0.11	0.77
19.31	63.16	56.01	1.65	92.37	2.21	0.11	0.77
19.39	64.16	56.73	1.64	93.26	2.21	0.11	0.77
19.43	64.57	56.99	1.65	93.87	2.21	0.12	0.78
19.49	64.57	56.83	1.70	96.85	2.23	0.12	0.78
19.57	62.76	54.97	1.80	98.84	2.26	0.12	0.78
19.65	55.82	48.48	2.20	106.47	2.36	0.11	0.77
19.69	52.90	45.73	2.49	113.74	2.42	0.11	0.76
19.79	38.72	32.82	4.03	132.26	2.63	0.10	0.62
19.83	34.60	29.10	4.71	137.07	2.70	0.10	0.62
19.89	29.06	24.12	5.85	141.16	2.80	0.10	0.62
19.97	25.65	21.03	6.56	137.89	2.85	0.09	0.62
20.03	17.70	14.15	10.08	142.64	3.07	0.08	1.01
20.08	15.69	12.39	11.27	139.72	3.13	0.08	0.89
20.17	13.78	10.72	12.93	138.59	3.21	0.08	0.77
20.23	12.77	9.82	13.58	133.39	3.24	0.08	0.70
20.28	11.97	9.12	13.95	127.31	3.25	0.08	0.65
20.37	11.26	8.48	13.75	116.56	3.24	0.08	0.61
20.42	10.96	8.21	13.94	114.38	3.25	0.08	0.59
20.47	10.86	8.10	13.95	113.02	3.25	0.08	0.58
20.55	11.16	8.32	13.37	111.20	3.23	0.08	0.59
20.63	10.76	7.95	13.94	110.84	3.25	0.08	0.57
20.67	10.66	7.85	14.06	110.37	3.26	0.08	0.56
20.77	10.46	7.64	14.32	109.48	3.27	0.08	0.55
20.82	10.56	7.71	14.18	109.31	3.26	0.08	0.55
20.88	10.56	7.68	14.22	109.29	3.26	0.08	0.55
20.96	10.56	7.65	14.28	109.29	3.26	0.08	0.55
21.01	10.56	7.63	14.39	109.82	3.27	0.08	0.55
21.06	10.66	7.69	14.41	110.90	3.27	0.08	0.55
21.17	11.06	7.98	14.14	112.82	3.26	0.08	0.57
21.21	11.57	8.37	13.54	113.37	3.23	0.08	0.60
21.26	12.07	8.75	13.09	114.62	3.22	0.08	0.63
21.33	12.88	9.37	12.43	116.45	3.19	0.08	0.67
21.40	13.29	9.66	12.30	118.91	3.18	0.08	0.69
21.46	13.69	9.95	12.23	121.70	3.18	0.08	0.71
21.55	14.29	10.39	11.96	124.30	3.17	0.08	0.74
21.61	14.59	10.60	11.93	126.41	3.16	0.08	0.76
21.66	15.10	10.97	11.71	128.50	3.15	0.08	0.78
21.75	15.10	10.93	12.01	131.27	3.17	0.08	0.78
21.81	15.30	11.05	11.94	131.94	3.16	0.08	0.79
21.86	15.30	11.02	11.99	132.21	3.17	0.08	0.79
21.94	15.30	10.98	11.83	129.89	3.16	0.08	0.78
22.00	14.99	10.71	11.31	121.09	3.13	0.08	0.76
22.06	14.99	10.68	9.24	98.69	3.03	0.08	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
22.14	14.99	10.63	11.41	121.28	3.14	0.08	0.76
22.20	14.99	10.60	11.15	118.23	3.13	0.08	0.76
22.25	15.10	10.66	11.63	123.94	3.15	0.08	0.76
22.34	13.39	9.30	14.21	132.16	3.26	0.08	0.66
22.40	16.00	11.28	12.00	135.32	3.17	0.08	0.81
22.47	16.30	11.47	12.10	138.76	3.17	0.08	0.82
22.52	16.20	11.36	12.35	140.29	3.18	0.08	0.81
22.61	16.10	11.23	12.50	140.41	3.19	0.08	0.80
22.67	16.10	11.20	12.53	140.34	3.19	0.08	0.80
22.72	16.10	11.18	12.55	140.27	3.19	0.08	0.80
22.78	16.10	11.15	12.56	140.02	3.19	0.08	0.80
22.86	16.10	11.10	12.56	139.44	3.19	0.08	0.79
22.92	16.10	11.07	12.61	139.61	3.19	0.08	0.79
22.97	16.10	11.04	12.74	140.73	3.20	0.08	0.79
23.06	16.10	10.99	12.96	142.54	3.21	0.08	0.79
23.12	16.40	11.19	12.79	143.08	3.20	0.08	0.80
23.17	16.81	11.47	12.49	143.21	3.19	0.08	0.82
23.26	17.91	12.23	11.64	142.27	3.15	0.08	0.87
23.31	18.62	12.72	11.13	141.58	3.13	0.08	0.91
23.41	19.22	13.11	10.79	141.41	3.11	0.08	0.94
23.46	19.12	13.00	10.78	140.12	3.11	0.08	0.93
23.51	19.02	12.90	10.78	139.06	3.11	0.08	0.92
23.56	18.72	12.65	10.94	138.42	3.12	0.08	0.90
23.65	18.01	12.08	11.56	139.63	3.15	0.08	0.86
23.71	17.71	11.83	11.81	139.73	3.16	0.08	0.85
23.75	17.61	11.73	11.96	140.28	3.17	0.08	0.84
23.85	17.21	11.39	12.39	141.16	3.18	0.08	0.81
23.91	17.11	11.29	12.51	141.21	3.19	0.08	0.81
23.95	17.01	11.19	12.63	141.43	3.20	0.08	0.80
24.04	16.70	10.93	13.09	143.05	3.22	0.08	0.78
24.10	16.81	10.98	13.09	143.73	3.22	0.08	0.78
24.15	16.91	11.02	13.15	144.96	3.22	0.08	0.79
24.25	17.71	11.54	12.66	146.10	3.20	0.08	0.82
24.30	18.41	12.01	12.22	146.75	3.18	0.08	0.86
24.36	19.12	12.48	11.93	148.82	3.16	0.08	0.89
24.45	19.72	12.85	11.57	148.65	3.15	0.08	0.92
24.50	19.52	12.68	11.72	148.55	3.15	0.08	0.91
24.55	19.22	12.44	12.04	149.78	3.17	0.08	0.89
24.64	19.42	12.52	12.25	153.48	3.18	0.08	0.89
24.69	20.53	13.27	11.50	152.63	3.14	0.09	0.95
24.75	22.64	14.70	10.05	147.68	3.07	0.09	1.05
24.84	28.37	18.60	7.33	136.30	2.91	0.09	0.62
24.89	33.10	21.91	5.87	128.72	2.80	0.10	0.62
24.95	41.55	28.28	4.01	113.51	2.63	0.10	0.62
25.02	52.81	37.16	2.35	87.15	2.39	0.10	0.75
25.07	58.54	41.51	2.10	87.00	2.34	0.11	0.76
25.14	65.88	47.02	1.89	88.98	2.29	0.11	0.77
25.23	69.00	49.24	1.83	90.27	2.27	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
25.29	68.80	48.97	1.85	90.76	2.28	0.12	0.77
25.36	64.48	45.41	2.06	93.35	2.33	0.11	0.77
25.41	62.26	43.55	2.20	95.63	2.36	0.11	0.77
25.48	55.22	37.99	2.66	100.92	2.45	0.11	0.76
25.55	48.48	32.75	3.28	107.55	2.54	0.11	0.75
25.61	37.52	24.49	4.87	119.22	2.72	0.10	0.62
25.66	30.48	19.35	6.47	125.26	2.85	0.09	0.62
25.75	24.35	15.20	8.34	126.83	2.97	0.09	0.62
25.80	21.73	13.43	9.30	124.92	3.03	0.09	0.96
25.86	20.33	12.47	9.70	121.04	3.05	0.08	0.89
25.94	18.51	11.23	10.10	113.35	3.07	0.08	0.80
25.99	18.51	11.20	9.56	107.08	3.04	0.08	0.80
26.06	18.21	10.98	8.79	96.48	3.00	0.08	0.78
26.12	17.51	10.49	8.77	91.98	3.00	0.08	0.62
26.19	17.31	10.33	8.51	87.89	2.98	0.08	0.62
26.25	17.41	10.37	8.43	87.41	2.98	0.08	0.62
26.34	17.62	10.47	8.30	86.82	2.97	0.08	0.62
26.38	18.22	10.84	7.92	85.82	2.95	0.08	0.62
26.45	18.52	11.01	7.80	85.91	2.94	0.08	0.62
26.54	17.93	10.59	8.76	92.74	3.00	0.08	0.62
26.59	18.04	10.63	9.18	97.60	3.02	0.08	0.76
26.65	18.34	10.80	10.10	109.14	3.07	0.08	0.77
26.71	19.25	11.36	10.43	118.52	3.09	0.08	0.81
26.78	20.77	12.30	10.20	125.46	3.08	0.08	0.88
26.84	25.91	15.55	8.16	126.83	2.96	0.09	0.62
26.94	32.25	19.52	6.54	127.65	2.85	0.09	0.62
26.98	32.15	19.43	6.64	129.12	2.86	0.09	0.62
27.04	30.64	18.43	7.14	131.49	2.90	0.09	0.62
27.11	29.03	17.36	7.53	130.62	2.92	0.09	0.62
27.18	28.23	16.81	7.54	126.64	2.92	0.09	0.62
27.23	26.32	15.56	7.83	121.86	2.94	0.09	0.62
27.32	22.50	13.12	8.92	117.02	3.01	0.09	0.94
27.38	20.59	11.89	9.43	112.11	3.04	0.08	0.85
27.43	18.47	10.54	10.49	110.51	3.09	0.08	0.75
27.52	15.96	8.94	12.37	110.56	3.18	0.08	0.64
27.58	14.55	8.04	13.77	110.76	3.24	0.08	0.57
27.63	14.05	7.72	14.20	109.58	3.26	0.08	0.55
27.73	13.55	7.38	14.33	105.75	3.27	0.08	0.53
27.78	13.35	7.24	14.41	104.37	3.27	0.08	0.52
27.83	13.65	7.41	13.85	102.66	3.25	0.08	0.53
27.91	14.35	7.82	12.80	100.09	3.20	0.08	0.56
27.98	14.85	8.10	12.18	98.70	3.18	0.08	0.58
28.03	15.16	8.28	11.67	96.63	3.15	0.08	0.59
28.11	15.26	8.32	11.57	96.21	3.15	0.08	0.59
28.18	15.96	8.72	12.14	105.89	3.17	0.08	0.62
28.22	17.17	9.44	11.75	110.90	3.16	0.08	0.67
28.32	27.54	15.68	7.09	111.15	2.89	0.09	0.62
28.35	32.46	18.69	5.82	108.79	2.80	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
28.43	56.50	35.12	2.73	95.97	2.46	0.11	0.75
28.48	62.23	39.03	2.47	96.22	2.42	0.11	0.76
28.56	73.09	46.51	2.09	97.16	2.34	0.12	0.78
28.63	77.12	49.17	2.02	99.41	2.32	0.13	0.78
28.68	78.62	50.12	2.00	100.02	2.32	0.13	0.79
28.74	81.14	51.77	1.95	100.86	2.31	0.13	0.79
28.82	84.66	54.11	1.87	101.42	2.29	0.13	0.79
28.88	87.17	55.81	1.82	101.55	2.27	0.13	0.80
28.95	95.02	61.33	1.67	102.32	2.22	0.14	0.80
29.02	99.74	64.59	1.60	103.58	2.20	0.15	0.81
29.08	102.76	66.68	1.56	104.06	2.18	0.15	0.81
29.15	102.66	66.44	1.57	104.15	2.18	0.15	0.81
29.21	98.93	63.58	1.63	103.65	2.21	0.14	0.81
29.27	92.59	58.81	1.76	103.62	2.25	0.14	0.80
29.37	79.92	49.44	2.19	108.11	2.36	0.13	0.79
29.40	69.86	42.30	2.70	114.14	2.46	0.12	0.78
29.46	60.41	35.63	3.46	123.20	2.56	0.12	0.76
29.54	45.02	25.31	5.32	134.69	2.76	0.10	0.62
29.60	36.28	19.97	7.00	139.73	2.89	0.10	0.62
29.67	30.54	16.61	8.23	136.70	2.97	0.09	0.62
29.73	24.51	13.10	10.34	135.46	3.09	0.09	0.94
29.81	20.79	10.93	11.80	128.93	3.16	0.08	0.78
29.86	20.18	10.56	11.95	126.25	3.16	0.08	0.75
29.96	23.00	12.13	10.43	126.57	3.09	0.09	0.87
29.99	27.22	14.52	8.64	125.43	2.99	0.09	0.62
30.06	32.35	17.42	54.25	944.77	4.06	0.09	1.24
30.14	38.69	20.98	54.25	1138.15	4.06	0.10	1.50
30.20	46.33	25.28	54.25	1371.66	4.06	0.11	1.81
30.26	52.47	28.72	54.25	1558.07	4.06	0.12	2.05
30.33	60.41	33.16	54.25	1798.79	4.06	0.13	2.37
30.38	62.93	34.54	54.25	1873.61	4.06	0.13	2.47

Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

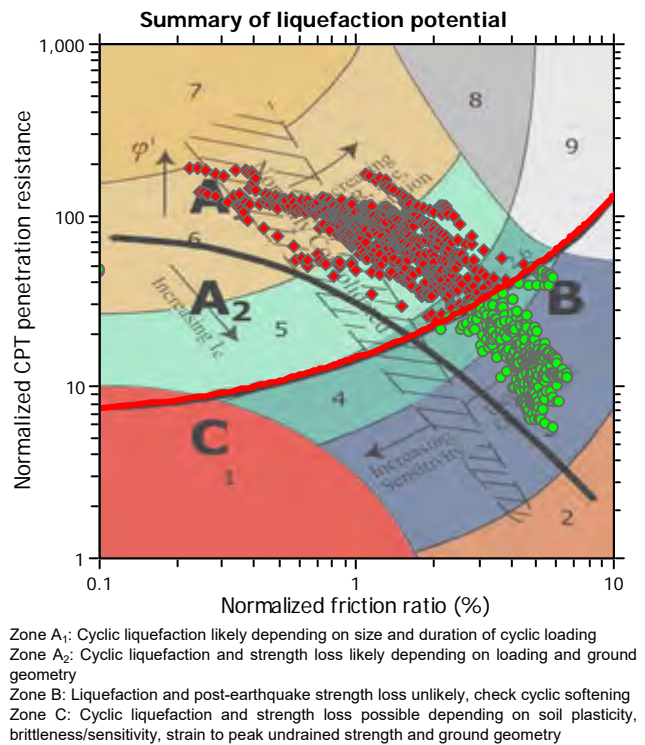
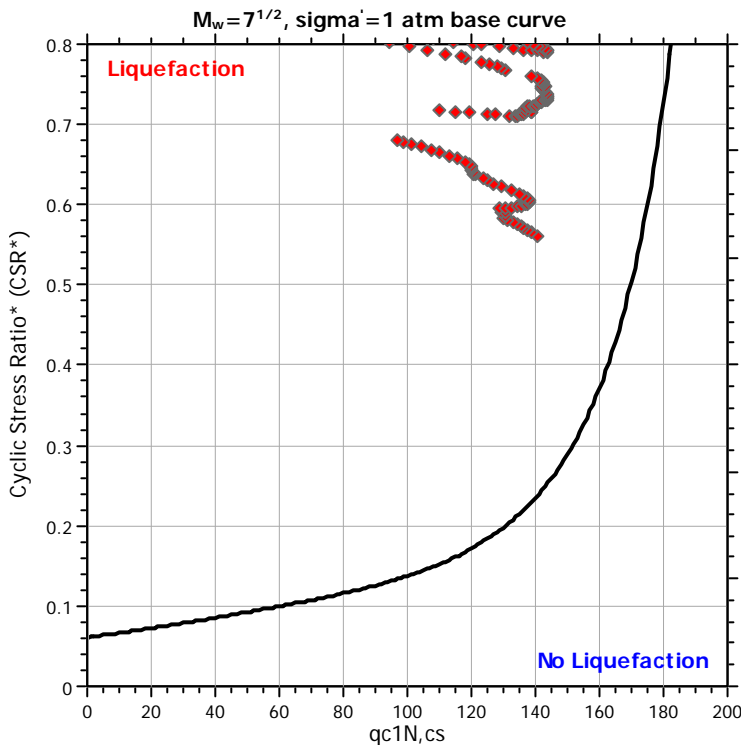
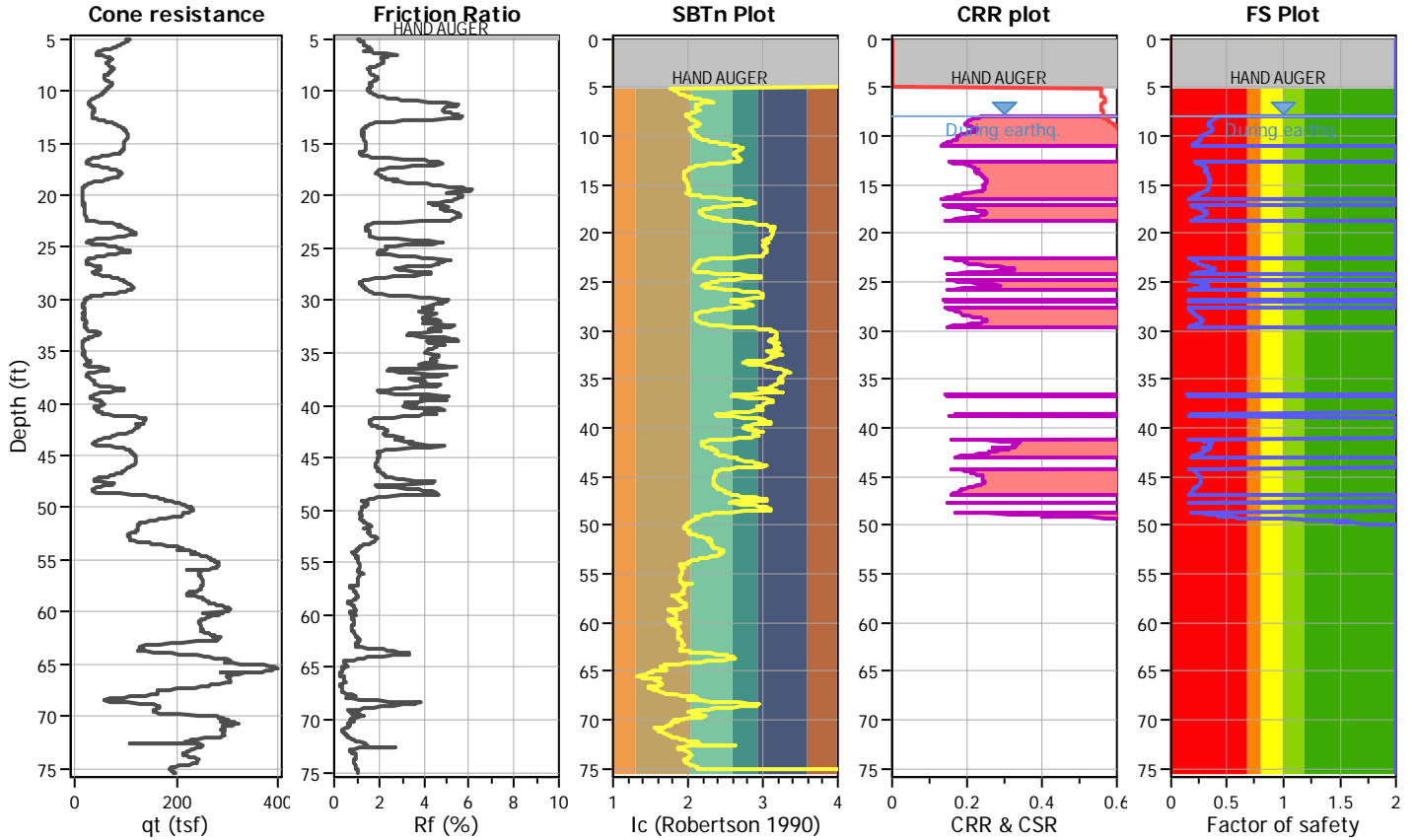
LIQUEFACTION ANALYSIS REPORT

Project title : Universal Engineering Services / Compton
CPT file : CPT-4

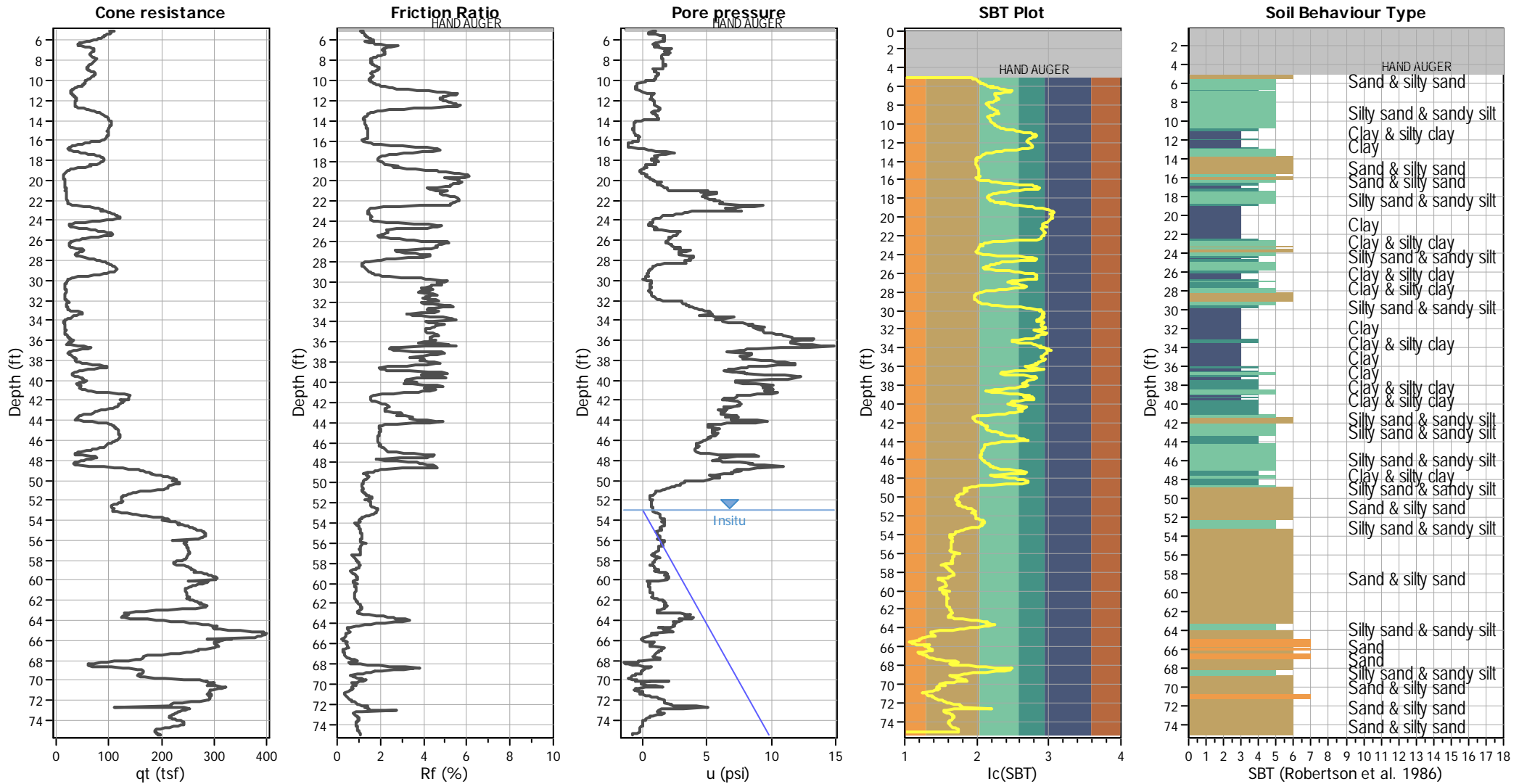
Location : 1111 E. Artesia Blvd, Compton, CA

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	52.90 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	1	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w :	7.30	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method
Peak ground acceleration:	0.77	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



CPT basic interpretation plots



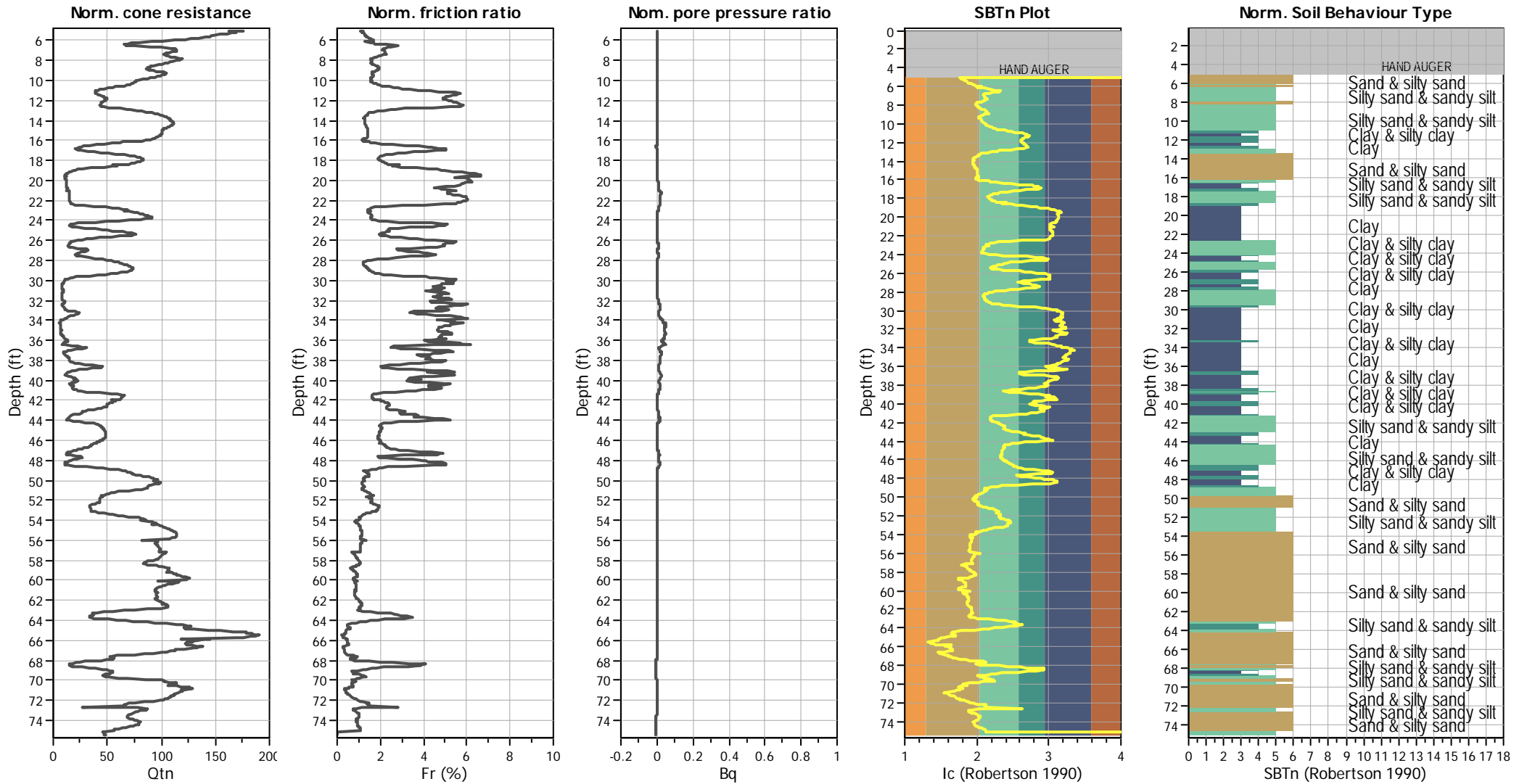
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_g applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

■ 1. Sensitive fine grained	■ 4. Clayey silt to silty	■ 7. Gravely sand to sand
■ 2. Organic material	■ 5. Silty sand to sandy silt	■ 8. Very stiff sand to
■ 3. Clay to silty clay	■ 6. Clean sand to silty sand	■ 9. Very stiff fine grained

CPT basic interpretation plots (normalized)



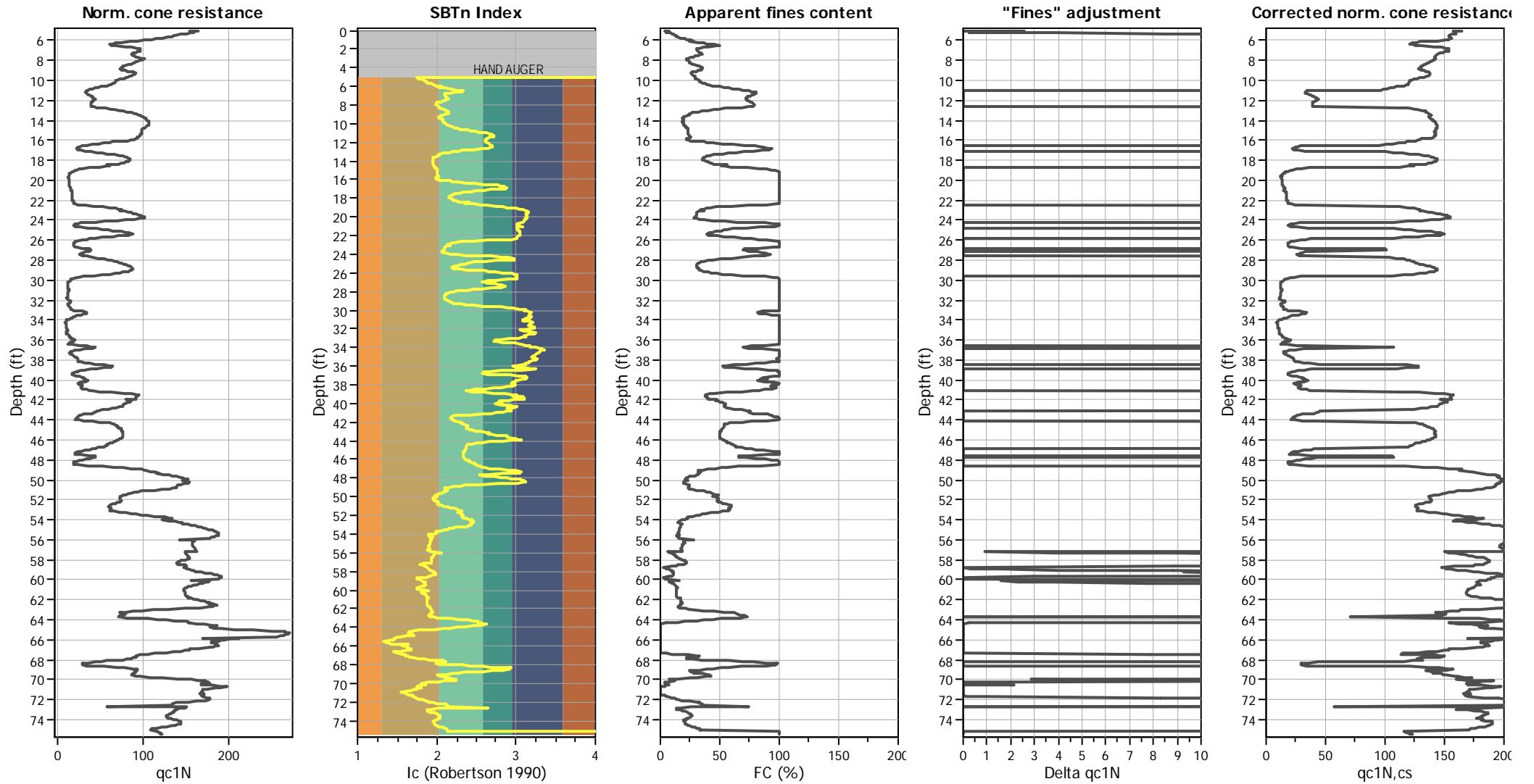
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

■ 1. Sensitive fine grained	■ 4. Clayey silt to silty	■ 7. Gravely sand to sand
■ 2. Organic material	■ 5. Silty sand to sandy silt	■ 8. Very stiff sand to
■ 3. Clay to silty clay	■ 6. Clean sand to silty sand	■ 9. Very stiff fine grained

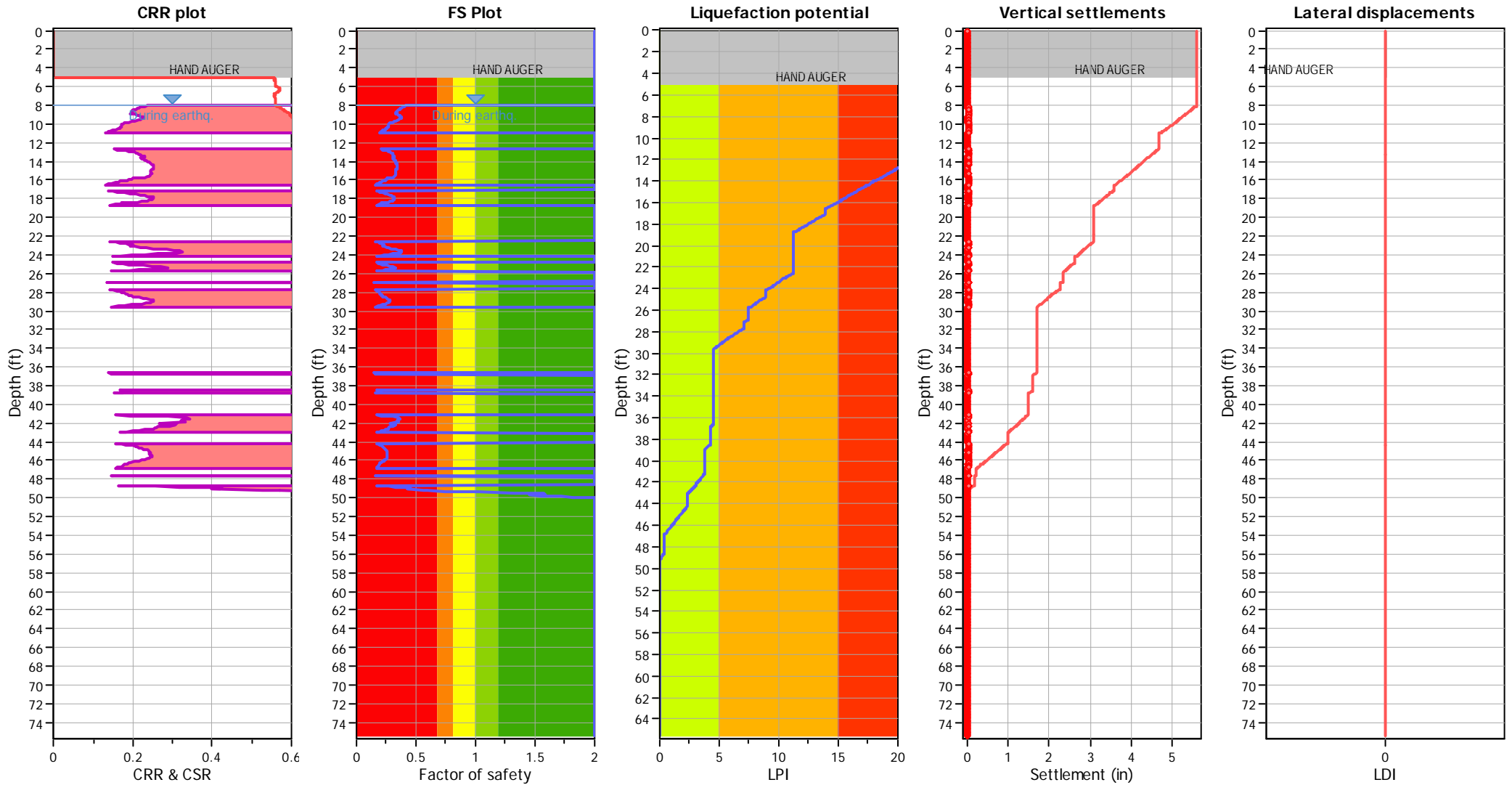
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

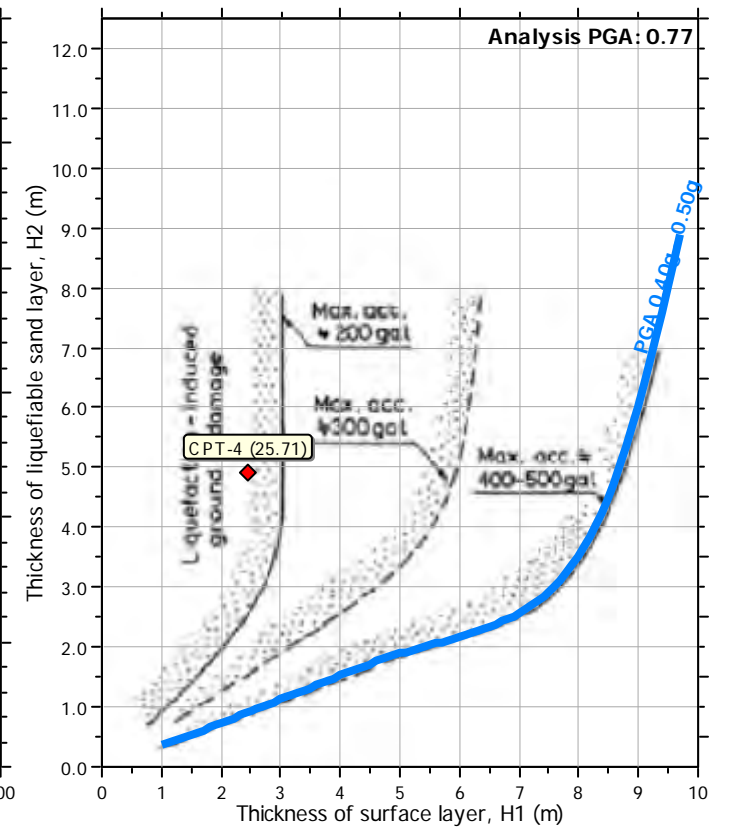
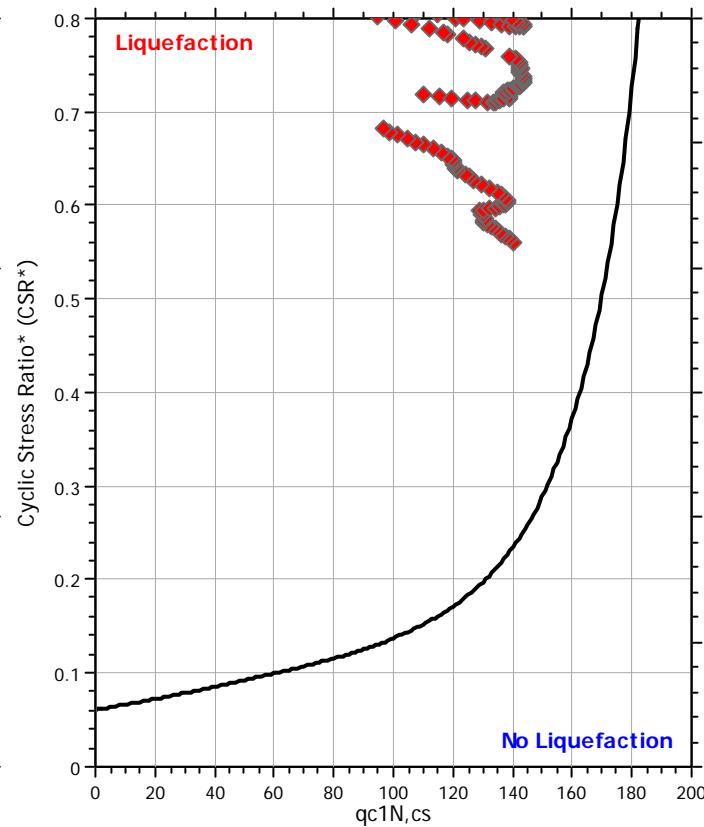
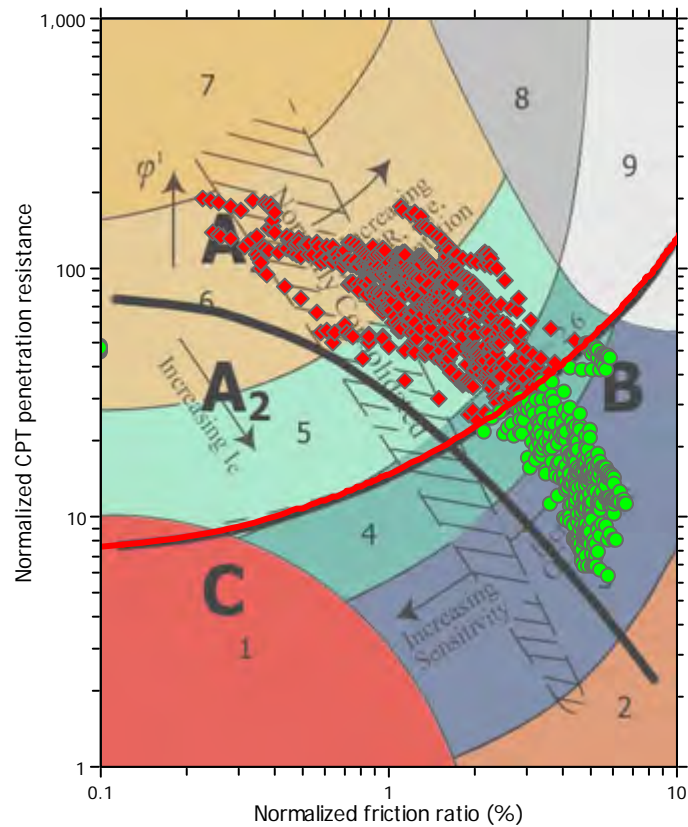
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

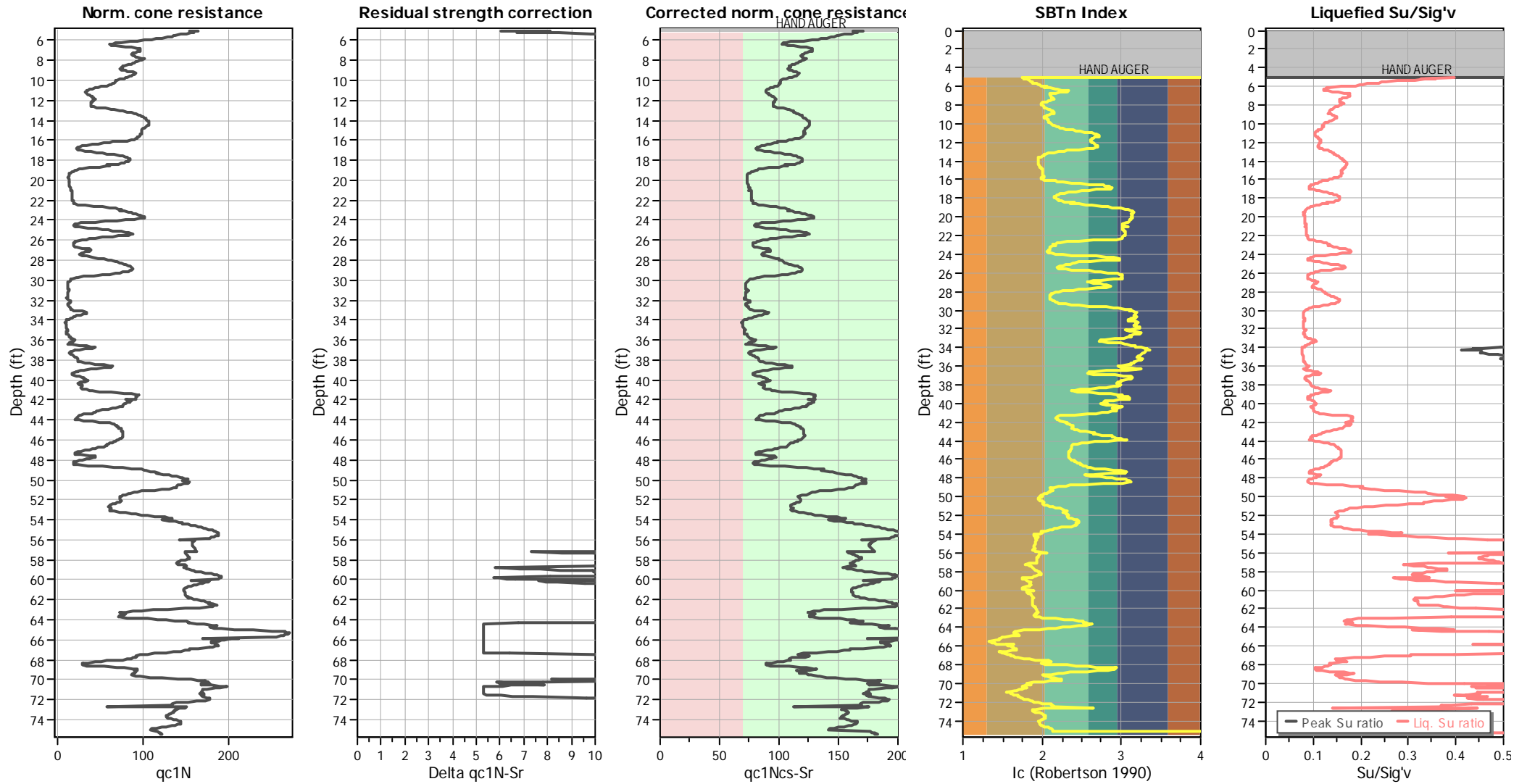
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.07	-9999.00	-9999.00	-9999.00	100.00	120.90
2	0.14	-9999.00	-9999.00	-9999.00	100.00	120.90
3	0.21	-9999.00	-9999.00	-9999.00	100.00	120.90
4	0.28	-9999.00	-9999.00	-9999.00	100.00	120.90
5	0.33	-9999.00	-9999.00	-9999.00	100.00	120.90
6	0.41	-9999.00	-9999.00	-9999.00	100.00	120.90
7	0.46	-9999.00	-9999.00	-9999.00	100.00	120.90
8	0.54	-9999.00	-9999.00	-9999.00	100.00	120.90
9	0.60	-9999.00	-9999.00	-9999.00	100.00	120.90
10	0.66	-9999.00	-9999.00	-9999.00	100.00	120.90
11	0.72	-9999.00	-9999.00	-9999.00	100.00	120.90
12	0.80	-9999.00	-9999.00	-9999.00	100.00	120.90
13	0.86	-9999.00	-9999.00	-9999.00	100.00	120.90
14	0.92	-9999.00	-9999.00	-9999.00	100.00	120.90
15	0.99	-9999.00	-9999.00	-9999.00	100.00	120.90
16	1.06	-9999.00	-9999.00	-9999.00	100.00	120.90
17	1.11	-9999.00	-9999.00	-9999.00	100.00	120.90
18	1.18	-9999.00	-9999.00	-9999.00	100.00	120.90
19	1.26	-9999.00	-9999.00	-9999.00	100.00	120.90
20	1.33	-9999.00	-9999.00	-9999.00	100.00	120.90
21	1.39	-9999.00	-9999.00	-9999.00	100.00	120.90
22	1.46	-9999.00	-9999.00	-9999.00	100.00	120.90
23	1.51	-9999.00	-9999.00	-9999.00	100.00	120.90
24	1.59	-9999.00	-9999.00	-9999.00	100.00	120.90
25	1.65	-9999.00	-9999.00	-9999.00	100.00	120.90
26	1.71	-9999.00	-9999.00	-9999.00	100.00	120.90
27	1.79	-9999.00	-9999.00	-9999.00	100.00	120.90
28	1.84	-9999.00	-9999.00	-9999.00	100.00	120.90
29	1.92	-9999.00	-9999.00	-9999.00	100.00	120.90
30	1.97	-9999.00	-9999.00	-9999.00	100.00	120.90
31	2.05	-9999.00	-9999.00	-9999.00	100.00	120.90
32	2.11	-9999.00	-9999.00	-9999.00	100.00	120.90
33	2.18	-9999.00	-9999.00	-9999.00	100.00	120.90
34	2.24	-9999.00	-9999.00	-9999.00	100.00	120.90
35	2.31	-9999.00	-9999.00	-9999.00	100.00	120.90
36	2.37	-9999.00	-9999.00	-9999.00	100.00	120.90
37	2.44	-9999.00	-9999.00	-9999.00	100.00	120.90
38	2.50	-9999.00	-9999.00	-9999.00	100.00	120.90
39	2.58	-9999.00	-9999.00	-9999.00	100.00	120.90
40	2.64	-9999.00	-9999.00	-9999.00	100.00	120.90
41	2.71	-9999.00	-9999.00	-9999.00	100.00	120.90
42	2.76	-9999.00	-9999.00	-9999.00	100.00	120.90
43	2.82	-9999.00	-9999.00	-9999.00	100.00	120.90
44	2.90	-9999.00	-9999.00	-9999.00	100.00	120.90
45	2.97	-9999.00	-9999.00	-9999.00	100.00	120.90
46	3.03	-9999.00	-9999.00	-9999.00	100.00	120.90
47	3.09	-9999.00	-9999.00	-9999.00	100.00	120.90
48	3.15	-9999.00	-9999.00	-9999.00	100.00	120.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.22	-9999.00	-9999.00	-9999.00	100.00	120.90
50	3.30	-9999.00	-9999.00	-9999.00	100.00	120.90
51	3.36	-9999.00	-9999.00	-9999.00	100.00	120.90
52	3.42	-9999.00	-9999.00	-9999.00	100.00	120.90
53	3.48	-9999.00	-9999.00	-9999.00	100.00	120.90
54	3.55	-9999.00	-9999.00	-9999.00	100.00	120.90
55	3.61	-9999.00	-9999.00	-9999.00	100.00	120.90
56	3.70	-9999.00	-9999.00	-9999.00	100.00	120.90
57	3.76	-9999.00	-9999.00	-9999.00	100.00	120.90
58	3.82	-9999.00	-9999.00	-9999.00	100.00	120.90
59	3.88	-9999.00	-9999.00	-9999.00	100.00	120.90
60	3.95	-9999.00	-9999.00	-9999.00	100.00	120.90
61	4.01	-9999.00	-9999.00	-9999.00	100.00	120.90
62	4.07	-9999.00	-9999.00	-9999.00	100.00	120.90
63	4.14	-9999.00	-9999.00	-9999.00	100.00	120.90
64	4.20	-9999.00	-9999.00	-9999.00	100.00	120.90
65	4.28	-9999.00	-9999.00	-9999.00	100.00	120.90
66	4.33	-9999.00	-9999.00	-9999.00	100.00	120.90
67	4.42	-9999.00	-9999.00	-9999.00	100.00	120.90
68	4.48	-9999.00	-9999.00	-9999.00	100.00	120.90
69	4.54	-9999.00	-9999.00	-9999.00	100.00	120.90
70	4.60	-9999.00	-9999.00	-9999.00	100.00	120.90
71	4.66	-9999.00	-9999.00	-9999.00	100.00	120.90
72	4.74	-9999.00	-9999.00	-9999.00	100.00	120.90
73	4.80	-9999.00	-9999.00	-9999.00	100.00	120.90
74	4.86	-9999.00	-9999.00	-9999.00	100.00	120.90
75	4.93	-9999.00	-9999.00	-9999.00	100.00	120.90
76	5.00	-9999.00	-9999.00	-9999.00	100.00	120.90
77	5.07	109.33	1.19	1.02	7.24	123.01
78	5.13	101.26	1.19	0.80	8.24	122.84
79	5.18	105.76	1.19	0.45	7.63	122.89
80	5.26	103.23	1.27	0.57	8.40	123.33
81	5.33	100.88	1.30	0.45	8.89	123.46
82	5.38	96.29	1.23	1.02	9.14	122.95
83	5.46	92.25	1.20	1.36	9.53	122.62
84	5.52	91.03	1.20	1.70	9.75	122.62
85	5.59	90.19	1.21	1.70	9.93	122.64
86	5.66	88.03	1.22	1.70	10.37	122.66
87	5.72	83.90	1.24	1.70	11.18	122.63
88	5.79	81.74	1.24	1.59	11.61	122.59
89	5.85	79.58	1.24	1.70	12.02	122.50
90	5.91	76.11	1.22	1.70	12.63	122.30
91	5.98	70.57	1.20	1.70	13.75	121.97
92	6.04	63.35	1.07	1.70	14.63	120.87
93	6.10	56.78	0.73	1.48	13.40	117.85
94	6.19	49.55	0.75	1.14	16.01	117.67
95	6.25	45.23	0.75	1.02	17.80	117.46
96	6.31	42.98	0.75	0.80	18.87	117.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.37	41.10	0.82	0.91	20.74	117.93
98	6.44	42.70	0.97	1.04	21.59	119.18
99	6.51	42.42	1.18	0.91	23.98	120.60
100	6.57	47.02	1.31	1.25	22.87	121.66
101	6.63	56.03	1.40	0.91	19.68	122.53
102	6.70	62.60	1.48	1.14	17.98	123.21
103	6.76	67.66	1.51	1.59	16.70	123.58
104	6.83	70.76	1.50	2.27	15.79	123.64
105	6.89	70.99	1.49	2.04	15.64	123.57
106	6.96	71.60	1.53	1.82	15.78	123.82
107	7.03	71.23	1.57	2.04	16.08	123.96
108	7.09	70.29	1.54	1.70	16.14	123.78
109	7.16	69.07	1.51	2.04	16.28	123.60
110	7.22	67.29	1.48	2.16	16.61	123.41
111	7.29	65.88	1.45	2.04	16.83	123.22
112	7.35	63.82	1.43	2.04	17.26	123.01
113	7.42	64.10	1.37	1.59	16.81	122.75
114	7.50	65.41	1.30	1.48	15.92	122.41
115	7.56	66.72	1.27	1.48	15.29	122.26
116	7.63	68.32	1.24	1.48	14.62	122.13
117	7.69	70.76	1.21	1.48	13.83	122.06
118	7.76	74.23	1.19	1.48	13.00	122.06
119	7.82	76.95	1.19	1.48	12.46	122.11
120	7.88	77.05	1.17	1.59	12.40	122.04
121	7.94	75.45	1.17	1.59	12.70	121.93
122	8.01	73.58	1.16	1.59	13.08	121.83
123	8.09	71.70	1.14	1.59	13.39	121.64
124	8.15	70.57	1.11	1.59	13.50	121.43
125	8.21	69.54	1.09	1.59	13.58	121.22
126	8.27	68.13	1.08	1.59	13.87	121.10
127	8.34	66.26	1.07	1.59	14.35	121.02
128	8.40	63.91	1.07	1.82	14.94	120.90
129	8.48	60.72	1.07	1.82	15.90	120.81
130	8.55	59.12	1.08	1.70	16.44	120.76
131	8.61	59.12	1.10	1.59	16.66	120.91
132	8.68	59.12	1.12	1.59	16.84	121.02
133	8.74	57.72	1.11	1.59	17.30	120.95
134	8.80	59.31	1.11	1.59	16.85	121.01
135	8.87	56.96	1.12	0.80	17.66	120.93
136	8.93	59.50	1.12	1.02	16.96	121.08
137	9.00	62.69	1.13	0.91	16.12	121.24
138	9.06	65.60	1.14	1.02	15.44	121.41
139	9.13	69.16	1.14	0.91	14.60	121.54
140	9.19	71.60	1.14	1.02	14.07	121.64
141	9.26	73.67	1.15	1.14	13.76	121.80
142	9.34	74.04	1.17	1.25	13.85	121.94
143	9.39	73.11	1.18	1.25	14.14	121.96
144	9.45	71.89	1.18	1.14	14.44	121.90

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.53	70.48	1.16	1.14	14.72	121.77
146	9.59	68.88	1.15	1.02	15.05	121.63
147	9.66	67.19	1.09	1.02	15.03	121.14
148	9.71	65.04	1.02	1.02	15.07	120.58
149	9.79	63.25	0.96	1.02	15.13	120.09
150	9.86	61.75	0.92	1.02	15.27	119.75
151	9.92	60.25	0.90	0.91	15.55	119.53
152	9.98	56.50	0.89	0.91	16.57	119.24
153	10.04	56.35	0.88	0.23	16.55	119.13
154	10.11	56.21	0.87	0.23	16.62	119.11
155	10.18	55.56	0.88	0.23	16.94	119.14
156	10.24	54.52	0.90	-0.45	17.52	119.26
157	10.31	53.40	0.95	-0.45	18.43	119.59
158	10.37	52.37	0.96	-0.45	18.95	119.63
159	10.44	50.68	0.97	-0.45	19.77	119.64
160	10.51	48.33	0.98	-0.45	20.91	119.61
161	10.57	45.42	1.00	-0.49	22.40	119.55
162	10.64	42.23	1.01	-0.53	24.21	119.46
163	10.71	39.79	1.03	-0.53	25.84	119.44
164	10.77	36.79	1.02	-0.49	27.74	119.21
165	10.84	34.07	1.01	-0.45	29.68	118.98
166	10.90	31.53	1.05	-0.57	32.18	119.01
167	10.97	30.03	1.11	-0.28	34.40	119.32
168	11.03	28.53	1.20	-0.28	37.13	119.79
169	11.10	28.15	1.30	0.02	38.78	120.33
170	11.16	28.06	1.39	0.02	40.02	120.83
171	11.23	27.78	1.48	0.02	41.41	121.25
172	11.30	28.34	1.57	0.34	41.79	121.73
173	11.37	29.56	1.63	0.91	41.16	122.12
174	11.42	30.78	1.66	0.80	40.22	122.35
175	11.49	32.19	1.68	0.68	39.06	122.54
176	11.55	33.60	1.69	0.68	37.90	122.68
177	11.62	34.91	1.72	0.68	37.07	122.90
178	11.68	36.04	1.76	0.68	36.52	123.14
179	11.75	37.35	1.79	0.68	35.80	123.35
180	11.82	37.91	1.82	0.57	35.67	123.50
181	11.88	38.10	1.84	0.57	35.81	123.62
182	11.95	37.82	1.86	0.80	36.28	123.69
183	12.02	37.35	1.88	0.80	36.88	123.73
184	12.09	36.60	1.89	0.91	37.65	123.72
185	12.15	36.04	1.90	0.91	38.23	123.69
186	12.22	35.19	1.90	0.91	39.06	123.64
187	12.29	34.54	1.89	0.91	39.71	123.59
188	12.36	34.82	1.92	0.91	39.70	123.69
189	12.42	34.72	1.96	0.91	40.23	123.84
190	12.49	34.63	1.99	0.91	40.62	123.94
191	12.56	35.57	1.98	1.14	39.82	123.99
192	12.62	37.82	1.94	1.14	37.62	123.98

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.69	42.04	1.83	1.36	33.68	123.81
194	12.76	47.39	1.70	1.36	29.42	123.55
195	12.83	52.08	1.60	1.36	26.35	123.36
196	12.89	58.28	1.53	1.36	23.17	123.28
197	12.93	61.19	1.49	1.25	21.85	123.22
198	12.99	67.48	1.42	1.25	19.32	123.10
199	13.06	71.89	1.34	0.91	17.54	122.82
200	13.13	75.64	1.25	0.68	15.99	122.43
201	13.20	78.74	1.21	0.80	15.05	122.31
202	13.26	81.65	1.20	0.80	14.38	122.35
203	13.33	84.46	1.20	0.80	13.84	122.43
204	13.39	86.24	1.21	1.02	13.55	122.51
205	13.47	89.53	1.24	1.02	13.22	122.84
206	13.53	91.69	1.24	1.14	12.83	122.88
207	13.59	93.56	1.20	1.14	12.27	122.67
208	13.67	96.00	1.19	1.14	11.82	122.66
209	13.72	97.88	1.20	1.14	11.65	122.81
210	13.80	99.38	1.22	1.25	11.56	122.97
211	13.85	100.04	1.25	1.25	11.62	123.13
212	13.93	99.76	1.27	0.11	11.84	123.27
213	13.99	101.17	1.29	-0.11	11.72	123.37
214	14.04	101.73	1.28	-0.34	11.65	123.38
215	14.12	103.42	1.31	-0.57	11.57	123.56
216	14.18	103.89	1.33	-0.57	11.61	123.67
217	14.27	104.83	1.33	-0.68	11.52	123.70
218	14.34	104.54	1.35	-0.68	11.68	123.79
219	14.37	104.45	1.35	-0.68	11.75	123.83
220	14.44	103.98	1.36	-0.68	11.90	123.87
221	14.51	103.42	1.37	-0.68	12.02	123.86
222	14.57	103.04	1.37	-0.68	12.12	123.87
223	14.64	102.39	1.37	-0.68	12.27	123.88
224	14.70	101.35	1.38	-0.68	12.47	123.87
225	14.77	99.85	1.38	-0.68	12.73	123.83
226	14.84	98.54	1.37	-0.80	12.96	123.78
227	14.90	97.79	1.37	-0.68	13.08	123.73
228	14.97	97.74	1.35	-0.80	13.04	123.67
229	15.03	97.41	1.35	-0.68	13.11	123.65
230	15.10	97.69	1.35	-0.68	13.06	123.63
231	15.16	97.69	1.35	-0.68	13.10	123.64
232	15.26	98.35	1.38	-0.68	13.19	123.81
233	15.32	98.35	1.37	-0.57	13.14	123.75
234	15.39	98.07	1.36	-0.57	13.20	123.73
235	15.45	98.07	1.36	-0.57	13.23	123.73
236	15.52	97.69	1.36	-0.57	13.28	123.69
237	15.55	97.22	1.36	-0.34	13.36	123.66
238	15.62	96.10	1.35	-0.23	13.55	123.60
239	15.69	95.35	1.34	-0.34	13.67	123.55
240	15.75	94.50	1.28	-0.34	13.48	123.20

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.82	93.00	1.08	-0.34	12.45	121.90
242	15.89	90.75	1.05	-0.34	12.67	121.64
243	15.96	87.37	1.01	-0.34	13.05	121.28
244	16.02	82.68	0.97	-0.34	13.70	120.85
245	16.09	76.86	0.95	-0.34	14.78	120.46
246	16.15	65.32	0.94	-0.80	17.84	120.03
247	16.22	62.60	0.95	-0.80	18.81	120.00
248	16.28	55.84	0.95	-1.14	21.24	119.68
249	16.35	48.33	0.97	-1.14	24.94	119.53
250	16.42	41.48	1.03	-1.14	29.61	119.59
251	16.48	35.00	1.06	-1.14	34.94	119.39
252	16.55	29.94	1.09	-1.14	40.32	119.18
253	16.61	26.46	1.07	-1.14	44.48	118.78
254	16.68	25.24	1.06	-0.91	45.99	118.55
255	16.75	23.56	1.05	-0.34	48.55	118.35
256	16.82	22.43	1.05	-0.23	50.43	118.18
257	16.88	22.34	1.07	0.11	51.07	118.34
258	16.95	23.93	1.15	0.45	49.66	119.01
259	17.02	27.87	1.24	0.68	45.34	119.95
260	17.09	33.97	1.34	1.02	39.86	121.03
261	17.15	40.45	1.41	1.82	35.04	121.80
262	17.22	47.96	1.48	2.50	30.81	122.59
263	17.29	54.90	1.52	2.27	27.56	123.13
264	17.36	61.84	1.56	1.82	24.87	123.58
265	17.39	64.66	1.57	1.59	23.92	123.76
266	17.46	71.04	1.59	1.48	21.85	124.05
267	17.53	76.77	1.58	0.91	20.14	124.22
268	17.59	81.27	1.60	1.14	19.06	124.43
269	17.66	84.46	1.63	1.14	18.50	124.67
270	17.73	87.28	1.66	1.02	18.02	124.87
271	17.79	89.62	1.68	0.91	17.66	125.05
272	17.86	91.12	1.72	0.68	17.55	125.23
273	17.93	91.03	1.73	0.68	17.69	125.29
274	17.99	90.00	1.78	1.14	18.24	125.48
275	18.06	88.59	1.81	1.25	18.75	125.56
276	18.13	87.28	1.80	0.91	19.04	125.49
277	18.20	85.87	1.82	1.02	19.52	125.52
278	18.26	83.80	1.82	0.91	20.08	125.46
279	18.33	81.18	1.82	1.02	20.81	125.38
280	18.40	77.80	1.79	1.02	21.62	125.16
281	18.45	62.41	1.76	0.23	26.78	124.49
282	18.51	67.29	1.70	0.23	24.52	124.43
283	18.57	62.13	1.62	0.23	25.99	123.89
284	18.64	54.52	1.56	0.34	28.96	123.27
285	18.72	46.64	1.50	0.23	32.91	122.60
286	18.77	40.26	1.45	0.11	37.00	121.99
287	18.86	32.19	1.32	0.11	43.20	120.78
288	18.91	27.87	1.23	0.00	47.38	119.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.98	24.87	1.15	-0.23	50.68	119.12
290	19.04	22.80	1.08	-0.23	53.08	118.43
291	19.11	19.99	1.01	-0.23	57.55	117.66
292	19.18	18.11	0.98	-0.11	61.38	117.18
293	19.24	17.08	0.97	-0.11	63.95	116.95
294	19.31	16.05	0.95	0.11	66.60	116.66
295	19.37	15.01	0.91	0.23	69.10	116.19
296	19.44	14.55	0.89	0.34	70.28	115.95
297	19.51	14.45	0.88	0.34	70.47	115.84
298	19.58	14.83	0.88	0.34	69.21	115.89
299	19.64	14.45	0.79	0.23	68.40	115.05
300	19.71	14.45	0.72	0.45	66.53	114.35
301	19.78	14.45	0.78	0.57	68.45	115.01
302	19.84	14.73	0.83	0.57	68.70	115.45
303	19.91	15.20	0.85	0.68	67.67	115.68
304	19.98	15.39	0.87	0.91	67.68	115.90
305	20.02	15.30	0.87	0.80	68.20	115.94
306	20.10	15.20	0.87	1.14	68.60	115.93
307	20.15	15.48	0.87	1.48	67.66	115.94
308	20.22	15.67	0.86	1.48	66.89	115.88
309	20.28	15.67	0.85	1.25	66.67	115.76
310	20.34	15.86	0.84	1.14	66.11	115.77
311	20.41	16.05	0.85	1.14	65.67	115.81
312	20.48	15.95	0.84	1.36	65.93	115.75
313	20.55	16.33	0.82	1.59	64.41	115.64
314	20.61	16.61	0.78	1.59	62.60	115.27
315	20.68	17.08	0.72	1.70	59.89	114.75
316	20.74	17.64	0.75	1.70	59.49	115.21
317	20.81	18.11	0.79	1.93	59.31	115.64
318	20.88	18.58	0.84	1.93	59.39	116.15
319	20.95	18.68	0.87	1.93	59.73	116.36
320	21.00	17.27	0.88	2.04	63.82	116.33
321	21.08	19.33	0.92	5.11	59.42	116.89
322	21.13	19.33	0.94	4.54	59.88	117.04
323	21.22	19.80	0.95	5.79	59.07	117.17
324	21.29	19.99	0.96	5.79	58.97	117.29
325	21.36	19.99	0.98	5.79	59.42	117.43
326	21.42	19.90	1.01	4.77	60.23	117.61
327	21.49	19.90	1.05	5.11	61.14	117.93
328	21.55	19.90	1.08	4.66	61.84	118.16
329	21.62	19.90	1.11	4.88	62.37	118.33
330	21.65	20.08	1.12	4.88	62.19	118.42
331	21.72	20.27	1.14	4.88	62.17	118.57
332	21.79	20.46	1.15	5.00	62.03	118.67
333	21.85	20.36	1.15	5.22	62.38	118.68
334	21.92	20.36	1.15	5.68	62.47	118.68
335	21.99	20.93	1.17	5.56	61.54	118.84
336	22.06	21.58	1.18	6.02	60.46	119.00

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.12	22.24	1.19	6.13	59.33	119.13
338	22.19	22.43	1.19	6.24	59.04	119.15
339	22.26	22.43	1.19	6.13	59.00	119.11
340	22.32	22.43	1.17	6.02	58.84	119.02
341	22.39	24.49	1.15	6.13	54.74	119.07
342	22.45	29.37	1.13	7.49	47.31	119.43
343	22.52	38.76	1.13	9.31	37.35	120.08
344	22.59	51.33	1.12	8.63	28.78	120.71
345	22.66	63.72	1.10	7.72	23.02	121.13
346	22.73	73.20	1.13	6.93	20.10	121.65
347	22.79	80.14	1.21	6.47	18.78	122.35
348	22.86	85.02	1.25	6.70	17.85	122.71
349	22.93	88.78	1.26	7.04	17.08	122.90
350	22.99	91.31	1.27	7.27	16.63	123.04
351	23.05	86.24	1.29	7.61	17.94	123.00
352	23.10	92.44	1.32	3.86	16.75	123.33
353	23.19	98.91	1.37	3.52	15.80	123.78
354	23.26	102.67	1.46	3.29	15.66	124.34
355	23.32	106.05	1.59	3.06	15.80	125.02
356	23.39	109.24	1.68	2.61	15.77	125.51
357	23.45	112.52	1.76	2.38	15.65	125.93
358	23.52	115.43	1.83	1.59	15.52	126.26
359	23.59	118.72	1.86	1.48	15.19	126.48
360	23.65	120.59	1.87	1.48	14.95	126.55
361	23.72	120.87	1.86	1.36	14.88	126.51
362	23.78	118.34	1.83	1.14	15.13	126.32
363	23.82	115.62	1.79	1.02	15.40	126.11
364	23.89	107.74	1.70	0.80	16.31	125.55
365	23.96	96.57	1.64	0.80	18.24	125.02
366	24.02	83.71	1.60	0.80	21.21	124.51
367	24.09	69.73	1.57	0.80	25.51	123.92
368	24.16	55.65	1.55	0.80	31.72	123.29
369	24.22	43.45	1.54	0.57	39.66	122.64
370	24.29	35.00	1.47	0.68	46.90	121.77
371	24.36	29.37	1.36	0.45	52.49	120.78
372	24.43	25.71	1.24	0.68	56.42	119.78
373	24.49	24.02	1.12	0.45	57.44	118.84
374	24.56	24.02	1.06	0.68	56.61	118.48
375	24.63	26.84	1.11	0.91	52.84	119.09
376	24.69	33.13	1.05	1.02	43.72	119.19
377	24.76	44.11	1.20	1.14	35.80	120.86
378	24.83	57.62	1.37	0.91	29.44	122.47
379	24.89	66.63	1.53	0.91	26.86	123.65
380	24.96	73.11	1.71	1.48	25.73	124.66
381	25.03	79.39	1.87	2.16	24.75	125.54
382	25.09	86.24	2.01	2.95	23.51	126.24
383	25.16	91.88	2.09	2.95	22.44	126.68
384	25.23	97.41	2.10	2.73	21.17	126.88

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.29	103.14	2.12	2.73	19.97	127.07
386	25.36	108.20	2.10	2.73	18.84	127.13
387	25.43	107.55	2.06	2.73	18.78	126.96
388	25.49	103.23	2.03	2.50	19.55	126.75
389	25.53	99.10	2.01	2.61	20.42	126.60
390	25.60	89.81	2.00	2.38	22.68	126.30
391	25.66	79.96	1.97	2.27	25.49	125.93
392	25.73	66.26	1.91	2.04	30.34	125.25
393	25.80	56.31	1.82	2.16	34.66	124.49
394	25.85	48.71	1.75	2.04	38.90	123.84
395	25.93	42.89	1.68	2.04	42.82	123.23
396	25.99	37.73	1.63	2.04	47.29	122.72
397	26.07	29.84	1.52	1.82	55.47	121.64
398	26.13	27.78	1.43	1.82	57.42	121.02
399	26.18	26.56	1.34	1.82	58.11	120.40
400	26.26	25.15	1.22	1.82	58.80	119.59
401	26.32	24.59	1.16	1.93	58.94	119.18
402	26.39	24.59	1.15	2.16	58.76	119.09
403	26.46	24.59	1.12	2.27	58.44	118.93
404	26.51	24.21	1.12	2.27	59.11	118.87
405	26.58	24.21	1.11	2.27	59.04	118.82
406	26.66	26.37	1.14	2.50	55.93	119.24
407	26.72	29.94	1.21	2.95	51.67	119.94
408	26.80	39.23	1.27	2.95	42.23	120.99
409	26.85	45.05	1.29	2.50	37.61	121.44
410	26.91	49.64	1.33	2.73	34.85	121.89
411	26.98	52.08	1.43	3.06	34.37	122.53
412	27.04	51.99	1.49	3.75	35.05	122.83
413	27.11	48.99	1.56	3.41	37.73	123.00
414	27.19	43.73	1.59	2.84	42.15	122.88
415	27.24	40.64	1.56	2.84	44.63	122.57
416	27.30	38.57	1.53	2.84	46.41	122.32
417	27.37	35.29	1.52	3.06	49.70	122.03
418	27.43	35.00	1.51	2.84	49.98	121.97
419	27.52	37.82	1.51	3.52	47.00	122.13
420	27.58	41.01	1.49	3.75	43.76	122.25
421	27.63	44.67	1.48	3.97	40.48	122.39
422	27.72	54.90	1.46	3.97	33.46	122.83
423	27.79	62.97	1.44	3.63	29.10	123.02
424	27.85	69.73	1.41	3.63	26.03	123.12
425	27.89	72.17	1.34	3.63	24.59	122.86
426	27.95	78.08	1.16	3.75	21.12	122.02
427	28.02	83.34	1.13	3.29	19.38	121.98
428	28.09	88.12	1.12	3.29	18.08	122.04
429	28.16	92.25	1.12	3.29	17.12	122.15
430	28.23	95.72	1.12	3.41	16.38	122.23
431	28.28	96.76	1.12	1.93	16.19	122.27
432	28.36	97.79	1.14	1.70	16.16	122.43

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.42	101.82	1.19	1.36	15.69	122.80
434	28.48	104.36	1.24	1.14	15.60	123.18
435	28.57	107.92	1.37	0.91	15.81	123.98
436	28.63	110.36	1.43	0.80	15.80	124.38
437	28.69	112.33	1.49	0.80	15.84	124.72
438	28.76	113.93	1.55	0.80	15.91	125.03
439	28.82	114.40	1.59	0.68	16.10	125.23
440	28.89	114.21	1.63	0.57	16.35	125.39
441	28.96	113.27	1.67	0.57	16.77	125.54
442	29.02	111.40	1.68	0.45	17.24	125.58
443	29.09	109.05	1.70	0.45	17.78	125.58
444	29.16	105.86	1.69	0.45	18.39	125.46
445	29.23	101.73	1.68	0.45	19.28	125.35
446	29.29	96.29	1.67	0.45	20.46	125.14
447	29.36	89.44	1.72	0.34	22.62	125.20
448	29.43	81.27	1.70	0.34	24.97	124.88
449	29.49	71.14	1.73	0.34	28.91	124.69
450	29.56	59.12	1.75	0.34	34.81	124.32
451	29.59	52.93	1.74	0.45	38.52	124.02
452	29.66	41.57	1.62	0.23	46.27	122.88
453	29.73	32.66	1.33	0.23	52.34	120.84
454	29.79	30.12	1.29	0.23	55.29	120.45
455	29.88	25.06	1.21	0.23	62.30	119.53
456	29.94	22.34	1.14	0.00	66.53	118.78
457	30.01	21.21	1.06	0.38	67.65	118.11
458	30.06	21.30	0.99	0.68	66.16	117.64
459	30.12	19.61	0.91	0.68	68.78	116.87
460	30.19	18.39	0.89	0.68	71.52	116.49
461	30.26	18.02	0.87	0.68	72.25	116.30
462	30.32	17.83	0.81	0.68	71.41	115.75
463	30.39	17.46	0.76	0.57	71.25	115.21
464	30.45	17.17	0.74	0.57	71.83	115.04
465	30.52	17.17	0.74	0.57	71.73	114.98
466	30.59	17.17	0.69	0.57	70.44	114.48
467	30.66	17.17	0.67	0.68	70.09	114.32
468	30.72	17.36	0.77	0.68	72.09	115.28
469	30.79	17.55	0.77	0.57	71.67	115.33
470	30.85	17.83	0.77	0.57	70.91	115.37
471	30.92	19.24	0.77	0.57	67.11	115.56
472	30.97	19.71	0.77	0.45	65.98	115.62
473	31.07	20.46	0.76	0.57	64.13	115.66
474	31.10	20.18	0.76	0.45	64.62	115.55
475	31.19	18.77	0.79	0.57	69.14	115.70
476	31.24	18.21	0.81	0.68	71.22	115.80
477	31.30	17.27	0.79	0.68	73.71	115.54
478	31.38	17.83	0.77	0.68	71.34	115.34
479	31.43	17.36	0.75	0.68	72.32	115.10
480	31.50	17.78	0.73	0.68	70.75	115.02

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.57	17.64	0.72	0.80	70.86	114.87
482	31.63	17.74	0.71	0.91	70.25	114.74
483	31.70	17.46	0.69	0.91	70.66	114.52
484	31.77	17.08	0.73	1.02	72.91	114.85
485	31.84	16.52	0.76	1.02	75.60	115.06
486	31.90	16.89	0.80	1.14	75.53	115.50
487	31.97	18.21	0.80	1.36	71.71	115.73
488	32.03	20.55	0.85	1.59	66.75	116.45
489	32.10	23.27	0.91	3.06	62.17	117.28
490	32.17	23.84	0.96	3.06	62.08	117.72
491	32.23	22.24	0.99	3.06	65.99	117.77
492	32.29	20.08	1.00	3.18	71.33	117.58
493	32.35	18.77	0.99	3.18	74.79	117.36
494	32.42	17.83	0.96	3.41	77.07	117.04
495	32.49	17.83	0.92	3.41	76.16	116.70
496	32.56	18.39	0.90	3.63	73.99	116.59
497	32.62	19.90	0.90	3.63	69.96	116.79
498	32.68	21.40	0.91	3.86	66.66	117.08
499	32.75	22.34	0.94	4.09	65.10	117.36
500	32.82	22.52	0.98	4.20	65.61	117.70
501	32.88	22.90	1.07	4.43	66.54	118.38
502	32.95	24.87	1.18	4.66	64.60	119.32
503	33.01	28.25	1.27	4.88	60.20	120.19
504	33.08	33.97	1.33	5.00	53.08	120.94
505	33.15	41.67	1.40	5.22	46.06	121.84
506	33.21	48.61	1.56	5.34	42.10	123.01
507	33.28	50.58	1.69	5.34	41.96	123.69
508	33.35	49.18	1.73	5.11	43.50	123.81
509	33.41	44.67	1.74	5.39	47.18	123.61
510	33.48	39.70	1.71	4.43	51.52	123.20
511	33.55	33.60	1.65	5.45	57.85	122.52
512	33.62	30.12	1.59	5.68	62.02	121.97
513	33.68	28.81	1.53	7.04	63.40	121.60
514	33.75	26.18	1.43	6.47	66.63	120.86
515	33.82	22.90	1.27	6.47	70.83	119.64
516	33.88	19.99	0.89	5.68	70.67	116.74
517	33.95	17.83	0.73	6.13	72.85	115.05
518	34.02	16.24	0.69	6.24	76.80	114.39
519	34.09	15.11	0.69	6.24	80.82	114.17
520	34.15	14.64	0.69	6.24	82.88	114.13
521	34.19	15.11	0.69	6.70	81.03	114.21
522	34.25	13.89	0.69	7.72	86.09	114.01
523	34.33	15.11	0.69	8.06	81.16	114.23
524	34.40	15.20	0.70	8.52	80.92	114.26
525	34.46	15.20	0.69	8.17	80.84	114.21
526	34.52	15.20	0.68	8.17	80.47	114.06
527	34.59	15.20	0.66	8.40	79.99	113.87
528	34.66	15.39	0.65	9.42	78.95	113.78

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.73	15.77	0.65	8.52	77.68	113.84
530	34.79	16.33	0.67	8.74	76.53	114.19
531	34.86	16.80	0.69	8.74	75.71	114.51
532	34.93	17.55	0.72	9.08	74.08	114.86
533	34.99	18.02	0.74	9.31	73.21	115.11
534	35.06	17.64	0.74	9.31	74.39	115.05
535	35.13	16.99	0.76	9.31	77.15	115.18
536	35.20	16.70	0.77	9.42	78.53	115.27
537	35.26	16.89	0.78	9.99	78.25	115.41
538	35.33	17.46	0.82	10.33	77.46	115.84
539	35.40	18.58	0.84	10.67	74.43	116.10
540	35.47	19.90	0.87	10.79	71.55	116.52
541	35.53	20.65	0.89	10.90	70.36	116.86
542	35.60	21.12	0.92	11.01	69.72	117.08
543	35.66	22.15	0.98	11.58	68.64	117.67
544	35.70	23.37	1.01	11.58	66.60	118.02
545	35.77	24.40	1.06	11.58	65.52	118.49
546	35.83	24.31	1.11	11.69	66.77	118.86
547	35.90	26.56	1.19	13.28	63.83	119.56
548	35.97	30.78	1.25	13.17	58.03	120.25
549	36.03	32.56	1.24	12.38	55.55	120.34
550	36.10	30.22	1.18	11.47	58.02	119.82
551	36.17	25.71	1.16	11.47	65.05	119.27
552	36.23	22.15	1.15	11.47	72.36	118.84
553	36.30	26.04	1.13	11.47	64.08	119.12
554	36.37	19.90	1.10	12.26	77.30	118.27
555	36.43	26.37	1.09	13.17	62.90	118.90
556	36.50	39.79	1.15	13.85	46.63	120.28
557	36.57	50.96	1.27	14.87	39.07	121.62
558	36.64	60.06	1.44	12.83	35.17	122.92
559	36.70	64.66	1.63	11.47	34.52	124.00
560	36.77	66.63	1.73	10.67	34.47	124.53
561	36.84	60.91	1.76	8.86	37.83	124.41
562	36.91	49.74	1.75	8.06	45.24	123.89
563	36.97	39.23	1.68	7.83	53.82	123.02
564	37.04	32.00	1.54	7.49	61.15	121.91
565	37.11	27.78	1.38	6.81	65.70	120.76
566	37.14	26.65	1.31	7.38	66.56	120.24
567	37.21	24.49	1.14	6.58	68.12	119.04
568	37.27	22.99	0.99	8.06	68.48	117.85
569	37.34	23.37	0.94	8.40	66.63	117.48
570	37.41	25.06	0.98	8.40	64.22	118.01
571	37.48	27.40	0.93	8.40	59.13	117.81
572	37.54	29.47	1.06	8.06	58.30	118.97
573	37.61	31.34	1.20	7.49	57.87	120.03
574	37.68	32.75	1.32	7.72	57.64	120.81
575	37.74	34.54	1.38	7.72	56.20	121.28
576	37.81	37.07	1.43	7.72	53.91	121.72

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.88	36.79	1.48	8.29	54.90	121.96
578	37.94	36.88	1.56	9.20	55.74	122.35
579	38.01	36.88	1.67	9.31	56.95	122.82
580	38.08	36.98	1.76	9.99	57.88	123.22
581	38.15	39.32	1.81	10.33	55.77	123.56
582	38.21	43.54	1.81	11.01	51.61	123.82
583	38.28	49.64	1.81	11.47	46.62	124.15
584	38.34	57.72	1.86	11.81	41.60	124.70
585	38.41	68.79	1.90	11.81	35.67	125.31
586	38.48	81.46	1.90	10.45	30.17	125.71
587	38.55	91.97	1.88	9.54	26.48	125.94
588	38.61	96.66	1.89	8.17	25.18	126.10
589	38.68	95.16	1.93	8.06	25.89	126.20
590	38.75	87.65	1.91	7.83	28.19	125.94
591	38.78	82.58	1.91	7.61	29.97	125.78
592	38.85	71.14	1.93	7.04	35.01	125.50
593	38.92	60.06	2.03	6.70	41.93	125.43
594	38.98	49.83	2.12	6.98	49.52	125.30
595	39.05	42.89	2.08	6.36	55.31	124.80
596	39.11	37.07	1.89	6.93	59.88	123.75
597	39.19	37.44	1.51	7.83	55.32	122.13
598	39.24	35.10	1.37	7.27	56.39	121.26
599	39.32	29.47	1.37	8.06	64.27	120.82
600	39.38	29.47	1.39	7.95	64.71	120.97
601	39.45	29.47	1.45	9.42	65.48	121.24
602	39.51	29.47	1.49	11.01	66.03	121.45
603	39.58	36.22	1.51	12.03	56.97	122.07
604	39.64	40.92	1.51	12.26	51.85	122.34
605	39.72	47.02	1.54	11.81	46.87	122.84
606	39.77	49.55	1.59	11.81	45.44	123.19
607	39.84	52.37	1.66	11.24	44.13	123.63
608	39.90	53.02	1.74	10.45	44.46	124.01
609	39.96	49.18	1.82	9.88	48.05	124.18
610	40.03	55.84	1.81	8.17	43.33	124.44
611	40.09	57.06	1.77	7.15	42.27	124.32
612	40.17	51.05	1.77	7.15	46.31	124.05
613	40.25	44.76	1.82	7.27	51.88	123.93
614	40.31	40.17	1.87	7.72	56.91	123.87
615	40.37	38.66	1.91	8.74	58.99	123.93
616	40.42	41.95	1.91	10.10	55.47	124.12
617	40.51	47.20	1.91	9.20	50.70	124.40
618	40.56	47.11	1.89	9.54	50.67	124.34
619	40.62	46.08	1.93	9.31	51.95	124.44
620	40.71	44.20	2.00	9.31	54.30	124.58
621	40.78	44.58	2.03	9.99	54.29	124.73
622	40.85	48.24	2.08	10.10	51.50	125.08
623	40.91	52.93	2.10	9.76	48.10	125.38
624	40.95	55.46	2.11	9.88	46.41	125.52

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.02	60.06	2.09	9.42	43.46	125.67
626	41.08	65.60	2.04	9.42	39.99	125.70
627	41.15	77.42	2.03	10.22	34.03	126.07
628	41.22	98.07	2.05	10.45	26.79	126.71
629	41.28	119.00	2.09	9.99	21.80	127.33
630	41.34	128.76	2.14	8.86	20.12	127.69
631	41.44	139.36	2.18	8.29	18.46	128.00
632	41.50	140.30	2.18	7.83	18.32	128.02
633	41.57	139.17	2.18	7.27	18.54	128.01
634	41.60	138.24	2.17	7.27	18.68	127.97
635	41.67	137.20	2.15	7.27	18.76	127.87
636	41.74	136.92	2.16	7.04	18.86	127.89
637	41.81	136.73	2.23	6.36	19.29	128.15
638	41.87	136.55	2.28	6.58	19.57	128.30
639	41.94	135.23	2.33	6.24	20.05	128.42
640	42.00	121.81	2.39	6.47	22.99	128.35
641	42.07	129.41	2.54	7.15	22.17	128.95
642	42.14	126.97	2.66	7.27	23.28	129.26
643	42.20	127.07	2.79	7.49	23.85	129.59
644	42.28	123.50	2.86	7.55	25.00	129.72
645	42.35	120.59	2.87	7.55	25.74	129.69
646	42.42	118.15	2.83	7.61	26.13	129.52
647	42.48	117.12	2.78	7.27	26.16	129.36
648	42.55	117.21	2.70	7.49	25.81	129.17
649	42.62	116.46	2.61	6.81	25.54	128.89
650	42.68	113.93	2.51	6.36	25.70	128.56
651	42.72	111.77	2.46	6.93	25.99	128.36
652	42.78	106.89	2.36	6.58	26.76	127.95
653	42.85	101.26	2.28	6.36	27.92	127.56
654	42.92	93.10	2.22	6.53	30.15	127.15
655	42.99	83.99	2.23	5.90	33.61	126.94
656	43.05	76.86	2.27	6.47	37.01	126.86
657	43.12	73.48	2.24	6.47	38.48	126.66
658	43.18	71.98	2.11	6.13	38.30	126.18
659	43.25	70.29	1.93	6.36	37.79	125.47
660	43.32	66.26	1.88	6.13	39.56	125.11
661	43.38	58.37	1.86	6.13	43.85	124.72
662	43.45	51.15	1.77	6.13	48.04	124.07
663	43.52	46.17	1.63	6.93	50.66	123.20
664	43.59	43.45	1.45	7.27	51.17	122.19
665	43.65	41.57	1.39	6.47	52.28	121.76
666	43.72	40.17	1.50	7.38	55.00	122.23
667	43.79	39.13	1.64	6.81	57.76	122.82
668	43.86	37.82	1.72	7.27	60.27	123.12
669	43.92	36.13	1.76	6.81	62.86	123.18
670	43.98	42.70	1.83	8.86	56.10	123.85
671	44.04	52.84	1.86	9.65	47.82	124.48
672	44.12	68.13	1.87	9.42	38.89	125.16

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.19	80.14	1.94	8.74	33.69	125.82
674	44.25	89.62	2.01	7.27	30.57	126.35
675	44.31	96.85	2.02	6.58	28.27	126.58
676	44.38	101.82	2.01	6.13	26.72	126.66
677	44.45	105.30	2.04	5.11	25.94	126.84
678	44.52	107.74	2.07	5.11	25.54	127.03
679	44.58	109.14	2.13	5.45	25.50	127.24
680	44.65	110.46	2.20	5.11	25.63	127.53
681	44.72	112.24	2.27	5.45	25.56	127.77
682	44.78	113.84	2.30	5.90	25.35	127.91
683	44.85	115.34	2.32	5.45	25.14	128.01
684	44.88	116.28	2.33	6.02	24.95	128.05
685	44.95	117.50	2.32	5.45	24.66	128.06
686	45.02	118.25	2.31	5.68	24.46	128.05
687	45.09	118.72	2.30	5.45	24.33	128.03
688	45.16	119.28	2.30	5.45	24.21	128.03
689	45.22	119.28	2.29	5.45	24.20	128.01
690	45.29	119.28	2.28	5.90	24.17	127.98
691	45.35	119.28	2.28	5.79	24.16	127.96
692	45.42	119.75	2.28	5.79	24.08	127.97
693	45.49	120.69	2.27	5.68	23.84	127.96
694	45.56	121.06	2.26	5.56	23.72	127.93
695	45.62	121.16	2.26	5.45	23.70	127.93
696	45.69	120.78	2.25	5.11	23.77	127.89
697	45.76	119.94	2.23	5.34	23.91	127.83
698	45.82	118.53	2.21	5.11	24.15	127.74
699	45.89	116.93	2.20	5.11	24.46	127.65
700	45.96	114.87	2.18	4.88	24.89	127.55
701	46.02	111.96	2.16	4.77	25.54	127.43
702	46.09	109.71	2.15	4.66	26.05	127.32
703	46.16	106.89	2.13	4.66	26.72	127.20
704	46.22	104.17	2.00	4.31	26.73	126.69
705	46.29	101.35	1.95	4.20	27.25	126.44
706	46.36	99.01	2.00	4.20	28.29	126.55
707	46.42	97.04	2.04	4.20	29.23	126.66
708	46.46	96.29	2.05	4.20	29.55	126.67
709	46.52	94.32	2.05	4.20	30.23	126.62
710	46.61	92.63	2.03	4.43	30.70	126.50
711	46.66	90.84	2.00	4.31	31.14	126.34
712	46.74	84.46	1.92	4.20	33.02	125.88
713	46.79	81.46	1.86	4.20	33.79	125.54
714	46.86	76.11	1.80	4.09	35.76	125.16
715	46.94	69.82	1.80	4.09	38.92	124.95
716	46.99	64.66	1.80	4.09	41.49	124.75
717	47.06	56.40	1.75	4.09	45.94	124.19
718	47.14	47.20	1.69	4.20	52.39	123.52
719	47.19	41.76	1.69	4.20	57.53	123.21
720	47.25	37.16	1.68	4.54	62.73	122.89

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.34	36.98	1.63	5.22	62.41	122.65
722	47.39	36.98	1.59	5.90	61.96	122.47
723	47.45	36.79	1.52	6.58	61.43	122.15
724	47.51	48.52	1.42	8.63	48.53	122.29
725	47.58	65.13	1.34	8.97	37.35	122.63
726	47.65	75.08	1.36	7.27	32.57	123.08
727	47.72	77.24	1.46	6.47	32.58	123.65
728	47.78	73.76	1.62	6.02	35.74	124.31
729	47.85	66.44	1.83	6.02	41.11	124.91
730	47.91	59.03	1.94	6.02	46.30	125.08
731	47.98	51.15	1.90	5.45	51.52	124.58
732	48.05	45.70	1.74	6.13	54.68	123.67
733	48.11	41.10	1.62	6.24	58.01	122.89
734	48.18	37.16	1.54	6.24	61.60	122.25
735	48.24	34.82	1.54	7.49	64.65	122.09
736	48.31	33.78	1.56	8.52	66.37	122.10
737	48.38	33.50	1.53	8.17	66.48	121.95
738	48.45	35.19	1.64	8.63	65.46	122.57
739	48.52	42.04	1.78	9.42	58.81	123.60
740	48.58	62.03	1.86	10.90	44.07	124.89
741	48.65	89.44	2.01	10.90	32.58	126.35
742	48.72	110.74	2.22	9.08	27.17	127.60
743	48.78	125.19	2.38	8.86	24.50	128.38
744	48.85	138.70	2.46	8.17	22.14	128.88
745	48.92	150.62	2.48	7.27	20.16	129.15
746	48.95	155.32	2.47	7.27	19.36	129.19
747	49.02	160.57	2.21	7.04	17.44	128.47
748	49.09	164.61	2.00	7.61	15.90	127.79
749	49.16	169.39	2.38	6.98	17.01	129.14
750	49.23	175.68	2.34	6.81	16.03	129.10
751	49.29	182.06	2.48	6.93	15.87	129.63
752	49.35	178.96	2.60	6.36	16.71	129.92
753	49.42	188.72	2.76	5.68	16.16	130.48
754	49.49	197.64	2.84	5.22	15.46	130.80
755	49.56	202.43	2.90	5.56	15.19	131.02
756	49.62	206.84	2.82	6.02	14.47	130.86
757	49.69	211.53	2.69	6.02	13.59	130.57
758	49.76	216.88	2.69	6.02	13.12	130.63
759	49.82	221.38	2.69	5.56	12.75	130.70
760	49.89	224.29	2.71	5.22	12.57	130.78
761	49.95	229.17	2.73	5.22	12.22	130.86
762	50.00	220.26	2.72	4.77	12.97	130.76
763	50.07	227.77	2.72	3.29	12.33	130.82
764	50.14	231.80	2.69	3.29	11.92	130.78
765	50.20	232.74	2.66	3.29	11.79	130.73
766	50.28	232.36	2.64	2.95	11.77	130.68
767	50.35	228.70	2.60	2.95	11.95	130.53
768	50.41	224.10	2.59	2.95	12.31	130.45

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.48	218.29	2.61	2.95	12.88	130.43
770	50.55	213.78	2.60	2.61	13.27	130.36
771	50.61	211.72	2.62	2.50	13.54	130.38
772	50.68	212.75	2.59	2.27	13.36	130.32
773	50.74	213.03	2.49	2.04	12.99	130.03
774	50.81	209.56	2.39	1.93	12.96	129.68
775	50.88	202.33	2.33	1.70	13.45	129.42
776	50.94	191.63	2.29	1.59	14.41	129.16
777	51.01	178.96	2.23	1.36	15.62	128.79
778	51.08	167.42	2.17	1.14	16.84	128.43
779	51.15	158.32	2.13	1.02	17.94	128.14
780	51.21	151.75	2.08	1.02	18.76	127.89
781	51.28	145.46	2.11	1.02	19.94	127.87
782	51.34	140.02	2.09	0.91	20.85	127.73
783	51.38	137.30	2.09	0.91	21.37	127.68
784	51.45	132.60	2.12	0.80	22.44	127.68
785	51.51	129.60	2.11	0.57	23.07	127.61
786	51.58	127.26	2.00	0.57	22.92	127.15
787	51.65	125.47	1.64	0.57	21.11	125.68
788	51.71	123.69	1.74	0.57	22.17	126.09
789	51.78	123.60	1.82	0.57	22.69	126.39
790	51.85	122.84	1.90	0.57	23.39	126.70
791	51.92	123.50	1.95	0.57	23.55	126.89
792	51.99	124.06	1.94	0.80	23.43	126.89
793	52.05	124.63	1.92	0.68	23.17	126.80
794	52.11	125.10	1.90	0.68	22.97	126.74
795	52.18	122.94	1.88	0.68	23.36	126.63
796	52.24	120.69	1.87	0.68	23.81	126.53
797	52.31	118.34	1.86	0.68	24.32	126.44
798	52.38	115.52	1.85	0.68	25.00	126.36
799	52.44	110.64	1.87	0.68	26.45	126.35
800	52.51	105.11	1.93	0.68	28.46	126.44
801	52.58	104.92	1.97	0.68	28.80	126.58
802	52.64	104.92	1.99	0.68	28.97	126.66
803	52.71	104.73	1.99	0.80	29.05	126.65
804	52.78	107.74	1.99	0.80	28.17	126.71
805	52.84	108.77	1.98	0.80	27.82	126.69
806	52.91	107.74	1.94	0.80	27.90	126.53
807	52.98	106.61	1.90	0.80	27.99	126.37
808	53.04	107.74	1.88	0.80	27.51	126.30
809	53.11	110.64	1.86	0.80	26.57	126.29
810	53.17	115.43	1.84	0.80	25.22	126.33
811	53.24	123.78	1.83	1.02	23.15	126.44
812	53.31	134.29	1.80	1.14	20.79	126.51
813	53.38	145.18	1.76	1.36	18.64	126.56
814	53.42	151.84	1.78	1.36	17.66	126.73
815	53.49	161.23	1.84	1.36	16.63	127.13
816	53.56	171.36	1.91	1.36	15.62	127.54

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.63	183.28	1.94	1.36	14.33	127.82
818	53.68	191.73	1.96	1.36	13.52	128.01
819	53.75	201.68	2.03	1.36	12.83	128.40
820	53.82	207.21	2.14	1.48	12.74	128.83
821	53.89	211.44	2.27	1.70	12.88	129.34
822	53.94	214.53	2.12	1.70	12.01	128.86
823	54.00	201.58	1.74	1.59	11.59	127.25
824	54.07	215.85	1.76	1.70	10.49	127.54
825	54.15	224.29	1.93	1.48	10.48	128.27
826	54.21	230.39	2.03	1.70	10.42	128.74
827	54.27	234.71	2.15	1.70	10.54	129.19
828	54.34	232.32	2.27	1.70	11.12	129.54
829	54.40	229.92	2.34	1.70	11.59	129.76
830	54.47	240.06	2.41	1.70	11.06	130.09
831	54.53	244.84	2.48	1.70	10.93	130.34
832	54.60	249.44	2.60	1.59	10.98	130.73
833	54.67	253.48	2.70	1.36	11.00	131.03
834	54.73	257.61	2.77	1.36	10.93	131.26
835	54.80	261.64	2.83	1.36	10.83	131.45
836	54.87	265.12	2.87	1.48	10.71	131.59
837	54.93	268.02	2.91	1.48	10.66	131.73
838	54.99	270.65	2.97	1.48	10.64	131.89
839	55.05	273.56	3.03	1.36	10.63	132.07
840	55.12	276.57	3.06	1.02	10.54	132.18
841	55.19	279.10	3.10	1.14	10.48	132.29
842	55.26	281.35	3.13	1.14	10.41	132.37
843	55.33	282.85	3.15	1.14	10.39	132.44
844	55.39	283.13	3.17	1.14	10.43	132.48
845	55.45	282.57	3.18	1.14	10.50	132.51
846	55.52	282.57	3.20	1.36	10.54	132.54
847	55.59	282.57	3.12	1.36	10.34	132.35
848	55.64	280.60	2.96	1.36	10.04	131.95
849	55.72	277.88	2.96	1.36	10.24	131.94
850	55.79	274.31	2.96	1.25	10.46	131.90
851	55.86	269.81	2.95	1.25	10.72	131.84
852	55.92	263.90	2.92	1.14	11.04	131.71
853	55.98	219.32	2.88	1.59	14.53	131.16
854	56.05	247.85	2.83	1.70	11.96	131.34
855	56.11	246.25	2.79	1.70	11.95	131.21
856	56.18	244.38	2.75	1.70	11.97	131.08
857	56.24	243.16	2.74	1.48	12.04	131.03
858	56.31	244.47	2.69	1.48	11.80	130.93
859	56.37	244.84	2.66	1.48	11.69	130.85
860	56.45	244.56	2.63	1.48	11.63	130.77
861	56.51	246.63	2.61	1.59	11.40	130.72
862	56.58	246.82	2.58	1.59	11.31	130.65
863	56.64	247.19	2.57	1.25	11.25	130.62
864	56.71	247.94	2.59	1.25	11.25	130.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.78	249.54	2.61	1.25	11.22	130.76
866	56.84	251.13	2.63	1.25	11.16	130.81
867	56.91	251.41	2.64	1.25	11.17	130.84
868	56.98	251.13	2.66	1.25	11.28	130.91
869	57.05	251.13	2.69	1.25	11.37	130.99
870	57.11	252.45	2.71	1.02	11.34	131.05
871	57.18	252.73	2.06	1.02	9.22	129.06
872	57.24	253.01	1.70	1.02	7.93	127.67
873	57.31	251.60	1.82	0.91	8.43	128.12
874	57.38	250.29	1.93	0.80	8.93	128.54
875	57.45	249.82	2.02	0.91	9.29	128.88
876	57.48	249.26	2.06	0.68	9.46	129.01
877	57.56	248.65	2.11	0.91	9.71	129.20
878	57.62	248.65	2.14	1.14	9.81	129.30
879	57.71	248.04	2.21	1.36	10.10	129.52
880	57.77	247.75	2.30	1.14	10.44	129.82
881	57.84	245.78	2.33	1.02	10.68	129.88
882	57.91	243.06	2.33	1.02	10.87	129.85
883	57.97	238.56	2.34	0.91	11.25	129.83
884	58.01	235.65	2.34	0.91	11.50	129.82
885	58.08	229.36	2.34	0.91	12.02	129.76
886	58.14	225.79	2.34	0.91	12.32	129.71
887	58.21	223.35	2.33	0.80	12.48	129.64
888	58.28	221.48	2.30	0.80	12.56	129.55
889	58.34	221.85	2.27	0.80	12.41	129.44
890	58.41	227.20	2.23	0.80	11.81	129.36
891	58.48	236.12	2.18	0.57	10.92	129.29
892	58.54	242.12	2.14	0.80	10.35	129.22
893	58.61	247.00	2.14	0.91	10.01	129.27
894	58.67	250.57	1.90	0.91	8.92	128.44
895	58.74	252.35	1.44	0.91	7.07	126.45
896	58.80	255.45	1.50	0.91	7.13	126.78
897	58.87	256.95	1.67	1.14	7.68	127.54
898	58.94	259.11	1.81	1.25	8.07	128.16
899	59.01	262.96	1.97	1.25	8.42	128.83
900	59.07	262.68	2.10	0.91	8.90	129.30
901	59.13	262.39	2.21	1.36	9.27	129.66
902	59.22	273.94	2.32	1.82	8.91	130.12
903	59.28	279.10	2.46	1.93	9.05	130.61
904	59.32	281.35	2.53	1.82	9.13	130.83
905	59.38	285.11	2.65	1.93	9.24	131.18
906	59.45	288.39	2.73	1.70	9.28	131.42
907	59.52	292.89	2.78	1.93	9.18	131.61
908	59.59	297.96	2.82	2.04	9.01	131.75
909	59.65	302.09	2.62	2.04	8.25	131.24
910	59.72	303.87	2.20	2.04	7.01	129.99
911	59.79	302.09	2.17	2.04	7.01	129.87
912	59.85	302.09	2.22	1.82	7.15	130.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.92	301.06	2.28	1.93	7.39	130.23
914	59.98	299.56	2.32	1.93	7.59	130.35
915	60.04	251.32	2.33	1.23	10.49	129.94
916	60.11	288.76	2.29	0.34	8.05	130.14
917	60.19	286.89	2.29	0.45	8.17	130.14
918	60.25	283.32	2.29	0.57	8.38	130.12
919	60.32	277.13	2.31	0.57	8.78	130.11
920	60.38	269.90	2.33	0.45	9.28	130.10
921	60.46	264.18	2.31	0.45	9.60	130.00
922	60.51	262.21	2.27	0.45	9.61	129.86
923	60.57	259.77	2.22	0.45	9.60	129.67
924	60.65	255.17	2.18	0.45	9.76	129.48
925	60.70	251.60	2.16	0.57	9.95	129.39
926	60.77	247.66	2.12	0.57	10.11	129.23
927	60.83	245.78	2.08	0.57	10.10	129.06
928	60.92	243.72	2.03	0.57	10.06	128.86
929	60.99	245.55	2.03	0.57	9.92	128.86
930	61.05	243.53	2.03	0.57	10.07	128.84
931	61.12	245.31	2.03	0.57	9.95	128.86
932	61.19	247.19	2.03	0.57	9.82	128.87
933	61.22	248.13	2.03	0.57	9.76	128.88
934	61.29	248.04	2.03	0.80	9.77	128.88
935	61.35	247.75	2.03	0.80	9.80	128.88
936	61.42	247.85	2.03	0.80	9.80	128.88
937	61.50	247.85	2.03	0.80	9.81	128.89
938	61.55	247.85	2.04	0.80	9.88	128.95
939	61.62	250.38	2.10	0.80	9.92	129.19
940	61.69	251.88	2.17	0.68	10.07	129.44
941	61.75	251.32	2.23	0.91	10.32	129.63
942	61.81	247.75	2.30	0.91	10.81	129.82
943	61.89	250.76	2.38	1.14	10.86	130.08
944	61.94	253.95	2.46	1.25	10.91	130.36
945	62.03	258.83	2.60	1.59	11.02	130.82
946	62.09	262.86	2.69	1.70	11.02	131.11
947	62.15	266.80	2.81	1.59	11.11	131.45
948	62.21	269.90	2.93	1.82	11.26	131.80
949	62.27	273.75	2.99	1.82	11.18	131.98
950	62.34	270.93	3.03	1.82	11.49	132.06
951	62.42	278.44	3.04	1.70	11.02	132.15
952	62.49	284.92	3.18	1.70	10.96	132.51
953	62.54	281.63	3.17	1.70	11.17	132.47
954	62.60	282.29	3.02	1.93	10.73	132.12
955	62.67	282.10	2.92	1.82	10.48	131.88
956	62.74	279.38	2.75	1.70	10.15	131.40
957	62.80	265.30	2.57	1.70	10.54	130.78
958	62.87	239.68	2.48	1.59	12.13	130.27
959	62.95	210.68	2.11	1.36	13.32	128.79
960	63.01	189.19	1.76	1.14	13.97	127.20

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	63.08	167.98	2.00	1.14	17.86	127.86
962	63.14	150.25	2.24	1.14	21.89	128.38
963	63.21	137.67	2.50	1.14	25.77	128.98
964	63.28	129.51	2.81	1.59	29.26	129.69
965	63.33	130.35	3.10	2.95	30.50	130.43
966	63.39	131.20	3.43	3.41	31.80	131.19
967	63.46	136.73	3.66	3.75	31.39	131.75
968	63.53	131.95	3.79	3.52	33.21	131.93
969	63.59	126.79	3.99	3.29	35.25	132.21
970	63.66	124.35	4.20	3.63	36.58	132.53
971	63.72	128.94	4.29	3.97	35.77	132.78
972	63.79	139.55	4.22	3.86	33.03	132.85
973	63.85	152.88	4.06	3.29	29.39	132.79
974	63.92	172.40	3.78	2.84	24.71	132.56
975	63.99	188.35	3.41	3.06	20.98	132.03
976	64.05	204.02	3.08	3.06	17.83	131.48
977	64.11	218.19	2.84	2.84	15.46	131.05
978	64.19	241.28	2.47	2.38	12.13	130.28
979	64.26	253.95	2.22	2.61	10.32	129.61
980	64.33	265.02	1.67	2.61	7.64	127.62
981	64.39	276.57	1.31	2.38	5.00	125.96
982	64.46	287.83	1.35	2.50	5.00	126.28
983	64.53	298.06	1.40	2.50	5.00	126.65
984	64.60	303.87	1.47	2.50	5.03	127.01
985	64.66	298.43	1.52	2.16	5.46	127.25
986	64.70	299.65	1.56	1.25	5.55	127.45
987	64.78	296.08	1.67	1.59	6.08	127.91
988	64.85	300.87	1.82	1.59	6.34	128.56
989	64.91	309.51	1.49	1.59	4.88	127.15
990	64.97	326.77	1.23	1.70	3.39	125.93
991	65.04	349.01	1.37	2.16	3.12	126.87
992	65.11	371.26	1.47	2.38	2.77	127.54
993	65.16	381.67	1.50	2.27	2.55	127.72
994	65.22	392.09	1.50	2.04	2.30	127.82
995	65.29	390.96	1.46	0.68	2.21	127.58
996	65.36	398.66	1.45	0.91	2.03	127.62
997	65.42	396.78	1.32	1.14	1.72	126.89
998	65.49	392.37	0.88	0.80	0.62	123.87
999	65.57	388.34	0.93	0.45	0.86	124.30
1000	65.63	382.99	0.98	0.45	1.10	124.61
1001	65.71	375.67	1.05	0.11	1.48	125.09
1002	65.76	366.66	1.11	0.00	1.87	125.43
1003	65.82	285.86	1.25	-0.06	5.00	125.69
1004	65.89	332.97	1.30	0.00	3.45	126.36
1005	65.95	322.55	1.28	-0.11	3.75	126.15
1006	66.02	314.76	1.37	0.00	4.34	126.58
1007	66.09	311.19	1.40	0.00	4.60	126.75
1008	66.14	307.25	1.38	0.23	4.70	126.62

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	66.21	298.53	1.36	0.91	4.99	126.44
1010	66.28	298.53	1.42	0.80	5.00	126.73
1011	66.35	300.87	1.55	0.57	5.56	127.41
1012	66.41	302.84	1.57	0.57	5.53	127.49
1013	66.48	305.66	1.35	0.57	4.67	126.42
1014	66.55	306.60	1.06	0.57	3.55	124.63
1015	66.61	307.16	0.74	0.57	2.33	122.09
1016	66.68	304.72	0.77	0.91	2.50	122.28
1017	66.75	300.68	0.78	1.70	2.67	122.33
1018	66.81	297.59	0.83	1.70	2.99	122.78
1019	66.87	282.29	0.88	1.48	3.80	123.12
1020	66.93	268.59	0.92	1.48	4.54	123.28
1021	67.00	268.96	0.92	1.48	4.55	123.33
1022	67.06	263.90	0.93	1.25	4.82	123.31
1023	67.14	256.39	0.91	1.25	5.00	123.14
1024	67.21	246.91	0.88	1.14	5.00	122.75
1025	67.27	234.24	0.87	1.02	5.00	122.53
1026	67.34	218.47	0.93	1.02	5.00	122.88
1027	67.41	202.05	0.97	0.91	5.00	123.02
1028	67.47	186.28	1.03	0.91	10.71	123.25
1029	67.54	172.96	1.19	0.91	13.16	124.12
1030	67.61	163.67	1.36	0.91	15.41	124.94
1031	67.67	163.76	1.52	0.80	16.43	125.79
1032	67.74	163.76	1.37	1.25	15.50	125.01
1033	67.81	163.86	0.97	1.36	12.76	122.48
1034	67.87	160.48	0.91	1.36	12.71	121.95
1035	67.94	150.90	0.94	0.91	14.25	122.06
1036	68.01	138.80	1.10	-0.11	17.42	122.99
1037	68.07	121.06	1.34	-0.30	22.91	124.09
1038	68.12	109.24	1.56	-0.30	27.87	124.99
1039	68.20	95.82	1.86	-0.30	34.49	125.94
1040	68.25	84.27	2.04	-1.48	39.81	126.29
1041	68.31	70.57	2.23	-1.36	47.54	126.52
1042	68.38	59.87	2.29	-1.14	54.58	126.31
1043	68.44	69.35	2.22	-0.80	48.18	126.46
1044	68.51	59.40	2.13	-0.34	53.70	125.76
1045	68.58	68.13	2.09	0.11	47.89	125.96
1046	68.64	83.62	2.17	0.45	40.99	126.72
1047	68.71	103.42	2.14	0.68	33.98	127.15
1048	68.78	125.85	2.18	0.45	27.80	127.78
1049	68.83	138.70	2.16	0.23	24.71	127.95
1050	68.91	153.72	2.03	0.11	21.06	127.72
1051	68.99	163.39	1.93	0.00	18.94	127.49
1052	69.05	164.89	1.53	0.00	16.51	125.85
1053	69.11	165.64	1.05	-0.11	13.27	123.09
1054	69.17	165.73	1.16	-0.11	14.03	123.82
1055	69.24	164.51	1.19	-0.11	14.38	123.97
1056	69.31	161.70	1.18	-0.11	14.74	123.92

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	69.37	158.51	1.32	-0.23	16.11	124.66
1058	69.44	155.88	1.51	-0.53	17.71	125.58
1059	69.51	153.06	1.70	-0.53	19.40	126.43
1060	69.56	153.25	1.84	-0.80	20.20	127.01
1061	69.64	160.38	2.13	-0.91	20.59	128.18
1062	69.69	167.70	2.02	-0.91	18.86	127.89
1063	69.78	187.41	1.89	-0.91	15.59	127.68
1064	69.82	206.37	1.93	-1.14	13.69	128.07
1065	69.89	242.69	1.88	-0.80	10.39	128.30
1066	69.95	272.81	1.85	-0.47	8.28	128.45
1067	70.02	279.94	2.08	-0.53	8.66	129.37
1068	70.08	285.01	2.43	2.04	9.47	130.55
1069	70.15	282.85	2.44	0.68	9.64	130.56
1070	70.21	289.05	2.07	-0.11	8.12	129.41
1071	70.30	298.53	1.91	-0.11	7.11	128.89
1072	70.37	288.11	1.90	-0.11	7.62	128.77
1073	70.41	300.12	1.96	-0.11	7.21	129.11
1074	70.49	286.70	2.03	0.34	8.15	129.26
1075	70.55	301.72	2.07	1.02	7.48	129.51
1076	70.61	312.88	2.17	1.59	7.25	129.97
1077	70.67	318.42	2.01	1.02	6.51	129.44
1078	70.74	321.71	1.78	0.23	5.66	128.56
1079	70.81	312.79	1.58	-0.34	5.41	127.63
1080	70.88	307.72	1.01	-0.57	3.55	124.28
1081	70.95	296.55	1.07	-0.34	4.25	124.68
1082	71.01	291.67	1.07	-0.68	4.43	124.60
1083	71.08	292.24	1.07	-0.34	4.41	124.61
1084	71.15	291.77	1.11	0.00	4.59	124.86
1085	71.20	289.19	1.19	-0.28	5.00	125.37
1086	71.27	292.24	1.33	0.00	5.00	126.20
1087	71.33	286.61	1.39	-0.23	5.00	126.50
1088	71.41	292.71	1.51	0.00	6.13	127.16
1089	71.47	294.21	1.58	0.00	6.30	127.49
1090	71.55	293.65	1.68	0.23	6.68	127.94
1091	71.60	289.23	1.77	0.57	7.23	128.29
1092	71.66	290.92	1.89	0.68	7.53	128.76
1093	71.72	290.45	2.00	1.14	7.94	129.18
1094	71.81	292.43	2.31	1.25	8.81	130.24
1095	71.87	291.02	2.50	1.36	9.49	130.82
1096	71.94	288.48	2.61	1.70	9.96	131.10
1097	72.00	284.82	2.68	1.70	10.40	131.27
1098	72.07	273.00	2.81	1.70	11.57	131.50
1099	72.14	256.01	2.94	1.70	13.24	131.68
1100	72.20	239.03	3.43	1.70	16.23	132.64
1101	72.27	226.54	3.12	1.70	16.50	131.83
1102	72.34	223.92	2.93	1.70	16.12	131.33
1103	72.41	217.82	2.98	2.27	16.96	131.40
1104	72.47	217.49	3.10	2.16	17.40	131.67

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	72.51	217.49	3.16	2.38	17.63	131.82
1106	72.58	217.16	3.17	4.20	17.68	131.83
1107	72.64	109.05	2.98	5.11	37.33	129.71
1108	72.72	241.94	2.69	4.77	13.66	130.89
1109	72.80	252.63	2.13	3.18	10.85	129.29
1110	72.86	251.79	1.85	2.61	9.85	128.24
1111	72.92	248.88	1.81	1.48	9.93	128.08
1112	72.97	245.60	1.74	1.25	9.89	127.76
1113	73.06	238.28	1.85	1.25	10.89	128.13
1114	73.12	233.68	1.93	1.14	11.59	128.39
1115	73.19	230.67	2.03	1.36	12.25	128.73
1116	73.25	227.11	2.12	1.48	12.92	129.00
1117	73.32	225.98	2.16	1.70	13.21	129.14
1118	73.38	222.70	2.18	1.48	13.59	129.16
1119	73.45	218.94	2.17	1.14	13.89	129.07
1120	73.52	215.94	2.13	0.80	14.04	128.91
1121	73.58	213.97	2.10	0.57	14.12	128.79
1122	73.65	216.03	2.07	0.57	13.81	128.72
1123	73.72	214.63	2.06	0.45	13.89	128.65
1124	73.78	216.13	2.07	0.45	13.80	128.71
1125	73.85	219.51	1.93	0.23	12.89	128.24
1126	73.92	225.61	2.01	0.23	12.68	128.59
1127	73.95	229.36	2.07	0.23	12.60	128.85
1128	74.02	235.55	2.03	0.00	11.91	128.77
1129	74.09	240.06	2.09	0.00	11.79	129.03
1130	74.16	242.50	2.17	0.00	11.90	129.32
1131	74.22	242.12	2.22	0.00	12.13	129.49
1132	74.30	241.75	2.23	0.00	12.23	129.54
1133	74.36	241.75	2.23	0.00	12.21	129.52
1134	74.43	240.72	2.23	0.00	12.31	129.51
1135	74.49	235.84	2.21	0.00	12.66	129.41
1136	74.55	230.96	2.19	0.00	13.00	129.28
1137	74.61	223.92	2.18	-0.11	13.60	129.17
1138	74.68	215.75	2.16	-0.23	14.31	129.01
1139	74.75	206.74	2.11	-0.23	15.02	128.73
1140	74.81	198.77	2.06	-0.23	15.72	128.48
1141	74.88	193.42	2.05	-0.23	16.31	128.38
1142	74.95	189.57	2.05	-0.23	16.76	128.31
1143	75.01	187.69	2.01	-0.23	16.85	128.16
1144	75.08	187.69	1.98	-0.23	16.68	128.04
1145	75.15	187.97	0.00	-0.23	100.00	87.36
1146	75.21	188.82	0.00	-0.23	100.00	87.36
1147	75.28	190.98	0.00	-0.45	100.00	87.36
1148	75.35	193.79	0.00	-0.80	100.00	87.36
1149	75.41	196.70	0.00	-0.80	100.00	87.36
1150	75.46	193.60	0.00	-0.80	100.00	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.07	0.00	0.00	0.00	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
2	0.14	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
3	0.21	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
4	0.28	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
5	0.33	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
6	0.41	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
7	0.46	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
8	0.54	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
9	0.60	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
10	0.66	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
11	0.72	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
12	0.80	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
13	0.86	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
14	0.92	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
15	0.99	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
16	1.06	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
17	1.11	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
18	1.18	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
19	1.26	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
20	1.33	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
21	1.39	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
22	1.46	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
23	1.51	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
24	1.59	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
25	1.65	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
26	1.71	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
27	1.79	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
28	1.84	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
29	1.92	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
30	1.97	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
31	2.05	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
32	2.11	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
33	2.18	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
34	2.24	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
35	2.31	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
36	2.37	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
37	2.44	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
38	2.50	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
39	2.58	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
40	2.64	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
41	2.71	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
42	2.76	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
43	2.82	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
44	2.90	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
45	2.97	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
46	3.03	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
47	3.09	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
48	3.15	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	3.22	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
50	3.30	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
51	3.36	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
52	3.42	0.21	0.00	0.21	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
53	3.48	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
54	3.55	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
55	3.61	0.22	0.00	0.22	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
56	3.70	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
57	3.76	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
58	3.82	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
59	3.88	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
60	3.95	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
61	4.01	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
62	4.07	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
63	4.14	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
64	4.20	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
65	4.28	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
66	4.33	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
67	4.42	0.27	0.00	0.27	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
68	4.48	0.27	0.00	0.27	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
69	4.54	0.27	0.00	0.27	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
70	4.60	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
71	4.66	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
72	4.74	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
73	4.80	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
74	4.86	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
75	4.93	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
76	5.00	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
77	5.07	0.31	0.00	0.31	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
78	5.13	0.31	0.00	0.31	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
79	5.18	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
80	5.26	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
81	5.33	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
82	5.38	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
83	5.46	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
84	5.52	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
85	5.59	0.34	0.00	0.34	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
86	5.66	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
87	5.72	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
88	5.79	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
89	5.85	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
90	5.91	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
91	5.98	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
92	6.04	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
93	6.10	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
94	6.19	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
95	6.25	0.38	0.00	0.38	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
96	6.31	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
97	6.37	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
98	6.44	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
99	6.51	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
100	6.57	0.40	0.00	0.40	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
101	6.63	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
102	6.70	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
103	6.76	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
104	6.83	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
105	6.89	0.42	0.00	0.42	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
106	6.96	0.42	0.00	0.42	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
107	7.03	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
108	7.09	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
109	7.16	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
110	7.22	0.44	0.00	0.44	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
111	7.29	0.44	0.00	0.44	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
112	7.35	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
113	7.42	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
114	7.50	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
115	7.56	0.46	0.00	0.46	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
116	7.63	0.46	0.00	0.46	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
117	7.69	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
118	7.76	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
119	7.82	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
120	7.88	0.48	0.00	0.48	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
121	7.94	0.48	0.00	0.48	0.98	0.493	1.05	0.468	1.10	1.30	2.000	No
122	8.01	0.49	0.00	0.49	0.98	0.493	1.05	0.468	1.10	1.30	0.561	No
123	8.09	0.49	0.00	0.49	0.98	0.496	1.05	0.470	1.10	1.30	0.565	No
124	8.15	0.49	0.00	0.49	0.98	0.497	1.05	0.472	1.10	1.30	0.567	No
125	8.21	0.50	0.01	0.49	0.98	0.499	1.05	0.473	1.10	1.30	0.570	No
126	8.27	0.50	0.01	0.49	0.98	0.501	1.05	0.475	1.10	1.30	0.572	No
127	8.34	0.51	0.01	0.50	0.98	0.503	1.05	0.477	1.10	1.30	0.574	No
128	8.40	0.51	0.01	0.50	0.98	0.505	1.05	0.479	1.10	1.30	0.577	No
129	8.48	0.51	0.02	0.50	0.98	0.507	1.05	0.481	1.10	1.30	0.580	No
130	8.55	0.52	0.02	0.50	0.98	0.509	1.05	0.483	1.10	1.30	0.583	No
131	8.61	0.52	0.02	0.50	0.98	0.511	1.05	0.484	1.10	1.30	0.585	No
132	8.68	0.53	0.02	0.51	0.98	0.512	1.05	0.486	1.10	1.30	0.587	No
133	8.74	0.53	0.02	0.51	0.98	0.514	1.05	0.488	1.10	1.30	0.590	No
134	8.80	0.53	0.03	0.51	0.98	0.516	1.05	0.489	1.10	1.30	0.591	No
135	8.87	0.54	0.03	0.51	0.98	0.518	1.05	0.491	1.10	1.30	0.595	No
136	8.93	0.54	0.03	0.51	0.98	0.519	1.05	0.492	1.10	1.30	0.596	No
137	9.00	0.55	0.03	0.51	0.98	0.521	1.05	0.494	1.10	1.30	0.596	No
138	9.06	0.55	0.03	0.52	0.98	0.523	1.05	0.496	1.10	1.30	0.597	No
139	9.13	0.55	0.04	0.52	0.98	0.525	1.05	0.498	1.10	1.30	0.599	No
140	9.19	0.56	0.04	0.52	0.98	0.526	1.05	0.499	1.10	1.30	0.600	No
141	9.26	0.56	0.04	0.52	0.98	0.528	1.05	0.501	1.10	1.30	0.602	No
142	9.34	0.57	0.04	0.52	0.98	0.530	1.05	0.502	1.10	1.30	0.604	No
143	9.39	0.57	0.04	0.53	0.98	0.531	1.05	0.504	1.10	1.30	0.606	No
144	9.45	0.57	0.05	0.53	0.98	0.533	1.05	0.505	1.10	1.30	0.607	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	9.53	0.58	0.05	0.53	0.98	0.535	1.05	0.507	1.10	1.30	0.611	No
146	9.59	0.58	0.05	0.53	0.98	0.536	1.05	0.508	1.10	1.30	0.614	No
147	9.66	0.59	0.05	0.53	0.98	0.538	1.05	0.510	1.09	1.30	0.618	No
148	9.71	0.59	0.05	0.54	0.98	0.539	1.05	0.511	1.09	1.30	0.622	No
149	9.79	0.59	0.06	0.54	0.98	0.541	1.05	0.513	1.09	1.30	0.627	No
150	9.86	0.60	0.06	0.54	0.98	0.543	1.05	0.515	1.09	1.30	0.630	No
151	9.92	0.60	0.06	0.54	0.98	0.544	1.05	0.516	1.09	1.30	0.633	No
152	9.98	0.61	0.06	0.54	0.98	0.545	1.05	0.517	1.08	1.30	0.637	No
153	10.04	0.61	0.06	0.55	0.98	0.547	1.05	0.519	1.08	1.30	0.639	No
154	10.11	0.61	0.07	0.55	0.98	0.548	1.05	0.520	1.08	1.30	0.641	No
155	10.18	0.62	0.07	0.55	0.98	0.550	1.05	0.522	1.08	1.30	0.644	No
156	10.24	0.62	0.07	0.55	0.98	0.551	1.05	0.523	1.08	1.30	0.646	No
157	10.31	0.62	0.07	0.55	0.98	0.553	1.05	0.524	1.08	1.30	0.648	No
158	10.37	0.63	0.07	0.55	0.98	0.554	1.05	0.526	1.08	1.30	0.650	No
159	10.44	0.63	0.08	0.56	0.98	0.556	1.05	0.527	1.08	1.30	0.653	No
160	10.51	0.64	0.08	0.56	0.98	0.557	1.05	0.529	1.08	1.30	0.657	No
161	10.57	0.64	0.08	0.56	0.98	0.559	1.05	0.530	1.08	1.30	0.660	No
162	10.64	0.64	0.08	0.56	0.98	0.560	1.05	0.531	1.07	1.30	0.664	No
163	10.71	0.65	0.08	0.56	0.98	0.562	1.05	0.533	1.07	1.30	0.668	No
164	10.77	0.65	0.09	0.57	0.98	0.563	1.05	0.534	1.07	1.30	0.672	No
165	10.84	0.66	0.09	0.57	0.98	0.564	1.05	0.535	1.07	1.30	0.675	No
166	10.90	0.66	0.09	0.57	0.98	0.566	1.05	0.537	1.07	1.30	0.679	No
167	10.97	0.66	0.09	0.57	0.98	0.567	1.05	0.538	1.06	1.30	0.681	No
168	11.03	0.67	0.09	0.57	0.97	0.568	1.05	0.539	1.06	1.30	0.684	No
169	11.10	0.67	0.10	0.58	0.97	0.570	1.05	0.540	1.06	1.30	0.686	No
170	11.16	0.68	0.10	0.58	0.97	0.571	1.05	0.542	1.06	1.30	0.688	No
171	11.23	0.68	0.10	0.58	0.97	0.572	1.05	0.543	1.06	1.30	0.690	No
172	11.30	0.68	0.10	0.58	0.97	0.574	1.05	0.544	1.06	1.30	0.691	No
173	11.37	0.69	0.11	0.58	0.97	0.575	1.05	0.545	1.06	1.30	0.692	No
174	11.42	0.69	0.11	0.58	0.97	0.576	1.05	0.546	1.06	1.30	0.693	No
175	11.49	0.70	0.11	0.59	0.97	0.577	1.05	0.548	1.06	1.30	0.694	No
176	11.55	0.70	0.11	0.59	0.97	0.579	1.05	0.549	1.06	1.30	0.695	No
177	11.62	0.70	0.11	0.59	0.97	0.580	1.05	0.550	1.06	1.30	0.696	No
178	11.68	0.71	0.11	0.59	0.97	0.581	1.05	0.551	1.06	1.30	0.697	No
179	11.75	0.71	0.12	0.59	0.97	0.582	1.05	0.552	1.06	1.30	0.697	No
180	11.82	0.72	0.12	0.60	0.97	0.584	1.05	0.554	1.06	1.30	0.699	No
181	11.88	0.72	0.12	0.60	0.97	0.585	1.05	0.555	1.06	1.30	0.700	No
182	11.95	0.72	0.12	0.60	0.97	0.586	1.05	0.556	1.06	1.30	0.702	No
183	12.02	0.73	0.13	0.60	0.97	0.587	1.05	0.557	1.06	1.30	0.704	No
184	12.09	0.73	0.13	0.61	0.97	0.589	1.05	0.558	1.06	1.30	0.707	No
185	12.15	0.74	0.13	0.61	0.97	0.590	1.05	0.559	1.06	1.30	0.709	No
186	12.22	0.74	0.13	0.61	0.97	0.591	1.05	0.560	1.06	1.30	0.711	No
187	12.29	0.75	0.13	0.61	0.97	0.592	1.05	0.561	1.06	1.30	0.713	No
188	12.36	0.75	0.14	0.61	0.97	0.593	1.05	0.563	1.06	1.30	0.715	No
189	12.42	0.75	0.14	0.62	0.97	0.594	1.05	0.564	1.06	1.30	0.717	No
190	12.49	0.76	0.14	0.62	0.97	0.595	1.05	0.565	1.06	1.30	0.718	No
191	12.56	0.76	0.14	0.62	0.97	0.597	1.05	0.566	1.06	1.30	0.719	No
192	12.62	0.77	0.14	0.62	0.97	0.598	1.05	0.567	1.06	1.30	0.719	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	12.69	0.77	0.15	0.62	0.97	0.599	1.05	0.568	1.06	1.30	0.718	No
194	12.76	0.77	0.15	0.63	0.97	0.600	1.05	0.569	1.06	1.30	0.716	No
195	12.83	0.78	0.15	0.63	0.97	0.601	1.05	0.570	1.06	1.30	0.715	No
196	12.89	0.78	0.15	0.63	0.97	0.602	1.05	0.571	1.07	1.30	0.713	No
197	12.93	0.78	0.15	0.63	0.97	0.603	1.05	0.572	1.07	1.30	0.712	No
198	12.99	0.79	0.16	0.63	0.97	0.604	1.05	0.573	1.07	1.30	0.710	No
199	13.06	0.79	0.16	0.63	0.97	0.605	1.05	0.574	1.07	1.30	0.710	No
200	13.13	0.80	0.16	0.64	0.97	0.606	1.05	0.575	1.07	1.30	0.711	No
201	13.20	0.80	0.16	0.64	0.97	0.607	1.05	0.576	1.07	1.30	0.712	No
202	13.26	0.81	0.16	0.64	0.97	0.608	1.05	0.577	1.07	1.30	0.713	No
203	13.33	0.81	0.17	0.64	0.97	0.609	1.05	0.577	1.07	1.30	0.714	No
204	13.39	0.81	0.17	0.64	0.97	0.610	1.05	0.578	1.07	1.30	0.715	No
205	13.47	0.82	0.17	0.65	0.97	0.611	1.05	0.580	1.07	1.30	0.715	No
206	13.53	0.82	0.17	0.65	0.97	0.612	1.05	0.580	1.07	1.30	0.716	No
207	13.59	0.83	0.17	0.65	0.97	0.613	1.05	0.581	1.07	1.30	0.719	No
208	13.67	0.83	0.18	0.65	0.97	0.614	1.05	0.582	1.07	1.30	0.721	No
209	13.72	0.83	0.18	0.65	0.97	0.615	1.05	0.583	1.07	1.30	0.722	No
210	13.80	0.84	0.18	0.66	0.96	0.616	1.05	0.584	1.07	1.30	0.723	No
211	13.85	0.84	0.18	0.66	0.96	0.617	1.05	0.585	1.07	1.30	0.723	No
212	13.93	0.85	0.18	0.66	0.96	0.618	1.05	0.586	1.07	1.30	0.723	No
213	13.99	0.85	0.19	0.66	0.96	0.619	1.05	0.587	1.07	1.30	0.725	No
214	14.04	0.85	0.19	0.66	0.96	0.619	1.05	0.587	1.07	1.30	0.726	No
215	14.12	0.86	0.19	0.67	0.96	0.621	1.05	0.588	1.07	1.30	0.727	No
216	14.18	0.86	0.19	0.67	0.96	0.621	1.05	0.589	1.07	1.30	0.727	No
217	14.27	0.87	0.20	0.67	0.96	0.623	1.05	0.590	1.07	1.30	0.729	No
218	14.34	0.87	0.20	0.67	0.96	0.623	1.05	0.591	1.07	1.30	0.730	No
219	14.37	0.87	0.20	0.67	0.96	0.624	1.05	0.592	1.07	1.30	0.730	No
220	14.44	0.88	0.20	0.68	0.96	0.625	1.05	0.593	1.07	1.30	0.731	No
221	14.51	0.88	0.20	0.68	0.96	0.626	1.05	0.593	1.07	1.30	0.732	No
222	14.57	0.89	0.20	0.68	0.96	0.627	1.05	0.594	1.07	1.30	0.734	No
223	14.64	0.89	0.21	0.68	0.96	0.627	1.05	0.595	1.07	1.30	0.735	No
224	14.70	0.89	0.21	0.68	0.96	0.628	1.05	0.596	1.07	1.30	0.736	No
225	14.77	0.90	0.21	0.69	0.96	0.629	1.05	0.597	1.07	1.30	0.738	No
226	14.84	0.90	0.21	0.69	0.96	0.630	1.05	0.597	1.06	1.30	0.739	No
227	14.90	0.91	0.22	0.69	0.96	0.631	1.05	0.598	1.06	1.30	0.741	No
228	14.97	0.91	0.22	0.69	0.96	0.632	1.05	0.599	1.06	1.30	0.743	No
229	15.03	0.91	0.22	0.69	0.96	0.632	1.05	0.600	1.06	1.30	0.744	No
230	15.10	0.92	0.22	0.70	0.96	0.633	1.05	0.601	1.06	1.30	0.745	No
231	15.16	0.92	0.22	0.70	0.96	0.634	1.05	0.601	1.06	1.30	0.747	No
232	15.26	0.93	0.23	0.70	0.96	0.635	1.05	0.602	1.06	1.30	0.748	No
233	15.32	0.93	0.23	0.70	0.96	0.636	1.05	0.603	1.06	1.30	0.749	No
234	15.39	0.94	0.23	0.71	0.96	0.637	1.05	0.604	1.06	1.30	0.751	No
235	15.45	0.94	0.23	0.71	0.96	0.637	1.05	0.605	1.06	1.30	0.752	No
236	15.52	0.94	0.23	0.71	0.96	0.638	1.05	0.605	1.06	1.30	0.753	No
237	15.55	0.95	0.24	0.71	0.96	0.639	1.05	0.606	1.06	1.30	0.754	No
238	15.62	0.95	0.24	0.71	0.96	0.639	1.05	0.606	1.06	1.30	0.756	No
239	15.69	0.95	0.24	0.71	0.96	0.640	1.05	0.607	1.06	1.30	0.757	No
240	15.75	0.96	0.24	0.72	0.96	0.641	1.05	0.608	1.06	1.30	0.760	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	15.82	0.96	0.24	0.72	0.96	0.642	1.05	0.609	1.05	1.30	0.768	No
242	15.89	0.97	0.25	0.72	0.96	0.643	1.05	0.609	1.05	1.30	0.770	No
243	15.96	0.97	0.25	0.72	0.96	0.643	1.05	0.610	1.05	1.30	0.773	No
244	16.02	0.98	0.25	0.72	0.96	0.644	1.05	0.611	1.05	1.30	0.775	No
245	16.09	0.98	0.25	0.73	0.96	0.645	1.05	0.612	1.05	1.30	0.778	No
246	16.15	0.98	0.25	0.73	0.96	0.646	1.05	0.612	1.05	1.30	0.783	No
247	16.22	0.99	0.26	0.73	0.96	0.646	1.05	0.613	1.04	1.30	0.785	No
248	16.28	0.99	0.26	0.73	0.96	0.647	1.05	0.614	1.04	1.30	0.789	No
249	16.35	0.99	0.26	0.73	0.96	0.648	1.05	0.614	1.04	1.30	0.793	No
250	16.42	1.00	0.26	0.74	0.96	0.648	1.05	0.615	1.04	1.30	0.797	No
251	16.48	1.00	0.26	0.74	0.95	0.649	1.05	0.616	1.04	1.30	0.801	No
252	16.55	1.01	0.27	0.74	0.95	0.650	1.05	0.616	1.04	1.30	0.805	No
253	16.61	1.01	0.27	0.74	0.95	0.651	1.05	0.617	1.03	1.30	0.807	No
254	16.68	1.01	0.27	0.74	0.95	0.651	1.05	0.618	1.03	1.30	0.809	No
255	16.75	1.02	0.27	0.75	0.95	0.652	1.05	0.618	1.03	1.30	0.811	No
256	16.82	1.02	0.28	0.75	0.95	0.653	1.05	0.619	1.03	1.30	0.812	No
257	16.88	1.03	0.28	0.75	0.95	0.654	1.05	0.620	1.03	1.30	0.813	No
258	16.95	1.03	0.28	0.75	0.95	0.654	1.05	0.620	1.03	1.30	0.814	No
259	17.02	1.03	0.28	0.75	0.95	0.655	1.05	0.621	1.03	1.30	0.813	No
260	17.09	1.04	0.28	0.76	0.95	0.656	1.05	0.622	1.03	1.30	0.811	No
261	17.15	1.04	0.29	0.76	0.95	0.656	1.05	0.622	1.04	1.30	0.809	No
262	17.22	1.05	0.29	0.76	0.95	0.657	1.05	0.623	1.04	1.30	0.806	No
263	17.29	1.05	0.29	0.76	0.95	0.658	1.05	0.624	1.04	1.30	0.804	No
264	17.36	1.06	0.29	0.76	0.95	0.658	1.05	0.624	1.04	1.30	0.801	No
265	17.39	1.06	0.29	0.76	0.95	0.659	1.05	0.625	1.04	1.30	0.800	No
266	17.46	1.06	0.30	0.77	0.95	0.659	1.05	0.625	1.04	1.30	0.797	No
267	17.53	1.07	0.30	0.77	0.95	0.660	1.05	0.626	1.04	1.30	0.795	No
268	17.59	1.07	0.30	0.77	0.95	0.660	1.05	0.626	1.05	1.30	0.793	No
269	17.66	1.07	0.30	0.77	0.95	0.661	1.05	0.627	1.05	1.30	0.792	No
270	17.73	1.08	0.30	0.77	0.95	0.662	1.05	0.627	1.05	1.30	0.792	No
271	17.79	1.08	0.31	0.78	0.95	0.662	1.05	0.628	1.05	1.30	0.791	No
272	17.86	1.09	0.31	0.78	0.95	0.663	1.05	0.629	1.05	1.30	0.791	No
273	17.93	1.09	0.31	0.78	0.95	0.663	1.05	0.629	1.05	1.30	0.792	No
274	17.99	1.10	0.31	0.78	0.95	0.664	1.05	0.630	1.05	1.30	0.793	No
275	18.06	1.10	0.31	0.79	0.95	0.664	1.05	0.630	1.04	1.30	0.795	No
276	18.13	1.10	0.32	0.79	0.95	0.665	1.05	0.631	1.04	1.30	0.797	No
277	18.20	1.11	0.32	0.79	0.95	0.666	1.05	0.631	1.04	1.30	0.798	No
278	18.26	1.11	0.32	0.79	0.95	0.666	1.05	0.632	1.04	1.30	0.801	No
279	18.33	1.12	0.32	0.79	0.95	0.667	1.05	0.632	1.04	1.30	0.803	No
280	18.40	1.12	0.32	0.80	0.95	0.667	1.05	0.633	1.04	1.30	0.807	No
281	18.45	1.12	0.33	0.80	0.95	0.668	1.05	0.633	1.04	1.30	0.816	No
282	18.51	1.13	0.33	0.80	0.95	0.668	1.05	0.634	1.04	1.30	0.815	No
283	18.57	1.13	0.33	0.80	0.95	0.669	1.05	0.634	1.03	1.30	0.819	No
284	18.64	1.14	0.33	0.80	0.95	0.669	1.05	0.635	1.03	1.30	0.824	No
285	18.72	1.14	0.33	0.81	0.95	0.670	1.05	0.635	1.03	1.30	0.829	No
286	18.77	1.14	0.34	0.81	0.95	0.670	1.05	0.636	1.03	1.30	0.833	No
287	18.86	1.15	0.34	0.81	0.95	0.671	1.05	0.636	1.03	1.30	0.838	No
288	18.91	1.15	0.34	0.81	0.95	0.671	1.05	0.637	1.03	1.30	0.840	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	18.98	1.16	0.34	0.81	0.94	0.672	1.05	0.637	1.02	1.30	0.842	No
290	19.04	1.16	0.34	0.82	0.94	0.673	1.05	0.638	1.02	1.30	0.844	No
291	19.11	1.16	0.35	0.82	0.94	0.673	1.05	0.638	1.02	1.30	0.846	No
292	19.18	1.17	0.35	0.82	0.94	0.674	1.05	0.639	1.02	1.30	0.847	No
293	19.24	1.17	0.35	0.82	0.94	0.674	1.05	0.639	1.02	1.30	0.848	No
294	19.31	1.18	0.35	0.82	0.94	0.675	1.05	0.640	1.02	1.30	0.850	No
295	19.37	1.18	0.35	0.82	0.94	0.675	1.05	0.640	1.02	1.30	0.851	No
296	19.44	1.18	0.36	0.83	0.94	0.676	1.05	0.641	1.02	1.30	0.852	No
297	19.51	1.19	0.36	0.83	0.94	0.676	1.05	0.642	1.02	1.30	0.853	No
298	19.58	1.19	0.36	0.83	0.94	0.677	1.05	0.642	1.02	1.30	0.853	No
299	19.64	1.19	0.36	0.83	0.94	0.677	1.05	0.643	1.02	1.30	0.854	No
300	19.71	1.20	0.37	0.83	0.94	0.678	1.05	0.643	1.02	1.30	0.855	No
301	19.78	1.20	0.37	0.83	0.94	0.679	1.05	0.644	1.02	1.30	0.856	No
302	19.84	1.21	0.37	0.84	0.94	0.679	1.05	0.644	1.02	1.30	0.857	No
303	19.91	1.21	0.37	0.84	0.94	0.680	1.05	0.645	1.02	1.30	0.858	No
304	19.98	1.21	0.37	0.84	0.94	0.680	1.05	0.645	1.02	1.30	0.858	No
305	20.02	1.22	0.38	0.84	0.94	0.681	1.05	0.645	1.02	1.30	0.859	No
306	20.10	1.22	0.38	0.84	0.94	0.681	1.05	0.646	1.02	1.30	0.860	No
307	20.15	1.22	0.38	0.84	0.94	0.682	1.05	0.646	1.02	1.30	0.860	No
308	20.22	1.23	0.38	0.85	0.94	0.682	1.05	0.647	1.02	1.30	0.861	No
309	20.28	1.23	0.38	0.85	0.94	0.682	1.05	0.647	1.02	1.30	0.862	No
310	20.34	1.24	0.39	0.85	0.94	0.683	1.05	0.648	1.02	1.30	0.863	No
311	20.41	1.24	0.39	0.85	0.94	0.683	1.05	0.648	1.02	1.30	0.863	No
312	20.48	1.24	0.39	0.85	0.94	0.684	1.05	0.649	1.02	1.30	0.864	No
313	20.55	1.25	0.39	0.86	0.94	0.684	1.05	0.649	1.02	1.30	0.865	No
314	20.61	1.25	0.39	0.86	0.94	0.685	1.05	0.650	1.02	1.30	0.866	No
315	20.68	1.25	0.40	0.86	0.94	0.685	1.05	0.650	1.02	1.30	0.866	No
316	20.74	1.26	0.40	0.86	0.94	0.686	1.05	0.651	1.02	1.30	0.867	No
317	20.81	1.26	0.40	0.86	0.94	0.686	1.05	0.651	1.02	1.30	0.867	No
318	20.88	1.27	0.40	0.86	0.94	0.687	1.05	0.651	1.02	1.30	0.868	No
319	20.95	1.27	0.40	0.87	0.94	0.687	1.05	0.652	1.02	1.30	0.869	No
320	21.00	1.27	0.41	0.87	0.94	0.688	1.05	0.652	1.02	1.30	0.870	No
321	21.08	1.28	0.41	0.87	0.94	0.688	1.05	0.653	1.02	1.30	0.870	No
322	21.13	1.28	0.41	0.87	0.94	0.689	1.05	0.653	1.02	1.30	0.871	No
323	21.22	1.29	0.41	0.87	0.94	0.689	1.05	0.654	1.02	1.30	0.871	No
324	21.29	1.29	0.41	0.88	0.94	0.690	1.05	0.654	1.02	1.30	0.872	No
325	21.36	1.29	0.42	0.88	0.93	0.690	1.05	0.655	1.02	1.30	0.873	No
326	21.42	1.30	0.42	0.88	0.93	0.691	1.05	0.655	1.02	1.30	0.874	No
327	21.49	1.30	0.42	0.88	0.93	0.691	1.05	0.655	1.02	1.30	0.874	No
328	21.55	1.31	0.42	0.88	0.93	0.691	1.05	0.656	1.02	1.30	0.875	No
329	21.62	1.31	0.42	0.88	0.93	0.692	1.05	0.656	1.02	1.30	0.876	No
330	21.65	1.31	0.43	0.89	0.93	0.692	1.05	0.656	1.02	1.30	0.876	No
331	21.72	1.32	0.43	0.89	0.93	0.692	1.05	0.657	1.02	1.30	0.877	No
332	21.79	1.32	0.43	0.89	0.93	0.693	1.05	0.657	1.02	1.30	0.877	No
333	21.85	1.32	0.43	0.89	0.93	0.693	1.05	0.657	1.02	1.30	0.878	No
334	21.92	1.33	0.43	0.89	0.93	0.694	1.05	0.658	1.01	1.30	0.879	No
335	21.99	1.33	0.44	0.89	0.93	0.694	1.05	0.658	1.01	1.30	0.879	No
336	22.06	1.34	0.44	0.90	0.93	0.694	1.05	0.659	1.01	1.30	0.880	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	22.12	1.34	0.44	0.90	0.93	0.695	1.05	0.659	1.01	1.30	0.880	No
338	22.19	1.34	0.44	0.90	0.93	0.695	1.05	0.659	1.01	1.30	0.881	No
339	22.26	1.35	0.44	0.90	0.93	0.696	1.05	0.660	1.01	1.30	0.881	No
340	22.32	1.35	0.45	0.90	0.93	0.696	1.05	0.660	1.01	1.30	0.882	No
341	22.39	1.36	0.45	0.91	0.93	0.696	1.05	0.660	1.01	1.30	0.882	No
342	22.45	1.36	0.45	0.91	0.93	0.697	1.05	0.661	1.01	1.30	0.881	No
343	22.52	1.36	0.45	0.91	0.93	0.697	1.05	0.661	1.02	1.30	0.879	No
344	22.59	1.37	0.46	0.91	0.93	0.697	1.05	0.661	1.02	1.30	0.876	No
345	22.66	1.37	0.46	0.91	0.93	0.698	1.05	0.662	1.02	1.30	0.872	No
346	22.73	1.38	0.46	0.92	0.93	0.698	1.05	0.662	1.02	1.30	0.869	No
347	22.79	1.38	0.46	0.92	0.93	0.698	1.05	0.662	1.02	1.30	0.867	No
348	22.86	1.38	0.46	0.92	0.93	0.699	1.05	0.663	1.02	1.30	0.866	No
349	22.93	1.39	0.47	0.92	0.93	0.699	1.05	0.663	1.02	1.30	0.865	No
350	22.99	1.39	0.47	0.92	0.93	0.699	1.05	0.663	1.02	1.30	0.865	No
351	23.05	1.40	0.47	0.93	0.93	0.700	1.05	0.664	1.02	1.30	0.867	No
352	23.10	1.40	0.47	0.93	0.93	0.700	1.05	0.664	1.02	1.30	0.865	No
353	23.19	1.40	0.47	0.93	0.93	0.700	1.05	0.664	1.02	1.30	0.863	No
354	23.26	1.41	0.48	0.93	0.93	0.701	1.05	0.664	1.02	1.30	0.862	No
355	23.32	1.41	0.48	0.93	0.93	0.701	1.05	0.665	1.02	1.30	0.859	No
356	23.39	1.42	0.48	0.94	0.93	0.701	1.05	0.665	1.02	1.30	0.858	No
357	23.45	1.42	0.48	0.94	0.93	0.701	1.05	0.665	1.02	1.30	0.856	No
358	23.52	1.42	0.48	0.94	0.93	0.702	1.05	0.665	1.02	1.30	0.855	No
359	23.59	1.43	0.49	0.94	0.93	0.702	1.05	0.666	1.02	1.30	0.854	No
360	23.65	1.43	0.49	0.94	0.92	0.702	1.05	0.666	1.02	1.30	0.854	No
361	23.72	1.44	0.49	0.95	0.92	0.702	1.05	0.666	1.02	1.30	0.854	No
362	23.78	1.44	0.49	0.95	0.92	0.703	1.05	0.666	1.02	1.30	0.856	No
363	23.82	1.44	0.49	0.95	0.92	0.703	1.05	0.667	1.02	1.30	0.858	No
364	23.89	1.45	0.50	0.95	0.92	0.703	1.05	0.667	1.02	1.30	0.863	No
365	23.96	1.45	0.50	0.95	0.92	0.703	1.05	0.667	1.01	1.30	0.869	No
366	24.02	1.46	0.50	0.96	0.92	0.704	1.05	0.667	1.01	1.30	0.875	No
367	24.09	1.46	0.50	0.96	0.92	0.704	1.05	0.668	1.01	1.30	0.881	No
368	24.16	1.46	0.50	0.96	0.92	0.704	1.05	0.668	1.01	1.30	0.887	No
369	24.22	1.47	0.51	0.96	0.92	0.704	1.05	0.668	1.01	1.30	0.892	No
370	24.29	1.47	0.51	0.96	0.92	0.705	1.05	0.668	1.01	1.30	0.895	No
371	24.36	1.48	0.51	0.97	0.92	0.705	1.05	0.669	1.01	1.30	0.897	No
372	24.43	1.48	0.51	0.97	0.92	0.705	1.05	0.669	1.01	1.30	0.899	No
373	24.49	1.48	0.51	0.97	0.92	0.706	1.05	0.669	1.01	1.30	0.899	No
374	24.56	1.49	0.52	0.97	0.92	0.706	1.05	0.669	1.01	1.30	0.900	No
375	24.63	1.49	0.52	0.97	0.92	0.706	1.05	0.670	1.01	1.30	0.900	No
376	24.69	1.50	0.52	0.98	0.92	0.706	1.05	0.670	1.01	1.30	0.899	No
377	24.76	1.50	0.52	0.98	0.92	0.707	1.05	0.670	1.01	1.30	0.897	No
378	24.83	1.50	0.52	0.98	0.92	0.707	1.05	0.670	1.01	1.30	0.893	No
379	24.89	1.51	0.53	0.98	0.92	0.707	1.05	0.671	1.01	1.30	0.890	No
380	24.96	1.51	0.53	0.98	0.92	0.707	1.05	0.671	1.01	1.30	0.887	No
381	25.03	1.52	0.53	0.99	0.92	0.708	1.05	0.671	1.01	1.30	0.884	No
382	25.09	1.52	0.53	0.99	0.92	0.708	1.05	0.671	1.01	1.30	0.881	No
383	25.16	1.53	0.54	0.99	0.92	0.708	1.05	0.671	1.01	1.30	0.879	No
384	25.23	1.53	0.54	0.99	0.92	0.708	1.05	0.672	1.01	1.30	0.877	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	25.29	1.53	0.54	0.99	0.92	0.708	1.05	0.672	1.01	1.30	0.874	No
386	25.36	1.54	0.54	1.00	0.92	0.709	1.05	0.672	1.01	1.30	0.873	No
387	25.43	1.54	0.54	1.00	0.92	0.709	1.05	0.672	1.01	1.30	0.874	No
388	25.49	1.55	0.55	1.00	0.92	0.709	1.05	0.672	1.01	1.30	0.877	No
389	25.53	1.55	0.55	1.00	0.92	0.709	1.05	0.672	1.01	1.30	0.879	No
390	25.60	1.55	0.55	1.00	0.92	0.709	1.05	0.673	1.01	1.30	0.884	No
391	25.66	1.56	0.55	1.01	0.92	0.709	1.05	0.673	1.01	1.30	0.889	No
392	25.73	1.56	0.55	1.01	0.92	0.710	1.05	0.673	1.01	1.30	0.895	No
393	25.80	1.57	0.56	1.01	0.92	0.710	1.05	0.673	1.01	1.30	0.899	No
394	25.85	1.57	0.56	1.01	0.92	0.710	1.05	0.673	1.00	1.30	0.902	No
395	25.93	1.57	0.56	1.02	0.91	0.710	1.05	0.674	1.00	1.30	0.905	No
396	25.99	1.58	0.56	1.02	0.91	0.710	1.05	0.674	1.00	1.30	0.906	No
397	26.07	1.58	0.56	1.02	0.91	0.711	1.05	0.674	1.00	1.30	0.909	No
398	26.13	1.59	0.57	1.02	0.91	0.711	1.05	0.674	1.00	1.30	0.910	No
399	26.18	1.59	0.57	1.02	0.91	0.711	1.05	0.674	1.00	1.30	0.910	No
400	26.26	1.59	0.57	1.02	0.91	0.711	1.05	0.675	1.00	1.30	0.911	No
401	26.32	1.60	0.57	1.03	0.91	0.711	1.05	0.675	1.00	1.30	0.912	No
402	26.39	1.60	0.57	1.03	0.91	0.712	1.05	0.675	1.00	1.30	0.912	No
403	26.46	1.61	0.58	1.03	0.91	0.712	1.05	0.675	1.00	1.30	0.913	No
404	26.51	1.61	0.58	1.03	0.91	0.712	1.05	0.675	1.00	1.30	0.913	No
405	26.58	1.61	0.58	1.03	0.91	0.712	1.05	0.676	1.00	1.30	0.913	No
406	26.66	1.62	0.58	1.04	0.91	0.713	1.05	0.676	1.00	1.30	0.914	No
407	26.72	1.62	0.58	1.04	0.91	0.713	1.05	0.676	1.00	1.30	0.913	No
408	26.80	1.63	0.59	1.04	0.91	0.713	1.05	0.676	1.00	1.30	0.912	No
409	26.85	1.63	0.59	1.04	0.91	0.713	1.05	0.676	1.00	1.30	0.911	No
410	26.91	1.63	0.59	1.04	0.91	0.713	1.05	0.676	1.00	1.30	0.910	No
411	26.98	1.64	0.59	1.05	0.91	0.713	1.05	0.677	1.00	1.30	0.910	No
412	27.04	1.64	0.59	1.05	0.91	0.714	1.05	0.677	1.00	1.30	0.910	No
413	27.11	1.65	0.60	1.05	0.91	0.714	1.05	0.677	1.00	1.30	0.911	No
414	27.19	1.65	0.60	1.05	0.91	0.714	1.05	0.677	1.00	1.30	0.913	No
415	27.24	1.65	0.60	1.05	0.91	0.714	1.05	0.677	1.00	1.30	0.914	No
416	27.30	1.66	0.60	1.06	0.91	0.714	1.05	0.677	1.00	1.30	0.915	No
417	27.37	1.66	0.60	1.06	0.91	0.714	1.05	0.678	1.00	1.30	0.916	No
418	27.43	1.67	0.61	1.06	0.91	0.715	1.05	0.678	1.00	1.30	0.916	No
419	27.52	1.67	0.61	1.06	0.91	0.715	1.05	0.678	1.00	1.30	0.916	No
420	27.58	1.67	0.61	1.06	0.91	0.715	1.05	0.678	1.00	1.30	0.916	No
421	27.63	1.68	0.61	1.06	0.91	0.715	1.05	0.678	1.00	1.30	0.915	No
422	27.72	1.68	0.62	1.07	0.91	0.715	1.05	0.678	1.00	1.30	0.913	No
423	27.79	1.69	0.62	1.07	0.91	0.715	1.05	0.678	1.00	1.30	0.912	No
424	27.85	1.69	0.62	1.07	0.91	0.715	1.05	0.679	1.00	1.30	0.910	No
425	27.89	1.69	0.62	1.07	0.91	0.716	1.05	0.679	1.00	1.30	0.910	No
426	27.95	1.70	0.62	1.07	0.91	0.716	1.05	0.679	1.00	1.30	0.909	No
427	28.02	1.70	0.62	1.08	0.91	0.716	1.05	0.679	1.00	1.30	0.909	No
428	28.09	1.71	0.63	1.08	0.90	0.716	1.05	0.679	1.00	1.30	0.908	No
429	28.16	1.71	0.63	1.08	0.90	0.716	1.05	0.679	1.00	1.30	0.908	No
430	28.23	1.71	0.63	1.08	0.90	0.716	1.05	0.679	1.00	1.30	0.907	No
431	28.28	1.72	0.63	1.08	0.90	0.716	1.05	0.679	1.00	1.30	0.908	No
432	28.36	1.72	0.64	1.09	0.90	0.717	1.05	0.680	1.00	1.30	0.908	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	28.42	1.73	0.64	1.09	0.90	0.717	1.05	0.680	1.00	1.30	0.907	No
434	28.48	1.73	0.64	1.09	0.90	0.717	1.05	0.680	1.00	1.30	0.906	No
435	28.57	1.73	0.64	1.09	0.90	0.717	1.05	0.680	1.00	1.30	0.904	No
436	28.63	1.74	0.64	1.09	0.90	0.717	1.05	0.680	1.00	1.30	0.904	No
437	28.69	1.74	0.65	1.10	0.90	0.717	1.05	0.680	0.99	1.30	0.903	No
438	28.76	1.75	0.65	1.10	0.90	0.717	1.05	0.680	0.99	1.30	0.902	No
439	28.82	1.75	0.65	1.10	0.90	0.717	1.05	0.680	0.99	1.30	0.902	No
440	28.89	1.76	0.65	1.10	0.90	0.717	1.05	0.680	0.99	1.30	0.902	No
441	28.96	1.76	0.65	1.11	0.90	0.718	1.05	0.681	0.99	1.30	0.902	No
442	29.02	1.76	0.66	1.11	0.90	0.718	1.05	0.681	0.99	1.30	0.903	No
443	29.09	1.77	0.66	1.11	0.90	0.718	1.05	0.681	0.99	1.30	0.904	No
444	29.16	1.77	0.66	1.11	0.90	0.718	1.05	0.681	0.99	1.30	0.906	No
445	29.23	1.78	0.66	1.11	0.90	0.718	1.05	0.681	0.99	1.30	0.907	No
446	29.29	1.78	0.66	1.12	0.90	0.718	1.05	0.681	0.99	1.30	0.909	No
447	29.36	1.78	0.67	1.12	0.90	0.718	1.05	0.681	0.99	1.30	0.912	No
448	29.43	1.79	0.67	1.12	0.90	0.718	1.05	0.681	0.99	1.30	0.915	No
449	29.49	1.79	0.67	1.12	0.90	0.718	1.05	0.681	0.99	1.30	0.918	No
450	29.56	1.80	0.67	1.12	0.90	0.718	1.05	0.681	0.99	1.30	0.922	No
451	29.59	1.80	0.67	1.13	0.90	0.718	1.05	0.681	0.99	1.30	0.923	No
452	29.66	1.80	0.68	1.13	0.90	0.718	1.05	0.681	0.99	1.30	0.926	No
453	29.73	1.81	0.68	1.13	0.90	0.719	1.05	0.682	0.99	1.30	0.928	No
454	29.79	1.81	0.68	1.13	0.90	0.719	1.05	0.682	0.99	1.30	0.929	No
455	29.88	1.82	0.68	1.13	0.90	0.719	1.05	0.682	0.99	1.30	0.930	No
456	29.94	1.82	0.68	1.14	0.90	0.719	1.05	0.682	0.99	1.30	0.930	No
457	30.01	1.82	0.69	1.14	0.90	0.719	1.05	0.682	0.99	1.30	0.931	No
458	30.06	1.83	0.69	1.14	0.90	0.719	1.05	0.682	0.99	1.30	0.931	No
459	30.12	1.83	0.69	1.14	0.90	0.719	1.05	0.682	0.99	1.30	0.931	No
460	30.19	1.83	0.69	1.14	0.90	0.719	1.05	0.682	0.99	1.30	0.932	No
461	30.26	1.84	0.69	1.14	0.89	0.720	1.05	0.682	0.99	1.30	0.932	No
462	30.32	1.84	0.70	1.15	0.89	0.720	1.05	0.683	0.99	1.30	0.933	No
463	30.39	1.85	0.70	1.15	0.89	0.720	1.05	0.683	0.99	1.30	0.933	No
464	30.45	1.85	0.70	1.15	0.89	0.720	1.05	0.683	0.99	1.30	0.933	No
465	30.52	1.85	0.70	1.15	0.89	0.720	1.05	0.683	0.99	1.30	0.933	No
466	30.59	1.86	0.70	1.15	0.89	0.720	1.05	0.683	0.99	1.30	0.934	No
467	30.66	1.86	0.71	1.15	0.89	0.720	1.05	0.683	0.99	1.30	0.934	No
468	30.72	1.87	0.71	1.16	0.89	0.721	1.05	0.683	0.99	1.30	0.934	No
469	30.79	1.87	0.71	1.16	0.89	0.721	1.05	0.684	0.99	1.30	0.935	No
470	30.85	1.87	0.71	1.16	0.89	0.721	1.05	0.684	0.99	1.30	0.935	No
471	30.92	1.88	0.72	1.16	0.89	0.721	1.05	0.684	0.99	1.30	0.935	No
472	30.97	1.88	0.72	1.16	0.89	0.721	1.05	0.684	0.99	1.30	0.935	No
473	31.07	1.89	0.72	1.17	0.89	0.721	1.05	0.684	0.99	1.30	0.936	No
474	31.10	1.89	0.72	1.17	0.89	0.721	1.05	0.684	0.99	1.30	0.936	No
475	31.19	1.89	0.72	1.17	0.89	0.721	1.05	0.684	0.99	1.30	0.936	No
476	31.24	1.89	0.72	1.17	0.89	0.722	1.05	0.684	0.99	1.30	0.936	No
477	31.30	1.90	0.73	1.17	0.89	0.722	1.05	0.684	0.99	1.30	0.937	No
478	31.38	1.90	0.73	1.17	0.89	0.722	1.05	0.685	0.99	1.30	0.937	No
479	31.43	1.91	0.73	1.18	0.89	0.722	1.05	0.685	0.99	1.30	0.937	No
480	31.50	1.91	0.73	1.18	0.89	0.722	1.05	0.685	0.99	1.30	0.938	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	31.57	1.91	0.74	1.18	0.89	0.722	1.05	0.685	0.99	1.30	0.938	No
482	31.63	1.92	0.74	1.18	0.89	0.722	1.05	0.685	0.99	1.30	0.938	No
483	31.70	1.92	0.74	1.18	0.89	0.722	1.05	0.685	0.99	1.30	0.938	No
484	31.77	1.93	0.74	1.18	0.89	0.722	1.05	0.685	0.99	1.30	0.939	No
485	31.84	1.93	0.74	1.19	0.89	0.723	1.05	0.685	0.99	1.30	0.939	No
486	31.90	1.93	0.75	1.19	0.89	0.723	1.05	0.685	0.99	1.30	0.939	No
487	31.97	1.94	0.75	1.19	0.89	0.723	1.05	0.685	0.99	1.30	0.939	No
488	32.03	1.94	0.75	1.19	0.89	0.723	1.05	0.686	0.99	1.30	0.939	No
489	32.10	1.94	0.75	1.19	0.89	0.723	1.05	0.686	0.99	1.30	0.939	No
490	32.17	1.95	0.75	1.19	0.89	0.723	1.05	0.686	0.99	1.30	0.940	No
491	32.23	1.95	0.76	1.20	0.89	0.723	1.05	0.686	0.99	1.30	0.940	No
492	32.29	1.96	0.76	1.20	0.89	0.723	1.05	0.686	0.99	1.30	0.940	No
493	32.35	1.96	0.76	1.20	0.88	0.723	1.05	0.686	0.99	1.30	0.941	No
494	32.42	1.96	0.76	1.20	0.88	0.723	1.05	0.686	0.99	1.30	0.941	No
495	32.49	1.97	0.76	1.20	0.88	0.723	1.05	0.686	0.99	1.30	0.941	No
496	32.56	1.97	0.77	1.21	0.88	0.723	1.05	0.686	0.99	1.30	0.941	No
497	32.62	1.98	0.77	1.21	0.88	0.724	1.05	0.686	0.99	1.30	0.942	No
498	32.68	1.98	0.77	1.21	0.88	0.724	1.05	0.686	0.99	1.30	0.942	No
499	32.75	1.98	0.77	1.21	0.88	0.724	1.05	0.686	0.99	1.30	0.942	No
500	32.82	1.99	0.77	1.21	0.88	0.724	1.05	0.686	0.99	1.30	0.942	No
501	32.88	1.99	0.78	1.21	0.88	0.724	1.05	0.686	0.99	1.30	0.942	No
502	32.95	1.99	0.78	1.22	0.88	0.724	1.05	0.687	0.99	1.30	0.942	No
503	33.01	2.00	0.78	1.22	0.88	0.724	1.05	0.687	0.99	1.30	0.942	No
504	33.08	2.00	0.78	1.22	0.88	0.724	1.05	0.687	0.99	1.30	0.942	No
505	33.15	2.01	0.78	1.22	0.88	0.724	1.05	0.687	0.99	1.30	0.941	No
506	33.21	2.01	0.79	1.22	0.88	0.724	1.05	0.687	0.99	1.30	0.940	No
507	33.28	2.01	0.79	1.23	0.88	0.724	1.05	0.687	0.98	1.30	0.940	No
508	33.35	2.02	0.79	1.23	0.88	0.724	1.05	0.687	0.98	1.30	0.940	No
509	33.41	2.02	0.79	1.23	0.88	0.724	1.05	0.687	0.98	1.30	0.941	No
510	33.48	2.03	0.80	1.23	0.88	0.724	1.05	0.687	0.99	1.30	0.942	No
511	33.55	2.03	0.80	1.23	0.88	0.724	1.05	0.687	0.99	1.30	0.943	No
512	33.62	2.04	0.80	1.24	0.88	0.724	1.05	0.687	0.99	1.30	0.943	No
513	33.68	2.04	0.80	1.24	0.88	0.724	1.05	0.687	0.99	1.30	0.944	No
514	33.75	2.04	0.80	1.24	0.88	0.724	1.05	0.687	0.99	1.30	0.944	No
515	33.82	2.05	0.81	1.24	0.88	0.724	1.05	0.687	0.99	1.30	0.944	No
516	33.88	2.05	0.81	1.24	0.88	0.724	1.05	0.687	0.99	1.30	0.945	No
517	33.95	2.06	0.81	1.25	0.88	0.724	1.05	0.687	0.99	1.30	0.945	No
518	34.02	2.06	0.81	1.25	0.88	0.724	1.05	0.687	0.99	1.30	0.945	No
519	34.09	2.06	0.81	1.25	0.88	0.724	1.05	0.687	0.99	1.30	0.946	No
520	34.15	2.07	0.82	1.25	0.88	0.724	1.05	0.687	0.99	1.30	0.946	No
521	34.19	2.07	0.82	1.25	0.88	0.725	1.05	0.687	0.99	1.30	0.946	No
522	34.25	2.07	0.82	1.25	0.88	0.725	1.05	0.687	0.99	1.30	0.946	No
523	34.33	2.08	0.82	1.26	0.88	0.725	1.05	0.687	0.99	1.30	0.946	No
524	34.40	2.08	0.82	1.26	0.87	0.725	1.05	0.687	0.99	1.30	0.947	No
525	34.46	2.08	0.83	1.26	0.87	0.725	1.05	0.687	0.99	1.30	0.947	No
526	34.52	2.09	0.83	1.26	0.87	0.725	1.05	0.687	0.99	1.30	0.947	No
527	34.59	2.09	0.83	1.26	0.87	0.725	1.05	0.687	0.99	1.30	0.947	No
528	34.66	2.10	0.83	1.26	0.87	0.725	1.05	0.688	0.99	1.30	0.947	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
529	34.73	2.10	0.83	1.27	0.87	0.725	1.05	0.688	0.99	1.30	0.947	No
530	34.79	2.10	0.84	1.27	0.87	0.725	1.05	0.688	0.99	1.30	0.948	No
531	34.86	2.11	0.84	1.27	0.87	0.725	1.05	0.688	0.98	1.30	0.948	No
532	34.93	2.11	0.84	1.27	0.87	0.725	1.05	0.688	0.98	1.30	0.948	No
533	34.99	2.11	0.84	1.27	0.87	0.725	1.05	0.688	0.98	1.30	0.948	No
534	35.06	2.12	0.84	1.27	0.87	0.725	1.05	0.688	0.98	1.30	0.948	No
535	35.13	2.12	0.85	1.28	0.87	0.725	1.05	0.688	0.98	1.30	0.948	No
536	35.20	2.13	0.85	1.28	0.87	0.725	1.05	0.688	0.98	1.30	0.949	No
537	35.26	2.13	0.85	1.28	0.87	0.725	1.05	0.688	0.98	1.30	0.949	No
538	35.33	2.13	0.85	1.28	0.87	0.725	1.05	0.688	0.98	1.30	0.949	No
539	35.40	2.14	0.85	1.28	0.87	0.725	1.05	0.688	0.98	1.30	0.949	No
540	35.47	2.14	0.86	1.29	0.87	0.725	1.05	0.688	0.98	1.30	0.949	No
541	35.53	2.15	0.86	1.29	0.87	0.725	1.05	0.688	0.98	1.30	0.949	No
542	35.60	2.15	0.86	1.29	0.87	0.726	1.05	0.688	0.98	1.30	0.949	No
543	35.66	2.15	0.86	1.29	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
544	35.70	2.16	0.86	1.29	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
545	35.77	2.16	0.87	1.29	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
546	35.83	2.16	0.87	1.30	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
547	35.90	2.17	0.87	1.30	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
548	35.97	2.17	0.87	1.30	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
549	36.03	2.18	0.87	1.30	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
550	36.10	2.18	0.88	1.30	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
551	36.17	2.18	0.88	1.31	0.87	0.726	1.05	0.688	0.98	1.30	0.950	No
552	36.23	2.19	0.88	1.31	0.87	0.726	1.05	0.688	0.98	1.30	0.951	No
553	36.30	2.19	0.88	1.31	0.87	0.725	1.05	0.688	0.98	1.30	0.951	No
554	36.37	2.20	0.89	1.31	0.87	0.725	1.05	0.688	0.98	1.30	0.951	No
555	36.43	2.20	0.89	1.31	0.86	0.725	1.05	0.688	0.98	1.30	0.951	No
556	36.50	2.20	0.89	1.31	0.86	0.725	1.05	0.688	0.98	1.30	0.950	No
557	36.57	2.21	0.89	1.32	0.86	0.725	1.05	0.688	0.98	1.30	0.949	No
558	36.64	2.21	0.89	1.32	0.86	0.725	1.05	0.688	0.98	1.30	0.949	No
559	36.70	2.22	0.90	1.32	0.86	0.725	1.05	0.688	0.98	1.30	0.948	No
560	36.77	2.22	0.90	1.32	0.86	0.725	1.05	0.688	0.97	1.30	0.948	No
561	36.84	2.22	0.90	1.32	0.86	0.725	1.05	0.688	0.98	1.30	0.949	No
562	36.91	2.23	0.90	1.33	0.86	0.725	1.05	0.688	0.98	1.30	0.950	No
563	36.97	2.23	0.90	1.33	0.86	0.725	1.05	0.688	0.98	1.30	0.951	No
564	37.04	2.24	0.91	1.33	0.86	0.725	1.05	0.688	0.98	1.30	0.951	No
565	37.11	2.24	0.91	1.33	0.86	0.725	1.05	0.688	0.98	1.30	0.951	No
566	37.14	2.24	0.91	1.33	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
567	37.21	2.25	0.91	1.34	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
568	37.27	2.25	0.91	1.34	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
569	37.34	2.25	0.92	1.34	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
570	37.41	2.26	0.92	1.34	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
571	37.48	2.26	0.92	1.34	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
572	37.54	2.27	0.92	1.35	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
573	37.61	2.27	0.92	1.35	0.86	0.725	1.05	0.688	0.98	1.30	0.952	No
574	37.68	2.27	0.93	1.35	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No
575	37.74	2.28	0.93	1.35	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No
576	37.81	2.28	0.93	1.35	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
577	37.88	2.29	0.93	1.35	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No
578	37.94	2.29	0.93	1.36	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No
579	38.01	2.30	0.94	1.36	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No
580	38.08	2.30	0.94	1.36	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No
581	38.15	2.30	0.94	1.36	0.86	0.725	1.05	0.687	0.98	1.30	0.952	No
582	38.21	2.31	0.94	1.37	0.86	0.724	1.05	0.687	0.98	1.30	0.952	No
583	38.28	2.31	0.94	1.37	0.86	0.724	1.05	0.687	0.97	1.30	0.952	No
584	38.34	2.32	0.95	1.37	0.86	0.724	1.05	0.687	0.97	1.30	0.951	No
585	38.41	2.32	0.95	1.37	0.86	0.724	1.05	0.687	0.97	1.30	0.950	No
586	38.48	2.32	0.95	1.37	0.85	0.724	1.05	0.687	0.97	1.30	0.949	No
587	38.55	2.33	0.95	1.38	0.85	0.724	1.05	0.687	0.97	1.30	0.947	No
588	38.61	2.33	0.96	1.38	0.85	0.724	1.05	0.687	0.96	1.30	0.946	No
589	38.68	2.34	0.96	1.38	0.85	0.724	1.05	0.687	0.96	1.30	0.947	No
590	38.75	2.34	0.96	1.38	0.85	0.724	1.05	0.686	0.97	1.30	0.948	No
591	38.78	2.34	0.96	1.38	0.85	0.724	1.05	0.686	0.97	1.30	0.949	No
592	38.85	2.35	0.96	1.39	0.85	0.724	1.05	0.686	0.97	1.30	0.950	No
593	38.92	2.35	0.96	1.39	0.85	0.724	1.05	0.686	0.97	1.30	0.951	No
594	38.98	2.36	0.97	1.39	0.85	0.723	1.05	0.686	0.97	1.30	0.952	No
595	39.05	2.36	0.97	1.39	0.85	0.723	1.05	0.686	0.97	1.30	0.953	No
596	39.11	2.36	0.97	1.39	0.85	0.723	1.05	0.686	0.97	1.30	0.953	No
597	39.19	2.37	0.97	1.40	0.85	0.723	1.05	0.686	0.97	1.30	0.953	No
598	39.24	2.37	0.97	1.40	0.85	0.723	1.05	0.686	0.97	1.30	0.953	No
599	39.32	2.38	0.98	1.40	0.85	0.723	1.05	0.686	0.98	1.30	0.953	No
600	39.38	2.38	0.98	1.40	0.85	0.723	1.05	0.686	0.98	1.30	0.953	No
601	39.45	2.38	0.98	1.40	0.85	0.723	1.05	0.686	0.97	1.30	0.953	No
602	39.51	2.39	0.98	1.40	0.85	0.723	1.05	0.686	0.97	1.30	0.953	No
603	39.58	2.39	0.99	1.41	0.85	0.723	1.05	0.686	0.97	1.30	0.953	No
604	39.64	2.40	0.99	1.41	0.85	0.723	1.05	0.685	0.97	1.30	0.953	No
605	39.72	2.40	0.99	1.41	0.85	0.723	1.05	0.685	0.97	1.30	0.953	No
606	39.77	2.40	0.99	1.41	0.85	0.723	1.05	0.685	0.97	1.30	0.953	No
607	39.84	2.41	0.99	1.42	0.85	0.723	1.05	0.685	0.97	1.30	0.953	No
608	39.90	2.41	1.00	1.42	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
609	39.96	2.42	1.00	1.42	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
610	40.03	2.42	1.00	1.42	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
611	40.09	2.42	1.00	1.42	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
612	40.17	2.43	1.00	1.43	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
613	40.25	2.43	1.01	1.43	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
614	40.31	2.44	1.01	1.43	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
615	40.37	2.44	1.01	1.43	0.85	0.722	1.05	0.685	0.97	1.30	0.953	No
616	40.42	2.44	1.01	1.43	0.85	0.722	1.05	0.684	0.97	1.30	0.953	No
617	40.51	2.45	1.01	1.44	0.84	0.722	1.05	0.684	0.97	1.30	0.953	No
618	40.56	2.45	1.02	1.44	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No
619	40.62	2.46	1.02	1.44	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No
620	40.71	2.46	1.02	1.44	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No
621	40.78	2.47	1.02	1.44	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No
622	40.85	2.47	1.02	1.45	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No
623	40.91	2.48	1.03	1.45	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No
624	40.95	2.48	1.03	1.45	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
625	41.02	2.48	1.03	1.45	0.84	0.721	1.05	0.684	0.97	1.30	0.953	No
626	41.08	2.49	1.03	1.45	0.84	0.721	1.05	0.683	0.96	1.30	0.952	No
627	41.15	2.49	1.03	1.46	0.84	0.721	1.05	0.683	0.96	1.30	0.951	No
628	41.22	2.49	1.04	1.46	0.84	0.720	1.05	0.683	0.96	1.30	0.949	No
629	41.28	2.50	1.04	1.46	0.84	0.720	1.05	0.683	0.95	1.30	0.946	No
630	41.34	2.50	1.04	1.46	0.84	0.720	1.05	0.683	0.95	1.30	0.944	No
631	41.44	2.51	1.04	1.47	0.84	0.720	1.05	0.683	0.94	1.30	0.943	No
632	41.50	2.51	1.05	1.47	0.84	0.720	1.05	0.683	0.94	1.30	0.943	No
633	41.57	2.52	1.05	1.47	0.84	0.720	1.05	0.683	0.94	1.30	0.943	No
634	41.60	2.52	1.05	1.47	0.84	0.720	1.05	0.683	0.94	1.30	0.943	No
635	41.67	2.52	1.05	1.47	0.84	0.719	1.05	0.682	0.94	1.30	0.943	No
636	41.74	2.53	1.05	1.47	0.84	0.719	1.05	0.682	0.94	1.30	0.944	No
637	41.81	2.53	1.05	1.48	0.84	0.719	1.05	0.682	0.94	1.30	0.943	No
638	41.87	2.54	1.06	1.48	0.84	0.719	1.05	0.682	0.94	1.30	0.943	No
639	41.94	2.54	1.06	1.48	0.84	0.719	1.05	0.682	0.94	1.30	0.944	No
640	42.00	2.54	1.06	1.48	0.84	0.719	1.05	0.682	0.95	1.30	0.946	No
641	42.07	2.55	1.06	1.49	0.84	0.719	1.05	0.682	0.94	1.30	0.944	No
642	42.14	2.55	1.07	1.49	0.84	0.719	1.05	0.681	0.94	1.30	0.945	No
643	42.20	2.56	1.07	1.49	0.84	0.718	1.05	0.681	0.94	1.30	0.944	No
644	42.28	2.56	1.07	1.49	0.84	0.718	1.05	0.681	0.94	1.30	0.945	No
645	42.35	2.57	1.07	1.50	0.84	0.718	1.05	0.681	0.95	1.30	0.946	No
646	42.42	2.57	1.07	1.50	0.84	0.718	1.05	0.681	0.95	1.30	0.946	No
647	42.48	2.58	1.08	1.50	0.84	0.718	1.05	0.681	0.95	1.30	0.946	No
648	42.55	2.58	1.08	1.50	0.83	0.718	1.05	0.681	0.95	1.30	0.946	No
649	42.62	2.58	1.08	1.50	0.83	0.717	1.05	0.680	0.95	1.30	0.947	No
650	42.68	2.59	1.08	1.51	0.83	0.717	1.05	0.680	0.95	1.30	0.947	No
651	42.72	2.59	1.08	1.51	0.83	0.717	1.05	0.680	0.95	1.30	0.948	No
652	42.78	2.60	1.09	1.51	0.83	0.717	1.05	0.680	0.95	1.30	0.948	No
653	42.85	2.60	1.09	1.51	0.83	0.717	1.05	0.680	0.95	1.30	0.949	No
654	42.92	2.60	1.09	1.51	0.83	0.717	1.05	0.680	0.95	1.30	0.950	No
655	42.99	2.61	1.09	1.52	0.83	0.717	1.05	0.680	0.96	1.30	0.951	No
656	43.05	2.61	1.09	1.52	0.83	0.716	1.05	0.680	0.96	1.30	0.951	No
657	43.12	2.62	1.10	1.52	0.83	0.716	1.05	0.679	0.96	1.30	0.951	No
658	43.18	2.62	1.10	1.52	0.83	0.716	1.05	0.679	0.96	1.30	0.951	No
659	43.25	2.62	1.10	1.52	0.83	0.716	1.05	0.679	0.96	1.30	0.951	No
660	43.32	2.63	1.10	1.53	0.83	0.716	1.05	0.679	0.96	1.30	0.951	No
661	43.38	2.63	1.10	1.53	0.83	0.716	1.05	0.679	0.96	1.30	0.952	No
662	43.45	2.64	1.11	1.53	0.83	0.716	1.05	0.679	0.96	1.30	0.952	No
663	43.52	2.64	1.11	1.53	0.83	0.716	1.05	0.679	0.96	1.30	0.952	No
664	43.59	2.65	1.11	1.54	0.83	0.715	1.05	0.679	0.96	1.30	0.951	No
665	43.65	2.65	1.11	1.54	0.83	0.715	1.05	0.678	0.96	1.30	0.951	No
666	43.72	2.65	1.11	1.54	0.83	0.715	1.05	0.678	0.96	1.30	0.951	No
667	43.79	2.66	1.12	1.54	0.83	0.715	1.05	0.678	0.96	1.30	0.951	No
668	43.86	2.66	1.12	1.54	0.83	0.715	1.05	0.678	0.97	1.30	0.951	No
669	43.92	2.67	1.12	1.55	0.83	0.715	1.05	0.678	0.97	1.30	0.951	No
670	43.98	2.67	1.12	1.55	0.83	0.715	1.05	0.678	0.96	1.30	0.951	No
671	44.04	2.67	1.12	1.55	0.83	0.715	1.05	0.678	0.96	1.30	0.951	No
672	44.12	2.68	1.13	1.55	0.83	0.714	1.05	0.678	0.96	1.30	0.951	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
673	44.19	2.68	1.13	1.55	0.83	0.714	1.05	0.677	0.95	1.30	0.951	No
674	44.25	2.69	1.13	1.56	0.83	0.714	1.05	0.677	0.95	1.30	0.950	No
675	44.31	2.69	1.13	1.56	0.83	0.714	1.05	0.677	0.95	1.30	0.950	No
676	44.38	2.69	1.14	1.56	0.83	0.714	1.05	0.677	0.95	1.30	0.949	No
677	44.45	2.70	1.14	1.56	0.83	0.714	1.05	0.677	0.95	1.30	0.949	No
678	44.52	2.70	1.14	1.56	0.82	0.714	1.05	0.677	0.95	1.30	0.949	No
679	44.58	2.71	1.14	1.57	0.82	0.713	1.05	0.677	0.95	1.30	0.949	No
680	44.65	2.71	1.14	1.57	0.82	0.713	1.05	0.677	0.94	1.30	0.949	No
681	44.72	2.72	1.15	1.57	0.82	0.713	1.05	0.676	0.94	1.30	0.948	No
682	44.78	2.72	1.15	1.57	0.82	0.713	1.05	0.676	0.94	1.30	0.948	No
683	44.85	2.72	1.15	1.57	0.82	0.713	1.05	0.676	0.94	1.30	0.948	No
684	44.88	2.73	1.15	1.58	0.82	0.713	1.05	0.676	0.94	1.30	0.948	No
685	44.95	2.73	1.15	1.58	0.82	0.713	1.05	0.676	0.94	1.30	0.948	No
686	45.02	2.74	1.15	1.58	0.82	0.712	1.05	0.676	0.94	1.30	0.948	No
687	45.09	2.74	1.16	1.58	0.82	0.712	1.05	0.676	0.94	1.30	0.948	No
688	45.16	2.74	1.16	1.59	0.82	0.712	1.05	0.675	0.94	1.30	0.948	No
689	45.22	2.75	1.16	1.59	0.82	0.712	1.05	0.675	0.94	1.30	0.948	No
690	45.29	2.75	1.16	1.59	0.82	0.712	1.05	0.675	0.94	1.30	0.948	No
691	45.35	2.76	1.17	1.59	0.82	0.712	1.05	0.675	0.94	1.30	0.948	No
692	45.42	2.76	1.17	1.59	0.82	0.711	1.05	0.675	0.94	1.30	0.948	No
693	45.49	2.77	1.17	1.60	0.82	0.711	1.05	0.675	0.94	1.30	0.948	No
694	45.56	2.77	1.17	1.60	0.82	0.711	1.05	0.674	0.94	1.30	0.948	No
695	45.62	2.77	1.17	1.60	0.82	0.711	1.05	0.674	0.94	1.30	0.948	No
696	45.69	2.78	1.18	1.60	0.82	0.711	1.05	0.674	0.94	1.30	0.948	No
697	45.76	2.78	1.18	1.60	0.82	0.711	1.05	0.674	0.94	1.30	0.948	No
698	45.82	2.79	1.18	1.61	0.82	0.710	1.05	0.674	0.94	1.30	0.948	No
699	45.89	2.79	1.18	1.61	0.82	0.710	1.05	0.674	0.94	1.30	0.948	No
700	45.96	2.80	1.18	1.61	0.82	0.710	1.05	0.673	0.94	1.30	0.948	No
701	46.02	2.80	1.19	1.61	0.82	0.710	1.05	0.673	0.94	1.30	0.948	No
702	46.09	2.80	1.19	1.62	0.82	0.710	1.05	0.673	0.94	1.30	0.948	No
703	46.16	2.81	1.19	1.62	0.82	0.710	1.05	0.673	0.94	1.30	0.948	No
704	46.22	2.81	1.19	1.62	0.82	0.709	1.05	0.673	0.94	1.30	0.949	No
705	46.29	2.82	1.19	1.62	0.82	0.709	1.05	0.673	0.94	1.30	0.949	No
706	46.36	2.82	1.20	1.62	0.82	0.709	1.05	0.673	0.94	1.30	0.949	No
707	46.42	2.83	1.20	1.63	0.82	0.709	1.05	0.672	0.94	1.30	0.949	No
708	46.46	2.83	1.20	1.63	0.82	0.709	1.05	0.672	0.94	1.30	0.949	No
709	46.52	2.83	1.20	1.63	0.81	0.709	1.05	0.672	0.95	1.30	0.949	No
710	46.61	2.84	1.20	1.63	0.81	0.709	1.05	0.672	0.95	1.30	0.949	No
711	46.66	2.84	1.21	1.63	0.81	0.708	1.05	0.672	0.95	1.30	0.949	No
712	46.74	2.85	1.21	1.64	0.81	0.708	1.05	0.672	0.95	1.30	0.949	No
713	46.79	2.85	1.21	1.64	0.81	0.708	1.05	0.672	0.95	1.30	0.949	No
714	46.86	2.85	1.21	1.64	0.81	0.708	1.05	0.671	0.95	1.30	0.949	No
715	46.94	2.86	1.21	1.64	0.81	0.708	1.05	0.671	0.95	1.30	0.949	No
716	46.99	2.86	1.22	1.64	0.81	0.708	1.05	0.671	0.95	1.30	0.948	No
717	47.06	2.87	1.22	1.65	0.81	0.707	1.05	0.671	0.95	1.30	0.948	No
718	47.14	2.87	1.22	1.65	0.81	0.707	1.05	0.671	0.96	1.30	0.947	No
719	47.19	2.87	1.22	1.65	0.81	0.707	1.05	0.671	0.96	1.30	0.947	No
720	47.25	2.88	1.22	1.65	0.81	0.707	1.05	0.671	0.96	1.30	0.947	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
721	47.34	2.88	1.23	1.65	0.81	0.707	1.05	0.670	0.96	1.30	0.946	No
722	47.39	2.89	1.23	1.66	0.81	0.707	1.05	0.670	0.96	1.30	0.946	No
723	47.45	2.89	1.23	1.66	0.81	0.707	1.05	0.670	0.96	1.30	0.946	No
724	47.51	2.89	1.23	1.66	0.81	0.707	1.05	0.670	0.96	1.30	0.947	No
725	47.58	2.90	1.23	1.66	0.81	0.706	1.05	0.670	0.95	1.30	0.948	No
726	47.65	2.90	1.24	1.66	0.81	0.706	1.05	0.670	0.95	1.30	0.948	No
727	47.72	2.91	1.24	1.67	0.81	0.706	1.05	0.670	0.95	1.30	0.948	No
728	47.78	2.91	1.24	1.67	0.81	0.706	1.05	0.669	0.95	1.30	0.948	No
729	47.85	2.91	1.24	1.67	0.81	0.706	1.05	0.669	0.95	1.30	0.948	No
730	47.91	2.92	1.25	1.67	0.81	0.706	1.05	0.669	0.95	1.30	0.947	No
731	47.98	2.92	1.25	1.67	0.81	0.705	1.05	0.669	0.95	1.30	0.947	No
732	48.05	2.93	1.25	1.68	0.81	0.705	1.05	0.669	0.96	1.30	0.946	No
733	48.11	2.93	1.25	1.68	0.81	0.705	1.05	0.669	0.96	1.30	0.946	No
734	48.18	2.93	1.25	1.68	0.81	0.705	1.05	0.669	0.96	1.30	0.945	No
735	48.24	2.94	1.26	1.68	0.81	0.705	1.05	0.668	0.96	1.30	0.945	No
736	48.31	2.94	1.26	1.68	0.81	0.705	1.05	0.668	0.96	1.30	0.945	No
737	48.38	2.95	1.26	1.69	0.81	0.705	1.05	0.668	0.96	1.30	0.945	No
738	48.45	2.95	1.26	1.69	0.81	0.704	1.05	0.668	0.96	1.30	0.945	No
739	48.52	2.95	1.26	1.69	0.81	0.704	1.05	0.668	0.96	1.30	0.945	No
740	48.58	2.96	1.27	1.69	0.80	0.704	1.05	0.668	0.95	1.30	0.946	No
741	48.65	2.96	1.27	1.69	0.80	0.704	1.05	0.668	0.94	1.30	0.947	No
742	48.72	2.97	1.27	1.70	0.80	0.704	1.05	0.667	0.93	1.30	0.947	No
743	48.78	2.97	1.27	1.70	0.80	0.704	1.05	0.667	0.93	1.30	0.947	No
744	48.85	2.98	1.27	1.70	0.80	0.703	1.05	0.667	0.92	1.30	0.946	No
745	48.92	2.98	1.28	1.70	0.80	0.703	1.05	0.667	0.92	1.30	0.946	No
746	48.95	2.98	1.28	1.70	0.80	0.703	1.05	0.667	0.91	1.30	0.946	No
747	49.02	2.99	1.28	1.71	0.80	0.703	1.05	0.667	0.91	1.30	0.946	No
748	49.09	2.99	1.28	1.71	0.80	0.703	1.05	0.666	0.91	1.30	0.946	No
749	49.16	3.00	1.28	1.71	0.80	0.702	1.05	0.666	0.91	1.30	0.946	No
750	49.23	3.00	1.29	1.71	0.80	0.702	1.05	0.666	0.90	1.30	0.946	No
751	49.29	3.00	1.29	1.72	0.80	0.702	1.05	0.666	0.90	1.30	0.947	No
752	49.35	3.01	1.29	1.72	0.80	0.702	1.05	0.666	0.90	1.30	0.947	No
753	49.42	3.01	1.29	1.72	0.80	0.702	1.05	0.665	0.89	1.30	0.948	No
754	49.49	3.02	1.29	1.72	0.80	0.701	1.05	0.665	0.88	1.30	0.956	No
755	49.56	3.02	1.30	1.73	0.80	0.701	1.05	0.665	0.88	1.30	0.961	No
756	49.62	3.03	1.30	1.73	0.80	0.701	1.05	0.665	0.88	1.30	0.961	No
757	49.69	3.03	1.30	1.73	0.80	0.701	1.05	0.665	0.88	1.30	0.959	No
758	49.76	3.03	1.30	1.73	0.80	0.701	1.05	0.665	0.88	1.30	0.961	No
759	49.82	3.04	1.30	1.73	0.80	0.700	1.05	0.664	0.88	1.30	0.962	No
760	49.89	3.04	1.31	1.74	0.80	0.700	1.05	0.664	0.87	1.30	0.964	No
761	49.95	3.05	1.31	1.74	0.80	0.700	1.05	0.664	0.87	1.30	0.966	No
762	50.00	3.05	1.31	1.74	0.80	0.700	1.05	0.664	0.87	1.30	2.000	No
763	50.07	3.06	1.31	1.74	0.80	0.700	1.05	0.664	0.87	1.30	2.000	No
764	50.14	3.06	1.31	1.75	0.80	0.699	1.05	0.663	0.87	1.30	2.000	No
765	50.20	3.06	1.32	1.75	0.80	0.699	1.05	0.663	0.87	1.30	2.000	No
766	50.28	3.07	1.32	1.75	0.80	0.699	1.05	0.663	0.87	1.30	2.000	No
767	50.35	3.07	1.32	1.75	0.80	0.699	1.05	0.663	0.88	1.30	2.000	No
768	50.41	3.08	1.32	1.75	0.80	0.699	1.05	0.663	0.88	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
769	50.48	3.08	1.33	1.76	0.80	0.698	1.05	0.662	0.88	1.30	2.000	No
770	50.55	3.09	1.33	1.76	0.80	0.698	1.05	0.662	0.88	1.30	2.000	No
771	50.61	3.09	1.33	1.76	0.79	0.698	1.05	0.662	0.88	1.30	2.000	No
772	50.68	3.09	1.33	1.76	0.79	0.698	1.05	0.662	0.88	1.30	2.000	No
773	50.74	3.10	1.33	1.77	0.79	0.698	1.05	0.662	0.88	1.30	2.000	No
774	50.81	3.10	1.34	1.77	0.79	0.697	1.05	0.661	0.89	1.30	2.000	No
775	50.88	3.11	1.34	1.77	0.79	0.697	1.05	0.661	0.89	1.30	2.000	No
776	50.94	3.11	1.34	1.77	0.79	0.697	1.05	0.661	0.89	1.30	2.000	No
777	51.01	3.12	1.34	1.77	0.79	0.697	1.05	0.661	0.90	1.30	2.000	No
778	51.08	3.12	1.34	1.78	0.79	0.697	1.05	0.661	0.90	1.30	2.000	No
779	51.15	3.13	1.35	1.78	0.79	0.696	1.05	0.661	0.91	1.30	2.000	No
780	51.21	3.13	1.35	1.78	0.79	0.696	1.05	0.660	0.91	1.30	2.000	No
781	51.28	3.13	1.35	1.78	0.79	0.696	1.05	0.660	0.91	1.30	2.000	No
782	51.34	3.14	1.35	1.79	0.79	0.696	1.05	0.660	0.92	1.30	2.000	No
783	51.38	3.14	1.35	1.79	0.79	0.696	1.05	0.660	0.92	1.30	2.000	No
784	51.45	3.14	1.36	1.79	0.79	0.696	1.05	0.660	0.92	1.30	2.000	No
785	51.51	3.15	1.36	1.79	0.79	0.695	1.05	0.660	0.92	1.30	2.000	No
786	51.58	3.15	1.36	1.79	0.79	0.695	1.05	0.659	0.92	1.30	2.000	No
787	51.65	3.16	1.36	1.80	0.79	0.695	1.05	0.659	0.92	1.30	2.000	No
788	51.71	3.16	1.36	1.80	0.79	0.695	1.05	0.659	0.92	1.30	2.000	No
789	51.78	3.17	1.37	1.80	0.79	0.695	1.05	0.659	0.92	1.30	2.000	No
790	51.85	3.17	1.37	1.80	0.79	0.694	1.05	0.659	0.92	1.30	2.000	No
791	51.92	3.17	1.37	1.80	0.79	0.694	1.05	0.658	0.92	1.30	2.000	No
792	51.99	3.18	1.37	1.81	0.79	0.694	1.05	0.658	0.92	1.30	2.000	No
793	52.05	3.18	1.37	1.81	0.79	0.694	1.05	0.658	0.92	1.30	2.000	No
794	52.11	3.19	1.38	1.81	0.79	0.694	1.05	0.658	0.92	1.30	2.000	No
795	52.18	3.19	1.38	1.81	0.79	0.694	1.05	0.658	0.92	1.30	2.000	No
796	52.24	3.19	1.38	1.81	0.79	0.693	1.05	0.658	0.92	1.30	2.000	No
797	52.31	3.20	1.38	1.82	0.79	0.693	1.05	0.657	0.92	1.30	2.000	No
798	52.38	3.20	1.38	1.82	0.79	0.693	1.05	0.657	0.93	1.30	2.000	No
799	52.44	3.21	1.39	1.82	0.79	0.693	1.05	0.657	0.93	1.30	2.000	No
800	52.51	3.21	1.39	1.82	0.79	0.693	1.05	0.657	0.93	1.30	2.000	No
801	52.58	3.22	1.39	1.83	0.79	0.692	1.05	0.657	0.93	1.30	2.000	No
802	52.64	3.22	1.39	1.83	0.78	0.692	1.05	0.657	0.93	1.30	2.000	No
803	52.71	3.22	1.39	1.83	0.78	0.692	1.05	0.656	0.93	1.30	2.000	No
804	52.78	3.23	1.40	1.83	0.78	0.692	1.05	0.656	0.93	1.30	2.000	No
805	52.84	3.23	1.40	1.83	0.78	0.692	1.05	0.656	0.93	1.30	2.000	No
806	52.91	3.24	1.40	1.84	0.78	0.691	1.05	0.656	0.93	1.30	2.000	No
807	52.98	3.24	1.40	1.84	0.78	0.691	1.05	0.656	0.93	1.30	2.000	No
808	53.04	3.25	1.41	1.84	0.78	0.691	1.05	0.655	0.93	1.30	2.000	No
809	53.11	3.25	1.41	1.84	0.78	0.691	1.05	0.655	0.93	1.30	2.000	No
810	53.17	3.25	1.41	1.84	0.78	0.691	1.05	0.655	0.92	1.30	2.000	No
811	53.24	3.26	1.41	1.85	0.78	0.691	1.05	0.655	0.92	1.30	2.000	No
812	53.31	3.26	1.41	1.85	0.78	0.690	1.05	0.655	0.92	1.30	2.000	No
813	53.38	3.27	1.42	1.85	0.78	0.690	1.05	0.655	0.91	1.30	2.000	No
814	53.42	3.27	1.42	1.85	0.78	0.690	1.05	0.654	0.91	1.30	2.000	No
815	53.49	3.27	1.42	1.85	0.78	0.690	1.05	0.654	0.90	1.30	2.000	No
816	53.56	3.28	1.42	1.86	0.78	0.690	1.05	0.654	0.90	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
817	53.63	3.28	1.42	1.86	0.78	0.689	1.05	0.654	0.90	1.30	2.000	No
818	53.68	3.29	1.43	1.86	0.78	0.689	1.05	0.654	0.89	1.30	2.000	No
819	53.75	3.29	1.43	1.86	0.78	0.689	1.05	0.653	0.89	1.30	2.000	No
820	53.82	3.29	1.43	1.87	0.78	0.689	1.05	0.653	0.88	1.30	2.000	No
821	53.89	3.30	1.43	1.87	0.78	0.689	1.05	0.653	0.88	1.30	2.000	No
822	53.94	3.30	1.43	1.87	0.78	0.688	1.05	0.653	0.88	1.30	2.000	No
823	54.00	3.31	1.44	1.87	0.78	0.688	1.05	0.653	0.90	1.30	2.000	No
824	54.07	3.31	1.44	1.87	0.78	0.688	1.05	0.653	0.90	1.30	2.000	No
825	54.15	3.32	1.44	1.88	0.78	0.688	1.05	0.652	0.90	1.30	2.000	No
826	54.21	3.32	1.44	1.88	0.78	0.688	1.05	0.652	0.89	1.30	2.000	No
827	54.27	3.32	1.44	1.88	0.78	0.687	1.05	0.652	0.88	1.30	2.000	No
828	54.34	3.33	1.45	1.88	0.78	0.687	1.05	0.652	0.88	1.30	2.000	No
829	54.40	3.33	1.45	1.88	0.78	0.687	1.05	0.652	0.87	1.30	2.000	No
830	54.47	3.34	1.45	1.89	0.78	0.687	1.05	0.651	0.87	1.30	2.000	No
831	54.53	3.34	1.45	1.89	0.78	0.687	1.05	0.651	0.86	1.30	2.000	No
832	54.60	3.35	1.45	1.89	0.78	0.686	1.05	0.651	0.85	1.30	2.000	No
833	54.67	3.35	1.46	1.89	0.78	0.686	1.05	0.651	0.85	1.30	2.000	No
834	54.73	3.35	1.46	1.90	0.77	0.686	1.05	0.651	0.84	1.30	2.000	No
835	54.80	3.36	1.46	1.90	0.77	0.686	1.05	0.650	0.84	1.30	2.000	No
836	54.87	3.36	1.46	1.90	0.77	0.685	1.05	0.650	0.83	1.30	2.000	No
837	54.93	3.37	1.46	1.90	0.77	0.685	1.05	0.650	0.83	1.30	2.000	No
838	54.99	3.37	1.47	1.90	0.77	0.685	1.05	0.650	0.82	1.30	2.000	No
839	55.05	3.38	1.47	1.91	0.77	0.685	1.05	0.650	0.82	1.30	2.000	No
840	55.12	3.38	1.47	1.91	0.77	0.685	1.05	0.649	0.82	1.30	2.000	No
841	55.19	3.38	1.47	1.91	0.77	0.684	1.05	0.649	0.82	1.30	2.000	No
842	55.26	3.39	1.47	1.91	0.77	0.684	1.05	0.649	0.82	1.30	2.000	No
843	55.33	3.39	1.48	1.92	0.77	0.684	1.05	0.649	0.82	1.30	2.000	No
844	55.39	3.40	1.48	1.92	0.77	0.684	1.05	0.648	0.82	1.30	2.000	No
845	55.45	3.40	1.48	1.92	0.77	0.684	1.05	0.648	0.82	1.30	2.000	No
846	55.52	3.41	1.48	1.92	0.77	0.683	1.05	0.648	0.82	1.30	2.000	No
847	55.59	3.41	1.48	1.93	0.77	0.683	1.05	0.648	0.82	1.30	2.000	No
848	55.64	3.41	1.49	1.93	0.77	0.683	1.05	0.648	0.82	1.30	2.000	No
849	55.72	3.42	1.49	1.93	0.77	0.683	1.05	0.647	0.82	1.30	2.000	No
850	55.79	3.42	1.49	1.93	0.77	0.682	1.05	0.647	0.82	1.30	2.000	No
851	55.86	3.43	1.49	1.94	0.77	0.682	1.05	0.647	0.82	1.30	2.000	No
852	55.92	3.43	1.50	1.94	0.77	0.682	1.05	0.647	0.82	1.30	2.000	No
853	55.98	3.44	1.50	1.94	0.77	0.682	1.05	0.647	0.84	1.30	2.000	No
854	56.05	3.44	1.50	1.94	0.77	0.681	1.05	0.646	0.83	1.30	2.000	No
855	56.11	3.44	1.50	1.94	0.77	0.681	1.05	0.646	0.83	1.30	2.000	No
856	56.18	3.45	1.50	1.95	0.77	0.681	1.05	0.646	0.83	1.30	2.000	No
857	56.24	3.45	1.50	1.95	0.77	0.681	1.05	0.646	0.83	1.30	2.000	No
858	56.31	3.46	1.51	1.95	0.77	0.681	1.05	0.646	0.84	1.30	2.000	No
859	56.37	3.46	1.51	1.95	0.77	0.680	1.05	0.645	0.84	1.30	2.000	No
860	56.45	3.47	1.51	1.96	0.77	0.680	1.05	0.645	0.84	1.30	2.000	No
861	56.51	3.47	1.51	1.96	0.77	0.680	1.05	0.645	0.84	1.30	2.000	No
862	56.58	3.48	1.52	1.96	0.77	0.680	1.05	0.645	0.84	1.30	2.000	No
863	56.64	3.48	1.52	1.96	0.77	0.680	1.05	0.644	0.84	1.30	2.000	No
864	56.71	3.48	1.52	1.96	0.77	0.679	1.05	0.644	0.84	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
865	56.78	3.49	1.52	1.97	0.76	0.679	1.05	0.644	0.84	1.30	2.000	No
866	56.84	3.49	1.52	1.97	0.76	0.679	1.05	0.644	0.84	1.30	2.000	No
867	56.91	3.50	1.53	1.97	0.76	0.679	1.05	0.644	0.84	1.30	2.000	No
868	56.98	3.50	1.53	1.97	0.76	0.678	1.05	0.643	0.84	1.30	2.000	No
869	57.05	3.51	1.53	1.98	0.76	0.678	1.05	0.643	0.83	1.30	2.000	No
870	57.11	3.51	1.53	1.98	0.76	0.678	1.05	0.643	0.83	1.30	2.000	No
871	57.18	3.51	1.53	1.98	0.76	0.678	1.05	0.643	0.88	1.30	2.000	No
872	57.24	3.52	1.54	1.98	0.76	0.678	1.05	0.643	0.90	1.30	2.000	No
873	57.31	3.52	1.54	1.98	0.76	0.677	1.05	0.642	0.90	1.30	2.000	No
874	57.38	3.53	1.54	1.99	0.76	0.677	1.05	0.642	0.89	1.30	2.000	No
875	57.45	3.53	1.54	1.99	0.76	0.677	1.05	0.642	0.88	1.30	2.000	No
876	57.48	3.53	1.54	1.99	0.76	0.677	1.05	0.642	0.88	1.30	2.000	No
877	57.56	3.54	1.55	1.99	0.76	0.677	1.05	0.642	0.88	1.30	2.000	No
878	57.62	3.54	1.55	2.00	0.76	0.676	1.05	0.641	0.87	1.30	2.000	No
879	57.71	3.55	1.55	2.00	0.76	0.676	1.05	0.641	0.87	1.30	2.000	No
880	57.77	3.55	1.55	2.00	0.76	0.676	1.05	0.641	0.86	1.30	2.000	No
881	57.84	3.56	1.55	2.00	0.76	0.676	1.05	0.641	0.86	1.30	2.000	No
882	57.91	3.56	1.56	2.00	0.76	0.675	1.05	0.641	0.86	1.30	2.000	No
883	57.97	3.57	1.56	2.01	0.76	0.675	1.05	0.640	0.85	1.30	2.000	No
884	58.01	3.57	1.56	2.01	0.76	0.675	1.05	0.640	0.85	1.30	2.000	No
885	58.08	3.57	1.56	2.01	0.76	0.675	1.05	0.640	0.85	1.30	2.000	No
886	58.14	3.58	1.56	2.01	0.76	0.675	1.05	0.640	0.85	1.30	2.000	No
887	58.21	3.58	1.57	2.01	0.76	0.674	1.05	0.640	0.85	1.30	2.000	No
888	58.28	3.59	1.57	2.02	0.76	0.674	1.05	0.639	0.85	1.30	2.000	No
889	58.34	3.59	1.57	2.02	0.76	0.674	1.05	0.639	0.86	1.30	2.000	No
890	58.41	3.59	1.57	2.02	0.76	0.674	1.05	0.639	0.86	1.30	2.000	No
891	58.48	3.60	1.57	2.02	0.76	0.674	1.05	0.639	0.86	1.30	2.000	No
892	58.54	3.60	1.58	2.03	0.76	0.673	1.05	0.639	0.87	1.30	2.000	No
893	58.61	3.61	1.58	2.03	0.76	0.673	1.05	0.638	0.87	1.30	2.000	No
894	58.67	3.61	1.58	2.03	0.76	0.673	1.05	0.638	0.89	1.30	2.000	No
895	58.74	3.62	1.58	2.03	0.76	0.673	1.05	0.638	0.90	1.30	2.000	No
896	58.80	3.62	1.59	2.03	0.76	0.673	1.05	0.638	0.90	1.30	2.000	No
897	58.87	3.62	1.59	2.04	0.75	0.672	1.05	0.638	0.89	1.30	2.000	No
898	58.94	3.63	1.59	2.04	0.75	0.672	1.05	0.637	0.89	1.30	2.000	No
899	59.01	3.63	1.59	2.04	0.75	0.672	1.05	0.637	0.88	1.30	2.000	No
900	59.07	3.64	1.59	2.04	0.75	0.672	1.05	0.637	0.88	1.30	2.000	No
901	59.13	3.64	1.60	2.05	0.75	0.672	1.05	0.637	0.87	1.30	2.000	No
902	59.22	3.65	1.60	2.05	0.75	0.671	1.05	0.637	0.86	1.30	2.000	No
903	59.28	3.65	1.60	2.05	0.75	0.671	1.05	0.636	0.85	1.30	2.000	No
904	59.32	3.65	1.60	2.05	0.75	0.671	1.05	0.636	0.85	1.30	2.000	No
905	59.38	3.66	1.60	2.05	0.75	0.671	1.05	0.636	0.84	1.30	2.000	No
906	59.45	3.66	1.61	2.06	0.75	0.670	1.05	0.636	0.83	1.30	2.000	No
907	59.52	3.67	1.61	2.06	0.75	0.670	1.05	0.636	0.82	1.30	2.000	No
908	59.59	3.67	1.61	2.06	0.75	0.670	1.05	0.635	0.82	1.30	2.000	No
909	59.65	3.67	1.61	2.06	0.75	0.670	1.05	0.635	0.84	1.30	2.000	No
910	59.72	3.68	1.61	2.07	0.75	0.670	1.05	0.635	0.84	1.30	2.000	No
911	59.79	3.68	1.62	2.07	0.75	0.669	1.05	0.635	0.84	1.30	2.000	No
912	59.85	3.69	1.62	2.07	0.75	0.669	1.05	0.635	0.84	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
913	59.92	3.69	1.62	2.07	0.75	0.669	1.05	0.634	0.84	1.30	2.000	No
914	59.98	3.70	1.62	2.07	0.75	0.669	1.05	0.634	0.85	1.30	2.000	No
915	60.04	3.70	1.62	2.08	0.75	0.668	1.05	0.634	0.85	1.30	2.000	No
916	60.11	3.70	1.63	2.08	0.75	0.668	1.05	0.634	0.86	1.30	2.000	No
917	60.19	3.71	1.63	2.08	0.75	0.668	1.05	0.634	0.86	1.30	2.000	No
918	60.25	3.71	1.63	2.08	0.75	0.668	1.05	0.633	0.86	1.30	2.000	No
919	60.32	3.72	1.63	2.09	0.75	0.668	1.05	0.633	0.86	1.30	2.000	No
920	60.38	3.72	1.63	2.09	0.75	0.667	1.05	0.633	0.86	1.30	2.000	No
921	60.46	3.73	1.64	2.09	0.75	0.667	1.05	0.633	0.85	1.30	2.000	No
922	60.51	3.73	1.64	2.09	0.75	0.667	1.05	0.633	0.86	1.30	2.000	No
923	60.57	3.73	1.64	2.09	0.75	0.667	1.05	0.632	0.86	1.30	2.000	No
924	60.65	3.74	1.64	2.10	0.75	0.667	1.05	0.632	0.86	1.30	2.000	No
925	60.70	3.74	1.64	2.10	0.75	0.666	1.05	0.632	0.86	1.30	2.000	No
926	60.77	3.75	1.65	2.10	0.75	0.666	1.05	0.632	0.86	1.30	2.000	No
927	60.83	3.75	1.65	2.10	0.75	0.666	1.05	0.632	0.86	1.30	2.000	No
928	60.92	3.76	1.65	2.11	0.75	0.666	1.05	0.631	0.87	1.30	2.000	No
929	60.99	3.76	1.65	2.11	0.75	0.665	1.05	0.631	0.87	1.30	2.000	No
930	61.05	3.77	1.66	2.11	0.74	0.665	1.05	0.631	0.87	1.30	2.000	No
931	61.12	3.77	1.66	2.11	0.74	0.665	1.05	0.631	0.87	1.30	2.000	No
932	61.19	3.77	1.66	2.11	0.74	0.665	1.05	0.630	0.87	1.30	2.000	No
933	61.22	3.78	1.66	2.12	0.74	0.665	1.05	0.630	0.87	1.30	2.000	No
934	61.29	3.78	1.66	2.12	0.74	0.664	1.05	0.630	0.87	1.30	2.000	No
935	61.35	3.79	1.66	2.12	0.74	0.664	1.05	0.630	0.87	1.30	2.000	No
936	61.42	3.79	1.67	2.12	0.74	0.664	1.05	0.630	0.87	1.30	2.000	No
937	61.50	3.79	1.67	2.13	0.74	0.664	1.05	0.630	0.87	1.30	2.000	No
938	61.55	3.80	1.67	2.13	0.74	0.664	1.05	0.629	0.87	1.30	2.000	No
939	61.62	3.80	1.67	2.13	0.74	0.663	1.05	0.629	0.86	1.30	2.000	No
940	61.69	3.81	1.68	2.13	0.74	0.663	1.05	0.629	0.86	1.30	2.000	No
941	61.75	3.81	1.68	2.13	0.74	0.663	1.05	0.629	0.85	1.30	2.000	No
942	61.81	3.81	1.68	2.14	0.74	0.663	1.05	0.629	0.84	1.30	2.000	No
943	61.89	3.82	1.68	2.14	0.74	0.663	1.05	0.628	0.84	1.30	2.000	No
944	61.94	3.82	1.68	2.14	0.74	0.662	1.05	0.628	0.83	1.30	2.000	No
945	62.03	3.83	1.69	2.14	0.74	0.662	1.05	0.628	0.82	1.30	2.000	No
946	62.09	3.83	1.69	2.15	0.74	0.662	1.05	0.628	0.80	1.30	2.000	No
947	62.15	3.84	1.69	2.15	0.74	0.662	1.05	0.627	0.79	1.30	2.000	No
948	62.21	3.84	1.69	2.15	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
949	62.27	3.84	1.69	2.15	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
950	62.34	3.85	1.70	2.15	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
951	62.42	3.85	1.70	2.16	0.74	0.661	1.05	0.627	0.79	1.30	2.000	No
952	62.49	3.86	1.70	2.16	0.74	0.660	1.05	0.626	0.79	1.30	2.000	No
953	62.54	3.86	1.70	2.16	0.74	0.660	1.05	0.626	0.79	1.30	2.000	No
954	62.60	3.87	1.70	2.16	0.74	0.660	1.05	0.626	0.79	1.30	2.000	No
955	62.67	3.87	1.71	2.17	0.74	0.660	1.05	0.626	0.79	1.30	2.000	No
956	62.74	3.88	1.71	2.17	0.74	0.660	1.05	0.626	0.80	1.30	2.000	No
957	62.80	3.88	1.71	2.17	0.74	0.659	1.05	0.625	0.82	1.30	2.000	No
958	62.87	3.88	1.71	2.17	0.74	0.659	1.05	0.625	0.82	1.30	2.000	No
959	62.95	3.89	1.71	2.17	0.74	0.659	1.05	0.625	0.85	1.30	2.000	No
960	63.01	3.89	1.72	2.18	0.74	0.659	1.05	0.625	0.87	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
961	63.08	3.90	1.72	2.18	0.74	0.659	1.05	0.625	0.87	1.30	2.000	No
962	63.14	3.90	1.72	2.18	0.74	0.658	1.05	0.624	0.88	1.30	2.000	No
963	63.21	3.91	1.72	2.18	0.74	0.658	1.05	0.624	0.89	1.30	2.000	No
964	63.28	3.91	1.72	2.19	0.73	0.658	1.05	0.624	0.89	1.30	2.000	No
965	63.33	3.91	1.73	2.19	0.73	0.658	1.05	0.624	0.89	1.30	2.000	No
966	63.39	3.92	1.73	2.19	0.73	0.658	1.05	0.624	0.89	1.30	2.000	No
967	63.46	3.92	1.73	2.19	0.73	0.657	1.05	0.623	0.88	1.30	2.000	No
968	63.53	3.93	1.73	2.19	0.73	0.657	1.05	0.623	0.89	1.30	2.000	No
969	63.59	3.93	1.73	2.20	0.73	0.657	1.05	0.623	0.89	1.30	2.000	No
970	63.66	3.94	1.74	2.20	0.73	0.657	1.05	0.623	0.89	1.30	2.000	No
971	63.72	3.94	1.74	2.20	0.73	0.656	1.05	0.622	0.89	1.30	2.000	No
972	63.79	3.94	1.74	2.20	0.73	0.656	1.05	0.622	0.88	1.30	2.000	No
973	63.85	3.95	1.74	2.21	0.73	0.656	1.05	0.622	0.87	1.30	2.000	No
974	63.92	3.95	1.74	2.21	0.73	0.656	1.05	0.622	0.85	1.30	2.000	No
975	63.99	3.96	1.75	2.21	0.73	0.655	1.05	0.622	0.83	1.30	2.000	No
976	64.05	3.96	1.75	2.21	0.73	0.655	1.05	0.621	0.81	1.30	2.000	No
977	64.11	3.97	1.75	2.21	0.73	0.655	1.05	0.621	0.80	1.30	2.000	No
978	64.19	3.97	1.75	2.22	0.73	0.655	1.05	0.621	0.81	1.30	2.000	No
979	64.26	3.97	1.76	2.22	0.73	0.655	1.05	0.621	0.84	1.30	2.000	No
980	64.33	3.98	1.76	2.22	0.73	0.654	1.05	0.621	0.88	1.30	2.000	No
981	64.39	3.98	1.76	2.22	0.73	0.654	1.05	0.620	0.87	1.30	2.000	No
982	64.46	3.99	1.76	2.23	0.73	0.654	1.05	0.620	0.85	1.30	2.000	No
983	64.53	3.99	1.76	2.23	0.73	0.654	1.05	0.620	0.84	1.30	2.000	No
984	64.60	4.00	1.77	2.23	0.73	0.654	1.05	0.620	0.83	1.30	2.000	No
985	64.66	4.00	1.77	2.23	0.73	0.653	1.05	0.620	0.84	1.30	2.000	No
986	64.70	4.00	1.77	2.23	0.73	0.653	1.05	0.620	0.84	1.30	2.000	No
987	64.78	4.01	1.77	2.24	0.73	0.653	1.05	0.619	0.84	1.30	2.000	No
988	64.85	4.01	1.77	2.24	0.73	0.653	1.05	0.619	0.83	1.30	2.000	No
989	64.91	4.02	1.78	2.24	0.73	0.653	1.05	0.619	0.82	1.30	2.000	No
990	64.97	4.02	1.78	2.24	0.73	0.652	1.05	0.619	0.78	1.30	2.000	No
991	65.04	4.02	1.78	2.24	0.73	0.652	1.05	0.618	0.77	1.30	2.000	No
992	65.11	4.03	1.78	2.25	0.73	0.652	1.05	0.618	0.77	1.30	2.000	No
993	65.16	4.03	1.78	2.25	0.73	0.652	1.05	0.618	0.77	1.30	2.000	No
994	65.22	4.04	1.79	2.25	0.73	0.652	1.05	0.618	0.77	1.30	2.000	No
995	65.29	4.04	1.79	2.25	0.73	0.651	1.05	0.618	0.77	1.30	2.000	No
996	65.36	4.05	1.79	2.26	0.73	0.651	1.05	0.618	0.77	1.30	2.000	No
997	65.42	4.05	1.79	2.26	0.73	0.651	1.05	0.617	0.77	1.30	2.000	No
998	65.49	4.05	1.79	2.26	0.72	0.651	1.05	0.617	0.77	1.30	2.000	No
999	65.57	4.06	1.80	2.26	0.72	0.651	1.05	0.617	0.77	1.30	2.000	No
1000	65.63	4.06	1.80	2.26	0.72	0.650	1.05	0.617	0.77	1.30	2.000	No
1001	65.71	4.07	1.80	2.27	0.72	0.650	1.05	0.617	0.77	1.30	2.000	No
1002	65.76	4.07	1.80	2.27	0.72	0.650	1.05	0.616	0.77	1.30	2.000	No
1003	65.82	4.07	1.80	2.27	0.72	0.650	1.05	0.616	0.85	1.30	2.000	No
1004	65.89	4.08	1.81	2.27	0.72	0.650	1.05	0.616	0.77	1.30	2.000	No
1005	65.95	4.08	1.81	2.27	0.72	0.649	1.05	0.616	0.79	1.30	2.000	No
1006	66.02	4.09	1.81	2.28	0.72	0.649	1.05	0.616	0.81	1.30	2.000	No
1007	66.09	4.09	1.81	2.28	0.72	0.649	1.05	0.616	0.82	1.30	2.000	No
1008	66.14	4.09	1.81	2.28	0.72	0.649	1.05	0.615	0.82	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1009	66.21	4.10	1.82	2.28	0.72	0.649	1.05	0.615	0.84	1.30	2.000	No
1010	66.28	4.10	1.82	2.28	0.72	0.648	1.05	0.615	0.84	1.30	2.000	No
1011	66.35	4.11	1.82	2.29	0.72	0.648	1.05	0.615	0.83	1.30	2.000	No
1012	66.41	4.11	1.82	2.29	0.72	0.648	1.05	0.615	0.83	1.30	2.000	No
1013	66.48	4.12	1.82	2.29	0.72	0.648	1.05	0.614	0.82	1.30	2.000	No
1014	66.55	4.12	1.83	2.29	0.72	0.648	1.05	0.614	0.82	1.30	2.000	No
1015	66.61	4.12	1.83	2.29	0.72	0.647	1.05	0.614	0.82	1.30	2.000	No
1016	66.68	4.13	1.83	2.30	0.72	0.647	1.05	0.614	0.83	1.30	2.000	No
1017	66.75	4.13	1.83	2.30	0.72	0.647	1.05	0.614	0.83	1.30	2.000	No
1018	66.81	4.14	1.83	2.30	0.72	0.647	1.05	0.613	0.84	1.30	2.000	No
1019	66.87	4.14	1.84	2.30	0.72	0.647	1.05	0.613	0.86	1.30	2.000	No
1020	66.93	4.14	1.84	2.30	0.72	0.647	1.05	0.613	0.87	1.30	2.000	No
1021	67.00	4.15	1.84	2.31	0.72	0.646	1.05	0.613	0.87	1.30	2.000	No
1022	67.06	4.15	1.84	2.31	0.72	0.646	1.05	0.613	0.88	1.30	2.000	No
1023	67.14	4.16	1.85	2.31	0.72	0.646	1.05	0.613	0.88	1.30	2.000	No
1024	67.21	4.16	1.85	2.31	0.72	0.646	1.05	0.612	0.89	1.30	2.000	No
1025	67.27	4.16	1.85	2.31	0.72	0.646	1.05	0.612	0.90	1.30	2.000	No
1026	67.34	4.17	1.85	2.32	0.72	0.645	1.05	0.612	0.91	1.30	2.000	No
1027	67.41	4.17	1.85	2.32	0.72	0.645	1.05	0.612	0.91	1.30	2.000	No
1028	67.47	4.18	1.86	2.32	0.72	0.645	1.05	0.612	0.90	1.30	2.000	No
1029	67.54	4.18	1.86	2.32	0.72	0.645	1.05	0.612	0.88	1.30	2.000	No
1030	67.61	4.18	1.86	2.33	0.72	0.645	1.05	0.611	0.88	1.30	2.000	No
1031	67.67	4.19	1.86	2.33	0.72	0.644	1.05	0.611	0.87	1.30	2.000	No
1032	67.74	4.19	1.86	2.33	0.72	0.644	1.05	0.611	0.88	1.30	2.000	No
1033	67.81	4.20	1.87	2.33	0.71	0.644	1.05	0.611	0.89	1.30	2.000	No
1034	67.87	4.20	1.87	2.33	0.71	0.644	1.05	0.611	0.90	1.30	2.000	No
1035	67.94	4.21	1.87	2.34	0.71	0.644	1.05	0.610	0.89	1.30	2.000	No
1036	68.01	4.21	1.87	2.34	0.71	0.643	1.05	0.610	0.89	1.30	2.000	No
1037	68.07	4.21	1.87	2.34	0.71	0.643	1.05	0.610	0.89	1.30	2.000	No
1038	68.12	4.22	1.88	2.34	0.71	0.643	1.05	0.610	0.90	1.30	2.000	No
1039	68.20	4.22	1.88	2.34	0.71	0.643	1.05	0.610	0.90	1.30	2.000	No
1040	68.25	4.22	1.88	2.34	0.71	0.643	1.05	0.610	0.91	1.30	2.000	No
1041	68.31	4.23	1.88	2.35	0.71	0.643	1.05	0.609	0.92	1.30	2.000	No
1042	68.38	4.23	1.88	2.35	0.71	0.642	1.05	0.609	0.92	1.30	2.000	No
1043	68.44	4.24	1.89	2.35	0.71	0.642	1.05	0.609	0.92	1.30	2.000	No
1044	68.51	4.24	1.89	2.35	0.71	0.642	1.05	0.609	0.92	1.30	2.000	No
1045	68.58	4.25	1.89	2.36	0.71	0.642	1.05	0.609	0.92	1.30	2.000	No
1046	68.64	4.25	1.89	2.36	0.71	0.642	1.05	0.608	0.91	1.30	2.000	No
1047	68.71	4.25	1.89	2.36	0.71	0.641	1.05	0.608	0.90	1.30	2.000	No
1048	68.78	4.26	1.90	2.36	0.71	0.641	1.05	0.608	0.89	1.30	2.000	No
1049	68.83	4.26	1.90	2.36	0.71	0.641	1.05	0.608	0.88	1.30	2.000	No
1050	68.91	4.27	1.90	2.37	0.71	0.641	1.05	0.608	0.87	1.30	2.000	No
1051	68.99	4.27	1.90	2.37	0.71	0.641	1.05	0.607	0.86	1.30	2.000	No
1052	69.05	4.28	1.90	2.37	0.71	0.640	1.05	0.607	0.87	1.30	2.000	No
1053	69.11	4.28	1.91	2.37	0.71	0.640	1.05	0.607	0.89	1.30	2.000	No
1054	69.17	4.28	1.91	2.37	0.71	0.640	1.05	0.607	0.88	1.30	2.000	No
1055	69.24	4.29	1.91	2.38	0.71	0.640	1.05	0.607	0.88	1.30	2.000	No
1056	69.31	4.29	1.91	2.38	0.71	0.640	1.05	0.607	0.88	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1057	69.37	4.30	1.91	2.38	0.71	0.639	1.05	0.606	0.88	1.30	2.000	No
1058	69.44	4.30	1.92	2.38	0.71	0.639	1.05	0.606	0.87	1.30	2.000	No
1059	69.51	4.30	1.92	2.39	0.71	0.639	1.05	0.606	0.87	1.30	2.000	No
1060	69.56	4.31	1.92	2.39	0.71	0.639	1.05	0.606	0.87	1.30	2.000	No
1061	69.64	4.31	1.92	2.39	0.71	0.639	1.05	0.606	0.86	1.30	2.000	No
1062	69.69	4.32	1.92	2.39	0.71	0.638	1.05	0.606	0.86	1.30	2.000	No
1063	69.78	4.32	1.93	2.39	0.71	0.638	1.05	0.605	0.85	1.30	2.000	No
1064	69.82	4.32	1.93	2.40	0.71	0.638	1.05	0.605	0.84	1.30	2.000	No
1065	69.89	4.33	1.93	2.40	0.71	0.638	1.05	0.605	0.85	1.30	2.000	No
1066	69.95	4.33	1.93	2.40	0.71	0.638	1.05	0.605	0.86	1.30	2.000	No
1067	70.02	4.34	1.94	2.40	0.71	0.637	1.05	0.605	0.84	1.30	2.000	No
1068	70.08	4.34	1.94	2.40	0.71	0.637	1.05	0.604	0.81	1.30	2.000	No
1069	70.15	4.35	1.94	2.41	0.70	0.637	1.05	0.604	0.80	1.30	2.000	No
1070	70.21	4.35	1.94	2.41	0.70	0.637	1.05	0.604	0.84	1.30	2.000	No
1071	70.30	4.36	1.94	2.41	0.70	0.637	1.05	0.604	0.83	1.30	2.000	No
1072	70.37	4.36	1.95	2.41	0.70	0.636	1.05	0.603	0.84	1.30	2.000	No
1073	70.41	4.36	1.95	2.42	0.70	0.636	1.05	0.603	0.83	1.30	2.000	No
1074	70.49	4.37	1.95	2.42	0.70	0.636	1.05	0.603	0.84	1.30	2.000	No
1075	70.55	4.37	1.95	2.42	0.70	0.636	1.05	0.603	0.82	1.30	2.000	No
1076	70.61	4.37	1.95	2.42	0.70	0.636	1.05	0.603	0.81	1.30	2.000	No
1077	70.67	4.38	1.96	2.42	0.70	0.635	1.05	0.603	0.79	1.30	2.000	No
1078	70.74	4.38	1.96	2.43	0.70	0.635	1.05	0.602	0.79	1.30	2.000	No
1079	70.81	4.39	1.96	2.43	0.70	0.635	1.05	0.602	0.81	1.30	2.000	No
1080	70.88	4.39	1.96	2.43	0.70	0.635	1.05	0.602	0.81	1.30	2.000	No
1081	70.95	4.40	1.96	2.43	0.70	0.635	1.05	0.602	0.83	1.30	2.000	No
1082	71.01	4.40	1.97	2.43	0.70	0.634	1.05	0.602	0.84	1.30	2.000	No
1083	71.08	4.40	1.97	2.44	0.70	0.634	1.05	0.601	0.84	1.30	2.000	No
1084	71.15	4.41	1.97	2.44	0.70	0.634	1.05	0.601	0.84	1.30	2.000	No
1085	71.20	4.41	1.97	2.44	0.70	0.634	1.05	0.601	0.84	1.30	2.000	No
1086	71.27	4.42	1.97	2.44	0.70	0.634	1.05	0.601	0.84	1.30	2.000	No
1087	71.33	4.42	1.98	2.44	0.70	0.633	1.05	0.601	0.85	1.30	2.000	No
1088	71.41	4.43	1.98	2.45	0.70	0.633	1.05	0.601	0.84	1.30	2.000	No
1089	71.47	4.43	1.98	2.45	0.70	0.633	1.05	0.600	0.84	1.30	2.000	No
1090	71.55	4.43	1.98	2.45	0.70	0.633	1.05	0.600	0.84	1.30	2.000	No
1091	71.60	4.44	1.98	2.45	0.70	0.633	1.05	0.600	0.84	1.30	2.000	No
1092	71.66	4.44	1.99	2.46	0.70	0.632	1.05	0.600	0.84	1.30	2.000	No
1093	71.72	4.45	1.99	2.46	0.70	0.632	1.05	0.600	0.84	1.30	2.000	No
1094	71.81	4.45	1.99	2.46	0.70	0.632	1.05	0.599	0.82	1.30	2.000	No
1095	71.87	4.46	1.99	2.46	0.70	0.632	1.05	0.599	0.79	1.30	2.000	No
1096	71.94	4.46	1.99	2.46	0.70	0.632	1.05	0.599	0.77	1.30	2.000	No
1097	72.00	4.46	2.00	2.47	0.70	0.631	1.05	0.599	0.76	1.30	2.000	No
1098	72.07	4.47	2.00	2.47	0.70	0.631	1.05	0.599	0.75	1.30	2.000	No
1099	72.14	4.47	2.00	2.47	0.70	0.631	1.05	0.598	0.75	1.30	2.000	No
1100	72.20	4.48	2.00	2.47	0.70	0.631	1.05	0.598	0.75	1.30	2.000	No
1101	72.27	4.48	2.01	2.48	0.70	0.630	1.05	0.598	0.75	1.30	2.000	No
1102	72.34	4.49	2.01	2.48	0.70	0.630	1.05	0.598	0.76	1.30	2.000	No
1103	72.41	4.49	2.01	2.48	0.70	0.630	1.05	0.598	0.77	1.30	2.000	No
1104	72.47	4.50	2.01	2.48	0.70	0.630	1.05	0.597	0.77	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1105	72.51	4.50	2.01	2.48	0.70	0.630	1.05	0.597	0.76	1.30	2.000	No
1106	72.58	4.50	2.01	2.49	0.69	0.629	1.05	0.597	0.76	1.30	2.000	No
1107	72.64	4.51	2.02	2.49	0.69	0.629	1.05	0.597	0.89	1.30	2.000	No
1108	72.72	4.51	2.02	2.49	0.69	0.629	1.05	0.597	0.76	1.30	2.000	No
1109	72.80	4.52	2.02	2.49	0.69	0.629	1.05	0.596	0.81	1.30	2.000	No
1110	72.86	4.52	2.02	2.50	0.69	0.629	1.05	0.596	0.84	1.30	2.000	No
1111	72.92	4.52	2.03	2.50	0.69	0.628	1.05	0.596	0.84	1.30	2.000	No
1112	72.97	4.53	2.03	2.50	0.69	0.628	1.05	0.596	0.85	1.30	2.000	No
1113	73.06	4.53	2.03	2.50	0.69	0.628	1.05	0.596	0.83	1.30	2.000	No
1114	73.12	4.54	2.03	2.51	0.69	0.628	1.05	0.595	0.83	1.30	2.000	No
1115	73.19	4.54	2.03	2.51	0.69	0.628	1.05	0.595	0.82	1.30	2.000	No
1116	73.25	4.55	2.04	2.51	0.69	0.627	1.05	0.595	0.81	1.30	2.000	No
1117	73.32	4.55	2.04	2.51	0.69	0.627	1.05	0.595	0.81	1.30	2.000	No
1118	73.38	4.55	2.04	2.51	0.69	0.627	1.05	0.595	0.80	1.30	2.000	No
1119	73.45	4.56	2.04	2.52	0.69	0.627	1.05	0.594	0.81	1.30	2.000	No
1120	73.52	4.56	2.04	2.52	0.69	0.627	1.05	0.594	0.81	1.30	2.000	No
1121	73.58	4.57	2.05	2.52	0.69	0.626	1.05	0.594	0.81	1.30	2.000	No
1122	73.65	4.57	2.05	2.52	0.69	0.626	1.05	0.594	0.81	1.30	2.000	No
1123	73.72	4.58	2.05	2.52	0.69	0.626	1.05	0.594	0.82	1.30	2.000	No
1124	73.78	4.58	2.05	2.53	0.69	0.626	1.05	0.594	0.81	1.30	2.000	No
1125	73.85	4.58	2.05	2.53	0.69	0.626	1.05	0.593	0.82	1.30	2.000	No
1126	73.92	4.59	2.06	2.53	0.69	0.625	1.05	0.593	0.82	1.30	2.000	No
1127	73.95	4.59	2.06	2.53	0.69	0.625	1.05	0.593	0.81	1.30	2.000	No
1128	74.02	4.59	2.06	2.53	0.69	0.625	1.05	0.593	0.81	1.30	2.000	No
1129	74.09	4.60	2.06	2.54	0.69	0.625	1.05	0.593	0.81	1.30	2.000	No
1130	74.16	4.60	2.06	2.54	0.69	0.625	1.05	0.592	0.80	1.30	2.000	No
1131	74.22	4.61	2.07	2.54	0.69	0.625	1.05	0.592	0.79	1.30	2.000	No
1132	74.30	4.61	2.07	2.54	0.69	0.624	1.05	0.592	0.79	1.30	2.000	No
1133	74.36	4.62	2.07	2.55	0.69	0.624	1.05	0.592	0.79	1.30	2.000	No
1134	74.43	4.62	2.07	2.55	0.69	0.624	1.05	0.592	0.79	1.30	2.000	No
1135	74.49	4.63	2.07	2.55	0.69	0.624	1.05	0.592	0.79	1.30	2.000	No
1136	74.55	4.63	2.08	2.55	0.69	0.624	1.05	0.591	0.80	1.30	2.000	No
1137	74.61	4.63	2.08	2.55	0.69	0.623	1.05	0.591	0.80	1.30	2.000	No
1138	74.68	4.64	2.08	2.56	0.69	0.623	1.05	0.591	0.81	1.30	2.000	No
1139	74.75	4.64	2.08	2.56	0.69	0.623	1.05	0.591	0.81	1.30	2.000	No
1140	74.81	4.65	2.08	2.56	0.69	0.623	1.05	0.591	0.82	1.30	2.000	No
1141	74.88	4.65	2.09	2.56	0.69	0.623	1.05	0.590	0.82	1.30	2.000	No
1142	74.95	4.65	2.09	2.57	0.69	0.622	1.05	0.590	0.83	1.30	2.000	No
1143	75.01	4.66	2.09	2.57	0.69	0.622	1.05	0.590	0.83	1.30	2.000	No
1144	75.08	4.66	2.09	2.57	0.68	0.622	1.05	0.590	0.83	1.30	2.000	No
1145	75.15	4.67	2.09	2.57	0.68	0.622	1.05	0.590	0.75	1.30	2.000	No
1146	75.21	4.67	2.10	2.57	0.68	0.622	1.05	0.590	0.75	1.30	2.000	No
1147	75.28	4.67	2.10	2.57	0.68	0.622	1.05	0.590	0.74	1.30	2.000	No
1148	75.35	4.67	2.10	2.57	0.68	0.622	1.05	0.590	0.73	1.30	2.000	No
1149	75.41	4.68	2.10	2.57	0.68	0.622	1.05	0.590	0.73	1.30	2.000	No
1150	75.46	4.68	2.10	2.57	0.68	0.622	1.05	0.590	0.73	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR_{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.07	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
2	0.14	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
3	0.21	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
4	0.28	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
5	0.33	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
6	0.41	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
7	0.46	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
8	0.54	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
9	0.60	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
10	0.66	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
11	0.72	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
12	0.80	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
13	0.86	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
14	0.92	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
15	0.99	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
16	1.06	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
17	1.11	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
18	1.18	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
19	1.26	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
20	1.33	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
21	1.39	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
22	1.46	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
23	1.51	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
24	1.59	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
25	1.65	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
26	1.71	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
27	1.79	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
28	1.84	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
29	1.92	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
30	1.97	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
31	2.05	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
32	2.11	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
33	2.18	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
34	2.24	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
35	2.31	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
36	2.37	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
37	2.44	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
38	2.50	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
39	2.58	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
40	2.64	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
41	2.71	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
42	2.76	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
43	2.82	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
44	2.90	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
45	2.97	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
46	3.03	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
47	3.09	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
48	3.15	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	3.22	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
50	3.30	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
51	3.36	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
52	3.42	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
53	3.48	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
54	3.55	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
55	3.61	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
56	3.70	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
57	3.76	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
58	3.82	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
59	3.88	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
60	3.95	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
61	4.01	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
62	4.07	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
63	4.14	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
64	4.20	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
65	4.28	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
66	4.33	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
67	4.42	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
68	4.48	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
69	4.54	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
70	4.60	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
71	4.66	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
72	4.74	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
73	4.80	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
74	4.86	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
75	4.93	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
76	5.00	0.00	100.00	4.06	0.78	1.70	-16064.81	0.00	-16064.81	4.000	No	Yes	2.00
77	5.07	109.34	3.60	1.76	0.38	1.60	164.99	0.01	164.99	4.000	No	No	2.00
78	5.13	101.27	7.44	1.81	0.39	1.61	154.45	2.58	157.03	4.000	No	No	2.00
79	5.18	105.77	5.13	1.78	0.39	1.60	159.72	0.23	159.95	4.000	No	No	2.00
80	5.26	103.24	8.03	1.81	0.39	1.59	155.32	3.78	159.10	4.000	No	No	2.00
81	5.33	100.89	9.80	1.84	0.39	1.58	150.86	8.51	159.36	4.000	No	No	2.00
82	5.38	96.30	10.72	1.85	0.39	1.59	144.44	11.30	155.74	4.000	No	No	2.00
83	5.46	92.27	12.06	1.86	0.40	1.58	138.13	15.72	153.85	4.000	No	No	2.00
84	5.52	91.05	12.83	1.87	0.40	1.58	135.68	18.33	154.01	4.000	No	No	2.00
85	5.59	90.21	13.45	1.88	0.40	1.57	133.66	20.42	154.08	4.000	No	No	2.00
86	5.66	88.05	14.92	1.90	0.39	1.56	129.66	25.26	154.92	4.000	No	No	2.00
87	5.72	83.92	17.57	1.93	0.39	1.55	122.80	33.17	155.98	4.000	No	No	2.00
88	5.79	81.76	18.94	1.95	0.39	1.54	119.15	36.71	155.87	4.000	No	No	2.00
89	5.85	79.60	20.20	1.96	0.39	1.54	115.64	39.62	155.27	4.000	No	No	2.00
90	5.91	76.13	22.06	1.99	0.40	1.54	110.43	43.37	153.80	4.000	No	No	2.00
91	5.98	70.59	25.33	2.03	0.40	1.54	102.45	48.66	151.11	4.000	No	No	2.00
92	6.04	63.37	27.82	2.06	0.41	1.55	92.81	51.01	143.82	4.000	No	No	2.00
93	6.10	56.80	24.34	2.02	0.44	1.59	85.16	43.89	129.05	4.000	No	No	2.00
94	6.19	49.56	31.54	2.11	0.44	1.59	74.27	52.14	126.41	4.000	No	No	2.00
95	6.25	45.24	36.10	2.16	0.45	1.59	68.03	55.29	123.33	4.000	No	No	2.00
96	6.31	42.99	38.70	2.20	0.46	1.59	64.62	56.58	121.21	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	6.37	41.11	43.07	2.25	0.46	1.59	61.62	58.76	120.38	4.000	No	No	2.00
98	6.44	42.71	44.96	2.27	0.45	1.57	63.33	60.28	123.61	4.000	No	No	2.00
99	6.51	42.43	50.09	2.34	0.45	1.56	62.44	62.58	125.02	4.000	No	No	2.00
100	6.57	47.04	47.75	2.31	0.44	1.53	68.07	62.96	131.04	4.000	No	No	2.00
101	6.63	56.04	40.61	2.22	0.42	1.50	79.41	61.53	140.94	4.000	No	No	2.00
102	6.70	62.61	36.54	2.17	0.41	1.48	87.41	60.12	147.53	4.000	No	No	2.00
103	6.76	67.68	33.33	2.13	0.40	1.46	93.47	58.27	151.74	4.000	No	No	2.00
104	6.83	70.79	30.94	2.10	0.40	1.45	97.13	56.21	153.33	4.000	No	No	2.00
105	6.89	71.02	30.54	2.09	0.40	1.45	97.14	55.69	152.83	4.000	No	No	2.00
106	6.96	71.62	30.91	2.10	0.40	1.44	97.46	56.23	153.69	4.000	No	No	2.00
107	7.03	71.26	31.72	2.11	0.40	1.44	96.61	57.07	153.68	4.000	No	No	2.00
108	7.09	70.31	31.86	2.11	0.40	1.43	95.21	56.95	152.16	4.000	No	No	2.00
109	7.16	69.10	32.22	2.12	0.40	1.43	93.42	56.99	150.42	4.000	No	No	2.00
110	7.22	67.32	33.09	2.13	0.41	1.43	90.95	57.45	148.40	4.000	No	No	2.00
111	7.29	65.91	33.65	2.13	0.41	1.43	88.96	57.62	146.58	4.000	No	No	2.00
112	7.35	63.85	34.76	2.15	0.41	1.43	86.17	58.15	144.31	4.000	No	No	2.00
113	7.42	64.12	33.60	2.13	0.41	1.43	86.34	57.00	143.34	4.000	No	No	2.00
114	7.50	65.43	31.28	2.10	0.42	1.42	87.79	54.68	142.48	4.000	No	No	2.00
115	7.56	66.74	29.60	2.08	0.42	1.42	89.29	52.85	142.14	4.000	No	No	2.00
116	7.63	68.34	27.79	2.06	0.42	1.41	91.15	50.65	141.80	4.000	No	No	2.00
117	7.69	70.78	25.56	2.03	0.42	1.41	94.08	47.60	141.68	4.000	No	No	2.00
118	7.76	74.25	23.16	2.00	0.42	1.40	98.29	43.82	142.11	4.000	No	No	2.00
119	7.82	76.97	21.53	1.98	0.42	1.40	101.52	40.82	142.34	4.000	No	No	2.00
120	7.88	77.07	21.36	1.98	0.42	1.39	101.39	40.41	141.80	4.000	No	No	2.00
121	7.94	75.47	22.25	1.99	0.42	1.39	99.05	42.03	141.09	4.000	No	No	2.00
122	8.01	73.60	23.38	2.00	0.42	1.39	96.38	43.94	140.32	0.236	No	No	0.42
123	8.09	71.72	24.29	2.02	0.42	1.38	93.69	45.25	138.94	0.230	No	No	0.41
124	8.15	70.59	24.60	2.02	0.42	1.38	92.09	45.55	137.64	0.225	No	No	0.40
125	8.21	69.56	24.83	2.02	0.43	1.38	90.61	45.71	136.32	0.219	No	No	0.39
126	8.27	68.15	25.68	2.03	0.43	1.38	88.60	46.82	135.42	0.216	No	No	0.38
127	8.34	66.28	27.03	2.05	0.43	1.37	85.99	48.51	134.50	0.213	No	No	0.37
128	8.40	63.93	28.66	2.07	0.43	1.37	82.82	50.28	133.10	0.208	No	No	0.36
129	8.48	60.74	31.25	2.10	0.44	1.37	78.61	52.72	131.33	0.202	No	No	0.35
130	8.55	59.14	32.66	2.12	0.44	1.37	76.39	53.83	130.22	0.198	No	No	0.34
131	8.61	59.14	33.23	2.13	0.44	1.36	76.11	54.37	130.49	0.199	No	No	0.34
132	8.68	59.14	33.68	2.13	0.44	1.36	75.85	54.78	130.63	0.200	No	No	0.34
133	8.74	57.74	34.86	2.15	0.44	1.36	73.92	55.50	129.42	0.196	No	No	0.33
134	8.80	59.33	33.70	2.13	0.44	1.35	75.63	54.76	130.39	0.199	No	No	0.34
135	8.87	56.97	35.76	2.16	0.44	1.35	72.57	56.02	128.59	0.193	No	No	0.33
136	8.93	59.51	33.99	2.14	0.44	1.34	75.40	54.99	130.39	0.199	No	No	0.33
137	9.00	62.70	31.82	2.11	0.43	1.33	78.99	53.47	132.45	0.206	No	No	0.34
138	9.06	65.61	30.02	2.09	0.43	1.33	82.23	51.97	134.20	0.212	No	No	0.35
139	9.13	69.17	27.71	2.06	0.43	1.32	86.25	49.59	135.84	0.218	No	No	0.36
140	9.19	71.61	26.24	2.04	0.43	1.31	88.98	47.82	136.80	0.221	No	No	0.37
141	9.26	73.68	25.35	2.03	0.42	1.31	91.06	46.70	137.76	0.225	No	No	0.37
142	9.34	74.06	25.61	2.03	0.42	1.30	91.15	47.17	138.33	0.227	No	No	0.38
143	9.39	73.13	26.45	2.04	0.42	1.30	89.85	48.32	138.17	0.227	No	No	0.37
144	9.45	71.90	27.28	2.05	0.43	1.30	88.18	49.32	137.50	0.224	No	No	0.37

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	9.53	70.49	28.05	2.06	0.43	1.29	86.25	50.10	136.35	0.220	No	No	0.36
146	9.59	68.89	28.96	2.07	0.43	1.29	84.18	50.97	135.14	0.215	No	No	0.35
147	9.66	67.20	28.89	2.07	0.43	1.29	82.07	50.46	132.53	0.206	No	No	0.33
148	9.71	65.05	29.02	2.08	0.44	1.29	79.49	50.12	129.61	0.196	No	No	0.32
149	9.79	63.26	29.18	2.08	0.44	1.29	77.25	49.88	127.13	0.189	No	No	0.30
150	9.86	61.76	29.55	2.08	0.45	1.29	75.33	49.98	125.30	0.184	No	No	0.29
151	9.92	60.26	30.30	2.09	0.45	1.29	73.41	50.52	123.93	0.181	No	No	0.29
152	9.98	56.51	32.99	2.12	0.45	1.29	68.84	52.55	121.39	0.175	No	No	0.27
153	10.04	56.35	32.93	2.12	0.46	1.29	68.50	52.41	120.91	0.173	No	No	0.27
154	10.11	56.21	33.11	2.13	0.46	1.28	68.14	52.52	120.66	0.173	No	No	0.27
155	10.18	55.56	33.93	2.14	0.46	1.28	67.17	53.12	120.30	0.172	No	No	0.27
156	10.24	54.51	35.41	2.16	0.46	1.28	65.76	54.17	119.93	0.171	No	No	0.27
157	10.31	53.39	37.65	2.18	0.46	1.27	64.21	55.68	119.89	0.171	No	No	0.26
158	10.37	52.36	38.90	2.20	0.46	1.27	62.86	56.31	119.17	0.170	No	No	0.26
159	10.44	50.67	40.84	2.22	0.46	1.27	60.72	57.14	117.87	0.167	No	No	0.26
160	10.51	48.32	43.45	2.26	0.47	1.27	57.84	58.04	115.89	0.163	No	No	0.25
161	10.57	45.41	46.73	2.30	0.47	1.27	54.36	58.90	113.26	0.158	No	No	0.24
162	10.64	42.22	50.56	2.34	0.48	1.27	50.54	59.63	110.17	0.152	No	No	0.23
163	10.71	39.78	53.87	2.39	0.48	1.27	47.59	60.10	107.70	0.148	No	No	0.22
164	10.77	36.78	57.56	2.43	0.49	1.27	44.03	60.35	104.38	0.143	No	No	0.21
165	10.84	34.06	61.18	2.48	0.50	1.27	40.79	60.47	101.26	0.139	No	No	0.21
166	10.90	31.52	65.64	2.53	0.50	1.27	37.76	60.70	98.45	0.135	No	No	0.20
167	10.97	30.03	69.42	2.58	0.51	1.27	35.92	60.97	96.88	0.134	No	No	0.20
168	11.03	28.53	73.86	2.64	0.51	1.26	34.08	0.00	34.08	4.000	No	Yes	2.00
169	11.10	28.15	76.45	2.67	0.51	1.26	33.54	0.00	33.54	4.000	No	Yes	2.00
170	11.16	28.06	78.34	2.69	0.51	1.26	33.33	0.00	33.33	4.000	No	Yes	2.00
171	11.23	27.78	80.42	2.72	0.51	1.25	32.90	0.00	32.90	4.000	No	Yes	2.00
172	11.30	28.34	80.98	2.72	0.51	1.25	33.43	0.00	33.43	4.000	No	Yes	2.00
173	11.37	29.57	80.05	2.71	0.50	1.24	34.71	0.00	34.71	4.000	No	Yes	2.00
174	11.42	30.79	78.65	2.70	0.50	1.24	36.00	0.00	36.00	4.000	No	Yes	2.00
175	11.49	32.20	76.88	2.67	0.50	1.23	37.48	0.00	37.48	4.000	No	Yes	2.00
176	11.55	33.61	75.07	2.65	0.49	1.23	38.95	0.00	38.95	4.000	No	Yes	2.00
177	11.62	34.92	73.76	2.63	0.49	1.22	40.30	0.00	40.30	4.000	No	Yes	2.00
178	11.68	36.05	72.89	2.62	0.49	1.22	41.45	0.00	41.45	4.000	No	Yes	2.00
179	11.75	37.36	71.72	2.61	0.48	1.21	42.78	0.00	42.78	4.000	No	Yes	2.00
180	11.82	37.92	71.51	2.61	0.48	1.21	43.28	0.00	43.28	4.000	No	Yes	2.00
181	11.88	38.11	71.74	2.61	0.48	1.20	43.36	0.00	43.36	4.000	No	Yes	2.00
182	11.95	37.83	72.50	2.62	0.48	1.20	42.94	0.00	42.94	4.000	No	Yes	2.00
183	12.02	37.36	73.46	2.63	0.49	1.20	42.31	0.00	42.31	4.000	No	Yes	2.00
184	12.09	36.61	74.68	2.65	0.49	1.20	41.38	0.00	41.38	4.000	No	Yes	2.00
185	12.15	36.05	75.59	2.66	0.49	1.19	40.66	0.00	40.66	4.000	No	Yes	2.00
186	12.22	35.20	76.88	2.67	0.49	1.19	39.62	0.00	39.62	4.000	No	Yes	2.00
187	12.29	34.55	77.87	2.69	0.49	1.19	38.81	0.00	38.81	4.000	No	Yes	2.00
188	12.36	34.83	77.86	2.69	0.49	1.19	39.01	0.00	39.01	4.000	No	Yes	2.00
189	12.42	34.73	78.66	2.70	0.49	1.18	38.80	0.00	38.80	4.000	No	Yes	2.00
190	12.49	34.64	79.25	2.70	0.49	1.18	38.59	0.00	38.59	4.000	No	Yes	2.00
191	12.56	35.58	78.04	2.69	0.49	1.18	39.50	0.00	39.50	4.000	No	Yes	2.00
192	12.62	37.83	74.64	2.65	0.49	1.17	41.83	0.00	41.83	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	12.69	42.06	68.22	2.57	0.48	1.16	46.24	63.71	109.95	0.152	No	No	0.21
194	12.76	47.41	60.71	2.47	0.47	1.16	51.81	63.45	115.26	0.162	No	No	0.23
195	12.83	52.10	54.89	2.40	0.46	1.15	56.65	62.93	119.58	0.170	No	No	0.24
196	12.89	58.30	48.40	2.32	0.45	1.14	63.04	61.97	125.00	0.183	No	No	0.26
197	12.93	61.21	45.54	2.28	0.44	1.14	66.02	61.28	127.31	0.190	No	No	0.27
198	12.99	67.50	39.78	2.21	0.43	1.14	72.47	59.25	131.72	0.203	No	No	0.29
199	13.06	71.90	35.45	2.16	0.43	1.13	76.95	56.74	133.69	0.210	No	No	0.30
200	13.13	75.65	31.48	2.11	0.43	1.13	80.76	53.44	134.21	0.212	No	No	0.30
201	13.20	78.75	28.96	2.07	0.43	1.13	83.87	50.90	134.76	0.214	No	No	0.30
202	13.26	81.66	27.12	2.05	0.43	1.12	86.75	48.81	135.55	0.216	No	No	0.30
203	13.33	84.47	25.58	2.03	0.43	1.12	89.51	46.83	136.33	0.219	No	No	0.31
204	13.39	86.25	24.75	2.02	0.43	1.12	91.19	45.67	136.86	0.222	No	No	0.31
205	13.47	89.54	23.79	2.01	0.42	1.11	94.34	44.41	138.75	0.229	No	No	0.32
206	13.53	91.70	22.66	2.00	0.42	1.11	96.43	42.49	138.92	0.230	No	No	0.32
207	13.59	93.57	20.97	1.97	0.42	1.11	98.28	39.06	137.35	0.223	No	No	0.31
208	13.67	96.01	19.59	1.96	0.43	1.11	100.61	36.07	136.68	0.221	No	No	0.31
209	13.72	97.89	19.06	1.95	0.43	1.11	102.38	34.93	137.31	0.223	No	No	0.31
210	13.80	99.40	18.77	1.95	0.42	1.10	103.68	34.34	138.01	0.226	No	No	0.31
211	13.85	100.06	18.97	1.95	0.42	1.10	104.16	34.92	139.08	0.231	No	No	0.32
212	13.93	99.76	19.65	1.96	0.42	1.10	103.58	36.60	140.18	0.235	No	No	0.33
213	13.99	101.17	19.27	1.95	0.42	1.10	104.81	35.79	140.60	0.237	No	No	0.33
214	14.04	101.73	19.05	1.95	0.42	1.09	105.23	35.27	140.51	0.237	No	No	0.33
215	14.12	103.41	18.79	1.95	0.42	1.09	106.68	34.75	141.43	0.241	No	No	0.33
216	14.18	103.88	18.94	1.95	0.42	1.09	106.96	35.19	142.14	0.244	No	No	0.34
217	14.27	104.82	18.63	1.95	0.42	1.09	107.64	34.45	142.09	0.244	No	No	0.34
218	14.34	104.53	19.15	1.95	0.42	1.08	107.10	35.77	142.87	0.248	No	No	0.34
219	14.37	104.44	19.37	1.95	0.41	1.08	106.89	36.31	143.20	0.250	No	No	0.34
220	14.44	103.97	19.82	1.96	0.41	1.08	106.18	37.38	143.56	0.252	No	No	0.34
221	14.51	103.41	20.19	1.96	0.41	1.08	105.41	38.21	143.62	0.252	No	No	0.34
222	14.57	103.03	20.50	1.97	0.41	1.08	104.82	38.89	143.71	0.252	No	No	0.34
223	14.64	102.38	20.97	1.97	0.41	1.07	103.96	39.88	143.83	0.253	No	No	0.34
224	14.70	101.34	21.56	1.98	0.41	1.07	102.70	41.06	143.77	0.253	No	No	0.34
225	14.77	99.84	22.36	1.99	0.41	1.07	101.00	42.57	143.57	0.252	No	No	0.34
226	14.84	98.53	23.03	2.00	0.41	1.07	99.49	43.75	143.25	0.250	No	No	0.34
227	14.90	97.78	23.38	2.00	0.42	1.07	98.56	44.30	142.87	0.248	No	No	0.33
228	14.97	97.73	23.27	2.00	0.42	1.06	98.34	44.05	142.39	0.246	No	No	0.33
229	15.03	97.40	23.47	2.01	0.42	1.06	97.84	44.36	142.20	0.245	No	No	0.33
230	15.10	97.68	23.33	2.00	0.42	1.06	97.94	44.11	142.06	0.244	No	No	0.33
231	15.16	97.68	23.43	2.01	0.42	1.06	97.77	44.28	142.05	0.244	No	No	0.33
232	15.26	98.34	23.70	2.01	0.42	1.06	98.15	44.88	143.02	0.249	No	No	0.33
233	15.32	98.34	23.57	2.01	0.42	1.05	97.98	44.58	142.56	0.246	No	No	0.33
234	15.39	98.06	23.75	2.01	0.42	1.05	97.53	44.86	142.38	0.246	No	No	0.33
235	15.45	98.06	23.83	2.01	0.42	1.05	97.35	44.98	142.33	0.245	No	No	0.33
236	15.52	97.68	23.98	2.01	0.42	1.05	96.80	45.19	141.99	0.244	No	No	0.32
237	15.55	97.22	24.20	2.02	0.42	1.05	96.25	45.52	141.77	0.243	No	No	0.32
238	15.62	96.10	24.75	2.02	0.42	1.05	94.98	46.32	141.30	0.240	No	No	0.32
239	15.69	95.35	25.10	2.03	0.42	1.04	94.07	46.79	140.86	0.238	No	No	0.31
240	15.75	94.50	24.57	2.02	0.42	1.04	93.10	45.66	138.76	0.229	No	No	0.30

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	15.82	93.00	21.52	1.98	0.44	1.04	91.58	39.33	130.90	0.200	No	No	0.26
242	15.89	90.75	22.17	1.99	0.44	1.04	89.22	40.35	129.57	0.196	No	No	0.25
243	15.96	87.37	23.31	2.00	0.44	1.04	85.76	42.08	127.84	0.191	No	No	0.25
244	16.02	82.68	25.19	2.03	0.45	1.04	81.03	44.66	125.69	0.185	No	No	0.24
245	16.09	76.86	28.22	2.07	0.45	1.04	75.21	48.20	123.41	0.179	No	No	0.23
246	16.15	65.31	36.19	2.16	0.46	1.03	63.86	54.41	118.27	0.168	No	No	0.21
247	16.22	62.59	38.57	2.19	0.46	1.03	61.10	55.65	116.75	0.165	No	No	0.21
248	16.28	55.83	44.19	2.26	0.47	1.03	54.44	57.60	112.04	0.156	No	No	0.20
249	16.35	48.32	52.05	2.36	0.48	1.03	47.06	59.29	106.35	0.146	No	No	0.18
250	16.42	41.47	61.06	2.48	0.50	1.03	40.34	60.31	100.65	0.138	No	No	0.17
251	16.48	34.99	70.32	2.59	0.51	1.03	34.00	60.58	94.58	0.131	No	No	0.16
252	16.55	29.93	78.80	2.70	0.52	1.03	29.04	0.00	29.04	4.000	No	Yes	2.00
253	16.61	26.45	84.87	2.77	0.53	1.02	25.62	0.00	25.62	4.000	No	Yes	2.00
254	16.68	25.23	86.99	2.80	0.53	1.02	24.39	0.00	24.39	4.000	No	Yes	2.00
255	16.75	23.56	90.49	2.84	0.54	1.02	22.73	0.00	22.73	4.000	No	Yes	2.00
256	16.82	22.43	92.97	2.87	0.54	1.02	21.59	0.00	21.59	4.000	No	Yes	2.00
257	16.88	22.34	93.80	2.89	0.54	1.02	21.46	0.00	21.46	4.000	No	Yes	2.00
258	16.95	23.94	91.97	2.86	0.54	1.01	22.94	0.00	22.94	4.000	No	Yes	2.00
259	17.02	27.88	86.09	2.79	0.53	1.01	26.65	0.00	26.65	4.000	No	Yes	2.00
260	17.09	33.98	78.10	2.69	0.51	1.01	32.41	0.00	32.41	4.000	No	Yes	2.00
261	17.15	40.47	70.47	2.59	0.50	1.01	38.51	61.93	100.43	0.138	No	No	0.17
262	17.22	47.99	63.23	2.50	0.48	1.01	45.56	62.35	107.91	0.149	No	No	0.18
263	17.29	54.93	57.23	2.43	0.47	1.00	52.05	62.46	114.51	0.160	No	No	0.20
264	17.36	61.86	51.92	2.36	0.46	1.00	58.51	62.31	120.82	0.173	No	No	0.22
265	17.39	64.68	49.96	2.34	0.45	1.00	61.13	62.18	123.30	0.179	No	No	0.22
266	17.46	71.06	45.53	2.28	0.44	1.00	67.04	61.54	128.58	0.193	No	No	0.24
267	17.53	76.78	41.70	2.23	0.43	1.00	72.32	60.55	132.87	0.207	No	No	0.26
268	17.59	81.28	39.16	2.20	0.43	1.00	76.44	59.74	136.18	0.219	No	No	0.28
269	17.66	84.47	37.81	2.19	0.42	0.99	79.32	59.35	138.66	0.229	No	No	0.29
270	17.73	87.29	36.65	2.17	0.42	0.99	81.84	58.94	140.78	0.238	No	No	0.30
271	17.79	89.63	35.76	2.16	0.42	0.99	83.90	58.60	142.50	0.246	No	No	0.31
272	17.86	91.13	35.48	2.16	0.41	0.99	85.17	58.63	143.80	0.253	No	No	0.32
273	17.93	91.04	35.82	2.16	0.41	0.99	84.95	58.90	143.85	0.253	No	No	0.32
274	17.99	90.01	37.17	2.18	0.41	0.99	83.86	59.86	143.72	0.252	No	No	0.32
275	18.06	88.61	38.43	2.19	0.42	0.98	82.41	60.58	142.99	0.249	No	No	0.31
276	18.13	87.29	39.12	2.20	0.42	0.98	81.05	60.81	141.86	0.243	No	No	0.31
277	18.20	85.88	40.25	2.22	0.42	0.98	79.61	61.32	140.93	0.239	No	No	0.30
278	18.26	83.81	41.55	2.23	0.42	0.98	77.56	61.74	139.30	0.232	No	No	0.29
279	18.33	81.19	43.21	2.25	0.43	0.98	75.00	62.19	137.19	0.223	No	No	0.28
280	18.40	77.81	45.03	2.28	0.43	0.98	71.74	62.46	134.19	0.212	No	No	0.26
281	18.45	62.41	55.72	2.41	0.46	0.97	57.40	63.43	120.83	0.173	No	No	0.21
282	18.51	67.29	51.22	2.35	0.45	0.97	61.81	62.90	124.71	0.183	No	No	0.22
283	18.57	62.13	54.17	2.39	0.46	0.97	56.95	62.75	119.70	0.171	No	No	0.21
284	18.64	54.52	59.86	2.46	0.47	0.97	49.84	62.65	112.49	0.156	No	No	0.19
285	18.72	46.64	66.89	2.55	0.49	0.96	42.50	62.34	104.85	0.144	No	No	0.17
286	18.77	40.26	73.65	2.63	0.50	0.96	36.60	0.00	36.60	4.000	No	Yes	2.00
287	18.86	32.19	83.05	2.75	0.52	0.96	29.15	0.00	29.15	4.000	No	Yes	2.00
288	18.91	27.87	88.91	2.82	0.53	0.96	25.18	0.00	25.18	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	18.98	24.87	93.29	2.88	0.54	0.95	22.41	0.00	22.41	4.000	No	Yes	2.00
290	19.04	22.80	96.37	2.92	0.54	0.95	20.50	0.00	20.50	4.000	No	Yes	2.00
291	19.11	19.99	100.00	2.99	0.55	0.95	17.92	0.00	17.92	4.000	No	Yes	2.00
292	19.18	18.11	100.00	3.04	0.56	0.95	16.20	0.00	16.20	4.000	No	Yes	2.00
293	19.24	17.08	100.00	3.08	0.56	0.94	15.24	0.00	15.24	4.000	No	Yes	2.00
294	19.31	16.05	100.00	3.12	0.57	0.94	14.29	0.00	14.29	4.000	No	Yes	2.00
295	19.37	15.01	100.00	3.15	0.57	0.94	13.34	0.00	13.34	4.000	No	Yes	2.00
296	19.44	14.55	100.00	3.16	0.57	0.94	12.90	0.00	12.90	4.000	No	Yes	2.00
297	19.51	14.45	100.00	3.17	0.57	0.94	12.79	0.00	12.79	4.000	No	Yes	2.00
298	19.58	14.83	100.00	3.15	0.57	0.93	13.10	0.00	13.10	4.000	No	Yes	2.00
299	19.64	14.45	100.00	3.14	0.57	0.93	12.74	0.00	12.74	4.000	No	Yes	2.00
300	19.71	14.46	100.00	3.11	0.57	0.93	12.72	0.00	12.72	4.000	No	Yes	2.00
301	19.78	14.46	100.00	3.14	0.57	0.93	12.69	0.00	12.69	4.000	No	Yes	2.00
302	19.84	14.74	100.00	3.14	0.57	0.93	12.92	0.00	12.92	4.000	No	Yes	2.00
303	19.91	15.21	100.00	3.13	0.57	0.93	13.31	0.00	13.31	4.000	No	Yes	2.00
304	19.98	15.40	100.00	3.13	0.57	0.92	13.45	0.00	13.45	4.000	No	Yes	2.00
305	20.02	15.31	100.00	3.14	0.57	0.92	13.35	0.00	13.35	4.000	No	Yes	2.00
306	20.10	15.21	100.00	3.14	0.57	0.92	13.24	0.00	13.24	4.000	No	Yes	2.00
307	20.15	15.50	100.00	3.13	0.57	0.92	13.47	0.00	13.47	4.000	No	Yes	2.00
308	20.22	15.69	100.00	3.12	0.57	0.92	13.61	0.00	13.61	4.000	No	Yes	2.00
309	20.28	15.69	100.00	3.12	0.57	0.92	13.59	0.00	13.59	4.000	No	Yes	2.00
310	20.34	15.87	100.00	3.11	0.57	0.92	13.73	0.00	13.73	4.000	No	Yes	2.00
311	20.41	16.06	100.00	3.10	0.57	0.91	13.87	0.00	13.87	4.000	No	Yes	2.00
312	20.48	15.97	100.00	3.11	0.57	0.91	13.76	0.00	13.76	4.000	No	Yes	2.00
313	20.55	16.35	100.00	3.09	0.57	0.91	14.06	0.00	14.06	4.000	No	Yes	2.00
314	20.61	16.63	100.00	3.06	0.57	0.91	14.28	0.00	14.28	4.000	No	Yes	2.00
315	20.68	17.10	100.00	3.02	0.56	0.91	14.66	0.00	14.66	4.000	No	Yes	2.00
316	20.74	17.66	100.00	3.01	0.56	0.91	15.12	0.00	15.12	4.000	No	Yes	2.00
317	20.81	18.13	100.00	3.01	0.56	0.91	15.50	0.00	15.50	4.000	No	Yes	2.00
318	20.88	18.60	100.00	3.01	0.56	0.90	15.88	0.00	15.88	4.000	No	Yes	2.00
319	20.95	18.70	100.00	3.02	0.56	0.90	15.94	0.00	15.94	4.000	No	Yes	2.00
320	21.00	17.30	100.00	3.08	0.56	0.90	14.70	0.00	14.70	4.000	No	Yes	2.00
321	21.08	19.39	100.00	3.01	0.56	0.90	16.44	0.00	16.44	4.000	No	Yes	2.00
322	21.13	19.39	100.00	3.02	0.56	0.90	16.42	0.00	16.42	4.000	No	Yes	2.00
323	21.22	19.87	100.00	3.01	0.56	0.90	16.79	0.00	16.79	4.000	No	Yes	2.00
324	21.29	20.06	100.00	3.01	0.56	0.90	16.92	0.00	16.92	4.000	No	Yes	2.00
325	21.36	20.06	100.00	3.01	0.56	0.89	16.89	0.00	16.89	4.000	No	Yes	2.00
326	21.42	19.96	100.00	3.03	0.56	0.89	16.78	0.00	16.78	4.000	No	Yes	2.00
327	21.49	19.96	100.00	3.04	0.56	0.89	16.76	0.00	16.76	4.000	No	Yes	2.00
328	21.55	19.96	100.00	3.05	0.56	0.89	16.73	0.00	16.73	4.000	No	Yes	2.00
329	21.62	19.96	100.00	3.06	0.56	0.89	16.70	0.00	16.70	4.000	No	Yes	2.00
330	21.65	20.14	100.00	3.05	0.56	0.89	16.84	0.00	16.84	4.000	No	Yes	2.00
331	21.72	20.33	100.00	3.05	0.56	0.89	16.97	0.00	16.97	4.000	No	Yes	2.00
332	21.79	20.52	100.00	3.05	0.56	0.88	17.10	0.00	17.10	4.000	No	Yes	2.00
333	21.85	20.42	100.00	3.06	0.56	0.88	16.99	0.00	16.99	4.000	No	Yes	2.00
334	21.92	20.43	100.00	3.06	0.56	0.88	16.96	0.00	16.96	4.000	No	Yes	2.00
335	21.99	21.00	100.00	3.04	0.55	0.88	17.41	0.00	17.41	4.000	No	Yes	2.00
336	22.06	21.65	100.00	3.03	0.55	0.88	17.93	0.00	17.93	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	22.12	22.32	100.00	3.01	0.55	0.88	18.46	0.00	18.46	4.000	No	Yes	2.00
338	22.19	22.51	100.00	3.01	0.55	0.88	18.59	0.00	18.59	4.000	No	Yes	2.00
339	22.26	22.51	100.00	3.01	0.55	0.88	18.56	0.00	18.56	4.000	No	Yes	2.00
340	22.32	22.50	100.00	3.01	0.55	0.87	18.53	0.00	18.53	4.000	No	Yes	2.00
341	22.39	24.57	98.45	2.94	0.55	0.87	20.22	0.00	20.22	4.000	No	Yes	2.00
342	22.45	29.46	88.81	2.82	0.53	0.87	24.28	0.00	24.28	4.000	No	Yes	2.00
343	22.52	38.87	74.20	2.64	0.51	0.88	32.16	0.00	32.16	4.000	No	Yes	2.00
344	22.59	51.44	59.52	2.46	0.49	0.88	42.77	60.57	103.34	0.142	No	No	0.16
345	22.66	63.81	48.07	2.31	0.47	0.88	53.29	59.27	112.56	0.157	No	No	0.18
346	22.73	73.28	41.58	2.23	0.46	0.89	61.34	57.78	119.12	0.169	No	No	0.19
347	22.79	80.22	38.49	2.19	0.45	0.89	67.24	57.04	124.28	0.182	No	No	0.21
348	22.86	85.10	36.21	2.17	0.44	0.89	71.35	56.15	127.50	0.190	No	No	0.22
349	22.93	88.87	34.29	2.14	0.44	0.89	74.49	55.09	129.57	0.196	No	No	0.23
350	22.99	91.40	33.14	2.13	0.44	0.89	76.56	54.38	130.94	0.201	No	No	0.23
351	23.05	86.33	36.45	2.17	0.44	0.89	72.15	56.53	128.69	0.194	No	No	0.22
352	23.10	92.49	33.45	2.13	0.43	0.89	77.41	54.89	132.29	0.205	No	No	0.24
353	23.19	98.95	30.97	2.10	0.43	0.89	82.84	53.28	136.12	0.219	No	No	0.25
354	23.26	102.71	30.61	2.10	0.42	0.89	86.02	53.49	139.52	0.233	No	No	0.27
355	23.32	106.09	30.98	2.10	0.41	0.89	88.92	54.55	143.47	0.251	No	No	0.29
356	23.39	109.27	30.89	2.10	0.41	0.89	91.63	55.00	146.63	0.268	No	No	0.31
357	23.45	112.55	30.57	2.09	0.40	0.89	94.41	55.17	149.58	0.286	No	No	0.33
358	23.52	115.45	30.24	2.09	0.40	0.89	96.85	55.23	152.08	0.303	No	No	0.35
359	23.59	118.74	29.35	2.08	0.40	0.89	99.59	54.56	154.15	0.319	No	No	0.37
360	23.65	120.61	28.69	2.07	0.40	0.89	101.08	53.91	154.99	0.326	No	No	0.38
361	23.72	120.89	28.49	2.07	0.40	0.89	101.19	53.63	154.82	0.324	No	No	0.38
362	23.78	118.35	29.17	2.08	0.40	0.88	98.87	54.16	153.03	0.310	No	No	0.36
363	23.82	115.63	29.90	2.09	0.40	0.88	96.45	54.70	151.15	0.297	No	No	0.35
364	23.89	107.75	32.33	2.12	0.41	0.88	89.52	56.28	145.80	0.263	No	No	0.31
365	23.96	96.58	37.17	2.18	0.42	0.87	79.84	58.93	138.77	0.229	No	No	0.26
366	24.02	83.72	44.11	2.26	0.44	0.87	68.78	61.18	129.95	0.197	No	No	0.23
367	24.09	69.74	53.22	2.38	0.46	0.86	56.85	62.37	119.22	0.170	No	No	0.19
368	24.16	55.66	64.84	2.52	0.48	0.85	44.97	62.58	107.54	0.148	No	No	0.17
369	24.22	43.46	77.79	2.68	0.50	0.85	34.80	0.00	34.80	4.000	No	Yes	2.00
370	24.29	35.01	88.25	2.82	0.52	0.84	27.82	0.00	27.82	4.000	No	Yes	2.00
371	24.36	29.38	95.63	2.91	0.54	0.84	23.21	0.00	23.21	4.000	No	Yes	2.00
372	24.43	25.72	100.00	2.97	0.55	0.83	20.23	0.00	20.23	4.000	No	Yes	2.00
373	24.49	24.03	100.00	2.98	0.55	0.83	18.84	0.00	18.84	4.000	No	Yes	2.00
374	24.56	24.03	100.00	2.97	0.55	0.83	18.81	0.00	18.81	4.000	No	Yes	2.00
375	24.63	26.85	96.08	2.91	0.54	0.83	21.04	0.00	21.04	4.000	No	Yes	2.00
376	24.69	33.14	83.80	2.76	0.53	0.83	26.05	0.00	26.05	4.000	No	Yes	2.00
377	24.76	44.12	71.73	2.61	0.51	0.84	34.92	0.00	34.92	4.000	No	Yes	2.00
378	24.83	57.63	60.74	2.47	0.48	0.84	45.96	61.81	107.77	0.149	No	No	0.17
379	24.89	66.64	55.87	2.41	0.47	0.85	53.39	62.38	115.77	0.163	No	No	0.18
380	24.96	73.13	53.65	2.38	0.45	0.85	58.75	63.05	121.79	0.176	No	No	0.20
381	25.03	79.42	51.68	2.36	0.44	0.85	63.96	63.67	127.64	0.191	No	No	0.22
382	25.09	86.28	49.11	2.33	0.43	0.85	69.68	64.04	133.72	0.210	No	No	0.24
383	25.16	91.92	46.83	2.30	0.42	0.86	74.37	64.12	138.50	0.228	No	No	0.26
384	25.23	97.44	44.03	2.26	0.42	0.86	78.97	63.70	142.67	0.247	No	No	0.28

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	25.29	103.17	41.29	2.23	0.41	0.86	83.74	63.07	146.81	0.269	No	No	0.31
386	25.36	108.23	38.64	2.20	0.40	0.86	87.92	62.06	149.98	0.289	No	No	0.33
387	25.43	107.58	38.49	2.19	0.41	0.86	87.24	61.78	149.01	0.282	No	No	0.32
388	25.49	103.26	40.31	2.22	0.41	0.86	83.47	62.30	145.76	0.263	No	No	0.30
389	25.53	99.13	42.33	2.24	0.42	0.85	79.93	62.85	142.78	0.248	No	No	0.28
390	25.60	89.84	47.34	2.30	0.43	0.85	72.02	63.78	135.80	0.217	No	No	0.25
391	25.66	79.99	53.18	2.38	0.44	0.84	63.69	64.21	127.90	0.191	No	No	0.22
392	25.73	66.29	62.39	2.49	0.46	0.83	52.27	64.04	116.31	0.164	No	No	0.18
393	25.80	56.34	69.85	2.59	0.48	0.83	44.05	63.42	107.47	0.148	No	No	0.16
394	25.85	48.74	76.63	2.67	0.50	0.82	37.84	0.00	37.84	4.000	No	Yes	2.00
395	25.93	42.92	82.50	2.74	0.51	0.82	33.12	0.00	33.12	4.000	No	Yes	2.00
396	25.99	37.76	88.78	2.82	0.52	0.81	28.98	0.00	28.98	4.000	No	Yes	2.00
397	26.07	29.86	99.36	2.95	0.54	0.81	22.72	0.00	22.72	4.000	No	Yes	2.00
398	26.13	27.80	100.00	2.98	0.54	0.80	21.08	0.00	21.08	4.000	No	Yes	2.00
399	26.18	26.58	100.00	2.99	0.55	0.80	20.10	0.00	20.10	4.000	No	Yes	2.00
400	26.26	25.17	100.00	3.00	0.55	0.80	18.98	0.00	18.98	4.000	No	Yes	2.00
401	26.32	24.61	100.00	3.01	0.55	0.80	18.52	0.00	18.52	4.000	No	Yes	2.00
402	26.39	24.62	100.00	3.00	0.55	0.80	18.49	0.00	18.49	4.000	No	Yes	2.00
403	26.46	24.62	100.00	3.00	0.55	0.79	18.46	0.00	18.46	4.000	No	Yes	2.00
404	26.51	24.24	100.00	3.01	0.55	0.79	18.15	0.00	18.15	4.000	No	Yes	2.00
405	26.58	24.24	100.00	3.01	0.55	0.79	18.12	0.00	18.12	4.000	No	Yes	2.00
406	26.66	26.40	99.92	2.96	0.55	0.79	19.76	0.00	19.76	4.000	No	Yes	2.00
407	26.72	29.98	94.58	2.89	0.54	0.79	22.48	0.00	22.48	4.000	No	Yes	2.00
408	26.80	39.27	81.63	2.73	0.52	0.80	29.66	0.00	29.66	4.000	No	Yes	2.00
409	26.85	45.08	74.62	2.65	0.51	0.80	34.19	0.00	34.19	4.000	No	Yes	2.00
410	26.91	49.67	70.16	2.59	0.50	0.81	37.77	61.65	99.42	0.137	No	No	0.15
411	26.98	52.12	69.37	2.58	0.49	0.81	39.65	62.04	101.70	0.140	No	No	0.15
412	27.04	52.04	70.50	2.59	0.49	0.80	39.55	62.24	101.79	0.140	No	No	0.15
413	27.11	49.03	74.81	2.65	0.50	0.80	37.13	0.00	37.13	4.000	No	Yes	2.00
414	27.19	43.76	81.51	2.73	0.51	0.80	32.96	0.00	32.96	4.000	No	Yes	2.00
415	27.24	40.67	85.09	2.78	0.52	0.79	30.51	0.00	30.51	4.000	No	Yes	2.00
416	27.30	38.60	87.57	2.81	0.52	0.79	28.87	0.00	28.87	4.000	No	Yes	2.00
417	27.37	35.33	92.01	2.86	0.53	0.79	26.30	0.00	26.30	4.000	No	Yes	2.00
418	27.43	35.03	92.38	2.87	0.53	0.79	26.04	0.00	26.04	4.000	No	Yes	2.00
419	27.52	37.86	88.38	2.82	0.52	0.79	28.16	0.00	28.16	4.000	No	Yes	2.00
420	27.58	41.06	83.85	2.76	0.52	0.79	30.59	0.00	30.59	4.000	No	Yes	2.00
421	27.63	44.72	79.04	2.70	0.51	0.79	33.40	0.00	33.40	4.000	No	Yes	2.00
422	27.72	54.95	67.84	2.56	0.49	0.80	41.31	62.21	103.52	0.142	No	No	0.16
423	27.79	63.01	60.13	2.46	0.48	0.80	47.63	62.10	109.73	0.152	No	No	0.17
424	27.85	69.77	54.25	2.39	0.47	0.80	52.93	61.69	114.62	0.160	No	No	0.18
425	27.89	72.21	51.36	2.35	0.46	0.80	54.82	61.09	115.91	0.163	No	No	0.18
426	27.95	78.13	43.93	2.26	0.46	0.80	59.35	58.70	118.05	0.167	No	No	0.18
427	28.02	83.38	39.91	2.21	0.46	0.81	63.43	57.17	120.60	0.173	No	No	0.19
428	28.09	88.16	36.80	2.17	0.45	0.81	67.13	55.67	122.80	0.178	No	No	0.20
429	28.16	92.29	34.40	2.14	0.45	0.81	70.31	54.26	124.57	0.182	No	No	0.20
430	28.23	95.76	32.49	2.12	0.45	0.81	72.96	52.92	125.88	0.186	No	No	0.20
431	28.28	96.78	31.99	2.11	0.45	0.81	73.71	52.54	126.25	0.187	No	No	0.21
432	28.36	97.81	31.93	2.11	0.44	0.81	74.47	52.63	127.10	0.189	No	No	0.21

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	28.42	101.84	30.68	2.10	0.44	0.81	77.62	51.85	129.46	0.196	No	No	0.22
434	28.48	104.37	30.45	2.09	0.44	0.81	79.64	51.98	131.61	0.203	No	No	0.22
435	28.57	107.93	31.01	2.10	0.43	0.81	82.54	53.26	135.80	0.217	No	No	0.24
436	28.63	110.37	30.99	2.10	0.42	0.81	84.50	53.64	138.14	0.227	No	No	0.25
437	28.69	112.34	31.09	2.10	0.42	0.81	86.07	54.09	140.16	0.235	No	No	0.26
438	28.76	113.94	31.27	2.10	0.42	0.81	87.34	54.58	141.92	0.243	No	No	0.27
439	28.82	114.41	31.76	2.11	0.42	0.81	87.69	55.23	142.92	0.248	No	No	0.28
440	28.89	114.22	32.42	2.12	0.41	0.81	87.50	55.96	143.46	0.251	No	No	0.28
441	28.96	113.28	33.50	2.13	0.41	0.81	86.71	56.97	143.68	0.252	No	No	0.28
442	29.02	111.41	34.69	2.15	0.42	0.81	85.14	57.85	142.99	0.249	No	No	0.28
443	29.09	109.06	36.05	2.16	0.42	0.81	83.19	58.71	141.89	0.243	No	No	0.27
444	29.16	105.87	37.54	2.18	0.42	0.80	80.54	59.40	139.94	0.234	No	No	0.26
445	29.23	101.74	39.67	2.21	0.43	0.80	77.14	60.29	137.44	0.224	No	No	0.25
446	29.29	96.30	42.42	2.24	0.43	0.80	72.71	61.12	133.82	0.210	No	No	0.23
447	29.36	89.44	47.21	2.30	0.44	0.80	67.20	62.46	129.66	0.197	No	No	0.22
448	29.43	81.27	52.12	2.36	0.45	0.79	60.64	62.96	123.61	0.180	No	No	0.20
449	29.49	71.14	59.77	2.46	0.46	0.78	52.62	63.40	116.02	0.163	No	No	0.18
450	29.56	59.12	70.11	2.59	0.48	0.77	43.24	63.23	106.47	0.147	No	No	0.16
451	29.59	52.94	76.04	2.66	0.50	0.77	38.46	0.00	38.46	4.000	No	Yes	2.00
452	29.66	41.57	87.38	2.80	0.52	0.76	29.82	0.00	29.82	4.000	No	Yes	2.00
453	29.73	32.66	95.44	2.91	0.54	0.75	23.17	0.00	23.17	4.000	No	Yes	2.00
454	29.79	30.12	99.13	2.95	0.54	0.75	21.28	0.00	21.28	4.000	No	Yes	2.00
455	29.88	25.06	100.00	3.06	0.55	0.74	17.55	0.00	17.55	4.000	No	Yes	2.00
456	29.94	22.34	100.00	3.11	0.56	0.74	15.57	0.00	15.57	4.000	No	Yes	2.00
457	30.01	21.21	100.00	3.13	0.56	0.74	14.74	0.00	14.74	4.000	No	Yes	2.00
458	30.06	21.31	100.00	3.11	0.56	0.73	14.79	0.00	14.79	4.000	No	Yes	2.00
459	30.12	19.62	100.00	3.14	0.57	0.73	13.57	0.00	13.57	4.000	No	Yes	2.00
460	30.19	18.40	100.00	3.18	0.57	0.73	12.69	0.00	12.69	4.000	No	Yes	2.00
461	30.26	18.03	100.00	3.19	0.57	0.73	12.41	0.00	12.41	4.000	No	Yes	2.00
462	30.32	17.84	100.00	3.18	0.57	0.73	12.26	0.00	12.26	4.000	No	Yes	2.00
463	30.39	17.47	100.00	3.18	0.57	0.73	11.98	0.00	11.98	4.000	No	Yes	2.00
464	30.45	17.18	100.00	3.18	0.58	0.73	11.77	0.00	11.77	4.000	No	Yes	2.00
465	30.52	17.18	100.00	3.18	0.58	0.72	11.75	0.00	11.75	4.000	No	Yes	2.00
466	30.59	17.18	100.00	3.17	0.58	0.72	11.74	0.00	11.74	4.000	No	Yes	2.00
467	30.66	17.18	100.00	3.16	0.58	0.72	11.72	0.00	11.72	4.000	No	Yes	2.00
468	30.72	17.37	100.00	3.19	0.58	0.72	11.84	0.00	11.84	4.000	No	Yes	2.00
469	30.79	17.56	100.00	3.18	0.57	0.72	11.96	0.00	11.96	4.000	No	Yes	2.00
470	30.85	17.84	100.00	3.17	0.57	0.72	12.14	0.00	12.14	4.000	No	Yes	2.00
471	30.92	19.25	100.00	3.12	0.57	0.72	13.11	0.00	13.11	4.000	No	Yes	2.00
472	30.97	19.72	100.00	3.11	0.57	0.72	13.43	0.00	13.43	4.000	No	Yes	2.00
473	31.07	20.47	100.00	3.08	0.57	0.72	13.93	0.00	13.93	4.000	No	Yes	2.00
474	31.10	20.19	100.00	3.09	0.57	0.72	13.73	0.00	13.73	4.000	No	Yes	2.00
475	31.19	18.78	100.00	3.15	0.57	0.72	12.72	0.00	12.72	4.000	No	Yes	2.00
476	31.24	18.22	100.00	3.18	0.57	0.72	12.32	0.00	12.32	4.000	No	Yes	2.00
477	31.30	17.28	100.00	3.21	0.58	0.71	11.66	0.00	11.66	4.000	No	Yes	2.00
478	31.38	17.84	100.00	3.18	0.57	0.71	12.03	0.00	12.03	4.000	No	Yes	2.00
479	31.43	17.37	100.00	3.19	0.58	0.71	11.69	0.00	11.69	4.000	No	Yes	2.00
480	31.50	17.79	100.00	3.17	0.57	0.71	11.97	0.00	11.97	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	31.57	17.65	100.00	3.17	0.58	0.71	11.86	0.00	11.86	4.000	No	Yes	2.00
482	31.63	17.75	100.00	3.16	0.57	0.71	11.91	0.00	11.91	4.000	No	Yes	2.00
483	31.70	17.47	100.00	3.17	0.58	0.71	11.70	0.00	11.70	4.000	No	Yes	2.00
484	31.77	17.09	100.00	3.20	0.58	0.71	11.43	0.00	11.43	4.000	No	Yes	2.00
485	31.84	16.53	100.00	3.23	0.58	0.71	11.03	0.00	11.03	4.000	No	Yes	2.00
486	31.90	16.90	100.00	3.23	0.58	0.71	11.27	0.00	11.27	4.000	No	Yes	2.00
487	31.97	18.23	100.00	3.18	0.57	0.71	12.16	0.00	12.16	4.000	No	Yes	2.00
488	32.03	20.57	100.00	3.12	0.57	0.71	13.76	0.00	13.76	4.000	No	Yes	2.00
489	32.10	23.31	100.00	3.05	0.56	0.71	15.63	0.00	15.63	4.000	No	Yes	2.00
490	32.17	23.88	100.00	3.05	0.56	0.71	16.01	0.00	16.01	4.000	No	Yes	2.00
491	32.23	22.28	100.00	3.11	0.56	0.71	14.88	0.00	14.88	4.000	No	Yes	2.00
492	32.29	20.12	100.00	3.18	0.57	0.70	13.38	0.00	13.38	4.000	No	Yes	2.00
493	32.35	18.81	100.00	3.22	0.57	0.70	12.46	0.00	12.46	4.000	No	Yes	2.00
494	32.42	17.87	100.00	3.25	0.58	0.70	11.81	0.00	11.81	4.000	No	Yes	2.00
495	32.49	17.87	100.00	3.24	0.58	0.70	11.79	0.00	11.79	4.000	No	Yes	2.00
496	32.56	18.43	100.00	3.21	0.57	0.70	12.16	0.00	12.16	4.000	No	Yes	2.00
497	32.62	19.94	100.00	3.16	0.57	0.70	13.18	0.00	13.18	4.000	No	Yes	2.00
498	32.68	21.45	100.00	3.12	0.57	0.70	14.19	0.00	14.19	4.000	No	Yes	2.00
499	32.75	22.39	100.00	3.09	0.56	0.70	14.82	0.00	14.82	4.000	No	Yes	2.00
500	32.82	22.57	100.00	3.10	0.56	0.70	14.92	0.00	14.92	4.000	No	Yes	2.00
501	32.88	22.95	100.00	3.11	0.56	0.70	15.16	0.00	15.16	4.000	No	Yes	2.00
502	32.95	24.93	100.00	3.09	0.56	0.70	16.50	0.00	16.50	4.000	No	Yes	2.00
503	33.01	28.31	100.00	3.03	0.55	0.70	18.82	0.00	18.82	4.000	No	Yes	2.00
504	33.08	34.03	96.38	2.92	0.54	0.71	22.79	0.00	22.79	4.000	No	Yes	2.00
505	33.15	41.73	87.10	2.80	0.52	0.72	28.20	0.00	28.20	4.000	No	Yes	2.00
506	33.21	48.68	81.44	2.73	0.51	0.72	33.15	0.00	33.15	4.000	No	Yes	2.00
507	33.28	50.65	81.25	2.73	0.50	0.72	34.54	0.00	34.54	4.000	No	Yes	2.00
508	33.35	49.24	83.48	2.76	0.51	0.72	33.50	0.00	33.50	4.000	No	Yes	2.00
509	33.41	44.74	88.64	2.82	0.52	0.72	30.23	0.00	30.23	4.000	No	Yes	2.00
510	33.48	39.75	94.39	2.89	0.53	0.71	26.67	0.00	26.67	4.000	No	Yes	2.00
511	33.55	33.67	100.00	2.99	0.54	0.70	22.36	0.00	22.36	4.000	No	Yes	2.00
512	33.62	30.19	100.00	3.05	0.55	0.70	19.92	0.00	19.92	4.000	No	Yes	2.00
513	33.68	28.90	100.00	3.07	0.55	0.70	18.99	0.00	18.99	4.000	No	Yes	2.00
514	33.75	26.26	100.00	3.12	0.56	0.69	17.16	0.00	17.16	4.000	No	Yes	2.00
515	33.82	22.98	100.00	3.17	0.56	0.69	14.92	0.00	14.92	4.000	No	Yes	2.00
516	33.88	20.06	100.00	3.17	0.57	0.69	12.95	0.00	12.95	4.000	No	Yes	2.00
517	33.95	17.91	100.00	3.20	0.58	0.68	11.49	0.00	11.49	4.000	No	Yes	2.00
518	34.02	16.32	100.00	3.25	0.58	0.68	10.43	0.00	10.43	4.000	No	Yes	2.00
519	34.09	15.19	100.00	3.30	0.58	0.68	9.67	0.00	9.67	4.000	No	Yes	2.00
520	34.15	14.72	100.00	3.32	0.58	0.68	9.35	0.00	9.35	4.000	No	Yes	2.00
521	34.19	15.19	100.00	3.30	0.58	0.68	9.66	0.00	9.66	4.000	No	Yes	2.00
522	34.25	13.98	100.00	3.36	0.59	0.67	8.85	0.00	8.85	4.000	No	Yes	2.00
523	34.33	15.21	100.00	3.30	0.58	0.67	9.63	0.00	9.63	4.000	No	Yes	2.00
524	34.40	15.30	100.00	3.30	0.58	0.67	9.68	0.00	9.68	4.000	No	Yes	2.00
525	34.46	15.30	100.00	3.30	0.58	0.67	9.67	0.00	9.67	4.000	No	Yes	2.00
526	34.52	15.30	100.00	3.29	0.58	0.67	9.66	0.00	9.66	4.000	No	Yes	2.00
527	34.59	15.30	100.00	3.29	0.58	0.67	9.65	0.00	9.65	4.000	No	Yes	2.00
528	34.66	15.51	100.00	3.27	0.58	0.67	9.76	0.00	9.76	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	34.73	15.87	100.00	3.26	0.58	0.67	10.00	0.00	10.00	4.000	No	Yes	2.00
530	34.79	16.44	100.00	3.24	0.58	0.67	10.35	0.00	10.35	4.000	No	Yes	2.00
531	34.86	16.91	100.00	3.23	0.58	0.67	10.65	0.00	10.65	4.000	No	Yes	2.00
532	34.93	17.66	100.00	3.21	0.58	0.67	11.13	0.00	11.13	4.000	No	Yes	2.00
533	34.99	18.13	100.00	3.20	0.58	0.67	11.42	0.00	11.42	4.000	No	Yes	2.00
534	35.06	17.75	100.00	3.22	0.58	0.67	11.16	0.00	11.16	4.000	No	Yes	2.00
535	35.13	17.10	100.00	3.25	0.58	0.67	10.73	0.00	10.73	4.000	No	Yes	2.00
536	35.20	16.82	100.00	3.27	0.58	0.67	10.53	0.00	10.53	4.000	No	Yes	2.00
537	35.26	17.01	100.00	3.27	0.58	0.67	10.64	0.00	10.64	4.000	No	Yes	2.00
538	35.33	17.59	100.00	3.26	0.58	0.67	11.00	0.00	11.00	4.000	No	Yes	2.00
539	35.40	18.71	100.00	3.22	0.58	0.67	11.71	0.00	11.71	4.000	No	Yes	2.00
540	35.47	20.03	100.00	3.18	0.57	0.67	12.56	0.00	12.56	4.000	No	Yes	2.00
541	35.53	20.78	100.00	3.17	0.57	0.67	13.04	0.00	13.04	4.000	No	Yes	2.00
542	35.60	21.25	100.00	3.16	0.57	0.67	13.33	0.00	13.33	4.000	No	Yes	2.00
543	35.66	22.29	100.00	3.14	0.57	0.67	13.99	0.00	13.99	4.000	No	Yes	2.00
544	35.70	23.51	100.00	3.12	0.56	0.67	14.78	0.00	14.78	4.000	No	Yes	2.00
545	35.77	24.54	100.00	3.10	0.56	0.67	15.44	0.00	15.44	4.000	No	Yes	2.00
546	35.83	24.45	100.00	3.12	0.56	0.67	15.37	0.00	15.37	4.000	No	Yes	2.00
547	35.90	26.72	100.00	3.08	0.56	0.67	16.84	0.00	16.84	4.000	No	Yes	2.00
548	35.97	30.94	100.00	2.99	0.55	0.67	19.63	0.00	19.63	4.000	No	Yes	2.00
549	36.03	32.71	99.46	2.96	0.54	0.68	20.80	0.00	20.80	4.000	No	Yes	2.00
550	36.10	30.36	100.00	2.99	0.55	0.67	19.21	0.00	19.21	4.000	No	Yes	2.00
551	36.17	25.85	100.00	3.09	0.56	0.67	16.20	0.00	16.20	4.000	No	Yes	2.00
552	36.23	22.29	100.00	3.19	0.57	0.66	13.86	0.00	13.86	4.000	No	Yes	2.00
553	36.30	26.18	100.00	3.08	0.56	0.67	16.39	0.00	16.39	4.000	No	Yes	2.00
554	36.37	20.05	100.00	3.25	0.57	0.66	12.38	0.00	12.38	4.000	No	Yes	2.00
555	36.43	26.53	100.00	3.06	0.56	0.66	16.57	0.00	16.57	4.000	No	Yes	2.00
556	36.50	39.96	87.88	2.81	0.53	0.68	25.48	0.00	25.48	4.000	No	Yes	2.00
557	36.57	51.14	76.89	2.67	0.51	0.69	33.10	0.00	33.10	4.000	No	Yes	2.00
558	36.64	60.22	70.70	2.60	0.49	0.69	39.40	62.23	101.63	0.140	No	No	0.15
559	36.70	64.80	69.61	2.58	0.49	0.70	42.66	62.97	105.63	0.145	No	No	0.15
560	36.77	66.76	69.53	2.58	0.48	0.70	44.04	63.35	107.40	0.148	No	No	0.16
561	36.84	61.02	74.97	2.65	0.49	0.69	39.94	0.00	39.94	4.000	No	Yes	2.00
562	36.91	49.84	85.95	2.79	0.51	0.68	32.16	0.00	32.16	4.000	No	Yes	2.00
563	36.97	39.33	97.31	2.93	0.53	0.67	24.96	0.00	24.96	4.000	No	Yes	2.00
564	37.04	32.09	100.00	3.04	0.55	0.66	20.11	0.00	20.11	4.000	No	Yes	2.00
565	37.11	27.86	100.00	3.10	0.56	0.66	17.31	0.00	17.31	4.000	No	Yes	2.00
566	37.14	26.74	100.00	3.11	0.56	0.66	16.57	0.00	16.57	4.000	No	Yes	2.00
567	37.21	24.57	100.00	3.14	0.56	0.65	15.15	0.00	15.15	4.000	No	Yes	2.00
568	37.27	23.09	100.00	3.14	0.57	0.65	14.17	0.00	14.17	4.000	No	Yes	2.00
569	37.34	23.47	100.00	3.12	0.57	0.65	14.40	0.00	14.40	4.000	No	Yes	2.00
570	37.41	25.16	100.00	3.08	0.56	0.65	15.47	0.00	15.47	4.000	No	Yes	2.00
571	37.48	27.50	100.00	3.01	0.56	0.66	16.97	0.00	16.97	4.000	No	Yes	2.00
572	37.54	29.57	100.00	3.00	0.55	0.66	18.29	0.00	18.29	4.000	No	Yes	2.00
573	37.61	31.43	100.00	2.99	0.55	0.66	19.50	0.00	19.50	4.000	No	Yes	2.00
574	37.68	32.84	100.00	2.99	0.54	0.66	20.40	0.00	20.40	4.000	No	Yes	2.00
575	37.74	34.63	100.00	2.97	0.54	0.66	21.56	0.00	21.56	4.000	No	Yes	2.00
576	37.81	37.16	97.42	2.93	0.54	0.66	23.21	0.00	23.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
577	37.88	36.89	98.65	2.95	0.54	0.66	23.00	0.00	23.00	4.000	No	Yes	2.00
578	37.94	36.99	99.69	2.96	0.54	0.66	23.04	0.00	23.04	4.000	No	Yes	2.00
579	38.01	36.99	100.00	2.98	0.54	0.66	23.02	0.00	23.02	4.000	No	Yes	2.00
580	38.08	37.10	100.00	2.99	0.54	0.66	23.07	0.00	23.07	4.000	No	Yes	2.00
581	38.15	39.45	99.72	2.96	0.53	0.66	24.60	0.00	24.60	4.000	No	Yes	2.00
582	38.21	43.67	94.51	2.89	0.52	0.67	27.37	0.00	27.37	4.000	No	Yes	2.00
583	38.28	49.78	87.86	2.81	0.51	0.67	31.44	0.00	31.44	4.000	No	Yes	2.00
584	38.34	57.86	80.71	2.72	0.50	0.68	36.93	0.00	36.93	4.000	No	Yes	2.00
585	38.41	68.93	71.51	2.61	0.48	0.69	44.60	0.00	44.60	4.000	No	Yes	2.00
586	38.48	81.59	62.08	2.49	0.46	0.70	53.55	64.32	117.87	0.167	No	No	0.18
587	38.55	92.09	55.14	2.40	0.45	0.70	61.08	64.24	125.32	0.184	No	No	0.19
588	38.61	96.76	52.55	2.37	0.44	0.71	64.45	64.16	128.61	0.193	No	No	0.20
589	38.68	95.26	53.97	2.39	0.44	0.70	63.32	64.41	127.73	0.191	No	No	0.20
590	38.75	87.75	58.42	2.44	0.45	0.70	57.81	64.44	122.25	0.177	No	No	0.19
591	38.78	82.67	61.72	2.48	0.46	0.69	54.14	64.38	118.52	0.168	No	No	0.18
592	38.85	71.23	70.43	2.59	0.48	0.68	45.98	64.10	110.08	0.152	No	No	0.16
593	38.92	60.14	81.20	2.73	0.49	0.67	38.24	0.00	38.24	4.000	No	Yes	2.00
594	38.98	49.92	91.78	2.86	0.51	0.66	31.27	0.00	31.27	4.000	No	Yes	2.00
595	39.05	42.97	99.16	2.95	0.52	0.66	26.62	0.00	26.62	4.000	No	Yes	2.00
596	39.11	37.15	100.00	3.02	0.54	0.65	22.76	0.00	22.76	4.000	No	Yes	2.00
597	39.19	37.54	99.17	2.95	0.54	0.65	22.97	0.00	22.97	4.000	No	Yes	2.00
598	39.24	35.19	100.00	2.97	0.54	0.65	21.44	0.00	21.44	4.000	No	Yes	2.00
599	39.32	29.57	100.00	3.08	0.55	0.64	17.80	0.00	17.80	4.000	No	Yes	2.00
600	39.38	29.57	100.00	3.09	0.55	0.64	17.78	0.00	17.78	4.000	No	Yes	2.00
601	39.45	29.59	100.00	3.10	0.55	0.64	17.76	0.00	17.76	4.000	No	Yes	2.00
602	39.51	29.60	100.00	3.11	0.55	0.64	17.75	0.00	17.75	4.000	No	Yes	2.00
603	39.58	36.37	100.00	2.98	0.54	0.64	22.06	0.00	22.06	4.000	No	Yes	2.00
604	39.64	41.07	94.81	2.90	0.53	0.65	25.08	0.00	25.08	4.000	No	Yes	2.00
605	39.72	47.16	88.21	2.82	0.52	0.65	29.04	0.00	29.04	4.000	No	Yes	2.00
606	39.77	49.69	86.23	2.79	0.51	0.66	30.69	0.00	30.69	4.000	No	Yes	2.00
607	39.84	52.51	84.38	2.77	0.51	0.66	32.57	0.00	32.57	4.000	No	Yes	2.00
608	39.90	53.15	84.85	2.77	0.51	0.66	32.98	0.00	32.98	4.000	No	Yes	2.00
609	39.96	49.30	89.81	2.84	0.51	0.65	30.39	0.00	30.39	4.000	No	Yes	2.00
610	40.03	55.94	83.23	2.75	0.50	0.66	34.80	0.00	34.80	4.000	No	Yes	2.00
611	40.09	57.15	81.69	2.73	0.50	0.66	35.59	0.00	35.59	4.000	No	Yes	2.00
612	40.17	51.14	87.44	2.81	0.51	0.65	31.53	0.00	31.53	4.000	No	Yes	2.00
613	40.25	44.85	94.85	2.90	0.52	0.65	27.37	0.00	27.37	4.000	No	Yes	2.00
614	40.31	40.26	100.00	2.98	0.53	0.64	24.37	0.00	24.37	4.000	No	Yes	2.00
615	40.37	38.77	100.00	3.01	0.53	0.64	23.37	0.00	23.37	4.000	No	Yes	2.00
616	40.42	42.07	99.36	2.95	0.53	0.64	25.49	0.00	25.49	4.000	No	Yes	2.00
617	40.51	47.31	93.32	2.88	0.52	0.65	28.87	0.00	28.87	4.000	No	Yes	2.00
618	40.56	47.23	93.29	2.88	0.52	0.65	28.78	0.00	28.78	4.000	No	Yes	2.00
619	40.62	46.19	94.94	2.90	0.52	0.65	28.09	0.00	28.09	4.000	No	Yes	2.00
620	40.71	44.31	97.91	2.94	0.52	0.64	26.84	0.00	26.84	4.000	No	Yes	2.00
621	40.78	44.70	97.90	2.94	0.52	0.64	27.06	0.00	27.06	4.000	No	Yes	2.00
622	40.85	48.36	94.37	2.89	0.52	0.65	29.42	0.00	29.42	4.000	No	Yes	2.00
623	40.91	53.05	89.88	2.84	0.51	0.65	32.49	0.00	32.49	4.000	No	Yes	2.00
624	40.95	55.58	87.58	2.81	0.50	0.65	34.15	0.00	34.15	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	41.02	60.18	83.43	2.76	0.50	0.65	37.17	0.00	37.17	4.000	No	Yes	2.00
626	41.08	65.72	78.29	2.69	0.49	0.66	40.88	0.00	40.88	4.000	No	Yes	2.00
627	41.15	77.55	68.80	2.57	0.47	0.67	48.95	64.62	113.57	0.158	No	No	0.17
628	41.22	98.20	55.74	2.41	0.44	0.68	63.48	65.11	128.59	0.193	No	No	0.20
629	41.28	119.12	45.42	2.28	0.41	0.70	78.74	64.47	143.21	0.250	No	No	0.26
630	41.34	128.87	41.63	2.23	0.40	0.71	85.96	63.86	149.82	0.288	No	No	0.30
631	41.44	139.46	37.71	2.18	0.39	0.71	93.80	62.65	156.46	0.338	No	No	0.36
632	41.50	140.40	37.38	2.18	0.39	0.71	94.44	62.52	156.96	0.342	No	No	0.36
633	41.57	139.26	37.90	2.19	0.39	0.71	93.53	62.76	156.30	0.337	No	No	0.36
634	41.60	138.33	38.24	2.19	0.39	0.71	92.80	62.88	155.68	0.331	No	No	0.35
635	41.67	137.29	38.43	2.19	0.40	0.71	91.92	62.84	154.75	0.324	No	No	0.34
636	41.74	137.01	38.68	2.20	0.40	0.71	91.65	62.98	154.63	0.323	No	No	0.34
637	41.81	136.81	39.70	2.21	0.39	0.71	91.55	63.78	155.33	0.328	No	No	0.35
638	41.87	136.63	40.35	2.22	0.39	0.71	91.41	64.25	155.67	0.331	No	No	0.35
639	41.94	135.31	41.48	2.23	0.40	0.71	90.42	64.85	155.27	0.328	No	No	0.35
640	42.00	121.89	48.01	2.31	0.41	0.70	80.41	66.32	146.73	0.269	No	No	0.28
641	42.07	129.50	46.24	2.29	0.40	0.70	86.13	66.83	152.97	0.310	No	No	0.33
642	42.14	127.06	48.62	2.32	0.40	0.70	84.34	67.66	152.00	0.303	No	No	0.32
643	42.20	127.16	49.82	2.34	0.40	0.70	84.44	68.29	152.73	0.308	No	No	0.33
644	42.28	123.59	52.18	2.36	0.40	0.70	81.72	68.65	150.37	0.291	No	No	0.31
645	42.35	120.68	53.67	2.38	0.41	0.70	79.49	68.68	148.17	0.277	No	No	0.29
646	42.42	118.24	54.45	2.39	0.41	0.69	77.58	68.48	146.06	0.265	No	No	0.28
647	42.48	117.21	54.50	2.39	0.41	0.69	76.73	68.27	145.00	0.259	No	No	0.27
648	42.55	117.30	53.82	2.39	0.41	0.69	76.70	67.99	144.69	0.257	No	No	0.27
649	42.62	116.54	53.28	2.38	0.41	0.69	76.04	67.59	143.62	0.252	No	No	0.27
650	42.68	114.01	53.60	2.38	0.42	0.69	73.97	67.16	141.13	0.240	No	No	0.25
651	42.72	111.85	54.17	2.39	0.42	0.68	72.34	66.94	139.28	0.231	No	No	0.24
652	42.78	106.97	55.68	2.41	0.43	0.68	68.71	66.52	135.22	0.215	No	No	0.23
653	42.85	101.34	57.91	2.44	0.44	0.67	64.58	66.16	130.74	0.200	No	No	0.21
654	42.92	93.18	62.04	2.49	0.45	0.67	58.73	65.77	124.51	0.182	No	No	0.19
655	42.99	84.06	68.08	2.56	0.46	0.66	52.35	65.45	117.80	0.167	No	No	0.18
656	43.05	76.94	73.66	2.63	0.47	0.65	47.42	0.00	47.42	4.000	No	Yes	2.00
657	43.12	73.56	75.98	2.66	0.48	0.65	45.09	0.00	45.09	4.000	No	Yes	2.00
658	43.18	72.06	75.70	2.66	0.48	0.65	44.02	0.00	44.02	4.000	No	Yes	2.00
659	43.25	70.37	74.90	2.65	0.48	0.64	42.81	0.00	42.81	4.000	No	Yes	2.00
660	43.32	66.34	77.65	2.68	0.49	0.64	40.06	0.00	40.06	4.000	No	Yes	2.00
661	43.38	58.45	83.98	2.76	0.50	0.63	34.89	0.00	34.89	4.000	No	Yes	2.00
662	43.45	51.23	89.80	2.84	0.52	0.62	30.20	0.00	30.20	4.000	No	Yes	2.00
663	43.52	46.25	93.27	2.88	0.52	0.62	27.01	0.00	27.01	4.000	No	Yes	2.00
664	43.59	43.54	93.93	2.89	0.53	0.62	25.28	0.00	25.28	4.000	No	Yes	2.00
665	43.65	41.65	95.36	2.90	0.53	0.61	24.09	0.00	24.09	4.000	No	Yes	2.00
666	43.72	40.26	98.77	2.95	0.54	0.61	23.21	0.00	23.21	4.000	No	Yes	2.00
667	43.79	39.21	100.00	2.99	0.54	0.61	22.55	0.00	22.55	4.000	No	Yes	2.00
668	43.86	37.91	100.00	3.03	0.54	0.61	21.72	0.00	21.72	4.000	No	Yes	2.00
669	43.92	36.21	100.00	3.06	0.54	0.61	20.67	0.00	20.67	4.000	No	Yes	2.00
670	43.98	42.81	100.00	2.96	0.53	0.61	24.71	0.00	24.71	4.000	No	Yes	2.00
671	44.04	52.96	89.50	2.83	0.51	0.62	31.05	0.00	31.05	4.000	No	Yes	2.00
672	44.12	68.25	76.62	2.67	0.49	0.64	40.92	0.00	40.92	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
673	44.19	80.25	68.23	2.57	0.47	0.65	48.91	64.49	113.39	0.158	No	No	0.17
674	44.25	89.71	62.79	2.50	0.46	0.65	55.35	65.02	120.36	0.172	No	No	0.18
675	44.31	96.93	58.58	2.44	0.45	0.66	60.30	65.18	125.48	0.185	No	No	0.19
676	44.38	101.90	55.60	2.41	0.44	0.66	63.71	65.12	128.83	0.194	No	No	0.20
677	44.45	105.36	54.07	2.39	0.44	0.66	66.12	65.21	131.33	0.202	No	No	0.21
678	44.52	107.80	53.27	2.38	0.43	0.67	67.81	65.36	133.17	0.208	No	No	0.22
679	44.58	109.21	53.20	2.38	0.43	0.67	68.78	65.59	134.37	0.212	No	No	0.22
680	44.65	110.52	53.46	2.38	0.43	0.67	69.71	65.95	135.66	0.217	No	No	0.23
681	44.72	112.31	53.30	2.38	0.43	0.67	70.96	66.22	137.19	0.223	No	No	0.23
682	44.78	113.91	52.90	2.37	0.42	0.67	72.07	66.36	138.43	0.228	No	No	0.24
683	44.85	115.41	52.46	2.37	0.42	0.67	73.21	66.48	139.69	0.233	No	No	0.25
684	44.88	116.35	52.08	2.36	0.42	0.67	73.86	66.50	140.36	0.236	No	No	0.25
685	44.95	117.57	51.49	2.36	0.42	0.67	74.68	66.46	141.14	0.240	No	No	0.25
686	45.02	118.32	51.09	2.35	0.42	0.67	75.16	66.41	141.57	0.242	No	No	0.26
687	45.09	118.79	50.81	2.35	0.42	0.67	75.43	66.36	141.79	0.243	No	No	0.26
688	45.16	119.35	50.56	2.34	0.42	0.67	75.78	66.34	142.11	0.244	No	No	0.26
689	45.22	119.35	50.54	2.34	0.42	0.67	75.72	66.31	142.03	0.244	No	No	0.26
690	45.29	119.35	50.48	2.34	0.42	0.67	75.66	66.27	141.92	0.243	No	No	0.26
691	45.35	119.35	50.47	2.34	0.42	0.67	75.60	66.25	141.84	0.243	No	No	0.26
692	45.42	119.82	50.29	2.34	0.42	0.67	75.88	66.24	142.12	0.244	No	No	0.26
693	45.49	120.76	49.80	2.34	0.42	0.67	76.49	66.17	142.67	0.247	No	No	0.26
694	45.56	121.13	49.55	2.33	0.42	0.67	76.70	66.11	142.80	0.248	No	No	0.26
695	45.62	121.23	49.51	2.33	0.42	0.67	76.71	66.09	142.80	0.248	No	No	0.26
696	45.69	120.84	49.66	2.33	0.42	0.67	76.38	66.07	142.45	0.246	No	No	0.26
697	45.76	120.01	49.95	2.34	0.42	0.67	75.71	66.03	141.74	0.243	No	No	0.26
698	45.82	118.59	50.45	2.34	0.42	0.67	74.63	65.98	140.61	0.237	No	No	0.25
699	45.89	116.99	51.08	2.35	0.42	0.66	73.42	65.95	139.37	0.232	No	No	0.24
700	45.96	114.93	51.95	2.36	0.43	0.66	71.79	65.89	137.67	0.225	No	No	0.24
701	46.02	112.02	53.26	2.38	0.43	0.66	69.68	65.86	135.54	0.216	No	No	0.23
702	46.09	109.77	54.28	2.39	0.43	0.66	68.04	65.81	133.85	0.210	No	No	0.22
703	46.16	106.95	55.61	2.41	0.44	0.65	66.01	65.75	131.77	0.203	No	No	0.21
704	46.22	104.22	55.63	2.41	0.44	0.65	64.01	65.21	129.22	0.195	No	No	0.21
705	46.29	101.40	56.62	2.42	0.44	0.65	61.99	65.00	126.99	0.189	No	No	0.20
706	46.36	99.06	58.61	2.45	0.45	0.65	60.36	65.21	125.57	0.185	No	No	0.19
707	46.42	97.09	60.36	2.47	0.45	0.64	58.99	65.36	124.36	0.182	No	No	0.19
708	46.46	96.34	60.95	2.47	0.45	0.64	58.46	65.39	123.85	0.181	No	No	0.19
709	46.52	94.37	62.18	2.49	0.45	0.64	57.08	65.34	122.42	0.177	No	No	0.19
710	46.61	92.68	63.03	2.50	0.46	0.64	55.87	65.23	121.10	0.174	No	No	0.18
711	46.66	90.89	63.81	2.51	0.46	0.64	54.62	65.08	119.70	0.171	No	No	0.18
712	46.74	84.51	67.10	2.55	0.47	0.63	50.28	64.63	114.91	0.161	No	No	0.17
713	46.79	81.51	68.39	2.57	0.47	0.63	48.25	64.33	112.58	0.157	No	No	0.17
714	46.86	76.16	71.66	2.61	0.48	0.62	44.69	0.00	44.69	4.000	No	Yes	2.00
715	46.94	69.87	76.66	2.67	0.49	0.61	40.55	0.00	40.55	4.000	No	Yes	2.00
716	46.99	64.71	80.55	2.72	0.50	0.61	37.27	0.00	37.27	4.000	No	Yes	2.00
717	47.06	56.45	86.93	2.80	0.51	0.60	32.09	0.00	32.09	4.000	No	Yes	2.00
718	47.14	47.25	95.50	2.91	0.53	0.59	26.40	0.00	26.40	4.000	No	Yes	2.00
719	47.19	41.81	100.00	2.99	0.54	0.59	23.12	0.00	23.12	4.000	No	Yes	2.00
720	47.25	37.22	100.00	3.06	0.54	0.58	20.37	0.00	20.37	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	47.34	37.04	100.00	3.06	0.54	0.58	20.25	0.00	20.25	4.000	No	Yes	2.00
722	47.39	37.05	100.00	3.05	0.54	0.58	20.23	0.00	20.23	4.000	No	Yes	2.00
723	47.45	36.87	100.00	3.04	0.55	0.58	20.11	0.00	20.11	4.000	No	Yes	2.00
724	47.51	48.63	90.46	2.84	0.52	0.59	27.05	0.00	27.05	4.000	No	Yes	2.00
725	47.58	65.24	74.20	2.64	0.50	0.60	37.22	0.00	37.22	4.000	No	Yes	2.00
726	47.65	75.17	66.32	2.54	0.49	0.61	43.49	62.50	105.99	0.146	No	No	0.15
727	47.72	77.32	66.34	2.54	0.48	0.61	44.88	62.90	107.78	0.149	No	No	0.16
728	47.78	73.83	71.63	2.61	0.49	0.61	42.67	0.00	42.67	4.000	No	Yes	2.00
729	47.85	66.51	79.98	2.71	0.50	0.61	38.01	0.00	38.01	4.000	No	Yes	2.00
730	47.91	59.10	87.43	2.81	0.51	0.60	33.40	0.00	33.40	4.000	No	Yes	2.00
731	47.98	51.22	94.39	2.89	0.52	0.59	28.53	0.00	28.53	4.000	No	Yes	2.00
732	48.05	45.78	98.39	2.94	0.53	0.58	25.23	0.00	25.23	4.000	No	Yes	2.00
733	48.11	41.18	100.00	2.99	0.54	0.58	22.47	0.00	22.47	4.000	No	Yes	2.00
734	48.18	37.24	100.00	3.05	0.55	0.57	20.14	0.00	20.14	4.000	No	Yes	2.00
735	48.24	34.91	100.00	3.09	0.55	0.57	18.77	0.00	18.77	4.000	No	Yes	2.00
736	48.31	33.88	100.00	3.11	0.55	0.57	18.15	0.00	18.15	4.000	No	Yes	2.00
737	48.38	33.60	100.00	3.11	0.55	0.57	17.98	0.00	17.98	4.000	No	Yes	2.00
738	48.45	35.30	100.00	3.10	0.55	0.57	18.93	0.00	18.93	4.000	No	Yes	2.00
739	48.52	42.16	100.00	3.00	0.54	0.58	22.92	0.00	22.92	4.000	No	Yes	2.00
740	48.58	62.16	84.30	2.77	0.50	0.60	34.98	0.00	34.98	4.000	No	Yes	2.00
741	48.65	89.57	66.33	2.54	0.46	0.62	52.53	65.10	117.63	0.166	No	No	0.18
742	48.72	110.85	56.48	2.42	0.43	0.64	66.94	66.32	133.26	0.208	No	No	0.22
743	48.78	125.30	51.16	2.35	0.41	0.65	77.21	66.99	144.20	0.255	No	No	0.27
744	48.85	138.80	46.18	2.29	0.40	0.66	86.91	67.00	153.91	0.317	No	No	0.33
745	48.92	150.71	41.72	2.23	0.38	0.67	95.55	66.28	161.83	0.391	No	No	0.41
746	48.95	155.41	39.87	2.21	0.38	0.67	98.94	65.69	164.63	0.425	No	No	0.45
747	49.02	160.66	35.19	2.15	0.38	0.67	102.17	62.18	164.36	0.421	No	No	0.45
748	49.09	164.70	31.25	2.10	0.38	0.67	104.37	58.10	162.47	0.399	No	No	0.42
749	49.16	169.48	34.11	2.14	0.37	0.68	108.84	62.51	171.35	0.528	No	No	0.56
750	49.23	175.76	31.59	2.11	0.37	0.68	113.21	60.41	173.61	0.571	No	No	0.60
751	49.29	182.14	31.16	2.10	0.36	0.69	118.23	60.88	179.11	0.702	No	No	0.74
752	49.35	179.04	33.36	2.13	0.36	0.69	116.24	63.26	179.50	0.713	No	No	0.75
753	49.42	188.79	31.91	2.11	0.35	0.69	123.85	63.08	186.92	0.976	No	No	1.03
754	49.49	197.70	30.08	2.09	0.34	0.70	130.68	61.90	192.58	1.276	No	No	1.34
755	49.56	202.50	29.33	2.08	0.34	0.70	134.40	61.49	195.88	1.512	No	No	1.57
756	49.62	206.91	27.35	2.05	0.34	0.70	137.27	58.69	195.96	1.518	No	No	1.58
757	49.69	211.60	24.88	2.02	0.34	0.70	139.99	54.36	194.35	1.396	No	No	1.46
758	49.76	216.95	23.50	2.01	0.34	0.70	143.71	51.92	195.63	1.491	No	No	1.55
759	49.82	221.45	22.41	1.99	0.34	0.70	146.81	49.80	196.62	1.571	No	No	1.63
760	49.89	224.35	21.88	1.99	0.33	0.70	148.88	48.77	197.65	1.662	No	No	1.72
761	49.95	229.23	20.81	1.97	0.33	0.70	152.26	46.37	198.63	1.753	No	No	1.82
762	50.00	220.32	23.07	2.00	0.33	0.70	146.03	51.29	197.32	4.000	No	No	2.00
763	50.07	227.81	21.15	1.98	0.33	0.70	151.11	47.15	198.26	4.000	No	No	2.00
764	50.14	231.84	19.88	1.96	0.33	0.70	153.52	43.90	197.42	4.000	No	No	2.00
765	50.20	232.78	19.48	1.96	0.34	0.70	153.91	42.74	196.65	4.000	No	No	2.00
766	50.28	232.40	19.43	1.96	0.34	0.70	153.41	42.52	195.93	4.000	No	No	2.00
767	50.35	228.74	19.98	1.96	0.34	0.70	150.60	43.79	194.39	4.000	No	No	2.00
768	50.41	224.14	21.08	1.98	0.34	0.70	147.38	46.42	193.80	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
769	50.48	218.33	22.78	2.00	0.34	0.70	143.47	50.19	193.66	4.000	No	No	2.00
770	50.55	213.81	23.95	2.01	0.34	0.69	140.23	52.38	192.61	4.000	No	No	2.00
771	50.61	211.75	24.71	2.02	0.34	0.69	138.82	53.80	192.62	4.000	No	No	2.00
772	50.68	212.78	24.21	2.02	0.34	0.69	139.33	52.80	192.13	4.000	No	No	2.00
773	50.74	213.06	23.13	2.00	0.35	0.69	138.83	50.27	189.10	4.000	No	No	2.00
774	50.81	209.58	23.04	2.00	0.35	0.69	135.73	49.56	185.29	4.000	No	No	2.00
775	50.88	202.35	24.47	2.02	0.36	0.68	130.39	51.84	182.23	4.000	No	No	2.00
776	50.94	191.65	27.19	2.05	0.36	0.68	122.72	55.66	178.38	4.000	No	No	2.00
777	51.01	178.98	30.50	2.09	0.37	0.67	113.51	59.00	172.51	4.000	No	No	2.00
778	51.08	167.43	33.68	2.13	0.38	0.66	105.08	61.20	166.29	4.000	No	No	2.00
779	51.15	158.33	36.44	2.17	0.39	0.66	98.47	62.58	161.05	4.000	No	No	2.00
780	51.21	151.76	38.43	2.19	0.39	0.65	93.68	63.25	156.93	4.000	No	No	2.00
781	51.28	145.47	41.22	2.23	0.40	0.65	89.24	64.37	153.62	4.000	No	No	2.00
782	51.34	140.03	43.31	2.25	0.40	0.64	85.34	64.84	150.19	4.000	No	No	2.00
783	51.38	137.31	44.49	2.27	0.41	0.64	83.41	65.10	148.51	4.000	No	No	2.00
784	51.45	132.61	46.83	2.30	0.41	0.64	80.11	65.61	145.72	4.000	No	No	2.00
785	51.51	129.61	48.18	2.31	0.41	0.64	77.97	65.76	143.73	4.000	No	No	2.00
786	51.58	127.27	47.86	2.31	0.42	0.63	76.18	65.13	141.31	4.000	No	No	2.00
787	51.65	125.48	43.90	2.26	0.43	0.63	74.44	62.48	136.92	4.000	No	No	2.00
788	51.71	123.70	46.25	2.29	0.43	0.63	73.34	63.55	136.89	4.000	No	No	2.00
789	51.78	123.61	47.36	2.30	0.42	0.63	73.33	64.13	137.46	4.000	No	No	2.00
790	51.85	122.85	48.86	2.32	0.42	0.63	72.86	64.76	137.62	4.000	No	No	2.00
791	51.92	123.51	49.19	2.33	0.42	0.63	73.31	65.04	138.35	4.000	No	No	2.00
792	51.99	124.07	48.94	2.32	0.42	0.63	73.64	65.01	138.65	4.000	No	No	2.00
793	52.05	124.64	48.39	2.32	0.42	0.63	73.95	64.82	138.78	4.000	No	No	2.00
794	52.11	125.11	47.97	2.31	0.42	0.63	74.21	64.68	138.89	4.000	No	No	2.00
795	52.18	122.95	48.80	2.32	0.43	0.63	72.68	64.69	137.36	4.000	No	No	2.00
796	52.24	120.70	49.73	2.33	0.43	0.62	71.09	64.71	135.81	4.000	No	No	2.00
797	52.31	118.35	50.79	2.35	0.43	0.62	69.32	64.72	134.05	4.000	No	No	2.00
798	52.38	115.53	52.18	2.36	0.44	0.62	67.39	64.80	132.20	4.000	No	No	2.00
799	52.44	110.65	55.08	2.40	0.44	0.61	64.13	65.05	129.18	4.000	No	No	2.00
800	52.51	105.12	58.92	2.45	0.45	0.61	60.49	65.34	125.83	4.000	No	No	2.00
801	52.58	104.93	59.56	2.46	0.45	0.61	60.35	65.50	125.85	4.000	No	No	2.00
802	52.64	104.93	59.87	2.46	0.45	0.61	60.32	65.59	125.90	4.000	No	No	2.00
803	52.71	104.74	60.03	2.46	0.45	0.61	60.15	65.59	125.74	4.000	No	No	2.00
804	52.78	107.75	58.38	2.44	0.44	0.61	62.09	65.62	127.71	4.000	No	No	2.00
805	52.84	108.78	57.73	2.43	0.44	0.61	62.72	65.58	128.30	4.000	No	No	2.00
806	52.91	107.75	57.86	2.44	0.44	0.61	61.98	65.42	127.40	4.000	No	No	2.00
807	52.98	106.62	58.04	2.44	0.45	0.61	61.20	65.26	126.46	4.000	No	No	2.00
808	53.04	107.75	57.14	2.43	0.44	0.61	61.90	65.16	127.06	4.000	No	No	2.00
809	53.11	110.65	55.31	2.40	0.44	0.61	63.77	65.03	128.80	4.000	No	No	2.00
810	53.17	115.44	52.63	2.37	0.44	0.61	66.90	64.85	131.75	4.000	No	No	2.00
811	53.24	123.79	48.35	2.32	0.43	0.62	72.58	64.44	137.02	4.000	No	No	2.00
812	53.31	134.30	43.17	2.25	0.42	0.63	79.62	63.32	142.94	4.000	No	No	2.00
813	53.38	145.20	38.16	2.19	0.41	0.63	86.92	61.43	148.35	4.000	No	No	2.00
814	53.42	151.86	35.74	2.16	0.40	0.64	91.46	60.30	151.76	4.000	No	No	2.00
815	53.49	161.25	33.13	2.13	0.39	0.64	98.01	59.03	157.03	4.000	No	No	2.00
816	53.56	171.38	30.50	2.09	0.38	0.65	105.11	57.27	162.38	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	53.63	183.30	26.98	2.05	0.38	0.65	113.22	53.52	166.74	4.000	No	No	2.00
818	53.68	191.75	24.67	2.02	0.37	0.66	118.89	50.27	169.16	4.000	No	No	2.00
819	53.75	201.70	22.65	2.00	0.37	0.66	125.79	47.08	172.87	4.000	No	No	2.00
820	53.82	207.23	22.37	1.99	0.36	0.66	130.12	47.10	177.22	4.000	No	No	2.00
821	53.89	211.46	22.81	2.00	0.36	0.67	133.89	48.74	182.62	4.000	No	No	2.00
822	53.94	214.55	20.18	1.96	0.36	0.66	134.52	42.16	176.68	4.000	No	No	2.00
823	54.00	201.60	18.87	1.95	0.39	0.64	122.84	37.00	159.84	4.000	No	No	2.00
824	54.07	215.87	15.33	1.90	0.39	0.64	131.01	26.78	157.78	4.000	No	No	2.00
825	54.15	224.31	15.27	1.90	0.38	0.65	137.79	27.19	164.98	4.000	No	No	2.00
826	54.21	230.41	15.11	1.90	0.37	0.66	142.62	27.01	169.63	4.000	No	No	2.00
827	54.27	234.73	15.48	1.91	0.37	0.66	146.63	28.68	175.31	4.000	No	No	2.00
828	54.34	232.34	17.39	1.93	0.36	0.67	146.66	35.25	181.91	4.000	No	No	2.00
829	54.40	229.94	18.87	1.95	0.35	0.67	146.04	39.87	185.91	4.000	No	No	2.00
830	54.47	240.08	17.17	1.93	0.35	0.67	152.97	35.22	188.19	4.000	No	No	2.00
831	54.53	244.86	16.77	1.92	0.34	0.68	156.61	34.22	190.82	4.000	No	No	2.00
832	54.60	249.46	16.94	1.92	0.34	0.68	160.77	35.24	196.01	4.000	No	No	2.00
833	54.67	253.50	16.98	1.92	0.33	0.69	164.33	35.75	200.07	4.000	No	No	2.00
834	54.73	257.63	16.75	1.92	0.33	0.69	167.67	35.29	202.97	4.000	No	No	2.00
835	54.80	261.66	16.42	1.92	0.33	0.69	170.81	34.41	205.23	4.000	No	No	2.00
836	54.87	265.14	16.06	1.91	0.32	0.69	173.42	33.32	206.73	4.000	No	No	2.00
837	54.93	268.04	15.88	1.91	0.32	0.70	176.30	32.90	209.20	4.000	No	No	2.00
838	54.99	270.67	15.81	1.91	0.32	0.70	178.58	32.86	211.43	4.000	No	No	2.00
839	55.05	273.58	15.78	1.91	0.31	0.70	181.16	32.96	214.12	4.000	No	No	2.00
840	55.12	276.58	15.47	1.91	0.31	0.70	183.45	31.98	215.43	4.000	No	No	2.00
841	55.19	279.11	15.28	1.90	0.31	0.70	185.46	31.37	216.83	4.000	No	No	2.00
842	55.26	281.36	15.06	1.90	0.31	0.70	187.17	30.65	217.81	4.000	No	No	2.00
843	55.33	282.86	14.99	1.90	0.31	0.70	188.39	30.46	218.85	4.000	No	No	2.00
844	55.39	283.14	15.12	1.90	0.31	0.71	188.80	31.00	219.80	4.000	No	No	2.00
845	55.45	282.58	15.36	1.90	0.30	0.71	188.59	31.95	220.54	4.000	No	No	2.00
846	55.52	282.59	15.50	1.91	0.30	0.71	188.75	32.57	221.32	4.000	No	No	2.00
847	55.59	282.59	14.83	1.90	0.31	0.70	187.66	29.73	217.39	4.000	No	No	2.00
848	55.64	280.62	13.83	1.89	0.32	0.69	184.23	25.36	209.58	4.000	No	No	2.00
849	55.72	277.90	14.48	1.89	0.32	0.70	182.66	27.90	210.56	4.000	No	No	2.00
850	55.79	274.33	15.22	1.90	0.32	0.70	180.42	30.69	211.11	4.000	No	No	2.00
851	55.86	269.83	16.09	1.91	0.32	0.70	177.48	33.83	211.31	4.000	No	No	2.00
852	55.92	263.91	17.12	1.93	0.32	0.70	173.38	37.24	210.63	4.000	No	No	2.00
853	55.98	219.34	27.54	2.06	0.33	0.69	141.99	59.92	201.91	4.000	No	No	2.00
854	56.05	247.87	20.01	1.96	0.32	0.69	161.55	45.35	206.89	4.000	No	No	2.00
855	56.11	246.27	19.99	1.96	0.33	0.69	160.06	45.08	205.14	4.000	No	No	2.00
856	56.18	244.40	20.05	1.96	0.33	0.69	158.41	45.05	203.47	4.000	No	No	2.00
857	56.24	243.18	20.25	1.97	0.33	0.69	157.48	45.51	202.99	4.000	No	No	2.00
858	56.31	244.49	19.53	1.96	0.33	0.68	157.88	43.40	201.28	4.000	No	No	2.00
859	56.37	244.86	19.19	1.95	0.33	0.68	157.82	42.34	200.15	4.000	No	No	2.00
860	56.45	244.58	18.97	1.95	0.33	0.68	157.30	41.61	198.91	4.000	No	No	2.00
861	56.51	246.65	18.26	1.94	0.33	0.68	158.31	39.45	197.77	4.000	No	No	2.00
862	56.58	246.84	17.98	1.94	0.34	0.68	158.12	38.49	196.61	4.000	No	No	2.00
863	56.64	247.21	17.79	1.93	0.34	0.68	158.18	37.88	196.06	4.000	No	No	2.00
864	56.71	247.96	17.80	1.93	0.34	0.68	158.80	37.97	196.77	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	56.78	249.56	17.70	1.93	0.33	0.68	160.04	37.79	197.83	4.000	No	No	2.00
866	56.84	251.15	17.49	1.93	0.33	0.68	161.15	37.20	198.34	4.000	No	No	2.00
867	56.91	251.43	17.54	1.93	0.33	0.68	161.40	37.39	198.79	4.000	No	No	2.00
868	56.98	251.15	17.89	1.94	0.33	0.68	161.50	38.58	200.08	4.000	No	No	2.00
869	57.05	251.15	18.17	1.94	0.33	0.68	161.78	39.58	201.35	4.000	No	No	2.00
870	57.11	252.46	18.06	1.94	0.33	0.68	162.77	39.31	202.08	4.000	No	No	2.00
871	57.18	252.74	10.99	1.85	0.38	0.64	153.71	12.59	166.31	4.000	No	No	2.00
872	57.24	253.02	6.26	1.79	0.40	0.63	149.47	0.94	150.42	4.000	No	No	2.00
873	57.31	251.61	8.16	1.81	0.40	0.63	149.44	3.99	153.43	4.000	No	No	2.00
874	57.38	250.30	9.95	1.84	0.39	0.63	150.19	8.95	159.14	4.000	No	No	2.00
875	57.45	249.83	11.24	1.85	0.38	0.64	151.39	13.39	164.77	4.000	No	No	2.00
876	57.48	249.27	11.85	1.86	0.38	0.64	151.71	15.61	167.32	4.000	No	No	2.00
877	57.56	248.66	12.69	1.87	0.37	0.65	152.28	18.80	171.08	4.000	No	No	2.00
878	57.62	248.66	13.05	1.88	0.37	0.65	152.72	20.18	172.90	4.000	No	No	2.00
879	57.71	248.06	14.02	1.89	0.36	0.65	153.44	23.89	177.33	4.000	No	No	2.00
880	57.77	247.76	15.15	1.90	0.36	0.66	154.63	28.20	182.84	4.000	No	No	2.00
881	57.84	245.79	15.93	1.91	0.35	0.66	153.88	30.99	184.87	4.000	No	No	2.00
882	57.91	243.07	16.56	1.92	0.35	0.66	152.26	33.05	185.31	4.000	No	No	2.00
883	57.97	238.57	17.80	1.93	0.35	0.66	149.75	36.94	186.68	4.000	No	No	2.00
884	58.01	235.66	18.57	1.94	0.35	0.66	148.04	39.20	187.24	4.000	No	No	2.00
885	58.08	229.37	20.19	1.96	0.35	0.67	144.17	43.50	187.67	4.000	No	No	2.00
886	58.14	225.80	21.11	1.98	0.35	0.66	141.88	45.70	187.58	4.000	No	No	2.00
887	58.21	223.36	21.60	1.98	0.35	0.66	140.17	46.74	186.90	4.000	No	No	2.00
888	58.28	221.49	21.85	1.99	0.35	0.66	138.74	47.17	185.90	4.000	No	No	2.00
889	58.34	221.86	21.38	1.98	0.35	0.66	138.64	45.94	184.57	4.000	No	No	2.00
890	58.41	227.21	19.55	1.96	0.36	0.66	141.53	41.32	182.85	4.000	No	No	2.00
891	58.48	236.13	16.73	1.92	0.36	0.65	146.13	32.99	179.12	4.000	No	No	2.00
892	58.54	242.13	14.85	1.90	0.37	0.65	148.88	26.62	175.49	4.000	No	No	2.00
893	58.61	247.01	13.71	1.88	0.37	0.65	151.46	22.59	174.05	4.000	No	No	2.00
894	58.67	250.58	9.93	1.84	0.39	0.63	149.35	8.87	158.22	4.000	No	No	2.00
895	58.74	252.36	2.94	1.75	0.41	0.62	147.32	0.00	147.32	4.000	No	No	2.00
896	58.80	255.46	3.19	1.75	0.41	0.62	149.80	0.00	149.80	4.000	No	No	2.00
897	58.87	256.96	5.32	1.78	0.40	0.62	151.10	0.30	151.40	4.000	No	No	2.00
898	58.94	259.13	6.81	1.80	0.40	0.63	153.34	1.58	154.92	4.000	No	No	2.00
899	59.01	262.98	8.11	1.81	0.39	0.63	157.44	3.98	161.41	4.000	No	No	2.00
900	59.07	262.69	9.84	1.84	0.38	0.64	159.06	8.83	167.89	4.000	No	No	2.00
901	59.13	262.41	11.18	1.85	0.37	0.65	160.57	13.53	174.10	4.000	No	No	2.00
902	59.22	273.96	9.90	1.84	0.36	0.65	168.67	9.30	177.96	4.000	No	No	2.00
903	59.28	279.12	10.40	1.84	0.35	0.66	173.81	11.18	185.00	4.000	No	No	2.00
904	59.32	281.37	10.68	1.85	0.35	0.66	176.18	12.28	188.46	4.000	No	No	2.00
905	59.38	285.13	11.05	1.85	0.34	0.67	180.67	13.85	194.52	4.000	No	No	2.00
906	59.45	288.41	11.19	1.85	0.33	0.67	183.82	14.52	198.33	4.000	No	No	2.00
907	59.52	292.91	10.86	1.85	0.33	0.68	187.34	13.38	200.71	4.000	No	No	2.00
908	59.59	297.99	10.23	1.84	0.33	0.68	190.92	11.10	202.02	4.000	No	No	2.00
909	59.65	302.12	7.47	1.81	0.34	0.67	191.08	2.92	194.00	4.000	No	No	2.00
910	59.72	303.90	2.68	1.75	0.34	0.67	191.33	0.00	191.33	4.000	No	No	2.00
911	59.79	302.12	2.67	1.75	0.34	0.66	189.65	0.00	189.65	4.000	No	No	2.00
912	59.85	302.11	3.24	1.75	0.34	0.66	189.59	0.00	189.59	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
913	59.92	301.08	4.18	1.76	0.35	0.66	188.61	0.04	188.65	4.000	No	No	2.00
914	59.98	299.58	4.97	1.77	0.35	0.66	186.58	0.20	186.77	4.000	No	No	2.00
915	60.04	251.34	15.31	1.90	0.35	0.66	156.20	28.95	185.15	4.000	No	No	2.00
916	60.11	288.76	6.75	1.80	0.36	0.65	177.53	1.61	179.15	4.000	No	No	2.00
917	60.19	286.90	7.19	1.80	0.36	0.65	176.12	2.29	178.41	4.000	No	No	2.00
918	60.25	283.33	7.96	1.81	0.36	0.65	173.61	3.81	177.42	4.000	No	No	2.00
919	60.32	277.14	9.44	1.83	0.36	0.65	169.87	7.82	177.69	4.000	No	No	2.00
920	60.38	269.91	11.19	1.85	0.36	0.65	166.02	13.82	179.83	4.000	No	No	2.00
921	60.46	264.19	12.32	1.87	0.36	0.65	162.69	17.94	180.63	4.000	No	No	2.00
922	60.51	262.22	12.34	1.87	0.36	0.65	160.99	17.94	178.92	4.000	No	No	2.00
923	60.57	259.78	12.30	1.87	0.36	0.65	158.80	17.69	176.48	4.000	No	No	2.00
924	60.65	255.18	12.86	1.87	0.37	0.65	155.62	19.62	175.24	4.000	No	No	2.00
925	60.70	251.61	13.53	1.88	0.37	0.65	153.50	22.03	175.52	4.000	No	No	2.00
926	60.77	247.67	14.04	1.89	0.37	0.64	150.82	23.77	174.59	4.000	No	No	2.00
927	60.83	245.79	14.01	1.89	0.37	0.64	149.15	23.53	172.68	4.000	No	No	2.00
928	60.92	243.73	13.90	1.89	0.37	0.64	147.21	23.00	170.21	4.000	No	No	2.00
929	60.99	245.56	13.41	1.88	0.38	0.64	148.03	21.22	169.25	4.000	No	No	2.00
930	61.05	243.54	13.91	1.89	0.37	0.64	146.97	23.02	170.00	4.000	No	No	2.00
931	61.12	245.32	13.51	1.88	0.37	0.64	147.86	21.58	169.44	4.000	No	No	2.00
932	61.19	247.20	13.08	1.88	0.38	0.64	148.80	20.04	168.83	4.000	No	No	2.00
933	61.22	248.14	12.87	1.87	0.38	0.64	149.26	19.27	168.53	4.000	No	No	2.00
934	61.29	248.05	12.91	1.87	0.38	0.64	149.19	19.42	168.61	4.000	No	No	2.00
935	61.35	247.76	13.00	1.87	0.38	0.64	149.03	19.76	168.79	4.000	No	No	2.00
936	61.42	247.86	13.00	1.88	0.38	0.64	149.07	19.78	168.85	4.000	No	No	2.00
937	61.50	247.86	13.04	1.88	0.38	0.64	149.06	19.90	168.95	4.000	No	No	2.00
938	61.55	247.86	13.27	1.88	0.37	0.64	149.34	20.78	170.12	4.000	No	No	2.00
939	61.62	250.39	13.42	1.88	0.37	0.64	151.62	21.49	173.11	4.000	No	No	2.00
940	61.69	251.89	13.93	1.89	0.36	0.65	153.55	23.54	177.10	4.000	No	No	2.00
941	61.75	251.33	14.75	1.90	0.36	0.65	154.17	26.68	180.85	4.000	No	No	2.00
942	61.81	247.76	16.38	1.92	0.35	0.65	153.21	32.51	185.72	4.000	No	No	2.00
943	61.89	250.77	16.53	1.92	0.35	0.66	155.93	33.30	189.24	4.000	No	No	2.00
944	61.94	253.97	16.69	1.92	0.34	0.66	158.86	34.15	193.01	4.000	No	No	2.00
945	62.03	258.85	17.04	1.93	0.33	0.67	163.52	35.88	199.41	4.000	No	No	2.00
946	62.09	262.88	17.07	1.93	0.32	0.68	167.70	36.43	204.13	4.000	No	No	2.00
947	62.15	266.82	17.33	1.93	0.32	0.68	171.57	37.77	209.34	4.000	No	No	2.00
948	62.21	269.92	17.83	1.94	0.31	0.69	175.03	39.93	214.96	4.000	No	No	2.00
949	62.27	273.77	17.55	1.93	0.31	0.69	178.16	39.30	217.46	4.000	No	No	2.00
950	62.34	270.95	18.54	1.94	0.31	0.69	176.82	42.62	219.44	4.000	No	No	2.00
951	62.42	278.46	17.05	1.93	0.31	0.69	181.70	37.87	219.57	4.000	No	No	2.00
952	62.49	284.94	16.87	1.92	0.30	0.70	187.46	37.80	225.26	4.000	No	No	2.00
953	62.54	281.65	17.53	1.93	0.30	0.70	185.28	40.02	225.29	4.000	No	No	2.00
954	62.60	282.31	16.10	1.91	0.31	0.69	183.71	34.44	218.15	4.000	No	No	2.00
955	62.67	282.12	15.28	1.90	0.31	0.68	182.20	31.09	213.29	4.000	No	No	2.00
956	62.74	279.40	14.21	1.89	0.32	0.67	177.90	26.43	204.33	4.000	No	No	2.00
957	62.80	265.32	15.50	1.91	0.33	0.67	167.15	30.59	197.74	4.000	No	No	2.00
958	62.87	239.70	20.53	1.97	0.34	0.66	150.08	45.29	195.37	4.000	No	No	2.00
959	62.95	210.70	24.09	2.01	0.36	0.64	128.39	50.70	179.10	4.000	No	No	2.00
960	63.01	189.20	25.97	2.04	0.38	0.63	112.17	51.56	163.74	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	63.08	167.99	36.24	2.17	0.39	0.63	99.24	62.56	161.80	4.000	No	No	2.00
962	63.14	150.26	45.63	2.28	0.40	0.62	87.51	66.83	154.33	4.000	No	No	2.00
963	63.21	137.68	53.74	2.38	0.41	0.61	79.13	68.61	147.74	4.000	No	No	2.00
964	63.28	129.53	60.42	2.47	0.42	0.60	73.75	69.53	143.27	4.000	No	No	2.00
965	63.33	130.39	62.68	2.50	0.41	0.60	74.45	70.41	144.86	4.000	No	No	2.00
966	63.39	131.24	64.99	2.52	0.41	0.61	75.16	71.26	146.42	4.000	No	No	2.00
967	63.46	136.78	64.26	2.52	0.40	0.61	79.06	72.17	151.24	4.000	No	No	2.00
968	63.53	131.99	67.41	2.56	0.41	0.61	75.76	72.06	147.83	4.000	No	No	2.00
969	63.59	126.83	70.82	2.60	0.41	0.60	72.23	71.84	144.07	4.000	No	No	2.00
970	63.66	124.39	72.99	2.62	0.42	0.60	70.58	0.00	70.58	4.000	No	Yes	2.00
971	63.72	128.99	71.67	2.61	0.41	0.61	73.74	0.00	73.74	4.000	No	Yes	2.00
972	63.79	139.60	67.10	2.55	0.40	0.62	81.14	73.54	154.67	4.000	No	No	2.00
973	63.85	152.92	60.66	2.47	0.38	0.63	90.62	74.34	164.96	4.000	No	No	2.00
974	63.92	172.43	51.60	2.36	0.36	0.64	104.84	74.58	179.42	4.000	No	No	2.00
975	63.99	188.39	43.59	2.26	0.35	0.65	116.43	72.83	189.26	4.000	No	No	2.00
976	64.05	204.06	36.17	2.16	0.34	0.66	127.60	68.99	196.59	4.000	No	No	2.00
977	64.11	218.22	30.06	2.09	0.33	0.67	137.26	63.21	200.47	4.000	No	No	2.00
978	64.19	241.31	20.53	1.97	0.34	0.66	150.56	45.35	195.91	4.000	No	No	2.00
979	64.26	253.98	14.77	1.90	0.36	0.64	154.55	26.78	181.33	4.000	No	No	2.00
980	64.33	265.05	5.17	1.78	0.40	0.61	153.14	0.24	153.38	4.000	No	No	2.00
981	64.39	276.60	0.00	1.68	0.39	0.62	162.59	0.00	162.59	4.000	No	No	2.00
982	64.46	287.86	0.00	1.66	0.37	0.63	172.14	0.00	172.14	4.000	No	No	2.00
983	64.53	298.09	0.00	1.64	0.36	0.64	180.99	0.00	180.99	4.000	No	No	2.00
984	64.60	303.90	0.00	1.64	0.35	0.65	186.85	0.00	186.85	4.000	No	No	2.00
985	64.66	298.46	0.00	1.66	0.36	0.64	181.21	0.00	181.21	4.000	No	No	2.00
986	64.70	299.67	0.00	1.67	0.35	0.65	182.97	0.00	182.97	4.000	No	No	2.00
987	64.78	296.10	0.00	1.70	0.36	0.64	179.04	0.00	179.04	4.000	No	No	2.00
988	64.85	300.89	0.00	1.71	0.35	0.65	183.94	0.00	183.94	4.000	No	No	2.00
989	64.91	309.53	0.00	1.63	0.34	0.66	191.70	0.00	191.70	4.000	No	No	2.00
990	64.97	326.79	0.00	1.54	0.32	0.67	207.69	0.00	207.69	4.000	No	No	2.00
991	65.04	349.04	0.00	1.52	0.29	0.69	229.16	0.00	229.16	4.000	No	No	2.00
992	65.11	371.29	0.00	1.50	0.27	0.72	251.61	0.00	251.61	4.000	No	No	2.00
993	65.16	381.70	0.00	1.48	0.26	0.72	260.13	0.00	260.13	4.000	No	No	2.00
994	65.22	392.12	0.00	1.46	0.26	0.72	267.20	0.00	267.20	4.000	No	No	2.00
995	65.29	390.97	0.00	1.45	0.26	0.72	266.38	0.00	266.38	4.000	No	No	2.00
996	65.36	398.67	0.00	1.44	0.26	0.72	271.59	0.00	271.59	4.000	No	No	2.00
997	65.42	396.79	0.00	1.42	0.26	0.72	270.27	0.00	270.27	4.000	No	No	2.00
998	65.49	392.38	0.00	1.32	0.26	0.72	267.22	0.00	267.22	4.000	No	No	2.00
999	65.57	388.35	0.00	1.34	0.26	0.72	264.43	0.00	264.43	4.000	No	No	2.00
1000	65.63	383.00	0.00	1.36	0.26	0.72	260.75	0.00	260.75	4.000	No	No	2.00
1001	65.71	375.67	0.00	1.40	0.26	0.72	255.64	0.00	255.64	4.000	No	No	2.00
1002	65.76	366.66	0.00	1.43	0.27	0.71	246.27	0.00	246.27	4.000	No	No	2.00
1003	65.82	285.86	0.00	1.64	0.38	0.63	169.32	0.00	169.32	4.000	No	No	2.00
1004	65.89	332.97	0.00	1.54	0.31	0.68	212.79	0.00	212.79	4.000	No	No	2.00
1005	65.95	322.55	0.00	1.56	0.33	0.67	202.87	0.00	202.87	4.000	No	No	2.00
1006	66.02	314.76	0.00	1.60	0.34	0.66	195.56	0.00	195.56	4.000	No	No	2.00
1007	66.09	311.19	0.00	1.61	0.34	0.65	192.23	0.00	192.23	4.000	No	No	2.00
1008	66.14	307.25	0.00	1.62	0.35	0.65	188.59	0.00	188.59	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1009	66.21	298.54	0.00	1.64	0.36	0.64	179.99	0.00	179.99	4.000	No	No	2.00
1010	66.28	298.54	0.00	1.65	0.36	0.64	179.93	0.00	179.93	4.000	No	No	2.00
1011	66.35	300.88	0.00	1.67	0.35	0.64	182.68	0.00	182.68	4.000	No	No	2.00
1012	66.41	302.85	0.00	1.67	0.35	0.64	184.39	0.00	184.39	4.000	No	No	2.00
1013	66.48	305.67	0.00	1.62	0.35	0.65	186.87	0.00	186.87	4.000	No	No	2.00
1014	66.55	306.61	0.00	1.55	0.35	0.65	187.66	0.00	187.66	4.000	No	No	2.00
1015	66.61	307.17	0.00	1.46	0.35	0.65	188.12	0.00	188.12	4.000	No	No	2.00
1016	66.68	304.73	0.00	1.48	0.35	0.65	185.86	0.00	185.86	4.000	No	No	2.00
1017	66.75	300.70	0.00	1.49	0.36	0.64	182.19	0.00	182.19	4.000	No	No	2.00
1018	66.81	297.61	0.00	1.51	0.36	0.64	178.67	0.00	178.67	4.000	No	No	2.00
1019	66.87	282.31	0.00	1.56	0.38	0.62	165.45	0.00	165.45	4.000	No	No	2.00
1020	66.93	268.61	0.00	1.61	0.40	0.61	153.96	0.00	153.96	4.000	No	No	2.00
1021	67.00	268.98	0.00	1.61	0.40	0.61	154.22	0.00	154.22	4.000	No	No	2.00
1022	67.06	263.92	0.00	1.63	0.41	0.60	150.03	0.00	150.03	4.000	No	No	2.00
1023	67.14	256.41	0.00	1.65	0.42	0.59	143.91	0.00	143.91	4.000	No	No	2.00
1024	67.21	246.92	0.00	1.66	0.43	0.58	136.35	0.00	136.35	4.000	No	No	2.00
1025	67.27	234.25	0.00	1.70	0.45	0.57	126.53	0.00	126.53	4.000	No	No	2.00
1026	67.34	218.48	4.41	1.77	0.47	0.55	114.45	0.06	114.50	4.000	No	No	2.00
1027	67.41	202.06	10.00	1.84	0.47	0.55	105.56	7.84	113.40	4.000	No	No	2.00
1028	67.47	186.29	16.05	1.91	0.44	0.57	100.69	26.29	126.99	4.000	No	No	2.00
1029	67.54	172.97	23.63	2.01	0.42	0.59	96.42	44.45	140.87	4.000	No	No	2.00
1030	67.61	163.68	29.92	2.09	0.41	0.60	92.25	53.88	146.13	4.000	No	No	2.00
1031	67.67	163.77	32.62	2.12	0.40	0.60	93.12	57.39	150.51	4.000	No	No	2.00
1032	67.74	163.78	30.16	2.09	0.41	0.60	92.34	54.21	146.55	4.000	No	No	2.00
1033	67.81	163.88	22.43	1.99	0.44	0.58	89.09	40.88	129.97	4.000	No	No	2.00
1034	67.87	160.50	22.30	1.99	0.45	0.57	86.35	40.18	126.53	4.000	No	No	2.00
1035	67.94	150.91	26.75	2.05	0.44	0.57	81.87	47.32	129.19	4.000	No	No	2.00
1036	68.01	138.80	35.14	2.15	0.43	0.58	75.77	56.18	131.95	4.000	No	No	2.00
1037	68.07	121.06	47.84	2.31	0.44	0.57	65.31	62.29	127.60	4.000	No	No	2.00
1038	68.12	109.24	57.81	2.44	0.45	0.56	58.26	64.37	122.63	4.000	No	No	2.00
1039	68.20	95.82	69.56	2.58	0.47	0.55	50.22	65.15	115.37	4.000	No	No	2.00
1040	68.25	84.25	78.02	2.69	0.48	0.54	43.35	0.00	43.35	4.000	No	Yes	2.00
1041	68.31	70.55	89.12	2.83	0.50	0.53	35.45	0.00	35.45	4.000	No	Yes	2.00
1042	68.38	59.86	98.26	2.94	0.52	0.52	29.48	0.00	29.48	4.000	No	Yes	2.00
1043	68.44	69.34	89.98	2.84	0.50	0.53	34.74	0.00	34.74	4.000	No	Yes	2.00
1044	68.51	59.40	97.16	2.93	0.52	0.52	29.19	0.00	29.19	4.000	No	Yes	2.00
1045	68.58	68.13	89.60	2.83	0.50	0.53	34.03	0.00	34.03	4.000	No	Yes	2.00
1046	68.64	83.63	79.81	2.71	0.48	0.54	42.91	0.00	42.91	4.000	No	Yes	2.00
1047	68.71	103.43	68.71	2.57	0.46	0.56	54.85	66.32	121.16	4.000	No	No	2.00
1048	68.78	125.86	57.69	2.43	0.43	0.58	69.23	67.37	136.61	4.000	No	No	2.00
1049	68.83	138.70	51.59	2.36	0.41	0.59	77.68	67.31	144.99	4.000	No	No	2.00
1050	68.91	153.72	43.78	2.26	0.40	0.60	87.55	65.70	153.25	4.000	No	No	2.00
1051	68.99	163.39	38.87	2.20	0.39	0.61	93.81	63.65	157.46	4.000	No	No	2.00
1052	69.05	164.89	32.83	2.12	0.40	0.60	93.45	57.70	151.15	4.000	No	No	2.00
1053	69.11	165.64	23.94	2.01	0.43	0.58	90.58	44.08	134.66	4.000	No	No	2.00
1054	69.17	165.73	26.14	2.04	0.42	0.59	91.65	48.15	139.80	4.000	No	No	2.00
1055	69.24	164.51	27.11	2.05	0.42	0.59	91.14	49.61	140.75	4.000	No	No	2.00
1056	69.31	161.70	28.12	2.06	0.42	0.59	89.48	50.82	140.30	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1057	69.37	158.51	31.79	2.11	0.41	0.59	88.36	55.41	143.77	4.000	No	No	2.00
1058	69.44	155.87	35.88	2.16	0.41	0.59	87.48	59.54	147.02	4.000	No	No	2.00
1059	69.51	153.05	39.95	2.21	0.41	0.60	86.22	62.69	148.91	4.000	No	No	2.00
1060	69.56	153.24	41.82	2.24	0.40	0.60	86.66	64.16	150.82	4.000	No	No	2.00
1061	69.64	160.37	42.72	2.25	0.39	0.61	92.02	66.11	158.13	4.000	No	No	2.00
1062	69.69	167.69	38.68	2.20	0.39	0.61	96.72	64.18	160.90	4.000	No	No	2.00
1063	69.78	187.40	30.41	2.09	0.38	0.62	109.41	58.03	167.43	4.000	No	No	2.00
1064	69.82	206.36	25.17	2.03	0.37	0.62	121.83	51.78	173.61	4.000	No	No	2.00
1065	69.89	242.68	14.99	1.90	0.38	0.62	141.70	26.53	168.23	4.000	No	No	2.00
1066	69.95	272.80	7.58	1.81	0.39	0.61	156.45	2.86	159.30	4.000	No	No	2.00
1067	70.02	279.93	8.97	1.82	0.37	0.62	163.88	6.29	170.17	4.000	No	No	2.00
1068	70.08	285.04	11.88	1.86	0.34	0.64	173.47	16.77	190.24	4.000	No	No	2.00
1069	70.15	282.86	12.45	1.87	0.34	0.65	172.50	19.00	191.50	4.000	No	No	2.00
1070	70.21	289.05	7.00	1.80	0.37	0.62	169.47	1.95	171.42	4.000	No	No	2.00
1071	70.30	298.53	3.07	1.75	0.37	0.63	176.65	0.00	176.65	4.000	No	No	2.00
1072	70.37	288.11	5.08	1.78	0.38	0.62	167.74	0.22	167.96	4.000	No	No	2.00
1073	70.41	300.12	3.47	1.76	0.36	0.63	178.71	0.01	178.71	4.000	No	No	2.00
1074	70.49	286.70	7.11	1.80	0.38	0.62	167.32	2.12	169.44	4.000	No	No	2.00
1075	70.55	301.73	4.54	1.77	0.36	0.63	180.06	0.09	180.14	4.000	No	No	2.00
1076	70.61	312.90	3.66	1.76	0.34	0.64	190.00	0.01	190.01	4.000	No	No	2.00
1077	70.67	318.43	0.67	1.72	0.34	0.65	195.01	0.00	195.01	4.000	No	No	2.00
1078	70.74	321.71	0.00	1.68	0.33	0.65	198.00	0.00	198.00	4.000	No	No	2.00
1079	70.81	312.79	0.00	1.66	0.34	0.64	189.74	0.00	189.74	4.000	No	No	2.00
1080	70.88	307.71	0.00	1.55	0.35	0.64	185.10	0.00	185.10	4.000	No	No	2.00
1081	70.95	296.55	0.00	1.59	0.37	0.62	174.40	0.00	174.40	4.000	No	No	2.00
1082	71.01	291.66	0.00	1.60	0.37	0.62	170.15	0.00	170.15	4.000	No	No	2.00
1083	71.08	292.24	0.00	1.60	0.37	0.62	170.58	0.00	170.58	4.000	No	No	2.00
1084	71.15	291.77	0.00	1.61	0.37	0.62	170.13	0.00	170.13	4.000	No	No	2.00
1085	71.20	289.19	0.00	1.64	0.38	0.61	167.88	0.00	167.88	4.000	No	No	2.00
1086	71.27	292.24	0.00	1.66	0.37	0.62	170.43	0.00	170.43	4.000	No	No	2.00
1087	71.33	286.61	0.00	1.69	0.38	0.61	165.60	0.00	165.60	4.000	No	No	2.00
1088	71.41	292.71	0.00	1.70	0.37	0.62	170.72	0.00	170.72	4.000	No	No	2.00
1089	71.47	294.21	0.00	1.71	0.37	0.62	171.97	0.00	171.97	4.000	No	No	2.00
1090	71.55	293.65	1.37	1.73	0.37	0.62	171.42	0.00	171.42	4.000	No	No	2.00
1091	71.60	289.24	3.55	1.76	0.38	0.61	167.60	0.01	167.61	4.000	No	No	2.00
1092	71.66	290.93	4.76	1.77	0.38	0.61	169.05	0.13	169.18	4.000	No	No	2.00
1093	71.72	290.46	6.30	1.79	0.37	0.62	169.03	1.04	170.07	4.000	No	No	2.00
1094	71.81	292.45	9.55	1.83	0.35	0.63	174.80	8.28	183.08	4.000	No	No	2.00
1095	71.87	291.04	11.94	1.86	0.34	0.65	177.62	17.23	194.85	4.000	No	No	2.00
1096	71.94	288.50	13.55	1.88	0.33	0.65	178.23	23.81	202.05	4.000	No	No	2.00
1097	72.00	284.84	15.03	1.90	0.32	0.66	177.46	29.68	207.15	4.000	No	No	2.00
1098	72.07	273.02	18.79	1.95	0.31	0.67	172.39	42.91	215.30	4.000	No	No	2.00
1099	72.14	256.03	23.86	2.01	0.31	0.67	162.46	55.88	218.33	4.000	No	No	2.00
1100	72.20	239.05	32.10	2.11	0.30	0.68	152.58	69.44	222.02	4.000	No	No	2.00
1101	72.27	226.56	32.81	2.12	0.32	0.66	141.77	68.11	209.88	4.000	No	No	2.00
1102	72.34	223.94	31.83	2.11	0.33	0.65	138.50	66.07	204.57	4.000	No	No	2.00
1103	72.41	217.85	34.00	2.14	0.33	0.65	134.18	67.97	202.15	4.000	No	No	2.00
1104	72.47	217.52	35.11	2.15	0.33	0.65	134.27	69.32	203.59	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1105	72.51	217.52	35.68	2.16	0.33	0.65	134.46	70.01	204.47	4.000	No	No	2.00
1106	72.58	217.21	35.81	2.16	0.33	0.65	134.19	70.10	204.29	4.000	No	No	2.00
1107	72.64	109.11	74.17	2.64	0.45	0.56	57.58	0.00	57.58	4.000	No	Yes	2.00
1108	72.72	242.00	25.06	2.03	0.32	0.66	150.48	56.56	207.04	4.000	No	No	2.00
1109	72.80	252.67	16.49	1.92	0.36	0.63	150.08	32.57	182.65	4.000	No	No	2.00
1110	72.86	251.82	13.17	1.88	0.38	0.61	144.56	20.13	164.69	4.000	No	No	2.00
1111	72.92	248.90	13.46	1.88	0.38	0.61	142.56	21.03	163.59	4.000	No	No	2.00
1112	72.97	245.62	13.33	1.88	0.39	0.60	139.67	20.37	160.04	4.000	No	No	2.00
1113	73.06	238.30	16.62	1.92	0.37	0.61	138.16	31.82	169.99	4.000	No	No	2.00
1114	73.12	233.69	18.85	1.95	0.37	0.62	136.95	38.69	175.64	4.000	No	No	2.00
1115	73.19	230.69	20.90	1.97	0.36	0.63	136.48	44.37	180.85	4.000	No	No	2.00
1116	73.25	227.13	22.92	2.00	0.35	0.63	135.25	49.20	184.46	4.000	No	No	2.00
1117	73.32	226.00	23.76	2.01	0.35	0.63	134.94	51.08	186.02	4.000	No	No	2.00
1118	73.38	222.72	24.86	2.02	0.35	0.63	132.98	53.11	186.08	4.000	No	No	2.00
1119	73.45	218.95	25.74	2.03	0.35	0.63	130.42	54.40	184.82	4.000	No	No	2.00
1120	73.52	215.95	26.14	2.04	0.36	0.63	128.17	54.77	182.95	4.000	No	No	2.00
1121	73.58	213.98	26.37	2.04	0.36	0.63	126.67	54.93	181.60	4.000	No	No	2.00
1122	73.65	216.04	25.49	2.03	0.36	0.63	127.77	53.45	181.21	4.000	No	No	2.00
1123	73.72	214.64	25.73	2.03	0.36	0.62	126.74	53.73	180.47	4.000	No	No	2.00
1124	73.78	216.14	25.49	2.03	0.36	0.63	127.77	53.44	181.22	4.000	No	No	2.00
1125	73.85	219.51	22.83	2.00	0.36	0.62	128.61	47.95	176.57	4.000	No	No	2.00
1126	73.92	225.61	22.19	1.99	0.36	0.62	133.03	47.12	180.16	4.000	No	No	2.00
1127	73.95	229.36	21.95	1.99	0.36	0.63	135.91	46.99	182.90	4.000	No	No	2.00
1128	74.02	235.55	19.87	1.96	0.36	0.62	139.03	41.92	180.94	4.000	No	No	2.00
1129	74.09	240.06	19.48	1.96	0.35	0.63	142.33	41.24	183.57	4.000	No	No	2.00
1130	74.16	242.50	19.83	1.96	0.35	0.63	144.72	42.57	187.29	4.000	No	No	2.00
1131	74.22	242.12	20.54	1.97	0.35	0.63	145.09	44.60	189.70	4.000	No	No	2.00
1132	74.30	241.75	20.83	1.97	0.35	0.63	145.03	45.42	190.45	4.000	No	No	2.00
1133	74.36	241.75	20.79	1.97	0.35	0.63	144.94	45.27	190.22	4.000	No	No	2.00
1134	74.43	240.72	21.07	1.98	0.35	0.63	144.32	45.96	190.28	4.000	No	No	2.00
1135	74.49	235.84	22.15	1.99	0.35	0.63	141.17	48.29	189.46	4.000	No	No	2.00
1136	74.55	230.96	23.15	2.00	0.35	0.63	137.90	50.18	188.08	4.000	No	No	2.00
1137	74.61	223.92	24.89	2.02	0.35	0.63	133.32	53.23	186.55	4.000	No	No	2.00
1138	74.68	215.75	26.91	2.05	0.35	0.63	127.86	56.13	183.99	4.000	No	No	2.00
1139	74.75	206.74	28.89	2.07	0.36	0.62	121.57	58.24	179.81	4.000	No	No	2.00
1140	74.81	198.77	30.75	2.10	0.37	0.62	116.01	59.86	175.87	4.000	No	No	2.00
1141	74.88	193.42	32.31	2.12	0.37	0.61	112.36	61.14	173.50	4.000	No	No	2.00
1142	74.95	189.57	33.47	2.13	0.37	0.61	109.73	61.97	171.70	4.000	No	No	2.00
1143	75.01	187.69	33.70	2.13	0.37	0.61	108.31	61.92	170.24	4.000	No	No	2.00
1144	75.08	187.69	33.28	2.13	0.37	0.61	108.14	61.40	169.55	4.000	No	No	2.00
1145	75.15	187.97	100.00	4.06	0.32	0.65	115.65	0.00	115.65	4.000	No	Yes	2.00
1146	75.21	188.82	100.00	4.06	0.32	0.65	116.34	0.00	116.34	4.000	No	Yes	2.00
1147	75.28	190.97	100.00	4.06	0.32	0.65	118.13	0.00	118.13	4.000	No	Yes	2.00
1148	75.35	193.78	100.00	4.06	0.32	0.66	120.47	0.00	120.47	4.000	No	Yes	2.00
1149	75.41	196.69	100.00	4.06	0.31	0.66	122.91	0.00	122.91	4.000	No	Yes	2.00
1150	75.46	193.59	100.00	4.06	0.32	0.66	120.29	0.00	120.29	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
$CRR_{7.5}$:	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.07	2.00	0.00	0.00	0.00	0.00	0.14	2.00	0.00	0.00	0.00	0.00
0.21	2.00	0.00	0.00	0.00	0.00	0.28	2.00	0.00	0.00	0.00	0.00
0.33	2.00	0.00	0.00	0.00	0.00	0.41	2.00	0.00	0.00	0.00	0.00
0.46	2.00	0.00	0.00	0.00	0.00	0.54	2.00	0.00	0.00	0.00	0.00
0.60	2.00	0.00	0.00	0.00	0.00	0.66	2.00	0.00	0.00	0.00	0.00
0.72	2.00	0.00	0.00	0.00	0.00	0.80	2.00	0.00	0.00	0.00	0.00
0.86	2.00	0.00	0.00	0.00	0.00	0.92	2.00	0.00	0.00	0.00	0.00
0.99	2.00	0.00	0.00	0.00	0.00	1.06	2.00	0.00	0.00	0.00	0.00
1.11	2.00	0.00	0.00	0.00	0.00	1.18	2.00	0.00	0.00	0.00	0.00
1.26	2.00	0.00	0.00	0.00	0.00	1.33	2.00	0.00	0.00	0.00	0.00
1.39	2.00	0.00	0.00	0.00	0.00	1.46	2.00	0.00	0.00	0.00	0.00
1.51	2.00	0.00	0.00	0.00	0.00	1.59	2.00	0.00	0.00	0.00	0.00
1.65	2.00	0.00	0.00	0.00	0.00	1.71	2.00	0.00	0.00	0.00	0.00
1.79	2.00	0.00	0.00	0.00	0.00	1.84	2.00	0.00	0.00	0.00	0.00
1.92	2.00	0.00	0.00	0.00	0.00	1.97	2.00	0.00	0.00	0.00	0.00
2.05	2.00	0.00	0.00	0.00	0.00	2.11	2.00	0.00	0.00	0.00	0.00
2.18	2.00	0.00	0.00	0.00	0.00	2.24	2.00	0.00	0.00	0.00	0.00
2.31	2.00	0.00	0.00	0.00	0.00	2.37	2.00	0.00	0.00	0.00	0.00
2.44	2.00	0.00	0.00	0.00	0.00	2.50	2.00	0.00	0.00	0.00	0.00
2.58	2.00	0.00	0.00	0.00	0.00	2.64	2.00	0.00	0.00	0.00	0.00
2.71	2.00	0.00	0.00	0.00	0.00	2.76	2.00	0.00	0.00	0.00	0.00
2.82	2.00	0.00	0.00	0.00	0.00	2.90	2.00	0.00	0.00	0.00	0.00
2.97	2.00	0.00	0.00	0.00	0.00	3.03	2.00	0.00	0.00	0.00	0.00
3.09	2.00	0.00	0.00	0.00	0.00	3.15	2.00	0.00	0.00	0.00	0.00
3.22	2.00	0.00	0.00	0.00	0.00	3.30	2.00	0.00	0.00	0.00	0.00
3.36	2.00	0.00	0.00	0.00	0.00	3.42	2.00	0.00	0.00	0.00	0.00
3.48	2.00	0.00	0.00	0.00	0.00	3.55	2.00	0.00	0.00	0.00	0.00
3.61	2.00	0.00	0.00	0.00	0.00	3.70	2.00	0.00	0.00	0.00	0.00
3.76	2.00	0.00	0.00	0.00	0.00	3.82	2.00	0.00	0.00	0.00	0.00
3.88	2.00	0.00	0.00	0.00	0.00	3.95	2.00	0.00	0.00	0.00	0.00
4.01	2.00	0.00	0.00	0.00	0.00	4.07	2.00	0.00	0.00	0.00	0.00
4.14	2.00	0.00	0.00	0.00	0.00	4.20	2.00	0.00	0.00	0.00	0.00
4.28	2.00	0.00	0.00	0.00	0.00	4.33	2.00	0.00	0.00	0.00	0.00
4.42	2.00	0.00	0.00	0.00	0.00	4.48	2.00	0.00	0.00	0.00	0.00
4.54	2.00	0.00	0.00	0.00	0.00	4.60	2.00	0.00	0.00	0.00	0.00
4.66	2.00	0.00	0.00	0.00	0.00	4.74	2.00	0.00	0.00	0.00	0.00
4.80	2.00	0.00	0.00	0.00	0.00	4.86	2.00	0.00	0.00	0.00	0.00
4.93	2.00	0.00	0.00	0.00	0.00	5.00	2.00	0.00	0.00	0.00	0.00
5.07	2.00	0.00	0.00	0.07	0.00	5.13	2.00	0.00	0.00	0.07	0.00
5.18	2.00	0.00	0.00	0.05	0.00	5.26	2.00	0.00	0.00	0.07	0.00
5.33	2.00	0.00	0.00	0.08	0.00	5.38	2.00	0.00	0.00	0.05	0.00
5.46	2.00	0.00	0.00	0.07	0.00	5.52	2.00	0.00	0.00	0.06	0.00
5.59	2.00	0.00	0.00	0.08	0.00	5.66	2.00	0.00	0.00	0.07	0.00
5.72	2.00	0.00	0.00	0.06	0.00	5.79	2.00	0.00	0.00	0.06	0.00
5.85	2.00	0.00	0.00	0.06	0.00	5.91	2.00	0.00	0.00	0.06	0.00
5.98	2.00	0.00	0.00	0.06	0.00	6.04	2.00	0.00	0.00	0.06	0.00
6.10	2.00	0.00	0.00	0.06	0.00	6.19	2.00	0.00	0.00	0.09	0.00
6.25	2.00	0.00	0.00	0.06	0.00	6.31	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
6.37	2.00	0.00	0.00	0.06	0.00	6.44	2.00	0.00	0.00	0.07	0.00
6.51	2.00	0.00	0.00	0.07	0.00	6.57	2.00	0.00	0.00	0.06	0.00
6.63	2.00	0.00	0.00	0.06	0.00	6.70	2.00	0.00	0.00	0.06	0.00
6.76	2.00	0.00	0.00	0.06	0.00	6.83	2.00	0.00	0.00	0.07	0.00
6.89	2.00	0.00	0.00	0.07	0.00	6.96	2.00	0.00	0.00	0.07	0.00
7.03	2.00	0.00	0.00	0.06	0.00	7.09	2.00	0.00	0.00	0.06	0.00
7.16	2.00	0.00	0.00	0.07	0.00	7.22	2.00	0.00	0.00	0.06	0.00
7.29	2.00	0.00	0.00	0.07	0.00	7.35	2.00	0.00	0.00	0.06	0.00
7.42	2.00	0.00	0.00	0.07	0.00	7.50	2.00	0.00	0.00	0.09	0.00
7.56	2.00	0.00	0.00	0.06	0.00	7.63	2.00	0.00	0.00	0.06	0.00
7.69	2.00	0.00	0.00	0.07	0.00	7.76	2.00	0.00	0.00	0.06	0.00
7.82	2.00	0.00	0.00	0.06	0.00	7.88	2.00	0.00	0.00	0.06	0.00
7.94	2.00	0.00	0.00	0.06	0.00	8.01	0.42	0.58	0.40	0.06	0.10
8.09	0.41	0.59	0.39	0.08	0.13	8.15	0.40	0.60	0.38	0.06	0.10
8.21	0.39	0.61	0.37	0.06	0.10	8.27	0.38	0.62	0.37	0.06	0.10
8.34	0.37	0.63	0.36	0.06	0.11	8.40	0.36	0.64	0.36	0.06	0.11
8.48	0.35	0.65	0.35	0.08	0.14	8.55	0.34	0.66	0.35	0.07	0.12
8.61	0.34	0.66	0.35	0.06	0.11	8.68	0.34	0.66	0.35	0.07	0.11
8.74	0.33	0.67	0.34	0.07	0.12	8.80	0.34	0.66	0.34	0.06	0.11
8.87	0.33	0.67	0.34	0.06	0.11	8.93	0.33	0.67	0.34	0.06	0.11
9.00	0.34	0.66	0.35	0.07	0.12	9.06	0.35	0.65	0.35	0.07	0.11
9.13	0.36	0.64	0.36	0.07	0.12	9.19	0.37	0.63	0.36	0.05	0.09
9.26	0.37	0.63	0.37	0.07	0.12	9.34	0.38	0.62	0.37	0.07	0.12
9.39	0.37	0.63	0.37	0.06	0.10	9.45	0.37	0.63	0.36	0.06	0.09
9.53	0.36	0.64	0.36	0.08	0.13	9.59	0.35	0.65	0.35	0.06	0.10
9.66	0.33	0.67	0.34	0.07	0.12	9.71	0.32	0.68	0.33	0.05	0.10
9.79	0.30	0.70	0.32	0.07	0.13	9.86	0.29	0.71	0.32	0.07	0.13
9.92	0.29	0.71	0.31	0.06	0.11	9.98	0.27	0.73	0.31	0.06	0.12
10.04	0.27	0.73	0.31	0.06	0.12	10.11	0.27	0.73	0.31	0.07	0.13
10.18	0.27	0.73	0.31	0.07	0.13	10.24	0.27	0.73	0.31	0.06	0.12
10.31	0.26	0.74	0.30	0.07	0.14	10.37	0.26	0.74	0.30	0.06	0.11
10.44	0.26	0.74	0.30	0.07	0.13	10.51	0.25	0.75	0.30	0.07	0.14
10.57	0.24	0.76	0.29	0.06	0.12	10.64	0.23	0.77	0.29	0.07	0.13
10.71	0.22	0.78	0.29	0.07	0.14	10.77	0.21	0.79	0.28	0.06	0.13
10.84	0.21	0.79	0.28	0.06	0.13	10.90	0.20	0.80	0.28	0.06	0.13
10.97	0.20	0.80	0.28	0.06	0.13	11.03	2.00	0.00	0.00	0.07	0.00
11.10	2.00	0.00	0.00	0.06	0.00	11.16	2.00	0.00	0.00	0.06	0.00
11.23	2.00	0.00	0.00	0.07	0.00	11.30	2.00	0.00	0.00	0.07	0.00
11.37	2.00	0.00	0.00	0.07	0.00	11.42	2.00	0.00	0.00	0.05	0.00
11.49	2.00	0.00	0.00	0.06	0.00	11.55	2.00	0.00	0.00	0.06	0.00
11.62	2.00	0.00	0.00	0.07	0.00	11.68	2.00	0.00	0.00	0.07	0.00
11.75	2.00	0.00	0.00	0.07	0.00	11.82	2.00	0.00	0.00	0.07	0.00
11.88	2.00	0.00	0.00	0.07	0.00	11.95	2.00	0.00	0.00	0.07	0.00
12.02	2.00	0.00	0.00	0.07	0.00	12.09	2.00	0.00	0.00	0.07	0.00
12.15	2.00	0.00	0.00	0.07	0.00	12.22	2.00	0.00	0.00	0.07	0.00
12.29	2.00	0.00	0.00	0.07	0.00	12.36	2.00	0.00	0.00	0.07	0.00
12.42	2.00	0.00	0.00	0.07	0.00	12.49	2.00	0.00	0.00	0.07	0.00
12.56	2.00	0.00	0.00	0.07	0.00	12.62	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
12.69	0.21	0.79	0.28	0.07	0.13	12.76	0.23	0.77	0.29	0.07	0.13
12.83	0.24	0.76	0.29	0.07	0.13	12.89	0.26	0.74	0.30	0.07	0.12
12.93	0.27	0.73	0.31	0.03	0.06	12.99	0.29	0.71	0.32	0.07	0.12
13.06	0.30	0.70	0.32	0.07	0.11	13.13	0.30	0.70	0.32	0.07	0.12
13.20	0.30	0.70	0.32	0.07	0.11	13.26	0.30	0.70	0.32	0.07	0.11
13.33	0.31	0.69	0.33	0.07	0.11	13.39	0.31	0.69	0.33	0.06	0.10
13.47	0.32	0.68	0.33	0.08	0.14	13.53	0.32	0.68	0.33	0.06	0.09
13.59	0.31	0.69	0.33	0.06	0.10	13.67	0.31	0.69	0.33	0.08	0.14
13.72	0.31	0.69	0.33	0.05	0.09	13.80	0.31	0.69	0.33	0.08	0.13
13.85	0.32	0.68	0.33	0.05	0.08	13.93	0.33	0.67	0.34	0.08	0.13
13.99	0.33	0.67	0.34	0.07	0.11	14.04	0.33	0.67	0.34	0.05	0.08
14.12	0.33	0.67	0.34	0.08	0.13	14.18	0.34	0.66	0.34	0.06	0.09
14.27	0.34	0.66	0.34	0.09	0.14	14.34	0.34	0.66	0.34	0.07	0.11
14.37	0.34	0.66	0.35	0.03	0.05	14.44	0.34	0.66	0.35	0.07	0.11
14.51	0.34	0.66	0.35	0.07	0.10	14.57	0.34	0.66	0.35	0.06	0.10
14.64	0.34	0.66	0.35	0.07	0.10	14.70	0.34	0.66	0.35	0.07	0.10
14.77	0.34	0.66	0.35	0.07	0.10	14.84	0.34	0.66	0.34	0.07	0.10
14.90	0.33	0.67	0.34	0.07	0.10	14.97	0.33	0.67	0.34	0.06	0.10
15.03	0.33	0.67	0.34	0.07	0.10	15.10	0.33	0.67	0.34	0.06	0.10
15.16	0.33	0.67	0.34	0.06	0.10	15.26	0.33	0.67	0.34	0.10	0.15
15.32	0.33	0.67	0.34	0.06	0.10	15.39	0.33	0.67	0.34	0.07	0.10
15.45	0.33	0.67	0.34	0.07	0.11	15.52	0.32	0.68	0.34	0.07	0.10
15.55	0.32	0.68	0.33	0.03	0.05	15.62	0.32	0.68	0.33	0.07	0.11
15.69	0.31	0.69	0.33	0.07	0.10	15.75	0.30	0.70	0.32	0.07	0.11
15.82	0.26	0.74	0.30	0.07	0.12	15.89	0.25	0.75	0.30	0.07	0.12
15.96	0.25	0.75	0.30	0.07	0.12	16.02	0.24	0.76	0.29	0.07	0.12
16.09	0.23	0.77	0.29	0.07	0.12	16.15	0.21	0.79	0.28	0.06	0.11
16.22	0.21	0.79	0.28	0.06	0.11	16.28	0.20	0.80	0.28	0.07	0.12
16.35	0.18	0.82	0.27	0.07	0.13	16.42	0.17	0.83	0.27	0.07	0.13
16.48	0.16	0.84	0.26	0.07	0.12	16.55	2.00	0.00	0.00	0.07	0.00
16.61	2.00	0.00	0.00	0.07	0.00	16.68	2.00	0.00	0.00	0.07	0.00
16.75	2.00	0.00	0.00	0.07	0.00	16.82	2.00	0.00	0.00	0.07	0.00
16.88	2.00	0.00	0.00	0.07	0.00	16.95	2.00	0.00	0.00	0.07	0.00
17.02	2.00	0.00	0.00	0.07	0.00	17.09	2.00	0.00	0.00	0.07	0.00
17.15	0.17	0.83	0.27	0.07	0.13	17.22	0.18	0.82	0.27	0.07	0.12
17.29	0.20	0.80	0.28	0.07	0.12	17.36	0.22	0.78	0.28	0.07	0.12
17.39	0.22	0.78	0.29	0.03	0.06	17.46	0.24	0.76	0.29	0.07	0.12
17.53	0.26	0.74	0.30	0.07	0.11	17.59	0.28	0.72	0.31	0.07	0.11
17.66	0.29	0.71	0.32	0.06	0.10	17.73	0.30	0.70	0.32	0.07	0.10
17.79	0.31	0.69	0.33	0.07	0.10	17.86	0.32	0.68	0.33	0.07	0.10
17.93	0.32	0.68	0.33	0.07	0.10	17.99	0.32	0.68	0.33	0.07	0.10
18.06	0.31	0.69	0.33	0.07	0.10	18.13	0.31	0.69	0.33	0.07	0.11
18.20	0.30	0.70	0.32	0.07	0.10	18.26	0.29	0.71	0.32	0.07	0.10
18.33	0.28	0.72	0.31	0.07	0.11	18.40	0.26	0.74	0.30	0.07	0.11
18.45	0.21	0.79	0.28	0.05	0.08	18.51	0.22	0.78	0.29	0.07	0.12
18.57	0.21	0.79	0.28	0.06	0.10	18.64	0.19	0.81	0.27	0.07	0.12
18.72	0.17	0.83	0.27	0.08	0.14	18.77	2.00	0.00	0.00	0.06	0.00
18.86	2.00	0.00	0.00	0.08	0.00	18.91	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
18.98	2.00	0.00	0.00	0.06	0.00	19.04	2.00	0.00	0.00	0.07	0.00
19.11	2.00	0.00	0.00	0.07	0.00	19.18	2.00	0.00	0.00	0.07	0.00
19.24	2.00	0.00	0.00	0.07	0.00	19.31	2.00	0.00	0.00	0.07	0.00
19.37	2.00	0.00	0.00	0.07	0.00	19.44	2.00	0.00	0.00	0.07	0.00
19.51	2.00	0.00	0.00	0.07	0.00	19.58	2.00	0.00	0.00	0.07	0.00
19.64	2.00	0.00	0.00	0.07	0.00	19.71	2.00	0.00	0.00	0.07	0.00
19.78	2.00	0.00	0.00	0.07	0.00	19.84	2.00	0.00	0.00	0.07	0.00
19.91	2.00	0.00	0.00	0.06	0.00	19.98	2.00	0.00	0.00	0.07	0.00
20.02	2.00	0.00	0.00	0.05	0.00	20.10	2.00	0.00	0.00	0.07	0.00
20.15	2.00	0.00	0.00	0.05	0.00	20.22	2.00	0.00	0.00	0.06	0.00
20.28	2.00	0.00	0.00	0.06	0.00	20.34	2.00	0.00	0.00	0.06	0.00
20.41	2.00	0.00	0.00	0.07	0.00	20.48	2.00	0.00	0.00	0.07	0.00
20.55	2.00	0.00	0.00	0.07	0.00	20.61	2.00	0.00	0.00	0.07	0.00
20.68	2.00	0.00	0.00	0.07	0.00	20.74	2.00	0.00	0.00	0.07	0.00
20.81	2.00	0.00	0.00	0.07	0.00	20.88	2.00	0.00	0.00	0.07	0.00
20.95	2.00	0.00	0.00	0.07	0.00	21.00	2.00	0.00	0.00	0.06	0.00
21.08	2.00	0.00	0.00	0.08	0.00	21.13	2.00	0.00	0.00	0.05	0.00
21.22	2.00	0.00	0.00	0.09	0.00	21.29	2.00	0.00	0.00	0.07	0.00
21.36	2.00	0.00	0.00	0.07	0.00	21.42	2.00	0.00	0.00	0.07	0.00
21.49	2.00	0.00	0.00	0.07	0.00	21.55	2.00	0.00	0.00	0.07	0.00
21.62	2.00	0.00	0.00	0.07	0.00	21.65	2.00	0.00	0.00	0.03	0.00
21.72	2.00	0.00	0.00	0.07	0.00	21.79	2.00	0.00	0.00	0.07	0.00
21.85	2.00	0.00	0.00	0.07	0.00	21.92	2.00	0.00	0.00	0.07	0.00
21.99	2.00	0.00	0.00	0.07	0.00	22.06	2.00	0.00	0.00	0.07	0.00
22.12	2.00	0.00	0.00	0.07	0.00	22.19	2.00	0.00	0.00	0.07	0.00
22.26	2.00	0.00	0.00	0.07	0.00	22.32	2.00	0.00	0.00	0.07	0.00
22.39	2.00	0.00	0.00	0.07	0.00	22.45	2.00	0.00	0.00	0.06	0.00
22.52	2.00	0.00	0.00	0.07	0.00	22.59	0.16	0.84	0.26	0.07	0.11
22.66	0.18	0.82	0.27	0.07	0.11	22.73	0.19	0.81	0.28	0.07	0.11
22.79	0.21	0.79	0.28	0.07	0.11	22.86	0.22	0.78	0.28	0.07	0.10
22.93	0.23	0.77	0.29	0.07	0.10	22.99	0.23	0.77	0.29	0.07	0.10
23.05	0.22	0.78	0.29	0.05	0.08	23.10	0.24	0.76	0.29	0.05	0.07
23.19	0.25	0.75	0.30	0.09	0.14	23.26	0.27	0.73	0.31	0.07	0.10
23.32	0.29	0.71	0.32	0.06	0.09	23.39	0.31	0.69	0.33	0.06	0.09
23.45	0.33	0.67	0.34	0.07	0.08	23.52	0.35	0.65	0.35	0.07	0.08
23.59	0.37	0.63	0.37	0.07	0.08	23.65	0.38	0.62	0.37	0.07	0.08
23.72	0.38	0.62	0.37	0.07	0.08	23.78	0.36	0.64	0.36	0.06	0.08
23.82	0.35	0.65	0.35	0.04	0.05	23.89	0.31	0.69	0.33	0.07	0.09
23.96	0.26	0.74	0.30	0.07	0.10	24.02	0.23	0.77	0.29	0.07	0.10
24.09	0.19	0.81	0.27	0.07	0.10	24.16	0.17	0.83	0.26	0.07	0.11
24.22	2.00	0.00	0.00	0.07	0.00	24.29	2.00	0.00	0.00	0.07	0.00
24.36	2.00	0.00	0.00	0.07	0.00	24.43	2.00	0.00	0.00	0.07	0.00
24.49	2.00	0.00	0.00	0.07	0.00	24.56	2.00	0.00	0.00	0.07	0.00
24.63	2.00	0.00	0.00	0.07	0.00	24.69	2.00	0.00	0.00	0.07	0.00
24.76	2.00	0.00	0.00	0.07	0.00	24.83	0.17	0.83	0.26	0.07	0.10
24.89	0.18	0.82	0.27	0.07	0.10	24.96	0.20	0.80	0.28	0.07	0.10
25.03	0.22	0.78	0.28	0.07	0.10	25.09	0.24	0.76	0.29	0.07	0.10
25.16	0.26	0.74	0.30	0.07	0.09	25.23	0.28	0.72	0.31	0.06	0.08

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
25.29	0.31	0.69	0.33	0.07	0.09	25.36	0.33	0.67	0.34	0.07	0.08
25.43	0.32	0.68	0.34	0.07	0.09	25.49	0.30	0.70	0.32	0.07	0.09
25.53	0.28	0.72	0.31	0.04	0.05	25.60	0.25	0.75	0.30	0.07	0.09
25.66	0.22	0.78	0.28	0.07	0.10	25.73	0.18	0.82	0.27	0.06	0.10
25.80	0.16	0.84	0.26	0.07	0.11	25.85	2.00	0.00	0.00	0.06	0.00
25.93	2.00	0.00	0.00	0.08	0.00	25.99	2.00	0.00	0.00	0.06	0.00
26.07	2.00	0.00	0.00	0.08	0.00	26.13	2.00	0.00	0.00	0.06	0.00
26.18	2.00	0.00	0.00	0.06	0.00	26.26	2.00	0.00	0.00	0.08	0.00
26.32	2.00	0.00	0.00	0.06	0.00	26.39	2.00	0.00	0.00	0.06	0.00
26.46	2.00	0.00	0.00	0.07	0.00	26.51	2.00	0.00	0.00	0.05	0.00
26.58	2.00	0.00	0.00	0.07	0.00	26.66	2.00	0.00	0.00	0.08	0.00
26.72	2.00	0.00	0.00	0.05	0.00	26.80	2.00	0.00	0.00	0.08	0.00
26.85	2.00	0.00	0.00	0.06	0.00	26.91	0.15	0.85	0.26	0.05	0.08
26.98	0.15	0.85	0.26	0.08	0.12	27.04	0.15	0.85	0.26	0.05	0.08
27.11	2.00	0.00	0.00	0.08	0.00	27.19	2.00	0.00	0.00	0.08	0.00
27.24	2.00	0.00	0.00	0.05	0.00	27.30	2.00	0.00	0.00	0.06	0.00
27.37	2.00	0.00	0.00	0.06	0.00	27.43	2.00	0.00	0.00	0.06	0.00
27.52	2.00	0.00	0.00	0.09	0.00	27.58	2.00	0.00	0.00	0.06	0.00
27.63	2.00	0.00	0.00	0.05	0.00	27.72	0.16	0.84	0.26	0.09	0.14
27.79	0.17	0.83	0.26	0.07	0.10	27.85	0.18	0.82	0.27	0.07	0.10
27.89	0.18	0.82	0.27	0.03	0.05	27.95	0.18	0.82	0.27	0.07	0.10
28.02	0.19	0.81	0.27	0.07	0.09	28.09	0.20	0.80	0.28	0.07	0.10
28.16	0.20	0.80	0.28	0.07	0.09	28.23	0.20	0.80	0.28	0.07	0.10
28.28	0.21	0.79	0.28	0.06	0.08	28.36	0.21	0.79	0.28	0.07	0.10
28.42	0.22	0.78	0.28	0.07	0.09	28.48	0.22	0.78	0.29	0.05	0.07
28.57	0.24	0.76	0.29	0.09	0.12	28.63	0.25	0.75	0.30	0.06	0.08
28.69	0.26	0.74	0.30	0.07	0.08	28.76	0.27	0.73	0.31	0.07	0.08
28.82	0.28	0.72	0.31	0.06	0.08	28.89	0.28	0.72	0.31	0.07	0.08
28.96	0.28	0.72	0.31	0.07	0.08	29.02	0.28	0.72	0.31	0.07	0.08
29.09	0.27	0.73	0.31	0.07	0.08	29.16	0.26	0.74	0.30	0.07	0.08
29.23	0.25	0.75	0.30	0.07	0.09	29.29	0.23	0.77	0.29	0.07	0.09
29.36	0.22	0.78	0.28	0.07	0.09	29.43	0.20	0.80	0.28	0.07	0.09
29.49	0.18	0.82	0.27	0.07	0.09	29.56	0.16	0.84	0.26	0.07	0.09
29.59	2.00	0.00	0.00	0.03	0.00	29.66	2.00	0.00	0.00	0.07	0.00
29.73	2.00	0.00	0.00	0.07	0.00	29.79	2.00	0.00	0.00	0.07	0.00
29.88	2.00	0.00	0.00	0.09	0.00	29.94	2.00	0.00	0.00	0.06	0.00
30.01	2.00	0.00	0.00	0.06	0.00	30.06	2.00	0.00	0.00	0.05	0.00
30.12	2.00	0.00	0.00	0.07	0.00	30.19	2.00	0.00	0.00	0.07	0.00
30.26	2.00	0.00	0.00	0.07	0.00	30.32	2.00	0.00	0.00	0.07	0.00
30.39	2.00	0.00	0.00	0.07	0.00	30.45	2.00	0.00	0.00	0.07	0.00
30.52	2.00	0.00	0.00	0.07	0.00	30.59	2.00	0.00	0.00	0.07	0.00
30.66	2.00	0.00	0.00	0.07	0.00	30.72	2.00	0.00	0.00	0.07	0.00
30.79	2.00	0.00	0.00	0.07	0.00	30.85	2.00	0.00	0.00	0.07	0.00
30.92	2.00	0.00	0.00	0.07	0.00	30.97	2.00	0.00	0.00	0.05	0.00
31.07	2.00	0.00	0.00	0.09	0.00	31.10	2.00	0.00	0.00	0.03	0.00
31.19	2.00	0.00	0.00	0.09	0.00	31.24	2.00	0.00	0.00	0.05	0.00
31.30	2.00	0.00	0.00	0.07	0.00	31.38	2.00	0.00	0.00	0.08	0.00
31.43	2.00	0.00	0.00	0.06	0.00	31.50	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
31.57	2.00	0.00	0.00	0.07	0.00	31.63	2.00	0.00	0.00	0.07	0.00
31.70	2.00	0.00	0.00	0.07	0.00	31.77	2.00	0.00	0.00	0.07	0.00
31.84	2.00	0.00	0.00	0.07	0.00	31.90	2.00	0.00	0.00	0.07	0.00
31.97	2.00	0.00	0.00	0.07	0.00	32.03	2.00	0.00	0.00	0.06	0.00
32.10	2.00	0.00	0.00	0.07	0.00	32.17	2.00	0.00	0.00	0.06	0.00
32.23	2.00	0.00	0.00	0.07	0.00	32.29	2.00	0.00	0.00	0.06	0.00
32.35	2.00	0.00	0.00	0.06	0.00	32.42	2.00	0.00	0.00	0.07	0.00
32.49	2.00	0.00	0.00	0.06	0.00	32.56	2.00	0.00	0.00	0.07	0.00
32.62	2.00	0.00	0.00	0.06	0.00	32.68	2.00	0.00	0.00	0.06	0.00
32.75	2.00	0.00	0.00	0.06	0.00	32.82	2.00	0.00	0.00	0.07	0.00
32.88	2.00	0.00	0.00	0.07	0.00	32.95	2.00	0.00	0.00	0.06	0.00
33.01	2.00	0.00	0.00	0.06	0.00	33.08	2.00	0.00	0.00	0.07	0.00
33.15	2.00	0.00	0.00	0.07	0.00	33.21	2.00	0.00	0.00	0.07	0.00
33.28	2.00	0.00	0.00	0.07	0.00	33.35	2.00	0.00	0.00	0.07	0.00
33.41	2.00	0.00	0.00	0.07	0.00	33.48	2.00	0.00	0.00	0.07	0.00
33.55	2.00	0.00	0.00	0.07	0.00	33.62	2.00	0.00	0.00	0.07	0.00
33.68	2.00	0.00	0.00	0.07	0.00	33.75	2.00	0.00	0.00	0.07	0.00
33.82	2.00	0.00	0.00	0.07	0.00	33.88	2.00	0.00	0.00	0.07	0.00
33.95	2.00	0.00	0.00	0.07	0.00	34.02	2.00	0.00	0.00	0.07	0.00
34.09	2.00	0.00	0.00	0.07	0.00	34.15	2.00	0.00	0.00	0.07	0.00
34.19	2.00	0.00	0.00	0.03	0.00	34.25	2.00	0.00	0.00	0.07	0.00
34.33	2.00	0.00	0.00	0.08	0.00	34.40	2.00	0.00	0.00	0.07	0.00
34.46	2.00	0.00	0.00	0.06	0.00	34.52	2.00	0.00	0.00	0.06	0.00
34.59	2.00	0.00	0.00	0.07	0.00	34.66	2.00	0.00	0.00	0.06	0.00
34.73	2.00	0.00	0.00	0.07	0.00	34.79	2.00	0.00	0.00	0.07	0.00
34.86	2.00	0.00	0.00	0.07	0.00	34.93	2.00	0.00	0.00	0.07	0.00
34.99	2.00	0.00	0.00	0.07	0.00	35.06	2.00	0.00	0.00	0.07	0.00
35.13	2.00	0.00	0.00	0.07	0.00	35.20	2.00	0.00	0.00	0.07	0.00
35.26	2.00	0.00	0.00	0.07	0.00	35.33	2.00	0.00	0.00	0.07	0.00
35.40	2.00	0.00	0.00	0.07	0.00	35.47	2.00	0.00	0.00	0.07	0.00
35.53	2.00	0.00	0.00	0.06	0.00	35.60	2.00	0.00	0.00	0.06	0.00
35.66	2.00	0.00	0.00	0.07	0.00	35.70	2.00	0.00	0.00	0.03	0.00
35.77	2.00	0.00	0.00	0.07	0.00	35.83	2.00	0.00	0.00	0.07	0.00
35.90	2.00	0.00	0.00	0.07	0.00	35.97	2.00	0.00	0.00	0.06	0.00
36.03	2.00	0.00	0.00	0.07	0.00	36.10	2.00	0.00	0.00	0.07	0.00
36.17	2.00	0.00	0.00	0.07	0.00	36.23	2.00	0.00	0.00	0.07	0.00
36.30	2.00	0.00	0.00	0.07	0.00	36.37	2.00	0.00	0.00	0.06	0.00
36.43	2.00	0.00	0.00	0.07	0.00	36.50	2.00	0.00	0.00	0.07	0.00
36.57	2.00	0.00	0.00	0.07	0.00	36.64	0.15	0.85	0.26	0.07	0.08
36.70	0.15	0.85	0.26	0.07	0.08	36.77	0.16	0.84	0.26	0.07	0.07
36.84	2.00	0.00	0.00	0.07	0.00	36.91	2.00	0.00	0.00	0.06	0.00
36.97	2.00	0.00	0.00	0.07	0.00	37.04	2.00	0.00	0.00	0.07	0.00
37.11	2.00	0.00	0.00	0.07	0.00	37.14	2.00	0.00	0.00	0.03	0.00
37.21	2.00	0.00	0.00	0.07	0.00	37.27	2.00	0.00	0.00	0.07	0.00
37.34	2.00	0.00	0.00	0.07	0.00	37.41	2.00	0.00	0.00	0.07	0.00
37.48	2.00	0.00	0.00	0.07	0.00	37.54	2.00	0.00	0.00	0.07	0.00
37.61	2.00	0.00	0.00	0.07	0.00	37.68	2.00	0.00	0.00	0.07	0.00
37.74	2.00	0.00	0.00	0.07	0.00	37.81	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
37.88	2.00	0.00	0.00	0.07	0.00	37.94	2.00	0.00	0.00	0.07	0.00
38.01	2.00	0.00	0.00	0.07	0.00	38.08	2.00	0.00	0.00	0.07	0.00
38.15	2.00	0.00	0.00	0.07	0.00	38.21	2.00	0.00	0.00	0.07	0.00
38.28	2.00	0.00	0.00	0.07	0.00	38.34	2.00	0.00	0.00	0.06	0.00
38.41	2.00	0.00	0.00	0.07	0.00	38.48	0.18	0.82	0.27	0.07	0.07
38.55	0.19	0.81	0.27	0.07	0.07	38.61	0.20	0.80	0.28	0.07	0.07
38.68	0.20	0.80	0.28	0.07	0.07	38.75	0.19	0.81	0.27	0.07	0.07
38.78	0.18	0.82	0.27	0.03	0.03	38.85	0.16	0.84	0.26	0.07	0.07
38.92	2.00	0.00	0.00	0.07	0.00	38.98	2.00	0.00	0.00	0.07	0.00
39.05	2.00	0.00	0.00	0.07	0.00	39.11	2.00	0.00	0.00	0.06	0.00
39.19	2.00	0.00	0.00	0.08	0.00	39.24	2.00	0.00	0.00	0.05	0.00
39.32	2.00	0.00	0.00	0.08	0.00	39.38	2.00	0.00	0.00	0.05	0.00
39.45	2.00	0.00	0.00	0.08	0.00	39.51	2.00	0.00	0.00	0.05	0.00
39.58	2.00	0.00	0.00	0.08	0.00	39.64	2.00	0.00	0.00	0.05	0.00
39.72	2.00	0.00	0.00	0.08	0.00	39.77	2.00	0.00	0.00	0.05	0.00
39.84	2.00	0.00	0.00	0.06	0.00	39.90	2.00	0.00	0.00	0.06	0.00
39.96	2.00	0.00	0.00	0.06	0.00	40.03	2.00	0.00	0.00	0.07	0.00
40.09	2.00	0.00	0.00	0.06	0.00	40.17	2.00	0.00	0.00	0.08	0.00
40.25	2.00	0.00	0.00	0.08	0.00	40.31	2.00	0.00	0.00	0.06	0.00
40.37	2.00	0.00	0.00	0.06	0.00	40.42	2.00	0.00	0.00	0.06	0.00
40.51	2.00	0.00	0.00	0.08	0.00	40.56	2.00	0.00	0.00	0.06	0.00
40.62	2.00	0.00	0.00	0.06	0.00	40.71	2.00	0.00	0.00	0.09	0.00
40.78	2.00	0.00	0.00	0.07	0.00	40.85	2.00	0.00	0.00	0.07	0.00
40.91	2.00	0.00	0.00	0.06	0.00	40.95	2.00	0.00	0.00	0.03	0.00
41.02	2.00	0.00	0.00	0.07	0.00	41.08	2.00	0.00	0.00	0.07	0.00
41.15	0.17	0.83	0.26	0.07	0.06	41.22	0.20	0.80	0.28	0.07	0.06
41.28	0.26	0.74	0.30	0.07	0.05	41.34	0.30	0.70	0.32	0.06	0.05
41.44	0.36	0.64	0.36	0.10	0.07	41.50	0.36	0.64	0.36	0.07	0.05
41.57	0.36	0.64	0.36	0.07	0.05	41.60	0.35	0.65	0.35	0.03	0.02
41.67	0.34	0.66	0.35	0.07	0.05	41.74	0.34	0.66	0.35	0.07	0.05
41.81	0.35	0.65	0.35	0.07	0.05	41.87	0.35	0.65	0.35	0.07	0.05
41.94	0.35	0.65	0.35	0.07	0.05	42.00	0.28	0.72	0.31	0.06	0.05
42.07	0.33	0.67	0.34	0.08	0.06	42.14	0.32	0.68	0.33	0.06	0.05
42.20	0.33	0.67	0.34	0.06	0.04	42.28	0.31	0.69	0.33	0.09	0.07
42.35	0.29	0.71	0.32	0.07	0.05	42.42	0.28	0.72	0.31	0.07	0.05
42.48	0.27	0.73	0.31	0.07	0.05	42.55	0.27	0.73	0.31	0.07	0.05
42.62	0.27	0.73	0.31	0.07	0.05	42.68	0.25	0.75	0.30	0.06	0.05
42.72	0.24	0.76	0.30	0.03	0.03	42.78	0.23	0.77	0.29	0.07	0.05
42.85	0.21	0.79	0.28	0.07	0.06	42.92	0.19	0.81	0.27	0.07	0.06
42.99	0.18	0.82	0.27	0.07	0.06	43.05	2.00	0.00	0.00	0.07	0.00
43.12	2.00	0.00	0.00	0.07	0.00	43.18	2.00	0.00	0.00	0.07	0.00
43.25	2.00	0.00	0.00	0.07	0.00	43.32	2.00	0.00	0.00	0.07	0.00
43.38	2.00	0.00	0.00	0.07	0.00	43.45	2.00	0.00	0.00	0.07	0.00
43.52	2.00	0.00	0.00	0.07	0.00	43.59	2.00	0.00	0.00	0.07	0.00
43.65	2.00	0.00	0.00	0.07	0.00	43.72	2.00	0.00	0.00	0.07	0.00
43.79	2.00	0.00	0.00	0.07	0.00	43.86	2.00	0.00	0.00	0.07	0.00
43.92	2.00	0.00	0.00	0.06	0.00	43.98	2.00	0.00	0.00	0.06	0.00
44.04	2.00	0.00	0.00	0.06	0.00	44.12	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
44.19	0.17	0.83	0.26	0.07	0.05	44.25	0.18	0.82	0.27	0.06	0.05
44.31	0.19	0.81	0.27	0.06	0.05	44.38	0.20	0.80	0.28	0.07	0.05
44.45	0.21	0.79	0.28	0.07	0.05	44.52	0.22	0.78	0.28	0.07	0.05
44.58	0.22	0.78	0.29	0.07	0.05	44.65	0.23	0.77	0.29	0.06	0.05
44.72	0.23	0.77	0.29	0.07	0.05	44.78	0.24	0.76	0.29	0.07	0.05
44.85	0.25	0.75	0.30	0.07	0.05	44.88	0.25	0.75	0.30	0.04	0.03
44.95	0.25	0.75	0.30	0.07	0.05	45.02	0.26	0.74	0.30	0.07	0.05
45.09	0.26	0.74	0.30	0.07	0.05	45.16	0.26	0.74	0.30	0.07	0.05
45.22	0.26	0.74	0.30	0.07	0.05	45.29	0.26	0.74	0.30	0.06	0.05
45.35	0.26	0.74	0.30	0.07	0.05	45.42	0.26	0.74	0.30	0.07	0.05
45.49	0.26	0.74	0.30	0.07	0.05	45.56	0.26	0.74	0.30	0.07	0.05
45.62	0.26	0.74	0.30	0.07	0.05	45.69	0.26	0.74	0.30	0.07	0.05
45.76	0.26	0.74	0.30	0.07	0.05	45.82	0.25	0.75	0.30	0.07	0.05
45.89	0.24	0.76	0.30	0.07	0.05	45.96	0.24	0.76	0.29	0.07	0.05
46.02	0.23	0.77	0.29	0.07	0.05	46.09	0.22	0.78	0.29	0.07	0.05
46.16	0.21	0.79	0.28	0.06	0.05	46.22	0.21	0.79	0.28	0.07	0.05
46.29	0.20	0.80	0.28	0.07	0.05	46.36	0.19	0.81	0.28	0.07	0.05
46.42	0.19	0.81	0.27	0.07	0.05	46.46	0.19	0.81	0.27	0.03	0.02
46.52	0.19	0.81	0.27	0.07	0.05	46.61	0.18	0.82	0.27	0.09	0.06
46.66	0.18	0.82	0.27	0.05	0.04	46.74	0.17	0.83	0.27	0.08	0.06
46.79	0.17	0.83	0.26	0.05	0.04	46.86	2.00	0.00	0.00	0.07	0.00
46.94	2.00	0.00	0.00	0.08	0.00	46.99	2.00	0.00	0.00	0.05	0.00
47.06	2.00	0.00	0.00	0.07	0.00	47.14	2.00	0.00	0.00	0.08	0.00
47.19	2.00	0.00	0.00	0.05	0.00	47.25	2.00	0.00	0.00	0.06	0.00
47.34	2.00	0.00	0.00	0.09	0.00	47.39	2.00	0.00	0.00	0.06	0.00
47.45	2.00	0.00	0.00	0.06	0.00	47.51	2.00	0.00	0.00	0.06	0.00
47.58	2.00	0.00	0.00	0.07	0.00	47.65	0.15	0.85	0.26	0.07	0.05
47.72	0.16	0.84	0.26	0.07	0.05	47.78	2.00	0.00	0.00	0.07	0.00
47.85	2.00	0.00	0.00	0.07	0.00	47.91	2.00	0.00	0.00	0.06	0.00
47.98	2.00	0.00	0.00	0.07	0.00	48.05	2.00	0.00	0.00	0.07	0.00
48.11	2.00	0.00	0.00	0.07	0.00	48.18	2.00	0.00	0.00	0.07	0.00
48.24	2.00	0.00	0.00	0.07	0.00	48.31	2.00	0.00	0.00	0.07	0.00
48.38	2.00	0.00	0.00	0.07	0.00	48.45	2.00	0.00	0.00	0.07	0.00
48.52	2.00	0.00	0.00	0.07	0.00	48.58	2.00	0.00	0.00	0.06	0.00
48.65	0.18	0.82	0.27	0.07	0.04	48.72	0.22	0.78	0.28	0.07	0.04
48.78	0.27	0.73	0.31	0.07	0.04	48.85	0.33	0.67	0.34	0.07	0.03
48.92	0.41	0.59	0.40	0.07	0.03	48.95	0.45	0.55	0.43	0.03	0.01
49.02	0.45	0.55	0.42	0.07	0.03	49.09	0.42	0.58	0.40	0.07	0.03
49.16	0.56	0.44	0.56	0.07	0.02	49.23	0.60	0.40	0.64	0.07	0.02
49.29	0.74	0.26	1.13	0.07	0.01	49.35	0.75	0.25	1.21	0.06	0.01
49.42	1.03	0.00	0.00	0.07	0.00	49.49	1.34	0.00	0.00	0.07	0.00
49.56	1.57	0.00	0.00	0.07	0.00	49.62	1.58	0.00	0.00	0.06	0.00
49.69	1.46	0.00	0.00	0.07	0.00	49.76	1.55	0.00	0.00	0.07	0.00
49.82	1.63	0.00	0.00	0.07	0.00	49.89	1.72	0.00	0.00	0.06	0.00
49.95	1.82	0.00	0.00	0.06	0.00	50.00	2.00	0.00	0.00	0.06	0.00
50.07	2.00	0.00	0.00	0.07	0.00	50.14	2.00	0.00	0.00	0.07	0.00
50.20	2.00	0.00	0.00	0.06	0.00	50.28	2.00	0.00	0.00	0.08	0.00
50.35	2.00	0.00	0.00	0.07	0.00	50.41	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
50.48	2.00	0.00	0.00	0.07	0.00	50.55	2.00	0.00	0.00	0.07	0.00
50.61	2.00	0.00	0.00	0.07	0.00	50.68	2.00	0.00	0.00	0.06	0.00
50.74	2.00	0.00	0.00	0.07	0.00	50.81	2.00	0.00	0.00	0.07	0.00
50.88	2.00	0.00	0.00	0.07	0.00	50.94	2.00	0.00	0.00	0.07	0.00
51.01	2.00	0.00	0.00	0.07	0.00	51.08	2.00	0.00	0.00	0.07	0.00
51.15	2.00	0.00	0.00	0.07	0.00	51.21	2.00	0.00	0.00	0.07	0.00
51.28	2.00	0.00	0.00	0.07	0.00	51.34	2.00	0.00	0.00	0.07	0.00
51.38	2.00	0.00	0.00	0.03	0.00	51.45	2.00	0.00	0.00	0.07	0.00
51.51	2.00	0.00	0.00	0.07	0.00	51.58	2.00	0.00	0.00	0.07	0.00
51.65	2.00	0.00	0.00	0.07	0.00	51.71	2.00	0.00	0.00	0.07	0.00
51.78	2.00	0.00	0.00	0.07	0.00	51.85	2.00	0.00	0.00	0.07	0.00
51.92	2.00	0.00	0.00	0.07	0.00	51.99	2.00	0.00	0.00	0.07	0.00
52.05	2.00	0.00	0.00	0.06	0.00	52.11	2.00	0.00	0.00	0.06	0.00
52.18	2.00	0.00	0.00	0.07	0.00	52.24	2.00	0.00	0.00	0.07	0.00
52.31	2.00	0.00	0.00	0.07	0.00	52.38	2.00	0.00	0.00	0.07	0.00
52.44	2.00	0.00	0.00	0.07	0.00	52.51	2.00	0.00	0.00	0.07	0.00
52.58	2.00	0.00	0.00	0.07	0.00	52.64	2.00	0.00	0.00	0.07	0.00
52.71	2.00	0.00	0.00	0.07	0.00	52.78	2.00	0.00	0.00	0.07	0.00
52.84	2.00	0.00	0.00	0.07	0.00	52.91	2.00	0.00	0.00	0.07	0.00
52.98	2.00	0.00	0.00	0.07	0.00	53.04	2.00	0.00	0.00	0.07	0.00
53.11	2.00	0.00	0.00	0.07	0.00	53.17	2.00	0.00	0.00	0.07	0.00
53.24	2.00	0.00	0.00	0.07	0.00	53.31	2.00	0.00	0.00	0.07	0.00
53.38	2.00	0.00	0.00	0.07	0.00	53.42	2.00	0.00	0.00	0.05	0.00
53.49	2.00	0.00	0.00	0.07	0.00	53.56	2.00	0.00	0.00	0.07	0.00
53.63	2.00	0.00	0.00	0.07	0.00	53.68	2.00	0.00	0.00	0.05	0.00
53.75	2.00	0.00	0.00	0.07	0.00	53.82	2.00	0.00	0.00	0.07	0.00
53.89	2.00	0.00	0.00	0.07	0.00	53.94	2.00	0.00	0.00	0.05	0.00
54.00	2.00	0.00	0.00	0.06	0.00	54.07	2.00	0.00	0.00	0.07	0.00
54.15	2.00	0.00	0.00	0.08	0.00	54.21	2.00	0.00	0.00	0.05	0.00
54.27	2.00	0.00	0.00	0.06	0.00	54.34	2.00	0.00	0.00	0.07	0.00
54.40	2.00	0.00	0.00	0.05	0.00	54.47	2.00	0.00	0.00	0.08	0.00
54.53	2.00	0.00	0.00	0.06	0.00	54.60	2.00	0.00	0.00	0.06	0.00
54.67	2.00	0.00	0.00	0.07	0.00	54.73	2.00	0.00	0.00	0.07	0.00
54.80	2.00	0.00	0.00	0.07	0.00	54.87	2.00	0.00	0.00	0.07	0.00
54.93	2.00	0.00	0.00	0.07	0.00	54.99	2.00	0.00	0.00	0.05	0.00
55.05	2.00	0.00	0.00	0.07	0.00	55.12	2.00	0.00	0.00	0.07	0.00
55.19	2.00	0.00	0.00	0.07	0.00	55.26	2.00	0.00	0.00	0.07	0.00
55.33	2.00	0.00	0.00	0.08	0.00	55.39	2.00	0.00	0.00	0.06	0.00
55.45	2.00	0.00	0.00	0.06	0.00	55.52	2.00	0.00	0.00	0.07	0.00
55.59	2.00	0.00	0.00	0.07	0.00	55.64	2.00	0.00	0.00	0.05	0.00
55.72	2.00	0.00	0.00	0.07	0.00	55.79	2.00	0.00	0.00	0.08	0.00
55.86	2.00	0.00	0.00	0.07	0.00	55.92	2.00	0.00	0.00	0.06	0.00
55.98	2.00	0.00	0.00	0.06	0.00	56.05	2.00	0.00	0.00	0.07	0.00
56.11	2.00	0.00	0.00	0.06	0.00	56.18	2.00	0.00	0.00	0.07	0.00
56.24	2.00	0.00	0.00	0.05	0.00	56.31	2.00	0.00	0.00	0.07	0.00
56.37	2.00	0.00	0.00	0.06	0.00	56.45	2.00	0.00	0.00	0.07	0.00
56.51	2.00	0.00	0.00	0.06	0.00	56.58	2.00	0.00	0.00	0.06	0.00
56.64	2.00	0.00	0.00	0.07	0.00	56.71	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
56.78	2.00	0.00	0.00	0.07	0.00	56.84	2.00	0.00	0.00	0.07	0.00
56.91	2.00	0.00	0.00	0.07	0.00	56.98	2.00	0.00	0.00	0.07	0.00
57.05	2.00	0.00	0.00	0.07	0.00	57.11	2.00	0.00	0.00	0.07	0.00
57.18	2.00	0.00	0.00	0.07	0.00	57.24	2.00	0.00	0.00	0.07	0.00
57.31	2.00	0.00	0.00	0.07	0.00	57.38	2.00	0.00	0.00	0.07	0.00
57.45	2.00	0.00	0.00	0.07	0.00	57.48	2.00	0.00	0.00	0.03	0.00
57.56	2.00	0.00	0.00	0.08	0.00	57.62	2.00	0.00	0.00	0.06	0.00
57.71	2.00	0.00	0.00	0.08	0.00	57.77	2.00	0.00	0.00	0.07	0.00
57.84	2.00	0.00	0.00	0.07	0.00	57.91	2.00	0.00	0.00	0.07	0.00
57.97	2.00	0.00	0.00	0.07	0.00	58.01	2.00	0.00	0.00	0.04	0.00
58.08	2.00	0.00	0.00	0.07	0.00	58.14	2.00	0.00	0.00	0.07	0.00
58.21	2.00	0.00	0.00	0.07	0.00	58.28	2.00	0.00	0.00	0.07	0.00
58.34	2.00	0.00	0.00	0.07	0.00	58.41	2.00	0.00	0.00	0.06	0.00
58.48	2.00	0.00	0.00	0.07	0.00	58.54	2.00	0.00	0.00	0.06	0.00
58.61	2.00	0.00	0.00	0.07	0.00	58.67	2.00	0.00	0.00	0.07	0.00
58.74	2.00	0.00	0.00	0.06	0.00	58.80	2.00	0.00	0.00	0.07	0.00
58.87	2.00	0.00	0.00	0.07	0.00	58.94	2.00	0.00	0.00	0.07	0.00
59.01	2.00	0.00	0.00	0.07	0.00	59.07	2.00	0.00	0.00	0.06	0.00
59.13	2.00	0.00	0.00	0.07	0.00	59.22	2.00	0.00	0.00	0.08	0.00
59.28	2.00	0.00	0.00	0.07	0.00	59.32	2.00	0.00	0.00	0.03	0.00
59.38	2.00	0.00	0.00	0.07	0.00	59.45	2.00	0.00	0.00	0.07	0.00
59.52	2.00	0.00	0.00	0.07	0.00	59.59	2.00	0.00	0.00	0.07	0.00
59.65	2.00	0.00	0.00	0.07	0.00	59.72	2.00	0.00	0.00	0.06	0.00
59.79	2.00	0.00	0.00	0.07	0.00	59.85	2.00	0.00	0.00	0.06	0.00
59.92	2.00	0.00	0.00	0.07	0.00	59.98	2.00	0.00	0.00	0.06	0.00
60.04	2.00	0.00	0.00	0.06	0.00	60.11	2.00	0.00	0.00	0.07	0.00
60.19	2.00	0.00	0.00	0.08	0.00	60.25	2.00	0.00	0.00	0.06	0.00
60.32	2.00	0.00	0.00	0.07	0.00	60.38	2.00	0.00	0.00	0.07	0.00
60.46	2.00	0.00	0.00	0.07	0.00	60.51	2.00	0.00	0.00	0.05	0.00
60.57	2.00	0.00	0.00	0.06	0.00	60.65	2.00	0.00	0.00	0.08	0.00
60.70	2.00	0.00	0.00	0.05	0.00	60.77	2.00	0.00	0.00	0.08	0.00
60.83	2.00	0.00	0.00	0.05	0.00	60.92	2.00	0.00	0.00	0.09	0.00
60.99	2.00	0.00	0.00	0.07	0.00	61.05	2.00	0.00	0.00	0.07	0.00
61.12	2.00	0.00	0.00	0.07	0.00	61.19	2.00	0.00	0.00	0.07	0.00
61.22	2.00	0.00	0.00	0.03	0.00	61.29	2.00	0.00	0.00	0.07	0.00
61.35	2.00	0.00	0.00	0.07	0.00	61.42	2.00	0.00	0.00	0.07	0.00
61.50	2.00	0.00	0.00	0.08	0.00	61.55	2.00	0.00	0.00	0.05	0.00
61.62	2.00	0.00	0.00	0.06	0.00	61.69	2.00	0.00	0.00	0.07	0.00
61.75	2.00	0.00	0.00	0.06	0.00	61.81	2.00	0.00	0.00	0.07	0.00
61.89	2.00	0.00	0.00	0.07	0.00	61.94	2.00	0.00	0.00	0.06	0.00
62.03	2.00	0.00	0.00	0.09	0.00	62.09	2.00	0.00	0.00	0.06	0.00
62.15	2.00	0.00	0.00	0.06	0.00	62.21	2.00	0.00	0.00	0.06	0.00
62.27	2.00	0.00	0.00	0.06	0.00	62.34	2.00	0.00	0.00	0.07	0.00
62.42	2.00	0.00	0.00	0.08	0.00	62.49	2.00	0.00	0.00	0.07	0.00
62.54	2.00	0.00	0.00	0.06	0.00	62.60	2.00	0.00	0.00	0.06	0.00
62.67	2.00	0.00	0.00	0.06	0.00	62.74	2.00	0.00	0.00	0.07	0.00
62.80	2.00	0.00	0.00	0.06	0.00	62.87	2.00	0.00	0.00	0.07	0.00
62.95	2.00	0.00	0.00	0.09	0.00	63.01	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
63.08	2.00	0.00	0.00	0.07	0.00	63.14	2.00	0.00	0.00	0.07	0.00
63.21	2.00	0.00	0.00	0.07	0.00	63.28	2.00	0.00	0.00	0.07	0.00
63.33	2.00	0.00	0.00	0.05	0.00	63.39	2.00	0.00	0.00	0.06	0.00
63.46	2.00	0.00	0.00	0.07	0.00	63.53	2.00	0.00	0.00	0.07	0.00
63.59	2.00	0.00	0.00	0.07	0.00	63.66	2.00	0.00	0.00	0.06	0.00
63.72	2.00	0.00	0.00	0.07	0.00	63.79	2.00	0.00	0.00	0.07	0.00
63.85	2.00	0.00	0.00	0.06	0.00	63.92	2.00	0.00	0.00	0.07	0.00
63.99	2.00	0.00	0.00	0.07	0.00	64.05	2.00	0.00	0.00	0.07	0.00
64.11	2.00	0.00	0.00	0.05	0.00	64.19	2.00	0.00	0.00	0.09	0.00
64.26	2.00	0.00	0.00	0.07	0.00	64.33	2.00	0.00	0.00	0.07	0.00
64.39	2.00	0.00	0.00	0.07	0.00	64.46	2.00	0.00	0.00	0.07	0.00
64.53	2.00	0.00	0.00	0.07	0.00	64.60	2.00	0.00	0.00	0.07	0.00
64.66	2.00	0.00	0.00	0.06	0.00	64.70	2.00	0.00	0.00	0.04	0.00
64.78	2.00	0.00	0.00	0.08	0.00	64.85	2.00	0.00	0.00	0.07	0.00
64.91	2.00	0.00	0.00	0.06	0.00	64.97	2.00	0.00	0.00	0.07	0.00
65.04	2.00	0.00	0.00	0.07	0.00	65.11	2.00	0.00	0.00	0.07	0.00
65.16	2.00	0.00	0.00	0.05	0.00	65.22	2.00	0.00	0.00	0.06	0.00
65.29	2.00	0.00	0.00	0.07	0.00	65.36	2.00	0.00	0.00	0.07	0.00
65.42	2.00	0.00	0.00	0.06	0.00	65.49	2.00	0.00	0.00	0.07	0.00
65.57	2.00	0.00	0.00	0.08	0.00	65.63	2.00	0.00	0.00	0.07	0.00
65.71	2.00	0.00	0.00	0.07	0.00	65.76	2.00	0.00	0.00	0.06	0.00
65.82	2.00	0.00	0.00	0.06	0.00	65.89	2.00	0.00	0.00	0.07	0.00
65.95	2.00	0.00	0.00	0.06	0.00	66.02	2.00	0.00	0.00	0.08	0.00
66.09	2.00	0.00	0.00	0.06	0.00	66.14	2.00	0.00	0.00	0.06	0.00
66.21	2.00	0.00	0.00	0.07	0.00	66.28	2.00	0.00	0.00	0.07	0.00
66.35	2.00	0.00	0.00	0.07	0.00	66.41	2.00	0.00	0.00	0.07	0.00
66.48	2.00	0.00	0.00	0.07	0.00	66.55	2.00	0.00	0.00	0.07	0.00
66.61	2.00	0.00	0.00	0.06	0.00	66.68	2.00	0.00	0.00	0.07	0.00
66.75	2.00	0.00	0.00	0.07	0.00	66.81	2.00	0.00	0.00	0.07	0.00
66.87	2.00	0.00	0.00	0.06	0.00	66.93	2.00	0.00	0.00	0.06	0.00
67.00	2.00	0.00	0.00	0.06	0.00	67.06	2.00	0.00	0.00	0.07	0.00
67.14	2.00	0.00	0.00	0.08	0.00	67.21	2.00	0.00	0.00	0.06	0.00
67.27	2.00	0.00	0.00	0.06	0.00	67.34	2.00	0.00	0.00	0.07	0.00
67.41	2.00	0.00	0.00	0.07	0.00	67.47	2.00	0.00	0.00	0.07	0.00
67.54	2.00	0.00	0.00	0.07	0.00	67.61	2.00	0.00	0.00	0.07	0.00
67.67	2.00	0.00	0.00	0.07	0.00	67.74	2.00	0.00	0.00	0.07	0.00
67.81	2.00	0.00	0.00	0.07	0.00	67.87	2.00	0.00	0.00	0.07	0.00
67.94	2.00	0.00	0.00	0.07	0.00	68.01	2.00	0.00	0.00	0.07	0.00
68.07	2.00	0.00	0.00	0.06	0.00	68.12	2.00	0.00	0.00	0.05	0.00
68.20	2.00	0.00	0.00	0.08	0.00	68.25	2.00	0.00	0.00	0.05	0.00
68.31	2.00	0.00	0.00	0.06	0.00	68.38	2.00	0.00	0.00	0.07	0.00
68.44	2.00	0.00	0.00	0.07	0.00	68.51	2.00	0.00	0.00	0.06	0.00
68.58	2.00	0.00	0.00	0.07	0.00	68.64	2.00	0.00	0.00	0.07	0.00
68.71	2.00	0.00	0.00	0.07	0.00	68.78	2.00	0.00	0.00	0.07	0.00
68.83	2.00	0.00	0.00	0.05	0.00	68.91	2.00	0.00	0.00	0.08	0.00
68.99	2.00	0.00	0.00	0.08	0.00	69.05	2.00	0.00	0.00	0.06	0.00
69.11	2.00	0.00	0.00	0.06	0.00	69.17	2.00	0.00	0.00	0.06	0.00
69.24	2.00	0.00	0.00	0.07	0.00	69.31	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
69.37	2.00	0.00	0.00	0.06	0.00	69.44	2.00	0.00	0.00	0.06	0.00
69.51	2.00	0.00	0.00	0.08	0.00	69.56	2.00	0.00	0.00	0.05	0.00
69.64	2.00	0.00	0.00	0.08	0.00	69.69	2.00	0.00	0.00	0.05	0.00
69.78	2.00	0.00	0.00	0.08	0.00	69.82	2.00	0.00	0.00	0.05	0.00
69.89	2.00	0.00	0.00	0.07	0.00	69.95	2.00	0.00	0.00	0.06	0.00
70.02	2.00	0.00	0.00	0.07	0.00	70.08	2.00	0.00	0.00	0.06	0.00
70.15	2.00	0.00	0.00	0.07	0.00	70.21	2.00	0.00	0.00	0.06	0.00
70.30	2.00	0.00	0.00	0.09	0.00	70.37	2.00	0.00	0.00	0.06	0.00
70.41	2.00	0.00	0.00	0.05	0.00	70.49	2.00	0.00	0.00	0.07	0.00
70.55	2.00	0.00	0.00	0.06	0.00	70.61	2.00	0.00	0.00	0.06	0.00
70.67	2.00	0.00	0.00	0.07	0.00	70.74	2.00	0.00	0.00	0.07	0.00
70.81	2.00	0.00	0.00	0.07	0.00	70.88	2.00	0.00	0.00	0.07	0.00
70.95	2.00	0.00	0.00	0.07	0.00	71.01	2.00	0.00	0.00	0.07	0.00
71.08	2.00	0.00	0.00	0.07	0.00	71.15	2.00	0.00	0.00	0.07	0.00
71.20	2.00	0.00	0.00	0.05	0.00	71.27	2.00	0.00	0.00	0.07	0.00
71.33	2.00	0.00	0.00	0.06	0.00	71.41	2.00	0.00	0.00	0.08	0.00
71.47	2.00	0.00	0.00	0.06	0.00	71.55	2.00	0.00	0.00	0.08	0.00
71.60	2.00	0.00	0.00	0.06	0.00	71.66	2.00	0.00	0.00	0.06	0.00
71.72	2.00	0.00	0.00	0.06	0.00	71.81	2.00	0.00	0.00	0.09	0.00
71.87	2.00	0.00	0.00	0.06	0.00	71.94	2.00	0.00	0.00	0.07	0.00
72.00	2.00	0.00	0.00	0.07	0.00	72.07	2.00	0.00	0.00	0.07	0.00
72.14	2.00	0.00	0.00	0.07	0.00	72.20	2.00	0.00	0.00	0.07	0.00
72.27	2.00	0.00	0.00	0.07	0.00	72.34	2.00	0.00	0.00	0.07	0.00
72.41	2.00	0.00	0.00	0.07	0.00	72.47	2.00	0.00	0.00	0.07	0.00
72.51	2.00	0.00	0.00	0.03	0.00	72.58	2.00	0.00	0.00	0.07	0.00
72.64	2.00	0.00	0.00	0.07	0.00	72.72	2.00	0.00	0.00	0.07	0.00
72.80	2.00	0.00	0.00	0.08	0.00	72.86	2.00	0.00	0.00	0.06	0.00
72.92	2.00	0.00	0.00	0.06	0.00	72.97	2.00	0.00	0.00	0.05	0.00
73.06	2.00	0.00	0.00	0.09	0.00	73.12	2.00	0.00	0.00	0.07	0.00
73.19	2.00	0.00	0.00	0.07	0.00	73.25	2.00	0.00	0.00	0.06	0.00
73.32	2.00	0.00	0.00	0.06	0.00	73.38	2.00	0.00	0.00	0.07	0.00
73.45	2.00	0.00	0.00	0.07	0.00	73.52	2.00	0.00	0.00	0.07	0.00
73.58	2.00	0.00	0.00	0.07	0.00	73.65	2.00	0.00	0.00	0.07	0.00
73.72	2.00	0.00	0.00	0.07	0.00	73.78	2.00	0.00	0.00	0.07	0.00
73.85	2.00	0.00	0.00	0.07	0.00	73.92	2.00	0.00	0.00	0.07	0.00
73.95	2.00	0.00	0.00	0.03	0.00	74.02	2.00	0.00	0.00	0.07	0.00
74.09	2.00	0.00	0.00	0.07	0.00	74.16	2.00	0.00	0.00	0.06	0.00
74.22	2.00	0.00	0.00	0.06	0.00	74.30	2.00	0.00	0.00	0.08	0.00
74.36	2.00	0.00	0.00	0.06	0.00	74.43	2.00	0.00	0.00	0.07	0.00
74.49	2.00	0.00	0.00	0.06	0.00	74.55	2.00	0.00	0.00	0.06	0.00
74.61	2.00	0.00	0.00	0.06	0.00	74.68	2.00	0.00	0.00	0.07	0.00
74.75	2.00	0.00	0.00	0.07	0.00	74.81	2.00	0.00	0.00	0.07	0.00
74.88	2.00	0.00	0.00	0.07	0.00	74.95	2.00	0.00	0.00	0.07	0.00
75.01	2.00	0.00	0.00	0.07	0.00	75.08	2.00	0.00	0.00	0.07	0.00
75.15	2.00	0.00	0.00	0.07	0.00	75.21	2.00	0.00	0.00	0.07	0.00
75.28	2.00	0.00	0.00	0.07	0.00	75.35	2.00	0.00	0.00	0.07	0.00
75.41	2.00	0.00	0.00	0.07	0.00	75.46	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}	Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}

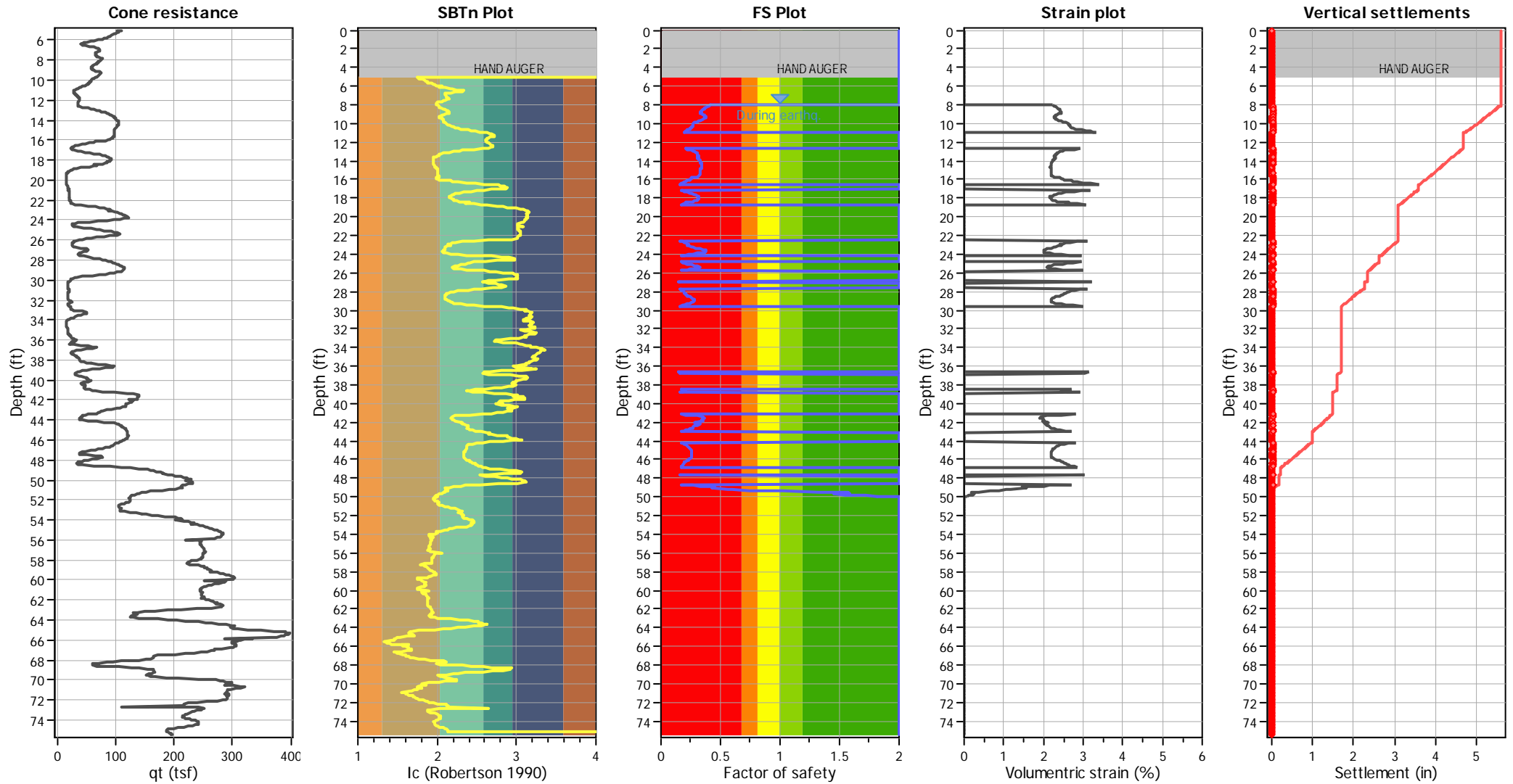
Overall liquefaction potential: 25.71

$LPI_{ISH} > 5.0$ - Liquefaction manifestation is expected

Abbreviations

- FS: Calculated factor of safety for test point
- d_z : Layer thickness (ft)
- LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- q_t : Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement due to soil liquefaction ::											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.01	140.32	0.42	2.24	1.00	0.02	8.09	138.94	0.41	2.26	1.00	0.02
8.15	137.64	0.40	2.29	1.00	0.02	8.21	136.32	0.39	2.31	1.00	0.02
8.27	135.42	0.38	2.33	1.00	0.02	8.34	134.50	0.37	2.35	1.00	0.02
8.40	133.10	0.36	2.37	1.00	0.02	8.48	131.33	0.35	2.41	1.00	0.02
8.55	130.22	0.34	2.43	1.00	0.02	8.61	130.49	0.34	2.42	1.00	0.02
8.68	130.63	0.34	2.42	1.00	0.02	8.74	129.42	0.33	2.45	1.00	0.02
8.80	130.39	0.34	2.43	1.00	0.02	8.87	128.59	0.33	2.46	1.00	0.02
8.93	130.39	0.33	2.43	1.00	0.02	9.00	132.45	0.34	2.39	1.00	0.02
9.06	134.20	0.35	2.35	1.00	0.02	9.13	135.84	0.36	2.32	1.00	0.02
9.19	136.80	0.37	2.30	1.00	0.01	9.26	137.76	0.37	2.28	1.00	0.02
9.34	138.33	0.38	2.27	1.00	0.02	9.39	138.17	0.37	2.28	1.00	0.02
9.45	137.50	0.37	2.29	1.00	0.02	9.53	136.35	0.36	2.31	1.00	0.02
9.59	135.14	0.35	2.33	1.00	0.02	9.66	132.53	0.33	2.38	1.00	0.02
9.71	129.61	0.32	2.44	1.00	0.02	9.79	127.13	0.30	2.49	1.00	0.02
9.86	125.30	0.29	2.53	1.00	0.02	9.92	123.93	0.29	2.56	1.00	0.02
9.98	121.39	0.27	2.62	1.00	0.02	10.04	120.91	0.27	2.63	1.00	0.02
10.11	120.66	0.27	2.64	1.00	0.02	10.18	120.30	0.27	2.65	1.00	0.02
10.24	119.93	0.27	2.66	1.00	0.02	10.31	119.89	0.26	2.66	1.00	0.02
10.37	119.17	0.26	2.67	1.00	0.02	10.44	117.87	0.26	2.71	1.00	0.02
10.51	115.89	0.25	2.76	1.00	0.02	10.57	113.26	0.24	2.82	1.00	0.02
10.64	110.17	0.23	2.91	1.00	0.02	10.71	107.70	0.22	2.98	1.00	0.03
10.77	104.38	0.21	3.07	1.00	0.02	10.84	101.26	0.21	3.17	1.00	0.02
10.90	98.45	0.20	3.26	1.00	0.03	10.97	96.88	0.20	3.32	1.00	0.03
11.03	34.08	2.00	0.00	1.00	0.00	11.10	33.54	2.00	0.00	1.00	0.00
11.16	33.33	2.00	0.00	1.00	0.00	11.23	32.90	2.00	0.00	1.00	0.00
11.30	33.43	2.00	0.00	1.00	0.00	11.37	34.71	2.00	0.00	1.00	0.00
11.42	36.00	2.00	0.00	1.00	0.00	11.49	37.48	2.00	0.00	1.00	0.00
11.55	38.95	2.00	0.00	1.00	0.00	11.62	40.30	2.00	0.00	1.00	0.00
11.68	41.45	2.00	0.00	1.00	0.00	11.75	42.78	2.00	0.00	1.00	0.00
11.82	43.28	2.00	0.00	1.00	0.00	11.88	43.36	2.00	0.00	1.00	0.00
11.95	42.94	2.00	0.00	1.00	0.00	12.02	42.31	2.00	0.00	1.00	0.00
12.09	41.38	2.00	0.00	1.00	0.00	12.15	40.66	2.00	0.00	1.00	0.00
12.22	39.62	2.00	0.00	1.00	0.00	12.29	38.81	2.00	0.00	1.00	0.00
12.36	39.01	2.00	0.00	1.00	0.00	12.42	38.80	2.00	0.00	1.00	0.00
12.49	38.59	2.00	0.00	1.00	0.00	12.56	39.50	2.00	0.00	1.00	0.00
12.62	41.83	2.00	0.00	1.00	0.00	12.69	109.95	0.21	2.91	1.00	0.02
12.76	115.26	0.23	2.77	1.00	0.02	12.83	119.58	0.24	2.67	1.00	0.02
12.89	125.00	0.26	2.54	1.00	0.02	12.93	127.31	0.27	2.49	1.00	0.01
12.99	131.72	0.29	2.40	1.00	0.02	13.06	133.69	0.30	2.36	1.00	0.02
13.13	134.21	0.30	2.35	1.00	0.02	13.20	134.76	0.30	2.34	1.00	0.02
13.26	135.55	0.30	2.33	1.00	0.02	13.33	136.33	0.31	2.31	1.00	0.02
13.39	136.86	0.31	2.30	1.00	0.02	13.47	138.75	0.32	2.27	1.00	0.02
13.53	138.92	0.32	2.26	1.00	0.02	13.59	137.35	0.31	2.29	1.00	0.02
13.67	136.68	0.31	2.30	1.00	0.02	13.72	137.31	0.31	2.29	1.00	0.01
13.80	138.01	0.31	2.28	1.00	0.02	13.85	139.08	0.32	2.26	1.00	0.01
13.93	140.18	0.33	2.24	1.00	0.02	13.99	140.60	0.33	2.23	1.00	0.02
14.04	140.51	0.33	2.23	1.00	0.01	14.12	141.43	0.33	2.22	1.00	0.02
14.18	142.14	0.34	2.21	1.00	0.02	14.27	142.09	0.34	2.21	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
14.34	142.87	0.34	2.19	1.00	0.02	14.37	143.20	0.34	2.19	1.00	0.01
14.44	143.56	0.34	2.18	1.00	0.02	14.51	143.62	0.34	2.18	1.00	0.02
14.57	143.71	0.34	2.18	1.00	0.02	14.64	143.83	0.34	2.18	1.00	0.02
14.70	143.77	0.34	2.18	1.00	0.02	14.77	143.57	0.34	2.18	1.00	0.02
14.84	143.25	0.34	2.19	1.00	0.02	14.90	142.87	0.33	2.19	1.00	0.02
14.97	142.39	0.33	2.20	1.00	0.02	15.03	142.20	0.33	2.20	1.00	0.02
15.10	142.06	0.33	2.21	1.00	0.02	15.16	142.05	0.33	2.21	1.00	0.02
15.26	143.02	0.33	2.19	1.00	0.03	15.32	142.56	0.33	2.20	1.00	0.02
15.39	142.38	0.33	2.20	1.00	0.02	15.45	142.33	0.33	2.20	1.00	0.02
15.52	141.99	0.32	2.21	1.00	0.02	15.55	141.77	0.32	2.21	1.00	0.01
15.62	141.30	0.32	2.22	1.00	0.02	15.69	140.86	0.31	2.23	1.00	0.02
15.75	138.76	0.30	2.27	1.00	0.02	15.82	130.90	0.26	2.42	1.00	0.02
15.89	129.57	0.25	2.44	1.00	0.02	15.96	127.84	0.25	2.48	1.00	0.02
16.02	125.69	0.24	2.53	1.00	0.02	16.09	123.41	0.23	2.58	1.00	0.02
16.15	118.27	0.21	2.70	1.00	0.02	16.22	116.75	0.21	2.73	1.00	0.02
16.28	112.04	0.20	2.86	1.00	0.02	16.35	106.35	0.18	3.02	1.00	0.02
16.42	100.65	0.17	3.19	1.00	0.03	16.48	94.58	0.16	3.40	1.00	0.03
16.55	29.04	2.00	0.00	1.00	0.00	16.61	25.62	2.00	0.00	1.00	0.00
16.68	24.39	2.00	0.00	1.00	0.00	16.75	22.73	2.00	0.00	1.00	0.00
16.82	21.59	2.00	0.00	1.00	0.00	16.88	21.46	2.00	0.00	1.00	0.00
16.95	22.94	2.00	0.00	1.00	0.00	17.02	26.65	2.00	0.00	1.00	0.00
17.09	32.41	2.00	0.00	1.00	0.00	17.15	100.43	0.17	3.20	1.00	0.03
17.22	107.91	0.18	2.97	1.00	0.02	17.29	114.51	0.20	2.79	1.00	0.02
17.36	120.82	0.22	2.64	1.00	0.02	17.39	123.30	0.22	2.58	1.00	0.01
17.46	128.58	0.24	2.46	1.00	0.02	17.53	132.87	0.26	2.38	1.00	0.02
17.59	136.18	0.28	2.31	1.00	0.02	17.66	138.66	0.29	2.27	1.00	0.02
17.73	140.78	0.30	2.23	1.00	0.02	17.79	142.50	0.31	2.20	1.00	0.02
17.86	143.80	0.32	2.18	1.00	0.02	17.93	143.85	0.32	2.18	1.00	0.02
17.99	143.72	0.32	2.18	1.00	0.02	18.06	142.99	0.31	2.19	1.00	0.02
18.13	141.86	0.31	2.21	1.00	0.02	18.20	140.93	0.30	2.23	1.00	0.02
18.26	139.30	0.29	2.26	1.00	0.02	18.33	137.19	0.28	2.29	1.00	0.02
18.40	134.19	0.26	2.35	1.00	0.02	18.45	120.83	0.21	2.64	1.00	0.01
18.51	124.71	0.22	2.55	1.00	0.02	18.57	119.70	0.21	2.66	1.00	0.02
18.64	112.49	0.19	2.84	1.00	0.02	18.72	104.85	0.17	3.06	1.00	0.03
18.77	36.60	2.00	0.00	1.00	0.00	18.86	29.15	2.00	0.00	1.00	0.00
18.91	25.18	2.00	0.00	1.00	0.00	18.98	22.41	2.00	0.00	1.00	0.00
19.04	20.50	2.00	0.00	1.00	0.00	19.11	17.92	2.00	0.00	1.00	0.00
19.18	16.20	2.00	0.00	1.00	0.00	19.24	15.24	2.00	0.00	1.00	0.00
19.31	14.29	2.00	0.00	1.00	0.00	19.37	13.34	2.00	0.00	1.00	0.00
19.44	12.90	2.00	0.00	1.00	0.00	19.51	12.79	2.00	0.00	1.00	0.00
19.58	13.10	2.00	0.00	1.00	0.00	19.64	12.74	2.00	0.00	1.00	0.00
19.71	12.72	2.00	0.00	1.00	0.00	19.78	12.69	2.00	0.00	1.00	0.00
19.84	12.92	2.00	0.00	1.00	0.00	19.91	13.31	2.00	0.00	1.00	0.00
19.98	13.45	2.00	0.00	1.00	0.00	20.02	13.35	2.00	0.00	1.00	0.00
20.10	13.24	2.00	0.00	1.00	0.00	20.15	13.47	2.00	0.00	1.00	0.00
20.22	13.61	2.00	0.00	1.00	0.00	20.28	13.59	2.00	0.00	1.00	0.00
20.34	13.73	2.00	0.00	1.00	0.00	20.41	13.87	2.00	0.00	1.00	0.00
20.48	13.76	2.00	0.00	1.00	0.00	20.55	14.06	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
20.61	14.28	2.00	0.00	1.00	0.00	20.68	14.66	2.00	0.00	1.00	0.00
20.74	15.12	2.00	0.00	1.00	0.00	20.81	15.50	2.00	0.00	1.00	0.00
20.88	15.88	2.00	0.00	1.00	0.00	20.95	15.94	2.00	0.00	1.00	0.00
21.00	14.70	2.00	0.00	1.00	0.00	21.08	16.44	2.00	0.00	1.00	0.00
21.13	16.42	2.00	0.00	1.00	0.00	21.22	16.79	2.00	0.00	1.00	0.00
21.29	16.92	2.00	0.00	1.00	0.00	21.36	16.89	2.00	0.00	1.00	0.00
21.42	16.78	2.00	0.00	1.00	0.00	21.49	16.76	2.00	0.00	1.00	0.00
21.55	16.73	2.00	0.00	1.00	0.00	21.62	16.70	2.00	0.00	1.00	0.00
21.65	16.84	2.00	0.00	1.00	0.00	21.72	16.97	2.00	0.00	1.00	0.00
21.79	17.10	2.00	0.00	1.00	0.00	21.85	16.99	2.00	0.00	1.00	0.00
21.92	16.96	2.00	0.00	1.00	0.00	21.99	17.41	2.00	0.00	1.00	0.00
22.06	17.93	2.00	0.00	1.00	0.00	22.12	18.46	2.00	0.00	1.00	0.00
22.19	18.59	2.00	0.00	1.00	0.00	22.26	18.56	2.00	0.00	1.00	0.00
22.32	18.53	2.00	0.00	1.00	0.00	22.39	20.22	2.00	0.00	1.00	0.00
22.45	24.28	2.00	0.00	1.00	0.00	22.52	32.16	2.00	0.00	1.00	0.00
22.59	103.34	0.16	3.11	1.00	0.03	22.66	112.56	0.18	2.84	1.00	0.02
22.73	119.12	0.19	2.68	1.00	0.02	22.79	124.28	0.21	2.56	1.00	0.02
22.86	127.50	0.22	2.49	1.00	0.02	22.93	129.57	0.23	2.44	1.00	0.02
22.99	130.94	0.23	2.42	1.00	0.02	23.05	128.69	0.22	2.46	1.00	0.02
23.10	132.29	0.24	2.39	1.00	0.01	23.19	136.12	0.25	2.31	1.00	0.03
23.26	139.52	0.27	2.25	1.00	0.02	23.32	143.47	0.29	2.18	1.00	0.02
23.39	146.63	0.31	2.13	1.00	0.02	23.45	149.58	0.33	2.08	1.00	0.02
23.52	152.08	0.35	2.04	1.00	0.02	23.59	154.15	0.37	2.01	1.00	0.02
23.65	154.99	0.38	2.00	1.00	0.02	23.72	154.82	0.38	2.00	1.00	0.02
23.78	153.03	0.36	2.03	1.00	0.02	23.82	151.15	0.35	2.06	1.00	0.01
23.89	145.80	0.31	2.14	1.00	0.02	23.96	138.77	0.26	2.27	1.00	0.02
24.02	129.95	0.23	2.44	1.00	0.02	24.09	119.22	0.19	2.67	1.00	0.02
24.16	107.54	0.17	2.98	1.00	0.02	24.22	34.80	2.00	0.00	1.00	0.00
24.29	27.82	2.00	0.00	1.00	0.00	24.36	23.21	2.00	0.00	1.00	0.00
24.43	20.23	2.00	0.00	1.00	0.00	24.49	18.84	2.00	0.00	1.00	0.00
24.56	18.81	2.00	0.00	1.00	0.00	24.63	21.04	2.00	0.00	1.00	0.00
24.69	26.05	2.00	0.00	1.00	0.00	24.76	34.92	2.00	0.00	1.00	0.00
24.83	107.77	0.17	2.97	1.00	0.02	24.89	115.77	0.18	2.76	1.00	0.02
24.96	121.79	0.20	2.61	1.00	0.02	25.03	127.64	0.22	2.48	1.00	0.02
25.09	133.72	0.24	2.36	1.00	0.02	25.16	138.50	0.26	2.27	1.00	0.02
25.23	142.67	0.28	2.20	1.00	0.02	25.29	146.81	0.31	2.13	1.00	0.02
25.36	149.98	0.33	2.08	1.00	0.02	25.43	149.01	0.32	2.09	1.00	0.02
25.49	145.76	0.30	2.14	1.00	0.02	25.53	142.78	0.28	2.19	1.00	0.01
25.60	135.80	0.25	2.32	1.00	0.02	25.66	127.90	0.22	2.48	1.00	0.02
25.73	116.31	0.18	2.75	1.00	0.02	25.80	107.47	0.16	2.98	1.00	0.02
25.85	37.84	2.00	0.00	1.00	0.00	25.93	33.12	2.00	0.00	1.00	0.00
25.99	28.98	2.00	0.00	1.00	0.00	26.07	22.72	2.00	0.00	1.00	0.00
26.13	21.08	2.00	0.00	1.00	0.00	26.18	20.10	2.00	0.00	1.00	0.00
26.26	18.98	2.00	0.00	1.00	0.00	26.32	18.52	2.00	0.00	1.00	0.00
26.39	18.49	2.00	0.00	1.00	0.00	26.46	18.46	2.00	0.00	1.00	0.00
26.51	18.15	2.00	0.00	1.00	0.00	26.58	18.12	2.00	0.00	1.00	0.00
26.66	19.76	2.00	0.00	1.00	0.00	26.72	22.48	2.00	0.00	1.00	0.00
26.80	29.66	2.00	0.00	1.00	0.00	26.85	34.19	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
26.91	99.42	0.15	3.23	1.00	0.02	26.98	101.70	0.15	3.16	1.00	0.03
27.04	101.79	0.15	3.16	1.00	0.02	27.11	37.13	2.00	0.00	1.00	0.00
27.19	32.96	2.00	0.00	1.00	0.00	27.24	30.51	2.00	0.00	1.00	0.00
27.30	28.87	2.00	0.00	1.00	0.00	27.37	26.30	2.00	0.00	1.00	0.00
27.43	26.04	2.00	0.00	1.00	0.00	27.52	28.16	2.00	0.00	1.00	0.00
27.58	30.59	2.00	0.00	1.00	0.00	27.63	33.40	2.00	0.00	1.00	0.00
27.72	103.52	0.16	3.10	1.00	0.03	27.79	109.73	0.17	2.92	1.00	0.02
27.85	114.62	0.18	2.79	1.00	0.02	27.89	115.91	0.18	2.76	1.00	0.01
27.95	118.05	0.18	2.70	1.00	0.02	28.02	120.60	0.19	2.64	1.00	0.02
28.09	122.80	0.20	2.59	1.00	0.02	28.16	124.57	0.20	2.55	1.00	0.02
28.23	125.88	0.20	2.52	1.00	0.02	28.28	126.25	0.21	2.51	1.00	0.02
28.36	127.10	0.21	2.50	1.00	0.02	28.42	129.46	0.22	2.45	1.00	0.02
28.48	131.61	0.22	2.40	1.00	0.02	28.57	135.80	0.24	2.32	1.00	0.02
28.63	138.14	0.25	2.28	1.00	0.02	28.69	140.16	0.26	2.24	1.00	0.02
28.76	141.92	0.27	2.21	1.00	0.02	28.82	142.92	0.28	2.19	1.00	0.02
28.89	143.46	0.28	2.18	1.00	0.02	28.96	143.68	0.28	2.18	1.00	0.02
29.02	142.99	0.28	2.19	1.00	0.02	29.09	141.89	0.27	2.21	1.00	0.02
29.16	139.94	0.26	2.24	1.00	0.02	29.23	137.44	0.25	2.29	1.00	0.02
29.29	133.82	0.23	2.36	1.00	0.02	29.36	129.66	0.22	2.44	1.00	0.02
29.43	123.61	0.20	2.57	1.00	0.02	29.49	116.02	0.18	2.75	1.00	0.02
29.56	106.47	0.16	3.01	1.00	0.02	29.59	38.46	2.00	0.00	1.00	0.00
29.66	29.82	2.00	0.00	1.00	0.00	29.73	23.17	2.00	0.00	1.00	0.00
29.79	21.28	2.00	0.00	1.00	0.00	29.88	17.55	2.00	0.00	1.00	0.00
29.94	15.57	2.00	0.00	1.00	0.00	30.01	14.74	2.00	0.00	1.00	0.00
30.06	14.79	2.00	0.00	1.00	0.00	30.12	13.57	2.00	0.00	1.00	0.00
30.19	12.69	2.00	0.00	1.00	0.00	30.26	12.41	2.00	0.00	1.00	0.00
30.32	12.26	2.00	0.00	1.00	0.00	30.39	11.98	2.00	0.00	1.00	0.00
30.45	11.77	2.00	0.00	1.00	0.00	30.52	11.75	2.00	0.00	1.00	0.00
30.59	11.74	2.00	0.00	1.00	0.00	30.66	11.72	2.00	0.00	1.00	0.00
30.72	11.84	2.00	0.00	1.00	0.00	30.79	11.96	2.00	0.00	1.00	0.00
30.85	12.14	2.00	0.00	1.00	0.00	30.92	13.11	2.00	0.00	1.00	0.00
30.97	13.43	2.00	0.00	1.00	0.00	31.07	13.93	2.00	0.00	1.00	0.00
31.10	13.73	2.00	0.00	1.00	0.00	31.19	12.72	2.00	0.00	1.00	0.00
31.24	12.32	2.00	0.00	1.00	0.00	31.30	11.66	2.00	0.00	1.00	0.00
31.38	12.03	2.00	0.00	1.00	0.00	31.43	11.69	2.00	0.00	1.00	0.00
31.50	11.97	2.00	0.00	1.00	0.00	31.57	11.86	2.00	0.00	1.00	0.00
31.63	11.91	2.00	0.00	1.00	0.00	31.70	11.70	2.00	0.00	1.00	0.00
31.77	11.43	2.00	0.00	1.00	0.00	31.84	11.03	2.00	0.00	1.00	0.00
31.90	11.27	2.00	0.00	1.00	0.00	31.97	12.16	2.00	0.00	1.00	0.00
32.03	13.76	2.00	0.00	1.00	0.00	32.10	15.63	2.00	0.00	1.00	0.00
32.17	16.01	2.00	0.00	1.00	0.00	32.23	14.88	2.00	0.00	1.00	0.00
32.29	13.38	2.00	0.00	1.00	0.00	32.35	12.46	2.00	0.00	1.00	0.00
32.42	11.81	2.00	0.00	1.00	0.00	32.49	11.79	2.00	0.00	1.00	0.00
32.56	12.16	2.00	0.00	1.00	0.00	32.62	13.18	2.00	0.00	1.00	0.00
32.68	14.19	2.00	0.00	1.00	0.00	32.75	14.82	2.00	0.00	1.00	0.00
32.82	14.92	2.00	0.00	1.00	0.00	32.88	15.16	2.00	0.00	1.00	0.00
32.95	16.50	2.00	0.00	1.00	0.00	33.01	18.82	2.00	0.00	1.00	0.00
33.08	22.79	2.00	0.00	1.00	0.00	33.15	28.20	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
33.21	33.15	2.00	0.00	1.00	0.00	33.28	34.54	2.00	0.00	1.00	0.00
33.35	33.50	2.00	0.00	1.00	0.00	33.41	30.23	2.00	0.00	1.00	0.00
33.48	26.67	2.00	0.00	1.00	0.00	33.55	22.36	2.00	0.00	1.00	0.00
33.62	19.92	2.00	0.00	1.00	0.00	33.68	18.99	2.00	0.00	1.00	0.00
33.75	17.16	2.00	0.00	1.00	0.00	33.82	14.92	2.00	0.00	1.00	0.00
33.88	12.95	2.00	0.00	1.00	0.00	33.95	11.49	2.00	0.00	1.00	0.00
34.02	10.43	2.00	0.00	1.00	0.00	34.09	9.67	2.00	0.00	1.00	0.00
34.15	9.35	2.00	0.00	1.00	0.00	34.19	9.66	2.00	0.00	1.00	0.00
34.25	8.85	2.00	0.00	1.00	0.00	34.33	9.63	2.00	0.00	1.00	0.00
34.40	9.68	2.00	0.00	1.00	0.00	34.46	9.67	2.00	0.00	1.00	0.00
34.52	9.66	2.00	0.00	1.00	0.00	34.59	9.65	2.00	0.00	1.00	0.00
34.66	9.76	2.00	0.00	1.00	0.00	34.73	10.00	2.00	0.00	1.00	0.00
34.79	10.35	2.00	0.00	1.00	0.00	34.86	10.65	2.00	0.00	1.00	0.00
34.93	11.13	2.00	0.00	1.00	0.00	34.99	11.42	2.00	0.00	1.00	0.00
35.06	11.16	2.00	0.00	1.00	0.00	35.13	10.73	2.00	0.00	1.00	0.00
35.20	10.53	2.00	0.00	1.00	0.00	35.26	10.64	2.00	0.00	1.00	0.00
35.33	11.00	2.00	0.00	1.00	0.00	35.40	11.71	2.00	0.00	1.00	0.00
35.47	12.56	2.00	0.00	1.00	0.00	35.53	13.04	2.00	0.00	1.00	0.00
35.60	13.33	2.00	0.00	1.00	0.00	35.66	13.99	2.00	0.00	1.00	0.00
35.70	14.78	2.00	0.00	1.00	0.00	35.77	15.44	2.00	0.00	1.00	0.00
35.83	15.37	2.00	0.00	1.00	0.00	35.90	16.84	2.00	0.00	1.00	0.00
35.97	19.63	2.00	0.00	1.00	0.00	36.03	20.80	2.00	0.00	1.00	0.00
36.10	19.21	2.00	0.00	1.00	0.00	36.17	16.20	2.00	0.00	1.00	0.00
36.23	13.86	2.00	0.00	1.00	0.00	36.30	16.39	2.00	0.00	1.00	0.00
36.37	12.38	2.00	0.00	1.00	0.00	36.43	16.57	2.00	0.00	1.00	0.00
36.50	25.48	2.00	0.00	1.00	0.00	36.57	33.10	2.00	0.00	1.00	0.00
36.64	101.63	0.15	3.16	1.00	0.03	36.70	105.63	0.15	3.04	1.00	0.02
36.77	107.40	0.16	2.99	1.00	0.02	36.84	39.94	2.00	0.00	1.00	0.00
36.91	32.16	2.00	0.00	1.00	0.00	36.97	24.96	2.00	0.00	1.00	0.00
37.04	20.11	2.00	0.00	1.00	0.00	37.11	17.31	2.00	0.00	1.00	0.00
37.14	16.57	2.00	0.00	1.00	0.00	37.21	15.15	2.00	0.00	1.00	0.00
37.27	14.17	2.00	0.00	1.00	0.00	37.34	14.40	2.00	0.00	1.00	0.00
37.41	15.47	2.00	0.00	1.00	0.00	37.48	16.97	2.00	0.00	1.00	0.00
37.54	18.29	2.00	0.00	1.00	0.00	37.61	19.50	2.00	0.00	1.00	0.00
37.68	20.40	2.00	0.00	1.00	0.00	37.74	21.56	2.00	0.00	1.00	0.00
37.81	23.21	2.00	0.00	1.00	0.00	37.88	23.00	2.00	0.00	1.00	0.00
37.94	23.04	2.00	0.00	1.00	0.00	38.01	23.02	2.00	0.00	1.00	0.00
38.08	23.07	2.00	0.00	1.00	0.00	38.15	24.60	2.00	0.00	1.00	0.00
38.21	27.37	2.00	0.00	1.00	0.00	38.28	31.44	2.00	0.00	1.00	0.00
38.34	36.93	2.00	0.00	1.00	0.00	38.41	44.60	2.00	0.00	1.00	0.00
38.48	117.87	0.18	2.71	1.00	0.02	38.55	125.32	0.19	2.53	1.00	0.02
38.61	128.61	0.20	2.46	1.00	0.02	38.68	127.73	0.20	2.48	1.00	0.02
38.75	122.25	0.19	2.60	1.00	0.02	38.78	118.52	0.18	2.69	1.00	0.01
38.85	110.08	0.16	2.91	1.00	0.02	38.92	38.24	2.00	0.00	1.00	0.00
38.98	31.27	2.00	0.00	1.00	0.00	39.05	26.62	2.00	0.00	1.00	0.00
39.11	22.76	2.00	0.00	1.00	0.00	39.19	22.97	2.00	0.00	1.00	0.00
39.24	21.44	2.00	0.00	1.00	0.00	39.32	17.80	2.00	0.00	1.00	0.00
39.38	17.78	2.00	0.00	1.00	0.00	39.45	17.76	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
39.51	17.75	2.00	0.00	1.00	0.00	39.58	22.06	2.00	0.00	1.00	0.00
39.64	25.08	2.00	0.00	1.00	0.00	39.72	29.04	2.00	0.00	1.00	0.00
39.77	30.69	2.00	0.00	1.00	0.00	39.84	32.57	2.00	0.00	1.00	0.00
39.90	32.98	2.00	0.00	1.00	0.00	39.96	30.39	2.00	0.00	1.00	0.00
40.03	34.80	2.00	0.00	1.00	0.00	40.09	35.59	2.00	0.00	1.00	0.00
40.17	31.53	2.00	0.00	1.00	0.00	40.25	27.37	2.00	0.00	1.00	0.00
40.31	24.37	2.00	0.00	1.00	0.00	40.37	23.37	2.00	0.00	1.00	0.00
40.42	25.49	2.00	0.00	1.00	0.00	40.51	28.87	2.00	0.00	1.00	0.00
40.56	28.78	2.00	0.00	1.00	0.00	40.62	28.09	2.00	0.00	1.00	0.00
40.71	26.84	2.00	0.00	1.00	0.00	40.78	27.06	2.00	0.00	1.00	0.00
40.85	29.42	2.00	0.00	1.00	0.00	40.91	32.49	2.00	0.00	1.00	0.00
40.95	34.15	2.00	0.00	1.00	0.00	41.02	37.17	2.00	0.00	1.00	0.00
41.08	40.88	2.00	0.00	1.00	0.00	41.15	113.57	0.17	2.82	1.00	0.02
41.22	128.59	0.20	2.46	1.00	0.02	41.28	143.21	0.26	2.19	1.00	0.02
41.34	149.82	0.30	2.08	1.00	0.01	41.44	156.46	0.36	1.95	1.00	0.02
41.50	156.96	0.36	1.91	1.00	0.01	41.57	156.30	0.36	1.96	1.00	0.02
41.60	155.68	0.35	1.99	1.00	0.01	41.67	154.75	0.34	2.00	1.00	0.02
41.74	154.63	0.34	2.00	1.00	0.02	41.81	155.33	0.35	1.99	1.00	0.02
41.87	155.67	0.35	1.99	1.00	0.02	41.94	155.27	0.35	2.00	1.00	0.02
42.00	146.73	0.28	2.13	1.00	0.01	42.07	152.97	0.33	2.03	1.00	0.02
42.14	152.00	0.32	2.04	1.00	0.02	42.20	152.73	0.33	2.03	1.00	0.01
42.28	150.37	0.31	2.07	1.00	0.02	42.35	148.17	0.29	2.10	1.00	0.02
42.42	146.06	0.28	2.14	1.00	0.02	42.48	145.00	0.27	2.16	1.00	0.02
42.55	144.69	0.27	2.16	1.00	0.02	42.62	143.62	0.27	2.18	1.00	0.02
42.68	141.13	0.25	2.22	1.00	0.02	42.72	139.28	0.24	2.26	1.00	0.01
42.78	135.22	0.23	2.33	1.00	0.02	42.85	130.74	0.21	2.42	1.00	0.02
42.92	124.51	0.19	2.55	1.00	0.02	42.99	117.80	0.18	2.71	1.00	0.02
43.05	47.42	2.00	0.00	1.00	0.00	43.12	45.09	2.00	0.00	1.00	0.00
43.18	44.02	2.00	0.00	1.00	0.00	43.25	42.81	2.00	0.00	1.00	0.00
43.32	40.06	2.00	0.00	1.00	0.00	43.38	34.89	2.00	0.00	1.00	0.00
43.45	30.20	2.00	0.00	1.00	0.00	43.52	27.01	2.00	0.00	1.00	0.00
43.59	25.28	2.00	0.00	1.00	0.00	43.65	24.09	2.00	0.00	1.00	0.00
43.72	23.21	2.00	0.00	1.00	0.00	43.79	22.55	2.00	0.00	1.00	0.00
43.86	21.72	2.00	0.00	1.00	0.00	43.92	20.67	2.00	0.00	1.00	0.00
43.98	24.71	2.00	0.00	1.00	0.00	44.04	31.05	2.00	0.00	1.00	0.00
44.12	40.92	2.00	0.00	1.00	0.00	44.19	113.39	0.17	2.82	1.00	0.02
44.25	120.36	0.18	2.65	1.00	0.02	44.31	125.48	0.19	2.53	1.00	0.02
44.38	128.83	0.20	2.46	1.00	0.02	44.45	131.33	0.21	2.41	1.00	0.02
44.52	133.17	0.22	2.37	1.00	0.02	44.58	134.37	0.22	2.35	1.00	0.02
44.65	135.66	0.23	2.32	1.00	0.02	44.72	137.19	0.23	2.29	1.00	0.02
44.78	138.43	0.24	2.27	1.00	0.02	44.85	139.69	0.25	2.25	1.00	0.02
44.88	140.36	0.25	2.24	1.00	0.01	44.95	141.14	0.25	2.22	1.00	0.02
45.02	141.57	0.26	2.22	1.00	0.02	45.09	141.79	0.26	2.21	1.00	0.02
45.16	142.11	0.26	2.21	1.00	0.02	45.22	142.03	0.26	2.21	1.00	0.02
45.29	141.92	0.26	2.21	1.00	0.02	45.35	141.84	0.26	2.21	1.00	0.02
45.42	142.12	0.26	2.21	1.00	0.02	45.49	142.67	0.26	2.20	1.00	0.02
45.56	142.80	0.26	2.19	1.00	0.02	45.62	142.80	0.26	2.19	1.00	0.02
45.69	142.45	0.26	2.20	1.00	0.02	45.76	141.74	0.26	2.21	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
45.82	140.61	0.25	2.23	1.00	0.02	45.89	139.37	0.24	2.25	1.00	0.02
45.96	137.67	0.24	2.29	1.00	0.02	46.02	135.54	0.23	2.33	1.00	0.02
46.09	133.85	0.22	2.36	1.00	0.02	46.16	131.77	0.21	2.40	1.00	0.02
46.22	129.22	0.21	2.45	1.00	0.02	46.29	126.99	0.20	2.50	1.00	0.02
46.36	125.57	0.19	2.53	1.00	0.02	46.42	124.36	0.19	2.56	1.00	0.02
46.46	123.85	0.19	2.57	1.00	0.01	46.52	122.42	0.19	2.60	1.00	0.02
46.61	121.10	0.18	2.63	1.00	0.03	46.66	119.70	0.18	2.66	1.00	0.02
46.74	114.91	0.17	2.78	1.00	0.03	46.79	112.58	0.17	2.84	1.00	0.02
46.86	44.69	2.00	0.00	1.00	0.00	46.94	40.55	2.00	0.00	1.00	0.00
46.99	37.27	2.00	0.00	1.00	0.00	47.06	32.09	2.00	0.00	1.00	0.00
47.14	26.40	2.00	0.00	1.00	0.00	47.19	23.12	2.00	0.00	1.00	0.00
47.25	20.37	2.00	0.00	1.00	0.00	47.34	20.25	2.00	0.00	1.00	0.00
47.39	20.23	2.00	0.00	1.00	0.00	47.45	20.11	2.00	0.00	1.00	0.00
47.51	27.05	2.00	0.00	1.00	0.00	47.58	37.22	2.00	0.00	1.00	0.00
47.65	105.99	0.15	3.03	1.00	0.02	47.72	107.78	0.16	2.97	1.00	0.02
47.78	42.67	2.00	0.00	1.00	0.00	47.85	38.01	2.00	0.00	1.00	0.00
47.91	33.40	2.00	0.00	1.00	0.00	47.98	28.53	2.00	0.00	1.00	0.00
48.05	25.23	2.00	0.00	1.00	0.00	48.11	22.47	2.00	0.00	1.00	0.00
48.18	20.14	2.00	0.00	1.00	0.00	48.24	18.77	2.00	0.00	1.00	0.00
48.31	18.15	2.00	0.00	1.00	0.00	48.38	17.98	2.00	0.00	1.00	0.00
48.45	18.93	2.00	0.00	1.00	0.00	48.52	22.92	2.00	0.00	1.00	0.00
48.58	34.98	2.00	0.00	1.00	0.00	48.65	117.63	0.18	2.71	1.00	0.02
48.72	133.26	0.22	2.37	1.00	0.02	48.78	144.20	0.27	2.17	1.00	0.02
48.85	153.91	0.33	2.02	1.00	0.02	48.92	161.83	0.41	1.62	1.00	0.01
48.95	164.63	0.45	1.47	1.00	0.01	49.02	164.36	0.45	1.49	1.00	0.01
49.09	162.47	0.42	1.59	1.00	0.01	49.16	171.35	0.56	1.17	1.00	0.01
49.23	173.61	0.60	1.08	1.00	0.01	49.29	179.11	0.74	0.89	1.00	0.01
49.35	179.50	0.75	0.87	1.00	0.01	49.42	186.92	1.03	0.66	1.00	0.01
49.49	192.58	1.34	0.36	1.00	0.00	49.56	195.88	1.57	0.20	1.00	0.00
49.62	195.96	1.58	0.20	1.00	0.00	49.69	194.35	1.46	0.27	1.00	0.00
49.76	195.63	1.55	0.21	1.00	0.00	49.82	196.62	1.63	0.17	1.00	0.00
49.89	197.65	1.72	0.12	1.00	0.00	49.95	198.63	1.82	0.08	1.00	0.00
50.00	197.32	2.00	0.00	1.00	0.00	50.07	198.26	2.00	0.00	1.00	0.00
50.14	197.42	2.00	0.00	1.00	0.00	50.20	196.65	2.00	0.00	1.00	0.00
50.28	195.93	2.00	0.00	1.00	0.00	50.35	194.39	2.00	0.00	1.00	0.00
50.41	193.80	2.00	0.00	1.00	0.00	50.48	193.66	2.00	0.00	1.00	0.00
50.55	192.61	2.00	0.00	1.00	0.00	50.61	192.62	2.00	0.00	1.00	0.00
50.68	192.13	2.00	0.00	1.00	0.00	50.74	189.10	2.00	0.00	1.00	0.00
50.81	185.29	2.00	0.00	1.00	0.00	50.88	182.23	2.00	0.00	1.00	0.00
50.94	178.38	2.00	0.00	1.00	0.00	51.01	172.51	2.00	0.00	1.00	0.00
51.08	166.29	2.00	0.00	1.00	0.00	51.15	161.05	2.00	0.00	1.00	0.00
51.21	156.93	2.00	0.00	1.00	0.00	51.28	153.62	2.00	0.00	1.00	0.00
51.34	150.19	2.00	0.00	1.00	0.00	51.38	148.51	2.00	0.00	1.00	0.00
51.45	145.72	2.00	0.00	1.00	0.00	51.51	143.73	2.00	0.00	1.00	0.00
51.58	141.31	2.00	0.00	1.00	0.00	51.65	136.92	2.00	0.00	1.00	0.00
51.71	136.89	2.00	0.00	1.00	0.00	51.78	137.46	2.00	0.00	1.00	0.00
51.85	137.62	2.00	0.00	1.00	0.00	51.92	138.35	2.00	0.00	1.00	0.00
51.99	138.65	2.00	0.00	1.00	0.00	52.05	138.78	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
52.11	138.89	2.00	0.00	1.00	0.00	52.18	137.36	2.00	0.00	1.00	0.00
52.24	135.81	2.00	0.00	1.00	0.00	52.31	134.05	2.00	0.00	1.00	0.00
52.38	132.20	2.00	0.00	1.00	0.00	52.44	129.18	2.00	0.00	1.00	0.00
52.51	125.83	2.00	0.00	1.00	0.00	52.58	125.85	2.00	0.00	1.00	0.00
52.64	125.90	2.00	0.00	1.00	0.00	52.71	125.74	2.00	0.00	1.00	0.00
52.78	127.71	2.00	0.00	1.00	0.00	52.84	128.30	2.00	0.00	1.00	0.00
52.91	127.40	2.00	0.00	1.00	0.00	52.98	126.46	2.00	0.00	1.00	0.00
53.04	127.06	2.00	0.00	1.00	0.00	53.11	128.80	2.00	0.00	1.00	0.00
53.17	131.75	2.00	0.00	1.00	0.00	53.24	137.02	2.00	0.00	1.00	0.00
53.31	142.94	2.00	0.00	1.00	0.00	53.38	148.35	2.00	0.00	1.00	0.00
53.42	151.76	2.00	0.00	1.00	0.00	53.49	157.03	2.00	0.00	1.00	0.00
53.56	162.38	2.00	0.00	1.00	0.00	53.63	166.74	2.00	0.00	1.00	0.00
53.68	169.16	2.00	0.00	1.00	0.00	53.75	172.87	2.00	0.00	1.00	0.00
53.82	177.22	2.00	0.00	1.00	0.00	53.89	182.62	2.00	0.00	1.00	0.00
53.94	176.68	2.00	0.00	1.00	0.00	54.00	159.84	2.00	0.00	1.00	0.00
54.07	157.78	2.00	0.00	1.00	0.00	54.15	164.98	2.00	0.00	1.00	0.00
54.21	169.63	2.00	0.00	1.00	0.00	54.27	175.31	2.00	0.00	1.00	0.00
54.34	181.91	2.00	0.00	1.00	0.00	54.40	185.91	2.00	0.00	1.00	0.00
54.47	188.19	2.00	0.00	1.00	0.00	54.53	190.82	2.00	0.00	1.00	0.00
54.60	196.01	2.00	0.00	1.00	0.00	54.67	200.07	2.00	0.00	1.00	0.00
54.73	202.97	2.00	0.00	1.00	0.00	54.80	205.23	2.00	0.00	1.00	0.00
54.87	206.73	2.00	0.00	1.00	0.00	54.93	209.20	2.00	0.00	1.00	0.00
54.99	211.43	2.00	0.00	1.00	0.00	55.05	214.12	2.00	0.00	1.00	0.00
55.12	215.43	2.00	0.00	1.00	0.00	55.19	216.83	2.00	0.00	1.00	0.00
55.26	217.81	2.00	0.00	1.00	0.00	55.33	218.85	2.00	0.00	1.00	0.00
55.39	219.80	2.00	0.00	1.00	0.00	55.45	220.54	2.00	0.00	1.00	0.00
55.52	221.32	2.00	0.00	1.00	0.00	55.59	217.39	2.00	0.00	1.00	0.00
55.64	209.58	2.00	0.00	1.00	0.00	55.72	210.56	2.00	0.00	1.00	0.00
55.79	211.11	2.00	0.00	1.00	0.00	55.86	211.31	2.00	0.00	1.00	0.00
55.92	210.63	2.00	0.00	1.00	0.00	55.98	201.91	2.00	0.00	1.00	0.00
56.05	206.89	2.00	0.00	1.00	0.00	56.11	205.14	2.00	0.00	1.00	0.00
56.18	203.47	2.00	0.00	1.00	0.00	56.24	202.99	2.00	0.00	1.00	0.00
56.31	201.28	2.00	0.00	1.00	0.00	56.37	200.15	2.00	0.00	1.00	0.00
56.45	198.91	2.00	0.00	1.00	0.00	56.51	197.77	2.00	0.00	1.00	0.00
56.58	196.61	2.00	0.00	1.00	0.00	56.64	196.06	2.00	0.00	1.00	0.00
56.71	196.77	2.00	0.00	1.00	0.00	56.78	197.83	2.00	0.00	1.00	0.00
56.84	198.34	2.00	0.00	1.00	0.00	56.91	198.79	2.00	0.00	1.00	0.00
56.98	200.08	2.00	0.00	1.00	0.00	57.05	201.35	2.00	0.00	1.00	0.00
57.11	202.08	2.00	0.00	1.00	0.00	57.18	166.31	2.00	0.00	1.00	0.00
57.24	150.42	2.00	0.00	1.00	0.00	57.31	153.43	2.00	0.00	1.00	0.00
57.38	159.14	2.00	0.00	1.00	0.00	57.45	164.77	2.00	0.00	1.00	0.00
57.48	167.32	2.00	0.00	1.00	0.00	57.56	171.08	2.00	0.00	1.00	0.00
57.62	172.90	2.00	0.00	1.00	0.00	57.71	177.33	2.00	0.00	1.00	0.00
57.77	182.84	2.00	0.00	1.00	0.00	57.84	184.87	2.00	0.00	1.00	0.00
57.91	185.31	2.00	0.00	1.00	0.00	57.97	186.68	2.00	0.00	1.00	0.00
58.01	187.24	2.00	0.00	1.00	0.00	58.08	187.67	2.00	0.00	1.00	0.00
58.14	187.58	2.00	0.00	1.00	0.00	58.21	186.90	2.00	0.00	1.00	0.00
58.28	185.90	2.00	0.00	1.00	0.00	58.34	184.57	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
58.41	182.85	2.00	0.00	1.00	0.00	58.48	179.12	2.00	0.00	1.00	0.00
58.54	175.49	2.00	0.00	1.00	0.00	58.61	174.05	2.00	0.00	1.00	0.00
58.67	158.22	2.00	0.00	1.00	0.00	58.74	147.32	2.00	0.00	1.00	0.00
58.80	149.80	2.00	0.00	1.00	0.00	58.87	151.40	2.00	0.00	1.00	0.00
58.94	154.92	2.00	0.00	1.00	0.00	59.01	161.41	2.00	0.00	1.00	0.00
59.07	167.89	2.00	0.00	1.00	0.00	59.13	174.10	2.00	0.00	1.00	0.00
59.22	177.96	2.00	0.00	1.00	0.00	59.28	185.00	2.00	0.00	1.00	0.00
59.32	188.46	2.00	0.00	1.00	0.00	59.38	194.52	2.00	0.00	1.00	0.00
59.45	198.33	2.00	0.00	1.00	0.00	59.52	200.71	2.00	0.00	1.00	0.00
59.59	202.02	2.00	0.00	1.00	0.00	59.65	194.00	2.00	0.00	1.00	0.00
59.72	191.33	2.00	0.00	1.00	0.00	59.79	189.65	2.00	0.00	1.00	0.00
59.85	189.59	2.00	0.00	1.00	0.00	59.92	188.65	2.00	0.00	1.00	0.00
59.98	186.77	2.00	0.00	1.00	0.00	60.04	185.15	2.00	0.00	1.00	0.00
60.11	179.15	2.00	0.00	1.00	0.00	60.19	178.41	2.00	0.00	1.00	0.00
60.25	177.42	2.00	0.00	1.00	0.00	60.32	177.69	2.00	0.00	1.00	0.00
60.38	179.83	2.00	0.00	1.00	0.00	60.46	180.63	2.00	0.00	1.00	0.00
60.51	178.92	2.00	0.00	1.00	0.00	60.57	176.48	2.00	0.00	1.00	0.00
60.65	175.24	2.00	0.00	1.00	0.00	60.70	175.52	2.00	0.00	1.00	0.00
60.77	174.59	2.00	0.00	1.00	0.00	60.83	172.68	2.00	0.00	1.00	0.00
60.92	170.21	2.00	0.00	1.00	0.00	60.99	169.25	2.00	0.00	1.00	0.00
61.05	170.00	2.00	0.00	1.00	0.00	61.12	169.44	2.00	0.00	1.00	0.00
61.19	168.83	2.00	0.00	1.00	0.00	61.22	168.53	2.00	0.00	1.00	0.00
61.29	168.61	2.00	0.00	1.00	0.00	61.35	168.79	2.00	0.00	1.00	0.00
61.42	168.85	2.00	0.00	1.00	0.00	61.50	168.95	2.00	0.00	1.00	0.00
61.55	170.12	2.00	0.00	1.00	0.00	61.62	173.11	2.00	0.00	1.00	0.00
61.69	177.10	2.00	0.00	1.00	0.00	61.75	180.85	2.00	0.00	1.00	0.00
61.81	185.72	2.00	0.00	1.00	0.00	61.89	189.24	2.00	0.00	1.00	0.00
61.94	193.01	2.00	0.00	1.00	0.00	62.03	199.41	2.00	0.00	1.00	0.00
62.09	204.13	2.00	0.00	1.00	0.00	62.15	209.34	2.00	0.00	1.00	0.00
62.21	214.96	2.00	0.00	1.00	0.00	62.27	217.46	2.00	0.00	1.00	0.00
62.34	219.44	2.00	0.00	1.00	0.00	62.42	219.57	2.00	0.00	1.00	0.00
62.49	225.26	2.00	0.00	1.00	0.00	62.54	225.29	2.00	0.00	1.00	0.00
62.60	218.15	2.00	0.00	1.00	0.00	62.67	213.29	2.00	0.00	1.00	0.00
62.74	204.33	2.00	0.00	1.00	0.00	62.80	197.74	2.00	0.00	1.00	0.00
62.87	195.37	2.00	0.00	1.00	0.00	62.95	179.10	2.00	0.00	1.00	0.00
63.01	163.74	2.00	0.00	1.00	0.00	63.08	161.80	2.00	0.00	1.00	0.00
63.14	154.33	2.00	0.00	1.00	0.00	63.21	147.74	2.00	0.00	1.00	0.00
63.28	143.27	2.00	0.00	1.00	0.00	63.33	144.86	2.00	0.00	1.00	0.00
63.39	146.42	2.00	0.00	1.00	0.00	63.46	151.24	2.00	0.00	1.00	0.00
63.53	147.83	2.00	0.00	1.00	0.00	63.59	144.07	2.00	0.00	1.00	0.00
63.66	70.58	2.00	0.00	1.00	0.00	63.72	73.74	2.00	0.00	1.00	0.00
63.79	154.67	2.00	0.00	1.00	0.00	63.85	164.96	2.00	0.00	1.00	0.00
63.92	179.42	2.00	0.00	1.00	0.00	63.99	189.26	2.00	0.00	1.00	0.00
64.05	196.59	2.00	0.00	1.00	0.00	64.11	200.47	2.00	0.00	1.00	0.00
64.19	195.91	2.00	0.00	1.00	0.00	64.26	181.33	2.00	0.00	1.00	0.00
64.33	153.38	2.00	0.00	1.00	0.00	64.39	162.59	2.00	0.00	1.00	0.00
64.46	172.14	2.00	0.00	1.00	0.00	64.53	180.99	2.00	0.00	1.00	0.00
64.60	186.85	2.00	0.00	1.00	0.00	64.66	181.21	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
64.70	182.97	2.00	0.00	1.00	0.00	64.78	179.04	2.00	0.00	1.00	0.00
64.85	183.94	2.00	0.00	1.00	0.00	64.91	191.70	2.00	0.00	1.00	0.00
64.97	207.69	2.00	0.00	1.00	0.00	65.04	229.16	2.00	0.00	1.00	0.00
65.11	251.61	2.00	0.00	1.00	0.00	65.16	260.13	2.00	0.00	1.00	0.00
65.22	267.20	2.00	0.00	1.00	0.00	65.29	266.38	2.00	0.00	1.00	0.00
65.36	271.59	2.00	0.00	1.00	0.00	65.42	270.27	2.00	0.00	1.00	0.00
65.49	267.22	2.00	0.00	1.00	0.00	65.57	264.43	2.00	0.00	1.00	0.00
65.63	260.75	2.00	0.00	1.00	0.00	65.71	255.64	2.00	0.00	1.00	0.00
65.76	246.27	2.00	0.00	1.00	0.00	65.82	169.32	2.00	0.00	1.00	0.00
65.89	212.79	2.00	0.00	1.00	0.00	65.95	202.87	2.00	0.00	1.00	0.00
66.02	195.56	2.00	0.00	1.00	0.00	66.09	192.23	2.00	0.00	1.00	0.00
66.14	188.59	2.00	0.00	1.00	0.00	66.21	179.99	2.00	0.00	1.00	0.00
66.28	179.93	2.00	0.00	1.00	0.00	66.35	182.68	2.00	0.00	1.00	0.00
66.41	184.39	2.00	0.00	1.00	0.00	66.48	186.87	2.00	0.00	1.00	0.00
66.55	187.66	2.00	0.00	1.00	0.00	66.61	188.12	2.00	0.00	1.00	0.00
66.68	185.86	2.00	0.00	1.00	0.00	66.75	182.19	2.00	0.00	1.00	0.00
66.81	178.67	2.00	0.00	1.00	0.00	66.87	165.45	2.00	0.00	1.00	0.00
66.93	153.96	2.00	0.00	1.00	0.00	67.00	154.22	2.00	0.00	1.00	0.00
67.06	150.03	2.00	0.00	1.00	0.00	67.14	143.91	2.00	0.00	1.00	0.00
67.21	136.35	2.00	0.00	1.00	0.00	67.27	126.53	2.00	0.00	1.00	0.00
67.34	114.50	2.00	0.00	1.00	0.00	67.41	113.40	2.00	0.00	1.00	0.00
67.47	126.99	2.00	0.00	1.00	0.00	67.54	140.87	2.00	0.00	1.00	0.00
67.61	146.13	2.00	0.00	1.00	0.00	67.67	150.51	2.00	0.00	1.00	0.00
67.74	146.55	2.00	0.00	1.00	0.00	67.81	129.97	2.00	0.00	1.00	0.00
67.87	126.53	2.00	0.00	1.00	0.00	67.94	129.19	2.00	0.00	1.00	0.00
68.01	131.95	2.00	0.00	1.00	0.00	68.07	127.60	2.00	0.00	1.00	0.00
68.12	122.63	2.00	0.00	1.00	0.00	68.20	115.37	2.00	0.00	1.00	0.00
68.25	43.35	2.00	0.00	1.00	0.00	68.31	35.45	2.00	0.00	1.00	0.00
68.38	29.48	2.00	0.00	1.00	0.00	68.44	34.74	2.00	0.00	1.00	0.00
68.51	29.19	2.00	0.00	1.00	0.00	68.58	34.03	2.00	0.00	1.00	0.00
68.64	42.91	2.00	0.00	1.00	0.00	68.71	121.16	2.00	0.00	1.00	0.00
68.78	136.61	2.00	0.00	1.00	0.00	68.83	144.99	2.00	0.00	1.00	0.00
68.91	153.25	2.00	0.00	1.00	0.00	68.99	157.46	2.00	0.00	1.00	0.00
69.05	151.15	2.00	0.00	1.00	0.00	69.11	134.66	2.00	0.00	1.00	0.00
69.17	139.80	2.00	0.00	1.00	0.00	69.24	140.75	2.00	0.00	1.00	0.00
69.31	140.30	2.00	0.00	1.00	0.00	69.37	143.77	2.00	0.00	1.00	0.00
69.44	147.02	2.00	0.00	1.00	0.00	69.51	148.91	2.00	0.00	1.00	0.00
69.56	150.82	2.00	0.00	1.00	0.00	69.64	158.13	2.00	0.00	1.00	0.00
69.69	160.90	2.00	0.00	1.00	0.00	69.78	167.43	2.00	0.00	1.00	0.00
69.82	173.61	2.00	0.00	1.00	0.00	69.89	168.23	2.00	0.00	1.00	0.00
69.95	159.30	2.00	0.00	1.00	0.00	70.02	170.17	2.00	0.00	1.00	0.00
70.08	190.24	2.00	0.00	1.00	0.00	70.15	191.50	2.00	0.00	1.00	0.00
70.21	171.42	2.00	0.00	1.00	0.00	70.30	176.65	2.00	0.00	1.00	0.00
70.37	167.96	2.00	0.00	1.00	0.00	70.41	178.71	2.00	0.00	1.00	0.00
70.49	169.44	2.00	0.00	1.00	0.00	70.55	180.14	2.00	0.00	1.00	0.00
70.61	190.01	2.00	0.00	1.00	0.00	70.67	195.01	2.00	0.00	1.00	0.00
70.74	198.00	2.00	0.00	1.00	0.00	70.81	189.74	2.00	0.00	1.00	0.00
70.88	185.10	2.00	0.00	1.00	0.00	70.95	174.40	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
71.01	170.15	2.00	0.00	1.00	0.00	71.08	170.58	2.00	0.00	1.00	0.00
71.15	170.13	2.00	0.00	1.00	0.00	71.20	167.88	2.00	0.00	1.00	0.00
71.27	170.43	2.00	0.00	1.00	0.00	71.33	165.60	2.00	0.00	1.00	0.00
71.41	170.72	2.00	0.00	1.00	0.00	71.47	171.97	2.00	0.00	1.00	0.00
71.55	171.42	2.00	0.00	1.00	0.00	71.60	167.61	2.00	0.00	1.00	0.00
71.66	169.18	2.00	0.00	1.00	0.00	71.72	170.07	2.00	0.00	1.00	0.00
71.81	183.08	2.00	0.00	1.00	0.00	71.87	194.85	2.00	0.00	1.00	0.00
71.94	202.05	2.00	0.00	1.00	0.00	72.00	207.15	2.00	0.00	1.00	0.00
72.07	215.30	2.00	0.00	1.00	0.00	72.14	218.33	2.00	0.00	1.00	0.00
72.20	222.02	2.00	0.00	1.00	0.00	72.27	209.88	2.00	0.00	1.00	0.00
72.34	204.57	2.00	0.00	1.00	0.00	72.41	202.15	2.00	0.00	1.00	0.00
72.47	203.59	2.00	0.00	1.00	0.00	72.51	204.47	2.00	0.00	1.00	0.00
72.58	204.29	2.00	0.00	1.00	0.00	72.64	57.58	2.00	0.00	1.00	0.00
72.72	207.04	2.00	0.00	1.00	0.00	72.80	182.65	2.00	0.00	1.00	0.00
72.86	164.69	2.00	0.00	1.00	0.00	72.92	163.59	2.00	0.00	1.00	0.00
72.97	160.04	2.00	0.00	1.00	0.00	73.06	169.99	2.00	0.00	1.00	0.00
73.12	175.64	2.00	0.00	1.00	0.00	73.19	180.85	2.00	0.00	1.00	0.00
73.25	184.46	2.00	0.00	1.00	0.00	73.32	186.02	2.00	0.00	1.00	0.00
73.38	186.08	2.00	0.00	1.00	0.00	73.45	184.82	2.00	0.00	1.00	0.00
73.52	182.95	2.00	0.00	1.00	0.00	73.58	181.60	2.00	0.00	1.00	0.00
73.65	181.21	2.00	0.00	1.00	0.00	73.72	180.47	2.00	0.00	1.00	0.00
73.78	181.22	2.00	0.00	1.00	0.00	73.85	176.57	2.00	0.00	1.00	0.00
73.92	180.16	2.00	0.00	1.00	0.00	73.95	182.90	2.00	0.00	1.00	0.00
74.02	180.94	2.00	0.00	1.00	0.00	74.09	183.57	2.00	0.00	1.00	0.00
74.16	187.29	2.00	0.00	1.00	0.00	74.22	189.70	2.00	0.00	1.00	0.00
74.30	190.45	2.00	0.00	1.00	0.00	74.36	190.22	2.00	0.00	1.00	0.00
74.43	190.28	2.00	0.00	1.00	0.00	74.49	189.46	2.00	0.00	1.00	0.00
74.55	188.08	2.00	0.00	1.00	0.00	74.61	186.55	2.00	0.00	1.00	0.00
74.68	183.99	2.00	0.00	1.00	0.00	74.75	179.81	2.00	0.00	1.00	0.00
74.81	175.87	2.00	0.00	1.00	0.00	74.88	173.50	2.00	0.00	1.00	0.00
74.95	171.70	2.00	0.00	1.00	0.00	75.01	170.24	2.00	0.00	1.00	0.00
75.08	169.55	2.00	0.00	1.00	0.00	75.15	115.65	2.00	0.00	1.00	0.00
75.21	116.34	2.00	0.00	1.00	0.00	75.28	118.13	2.00	0.00	1.00	0.00
75.35	120.47	2.00	0.00	1.00	0.00	75.41	122.91	2.00	0.00	1.00	0.00
75.46	120.29	2.00	0.00	1.00	0.00						

Total estimated settlement: 5.60

Abbreviations

- Q_{tn,cs}: Equivalent clean sand normalized cone resistance
- FS: Factor of safety against liquefaction
- e_v (%): Post-liquefaction volumetric strain
- DF: e_v depth weighting factor
- Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
0.07	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.14	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.21	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.28	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.33	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.41	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.46	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.54	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.60	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.66	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.72	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.80	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.86	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.92	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
0.99	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.06	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.11	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.18	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.26	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.33	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.39	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.46	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.51	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.59	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.65	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.71	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.79	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.84	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.92	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
1.97	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.05	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.11	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.18	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.24	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.31	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.37	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.44	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.50	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.58	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.64	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.71	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.76	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.82	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.90	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
2.97	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.03	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.09	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.15	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ _v	S _{u(peak)} /σ _v
3.22	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.30	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.36	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.42	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.48	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.55	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.61	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.70	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.76	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.82	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.88	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
3.95	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.01	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.07	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.14	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.20	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.28	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.33	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.42	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.48	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.54	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.60	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.66	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.74	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.80	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.86	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
4.93	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
5.00	0.00	-1.00	54.25	-54.25	4.06	N/A	0.00
5.07	109.34	175.18	1.10	192.08	1.76	0.40	0.85
5.13	101.27	162.21	1.16	187.99	1.81	0.33	0.84
5.18	105.77	169.42	1.12	190.45	1.78	0.36	0.84
5.26	103.24	165.35	1.17	192.94	1.81	0.34	0.84
5.33	100.89	161.57	1.19	191.94	1.84	0.31	0.84
5.38	96.30	154.20	1.20	184.69	1.85	0.28	0.83
5.46	92.27	147.71	1.21	178.88	1.86	0.25	0.83
5.52	91.05	145.75	1.22	177.54	1.87	0.24	0.83
5.59	90.21	144.39	1.22	176.69	1.88	0.24	0.83
5.66	88.05	140.92	1.24	174.20	1.90	0.23	0.83
5.72	83.92	134.27	1.26	168.92	1.93	0.21	0.83
5.79	81.76	130.79	1.27	166.04	1.95	0.20	0.83
5.85	79.60	127.32	1.28	163.02	1.96	0.20	0.83
5.91	76.13	121.74	1.30	157.99	1.99	0.19	0.83
5.98	70.59	112.83	1.33	150.44	2.03	0.18	0.83
6.04	63.37	101.23	1.37	138.33	2.06	0.16	0.82
6.10	56.80	90.66	1.32	119.82	2.02	0.14	0.80
6.19	49.56	79.03	1.43	112.92	2.11	0.13	0.79
6.25	45.24	72.08	1.53	110.39	2.16	0.12	0.79
6.31	42.99	68.46	1.60	109.86	2.20	0.12	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
6.37	41.11	65.43	1.76	114.89	2.25	0.12	0.78
6.44	42.71	68.00	1.83	124.63	2.27	0.13	0.79
6.51	42.43	67.54	2.08	140.53	2.34	0.13	0.79
6.57	47.04	74.93	1.96	146.90	2.31	0.14	0.80
6.63	56.04	89.39	1.67	148.96	2.22	0.15	0.81
6.70	62.61	99.95	1.54	154.22	2.17	0.16	0.82
6.76	67.68	108.08	1.47	158.39	2.13	0.17	0.83
6.83	70.79	113.07	1.42	160.30	2.10	0.18	0.83
6.89	71.02	113.42	1.41	159.99	2.09	0.17	0.83
6.96	71.62	114.39	1.42	162.11	2.10	0.18	0.83
7.03	71.26	113.80	1.43	163.00	2.11	0.18	0.83
7.09	70.31	112.27	1.44	161.14	2.11	0.17	0.83
7.16	69.10	110.31	1.44	159.11	2.12	0.17	0.83
7.22	67.32	107.45	1.46	156.90	2.13	0.17	0.82
7.29	65.91	105.18	1.47	154.86	2.13	0.16	0.82
7.35	63.85	101.86	1.50	152.58	2.15	0.16	0.82
7.42	64.12	102.29	1.47	150.51	2.13	0.16	0.82
7.50	65.43	104.39	1.42	148.65	2.10	0.15	0.82
7.56	66.74	106.49	1.39	148.48	2.08	0.15	0.82
7.63	68.34	109.05	1.37	148.97	2.06	0.15	0.82
7.69	70.78	112.81	1.34	150.73	2.03	0.16	0.82
7.76	74.25	116.67	1.31	152.71	2.00	0.16	0.82
7.82	76.97	119.63	1.29	154.64	1.98	0.16	0.82
7.88	77.07	119.14	1.29	153.81	1.98	0.16	0.82
7.94	75.47	116.46	1.30	151.36	1.99	0.16	0.81
8.01	73.60	113.48	1.31	148.79	2.00	0.16	0.81
8.09	71.72	110.22	1.32	145.62	2.02	0.15	0.81
8.15	70.59	108.09	1.32	143.19	2.02	0.15	0.81
8.21	69.56	106.08	1.33	140.81	2.02	0.15	0.81
8.27	68.15	103.74	1.34	138.76	2.03	0.14	0.81
8.34	66.28	100.85	1.36	136.68	2.05	0.14	0.81
8.40	63.93	97.33	1.38	134.23	2.07	0.14	0.80
8.48	60.74	92.66	1.42	131.90	2.10	0.14	0.80
8.55	59.14	90.16	1.45	130.85	2.12	0.13	0.80
8.61	59.14	89.89	1.46	131.53	2.13	0.13	0.80
8.68	59.14	89.57	1.47	131.96	2.13	0.14	0.80
8.74	57.74	87.32	1.50	131.02	2.15	0.13	0.80
8.80	59.33	88.99	1.47	131.15	2.13	0.13	0.80
8.87	56.97	85.57	1.52	130.29	2.16	0.13	0.80
8.93	59.51	88.50	1.48	130.97	2.14	0.13	0.80
9.00	62.70	92.12	1.43	132.14	2.11	0.14	0.80
9.06	65.61	95.43	1.40	133.74	2.09	0.14	0.80
9.13	69.17	99.43	1.36	135.72	2.06	0.14	0.81
9.19	71.61	102.12	1.34	137.33	2.04	0.15	0.81
9.26	73.68	104.27	1.33	139.06	2.03	0.15	0.81
9.34	74.06	104.35	1.34	139.50	2.03	0.15	0.81
9.39	73.13	102.86	1.35	138.60	2.04	0.15	0.81
9.45	71.90	100.97	1.36	137.20	2.05	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
9.53	70.49	98.67	1.37	135.17	2.06	0.14	0.81
9.59	68.89	96.27	1.38	133.23	2.07	0.14	0.81
9.66	67.20	93.41	1.38	129.17	2.07	0.14	0.80
9.71	65.05	90.09	1.38	124.76	2.08	0.13	0.80
9.79	63.26	87.19	1.39	120.96	2.08	0.13	0.79
9.86	61.76	84.79	1.39	118.15	2.08	0.13	0.79
9.92	60.26	82.57	1.41	116.10	2.09	0.13	0.79
9.98	56.51	77.62	1.46	113.18	2.12	0.12	0.79
10.04	56.35	77.06	1.46	112.26	2.12	0.12	0.78
10.11	56.21	76.55	1.46	111.83	2.13	0.12	0.78
10.18	55.56	75.48	1.48	111.62	2.14	0.12	0.78
10.24	54.51	74.01	1.51	112.03	2.16	0.12	0.78
10.31	53.39	72.53	1.57	114.16	2.18	0.12	0.78
10.37	52.36	71.06	1.61	114.48	2.20	0.12	0.78
10.44	50.67	68.74	1.67	115.09	2.22	0.12	0.78
10.51	48.32	65.61	1.77	116.19	2.26	0.12	0.78
10.57	45.41	61.82	1.91	118.21	2.30	0.12	0.77
10.64	42.22	57.66	2.11	121.46	2.34	0.11	0.77
10.71	39.78	54.42	2.30	125.25	2.39	0.11	0.76
10.77	36.78	50.45	2.55	128.64	2.43	0.11	0.76
10.84	34.06	46.82	2.83	132.36	2.48	0.11	0.75
10.90	31.52	43.49	3.21	139.82	2.53	0.10	0.75
10.97	30.03	41.52	3.59	148.90	2.58	0.10	0.74
11.03	28.53	39.58	4.07	161.20	2.64	0.10	0.62
11.10	28.15	39.06	4.38	171.17	2.67	0.10	0.62
11.16	28.06	38.89	4.62	179.68	2.69	0.10	0.62
11.23	27.78	38.44	4.90	188.22	2.72	0.10	0.62
11.30	28.34	39.05	4.97	194.19	2.72	0.10	0.62
11.37	29.57	40.48	4.85	196.13	2.71	0.11	0.62
11.42	30.79	41.88	4.66	195.22	2.70	0.11	0.62
11.49	32.20	43.46	4.44	192.77	2.67	0.11	0.62
11.55	33.61	45.01	4.22	189.71	2.65	0.11	0.62
11.62	34.92	46.44	4.06	188.59	2.63	0.11	0.62
11.68	36.05	47.65	3.96	188.73	2.62	0.11	0.62
11.75	37.36	49.05	3.83	187.91	2.61	0.11	0.62
11.82	37.92	49.53	3.81	188.59	2.61	0.12	0.62
11.88	38.11	49.54	3.83	189.89	2.61	0.12	0.62
11.95	37.83	48.99	3.92	191.94	2.62	0.11	0.62
12.02	37.36	48.21	4.03	194.11	2.63	0.11	0.62
12.09	36.61	47.08	4.17	196.21	2.65	0.11	0.62
12.15	36.05	46.18	4.28	197.51	2.66	0.11	0.62
12.22	35.20	44.93	4.43	199.28	2.67	0.11	0.62
12.29	34.55	43.94	4.56	200.37	2.69	0.11	0.62
12.36	34.83	44.08	4.56	200.95	2.69	0.11	0.62
12.42	34.73	43.79	4.66	204.14	2.70	0.11	0.62
12.49	34.64	43.49	4.74	206.09	2.70	0.11	0.62
12.56	35.58	44.38	4.58	203.38	2.69	0.11	0.62
12.62	37.83	46.78	4.16	194.75	2.65	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
12.69	42.06	51.35	3.46	177.85	2.57	0.12	0.77
12.76	47.41	57.10	2.79	159.24	2.47	0.12	0.78
12.83	52.10	62.02	2.37	146.77	2.40	0.13	0.78
12.89	58.30	68.57	1.99	136.63	2.32	0.13	0.79
12.93	61.21	71.61	1.86	133.05	2.28	0.13	0.79
12.99	67.50	78.11	1.64	128.00	2.21	0.14	0.80
13.06	71.90	82.46	1.51	124.92	2.16	0.14	0.80
13.13	75.65	86.02	1.43	122.82	2.11	0.14	0.80
13.20	78.75	88.97	1.38	123.12	2.07	0.14	0.81
13.26	81.66	91.76	1.36	124.49	2.05	0.14	0.81
13.33	84.47	94.45	1.34	126.23	2.03	0.15	0.81
13.39	86.25	96.07	1.33	127.43	2.02	0.15	0.81
13.47	89.54	99.24	1.32	130.56	2.01	0.15	0.81
13.53	91.70	101.24	1.30	131.98	2.00	0.15	0.81
13.59	93.57	102.82	1.29	132.36	1.97	0.15	0.81
13.67	96.01	104.94	1.28	133.80	1.96	0.16	0.81
13.72	97.89	106.68	1.27	135.54	1.95	0.16	0.81
13.80	99.40	107.92	1.27	136.85	1.95	0.16	0.81
13.85	100.06	108.42	1.27	137.67	1.95	0.16	0.81
13.93	99.76	107.79	1.28	137.50	1.96	0.16	0.81
13.99	101.17	108.95	1.27	138.62	1.95	0.17	0.81
14.04	101.73	109.28	1.27	138.83	1.95	0.17	0.81
14.12	103.41	110.67	1.27	140.35	1.95	0.17	0.82
14.18	103.88	110.90	1.27	140.78	1.95	0.17	0.82
14.27	104.82	111.42	1.27	141.16	1.95	0.17	0.82
14.34	104.53	110.83	1.27	140.89	1.95	0.17	0.82
14.37	104.44	110.59	1.27	140.79	1.95	0.17	0.82
14.44	103.97	109.79	1.28	140.21	1.96	0.17	0.82
14.51	103.41	108.91	1.28	139.44	1.96	0.17	0.82
14.57	103.03	108.21	1.28	138.85	1.97	0.17	0.82
14.64	102.38	107.25	1.29	138.07	1.97	0.17	0.82
14.70	101.34	105.88	1.29	136.89	1.98	0.17	0.82
14.77	99.84	104.06	1.30	135.34	1.99	0.16	0.82
14.84	98.53	102.42	1.31	133.92	2.00	0.16	0.82
14.90	97.78	101.36	1.31	132.91	2.00	0.16	0.82
14.97	97.73	101.01	1.31	132.32	2.00	0.16	0.82
15.03	97.40	100.39	1.31	131.72	2.01	0.16	0.82
15.10	97.68	100.38	1.31	131.57	2.00	0.16	0.82
15.16	97.68	100.11	1.31	131.32	2.01	0.16	0.82
15.26	98.34	100.37	1.31	131.96	2.01	0.16	0.82
15.32	98.34	100.08	1.31	131.42	2.01	0.16	0.82
15.39	98.06	99.51	1.32	130.87	2.01	0.16	0.82
15.45	98.06	99.23	1.32	130.58	2.01	0.16	0.82
15.52	97.68	98.56	1.32	129.88	2.01	0.16	0.82
15.55	97.22	97.95	1.32	129.31	2.02	0.16	0.82
15.62	96.10	96.56	1.33	128.08	2.02	0.16	0.81
15.69	95.35	95.53	1.33	127.11	2.03	0.15	0.81
15.75	94.50	94.38	1.32	124.99	2.02	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
15.82	93.00	92.47	1.29	119.52	1.98	0.14	0.80
15.89	90.75	89.98	1.30	116.87	1.99	0.14	0.80
15.96	87.37	86.40	1.31	113.21	2.00	0.13	0.80
16.02	82.68	81.53	1.33	108.57	2.03	0.13	0.79
16.09	76.86	75.60	1.37	103.75	2.07	0.13	0.79
16.15	65.31	64.10	1.53	98.32	2.16	0.12	0.78
16.22	62.59	61.27	1.60	98.08	2.19	0.12	0.78
16.28	55.83	54.48	1.80	98.10	2.26	0.11	0.77
16.35	48.32	46.98	2.19	102.92	2.36	0.11	0.76
16.42	41.47	40.14	2.82	113.09	2.48	0.11	0.75
16.48	34.99	33.68	3.68	123.93	2.59	0.10	0.74
16.55	29.93	28.62	4.68	133.96	2.70	0.10	0.62
16.61	26.45	25.12	5.53	138.85	2.77	0.09	0.62
16.68	25.23	23.83	5.85	139.43	2.80	0.09	0.62
16.75	23.56	22.11	6.42	141.84	2.84	0.09	0.62
16.82	22.43	20.92	6.84	143.15	2.87	0.09	0.62
16.88	22.34	20.76	6.99	145.10	2.89	0.09	0.62
16.95	23.94	22.22	6.67	148.13	2.86	0.09	0.62
17.02	27.88	25.92	5.71	148.10	2.79	0.10	0.62
17.09	33.98	31.67	4.59	145.35	2.69	0.10	0.62
17.15	40.47	37.75	3.70	139.51	2.59	0.11	0.75
17.22	47.99	44.77	3.00	134.25	2.50	0.11	0.76
17.29	54.93	51.20	2.53	129.34	2.43	0.12	0.77
17.36	61.86	57.59	2.18	125.72	2.36	0.13	0.78
17.39	64.68	60.16	2.07	124.73	2.34	0.13	0.79
17.46	71.06	65.98	1.86	122.58	2.28	0.14	0.80
17.53	76.78	71.16	1.70	121.29	2.23	0.14	0.80
17.59	81.28	75.18	1.62	121.72	2.20	0.14	0.81
17.66	84.47	77.96	1.58	123.04	2.19	0.15	0.81
17.73	87.29	80.37	1.55	124.24	2.17	0.15	0.81
17.79	89.63	82.32	1.52	125.34	2.16	0.15	0.82
17.86	91.13	83.48	1.52	126.52	2.16	0.16	0.82
17.93	91.04	83.15	1.52	126.74	2.16	0.16	0.82
17.99	90.01	81.95	1.56	127.86	2.18	0.16	0.82
18.06	88.61	80.41	1.60	128.37	2.19	0.16	0.82
18.13	87.29	78.95	1.62	127.73	2.20	0.15	0.82
18.20	85.88	77.42	1.65	128.08	2.22	0.15	0.81
18.26	83.81	75.29	1.70	127.93	2.23	0.15	0.81
18.33	81.19	72.66	1.76	127.99	2.25	0.15	0.81
18.40	77.81	69.35	1.84	127.32	2.28	0.14	0.80
18.45	62.41	55.14	2.42	133.54	2.41	0.13	0.78
18.51	67.29	59.43	2.14	127.34	2.35	0.13	0.79
18.57	62.13	54.60	2.32	126.66	2.39	0.13	0.78
18.64	54.52	47.55	2.72	129.41	2.46	0.12	0.77
18.72	46.64	40.28	3.33	134.28	2.55	0.11	0.76
18.77	40.26	34.45	4.05	139.47	2.63	0.11	0.62
18.86	32.19	27.13	5.26	142.76	2.75	0.10	0.62
18.91	27.87	23.23	6.16	143.01	2.82	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
18.98	24.87	20.52	6.90	141.53	2.88	0.09	0.62
19.04	22.80	18.66	7.46	139.18	2.92	0.09	0.62
19.11	19.99	16.18	8.55	138.29	2.99	0.09	0.62
19.18	18.11	14.51	9.53	138.22	3.04	0.09	1.04
19.24	17.08	13.58	10.20	138.54	3.08	0.08	0.97
19.31	16.05	12.66	10.92	138.24	3.12	0.08	0.90
19.37	15.01	11.73	11.62	136.30	3.15	0.08	0.84
19.44	14.55	11.30	11.95	135.07	3.16	0.08	0.81
19.51	14.45	11.18	12.00	134.14	3.17	0.08	0.80
19.58	14.83	11.46	11.65	133.43	3.15	0.08	0.82
19.64	14.45	11.10	11.42	126.74	3.14	0.08	0.79
19.71	14.46	11.06	10.90	120.59	3.11	0.08	0.79
19.78	14.46	11.02	11.43	126.04	3.14	0.08	0.79
19.84	14.74	11.22	11.50	129.02	3.14	0.08	0.80
19.91	15.21	11.57	11.21	129.75	3.13	0.08	0.83
19.98	15.40	11.69	11.22	131.10	3.13	0.08	0.83
20.02	15.31	11.58	11.36	131.62	3.14	0.08	0.83
20.10	15.21	11.46	11.47	131.50	3.14	0.08	0.82
20.15	15.50	11.66	11.21	130.75	3.13	0.08	0.83
20.22	15.69	11.78	11.00	129.57	3.12	0.08	0.84
20.28	15.69	11.74	10.94	128.42	3.12	0.08	0.84
20.34	15.87	11.85	10.79	127.85	3.11	0.08	0.85
20.41	16.06	11.96	10.67	127.64	3.10	0.08	0.85
20.48	15.97	11.85	10.74	127.18	3.11	0.08	0.85
20.55	16.35	12.11	10.33	125.09	3.09	0.08	0.87
20.61	16.63	12.30	9.84	121.05	3.06	0.08	0.88
20.68	17.10	12.63	9.14	115.46	3.02	0.08	0.90
20.74	17.66	13.04	9.04	117.83	3.01	0.08	0.93
20.81	18.13	13.37	8.99	120.20	3.01	0.08	0.95
20.88	18.60	13.69	9.01	123.44	3.01	0.08	0.98
20.95	18.70	13.73	9.10	124.93	3.02	0.08	0.98
21.00	17.30	12.58	10.17	127.95	3.08	0.08	0.90
21.08	19.39	14.17	9.02	127.88	3.01	0.09	1.01
21.13	19.39	14.14	9.14	129.18	3.02	0.09	1.01
21.22	19.87	14.45	8.93	129.06	3.01	0.09	1.03
21.29	20.06	14.55	8.91	129.59	3.01	0.09	1.04
21.36	20.06	14.50	9.02	130.82	3.01	0.09	1.04
21.42	19.96	14.38	9.23	132.68	3.03	0.09	1.03
21.49	19.96	14.33	9.46	135.66	3.04	0.09	1.02
21.55	19.96	14.28	9.64	137.77	3.05	0.09	1.02
21.62	19.96	14.24	9.78	139.34	3.06	0.09	1.02
21.65	20.14	14.36	9.74	139.79	3.05	0.09	1.03
21.72	20.33	14.45	9.73	140.67	3.05	0.09	1.03
21.79	20.52	14.55	9.70	141.09	3.05	0.09	1.04
21.85	20.42	14.43	9.79	141.28	3.06	0.09	1.03
21.92	20.43	14.39	9.81	141.17	3.06	0.09	1.03
21.99	21.00	14.77	9.57	141.31	3.04	0.09	1.06
22.06	21.65	15.21	9.29	141.29	3.03	0.09	1.09

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
22.12	22.32	15.66	9.00	140.90	3.01	0.09	1.12
22.19	22.51	15.75	8.92	140.58	3.01	0.09	1.13
22.26	22.51	15.70	8.91	139.99	3.01	0.09	1.12
22.32	22.50	15.65	8.87	138.89	3.01	0.09	1.12
22.39	24.57	17.13	7.86	134.57	2.94	0.09	0.62
22.45	29.46	20.73	6.14	127.29	2.82	0.09	0.62
22.52	38.87	28.08	4.11	115.46	2.64	0.10	0.62
22.59	51.44	38.05	2.70	102.54	2.46	0.11	0.75
22.66	63.81	48.00	1.98	94.87	2.31	0.11	0.77
22.73	73.28	55.59	1.70	94.53	2.23	0.12	0.78
22.79	80.22	61.04	1.60	97.57	2.19	0.13	0.79
22.86	85.10	64.86	1.53	99.52	2.17	0.13	0.79
22.93	88.87	67.79	1.49	100.80	2.14	0.13	0.80
22.99	91.40	69.70	1.46	101.85	2.13	0.14	0.80
23.05	86.33	65.37	1.54	100.71	2.17	0.13	0.80
23.10	92.49	70.27	1.47	103.16	2.13	0.14	0.80
23.19	98.95	75.27	1.42	106.76	2.10	0.14	0.81
23.26	102.71	78.04	1.41	110.17	2.10	0.15	0.81
23.32	106.09	80.42	1.42	114.08	2.10	0.16	0.82
23.39	109.27	82.71	1.42	117.17	2.10	0.16	0.82
23.45	112.55	85.07	1.41	120.04	2.09	0.17	0.83
23.52	115.45	87.14	1.41	122.45	2.09	0.17	0.83
23.59	118.74	89.57	1.39	124.52	2.08	0.18	0.83
23.65	120.61	90.89	1.38	125.40	2.07	0.18	0.83
23.72	120.89	90.93	1.38	125.17	2.07	0.18	0.83
23.78	118.35	88.73	1.39	123.08	2.08	0.18	0.83
23.82	115.63	86.47	1.40	121.00	2.09	0.17	0.83
23.89	107.75	80.03	1.44	115.59	2.12	0.16	0.82
23.96	96.58	70.93	1.56	110.67	2.18	0.15	0.81
24.02	83.72	60.56	1.80	108.86	2.26	0.14	0.80
24.09	69.74	49.46	2.26	111.80	2.38	0.13	0.78
24.16	55.66	38.46	3.14	120.84	2.52	0.11	0.76
24.22	43.46	29.13	4.55	132.56	2.68	0.10	0.62
24.29	35.01	22.82	6.05	138.10	2.82	0.10	0.62
24.36	29.38	18.89	7.32	138.27	2.91	0.09	0.62
24.43	25.72	16.37	8.27	135.32	2.97	0.09	0.62
24.49	24.03	15.18	8.52	129.35	2.98	0.09	0.62
24.56	24.03	15.14	8.31	125.87	2.97	0.09	0.62
24.63	26.85	16.99	7.40	125.77	2.91	0.09	0.62
24.69	33.14	21.34	5.37	114.62	2.76	0.09	0.62
24.76	44.12	29.25	3.83	112.07	2.61	0.10	0.62
24.83	57.63	39.14	2.79	109.24	2.47	0.11	0.76
24.89	66.64	45.68	2.43	111.08	2.41	0.12	0.78
24.96	73.13	50.29	2.29	115.04	2.38	0.13	0.79
25.03	79.42	54.76	2.17	118.79	2.36	0.14	0.79
25.09	86.28	59.70	2.03	121.12	2.33	0.14	0.80
25.16	91.92	63.78	1.92	122.23	2.30	0.15	0.81
25.23	97.44	67.86	1.79	121.76	2.26	0.16	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
25.29	103.17	72.10	1.69	121.85	2.23	0.16	0.82
25.36	108.23	75.89	1.60	121.66	2.20	0.17	0.83
25.43	107.58	75.28	1.60	120.33	2.19	0.17	0.83
25.49	103.26	71.81	1.66	118.94	2.22	0.16	0.82
25.53	99.13	68.55	1.73	118.45	2.24	0.16	0.82
25.60	89.84	61.32	1.94	119.02	2.30	0.15	0.81
25.66	79.99	53.77	2.26	121.45	2.38	0.14	0.80
25.73	66.29	43.53	2.93	127.41	2.49	0.12	0.78
25.80	56.34	36.24	3.63	131.57	2.59	0.12	0.76
25.85	48.74	30.75	4.40	135.40	2.67	0.11	0.62
25.93	42.92	26.57	5.18	137.75	2.74	0.10	0.62
25.99	37.76	22.93	6.13	140.66	2.82	0.10	0.62
26.07	29.86	17.87	8.04	143.57	2.95	0.09	0.62
26.13	27.80	16.53	8.52	140.74	2.98	0.09	0.62
26.18	26.58	15.72	8.69	136.58	2.99	0.09	0.62
26.26	25.17	14.79	8.86	131.08	3.00	0.09	1.06
26.32	24.61	14.40	8.90	128.18	3.01	0.09	1.03
26.39	24.62	14.37	8.85	127.21	3.00	0.09	1.03
26.46	24.62	14.33	8.77	125.70	3.00	0.09	0.62
26.51	24.24	14.06	8.94	125.75	3.01	0.09	1.00
26.58	24.24	14.02	8.92	125.13	3.01	0.09	1.00
26.66	26.40	15.31	8.15	124.79	2.96	0.09	0.62
26.72	29.98	17.49	7.13	124.64	2.89	0.09	0.62
26.80	39.27	23.46	5.06	118.75	2.73	0.10	0.62
26.85	45.08	27.42	4.16	114.09	2.65	0.10	0.62
26.91	49.67	30.54	3.66	111.85	2.59	0.11	0.75
26.98	52.12	32.05	3.58	114.75	2.58	0.11	0.75
27.04	52.04	31.86	3.70	117.85	2.59	0.11	0.75
27.11	49.03	29.61	4.18	123.86	2.65	0.11	0.62
27.19	43.76	25.87	5.05	130.54	2.73	0.10	0.62
27.24	40.67	23.75	5.56	132.03	2.78	0.10	0.62
27.30	38.60	22.31	5.94	132.59	2.81	0.10	0.62
27.37	35.33	20.27	6.67	135.26	2.86	0.10	0.62
27.43	35.03	20.04	6.74	135.06	2.87	0.10	0.62
27.52	37.86	21.66	6.07	131.53	2.82	0.10	0.62
27.58	41.06	23.73	5.38	127.60	2.76	0.10	0.62
27.63	44.72	26.16	4.71	123.26	2.70	0.10	0.62
27.72	54.95	33.07	3.43	113.29	2.56	0.11	0.75
27.79	63.01	38.64	2.74	105.98	2.46	0.12	0.77
27.85	69.77	43.37	2.33	100.85	2.39	0.12	0.77
27.89	72.21	45.17	2.15	97.15	2.35	0.12	0.78
27.95	78.13	49.68	1.79	88.93	2.26	0.12	0.78
28.02	83.38	53.47	1.64	87.86	2.21	0.12	0.78
28.09	88.16	56.89	1.55	88.17	2.17	0.12	0.79
28.16	92.29	59.81	1.49	89.10	2.14	0.13	0.79
28.23	95.76	62.26	1.45	90.14	2.12	0.13	0.79
28.28	96.78	62.90	1.44	90.44	2.11	0.13	0.79
28.36	97.81	63.46	1.44	91.17	2.11	0.13	0.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
28.42	101.84	66.19	1.41	93.52	2.10	0.13	0.80
28.48	104.37	67.80	1.41	95.52	2.09	0.14	0.80
28.57	107.93	69.88	1.42	99.16	2.10	0.14	0.81
28.63	110.37	71.37	1.42	101.24	2.10	0.15	0.81
28.69	112.34	72.51	1.42	102.99	2.10	0.15	0.81
28.76	113.94	73.39	1.42	104.50	2.10	0.15	0.82
28.82	114.41	73.47	1.43	105.29	2.11	0.16	0.82
28.89	114.22	73.09	1.45	105.72	2.12	0.16	0.82
28.96	113.28	72.15	1.47	106.01	2.13	0.16	0.82
29.02	111.41	70.60	1.50	105.65	2.15	0.16	0.82
29.09	109.06	68.73	1.53	105.16	2.16	0.15	0.82
29.16	105.87	66.32	1.57	104.15	2.18	0.15	0.81
29.23	101.74	63.23	1.64	103.39	2.21	0.15	0.81
29.29	96.30	59.26	1.73	102.58	2.24	0.14	0.80
29.36	89.44	54.20	1.93	104.84	2.30	0.14	0.80
29.43	81.27	48.45	2.20	106.36	2.36	0.13	0.79
29.49	71.14	41.38	2.71	112.32	2.46	0.12	0.78
29.56	59.12	33.26	3.66	121.62	2.59	0.11	0.76
29.59	52.94	29.19	4.33	126.44	2.66	0.11	0.62
29.66	41.57	22.06	5.91	130.41	2.80	0.10	0.62
29.73	32.66	17.08	7.29	124.42	2.91	0.09	0.62
29.79	30.12	15.63	7.99	124.92	2.95	0.09	0.62
29.88	25.06	12.80	9.77	124.97	3.06	0.09	0.91
29.94	22.34	11.27	10.90	122.90	3.11	0.08	0.81
30.01	21.21	10.63	11.21	119.20	3.13	0.08	0.76
30.06	21.31	10.66	10.80	115.17	3.11	0.08	0.76
30.12	19.62	9.72	11.52	111.98	3.14	0.08	0.69
30.19	18.40	9.03	12.30	111.10	3.18	0.08	0.64
30.26	18.03	8.81	12.51	110.21	3.19	0.08	0.63
30.32	17.84	8.68	12.27	106.55	3.18	0.08	0.62
30.39	17.47	8.46	12.23	103.45	3.18	0.08	0.60
30.45	17.18	8.29	12.39	102.68	3.18	0.08	0.59
30.52	17.18	8.27	12.36	102.21	3.18	0.08	0.59
30.59	17.18	8.25	11.99	98.92	3.17	0.08	0.59
30.66	17.18	8.23	11.89	97.88	3.16	0.08	0.59
30.72	17.37	8.31	12.47	103.64	3.19	0.08	0.59
30.79	17.56	8.39	12.35	103.64	3.18	0.08	0.60
30.85	17.84	8.52	12.13	103.39	3.17	0.08	0.61
30.92	19.25	9.26	11.06	102.39	3.12	0.08	0.66
30.97	19.72	9.49	10.75	102.00	3.11	0.08	0.68
31.07	20.47	9.86	10.25	101.05	3.08	0.08	0.70
31.10	20.19	9.70	10.38	100.68	3.09	0.08	0.69
31.19	18.78	8.92	11.63	103.73	3.15	0.08	0.64
31.24	18.22	8.61	12.22	105.24	3.18	0.08	0.62
31.30	17.28	8.10	12.94	104.84	3.21	0.08	0.58
31.38	17.84	8.37	12.25	102.59	3.18	0.08	0.60
31.43	17.37	8.11	12.53	101.67	3.19	0.08	0.58
31.50	17.79	8.31	12.08	100.46	3.17	0.08	0.59

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
31.57	17.65	8.22	12.11	99.60	3.17	0.08	0.59
31.63	17.75	8.26	11.94	98.58	3.16	0.08	0.59
31.70	17.47	8.09	12.06	97.58	3.17	0.08	0.58
31.77	17.09	7.88	12.71	100.10	3.20	0.08	0.56
31.84	16.53	7.57	13.50	102.21	3.23	0.08	0.54
31.90	16.90	7.74	13.48	104.40	3.23	0.08	0.55
31.97	18.23	8.41	12.36	103.94	3.18	0.08	0.60
32.03	20.57	9.60	10.96	105.23	3.12	0.08	0.69
32.10	23.31	10.98	9.73	106.91	3.05	0.08	0.78
32.17	23.88	11.25	9.71	109.24	3.05	0.08	0.80
32.23	22.28	10.41	10.75	111.94	3.11	0.08	0.74
32.29	20.12	9.29	12.25	113.73	3.18	0.08	0.66
32.35	18.81	8.60	13.26	114.04	3.22	0.08	0.61
32.42	17.87	8.10	13.95	112.97	3.25	0.08	0.58
32.49	17.87	8.08	13.67	110.50	3.24	0.08	0.58
32.56	18.43	8.35	13.03	108.75	3.21	0.08	0.60
32.62	19.94	9.10	11.86	107.87	3.16	0.08	0.65
32.68	21.45	9.84	10.94	107.60	3.12	0.08	0.70
32.75	22.39	10.29	10.51	108.19	3.09	0.08	0.74
32.82	22.57	10.36	10.65	110.34	3.10	0.08	0.74
32.88	22.95	10.53	10.90	114.83	3.11	0.08	0.75
32.95	24.93	11.50	10.38	119.31	3.09	0.09	0.82
33.01	28.31	13.17	9.22	121.39	3.03	0.09	0.94
33.08	34.03	15.99	7.46	119.32	2.92	0.09	0.62
33.15	41.73	19.80	5.87	116.18	2.80	0.10	0.62
33.21	48.68	23.43	5.04	117.97	2.73	0.10	0.62
33.28	50.65	24.37	5.01	122.08	2.73	0.11	0.62
33.35	49.24	23.45	5.32	124.86	2.76	0.10	0.62
33.41	44.74	21.11	6.11	129.04	2.82	0.10	0.62
33.48	39.75	18.61	7.09	132.02	2.89	0.10	0.62
33.55	33.67	15.57	8.62	134.32	2.99	0.09	0.62
33.62	30.19	13.83	9.69	134.07	3.05	0.09	0.99
33.68	28.90	13.17	10.06	132.43	3.07	0.09	0.94
33.75	26.26	11.85	10.93	129.50	3.12	0.09	0.85
33.82	22.98	10.22	12.10	123.74	3.17	0.08	0.73
33.88	20.06	8.78	12.06	105.88	3.17	0.08	0.63
33.95	17.91	7.71	12.69	97.87	3.20	0.08	0.55
34.02	16.32	6.92	13.86	95.99	3.25	0.08	0.49
34.09	15.19	6.36	15.11	96.11	3.30	0.08	0.45
34.15	14.72	6.12	15.76	96.48	3.32	0.08	0.44
34.19	15.19	6.34	15.17	96.26	3.30	0.08	0.45
34.25	13.98	5.75	16.81	96.63	3.36	0.08	0.41
34.33	15.21	6.32	15.22	96.20	3.30	0.08	0.45
34.40	15.30	6.36	15.14	96.21	3.30	0.08	0.45
34.46	15.30	6.34	15.11	95.82	3.30	0.08	0.45
34.52	15.30	6.33	15.00	94.89	3.29	0.08	0.45
34.59	15.30	6.31	14.85	93.76	3.29	0.08	0.45
34.66	15.51	6.40	14.52	92.92	3.27	0.08	0.46

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
34.73	15.87	6.56	14.13	92.73	3.26	0.08	0.47
34.79	16.44	6.81	13.78	93.92	3.24	0.08	0.49
34.86	16.91	7.02	13.53	95.06	3.23	0.08	0.50
34.93	17.66	7.37	13.05	96.13	3.21	0.08	0.53
34.99	18.13	7.57	12.79	96.90	3.20	0.08	0.54
35.06	17.75	7.38	13.14	96.98	3.22	0.08	0.53
35.13	17.10	7.06	13.97	98.58	3.25	0.08	0.50
35.20	16.82	6.91	14.39	99.41	3.27	0.08	0.49
35.26	17.01	6.99	14.31	99.95	3.27	0.08	0.50
35.33	17.59	7.24	14.07	101.84	3.26	0.08	0.52
35.40	18.71	7.75	13.15	101.94	3.22	0.08	0.55
35.47	20.03	8.35	12.31	102.82	3.18	0.08	0.60
35.53	20.78	8.68	11.97	103.97	3.17	0.08	0.62
35.60	21.25	8.89	11.79	104.78	3.16	0.08	0.63
35.66	22.29	9.35	11.49	107.39	3.14	0.08	0.67
35.70	23.51	9.91	10.92	108.20	3.12	0.08	0.71
35.77	24.54	10.36	10.63	110.11	3.10	0.08	0.74
35.83	24.45	10.30	10.97	112.97	3.12	0.08	0.74
35.90	26.72	11.33	10.17	115.19	3.08	0.09	0.81
35.97	30.94	13.25	8.67	114.85	2.99	0.09	0.62
36.03	32.71	14.03	8.06	113.05	2.96	0.09	0.62
36.10	30.36	12.93	8.67	112.03	2.99	0.09	0.62
36.17	25.85	10.84	10.50	113.77	3.09	0.09	0.77
36.23	22.29	9.19	12.55	115.28	3.19	0.08	0.66
36.30	26.18	10.94	10.24	112.05	3.08	0.09	0.78
36.37	20.05	8.13	14.02	113.98	3.25	0.08	0.58
36.43	26.53	11.06	9.93	109.79	3.06	0.09	0.79
36.50	39.96	17.13	5.99	102.64	2.81	0.09	0.62
36.57	51.14	22.60	4.44	100.30	2.67	0.10	0.62
36.64	60.22	27.32	3.72	101.64	2.60	0.11	0.75
36.70	64.80	29.54	3.61	106.50	2.58	0.11	0.76
36.77	66.76	30.41	3.60	109.40	2.58	0.12	0.76
36.84	61.02	27.13	4.20	114.01	2.65	0.11	0.62
36.91	49.84	21.36	5.69	121.58	2.79	0.10	0.62
36.97	39.33	16.61	7.64	126.89	2.93	0.10	0.62
37.04	32.09	13.35	9.47	126.33	3.04	0.09	0.95
37.11	27.86	11.43	10.67	122.04	3.10	0.09	0.82
37.14	26.74	10.92	10.91	119.15	3.11	0.09	0.78
37.21	24.57	9.93	11.34	112.66	3.14	0.08	0.71
37.27	23.09	9.26	11.44	105.90	3.14	0.08	0.66
37.34	23.47	9.41	10.93	102.83	3.12	0.08	0.67
37.41	25.16	10.14	10.27	104.18	3.08	0.08	0.72
37.48	27.50	11.15	8.95	99.79	3.01	0.09	0.80
37.54	29.57	12.04	8.74	105.24	3.00	0.09	0.62
37.61	31.43	12.84	8.63	110.82	2.99	0.09	0.62
37.68	32.84	13.44	8.57	115.18	2.99	0.09	0.62
37.74	34.63	14.20	8.21	116.63	2.97	0.09	0.62
37.81	37.16	15.28	7.66	117.01	2.93	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
37.88	36.89	15.13	7.90	119.48	2.95	0.09	0.62
37.94	36.99	15.15	8.10	122.72	2.96	0.09	0.62
38.01	36.99	15.12	8.40	126.98	2.98	0.09	0.62
38.08	37.10	15.14	8.63	130.65	2.99	0.09	0.62
38.15	39.45	16.12	8.11	130.74	2.96	0.10	0.62
38.21	43.67	17.93	7.12	127.56	2.89	0.10	0.62
38.28	49.78	20.53	5.99	122.96	2.81	0.10	0.62
38.34	57.86	24.05	4.93	118.68	2.72	0.11	0.62
38.41	68.93	29.79	3.81	113.43	2.61	0.12	0.62
38.48	81.59	36.64	2.90	106.29	2.49	0.13	0.78
38.55	92.09	42.53	2.38	101.35	2.40	0.13	0.79
38.61	96.76	45.10	2.22	100.16	2.37	0.14	0.80
38.68	95.26	44.08	2.31	101.69	2.39	0.14	0.79
38.75	87.75	39.74	2.61	103.80	2.44	0.13	0.79
38.78	82.67	36.88	2.87	105.87	2.48	0.13	0.78
38.85	71.23	30.55	3.69	112.78	2.59	0.12	0.77
38.92	60.14	24.57	5.00	122.91	2.73	0.11	0.62
38.98	49.92	20.19	6.64	133.93	2.86	0.10	0.62
39.05	42.97	17.20	8.00	137.57	2.95	0.10	0.62
39.11	37.15	14.72	9.14	134.49	3.02	0.09	1.05
39.19	37.54	14.85	8.00	118.75	2.95	0.09	0.62
39.24	35.19	13.84	8.26	114.30	2.97	0.09	0.62
39.32	29.57	11.44	10.29	117.70	3.08	0.09	0.82
39.38	29.57	11.42	10.41	118.88	3.09	0.09	0.82
39.45	29.59	11.41	10.61	121.08	3.10	0.09	0.81
39.51	29.60	11.40	10.76	122.69	3.11	0.09	0.81
39.58	36.37	14.20	8.41	119.36	2.98	0.09	0.62
39.64	41.07	16.14	7.17	115.76	2.90	0.10	0.62
39.72	47.16	18.64	6.04	112.65	2.82	0.10	0.62
39.77	49.69	19.67	5.73	112.76	2.79	0.10	0.62
39.84	52.51	20.80	5.46	113.49	2.77	0.10	0.62
39.90	53.15	21.03	5.53	116.20	2.77	0.10	0.62
39.96	49.30	19.41	6.30	122.32	2.84	0.10	0.62
40.03	55.94	22.11	5.29	116.93	2.75	0.11	0.62
40.09	57.15	22.57	5.07	114.45	2.73	0.11	0.62
40.17	51.14	20.05	5.92	118.74	2.81	0.10	0.62
40.25	44.85	17.43	7.18	125.10	2.90	0.10	0.62
40.31	40.26	15.52	8.39	130.20	2.98	0.10	0.62
40.37	38.77	14.88	8.91	132.63	3.01	0.09	1.06
40.42	42.07	16.21	8.04	130.27	2.95	0.10	0.62
40.51	47.31	18.31	6.90	126.42	2.88	0.10	0.62
40.56	47.23	18.25	6.90	125.89	2.88	0.10	0.62
40.62	46.19	17.80	7.20	128.09	2.90	0.10	0.62
40.71	44.31	16.99	7.75	131.73	2.94	0.10	0.62
40.78	44.70	17.12	7.75	132.70	2.94	0.10	0.62
40.85	48.36	18.57	7.09	131.68	2.89	0.10	0.62
40.91	53.05	20.43	6.31	129.02	2.84	0.11	0.62
40.95	55.58	21.44	5.94	127.42	2.81	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
41.02	60.18	23.25	5.32	123.59	2.76	0.11	0.62
41.08	65.72	25.58	4.61	118.04	2.69	0.11	0.62
41.15	77.55	31.50	3.52	110.97	2.57	0.12	0.77
41.22	98.20	42.31	2.42	102.51	2.41	0.14	0.80
41.28	119.12	53.69	1.85	99.48	2.28	0.16	0.82
41.34	128.87	59.01	1.70	100.43	2.23	0.17	0.83
41.44	139.46	64.84	1.58	102.15	2.18	0.18	0.84
41.50	140.40	65.27	1.57	102.23	2.18	0.18	0.84
41.57	139.26	64.49	1.58	101.97	2.19	0.18	0.84
41.60	138.33	63.92	1.59	101.69	2.19	0.18	0.83
41.67	137.29	63.28	1.60	101.03	2.19	0.18	0.83
41.74	137.01	62.98	1.60	101.03	2.20	0.18	0.83
41.81	136.81	62.52	1.64	102.28	2.21	0.18	0.83
41.87	136.63	62.17	1.66	103.05	2.22	0.18	0.83
41.94	135.31	61.17	1.70	103.78	2.23	0.18	0.83
42.00	121.89	53.43	1.97	105.44	2.31	0.17	0.82
42.07	129.50	57.15	1.89	108.00	2.29	0.18	0.83
42.14	127.06	55.42	2.00	111.04	2.32	0.18	0.83
42.20	127.16	55.10	2.07	113.85	2.34	0.18	0.83
42.28	123.59	52.88	2.20	116.23	2.36	0.18	0.83
42.35	120.68	51.19	2.29	117.17	2.38	0.17	0.82
42.42	118.24	49.89	2.34	116.63	2.39	0.17	0.82
42.48	117.21	49.35	2.34	115.53	2.39	0.17	0.82
42.55	117.30	49.45	2.30	113.63	2.39	0.17	0.82
42.62	116.54	49.15	2.26	111.30	2.38	0.16	0.82
42.68	114.01	47.91	2.28	109.45	2.38	0.16	0.81
42.72	111.85	46.83	2.32	108.65	2.39	0.16	0.81
42.78	106.97	44.38	2.42	107.33	2.41	0.15	0.81
42.85	101.34	41.48	2.57	106.80	2.44	0.14	0.80
42.92	93.18	37.32	2.90	108.14	2.49	0.14	0.79
42.99	84.06	32.66	3.45	112.68	2.56	0.13	0.78
43.05	76.94	29.05	4.05	117.64	2.63	0.12	0.62
43.12	73.56	27.41	4.32	118.52	2.66	0.12	0.62
43.18	72.06	26.81	4.29	115.05	2.66	0.12	0.62
43.25	70.37	26.20	4.19	109.90	2.65	0.12	0.62
43.32	66.34	24.30	4.53	110.14	2.68	0.11	0.62
43.38	58.45	21.20	5.40	114.38	2.76	0.11	0.62
43.45	51.23	18.42	6.30	116.12	2.84	0.10	0.62
43.52	46.25	16.51	6.90	113.86	2.88	0.10	0.62
43.59	43.54	15.46	7.01	108.39	2.89	0.10	0.62
43.65	41.65	14.72	7.27	107.04	2.90	0.09	0.62
43.72	40.26	14.17	7.92	112.25	2.95	0.09	0.62
43.79	39.21	13.75	8.60	118.32	2.99	0.09	0.62
43.86	37.91	13.24	9.24	122.31	3.03	0.09	0.95
43.92	36.21	12.58	9.91	124.76	3.06	0.09	0.90
43.98	42.81	15.04	8.19	123.16	2.96	0.10	0.62
44.04	52.96	18.81	6.25	117.58	2.83	0.10	0.62
44.12	68.25	24.60	4.40	108.33	2.67	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
44.19	80.25	30.16	3.46	104.49	2.57	0.12	0.77
44.25	89.71	34.60	2.96	102.43	2.50	0.13	0.78
44.31	96.93	38.10	2.62	99.98	2.44	0.14	0.79
44.38	101.90	40.62	2.41	98.03	2.41	0.14	0.80
44.45	105.36	42.25	2.31	97.77	2.39	0.14	0.80
44.52	107.80	43.34	2.26	98.12	2.38	0.15	0.80
44.58	109.21	43.86	2.26	99.11	2.38	0.15	0.80
44.65	110.52	44.29	2.28	100.77	2.38	0.15	0.81
44.72	112.31	44.98	2.27	101.91	2.38	0.15	0.81
44.78	113.91	45.64	2.24	102.31	2.37	0.15	0.81
44.85	115.41	46.27	2.22	102.50	2.37	0.16	0.81
44.88	116.35	46.70	2.19	102.41	2.36	0.16	0.81
44.95	117.57	47.25	2.16	101.98	2.36	0.16	0.81
45.02	118.32	47.57	2.14	101.60	2.35	0.16	0.82
45.09	118.79	47.74	2.12	101.21	2.35	0.16	0.82
45.16	119.35	47.95	2.11	100.99	2.34	0.16	0.82
45.22	119.35	47.88	2.11	100.79	2.34	0.16	0.82
45.29	119.35	47.82	2.10	100.51	2.34	0.16	0.82
45.35	119.35	47.74	2.10	100.32	2.34	0.16	0.82
45.42	119.82	47.90	2.09	100.18	2.34	0.16	0.82
45.49	120.76	48.32	2.07	99.77	2.34	0.16	0.82
45.56	121.13	48.45	2.05	99.40	2.33	0.16	0.82
45.62	121.23	48.42	2.05	99.25	2.33	0.16	0.82
45.69	120.84	48.15	2.06	99.07	2.33	0.16	0.82
45.76	120.01	47.67	2.07	98.82	2.34	0.16	0.82
45.82	118.59	46.92	2.10	98.53	2.34	0.16	0.81
45.89	116.99	46.06	2.14	98.35	2.35	0.15	0.81
45.96	114.93	44.98	2.19	98.28	2.36	0.15	0.81
46.02	112.02	43.47	2.26	98.41	2.38	0.15	0.81
46.09	109.77	42.31	2.33	98.46	2.39	0.15	0.80
46.16	106.95	40.88	2.41	98.68	2.41	0.14	0.80
46.22	104.22	39.74	2.42	95.99	2.41	0.14	0.80
46.29	101.40	38.40	2.48	95.35	2.42	0.14	0.79
46.36	99.06	37.04	2.63	97.29	2.45	0.14	0.79
46.42	97.09	35.93	2.76	99.22	2.47	0.13	0.79
46.46	96.34	35.52	2.81	99.75	2.47	0.13	0.79
46.52	94.37	34.52	2.91	100.43	2.49	0.13	0.79
46.61	92.68	33.68	2.98	100.40	2.50	0.13	0.78
46.66	90.89	32.85	3.05	100.17	2.51	0.13	0.78
46.74	84.51	29.95	3.35	100.41	2.55	0.12	0.77
46.79	81.51	28.64	3.48	99.69	2.57	0.12	0.77
46.86	76.16	26.24	3.82	100.35	2.61	0.12	0.62
46.94	69.87	23.45	4.41	103.37	2.67	0.11	0.62
46.99	64.71	21.62	4.91	106.23	2.72	0.11	0.62
47.06	56.45	18.70	5.84	109.25	2.80	0.10	0.62
47.14	47.25	15.46	7.30	112.84	2.91	0.10	0.62
47.19	41.81	13.55	8.54	115.78	2.99	0.09	0.62
47.25	37.22	11.94	9.88	117.93	3.06	0.09	0.85

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
47.34	37.04	11.85	9.80	116.11	3.06	0.09	0.85
47.39	37.05	11.84	9.68	114.57	3.05	0.09	0.85
47.45	36.87	11.76	9.54	112.19	3.04	0.09	0.84
47.51	48.63	15.81	6.41	101.36	2.84	0.10	0.62
47.58	65.24	21.66	4.11	89.06	2.64	0.11	0.62
47.65	75.17	26.04	3.28	85.36	2.54	0.11	0.76
47.72	77.32	26.77	3.28	87.80	2.54	0.11	0.76
47.78	73.83	24.84	3.82	94.92	2.61	0.11	0.62
47.85	66.51	21.83	4.84	105.56	2.71	0.11	0.62
47.91	59.10	19.26	5.92	114.00	2.81	0.11	0.62
47.98	51.22	16.53	7.09	117.27	2.89	0.10	0.62
48.05	45.78	14.64	7.84	114.88	2.94	0.10	0.62
48.11	41.18	13.05	8.67	113.12	2.99	0.09	0.62
48.18	37.24	11.69	9.58	112.02	3.05	0.09	0.84
48.24	34.91	10.88	10.39	113.09	3.09	0.09	0.78
48.31	33.88	10.52	10.86	114.18	3.11	0.09	0.75
48.38	33.60	10.40	10.89	113.28	3.11	0.09	0.74
48.45	35.30	10.96	10.61	116.32	3.10	0.09	0.78
48.52	42.16	13.27	8.87	117.63	3.00	0.09	0.95
48.58	62.16	20.01	5.44	108.93	2.77	0.11	0.62
48.65	89.57	30.49	3.28	99.98	2.54	0.13	0.78
48.72	110.85	39.82	2.47	98.48	2.42	0.15	0.80
48.78	125.30	46.27	2.14	98.99	2.35	0.16	0.82
48.85	138.80	52.57	1.89	99.18	2.29	0.18	0.83
48.92	150.71	58.36	1.71	99.53	2.23	0.20	0.84
48.95	155.41	60.72	1.64	99.69	2.21	0.20	0.85
49.02	160.66	64.19	1.51	96.82	2.15	0.20	0.85
49.09	164.70	67.03	1.42	95.41	2.10	0.20	0.84
49.16	169.48	67.94	1.48	100.75	2.14	0.22	0.85
49.23	175.76	71.29	1.43	101.94	2.11	0.23	0.86
49.29	182.14	73.98	1.42	105.18	2.10	0.25	0.86
49.35	179.04	71.83	1.47	105.30	2.13	0.25	0.86
49.42	188.79	76.24	1.44	109.50	2.11	0.28	0.87
49.49	197.70	80.52	1.40	112.92	2.09	0.31	0.88
49.56	202.50	82.68	1.39	114.92	2.08	0.33	0.88
49.62	206.91	85.25	1.36	115.92	2.05	0.34	0.88
49.69	211.60	88.17	1.33	117.09	2.02	0.34	0.88
49.76	216.95	90.94	1.31	119.35	2.01	0.36	0.88
49.82	221.45	93.23	1.30	121.31	1.99	0.38	0.88
49.89	224.35	94.60	1.30	122.61	1.99	0.39	0.88
49.95	229.23	97.10	1.29	124.86	1.97	0.42	0.89
50.00	220.32	92.11	1.31	120.48	2.00	0.38	0.88
50.07	227.81	96.08	1.29	123.86	1.98	0.41	0.88
50.14	231.84	98.30	1.28	125.59	1.96	0.42	0.88
50.20	232.78	98.79	1.27	125.88	1.96	0.42	0.88
50.28	232.40	98.50	1.27	125.46	1.96	0.41	0.88
50.35	228.74	96.53	1.28	123.42	1.96	0.39	0.88
50.41	224.14	93.92	1.29	121.01	1.98	0.37	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
50.48	218.33	90.55	1.30	118.16	2.00	0.35	0.88
50.55	213.81	88.01	1.32	115.94	2.01	0.34	0.88
50.61	211.75	86.69	1.33	114.96	2.02	0.33	0.88
50.68	212.78	87.23	1.32	115.17	2.02	0.33	0.88
50.74	213.06	87.72	1.31	114.78	2.00	0.32	0.87
50.81	209.58	86.19	1.31	112.71	2.00	0.30	0.87
50.88	202.35	82.46	1.32	109.11	2.02	0.28	0.87
50.94	191.65	76.85	1.36	104.32	2.05	0.25	0.86
51.01	178.98	70.38	1.41	99.22	2.09	0.23	0.86
51.08	167.43	64.60	1.47	95.18	2.13	0.21	0.85
51.15	158.33	60.09	1.54	92.55	2.17	0.19	0.84
51.21	151.76	56.88	1.60	90.81	2.19	0.18	0.84
51.28	145.47	53.62	1.69	90.49	2.23	0.18	0.83
51.34	140.03	50.94	1.77	89.93	2.25	0.17	0.83
51.38	137.31	49.59	1.81	89.91	2.27	0.17	0.82
51.45	132.61	47.21	1.92	90.48	2.30	0.16	0.82
51.51	129.61	45.73	1.98	90.61	2.31	0.16	0.82
51.58	127.27	44.89	1.97	88.24	2.31	0.16	0.81
51.65	125.48	45.10	1.79	80.67	2.26	0.15	0.81
51.71	123.70	43.84	1.89	82.85	2.29	0.15	0.81
51.78	123.61	43.49	1.94	84.45	2.30	0.15	0.81
51.85	122.85	42.82	2.02	86.31	2.32	0.15	0.81
51.92	123.51	42.92	2.03	87.26	2.33	0.15	0.81
51.99	124.07	43.11	2.02	87.09	2.32	0.15	0.81
52.05	124.64	43.38	1.99	86.42	2.32	0.15	0.81
52.11	125.11	43.59	1.97	85.92	2.31	0.15	0.81
52.18	122.95	42.57	2.01	85.69	2.32	0.15	0.81
52.24	120.70	41.51	2.06	85.56	2.33	0.15	0.81
52.31	118.35	40.39	2.12	85.60	2.35	0.15	0.80
52.38	115.53	39.06	2.20	85.88	2.36	0.14	0.80
52.44	110.65	36.75	2.38	87.41	2.40	0.14	0.80
52.51	105.12	34.07	2.65	90.27	2.45	0.14	0.79
52.58	104.93	33.84	2.70	91.33	2.46	0.14	0.79
52.64	104.93	33.73	2.72	91.85	2.46	0.14	0.79
52.71	104.74	33.59	2.73	91.87	2.46	0.14	0.79
52.78	107.75	34.84	2.61	90.90	2.44	0.14	0.79
52.84	108.78	35.25	2.56	90.29	2.43	0.14	0.80
52.91	107.75	34.83	2.57	89.57	2.44	0.14	0.79
52.98	106.62	34.40	2.58	88.90	2.44	0.14	0.79
53.04	107.75	34.91	2.52	87.95	2.43	0.14	0.79
53.11	110.65	36.25	2.39	86.78	2.40	0.14	0.80
53.17	115.44	38.38	2.22	85.39	2.37	0.14	0.80
53.24	123.79	42.16	1.99	83.89	2.32	0.15	0.81
53.31	134.30	47.08	1.76	82.85	2.25	0.16	0.82
53.38	145.20	52.34	1.59	83.14	2.19	0.17	0.82
53.42	151.86	55.48	1.52	84.44	2.16	0.17	0.83
53.49	161.25	59.77	1.46	87.33	2.13	0.18	0.84
53.56	171.38	64.46	1.41	90.87	2.09	0.20	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
53.63	183.30	70.29	1.35	95.21	2.05	0.21	0.85
53.68	191.75	74.47	1.33	98.70	2.02	0.23	0.85
53.75	201.70	79.20	1.30	103.24	2.00	0.25	0.86
53.82	207.23	81.47	1.30	105.97	1.99	0.26	0.86
53.89	211.46	82.90	1.31	108.21	2.00	0.29	0.87
53.94	214.55	85.28	1.28	109.19	1.96	0.28	0.86
54.00	201.60	80.57	1.27	102.24	1.95	0.22	0.84
54.07	215.87	87.97	1.24	109.05	1.90	0.23	0.84
54.15	224.31	91.42	1.24	113.29	1.90	0.27	0.85
54.21	230.41	93.98	1.24	116.33	1.90	0.29	0.85
54.27	234.73	95.52	1.24	118.53	1.91	0.32	0.86
54.34	232.34	93.50	1.26	117.50	1.93	0.33	0.87
54.40	229.94	91.75	1.27	116.41	1.95	0.34	0.87
54.47	240.08	96.66	1.25	121.29	1.93	0.39	0.87
54.53	244.86	98.76	1.25	123.61	1.92	0.42	0.88
54.60	249.46	100.49	1.25	125.91	1.92	0.47	0.88
54.67	253.50	102.05	1.25	127.89	1.92	0.52	0.89
54.73	257.63	103.80	1.25	129.89	1.92	0.56	0.89
54.80	261.66	105.56	1.25	131.81	1.92	0.61	0.89
54.87	265.14	107.12	1.25	133.44	1.91	0.66	0.89
54.93	268.04	108.34	1.24	134.80	1.91	0.72	0.90
54.99	270.67	109.40	1.24	136.06	1.91	0.77	0.90
55.05	273.58	110.54	1.24	137.45	1.91	0.84	0.90
55.12	276.58	111.88	1.24	138.83	1.91	0.84	0.90
55.19	279.11	112.97	1.24	139.99	1.90	0.84	0.90
55.26	281.36	113.94	1.24	141.00	1.90	0.85	0.91
55.33	282.86	114.51	1.24	141.64	1.90	0.85	0.91
55.39	283.14	114.49	1.24	141.72	1.90	0.85	0.91
55.45	282.58	114.04	1.24	141.40	1.90	0.85	0.91
55.52	282.59	113.87	1.24	141.33	1.91	0.85	0.91
55.59	282.59	114.21	1.24	141.11	1.90	0.85	0.90
55.64	280.62	113.97	1.23	139.83	1.89	0.85	0.90
55.72	277.90	112.37	1.23	138.50	1.89	0.84	0.90
55.79	274.33	110.38	1.24	136.73	1.90	0.81	0.90
55.86	269.83	107.96	1.25	134.51	1.91	0.75	0.90
55.92	263.91	104.90	1.25	131.59	1.93	0.68	0.90
55.98	219.34	82.10	1.36	111.86	2.06	0.38	0.89
56.05	247.87	96.79	1.28	123.76	1.96	0.52	0.89
56.11	246.27	96.10	1.28	122.87	1.96	0.50	0.89
56.18	244.40	95.26	1.28	121.85	1.96	0.48	0.89
56.24	243.18	94.62	1.28	121.20	1.97	0.47	0.89
56.31	244.49	95.45	1.27	121.65	1.96	0.47	0.89
56.37	244.86	95.71	1.27	121.71	1.95	0.46	0.89
56.45	244.58	95.64	1.27	121.44	1.95	0.45	0.89
56.51	246.65	96.78	1.26	122.31	1.94	0.45	0.88
56.58	246.84	96.95	1.26	122.29	1.94	0.45	0.88
56.64	247.21	97.13	1.26	122.37	1.93	0.45	0.88
56.71	247.96	97.36	1.26	122.67	1.93	0.45	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
56.78	249.56	97.99	1.26	123.38	1.93	0.47	0.88
56.84	251.15	98.67	1.26	124.07	1.93	0.48	0.89
56.91	251.43	98.69	1.26	124.13	1.93	0.48	0.89
56.98	251.15	98.33	1.26	123.96	1.94	0.49	0.89
57.05	251.15	98.11	1.26	123.91	1.94	0.50	0.89
57.11	252.46	98.63	1.26	124.48	1.94	0.51	0.89
57.18	252.74	102.59	1.20	123.17	1.85	0.34	0.85
57.24	253.02	105.35	1.14	120.33	1.79	0.29	0.83
57.31	251.61	103.60	1.17	121.05	1.81	0.30	0.83
57.38	250.30	101.98	1.19	121.31	1.84	0.31	0.84
57.45	249.83	101.00	1.20	121.51	1.85	0.33	0.85
57.48	249.27	100.40	1.21	121.39	1.86	0.33	0.85
57.56	248.66	99.62	1.22	121.22	1.87	0.34	0.85
57.62	248.66	99.36	1.22	121.24	1.88	0.35	0.86
57.71	248.06	98.51	1.23	121.03	1.89	0.36	0.86
57.77	247.76	97.72	1.24	120.99	1.90	0.38	0.87
57.84	245.79	96.45	1.24	120.05	1.91	0.38	0.87
57.91	243.07	94.97	1.25	118.70	1.92	0.37	0.87
57.97	238.57	92.50	1.26	116.54	1.93	0.36	0.87
58.01	235.66	90.93	1.27	115.15	1.94	0.36	0.87
58.08	229.37	87.61	1.28	112.17	1.96	0.34	0.87
58.14	225.80	85.73	1.29	110.48	1.98	0.33	0.87
58.21	223.36	84.50	1.29	109.29	1.98	0.32	0.87
58.28	221.49	83.61	1.30	108.34	1.99	0.31	0.87
58.34	221.86	83.92	1.29	108.36	1.98	0.31	0.87
58.41	227.21	86.81	1.27	110.65	1.96	0.31	0.87
58.48	236.13	91.64	1.25	114.65	1.92	0.33	0.86
58.54	242.13	94.94	1.24	117.31	1.90	0.33	0.86
58.61	247.01	97.43	1.23	119.45	1.88	0.34	0.86
58.67	250.58	100.91	1.19	120.02	1.84	0.30	0.84
58.74	252.36	105.61	1.08	114.40	1.75	0.27	0.82
58.80	255.46	106.72	1.09	116.15	1.75	0.28	0.83
58.87	256.96	106.03	1.13	119.52	1.78	0.30	0.83
58.94	259.13	105.99	1.15	121.91	1.80	0.32	0.83
59.01	262.98	106.74	1.17	124.66	1.81	0.35	0.84
59.07	262.69	105.54	1.19	125.42	1.84	0.38	0.85
59.13	262.41	104.58	1.20	125.75	1.85	0.40	0.86
59.22	273.96	109.95	1.19	130.74	1.84	0.48	0.86
59.28	279.12	111.67	1.19	133.38	1.84	0.57	0.87
59.32	281.37	112.37	1.20	134.55	1.85	0.61	0.87
59.38	285.13	113.59	1.20	136.44	1.85	0.71	0.88
59.45	288.41	114.75	1.20	137.99	1.85	0.79	0.89
59.52	292.91	116.71	1.20	139.96	1.85	0.85	0.89
59.59	297.99	119.10	1.19	142.05	1.84	0.85	0.89
59.65	302.12	122.59	1.16	142.13	1.81	0.86	0.88
59.72	303.90	126.61	1.08	136.48	1.75	0.86	0.88
59.79	302.12	125.79	1.08	135.56	1.75	0.81	0.88
59.85	302.11	125.31	1.09	136.52	1.75	0.81	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
59.92	301.08	124.15	1.11	137.49	1.76	0.80	0.87
59.98	299.58	122.91	1.12	137.82	1.77	0.75	0.87
60.04	251.34	96.97	1.24	120.20	1.90	0.40	0.87
60.11	288.76	117.09	1.15	134.57	1.80	0.58	0.86
60.19	286.90	115.96	1.16	133.99	1.80	0.56	0.86
60.25	283.33	113.93	1.17	132.83	1.81	0.53	0.86
60.32	277.14	110.41	1.18	130.72	1.83	0.49	0.86
60.38	269.91	106.37	1.20	127.92	1.85	0.46	0.86
60.46	264.19	103.35	1.21	125.41	1.87	0.44	0.87
60.51	262.22	102.51	1.21	124.40	1.87	0.42	0.86
60.57	259.78	101.50	1.21	123.15	1.87	0.40	0.86
60.65	255.18	99.30	1.22	120.98	1.87	0.37	0.86
60.70	251.61	97.47	1.22	119.33	1.88	0.36	0.86
60.77	247.67	95.57	1.23	117.44	1.89	0.34	0.86
60.83	245.79	94.80	1.23	116.47	1.89	0.33	0.86
60.92	243.73	93.97	1.23	115.36	1.89	0.31	0.85
60.99	245.56	94.90	1.22	116.09	1.88	0.32	0.85
61.05	243.54	93.78	1.23	115.13	1.89	0.31	0.85
61.12	245.32	94.64	1.22	115.85	1.88	0.32	0.85
61.19	247.20	95.55	1.22	116.60	1.88	0.32	0.85
61.22	248.14	96.00	1.22	116.98	1.87	0.32	0.85
61.29	248.05	95.89	1.22	116.87	1.87	0.32	0.85
61.35	247.76	95.67	1.22	116.68	1.87	0.32	0.85
61.42	247.86	95.64	1.22	116.66	1.88	0.32	0.85
61.50	247.86	95.56	1.22	116.58	1.88	0.32	0.85
61.55	247.86	95.39	1.22	116.57	1.88	0.32	0.85
61.62	250.39	96.24	1.22	117.73	1.88	0.34	0.86
61.69	251.89	96.48	1.23	118.46	1.89	0.36	0.86
61.75	251.33	95.76	1.23	118.25	1.90	0.37	0.87
61.81	247.76	93.44	1.25	116.65	1.92	0.38	0.87
61.89	250.77	94.45	1.25	118.02	1.92	0.41	0.88
61.94	253.97	95.54	1.25	119.50	1.92	0.44	0.88
62.03	258.85	97.13	1.25	121.77	1.93	0.51	0.89
62.09	262.88	98.59	1.25	123.63	1.93	0.57	0.89
62.15	266.82	99.89	1.26	125.47	1.93	0.65	0.90
62.21	269.92	100.72	1.26	126.92	1.94	0.74	0.90
62.27	273.77	102.28	1.26	128.65	1.93	0.81	0.90
62.34	270.95	100.56	1.27	127.33	1.94	0.80	0.91
62.42	278.46	104.21	1.25	130.66	1.93	0.83	0.91
62.49	284.94	106.71	1.25	133.64	1.92	0.84	0.91
62.54	281.65	105.00	1.26	132.07	1.93	0.83	0.91
62.60	282.31	106.06	1.25	132.15	1.91	0.84	0.91
62.67	282.12	106.42	1.24	131.89	1.90	0.84	0.90
62.74	279.40	105.97	1.23	130.36	1.89	0.72	0.89
62.80	265.32	99.75	1.24	123.79	1.91	0.54	0.88
62.87	239.70	87.34	1.28	112.09	1.97	0.39	0.88
62.95	210.70	74.97	1.32	98.88	2.01	0.27	0.86
63.01	189.20	66.41	1.34	89.08	2.04	0.21	0.84

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
63.08	167.99	55.39	1.53	85.02	2.17	0.19	0.84
63.14	150.26	46.76	1.86	87.07	2.28	0.18	0.83
63.21	137.68	40.69	2.29	93.29	2.38	0.17	0.82
63.28	129.53	36.75	2.77	101.66	2.47	0.17	0.82
63.33	130.39	36.51	2.95	107.74	2.50	0.17	0.82
63.39	131.24	36.25	3.15	114.36	2.52	0.17	0.82
63.46	136.78	37.95	3.09	117.25	2.52	0.18	0.83
63.53	131.99	35.87	3.38	121.38	2.56	0.18	0.82
63.59	126.83	34.16	3.73	127.53	2.60	0.17	0.82
63.66	124.39	33.46	3.97	132.92	2.62	0.17	0.68
63.72	128.99	34.72	3.82	132.79	2.61	0.18	0.69
63.79	139.60	37.94	3.35	127.24	2.55	0.19	0.83
63.85	152.92	43.25	2.78	120.44	2.47	0.21	0.85
63.92	172.43	51.56	2.16	111.61	2.36	0.26	0.86
63.99	188.39	59.10	1.78	104.99	2.26	0.29	0.88
64.05	204.06	66.91	1.53	102.59	2.16	0.33	0.88
64.11	218.22	74.20	1.40	104.03	2.09	0.36	0.89
64.19	241.31	86.82	1.28	111.42	1.97	0.40	0.88
64.26	253.98	94.52	1.23	116.73	1.90	0.38	0.87
64.33	265.05	104.32	1.12	117.34	1.78	0.31	0.83
64.39	276.60	114.13	1.00	114.13	1.68	0.37	0.84
64.46	287.86	119.92	1.00	119.92	1.66	0.47	0.86
64.53	298.09	125.01	1.00	125.01	1.64	0.60	0.87
64.60	303.90	127.52	1.00	127.52	1.64	0.73	0.87
64.66	298.46	123.70	1.00	123.70	1.66	0.61	0.87
64.70	299.67	123.90	1.00	123.90	1.67	0.64	0.87
64.78	296.10	120.69	1.00	120.69	1.70	0.57	0.86
64.85	300.89	121.80	1.01	123.28	1.71	0.66	0.87
64.91	309.53	130.11	1.00	130.11	1.63	0.86	0.88
64.97	326.79	143.73	1.00	143.73	1.54	0.88	0.89
65.04	349.04	154.90	1.00	154.90	1.52	0.89	0.92
65.11	371.29	166.73	1.00	166.73	1.50	0.90	0.94
65.16	381.70	172.66	1.00	172.66	1.48	0.91	0.94
65.22	392.12	178.89	1.00	178.89	1.46	0.91	0.95
65.29	390.97	178.85	1.00	178.85	1.45	0.91	0.95
65.36	398.67	183.55	1.00	183.55	1.44	0.92	0.95
65.42	396.79	184.68	1.00	184.68	1.42	0.92	0.95
65.49	392.38	190.95	1.00	190.95	1.32	0.92	0.95
65.57	388.35	186.92	1.00	186.92	1.34	0.92	0.95
65.63	383.00	182.36	1.00	182.36	1.36	0.92	0.95
65.71	375.67	176.03	1.00	176.03	1.40	0.91	0.94
65.76	366.66	169.13	1.00	169.13	1.43	0.90	0.93
65.82	285.86	118.48	1.00	118.48	1.64	0.44	0.85
65.89	332.97	145.23	1.00	145.23	1.54	0.88	0.90
65.95	322.55	139.03	1.00	139.03	1.56	0.87	0.89
66.02	314.76	133.23	1.00	133.23	1.60	0.87	0.88
66.09	311.19	130.62	1.00	130.62	1.61	0.87	0.88
66.14	307.25	128.55	1.00	128.55	1.62	0.77	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
66.21	298.54	123.78	1.00	123.78	1.64	0.59	0.86
66.28	298.54	123.03	1.00	123.03	1.65	0.59	0.86
66.35	300.88	122.75	1.00	122.75	1.67	0.64	0.87
66.41	302.85	123.61	1.00	123.61	1.67	0.67	0.87
66.48	305.67	127.66	1.00	127.66	1.62	0.73	0.87
66.55	306.61	132.53	1.00	132.53	1.55	0.75	0.87
66.61	307.17	138.23	1.00	138.23	1.46	0.76	0.87
66.68	304.73	136.23	1.00	136.23	1.48	0.70	0.87
66.75	300.70	133.56	1.00	133.56	1.49	0.63	0.87
66.81	297.61	130.68	1.00	130.68	1.51	0.56	0.86
66.87	282.31	120.67	1.00	120.67	1.56	0.39	0.85
66.93	268.61	112.19	1.00	112.19	1.61	0.30	0.83
67.00	268.98	112.26	1.00	112.26	1.61	0.31	0.83
67.06	263.92	109.03	1.00	109.03	1.63	0.28	0.83
67.14	256.41	104.91	1.00	104.91	1.65	0.25	0.82
67.21	246.92	100.07	1.00	100.07	1.66	0.22	0.81
67.27	234.25	93.20	1.00	93.20	1.70	0.19	0.79
67.34	218.48	83.97	1.00	83.97	1.77	0.16	0.77
67.41	202.06	74.96	1.00	74.96	1.84	0.15	0.77
67.47	186.29	66.51	1.25	82.84	1.91	0.15	0.79
67.54	172.97	58.89	1.31	77.37	2.01	0.16	0.81
67.61	163.68	53.57	1.40	74.98	2.09	0.16	0.82
67.67	163.77	52.71	1.45	76.45	2.12	0.17	0.83
67.74	163.78	53.46	1.40	75.05	2.09	0.16	0.82
67.81	163.88	55.98	1.30	72.86	1.99	0.14	0.80
67.87	160.50	54.81	1.30	71.26	1.99	0.13	0.79
67.94	150.91	50.07	1.35	67.67	2.05	0.13	0.80
68.01	138.80	43.66	1.51	65.80	2.15	0.14	0.80
68.07	121.06	35.11	1.96	68.99	2.31	0.13	0.79
68.12	109.24	29.68	2.57	76.21	2.44	0.13	0.79
68.20	95.82	24.46	3.60	88.08	2.58	0.13	0.78
68.25	84.25	21.36	4.58	97.84	2.69	0.12	0.62
68.31	70.55	17.70	6.19	109.55	2.83	0.11	0.62
68.38	59.86	14.83	7.82	116.00	2.94	0.10	0.62
68.44	69.34	17.35	6.33	109.86	2.84	0.11	0.62
68.51	59.40	14.69	7.61	111.78	2.93	0.10	0.62
68.58	68.13	17.01	6.27	106.62	2.83	0.11	0.62
68.64	83.63	21.12	4.81	101.65	2.71	0.12	0.62
68.71	103.43	26.37	3.51	92.66	2.57	0.13	0.78
68.78	125.86	34.17	2.56	87.43	2.43	0.15	0.81
68.83	138.70	39.21	2.16	84.86	2.36	0.16	0.82
68.91	153.72	45.65	1.78	81.44	2.26	0.18	0.83
68.99	163.39	50.03	1.61	80.54	2.20	0.19	0.84
69.05	164.89	52.34	1.45	76.14	2.12	0.17	0.83
69.11	165.64	55.44	1.32	73.03	2.01	0.15	0.81
69.17	165.73	54.71	1.34	73.50	2.04	0.15	0.81
69.24	164.51	53.95	1.36	73.18	2.05	0.15	0.81
69.31	161.70	52.65	1.37	72.18	2.06	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
69.37	158.51	50.43	1.43	72.29	2.11	0.16	0.82
69.44	155.87	48.33	1.53	73.74	2.16	0.16	0.82
69.51	153.05	46.24	1.64	76.04	2.21	0.17	0.83
69.56	153.24	45.76	1.71	78.20	2.24	0.17	0.83
69.64	160.37	47.65	1.74	83.03	2.25	0.19	0.84
69.69	167.69	51.09	1.60	81.97	2.20	0.19	0.84
69.78	187.40	60.15	1.41	84.70	2.09	0.21	0.85
69.82	206.36	68.49	1.33	91.19	2.03	0.24	0.86
69.89	242.68	85.89	1.24	106.23	1.90	0.29	0.85
69.95	272.80	101.14	1.16	117.41	1.81	0.34	0.84
70.02	279.93	102.89	1.18	121.26	1.82	0.42	0.85
70.08	285.04	102.92	1.21	124.46	1.86	0.58	0.88
70.15	282.86	101.71	1.21	123.54	1.87	0.57	0.88
70.21	289.05	107.40	1.15	123.82	1.80	0.47	0.85
70.30	298.53	113.56	1.09	123.33	1.75	0.54	0.86
70.37	288.11	108.15	1.12	121.48	1.78	0.43	0.85
70.41	300.12	113.80	1.09	124.49	1.76	0.58	0.86
70.49	286.70	106.19	1.15	122.60	1.80	0.44	0.85
70.55	301.73	113.55	1.11	126.49	1.77	0.61	0.86
70.61	312.90	118.39	1.10	129.96	1.76	0.83	0.88
70.67	318.43	122.66	1.03	126.47	1.72	0.86	0.88
70.74	321.71	126.63	1.00	126.63	1.68	0.86	0.88
70.81	312.79	123.84	1.00	123.84	1.66	0.80	0.88
70.88	307.71	128.87	1.00	128.87	1.55	0.69	0.87
70.95	296.55	121.38	1.00	121.38	1.59	0.50	0.86
71.01	291.66	118.66	1.00	118.66	1.60	0.44	0.85
71.08	292.24	118.88	1.00	118.88	1.60	0.45	0.85
71.15	291.77	118.01	1.00	118.01	1.61	0.44	0.85
71.20	289.19	115.15	1.00	115.15	1.64	0.42	0.85
71.27	292.24	115.05	1.00	115.05	1.66	0.45	0.85
71.33	286.61	111.21	1.00	111.21	1.69	0.40	0.85
71.41	292.71	113.06	1.00	113.06	1.70	0.45	0.85
71.47	294.21	113.10	1.01	113.88	1.71	0.47	0.85
71.55	293.65	111.71	1.05	117.12	1.73	0.46	0.85
71.60	289.24	108.50	1.10	118.87	1.76	0.42	0.85
71.66	290.93	108.29	1.12	121.04	1.77	0.45	0.85
71.72	290.46	107.05	1.14	122.32	1.79	0.46	0.85
71.81	292.45	105.59	1.19	125.13	1.83	0.57	0.87
71.87	291.04	103.48	1.21	125.20	1.86	0.66	0.88
71.94	288.50	101.50	1.22	124.29	1.88	0.71	0.89
72.00	284.84	99.23	1.24	122.76	1.90	0.73	0.89
72.07	273.02	92.81	1.27	117.71	1.95	0.70	0.90
72.14	256.03	84.22	1.32	110.86	2.01	0.60	0.91
72.20	239.05	74.60	1.44	107.42	2.11	0.57	0.91
72.27	226.56	70.27	1.45	102.21	2.12	0.43	0.90
72.34	223.94	69.82	1.43	100.15	2.11	0.39	0.89
72.41	217.85	66.93	1.48	99.08	2.14	0.37	0.89
72.47	217.52	66.33	1.51	99.92	2.15	0.38	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
72.51	217.52	66.08	1.52	100.47	2.16	0.38	0.89
72.58	217.21	65.88	1.52	100.40	2.16	0.38	0.89
72.64	109.11	26.89	4.11	110.48	2.64	0.14	0.65
72.72	242.00	78.50	1.33	104.41	2.03	0.45	0.89
72.80	252.67	86.41	1.25	107.95	1.92	0.35	0.87
72.86	251.82	87.85	1.22	107.28	1.88	0.29	0.85
72.92	248.90	86.62	1.22	105.99	1.88	0.28	0.84
72.97	245.62	85.48	1.22	104.51	1.88	0.27	0.84
73.06	238.30	81.15	1.25	101.46	1.92	0.28	0.85
73.12	233.69	78.42	1.27	99.49	1.95	0.28	0.86
73.19	230.69	76.37	1.29	98.27	1.97	0.29	0.87
73.25	227.13	74.19	1.31	96.92	2.00	0.30	0.87
73.32	226.00	73.39	1.32	96.53	2.01	0.30	0.87
73.38	222.72	71.76	1.33	95.29	2.02	0.30	0.87
73.45	218.95	70.10	1.34	93.82	2.03	0.29	0.87
73.52	215.95	68.90	1.34	92.57	2.04	0.28	0.87
73.58	213.98	68.12	1.35	91.72	2.04	0.27	0.87
73.65	216.04	69.13	1.34	92.30	2.03	0.27	0.87
73.72	214.64	68.52	1.34	91.70	2.03	0.27	0.87
73.78	216.14	69.07	1.34	92.23	2.03	0.27	0.87
73.85	219.51	71.30	1.31	93.08	2.00	0.26	0.86
73.92	225.61	73.57	1.30	95.57	1.99	0.28	0.86
73.95	229.36	74.91	1.30	97.14	1.99	0.29	0.87
74.02	235.55	77.93	1.28	99.55	1.96	0.30	0.87
74.09	240.06	79.59	1.27	101.41	1.96	0.32	0.87
74.16	242.50	80.20	1.28	102.43	1.96	0.34	0.87
74.22	242.12	79.67	1.28	102.26	1.97	0.35	0.88
74.30	241.75	79.34	1.29	102.05	1.97	0.35	0.88
74.36	241.75	79.32	1.29	101.98	1.97	0.35	0.88
74.43	240.72	78.79	1.29	101.50	1.98	0.35	0.88
74.49	235.84	76.60	1.30	99.47	1.99	0.33	0.88
74.55	230.96	74.47	1.31	97.47	2.00	0.32	0.87
74.61	223.92	71.33	1.33	94.74	2.02	0.30	0.87
74.68	215.75	67.77	1.35	91.75	2.05	0.28	0.87
74.75	206.74	64.04	1.38	88.56	2.07	0.26	0.86
74.81	198.77	60.76	1.41	85.94	2.10	0.24	0.86
74.88	193.42	58.48	1.44	84.45	2.12	0.23	0.86
74.95	189.57	56.84	1.47	83.46	2.13	0.22	0.85
75.01	187.69	56.14	1.47	82.73	2.13	0.22	0.85
75.08	187.69	56.26	1.46	82.38	2.13	0.22	0.85
75.15	187.97	46.15	54.25	2503.60	4.06	0.45	3.30
75.21	188.82	46.35	54.25	2514.65	4.06	0.46	3.31
75.28	190.97	46.89	54.25	2543.54	4.06	0.48	3.35
75.35	193.78	47.58	54.25	2581.25	4.06	0.51	3.40
75.41	196.69	48.30	54.25	2620.39	4.06	0.55	3.45
75.46	193.59	47.52	54.25	2577.66	4.06	0.51	3.39

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
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Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

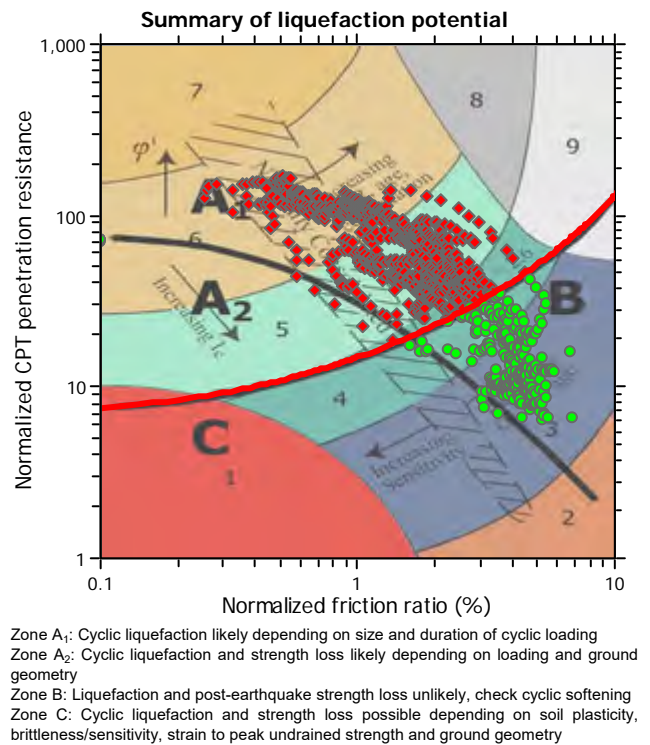
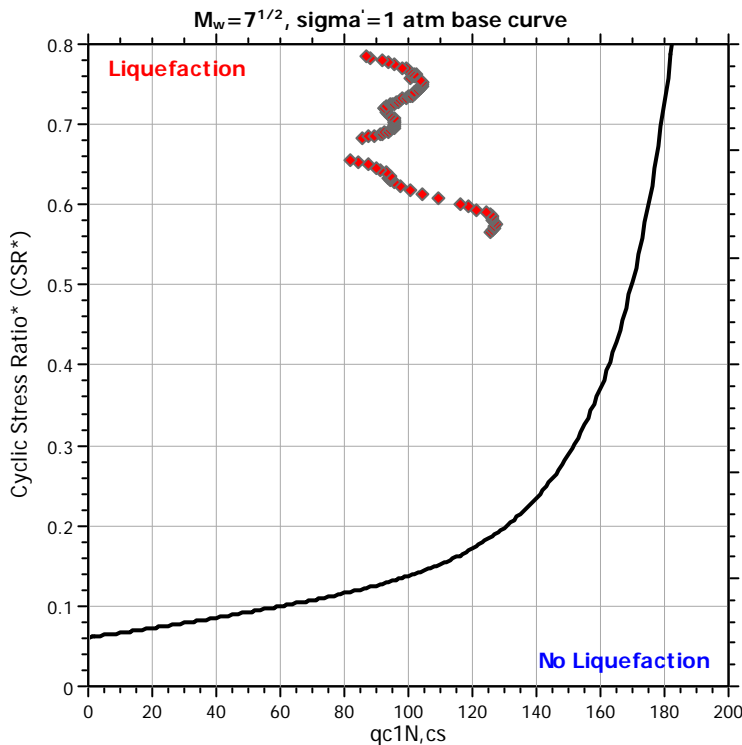
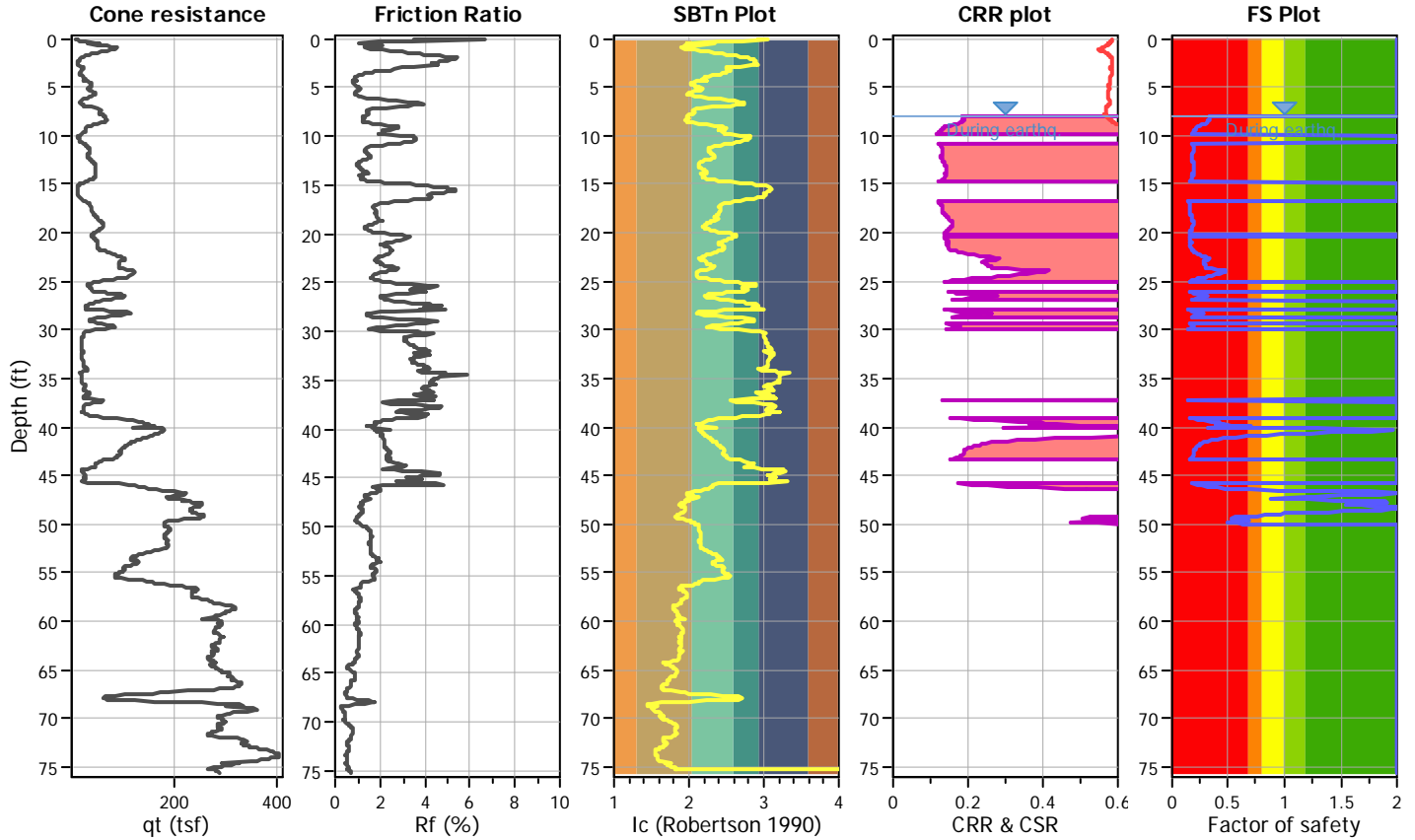
LIQUEFACTION ANALYSIS REPORT

Project title : Universal Engineering Services / Compton
CPT file : CPT-5

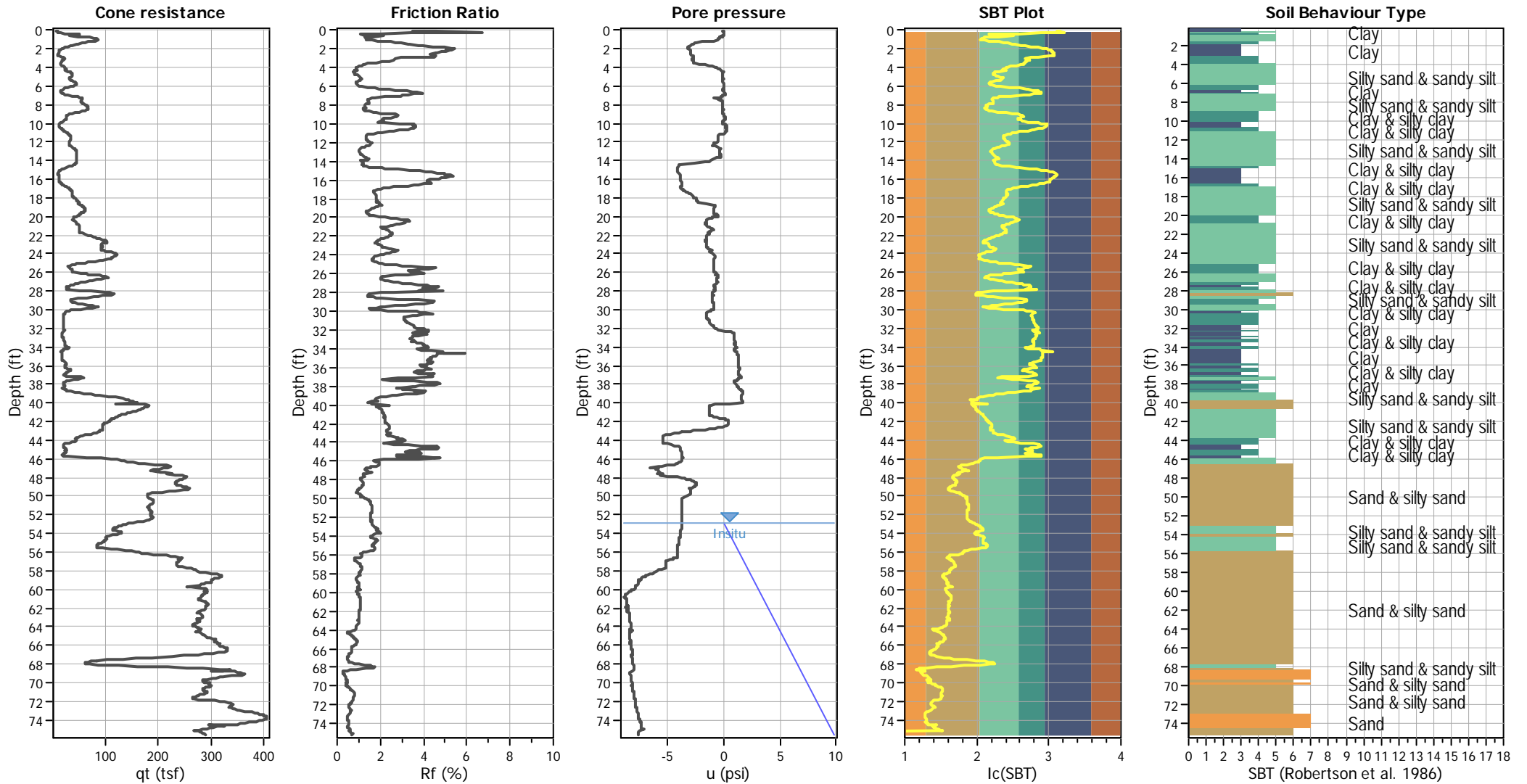
Location : 1111 E. Artesia Blvd, Compton, CA

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	52.90 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	1	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w :	7.30	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method
Peak ground acceleration:	0.77	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



CPT basic interpretation plots



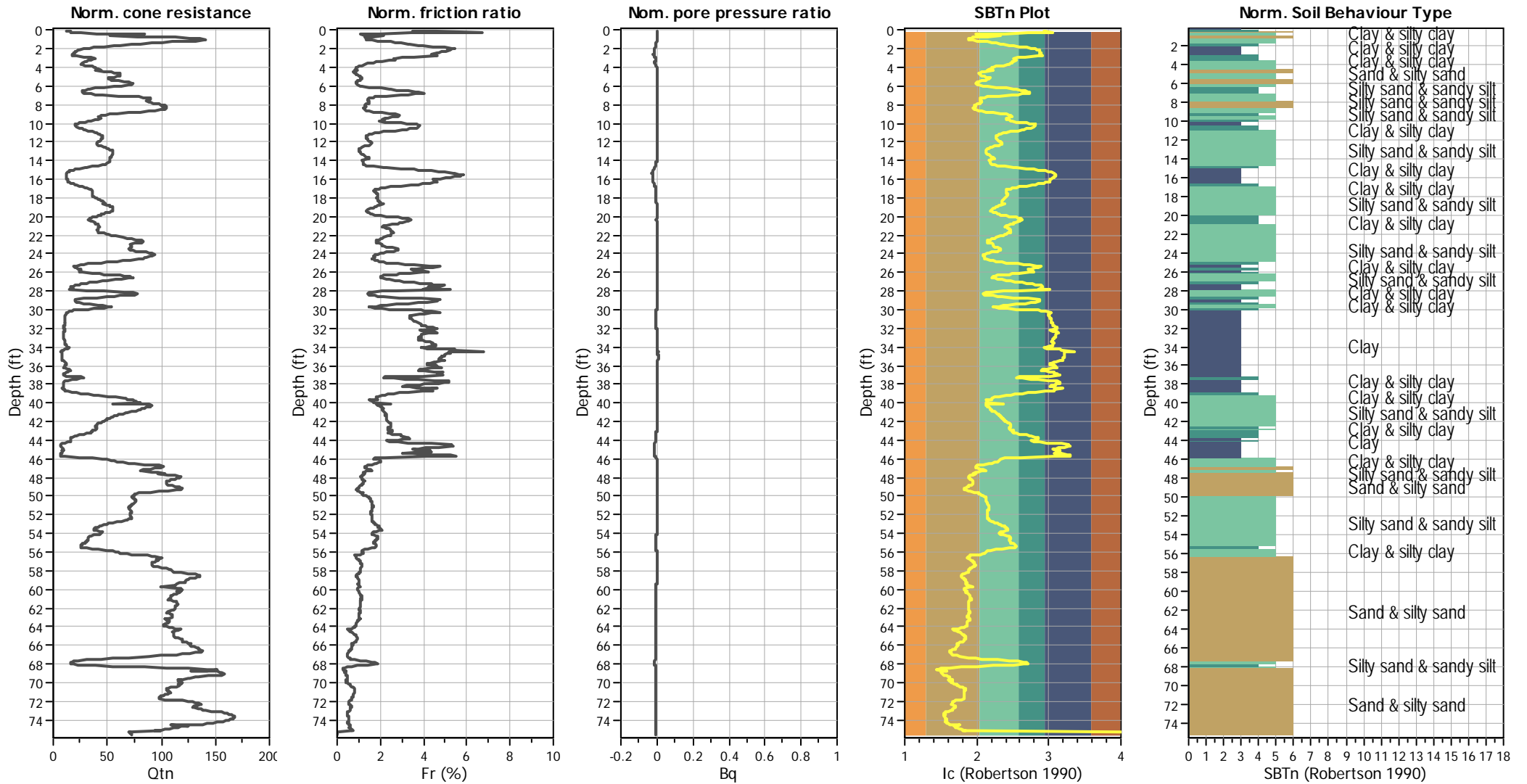
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



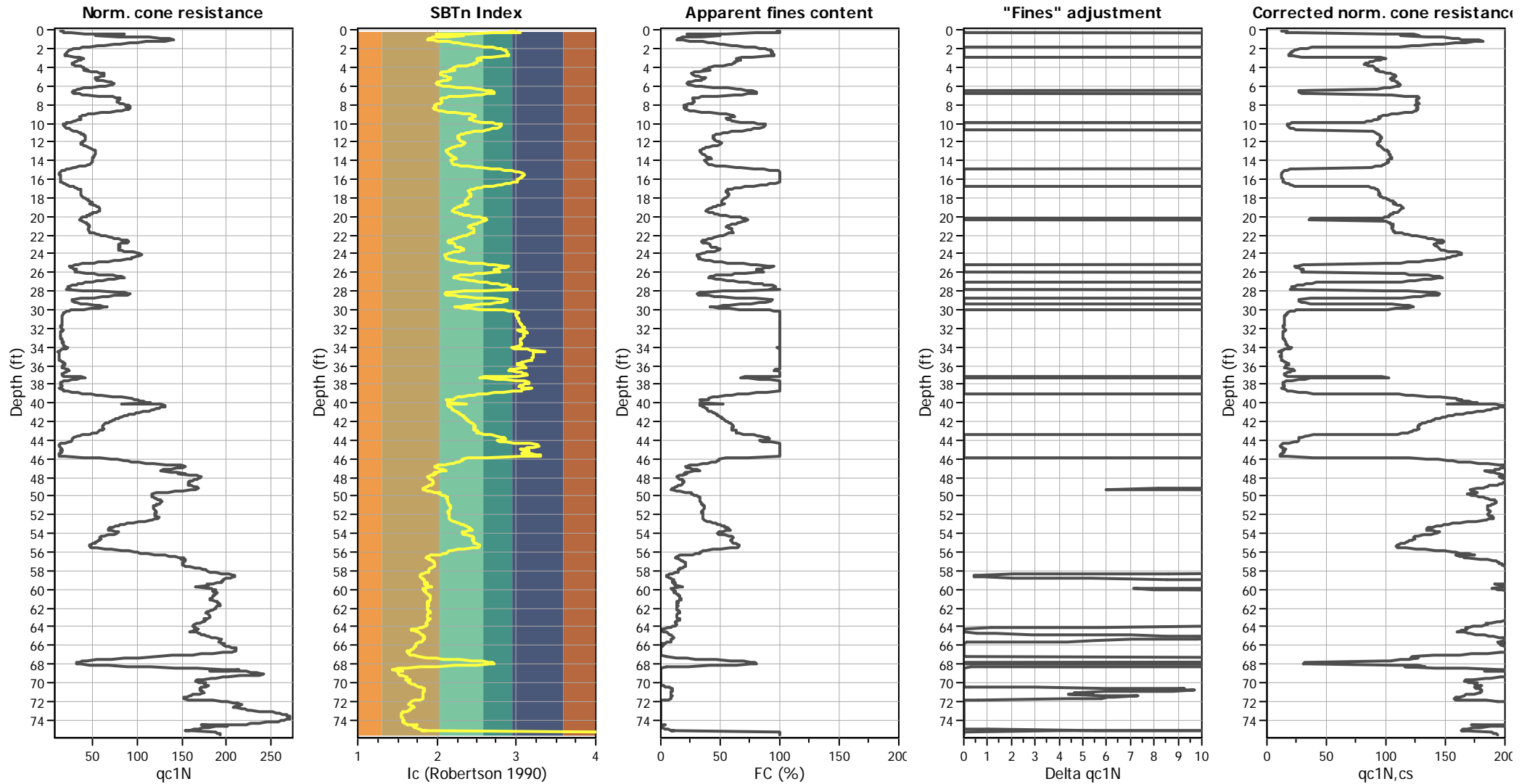
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

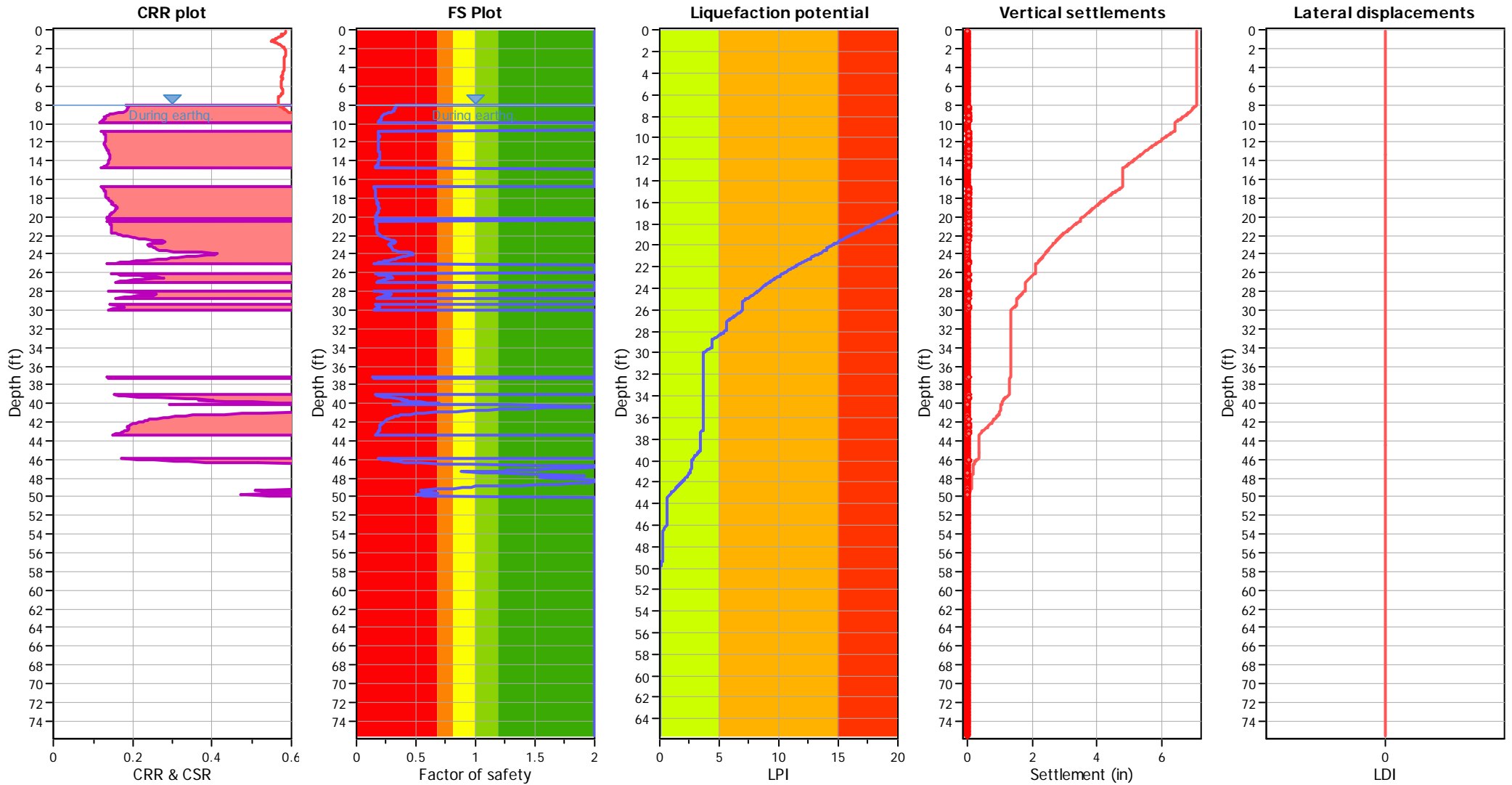
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

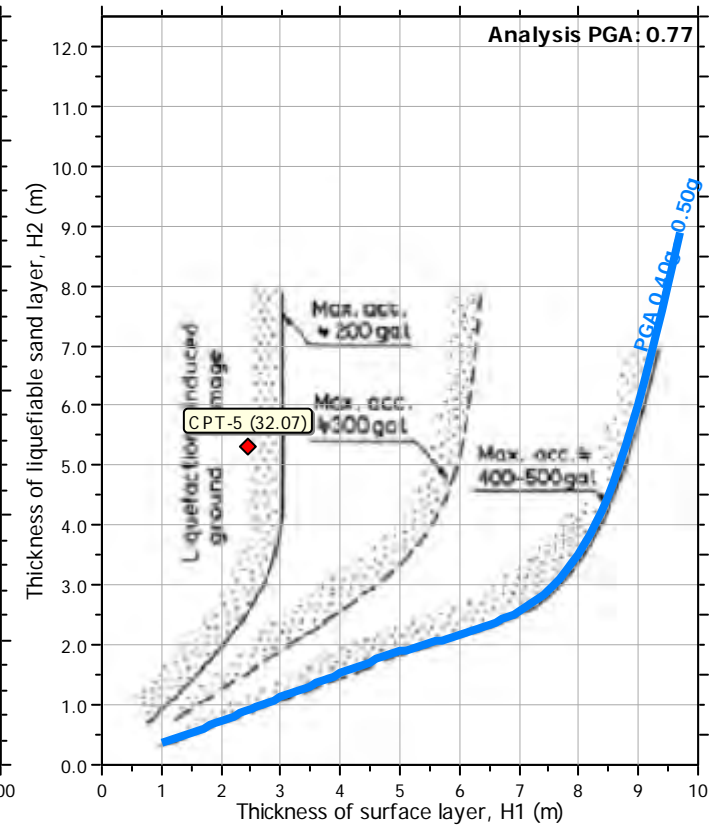
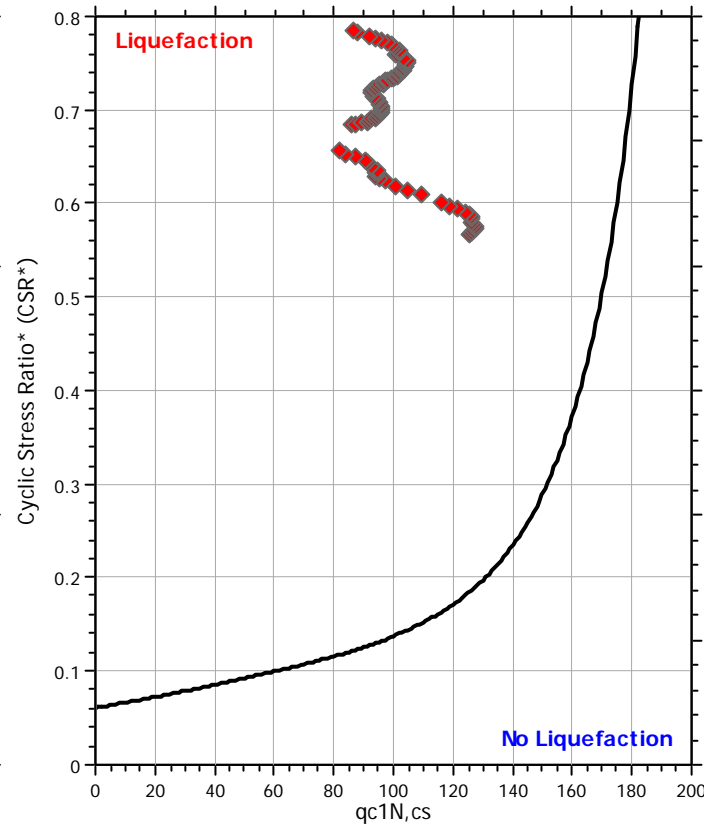
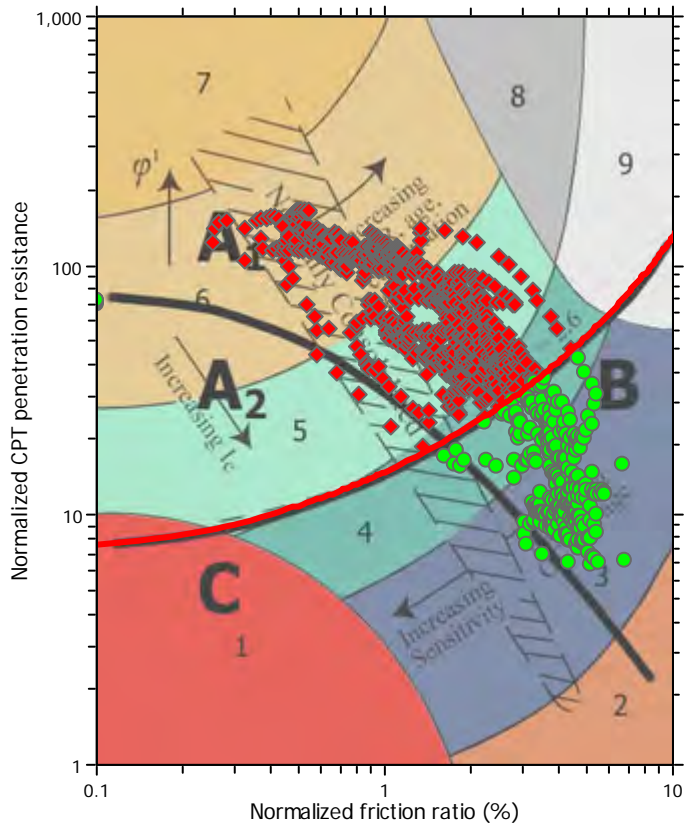
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

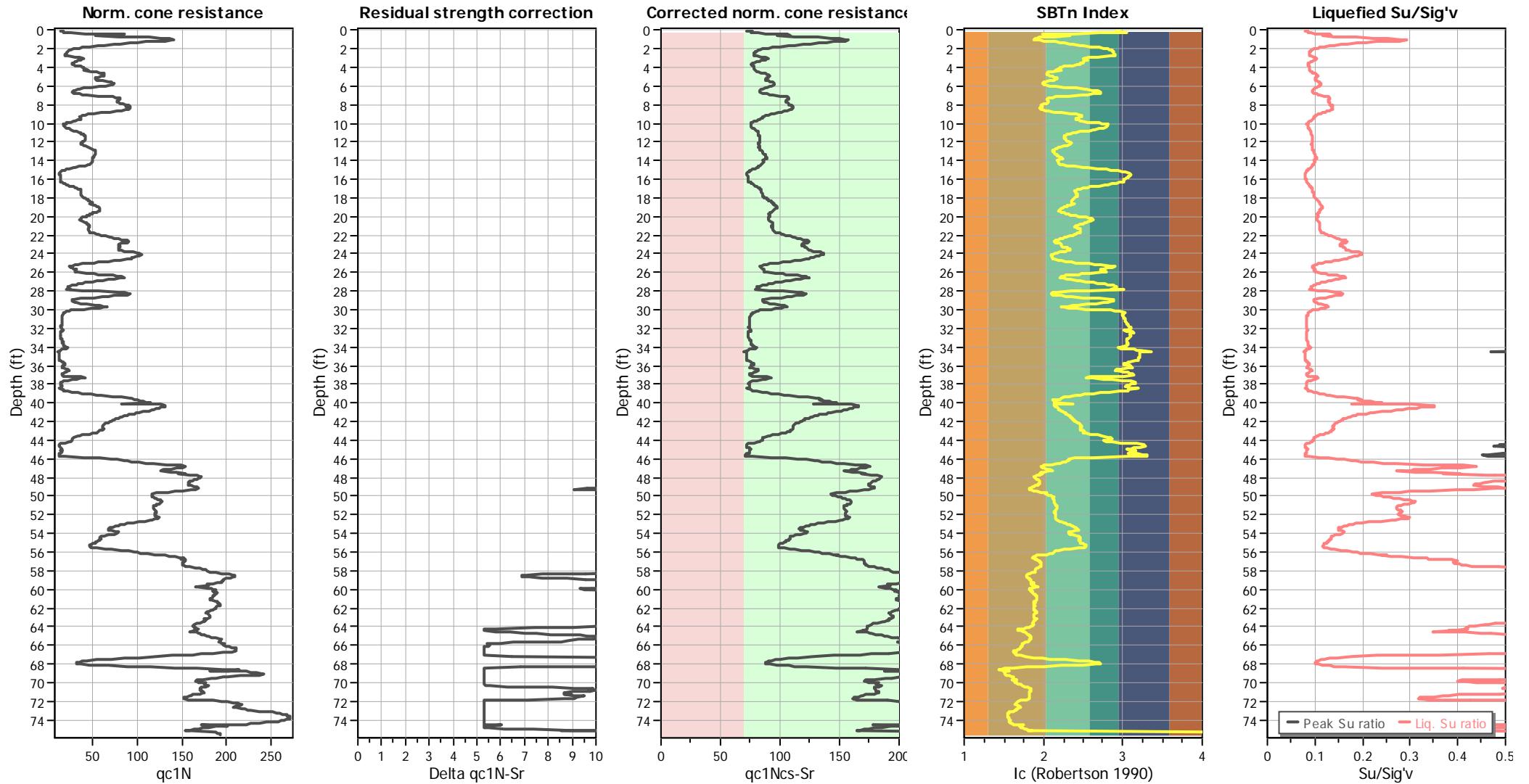
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	7.73	0.27	0.00	55.68	105.64
2	0.16	10.44	0.47	-0.10	53.67	110.51
3	0.20	10.04	0.67	0.00	61.96	112.99
4	0.28	15.86	0.54	0.00	40.97	112.55
5	0.34	25.10	0.49	0.00	26.35	112.87
6	0.41	44.98	0.49	0.00	14.21	114.38
7	0.48	52.61	0.56	0.00	12.57	115.73
8	0.55	50.55	0.64	0.00	14.26	116.61
9	0.60	32.73	0.70	-0.10	23.92	116.15
10	0.67	48.49	0.81	-0.38	17.02	118.20
11	0.74	58.13	0.87	-0.19	14.34	119.19
12	0.79	70.38	0.90	-0.38	11.46	119.92
13	0.89	78.81	1.05	-0.38	10.81	121.25
14	0.94	84.54	1.12	-0.48	10.28	121.93
15	0.98	88.15	1.18	-0.57	10.04	122.41
16	1.06	86.54	1.39	-0.57	11.60	123.57
17	1.12	81.62	1.51	-0.86	13.24	124.02
18	1.20	77.01	1.62	-1.24	14.87	124.38
19	1.25	68.37	1.69	-1.90	17.56	124.42
20	1.34	62.55	1.69	-2.47	19.38	124.21
21	1.38	56.83	1.68	-2.57	21.34	123.92
22	1.46	49.90	1.63	-2.67	23.95	123.38
23	1.54	45.58	1.53	-2.85	25.37	122.72
24	1.60	38.85	1.47	-3.04	28.84	121.99
25	1.66	34.84	1.38	-3.04	30.99	121.30
26	1.75	29.01	1.29	-3.24	35.23	120.32
27	1.80	26.40	1.23	-3.24	37.43	119.77
28	1.86	23.49	1.16	-3.14	40.23	119.05
29	1.91	21.08	1.11	-3.24	43.16	118.48
30	1.98	18.98	1.02	-3.24	45.39	117.62
31	2.04	17.37	0.92	-3.24	46.75	116.64
32	2.14	15.56	0.79	-3.04	47.97	115.20
33	2.17	14.46	0.75	-3.04	49.91	114.69
34	2.24	13.65	0.68	-3.04	50.38	113.84
35	2.32	12.95	0.62	-3.04	50.73	113.03
36	2.37	12.65	0.59	-2.95	50.62	112.55
37	2.43	11.95	0.55	-2.95	51.56	111.89
38	2.53	11.85	0.51	-2.95	50.69	111.36
39	2.58	11.45	0.51	-2.95	51.90	111.22
40	2.64	11.45	0.51	-2.95	51.99	111.26
41	2.70	11.45	0.52	-2.85	52.52	111.48
42	2.78	12.55	0.57	-2.76	50.48	112.32
43	2.82	13.35	0.60	-2.76	49.01	112.83
44	2.89	18.07	0.64	-2.76	39.41	114.00
45	2.96	21.69	0.64	-2.76	33.99	114.56
46	3.03	24.30	0.65	-2.76	30.77	114.85
47	3.12	23.39	0.61	-2.85	31.04	114.30
48	3.17	22.09	0.58	-2.85	32.16	113.88

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.23	20.98	0.55	-2.85	32.87	113.32
50	3.28	19.98	0.48	-2.67	32.55	112.23
51	3.35	19.38	0.40	-2.76	31.09	110.77
52	3.43	18.27	0.33	-2.76	30.41	109.19
53	3.48	17.27	0.28	-2.76	30.33	108.00
54	3.56	16.57	0.23	-2.57	29.24	106.41
55	3.61	16.26	0.21	-2.19	28.69	105.61
56	3.68	16.97	0.21	-1.71	27.58	105.72
57	3.77	18.77	0.21	-1.24	25.08	105.97
58	3.82	20.48	0.21	-1.14	23.11	106.23
59	3.87	22.39	0.22	-1.05	21.45	106.73
60	3.96	23.99	0.22	-0.76	20.00	106.92
61	4.02	24.50	0.21	-0.67	19.36	106.77
62	4.11	24.90	0.22	-0.57	19.14	106.92
63	4.16	25.50	0.22	-0.48	18.75	107.07
64	4.21	25.90	0.22	-0.38	18.53	107.19
65	4.27	27.71	0.23	-0.29	17.37	107.51
66	4.35	24.80	0.23	-0.24	19.80	107.44
67	4.40	29.82	0.24	-0.10	16.28	107.99
68	4.47	33.93	0.26	0.00	14.57	108.95
69	4.55	35.54	0.28	-0.10	14.32	109.66
70	4.61	37.05	0.29	-0.10	13.96	110.15
71	4.68	38.35	0.32	-0.10	13.93	110.83
72	4.75	38.85	0.34	-0.10	14.23	111.40
73	4.80	38.95	0.36	-0.10	14.47	111.70
74	4.86	38.45	0.38	-0.10	15.10	112.07
75	4.93	37.85	0.39	-0.10	15.57	112.21
76	5.00	36.85	0.39	-0.10	16.07	112.14
77	5.05	35.14	0.38	-0.10	16.86	111.92
78	5.14	32.43	0.38	-0.10	18.27	111.58
79	5.19	32.33	0.37	0.00	18.14	111.40
80	5.28	32.93	0.36	-0.10	17.59	111.28
81	5.34	34.14	0.36	-0.10	16.87	111.35
82	5.38	35.74	0.36	-0.10	16.01	111.46
83	5.45	37.75	0.36	-0.10	15.10	111.69
84	5.54	41.56	0.38	-0.10	13.72	112.22
85	5.59	43.77	0.38	-0.10	12.97	112.48
86	5.65	45.28	0.39	0.00	12.60	112.76
87	5.73	45.88	0.41	0.00	12.57	112.99
88	5.79	45.28	0.41	0.00	12.92	113.09
89	5.84	43.47	0.41	0.00	13.60	113.00
90	5.94	39.56	0.41	0.00	15.24	112.74
91	5.99	36.85	0.40	0.00	16.43	112.45
92	6.04	35.34	0.40	0.00	17.21	112.33
93	6.12	29.82	0.43	0.00	21.29	112.37
94	6.19	26.81	0.46	0.00	24.42	112.60
95	6.24	24.60	0.48	0.00	27.13	112.78
96	6.31	21.08	0.50	-0.10	31.57	112.56

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.37	20.08	0.49	0.00	32.76	112.33
98	6.44	18.37	0.50	-0.10	35.68	112.26
99	6.52	17.07	0.55	0.00	39.42	112.81
100	6.58	16.77	0.59	0.00	41.07	113.28
101	6.64	16.77	0.61	0.00	41.73	113.59
102	6.72	17.87	0.71	0.10	41.73	114.75
103	6.78	19.68	0.75	0.19	39.52	115.46
104	6.84	22.19	0.79	0.19	36.38	116.09
105	6.92	24.60	0.80	0.19	33.54	116.47
106	6.98	26.81	0.81	-0.19	31.23	116.77
107	7.03	28.41	0.83	-0.19	29.91	117.07
108	7.09	37.65	0.84	-0.19	22.99	117.88
109	7.18	49.60	0.85	-0.29	17.21	118.64
110	7.22	52.11	0.85	-0.29	16.26	118.76
111	7.33	56.12	0.81	-0.86	14.45	118.56
112	7.38	56.42	0.79	-0.29	14.13	118.38
113	7.43	56.02	0.78	-0.57	14.13	118.25
114	7.52	54.82	0.78	-0.29	14.54	118.22
115	7.58	54.42	0.78	-0.19	14.72	118.24
116	7.62	54.32	0.79	-0.19	14.80	118.28
117	7.72	55.32	0.81	-0.19	14.67	118.49
118	7.76	56.72	0.83	-0.19	14.43	118.73
119	7.82	58.43	0.87	-0.10	14.32	119.16
120	7.90	61.04	0.82	-0.10	13.08	118.83
121	7.97	62.75	0.79	-0.10	12.35	118.62
122	8.02	64.56	0.81	-0.10	12.12	118.85
123	8.07	65.96	0.82	-0.10	11.96	119.04
124	8.16	67.17	0.84	-0.10	11.94	119.28
125	8.21	65.26	0.85	-0.08	12.44	119.26
126	8.27	64.56	0.85	-0.08	12.67	119.26
127	8.35	68.07	0.84	-0.08	11.86	119.32
128	8.41	68.57	0.83	-0.10	11.71	119.26
129	8.49	67.47	0.84	-0.10	12.01	119.23
130	8.55	65.06	0.83	0.00	12.56	119.12
131	8.62	61.54	0.83	-0.10	13.44	118.97
132	8.67	57.63	0.84	-0.10	14.57	118.85
133	8.76	51.50	0.86	-0.10	16.80	118.80
134	8.80	47.99	0.88	-0.10	18.32	118.80
135	8.86	44.17	0.90	-0.10	20.15	118.74
136	8.95	37.55	0.89	-0.10	23.76	118.29
137	8.99	33.33	0.88	0.00	26.58	117.92
138	9.06	30.22	0.86	0.00	28.80	117.48
139	9.15	28.21	0.80	0.00	29.67	116.74
140	9.22	26.91	0.74	0.00	30.07	116.12
141	9.26	26.10	0.71	0.10	30.27	115.67
142	9.35	26.20	0.65	0.19	29.18	115.11
143	9.40	27.21	0.63	0.19	27.76	114.95
144	9.46	27.81	0.60	0.10	26.58	114.60

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.54	26.71	0.55	0.10	26.78	113.92
146	9.60	25.40	0.55	0.10	28.04	113.79
147	9.66	24.70	0.54	0.00	28.50	113.52
148	9.72	22.69	0.46	0.00	29.04	112.21
149	9.80	20.68	0.40	-0.10	29.81	110.87
150	9.85	18.57	0.40	-0.10	32.94	110.74
151	9.96	15.26	0.44	-0.10	40.22	110.86
152	10.00	14.56	0.45	-0.10	42.20	110.93
153	10.05	12.95	0.46	0.06	46.72	110.79
154	10.12	13.35	0.47	0.19	45.98	111.04
155	10.18	13.05	0.47	0.19	46.98	111.05
156	10.27	13.15	0.48	0.28	46.92	111.17
157	10.33	13.65	0.49	0.19	45.81	111.37
158	10.37	13.96	0.51	0.28	45.59	111.70
159	10.47	15.36	0.55	0.19	43.52	112.53
160	10.53	16.36	0.56	0.28	41.73	112.79
161	10.57	17.37	0.57	0.28	40.16	113.07
162	10.67	18.98	0.59	0.28	38.11	113.57
163	10.70	20.08	0.59	0.28	36.39	113.67
164	10.78	21.79	0.57	0.28	33.83	113.68
165	10.83	23.29	0.56	0.28	31.78	113.68
166	10.91	25.40	0.53	0.19	29.04	113.52
167	10.97	27.41	0.51	0.19	26.85	113.46
168	11.03	28.71	0.49	0.19	25.25	113.17
169	11.10	30.02	0.46	0.00	23.87	112.95
170	11.17	31.73	0.45	-0.38	22.48	112.90
171	11.26	32.93	0.45	-0.48	21.77	112.99
172	11.31	33.63	0.45	-0.57	21.37	113.04
173	11.36	34.14	0.45	-0.48	21.12	113.10
174	11.44	34.44	0.46	-0.57	21.07	113.19
175	11.50	34.54	0.46	-0.48	21.10	113.23
176	11.56	34.64	0.47	-0.48	21.19	113.32
177	11.63	34.54	0.47	-0.48	21.38	113.38
178	11.69	34.34	0.47	-0.48	21.59	113.40
179	11.76	34.14	0.47	-0.48	21.75	113.37
180	11.86	33.23	0.48	-0.48	22.53	113.40
181	11.89	33.03	0.48	-0.48	22.75	113.44
182	11.95	32.43	0.49	-0.57	23.44	113.58
183	12.01	31.53	0.50	-0.67	24.34	113.67
184	12.10	31.22	0.49	-0.86	24.40	113.47
185	12.15	31.12	0.49	-0.95	24.45	113.41
186	12.21	31.42	0.48	-0.95	24.17	113.35
187	12.28	31.93	0.48	-0.95	23.81	113.34
188	12.36	33.53	0.47	-1.05	22.65	113.37
189	12.40	34.74	0.47	-1.05	21.82	113.37
190	12.47	35.94	0.45	-0.76	20.88	113.23
191	12.55	38.05	0.44	-0.57	19.46	113.10
192	12.60	39.26	0.43	-0.48	18.72	113.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.69	41.06	0.43	-0.38	17.88	113.11
194	12.74	42.27	0.43	-0.29	17.40	113.21
195	12.82	44.07	0.44	-0.38	16.85	113.50
196	12.88	45.18	0.45	-0.38	16.64	113.75
197	12.94	46.08	0.46	-0.38	16.44	113.93
198	13.00	46.68	0.47	-0.38	16.41	114.13
199	13.09	46.99	0.49	-0.38	16.64	114.44
200	13.14	46.89	0.50	-0.38	16.79	114.51
201	13.20	46.89	0.50	-0.38	16.89	114.58
202	13.27	46.89	0.53	-0.29	17.39	115.01
203	13.34	46.89	0.55	-0.29	17.67	115.23
204	13.39	46.79	0.55	-0.38	17.85	115.32
205	13.47	46.58	0.57	-0.29	18.26	115.56
206	13.54	46.38	0.59	-0.38	18.63	115.76
207	13.59	45.98	0.61	-0.29	19.07	115.94
208	13.65	45.68	0.63	-0.57	19.53	116.17
209	13.72	45.38	0.65	-0.67	19.99	116.39
210	13.79	45.28	0.67	-0.86	20.37	116.61
211	13.85	45.18	0.62	-0.95	19.83	116.10
212	13.94	45.58	0.50	-1.14	17.85	114.50
213	13.98	45.78	0.51	-1.14	18.03	114.72
214	14.08	46.08	0.55	-1.33	18.45	115.19
215	14.13	46.08	0.55	-1.52	18.52	115.22
216	14.18	45.98	0.55	-1.71	18.64	115.26
217	14.27	44.78	0.53	-2.65	18.91	114.91
218	14.33	44.48	0.52	-2.65	18.84	114.68
219	14.39	43.07	0.51	-3.90	19.39	114.49
220	14.44	41.26	0.51	-4.00	20.34	114.40
221	14.53	38.05	0.51	-4.00	22.14	114.21
222	14.59	35.44	0.51	-4.00	23.83	114.07
223	14.64	32.83	0.53	-4.00	26.00	114.11
224	14.73	28.21	0.58	-4.09	31.01	114.40
225	14.77	26.81	0.60	-4.09	32.84	114.50
226	14.83	21.79	0.62	-4.19	39.66	114.23
227	14.93	18.07	0.61	-4.19	46.02	113.69
228	14.98	16.57	0.59	-4.19	48.90	113.29
229	15.03	15.36	0.58	-4.19	51.60	112.98
230	15.10	14.16	0.58	-4.09	54.92	112.73
231	15.17	13.25	0.58	-4.09	57.93	112.58
232	15.22	12.45	0.58	-4.09	60.64	112.37
233	15.29	11.55	0.57	-4.00	64.15	112.14
234	15.37	11.65	0.58	-4.00	64.13	112.26
235	15.44	11.65	0.61	-3.90	65.10	112.58
236	15.52	11.75	0.63	-3.90	65.60	112.87
237	15.56	11.95	0.64	-3.90	65.13	113.01
238	15.62	12.05	0.63	-3.90	64.63	112.96
239	15.70	12.25	0.61	-3.90	63.36	112.77
240	15.76	12.25	0.59	-3.90	62.89	112.55

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.82	12.35	0.57	-3.90	61.98	112.33
242	15.91	12.45	0.55	-3.90	60.98	112.05
243	15.95	12.65	0.54	-3.90	60.10	112.01
244	16.01	12.65	0.52	-3.90	59.35	111.67
245	16.08	12.75	0.53	-3.90	59.41	111.81
246	16.14	12.85	0.54	-3.90	59.39	111.92
247	16.22	13.25	0.57	-3.81	59.28	112.45
248	16.31	14.06	0.61	-3.81	57.98	113.07
249	16.36	14.96	0.63	-3.81	55.98	113.47
250	16.41	16.06	0.64	-3.81	53.47	113.81
251	16.50	18.17	0.68	-3.81	49.57	114.50
252	16.55	19.68	0.70	-3.81	47.06	114.89
253	16.61	21.18	0.69	-3.81	44.38	115.04
254	16.69	23.69	0.67	-3.81	40.18	115.10
255	16.74	25.20	0.66	-3.90	37.99	115.13
256	16.80	27.31	0.65	-3.90	35.34	115.22
257	16.88	29.42	0.64	-3.90	32.88	115.22
258	16.95	31.83	0.63	-3.90	30.55	115.33
259	17.00	33.53	0.62	-3.81	29.08	115.39
260	17.07	35.34	0.62	-3.71	27.58	115.42
261	17.15	36.04	0.62	-3.62	27.16	115.48
262	17.20	36.54	0.62	-3.62	26.81	115.50
263	17.26	37.15	0.61	-3.52	26.39	115.50
264	17.33	37.35	0.63	-3.43	26.56	115.70
265	17.41	37.55	0.65	-3.33	26.78	115.91
266	17.46	37.65	0.65	-3.24	26.89	116.02
267	17.52	37.65	0.67	-3.14	27.11	116.14
268	17.60	37.35	0.68	-3.04	27.56	116.24
269	17.65	37.45	0.68	-2.85	27.63	116.32
270	17.74	38.25	0.69	-2.85	27.31	116.48
271	17.80	38.75	0.70	-2.76	27.14	116.60
272	17.85	39.56	0.71	-2.76	26.82	116.77
273	17.93	40.86	0.73	-2.67	26.36	117.05
274	17.99	41.87	0.76	-2.57	26.22	117.40
275	18.07	43.47	0.79	-2.47	25.74	117.78
276	18.13	44.88	0.82	-2.47	25.38	118.12
277	18.18	45.88	0.85	-2.47	25.23	118.42
278	18.29	47.19	0.86	-2.47	24.73	118.57
279	18.32	48.09	0.88	-2.38	24.56	118.80
280	18.38	49.20	0.93	-2.28	24.66	119.28
281	18.44	50.20	0.96	-2.28	24.52	119.54
282	18.53	51.30	1.00	-2.28	24.51	119.90
283	18.58	52.01	1.02	-1.57	24.39	120.06
284	18.66	49.50	1.04	-1.57	25.89	120.09
285	18.71	53.81	1.04	-0.95	23.81	120.26
286	18.81	55.52	1.04	-0.86	23.12	120.33
287	18.85	56.83	1.04	-0.76	22.60	120.39
288	18.90	58.03	1.04	-0.76	22.15	120.44

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	19.01	60.14	1.01	-0.76	21.16	120.36
290	19.06	61.04	0.99	-0.86	20.61	120.21
291	19.11	61.34	0.97	-0.86	20.30	120.05
292	19.16	61.54	0.94	-0.86	19.96	119.83
293	19.26	61.74	0.87	-0.86	19.21	119.27
294	19.30	61.74	0.84	-0.86	18.97	119.06
295	19.36	61.74	0.82	-0.86	18.73	118.85
296	19.45	60.54	0.81	-0.86	19.15	118.77
297	19.50	59.03	0.81	-0.86	19.68	118.69
298	19.58	56.22	0.80	-0.86	20.62	118.44
299	19.64	54.52	0.79	-0.86	21.24	118.29
300	19.69	53.31	0.79	-0.86	21.76	118.23
301	19.78	50.70	0.79	-0.67	23.02	118.14
302	19.84	50.30	0.85	-0.57	23.94	118.62
303	19.90	47.49	0.94	-0.57	26.54	119.23
304	19.95	46.48	1.04	-0.57	28.33	119.91
305	20.03	45.08	1.11	-0.57	30.03	120.32
306	20.08	41.87	1.15	-1.05	32.69	120.41
307	20.16	40.86	1.20	-1.05	34.09	120.68
308	20.25	40.06	1.27	-1.24	35.56	121.04
309	20.30	39.36	1.30	-1.62	36.43	121.13
310	20.35	39.16	1.31	-1.52	36.80	121.20
311	20.45	42.07	1.34	-1.52	34.88	121.51
312	20.50	43.07	1.34	-1.52	34.26	121.60
313	20.54	42.87	1.34	-1.52	34.45	121.60
314	20.62	46.18	1.34	-1.62	32.27	121.78
315	20.69	47.39	1.34	-1.71	31.51	121.81
316	20.74	47.39	1.29	-1.62	31.05	121.53
317	20.83	48.79	1.25	-1.71	29.84	121.36
318	20.88	49.90	1.23	-1.62	29.08	121.32
319	20.94	50.90	1.15	-1.52	27.71	120.85
320	21.04	51.00	1.06	-1.52	26.80	120.29
321	21.08	51.91	1.06	-1.43	26.37	120.34
322	21.14	51.40	1.06	-1.24	26.67	120.32
323	21.23	50.70	1.11	-1.14	27.66	120.64
324	21.28	50.50	1.17	-1.14	28.34	120.96
325	21.33	50.60	1.20	-1.05	28.69	121.18
326	21.42	50.60	1.22	-0.86	28.99	121.33
327	21.48	50.70	1.23	-1.05	29.07	121.39
328	21.53	51.70	1.25	-1.14	28.73	121.53
329	21.62	52.21	1.30	-1.33	29.00	121.83
330	21.68	52.51	1.34	-1.43	29.24	122.05
331	21.73	54.52	1.39	-1.33	28.69	122.41
332	21.79	58.43	1.44	-1.43	27.37	122.88
333	21.86	61.74	1.50	-1.33	26.42	123.29
334	21.92	63.75	1.56	-1.43	26.12	123.67
335	22.00	67.87	1.64	-1.52	25.12	124.17
336	22.05	71.08	1.67	-1.62	24.19	124.40

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.12	72.79	1.68	-1.62	23.78	124.54
338	22.22	79.92	1.70	-1.62	21.69	124.83
339	22.27	81.42	1.72	-1.62	21.40	124.95
340	22.32	85.74	1.73	-1.62	20.36	125.15
341	22.38	89.86	1.76	-1.62	19.50	125.37
342	22.47	95.08	1.80	-1.62	18.58	125.69
343	22.52	97.99	1.82	-1.71	18.10	125.85
344	22.59	101.80	1.85	-1.62	17.48	126.05
345	22.65	104.01	1.86	-1.71	17.11	126.13
346	22.71	104.82	1.86	-1.62	16.98	126.16
347	22.77	102.61	1.86	-1.62	17.44	126.11
348	22.85	98.19	1.84	-1.62	18.29	125.93
349	22.90	94.98	1.85	-1.62	19.03	125.87
350	22.98	91.86	1.89	-1.62	20.02	125.94
351	23.06	91.76	1.90	-1.62	20.13	125.97
352	23.10	92.47	1.90	-1.62	20.02	126.02
353	23.17	94.17	2.00	-1.62	20.15	126.41
354	23.24	94.17	2.10	-1.62	20.76	126.80
355	23.32	92.77	2.23	-1.62	21.80	127.20
356	23.37	92.62	2.33	-1.38	22.33	127.49
357	23.45	92.62	2.55	-1.38	23.47	128.17
358	23.51	92.47	2.59	-1.38	23.74	128.28
359	23.56	93.47	2.60	-1.05	23.56	128.34
360	23.63	97.18	2.62	-1.14	22.70	128.47
361	23.71	101.10	2.61	-1.24	21.77	128.55
362	23.77	107.83	2.58	-1.33	20.19	128.61
363	23.84	112.45	2.54	-1.33	19.15	128.62
364	23.89	116.76	2.51	-1.05	18.23	128.62
365	23.95	119.67	2.42	-1.05	17.35	128.40
366	24.05	122.89	2.25	-0.86	16.13	127.93
367	24.09	123.09	2.19	-0.86	15.88	127.76
368	24.15	122.99	2.13	-0.86	15.66	127.56
369	24.24	120.68	2.04	-0.76	15.64	127.19
370	24.30	118.07	1.99	-0.76	15.82	126.93
371	24.37	113.75	1.93	-0.76	16.30	126.62
372	24.42	111.64	1.86	-0.76	16.33	126.30
373	24.48	110.94	1.80	-0.86	16.18	126.06
374	24.54	110.34	1.76	-0.86	16.12	125.90
375	24.61	106.42	1.74	-0.86	16.71	125.69
376	24.71	96.78	1.67	-0.86	18.35	125.19
377	24.76	88.75	1.62	-0.86	19.96	124.76
378	24.81	80.92	1.56	-0.86	21.70	124.26
379	24.90	69.27	1.45	-0.86	24.72	123.34
380	24.96	62.05	1.38	-0.86	27.07	122.72
381	25.00	55.22	1.34	-0.86	29.90	122.17
382	25.09	46.79	1.28	-0.86	34.41	121.47
383	25.16	42.07	1.28	-0.86	37.88	121.18
384	25.20	38.05	1.29	-0.86	41.62	121.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.30	32.43	1.34	-0.86	48.27	120.87
386	25.36	30.52	1.35	-0.95	50.89	120.81
387	25.40	29.92	1.36	-0.86	51.82	120.80
388	25.48	31.53	1.33	-0.95	49.41	120.76
389	25.53	33.43	1.30	-0.86	46.85	120.76
390	25.59	36.04	1.27	-0.86	43.56	120.73
391	25.67	38.85	1.28	-0.86	41.09	121.01
392	25.75	38.55	1.31	-0.86	41.78	121.15
393	25.80	36.95	1.33	-0.86	43.58	121.14
394	25.87	37.00	1.38	-0.86	44.27	121.45
395	25.95	37.05	1.50	-0.86	45.65	122.04
396	25.99	41.16	1.57	-0.76	42.50	122.62
397	26.09	54.32	1.78	-0.67	35.04	124.22
398	26.14	64.76	1.84	-0.67	30.17	124.89
399	26.19	69.07	1.87	-0.76	28.59	125.18
400	26.27	83.03	1.86	-0.48	23.70	125.61
401	26.33	89.66	1.89	-0.48	22.01	125.89
402	26.39	95.28	1.95	-0.57	20.95	126.27
403	26.45	102.10	2.04	-0.57	19.88	126.77
404	26.53	105.22	2.09	-0.57	19.50	127.02
405	26.59	105.82	2.10	-0.67	19.44	127.07
406	26.64	100.70	2.08	-0.67	20.47	126.87
407	26.73	91.96	2.03	-0.67	22.41	126.50
408	26.79	85.44	2.02	-0.67	24.18	126.26
409	26.86	76.10	2.00	-0.67	27.14	125.91
410	26.93	69.78	1.96	-0.67	29.37	125.57
411	26.99	63.05	1.92	-0.57	32.05	125.14
412	27.08	53.51	1.84	-0.67	36.74	124.44
413	27.13	49.09	1.83	-0.67	39.61	124.19
414	27.17	45.78	1.82	-0.67	42.06	123.98
415	27.25	42.67	1.79	-0.67	44.42	123.68
416	27.32	40.06	1.71	-0.86	46.12	123.19
417	27.38	34.14	1.61	-0.86	51.35	122.37
418	27.44	31.32	1.42	-0.86	52.65	121.26
419	27.53	28.91	1.17	-0.76	52.49	119.61
420	27.58	28.21	1.12	-0.76	52.85	119.26
421	27.63	27.81	1.11	-0.76	53.36	119.18
422	27.71	29.22	1.16	-0.80	52.06	119.57
423	27.77	32.13	1.21	-0.84	49.06	120.11
424	27.82	25.70	1.26	-0.89	59.14	119.88
425	27.90	50.40	1.33	-0.82	34.47	121.95
426	27.97	60.64	1.40	-0.82	29.54	122.77
427	28.02	73.19	1.47	-0.76	24.92	123.55
428	28.12	99.80	1.56	-1.05	18.26	124.77
429	28.17	109.43	1.59	-1.05	16.53	125.13
430	28.23	115.26	1.63	-1.05	15.72	125.43
431	28.31	116.16	1.63	-1.05	15.59	125.45
432	28.37	112.75	1.61	-1.05	16.09	125.29

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.42	106.62	1.60	-0.95	17.15	125.08
434	28.51	95.58	1.61	-1.05	19.65	124.88
435	28.55	87.25	1.60	-1.05	21.74	124.62
436	28.61	78.71	1.64	-1.05	24.65	124.56
437	28.71	65.96	1.84	-1.05	31.08	124.94
438	28.76	57.33	1.84	-1.05	35.54	124.62
439	28.81	49.30	1.85	-1.05	40.81	124.26
440	28.91	36.95	1.67	-1.05	50.09	122.83
441	28.95	35.84	1.61	-1.05	50.69	122.49
442	29.00	35.79	1.58	-1.05	50.47	122.35
443	29.07	35.74	1.57	-1.05	50.43	122.29
444	29.16	39.16	1.57	-1.05	46.98	122.50
445	29.21	43.17	1.57	-0.95	43.28	122.74
446	29.30	49.40	1.57	-0.86	38.46	123.07
447	29.36	51.30	1.56	-0.86	37.12	123.13
448	29.41	57.23	1.53	-0.86	33.33	123.28
449	29.50	69.17	1.54	-0.86	27.78	123.77
450	29.56	75.80	1.51	-0.86	25.04	123.84
451	29.61	82.53	1.49	-0.86	22.71	123.94
452	29.69	86.74	1.26	-0.95	19.83	122.86
453	29.76	83.13	1.28	-0.95	20.96	122.84
454	29.80	76.60	1.29	-0.95	23.12	122.74
455	29.89	64.15	1.29	-0.95	27.83	122.26
456	29.93	54.72	1.28	-0.95	32.56	121.86
457	30.00	46.08	1.28	-1.22	38.24	121.41
458	30.06	34.34	1.27	-1.22	49.13	120.63
459	30.13	31.63	1.21	-1.22	51.68	120.09
460	30.21	28.21	1.15	-1.33	55.54	119.42
461	30.27	24.70	1.09	-1.52	60.54	118.74
462	30.36	23.69	0.95	-1.52	59.92	117.61
463	30.41	23.49	0.87	-1.52	58.83	116.98
464	30.46	22.79	0.80	-1.52	58.60	116.24
465	30.55	21.79	0.69	-1.52	58.17	115.07
466	30.60	21.69	0.67	-1.52	57.82	114.80
467	30.65	21.49	0.66	-1.52	58.02	114.67
468	30.73	21.08	0.66	-1.52	58.94	114.62
469	30.80	20.98	0.65	-1.52	59.07	114.54
470	30.85	20.78	0.64	-1.52	59.28	114.41
471	30.95	20.58	0.63	-1.52	59.56	114.28
472	30.99	20.38	0.64	-1.43	60.21	114.33
473	31.05	20.48	0.65	-1.43	60.33	114.46
474	31.15	20.48	0.66	-1.33	60.62	114.55
475	31.18	20.48	0.66	-1.33	60.74	114.59
476	31.23	20.48	0.67	-1.33	60.99	114.67
477	31.30	20.78	0.69	-1.33	60.85	114.90
478	31.39	20.78	0.70	-1.24	61.43	115.11
479	31.45	20.78	0.72	-1.24	61.78	115.23
480	31.50	20.68	0.73	-1.14	62.37	115.36

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.58	20.68	0.73	-1.14	62.53	115.39
482	31.64	20.68	0.73	-1.05	62.55	115.38
483	31.70	20.68	0.74	-0.95	62.72	115.43
484	31.78	20.48	0.76	-0.95	63.75	115.60
485	31.84	20.28	0.77	-0.95	64.54	115.68
486	31.90	20.08	0.81	-0.86	66.04	116.03
487	31.96	20.58	0.85	-0.76	65.80	116.44
488	32.03	21.18	0.90	-0.76	65.54	116.92
489	32.09	21.18	0.89	-0.67	65.47	116.88
490	32.19	22.59	0.84	-0.57	61.32	116.57
491	32.24	23.49	0.82	-0.48	59.33	116.56
492	32.32	22.09	0.81	0.10	61.95	116.31
493	32.39	20.08	0.82	0.67	66.62	116.10
494	32.43	19.58	0.82	0.76	67.99	116.07
495	32.48	19.48	0.80	0.76	67.82	115.88
496	32.55	19.78	0.75	0.86	65.90	115.45
497	32.62	19.78	0.70	0.86	64.56	114.89
498	32.69	19.38	0.68	0.86	65.07	114.63
499	32.78	19.38	0.68	0.86	65.16	114.63
500	32.82	19.38	0.68	0.86	65.21	114.64
501	32.88	19.58	0.66	0.95	64.37	114.50
502	32.97	19.98	0.69	0.95	64.23	114.86
503	33.02	20.18	0.71	0.95	64.32	115.09
504	33.08	20.68	0.73	0.95	63.69	115.35
505	33.17	21.49	0.74	0.95	62.24	115.56
506	33.21	21.79	0.75	0.95	61.77	115.65
507	33.29	22.49	0.81	0.95	61.90	116.35
508	33.37	23.39	0.87	1.05	61.40	116.95
509	33.41	23.29	0.89	1.05	62.09	117.12
510	33.47	23.49	0.92	1.05	62.29	117.36
511	33.56	23.49	0.95	0.95	62.91	117.58
512	33.61	24.30	0.97	1.05	61.77	117.81
513	33.68	24.10	0.99	0.95	62.62	117.96
514	33.77	24.90	1.04	1.05	62.10	118.40
515	33.82	25.20	1.06	1.05	61.96	118.57
516	33.87	26.50	1.08	1.05	59.95	118.80
517	33.97	29.62	1.12	1.05	55.92	119.39
518	34.01	31.22	1.14	1.14	54.04	119.65
519	34.08	31.42	1.16	1.05	54.12	119.78
520	34.13	29.32	1.13	1.05	56.64	119.43
521	34.19	26.10	1.14	0.95	61.93	119.16
522	34.27	22.39	1.10	0.95	68.83	118.58
523	34.36	20.58	1.00	0.95	71.18	117.65
524	34.41	19.38	0.95	0.95	73.35	117.13
525	34.46	15.36	0.91	1.05	85.60	116.23
526	34.54	18.57	0.86	1.14	73.64	116.29
527	34.60	18.37	0.85	1.14	74.02	116.16
528	34.65	18.37	0.85	1.14	74.14	116.19

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.73	18.37	0.84	1.14	73.92	116.09
530	34.80	18.27	0.81	1.14	73.54	115.81
531	34.85	18.07	0.80	1.24	73.89	115.68
532	34.92	17.87	0.79	1.24	74.25	115.54
533	34.98	18.07	0.78	1.24	73.44	115.47
534	35.04	17.87	0.78	1.24	74.22	115.49
535	35.12	18.07	0.78	1.24	73.64	115.50
536	35.17	18.37	0.77	1.24	72.71	115.50
537	35.25	18.37	0.77	1.24	72.59	115.43
538	35.32	18.57	0.78	1.24	72.46	115.60
539	35.37	18.67	0.81	1.24	72.87	115.85
540	35.44	19.18	0.85	1.24	72.59	116.30
541	35.50	20.58	0.89	1.24	69.94	116.83
542	35.60	23.59	0.98	1.24	65.07	117.85
543	35.65	24.60	1.02	1.24	63.75	118.20
544	35.70	26.20	1.04	1.24	61.34	118.55
545	35.79	28.01	1.07	1.24	58.88	118.91
546	35.85	27.81	1.07	1.24	59.27	118.90
547	35.90	26.71	1.04	1.24	60.54	118.57
548	35.98	24.50	1.02	1.24	64.28	118.22
549	36.03	23.99	1.01	1.24	65.09	118.07
550	36.09	24.55	1.01	1.24	64.10	118.16
551	36.18	23.19	1.01	1.33	66.95	118.02
552	36.24	24.60	1.01	1.43	64.14	118.17
553	36.29	25.60	1.03	1.43	62.58	118.38
554	36.38	30.72	1.13	1.43	56.27	119.55
555	36.44	33.93	1.21	1.43	53.24	120.27
556	36.49	35.54	1.26	1.33	52.00	120.65
557	36.57	33.13	1.25	1.33	54.82	120.42
558	36.63	29.82	1.25	1.33	59.43	120.16
559	36.69	27.51	1.24	1.33	63.07	119.93
560	36.77	25.90	1.11	1.33	63.92	118.99
561	36.83	24.90	1.06	1.33	64.86	118.52
562	36.88	23.39	1.00	1.33	66.93	117.98
563	36.96	22.69	0.98	1.33	68.13	117.76
564	37.03	22.49	0.99	1.43	68.81	117.81
565	37.08	27.31	0.99	1.43	59.52	118.26
566	37.14	36.54	1.03	1.52	48.13	119.27
567	37.23	54.62	1.16	1.52	35.19	121.10
568	37.28	61.14	1.27	1.52	32.75	122.05
569	37.36	56.32	1.40	1.24	36.95	122.56
570	37.41	48.29	1.47	1.24	43.42	122.54
571	37.48	41.06	1.46	1.14	49.41	122.11
572	37.57	32.83	1.37	1.14	57.63	121.11
573	37.63	28.11	1.30	1.14	63.67	120.32
574	37.66	26.20	1.25	0.95	66.29	119.86
575	37.77	23.29	1.09	0.95	69.51	118.57
576	37.82	22.29	1.00	0.95	70.13	117.85

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.88	21.89	0.93	1.05	69.61	117.26
578	37.96	21.99	0.85	1.05	67.71	116.61
579	38.01	22.59	0.82	1.05	65.70	116.40
580	38.06	22.49	0.78	1.14	65.07	116.04
581	38.13	22.89	0.66	1.14	61.38	114.88
582	38.19	23.39	0.65	1.14	60.01	114.75
583	38.26	23.59	0.71	1.14	61.32	115.49
584	38.32	23.29	0.70	1.24	61.71	115.35
585	38.41	22.59	0.75	1.24	64.37	115.75
586	38.46	19.58	0.81	1.24	73.10	115.95
587	38.52	24.80	0.88	1.43	62.89	117.15
588	38.59	25.70	0.99	1.52	63.39	118.08
589	38.65	26.81	1.09	1.52	63.26	118.90
590	38.73	30.02	1.21	1.62	60.09	119.97
591	38.79	33.93	1.25	1.62	55.38	120.52
592	38.86	42.77	1.34	1.71	47.22	121.56
593	38.92	51.30	1.42	1.62	41.50	122.43
594	38.98	59.94	1.51	1.62	36.79	123.27
595	39.06	72.69	1.64	1.62	31.60	124.37
596	39.12	81.12	1.74	1.52	29.00	125.05
597	39.18	89.96	1.81	1.52	26.45	125.57
598	39.28	106.22	1.95	1.52	22.89	126.53
599	39.32	110.54	2.00	1.52	22.20	126.83
600	39.37	119.27	2.11	1.52	20.91	127.40
601	39.48	132.53	2.34	1.52	19.56	128.42
602	39.52	135.03	2.44	1.52	19.59	128.76
603	39.57	138.75	2.57	1.52	19.55	129.22
604	39.66	143.57	2.36	1.52	17.84	128.65
605	39.70	144.77	2.07	1.52	16.36	127.71
606	39.77	148.69	2.34	1.62	17.02	128.68
607	39.87	152.70	2.51	1.62	17.19	129.27
608	39.92	156.72	2.61	1.62	17.05	129.62
609	39.98	161.84	2.70	1.62	16.71	129.94
610	40.06	119.98	2.92	0.57	24.92	129.79
611	40.12	171.18	3.07	0.25	16.86	131.02
612	40.16	176.00	3.18	-0.76	16.64	131.34
613	40.25	182.12	3.42	-1.14	16.71	131.97
614	40.31	182.32	3.56	-1.33	17.12	132.26
615	40.37	181.42	3.62	-1.24	17.41	132.36
616	40.44	178.41	3.63	-1.24	17.84	132.35
617	40.50	175.50	3.62	-1.24	18.19	132.28
618	40.56	172.99	3.59	-1.24	18.44	132.18
619	40.63	169.17	3.53	-1.24	18.78	132.01
620	40.71	166.96	3.44	-1.24	18.83	131.79
621	40.77	163.55	3.39	-1.24	19.15	131.64
622	40.86	159.63	3.34	-1.24	19.58	131.47
623	40.90	156.52	3.32	-1.24	19.97	131.37
624	40.96	152.81	3.26	-1.24	20.37	131.18

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.03	146.68	3.19	-1.24	21.13	130.92
626	41.09	142.97	3.13	-1.24	21.56	130.72
627	41.15	139.25	3.08	-1.24	22.06	130.54
628	41.24	134.93	2.92	-1.24	22.25	130.07
629	41.28	131.62	2.87	-1.24	22.69	129.89
630	41.35	129.21	2.82	-1.24	22.96	129.70
631	41.41	125.00	2.76	-1.05	23.59	129.46
632	41.50	122.49	2.70	-0.86	23.90	129.26
633	41.55	119.88	2.66	-0.67	24.33	129.11
634	41.61	116.86	2.60	-0.38	24.75	128.88
635	41.71	114.25	2.52	0.00	25.01	128.59
636	41.75	112.95	2.50	0.10	25.22	128.50
637	41.80	111.44	2.48	0.19	25.53	128.42
638	41.87	109.94	2.46	0.38	25.85	128.33
639	41.93	108.23	2.46	0.38	26.27	128.27
640	42.00	105.32	2.44	0.38	27.00	128.15
641	42.09	102.51	2.41	0.38	27.66	128.00
642	42.14	100.60	2.39	0.38	28.12	127.88
643	42.20	99.09	2.37	0.38	28.48	127.78
644	42.29	96.98	2.33	0.38	28.97	127.62
645	42.34	96.18	2.32	0.38	29.16	127.56
646	42.39	95.28	2.31	0.28	29.43	127.52
647	42.48	94.47	2.31	0.19	29.69	127.47
648	42.54	94.37	2.29	-0.10	29.70	127.44
649	42.59	94.57	2.27	-0.38	29.51	127.37
650	42.68	95.48	2.20	-0.57	28.81	127.16
651	42.73	95.88	2.19	-0.76	28.68	127.15
652	42.79	96.18	2.21	-1.24	28.73	127.22
653	42.88	94.57	2.19	-1.71	29.11	127.09
654	42.93	92.87	2.22	-2.19	29.89	127.15
655	42.99	90.36	2.25	-2.67	30.99	127.19
656	43.06	89.15	2.22	-3.04	31.25	127.05
657	43.14	87.45	2.03	-3.71	30.66	126.36
658	43.18	85.24	1.93	-4.00	30.80	125.94
659	43.28	79.31	1.85	-4.47	32.58	125.45
660	43.33	73.99	1.82	-4.76	34.73	125.17
661	43.42	65.96	1.81	-5.14	38.79	124.84
662	43.44	63.45	1.78	-5.23	40.01	124.63
663	43.53	57.23	1.62	-5.42	42.26	123.69
664	43.58	55.22	1.53	-5.42	42.71	123.19
665	43.67	48.49	1.48	-5.42	46.90	122.59
666	43.73	46.08	1.44	-5.42	48.50	122.28
667	43.78	44.68	1.41	-5.42	49.38	122.05
668	43.86	46.03	1.38	-5.42	47.88	121.94
669	43.92	45.58	1.33	-5.42	47.76	121.67
670	43.97	45.98	1.22	-5.42	46.20	121.09
671	44.06	45.88	0.97	-5.42	43.02	119.40
672	44.12	43.57	1.00	-5.42	45.24	119.44

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.17	39.26	1.03	-5.42	49.78	119.45
674	44.26	32.23	0.97	-5.42	57.07	118.53
675	44.30	28.51	0.94	-5.07	62.15	118.02
676	44.37	23.59	0.92	-5.07	71.07	117.34
677	44.44	20.78	0.96	-4.71	78.97	117.37
678	44.50	21.49	0.96	-4.71	77.19	117.47
679	44.59	20.38	0.95	-4.35	79.98	117.24
680	44.64	20.48	0.95	-4.00	79.69	117.24
681	44.73	22.39	0.93	-3.90	74.36	117.32
682	44.77	23.79	0.91	-3.90	70.82	117.34
683	44.83	24.70	0.90	-3.90	68.61	117.31
684	44.88	26.40	0.89	-3.90	65.09	117.38
685	44.96	27.71	0.87	-3.90	62.35	117.31
686	45.03	26.20	0.91	-3.90	66.03	117.55
687	45.08	25.10	0.96	-3.90	69.30	117.86
688	45.17	26.20	1.00	-3.90	67.83	118.22
689	45.22	25.20	0.98	-3.81	69.41	117.96
690	45.28	26.20	0.91	-3.81	66.24	117.57
691	45.36	25.20	0.69	-3.81	63.09	115.38
692	45.41	23.19	0.63	-3.81	65.84	114.60
693	45.48	21.38	0.66	-3.81	70.65	114.65
694	45.54	20.28	0.77	-3.81	76.62	115.68
695	45.63	19.88	0.89	-3.81	80.94	116.74
696	45.67	20.38	0.98	-3.81	81.39	117.44
697	45.74	31.02	1.17	-3.71	62.91	119.78
698	45.83	65.56	1.41	-3.62	36.38	122.97
699	45.88	92.97	1.55	-3.71	26.36	124.55
700	45.97	112.14	1.86	-3.71	23.29	126.32
701	46.03	116.76	2.09	-3.71	23.59	127.27
702	46.07	121.98	2.30	-3.71	23.58	128.07
703	46.17	131.42	2.59	-3.81	23.07	129.14
704	46.22	136.54	2.70	-3.81	22.57	129.53
705	46.27	142.16	2.81	-3.90	22.00	129.91
706	46.36	149.19	2.94	-3.90	21.35	130.37
707	46.41	154.21	2.97	-4.00	20.63	130.51
708	46.49	164.85	2.98	-4.09	19.10	130.72
709	46.54	175.80	3.02	-4.28	17.75	130.97
710	46.62	193.67	3.03	-4.47	15.67	131.22
711	46.66	199.79	3.02	-4.57	15.00	131.28
712	46.73	215.76	2.96	-5.04	13.30	131.33
713	46.82	223.28	2.90	-5.61	12.48	131.26
714	46.85	223.49	2.87	-5.80	12.37	131.18
715	46.92	219.07	2.81	-6.57	12.58	130.98
716	47.01	210.43	2.80	-5.85	13.33	130.86
717	47.06	202.90	2.82	-6.09	14.11	130.80
718	47.15	191.86	2.86	-5.90	15.43	130.79
719	47.21	187.34	2.99	-5.80	16.39	131.04
720	47.25	186.34	2.96	-5.80	16.44	130.97

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.31	187.94	2.53	-5.80	14.72	129.84
722	47.41	204.61	2.51	-5.80	12.98	129.99
723	47.46	214.25	2.57	-5.71	12.33	130.28
724	47.54	226.30	2.66	-5.90	11.63	130.66
725	47.58	214.95	2.72	-5.46	12.76	130.68
726	47.67	232.52	2.79	-5.46	11.56	131.07
727	47.71	235.94	2.80	-5.46	11.33	131.12
728	47.77	245.37	2.77	-5.71	10.58	131.15
729	47.85	252.90	2.78	-5.04	10.09	131.24
730	47.92	255.01	2.77	-4.57	9.95	131.24
731	47.97	254.41	2.76	-4.19	9.98	131.22
732	48.06	251.70	2.79	-3.81	10.24	131.25
733	48.12	249.49	2.80	-3.52	10.45	131.28
734	48.17	246.18	2.83	-3.33	10.76	131.31
735	48.25	241.16	2.86	-3.04	11.23	131.34
736	48.31	237.94	2.88	-2.85	11.52	131.34
737	48.36	235.43	2.89	-2.76	11.76	131.35
738	48.45	234.03	2.84	-2.67	11.74	131.21
739	48.50	233.12	2.79	-2.57	11.68	131.08
740	48.57	234.03	2.77	-2.47	11.54	131.03
741	48.63	233.32	2.72	-2.47	11.48	130.90
742	48.72	234.03	2.67	-2.47	11.29	130.78
743	48.77	235.13	2.63	-2.47	11.08	130.67
744	48.85	238.95	2.56	-2.47	10.60	130.51
745	48.91	242.96	2.52	-2.57	10.18	130.42
746	48.97	246.88	2.52	-2.57	9.93	130.47
747	49.05	253.61	2.51	-2.67	9.48	130.51
748	49.11	257.12	2.49	-2.85	9.20	130.48
749	49.16	258.93	2.46	-3.14	9.00	130.40
750	49.21	258.83	2.39	-3.14	8.82	130.21
751	49.28	256.01	2.27	-3.04	8.62	129.79
752	49.35	249.49	2.24	-3.04	8.94	129.63
753	49.42	233.83	2.22	-3.04	9.95	129.40
754	49.48	220.37	2.16	-2.95	10.76	129.05
755	49.54	207.32	2.20	-2.95	12.05	129.06
756	49.61	193.27	2.06	-2.95	12.82	128.39
757	49.68	187.54	2.17	-2.95	13.90	128.72
758	49.76	182.52	2.00	-2.95	13.74	128.05
759	49.81	180.42	2.05	-2.95	14.18	128.19
760	49.88	180.01	2.19	-3.24	14.85	128.67
761	49.95	179.61	2.34	-3.24	15.52	129.14
762	50.02	179.96	2.46	-3.47	16.02	129.53
763	50.10	179.96	2.59	-3.47	16.53	129.90
764	50.15	180.31	2.66	-3.47	16.76	130.09
765	50.20	183.93	2.69	-3.81	16.47	130.24
766	50.28	186.04	2.78	-3.81	16.56	130.49
767	50.34	187.94	2.85	-3.81	16.60	130.70
768	50.44	190.76	2.95	-3.81	16.65	130.99

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	50.47	191.96	2.97	-3.81	16.59	131.06
770	50.54	192.66	3.01	-3.81	16.68	131.17
771	50.59	192.46	3.03	-3.71	16.78	131.22
772	50.69	191.16	3.06	-3.71	17.06	131.27
773	50.73	190.56	3.06	-3.81	17.14	131.26
774	50.84	188.65	3.01	-3.81	17.23	131.12
775	50.86	188.05	3.00	-3.81	17.26	131.09
776	50.93	186.14	2.98	-3.81	17.44	131.01
777	50.99	184.43	2.97	-3.81	17.64	130.97
778	51.05	182.12	2.96	-3.81	17.90	130.91
779	51.13	181.72	2.95	-3.81	17.92	130.87
780	51.20	182.02	2.93	-3.81	17.83	130.82
781	51.25	181.82	2.92	-3.81	17.84	130.80
782	51.34	181.92	2.92	-3.81	17.85	130.80
783	51.38	182.02	2.92	-3.71	17.85	130.80
784	51.48	183.63	2.92	-3.71	17.68	130.83
785	51.53	185.13	2.92	-3.71	17.50	130.85
786	51.58	186.24	2.92	-3.71	17.36	130.85
787	51.67	187.74	2.87	-3.71	17.03	130.75
788	51.72	187.44	2.85	-3.71	17.00	130.69
789	51.78	187.04	2.84	-3.71	17.04	130.67
790	51.86	185.64	2.85	-3.71	17.28	130.68
791	51.93	185.13	2.87	-3.71	17.41	130.71
792	51.97	184.73	2.88	-3.71	17.52	130.74
793	52.06	185.84	2.91	-3.71	17.52	130.83
794	52.11	187.04	2.93	-3.71	17.45	130.89
795	52.17	187.84	2.96	-3.71	17.47	130.98
796	52.24	189.65	2.99	-3.71	17.37	131.07
797	52.31	190.56	3.01	-3.71	17.35	131.14
798	52.37	189.75	2.99	-3.71	17.40	131.08
799	52.47	186.14	2.93	-3.71	17.67	130.89
800	52.52	182.12	2.91	-3.71	18.09	130.77
801	52.57	180.11	2.87	-3.71	18.21	130.64
802	52.67	171.78	2.76	-3.71	18.94	130.24
803	52.72	166.76	2.68	-3.71	19.37	129.96
804	52.77	161.34	2.62	-3.71	19.95	129.71
805	52.86	153.81	2.54	-3.71	20.85	129.38
806	52.91	149.09	2.51	-3.71	21.52	129.21
807	52.96	144.87	2.47	-3.71	22.09	129.01
808	53.02	140.56	2.43	-3.71	22.74	128.83
809	53.10	134.33	2.41	-3.71	23.91	128.67
810	53.16	130.42	2.40	-3.71	24.68	128.55
811	53.24	125.70	2.37	-3.71	25.61	128.38
812	53.30	122.69	2.26	-3.81	25.72	127.97
813	53.36	118.97	2.18	-3.81	26.17	127.62
814	53.42	117.06	2.21	-3.81	26.90	127.70
815	53.48	115.76	2.24	-3.81	27.42	127.77
816	53.56	115.96	2.29	-3.81	27.63	127.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	53.61	115.36	2.31	-3.85	27.96	127.99
818	53.69	120.68	2.31	-3.85	26.59	128.10
819	53.75	126.80	2.27	-3.85	24.92	128.09
820	53.82	130.42	2.21	-3.90	23.80	127.96
821	53.88	131.22	2.17	-3.90	23.40	127.83
822	53.97	130.12	2.07	-3.90	23.11	127.48
823	54.02	129.21	2.00	-3.90	22.90	127.21
824	54.09	123.99	1.92	-3.90	23.57	126.80
825	54.14	119.27	1.89	-3.90	24.48	126.59
826	54.21	114.55	1.86	-3.90	25.45	126.37
827	54.28	107.43	1.86	-3.90	27.45	126.23
828	54.33	103.51	1.87	-3.90	28.68	126.18
829	54.43	101.80	1.88	-3.90	29.27	126.16
830	54.48	102.00	1.88	-4.00	29.25	126.18
831	54.53	102.91	1.88	-4.00	28.92	126.17
832	54.62	102.81	1.83	-4.00	28.65	126.00
833	54.67	101.80	1.79	-4.00	28.68	125.80
834	54.73	101.20	1.74	-4.00	28.52	125.59
835	54.82	98.59	1.67	-4.00	28.80	125.21
836	54.87	96.88	1.62	-4.00	29.02	124.97
837	54.95	94.78	1.55	-4.00	29.10	124.56
838	55.01	93.57	1.53	-4.00	29.36	124.44
839	55.06	91.16	1.51	-4.00	30.09	124.31
840	55.12	88.55	1.49	-4.00	30.85	124.12
841	55.20	85.94	1.47	-4.00	31.70	123.95
842	55.26	84.64	1.46	-4.09	32.14	123.87
843	55.32	83.33	1.45	-4.09	32.59	123.78
844	55.41	83.33	1.44	-4.09	32.55	123.74
845	55.47	85.24	1.44	-4.09	31.80	123.80
846	55.51	88.25	1.46	-4.09	30.75	123.95
847	55.59	96.28	1.47	-4.09	28.11	124.24
848	55.67	110.74	1.49	-4.09	24.09	124.68
849	55.72	122.79	1.50	-4.09	21.35	124.99
850	55.81	138.45	1.56	-4.09	18.73	125.57
851	55.86	145.38	1.60	-4.09	17.79	125.86
852	55.92	150.80	1.66	-4.09	17.30	126.22
853	56.01	159.13	1.81	-4.09	16.91	126.99
854	56.06	163.85	1.89	-4.09	16.65	127.36
855	56.11	168.67	1.95	-4.09	16.33	127.68
856	56.21	181.12	2.05	-4.09	15.22	128.20
857	56.25	191.56	2.07	-4.09	14.13	128.41
858	56.31	203.10	2.05	-4.09	12.89	128.49
859	56.38	216.76	1.78	-4.09	10.54	127.60
860	56.44	224.19	1.87	-4.09	10.34	128.06
861	56.50	231.72	1.94	-4.09	10.04	128.41
862	56.58	241.46	2.01	-4.19	9.61	128.77
863	56.65	246.18	2.09	-4.57	9.57	129.10
864	56.73	236.84	2.23	-4.57	10.74	129.48

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.76	242.86	2.29	-4.57	10.50	129.73
866	56.84	244.17	2.36	-4.85	10.66	129.97
867	56.92	241.66	2.44	-5.04	11.11	130.19
868	56.98	239.55	2.49	-5.14	11.44	130.31
869	57.02	236.84	2.51	-5.23	11.70	130.33
870	57.12	234.23	2.53	-5.23	12.01	130.38
871	57.17	234.23	2.55	-5.23	12.06	130.42
872	57.23	234.23	2.56	-5.23	12.11	130.46
873	57.32	234.23	2.60	-5.14	12.27	130.58
874	57.36	234.53	2.62	-5.23	12.31	130.64
875	57.42	235.53	2.65	-5.14	12.33	130.73
876	57.50	237.24	2.68	-5.23	12.30	130.83
877	57.55	240.75	2.70	-5.14	12.07	130.90
878	57.62	245.97	2.73	-5.14	11.79	131.06
879	57.69	254.11	2.74	-5.14	11.23	131.17
880	57.77	262.64	2.77	-5.23	10.72	131.31
881	57.83	267.36	2.80	-5.52	10.49	131.43
882	57.91	271.68	2.82	-5.80	10.27	131.52
883	57.97	273.99	2.83	-6.00	10.18	131.58
884	58.01	274.99	2.86	-6.00	10.19	131.66
885	58.11	278.30	2.90	-6.18	10.11	131.79
886	58.16	282.72	2.91	-6.18	9.88	131.86
887	58.22	290.05	2.93	-6.28	9.48	131.96
888	58.31	301.19	2.90	-6.38	8.80	131.98
889	58.36	307.52	2.88	-6.38	8.43	131.98
890	58.41	313.34	2.87	-6.66	8.11	131.99
891	58.51	318.86	2.85	-6.85	7.80	131.99
892	58.55	320.77	2.85	-7.04	7.72	132.00
893	58.60	321.07	2.85	-6.95	7.71	132.01
894	58.67	318.56	2.86	-7.23	7.86	132.01
895	58.76	314.45	2.88	-7.42	8.11	132.03
896	58.80	312.84	2.88	-7.42	8.20	132.02
897	58.88	307.22	2.89	-7.42	8.51	132.00
898	58.94	303.90	2.93	-7.42	8.79	132.08
899	59.01	301.90	2.99	-7.61	9.06	132.21
900	59.06	301.09	3.01	-7.52	9.14	132.24
901	59.15	300.89	2.96	-7.61	9.04	132.12
902	59.20	300.09	2.93	-7.61	9.03	132.06
903	59.25	298.08	2.92	-7.61	9.12	132.02
904	59.34	290.35	2.97	-7.71	9.69	132.07
905	59.40	286.13	2.87	-7.71	9.67	131.78
906	59.45	283.22	2.62	-7.71	9.15	131.09
907	59.54	279.71	2.70	-7.80	9.60	131.29
908	59.60	278.60	2.72	-7.80	9.73	131.33
909	59.65	278.70	2.76	-7.86	9.84	131.44
910	59.74	255.81	2.74	-7.91	11.31	131.18
911	59.78	261.44	2.65	-7.91	10.65	130.99
912	59.87	285.83	2.56	-7.91	8.88	130.96

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	59.94	291.25	2.61	-7.90	8.70	131.12
914	59.99	292.06	2.65	-7.99	8.77	131.24
915	60.05	294.17	2.72	-8.27	8.87	131.46
916	60.14	287.24	2.81	-8.27	9.50	131.63
917	60.19	293.31	2.83	-8.27	9.22	131.74
918	60.24	288.04	2.82	-8.47	9.50	131.68
919	60.34	292.46	2.85	-8.56	9.33	131.78
920	60.38	292.96	2.89	-8.56	9.41	131.89
921	60.44	291.46	2.94	-8.56	9.63	132.00
922	60.53	288.34	3.00	-8.66	9.98	132.12
923	60.58	285.43	3.03	-8.76	10.24	132.17
924	60.63	283.52	3.06	-8.76	10.44	132.22
925	60.71	281.01	3.07	-8.76	10.65	132.24
926	60.78	281.52	3.09	-8.76	10.66	132.28
927	60.83	281.72	3.08	-8.95	10.64	132.27
928	60.91	279.71	3.05	-8.85	10.69	132.18
929	60.97	276.70	3.03	-8.66	10.82	132.09
930	61.03	276.75	3.05	-8.66	10.88	132.14
931	61.10	276.80	3.05	-8.66	10.88	132.14
932	61.16	279.61	3.02	-8.66	10.64	132.11
933	61.23	286.54	3.04	-8.66	10.26	132.21
934	61.32	290.35	3.04	-8.66	10.03	132.23
935	61.38	291.05	3.06	-8.66	10.06	132.30
936	61.43	291.15	3.10	-8.66	10.16	132.39
937	61.52	293.06	3.11	-8.66	10.07	132.42
938	61.56	294.97	3.09	-8.66	9.93	132.40
939	61.62	296.17	3.09	-8.66	9.85	132.40
940	61.71	293.86	3.09	-8.66	9.99	132.38
941	61.77	291.05	3.09	-8.56	10.17	132.36
942	61.84	290.35	3.07	-8.66	10.15	132.30
943	61.92	290.35	3.00	-8.56	9.98	132.14
944	61.94	290.35	2.98	-8.76	9.95	132.10
945	62.02	290.35	2.95	-8.56	9.87	132.02
946	62.12	290.05	2.95	-8.56	9.89	132.02
947	62.15	289.35	2.95	-8.66	9.92	132.00
948	62.22	286.64	2.93	-8.56	10.04	131.93
949	62.27	283.52	2.91	-8.66	10.20	131.87
950	62.36	277.50	2.87	-8.56	10.47	131.71
951	62.41	275.69	2.86	-8.66	10.57	131.68
952	62.48	275.09	2.84	-8.47	10.55	131.62
953	62.55	275.49	2.81	-8.47	10.44	131.54
954	62.61	278.70	2.80	-8.47	10.20	131.53
955	62.69	281.31	2.77	-8.47	9.97	131.48
956	62.74	282.72	2.75	-8.47	9.84	131.44
957	62.81	283.62	2.77	-8.37	9.83	131.49
958	62.87	284.73	2.77	-8.37	9.79	131.52
959	62.95	285.33	2.77	-8.37	9.76	131.52
960	63.00	284.13	2.78	-8.37	9.87	131.54

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	63.10	277.90	2.80	-8.37	10.32	131.54
962	63.13	272.88	2.81	-8.37	10.66	131.51
963	63.19	277.85	2.80	-8.37	10.33	131.54
964	63.26	273.99	2.78	-8.37	10.51	131.44
965	63.32	277.80	2.73	-8.37	10.14	131.35
966	63.39	279.81	2.67	-8.37	9.84	131.20
967	63.49	278.80	2.61	-8.37	9.75	131.03
968	63.52	277.60	2.57	-8.37	9.69	130.90
969	63.60	275.09	2.45	-8.28	9.51	130.54
970	63.69	270.47	2.37	-8.28	9.54	130.24
971	63.74	266.56	2.37	-8.28	9.79	130.20
972	63.79	266.41	2.37	-8.28	9.81	130.21
973	63.85	266.41	2.36	-8.28	9.77	130.16
974	63.92	266.26	2.28	-8.28	9.55	129.93
975	63.99	270.47	2.19	-8.28	9.01	129.68
976	64.05	273.68	2.13	-8.28	8.59	129.47
977	64.13	277.80	2.00	-8.28	7.96	129.08
978	64.18	279.81	1.76	-8.28	7.05	128.16
979	64.24	281.11	1.36	-8.37	5.00	126.25
980	64.34	278.20	1.39	-8.37	5.79	126.39
981	64.39	276.60	1.42	-8.18	6.00	126.56
982	64.45	278.00	1.50	-8.28	6.23	126.98
983	64.51	271.28	1.63	-8.37	7.06	127.52
984	64.59	275.09	1.78	-8.33	7.38	128.18
985	64.64	279.61	1.87	-8.40	7.44	128.57
986	64.73	282.12	2.01	-8.37	7.78	129.12
987	64.78	283.22	2.09	-8.47	8.00	129.44
988	64.83	285.63	2.22	-8.47	8.26	129.88
989	64.93	287.44	2.39	-8.47	8.70	130.46
990	64.98	289.05	2.46	-8.47	8.82	130.68
991	65.03	289.75	2.53	-8.37	8.97	130.88
992	65.12	292.26	2.62	-8.37	9.12	131.18
993	65.17	294.97	2.69	-8.37	9.15	131.37
994	65.23	299.29	2.74	-8.37	9.06	131.55
995	65.31	304.91	2.79	-8.37	8.90	131.74
996	65.36	307.22	2.79	-8.47	8.76	131.74
997	65.42	308.42	2.78	-8.47	8.68	131.72
998	65.50	307.72	2.70	-8.28	8.52	131.52
999	65.58	305.81	2.62	-8.28	8.42	131.29
1000	65.63	306.82	2.57	-8.28	8.22	131.14
1001	65.72	311.23	2.39	-8.37	7.52	130.66
1002	65.77	313.14	2.30	-8.28	7.18	130.39
1003	65.83	316.55	2.18	-8.37	6.69	130.03
1004	65.92	314.85	2.17	-8.28	6.72	129.95
1005	65.97	313.64	2.18	-8.28	6.83	130.00
1006	66.02	314.14	2.20	-8.28	6.85	130.05
1007	66.11	317.66	2.20	-8.28	6.72	130.11
1008	66.16	322.28	2.19	-8.28	6.47	130.08

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	66.22	325.79	2.18	-8.28	6.31	130.09
1010	66.30	329.41	2.23	-8.28	6.28	130.27
1011	66.35	331.11	2.26	-8.28	6.30	130.39
1012	66.42	331.31	2.21	-8.28	6.15	130.21
1013	66.50	330.21	1.99	-8.18	5.61	129.46
1014	66.55	329.61	1.86	-8.18	5.26	128.95
1015	66.61	330.01	1.72	-8.18	4.84	128.39
1016	66.70	326.09	1.65	-8.18	4.79	128.07
1017	66.76	321.17	1.69	-8.18	5.09	128.18
1018	66.80	315.45	1.65	-8.18	5.20	127.97
1019	66.88	303.50	1.48	-8.18	5.00	127.09
1020	66.96	288.54	1.29	-8.18	5.00	125.95
1021	67.01	276.60	1.21	-8.18	5.00	125.37
1022	67.06	260.63	1.15	-8.28	5.00	124.89
1023	67.13	249.99	1.14	-8.18	5.00	124.71
1024	67.19	226.80	1.07	-8.28	5.00	123.97
1025	67.29	190.05	1.00	-8.18	9.98	123.04
1026	67.35	175.29	0.98	-8.18	11.37	122.76
1027	67.40	158.03	0.89	-8.18	12.69	121.78
1028	67.50	133.23	0.75	-8.18	15.01	120.11
1029	67.55	117.57	0.77	-8.18	18.09	119.99
1030	67.60	102.41	0.80	-8.18	22.02	119.93
1031	67.68	83.73	0.83	-8.18	28.48	119.72
1032	67.73	73.69	0.95	-8.18	34.34	120.36
1033	67.79	67.57	1.02	-8.18	37.92	120.69
1034	67.87	62.95	1.03	-8.18	40.41	120.58
1035	67.93	62.55	1.08	-8.18	41.24	120.91
1036	67.98	65.16	1.15	-8.18	40.66	121.48
1037	68.05	71.28	1.20	-8.18	38.14	121.98
1038	68.11	88.55	1.19	-8.09	31.06	122.49
1039	68.19	125.30	1.12	-8.09	19.96	122.88
1040	68.25	162.34	1.01	-8.09	13.17	122.79
1041	68.34	218.67	0.98	-8.09	5.00	123.29
1042	68.39	253.40	0.81	-8.09	4.72	122.21
1043	68.44	284.13	0.71	-8.09	2.95	121.51
1044	68.54	316.25	0.81	-8.09	2.30	122.73
1045	68.59	328.70	0.85	-8.09	2.12	123.26
1046	68.64	335.63	0.93	-7.99	2.20	123.96
1047	68.71	322.98	1.04	-8.21	2.97	124.66
1048	68.77	301.50	1.10	-8.21	3.96	124.92
1049	68.84	344.77	1.22	-8.21	2.88	125.95
1050	68.91	350.19	1.27	-8.37	2.90	126.33
1051	68.97	355.51	1.36	-8.37	3.01	126.86
1052	69.04	362.03	1.44	-8.37	3.06	127.33
1053	69.12	363.64	1.49	-8.37	3.14	127.56
1054	69.17	359.63	1.52	-8.28	3.36	127.68
1055	69.27	344.26	1.50	-8.28	3.80	127.47
1056	69.29	338.64	1.48	-8.28	3.95	127.37

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	69.37	322.28	1.47	-8.28	4.51	127.20
1058	69.42	316.65	1.45	-8.28	4.66	127.04
1059	69.52	308.32	1.40	-8.28	4.82	126.71
1060	69.57	303.30	1.35	-8.28	4.85	126.40
1061	69.65	292.86	1.27	-8.28	4.99	125.84
1062	69.71	285.03	1.30	-8.28	5.00	125.97
1063	69.77	285.23	1.06	-8.28	4.53	124.51
1064	69.85	283.93	1.14	-8.28	4.92	125.03
1065	69.89	285.43	1.27	-8.28	5.00	125.81
1066	69.96	288.44	1.20	-8.18	4.94	125.41
1067	70.02	293.16	1.29	-8.21	5.00	126.01
1068	70.09	297.48	1.45	-8.23	5.00	126.88
1069	70.15	296.22	1.53	-8.23	5.85	127.29
1070	70.24	294.97	1.69	-8.21	6.45	127.97
1071	70.30	298.78	1.78	-8.28	6.59	128.41
1072	70.36	300.49	1.88	-8.18	6.82	128.80
1073	70.44	297.78	2.01	-8.18	7.37	129.26
1074	70.48	296.68	2.08	-8.18	7.65	129.50
1075	70.55	289.75	2.16	-8.18	8.28	129.72
1076	70.60	286.74	2.21	-8.18	8.61	129.87
1077	70.69	284.73	2.26	-8.18	8.91	130.03
1078	70.74	286.69	2.27	-8.18	8.84	130.08
1079	70.83	284.93	2.27	-8.18	8.94	130.07
1080	70.89	286.64	2.28	-8.18	8.86	130.10
1081	70.94	287.54	2.29	-8.18	8.85	130.14
1082	71.02	291.76	2.28	-8.09	8.60	130.16
1083	71.08	292.96	2.26	-8.09	8.47	130.09
1084	71.14	291.35	2.23	-8.09	8.48	129.99
1085	71.22	287.64	2.17	-8.09	8.50	129.76
1086	71.27	283.72	2.12	-8.09	8.57	129.55
1087	71.33	279.71	2.02	-8.09	8.46	129.15
1088	71.40	275.89	2.00	-8.09	8.61	129.04
1089	71.47	272.78	1.99	-8.09	8.76	128.97
1090	71.53	270.97	1.93	-7.99	8.67	128.73
1091	71.63	266.56	1.84	-7.99	8.65	128.37
1092	71.67	266.66	1.84	-7.99	8.63	128.35
1093	71.73	267.66	1.81	-7.95	8.47	128.24
1094	71.81	275.79	1.76	-7.95	7.82	128.11
1095	71.88	288.54	1.75	-7.95	7.11	128.19
1096	71.93	306.82	1.75	-7.90	6.22	128.34
1097	71.99	317.36	1.75	-7.90	5.75	128.42
1098	72.05	324.99	1.78	-7.90	5.52	128.59
1099	72.13	332.82	1.85	-7.90	5.42	128.93
1100	72.18	336.63	1.88	-7.90	5.36	129.07
1101	72.27	341.65	1.88	-7.90	5.19	129.13
1102	72.32	343.26	1.90	-7.90	5.17	129.20
1103	72.38	342.76	1.96	-7.90	5.36	129.41
1104	72.46	339.95	2.05	-7.90	5.74	129.74

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	72.52	335.73	2.12	-7.90	6.11	129.96
1106	72.62	333.32	2.13	-7.90	6.26	129.99
1107	72.66	334.22	2.12	-7.80	6.19	129.95
1108	72.71	336.53	2.10	-7.80	6.05	129.91
1109	72.82	342.56	2.04	-7.80	5.64	129.73
1110	72.85	346.17	2.04	-7.80	5.49	129.74
1111	72.91	349.18	2.03	-7.80	5.36	129.74
1112	72.97	354.10	2.02	-7.80	5.16	129.75
1113	73.06	362.94	1.92	-7.80	4.59	129.44
1114	73.11	368.26	1.89	-7.80	4.31	129.32
1115	73.17	378.10	1.86	-7.80	3.94	129.30
1116	73.24	383.42	1.85	-7.71	3.75	129.30
1117	73.31	388.34	1.84	-7.71	3.58	129.28
1118	73.37	392.15	1.88	-7.71	3.58	129.47
1119	73.43	394.76	1.94	-7.71	3.65	129.70
1120	73.51	399.08	1.97	-7.71	3.59	129.83
1121	73.56	400.49	1.97	-7.61	3.56	129.85
1122	73.65	404.50	2.03	-7.61	3.60	130.10
1123	73.71	404.80	2.06	-7.61	3.65	130.19
1124	73.76	405.31	2.11	-7.61	3.76	130.37
1125	73.84	405.00	2.18	-7.61	3.94	130.61
1126	73.90	403.50	2.17	-7.52	3.96	130.57
1127	73.95	401.29	2.13	-7.52	3.95	130.44
1128	74.06	396.97	2.04	-7.52	3.86	130.09
1129	74.10	391.45	2.04	-7.52	4.01	130.03
1130	74.15	385.73	1.94	-7.42	3.95	129.65
1131	74.22	376.49	1.79	-7.52	3.84	128.98
1132	74.29	371.57	1.78	-7.52	3.97	128.91
1133	74.35	364.65	1.79	-7.33	4.24	128.92
1134	74.43	355.41	1.79	-7.33	4.54	128.84
1135	74.48	349.48	1.80	-7.35	4.79	128.85
1136	74.54	295.17	1.83	-7.38	7.24	128.58
1137	74.64	327.00	1.89	-7.35	5.94	129.04
1138	74.69	319.87	1.92	-7.35	6.35	129.11
1139	74.75	312.84	1.81	-7.33	6.33	128.62
1140	74.83	303.70	1.66	-7.33	6.27	127.94
1141	74.87	297.68	1.72	-7.33	6.77	128.15
1142	74.94	291.76	1.79	-7.33	7.31	128.38
1143	75.02	285.43	1.87	-7.14	7.93	128.66
1144	75.08	276.90	1.92	-7.49	8.59	128.77
1145	75.13	267.16	1.94	-7.49	9.25	128.74
1146	75.22	278.70	1.90	-7.49	8.42	128.70
1147	75.28	280.41	0.00	-7.71	100.00	87.36
1148	75.33	282.42	0.00	-7.71	100.00	87.36
1149	75.42	284.73	0.00	-7.71	100.00	87.36
1150	75.47	286.54	0.00	-7.71	100.00	87.36
1151	75.53	288.24	0.00	-7.71	100.00	87.36
1152	75.62	289.55	0.00	-7.61	100.00	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
2	0.16	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
3	0.20	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
4	0.28	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
5	0.34	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
6	0.41	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
7	0.48	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
8	0.55	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
9	0.60	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
10	0.67	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
11	0.74	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
12	0.79	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
13	0.89	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
14	0.94	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
15	0.98	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
16	1.06	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
17	1.12	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
18	1.20	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
19	1.25	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
20	1.34	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
21	1.38	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
22	1.46	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
23	1.54	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
24	1.60	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
25	1.66	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
26	1.75	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
27	1.80	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
28	1.86	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
29	1.91	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
30	1.98	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
31	2.04	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
32	2.14	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
33	2.17	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
34	2.24	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
35	2.32	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
36	2.37	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
37	2.43	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
38	2.53	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
39	2.58	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
40	2.64	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
41	2.70	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
42	2.78	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
43	2.82	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
44	2.89	0.17	0.00	0.17	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
45	2.96	0.17	0.00	0.17	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
46	3.03	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
47	3.12	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
48	3.17	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	3.23	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
50	3.28	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
51	3.35	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
52	3.43	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
53	3.48	0.20	0.00	0.20	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
54	3.56	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
55	3.61	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
56	3.68	0.21	0.00	0.21	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
57	3.77	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
58	3.82	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
59	3.87	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
60	3.96	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
61	4.02	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
62	4.11	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
63	4.16	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
64	4.21	0.24	0.00	0.24	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
65	4.27	0.24	0.00	0.24	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
66	4.35	0.25	0.00	0.25	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
67	4.40	0.25	0.00	0.25	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
68	4.47	0.26	0.00	0.26	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
69	4.55	0.26	0.00	0.26	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
70	4.61	0.26	0.00	0.26	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
71	4.68	0.27	0.00	0.27	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
72	4.75	0.27	0.00	0.27	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
73	4.80	0.27	0.00	0.27	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
74	4.86	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
75	4.93	0.28	0.00	0.28	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
76	5.00	0.28	0.00	0.28	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
77	5.05	0.29	0.00	0.29	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
78	5.14	0.29	0.00	0.29	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
79	5.19	0.30	0.00	0.30	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
80	5.28	0.30	0.00	0.30	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
81	5.34	0.30	0.00	0.30	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
82	5.38	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
83	5.45	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
84	5.54	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
85	5.59	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
86	5.65	0.32	0.00	0.32	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
87	5.73	0.33	0.00	0.33	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
88	5.79	0.33	0.00	0.33	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
89	5.84	0.33	0.00	0.33	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
90	5.94	0.34	0.00	0.34	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
91	5.99	0.34	0.00	0.34	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
92	6.04	0.34	0.00	0.34	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
93	6.12	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
94	6.19	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
95	6.24	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
96	6.31	0.36	0.00	0.36	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	6.37	0.36	0.00	0.36	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
98	6.44	0.37	0.00	0.37	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
99	6.52	0.37	0.00	0.37	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
100	6.58	0.37	0.00	0.37	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
101	6.64	0.38	0.00	0.38	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
102	6.72	0.38	0.00	0.38	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
103	6.78	0.38	0.00	0.38	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
104	6.84	0.39	0.00	0.39	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
105	6.92	0.39	0.00	0.39	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
106	6.98	0.40	0.00	0.40	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
107	7.03	0.40	0.00	0.40	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
108	7.09	0.40	0.00	0.40	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
109	7.18	0.41	0.00	0.41	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
110	7.22	0.41	0.00	0.41	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
111	7.33	0.42	0.00	0.42	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
112	7.38	0.42	0.00	0.42	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
113	7.43	0.42	0.00	0.42	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
114	7.52	0.43	0.00	0.43	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
115	7.58	0.43	0.00	0.43	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
116	7.62	0.43	0.00	0.43	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
117	7.72	0.44	0.00	0.44	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
118	7.76	0.44	0.00	0.44	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
119	7.82	0.45	0.00	0.45	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
120	7.90	0.45	0.00	0.45	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
121	7.97	0.45	0.00	0.45	0.98	0.493	1.05	0.468	1.10	1.30	2.000	No
122	8.02	0.46	0.00	0.46	0.98	0.493	1.05	0.468	1.10	1.30	0.567	No
123	8.07	0.46	0.00	0.46	0.98	0.495	1.05	0.470	1.10	1.30	0.568	No
124	8.16	0.47	0.01	0.46	0.98	0.498	1.05	0.472	1.10	1.30	0.572	No
125	8.21	0.47	0.01	0.46	0.98	0.499	1.05	0.474	1.10	1.30	0.573	No
126	8.27	0.47	0.01	0.46	0.98	0.501	1.05	0.476	1.10	1.30	0.575	No
127	8.35	0.48	0.01	0.47	0.98	0.504	1.05	0.478	1.10	1.30	0.578	No
128	8.41	0.48	0.01	0.47	0.98	0.506	1.05	0.480	1.10	1.30	0.580	No
129	8.49	0.49	0.02	0.47	0.98	0.508	1.05	0.482	1.10	1.30	0.583	No
130	8.55	0.49	0.02	0.47	0.98	0.510	1.05	0.484	1.10	1.30	0.585	No
131	8.62	0.49	0.02	0.47	0.98	0.512	1.05	0.485	1.10	1.30	0.588	No
132	8.67	0.50	0.02	0.48	0.98	0.513	1.05	0.487	1.10	1.30	0.590	No
133	8.76	0.50	0.02	0.48	0.98	0.516	1.05	0.489	1.10	1.30	0.594	No
134	8.80	0.50	0.03	0.48	0.98	0.517	1.05	0.491	1.10	1.30	0.597	No
135	8.86	0.51	0.03	0.48	0.98	0.519	1.05	0.492	1.09	1.30	0.601	No
136	8.95	0.51	0.03	0.48	0.98	0.522	1.05	0.495	1.09	1.30	0.609	No
137	8.99	0.52	0.03	0.48	0.98	0.523	1.05	0.496	1.09	1.30	0.614	No
138	9.06	0.52	0.03	0.49	0.98	0.525	1.05	0.497	1.08	1.30	0.619	No
139	9.15	0.53	0.04	0.49	0.98	0.527	1.05	0.500	1.08	1.30	0.624	No
140	9.22	0.53	0.04	0.49	0.98	0.529	1.05	0.502	1.08	1.30	0.627	No
141	9.26	0.53	0.04	0.49	0.98	0.530	1.05	0.503	1.08	1.30	0.629	No
142	9.35	0.54	0.04	0.49	0.98	0.532	1.05	0.505	1.08	1.30	0.633	No
143	9.40	0.54	0.04	0.50	0.98	0.534	1.05	0.506	1.08	1.30	0.634	No
144	9.46	0.54	0.05	0.50	0.98	0.535	1.05	0.508	1.08	1.30	0.636	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
145	9.54	0.55	0.05	0.50	0.98	0.538	1.05	0.510	1.08	1.30	0.640	No
146	9.60	0.55	0.05	0.50	0.98	0.539	1.05	0.511	1.07	1.30	0.643	No
147	9.66	0.55	0.05	0.50	0.98	0.541	1.05	0.513	1.07	1.30	0.645	No
148	9.72	0.56	0.05	0.50	0.98	0.542	1.05	0.514	1.07	1.30	0.649	No
149	9.80	0.56	0.06	0.51	0.98	0.544	1.05	0.516	1.07	1.30	0.653	No
150	9.85	0.56	0.06	0.51	0.98	0.546	1.05	0.517	1.07	1.30	0.656	No
151	9.96	0.57	0.06	0.51	0.98	0.548	1.05	0.520	1.07	1.30	0.661	No
152	10.00	0.57	0.06	0.51	0.98	0.550	1.05	0.521	1.06	1.30	0.663	No
153	10.05	0.58	0.06	0.51	0.98	0.551	1.05	0.522	1.06	1.30	0.666	No
154	10.12	0.58	0.07	0.51	0.98	0.552	1.05	0.524	1.06	1.30	0.668	No
155	10.18	0.58	0.07	0.52	0.98	0.554	1.05	0.525	1.06	1.30	0.670	No
156	10.27	0.59	0.07	0.52	0.98	0.556	1.05	0.528	1.06	1.30	0.673	No
157	10.33	0.59	0.07	0.52	0.98	0.558	1.05	0.529	1.06	1.30	0.674	No
158	10.37	0.59	0.07	0.52	0.98	0.559	1.05	0.530	1.06	1.30	0.676	No
159	10.47	0.60	0.08	0.52	0.98	0.561	1.05	0.532	1.06	1.30	0.678	No
160	10.53	0.60	0.08	0.52	0.98	0.562	1.05	0.533	1.06	1.30	0.679	No
161	10.57	0.60	0.08	0.52	0.98	0.563	1.05	0.534	1.06	1.30	0.680	No
162	10.67	0.61	0.08	0.53	0.98	0.566	1.05	0.537	1.06	1.30	0.682	No
163	10.70	0.61	0.08	0.53	0.98	0.566	1.05	0.537	1.07	1.30	0.682	No
164	10.78	0.62	0.09	0.53	0.98	0.568	1.05	0.539	1.07	1.30	0.684	No
165	10.83	0.62	0.09	0.53	0.98	0.569	1.05	0.540	1.07	1.30	0.685	No
166	10.91	0.62	0.09	0.53	0.98	0.571	1.05	0.542	1.07	1.30	0.686	No
167	10.97	0.63	0.09	0.54	0.98	0.573	1.05	0.543	1.07	1.30	0.687	No
168	11.03	0.63	0.09	0.54	0.97	0.574	1.05	0.544	1.07	1.30	0.688	No
169	11.10	0.63	0.10	0.54	0.97	0.575	1.05	0.546	1.07	1.30	0.690	No
170	11.17	0.64	0.10	0.54	0.97	0.577	1.05	0.547	1.07	1.30	0.691	No
171	11.26	0.64	0.10	0.54	0.97	0.579	1.05	0.549	1.07	1.30	0.694	No
172	11.31	0.65	0.10	0.54	0.97	0.580	1.05	0.550	1.07	1.30	0.695	No
173	11.36	0.65	0.10	0.55	0.97	0.581	1.05	0.551	1.07	1.30	0.696	No
174	11.44	0.65	0.11	0.55	0.97	0.583	1.05	0.553	1.07	1.30	0.698	No
175	11.50	0.66	0.11	0.55	0.97	0.584	1.05	0.554	1.07	1.30	0.700	No
176	11.56	0.66	0.11	0.55	0.97	0.585	1.05	0.555	1.07	1.30	0.702	No
177	11.63	0.67	0.11	0.55	0.97	0.587	1.05	0.556	1.07	1.30	0.703	No
178	11.69	0.67	0.12	0.55	0.97	0.588	1.05	0.558	1.07	1.30	0.705	No
179	11.76	0.67	0.12	0.56	0.97	0.589	1.05	0.559	1.07	1.30	0.707	No
180	11.86	0.68	0.12	0.56	0.97	0.591	1.05	0.561	1.07	1.30	0.710	No
181	11.89	0.68	0.12	0.56	0.97	0.592	1.05	0.562	1.07	1.30	0.711	No
182	11.95	0.68	0.12	0.56	0.97	0.593	1.05	0.563	1.06	1.30	0.713	No
183	12.01	0.69	0.13	0.56	0.97	0.595	1.05	0.564	1.06	1.30	0.715	No
184	12.10	0.69	0.13	0.56	0.97	0.596	1.05	0.566	1.06	1.30	0.718	No
185	12.15	0.69	0.13	0.57	0.97	0.597	1.05	0.566	1.06	1.30	0.719	No
186	12.21	0.70	0.13	0.57	0.97	0.598	1.05	0.568	1.06	1.30	0.721	No
187	12.28	0.70	0.13	0.57	0.97	0.600	1.05	0.569	1.06	1.30	0.723	No
188	12.36	0.71	0.14	0.57	0.97	0.601	1.05	0.570	1.06	1.30	0.724	No
189	12.40	0.71	0.14	0.57	0.97	0.602	1.05	0.571	1.06	1.30	0.725	No
190	12.47	0.71	0.14	0.57	0.97	0.604	1.05	0.572	1.06	1.30	0.726	No
191	12.55	0.72	0.14	0.58	0.97	0.605	1.05	0.574	1.06	1.30	0.728	No
192	12.60	0.72	0.14	0.58	0.97	0.606	1.05	0.575	1.06	1.30	0.729	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
193	12.69	0.73	0.15	0.58	0.97	0.608	1.05	0.576	1.06	1.30	0.731	No
194	12.74	0.73	0.15	0.58	0.97	0.609	1.05	0.577	1.06	1.30	0.732	No
195	12.82	0.73	0.15	0.58	0.97	0.610	1.05	0.578	1.06	1.30	0.733	No
196	12.88	0.74	0.15	0.58	0.97	0.611	1.05	0.580	1.06	1.30	0.734	No
197	12.94	0.74	0.15	0.59	0.97	0.612	1.05	0.581	1.06	1.30	0.735	No
198	13.00	0.74	0.16	0.59	0.97	0.613	1.05	0.582	1.06	1.30	0.736	No
199	13.09	0.75	0.16	0.59	0.97	0.615	1.05	0.583	1.06	1.30	0.738	No
200	13.14	0.75	0.16	0.59	0.97	0.616	1.05	0.584	1.06	1.30	0.739	No
201	13.20	0.75	0.16	0.59	0.97	0.617	1.05	0.585	1.06	1.30	0.741	No
202	13.27	0.76	0.16	0.59	0.97	0.618	1.05	0.586	1.06	1.30	0.742	No
203	13.34	0.76	0.17	0.60	0.97	0.619	1.05	0.587	1.06	1.30	0.743	No
204	13.39	0.77	0.17	0.60	0.97	0.620	1.05	0.588	1.06	1.30	0.744	No
205	13.47	0.77	0.17	0.60	0.97	0.621	1.05	0.589	1.06	1.30	0.746	No
206	13.54	0.77	0.17	0.60	0.97	0.622	1.05	0.590	1.06	1.30	0.747	No
207	13.59	0.78	0.17	0.60	0.97	0.623	1.05	0.591	1.06	1.30	0.749	No
208	13.65	0.78	0.18	0.60	0.97	0.624	1.05	0.592	1.06	1.30	0.750	No
209	13.72	0.78	0.18	0.61	0.97	0.625	1.05	0.593	1.06	1.30	0.751	No
210	13.79	0.79	0.18	0.61	0.97	0.626	1.05	0.594	1.06	1.30	0.753	No
211	13.85	0.79	0.18	0.61	0.96	0.628	1.05	0.595	1.06	1.30	0.755	No
212	13.94	0.80	0.19	0.61	0.96	0.629	1.05	0.596	1.06	1.30	0.759	No
213	13.98	0.80	0.19	0.61	0.96	0.630	1.05	0.597	1.06	1.30	0.759	No
214	14.08	0.81	0.19	0.62	0.96	0.631	1.05	0.599	1.06	1.30	0.761	No
215	14.13	0.81	0.19	0.62	0.96	0.632	1.05	0.599	1.06	1.30	0.762	No
216	14.18	0.81	0.19	0.62	0.96	0.633	1.05	0.600	1.06	1.30	0.763	No
217	14.27	0.82	0.20	0.62	0.96	0.634	1.05	0.601	1.06	1.30	0.766	No
218	14.33	0.82	0.20	0.62	0.96	0.635	1.05	0.602	1.06	1.30	0.768	No
219	14.39	0.82	0.20	0.62	0.96	0.636	1.05	0.603	1.06	1.30	0.769	No
220	14.44	0.83	0.20	0.62	0.96	0.637	1.05	0.604	1.06	1.30	0.771	No
221	14.53	0.83	0.20	0.63	0.96	0.638	1.05	0.605	1.05	1.30	0.775	No
222	14.59	0.83	0.21	0.63	0.96	0.639	1.05	0.606	1.05	1.30	0.777	No
223	14.64	0.84	0.21	0.63	0.96	0.640	1.05	0.607	1.05	1.30	0.779	No
224	14.73	0.84	0.21	0.63	0.96	0.641	1.05	0.608	1.05	1.30	0.783	No
225	14.77	0.84	0.21	0.63	0.96	0.642	1.05	0.609	1.05	1.30	0.784	No
226	14.83	0.85	0.21	0.63	0.96	0.642	1.05	0.609	1.05	1.30	0.788	No
227	14.93	0.85	0.22	0.64	0.96	0.644	1.05	0.611	1.05	1.30	0.792	No
228	14.98	0.86	0.22	0.64	0.96	0.645	1.05	0.611	1.04	1.30	0.793	No
229	15.03	0.86	0.22	0.64	0.96	0.645	1.05	0.612	1.04	1.30	0.795	No
230	15.10	0.86	0.22	0.64	0.96	0.646	1.05	0.613	1.04	1.30	0.797	No
231	15.17	0.87	0.22	0.64	0.96	0.647	1.05	0.614	1.04	1.30	0.799	No
232	15.22	0.87	0.23	0.64	0.96	0.648	1.05	0.615	1.04	1.30	0.800	No
233	15.29	0.87	0.23	0.65	0.96	0.649	1.05	0.616	1.04	1.30	0.802	No
234	15.37	0.88	0.23	0.65	0.96	0.650	1.05	0.617	1.04	1.30	0.804	No
235	15.44	0.88	0.23	0.65	0.96	0.651	1.05	0.618	1.04	1.30	0.805	No
236	15.52	0.89	0.23	0.65	0.96	0.652	1.05	0.619	1.04	1.30	0.807	No
237	15.56	0.89	0.24	0.65	0.96	0.653	1.05	0.619	1.04	1.30	0.807	No
238	15.62	0.89	0.24	0.65	0.96	0.654	1.05	0.620	1.04	1.30	0.808	No
239	15.70	0.90	0.24	0.66	0.96	0.655	1.05	0.621	1.04	1.30	0.810	No
240	15.76	0.90	0.24	0.66	0.96	0.656	1.05	0.622	1.04	1.30	0.811	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	15.82	0.90	0.24	0.66	0.96	0.656	1.05	0.622	1.04	1.30	0.812	No
242	15.91	0.91	0.25	0.66	0.96	0.658	1.05	0.624	1.04	1.30	0.814	No
243	15.95	0.91	0.25	0.66	0.96	0.658	1.05	0.624	1.04	1.30	0.814	No
244	16.01	0.91	0.25	0.66	0.96	0.659	1.05	0.625	1.04	1.30	0.816	No
245	16.08	0.92	0.25	0.67	0.96	0.660	1.05	0.626	1.04	1.30	0.817	No
246	16.14	0.92	0.25	0.67	0.96	0.661	1.05	0.626	1.04	1.30	0.818	No
247	16.22	0.93	0.26	0.67	0.96	0.662	1.05	0.627	1.04	1.30	0.819	No
248	16.31	0.93	0.26	0.67	0.96	0.663	1.05	0.628	1.04	1.30	0.820	No
249	16.36	0.93	0.26	0.67	0.96	0.663	1.05	0.629	1.04	1.30	0.821	No
250	16.41	0.94	0.26	0.67	0.96	0.664	1.05	0.630	1.04	1.30	0.821	No
251	16.50	0.94	0.27	0.68	0.95	0.665	1.05	0.631	1.04	1.30	0.822	No
252	16.55	0.95	0.27	0.68	0.95	0.666	1.05	0.631	1.04	1.30	0.822	No
253	16.61	0.95	0.27	0.68	0.95	0.666	1.05	0.632	1.04	1.30	0.823	No
254	16.69	0.95	0.27	0.68	0.95	0.667	1.05	0.633	1.04	1.30	0.823	No
255	16.74	0.96	0.27	0.68	0.95	0.668	1.05	0.633	1.04	1.30	0.823	No
256	16.80	0.96	0.27	0.69	0.95	0.669	1.05	0.634	1.04	1.30	0.824	No
257	16.88	0.96	0.28	0.69	0.95	0.669	1.05	0.635	1.04	1.30	0.824	No
258	16.95	0.97	0.28	0.69	0.95	0.670	1.05	0.636	1.04	1.30	0.824	No
259	17.00	0.97	0.28	0.69	0.95	0.671	1.05	0.636	1.04	1.30	0.824	No
260	17.07	0.98	0.28	0.69	0.95	0.672	1.05	0.637	1.04	1.30	0.825	No
261	17.15	0.98	0.29	0.69	0.95	0.673	1.05	0.638	1.04	1.30	0.826	No
262	17.20	0.98	0.29	0.70	0.95	0.673	1.05	0.638	1.04	1.30	0.826	No
263	17.26	0.99	0.29	0.70	0.95	0.674	1.05	0.639	1.04	1.30	0.827	No
264	17.33	0.99	0.29	0.70	0.95	0.674	1.05	0.640	1.04	1.30	0.828	No
265	17.41	0.99	0.29	0.70	0.95	0.675	1.05	0.640	1.04	1.30	0.829	No
266	17.46	1.00	0.30	0.70	0.95	0.676	1.05	0.641	1.04	1.30	0.830	No
267	17.52	1.00	0.30	0.70	0.95	0.677	1.05	0.642	1.04	1.30	0.831	No
268	17.60	1.01	0.30	0.71	0.95	0.677	1.05	0.642	1.04	1.30	0.833	No
269	17.65	1.01	0.30	0.71	0.95	0.678	1.05	0.643	1.04	1.30	0.833	No
270	17.74	1.01	0.30	0.71	0.95	0.679	1.05	0.644	1.04	1.30	0.834	No
271	17.80	1.02	0.31	0.71	0.95	0.679	1.05	0.644	1.04	1.30	0.835	No
272	17.85	1.02	0.31	0.71	0.95	0.680	1.05	0.645	1.04	1.30	0.836	No
273	17.93	1.03	0.31	0.72	0.95	0.681	1.05	0.646	1.04	1.30	0.836	No
274	17.99	1.03	0.31	0.72	0.95	0.681	1.05	0.646	1.04	1.30	0.837	No
275	18.07	1.03	0.31	0.72	0.95	0.682	1.05	0.647	1.04	1.30	0.837	No
276	18.13	1.04	0.32	0.72	0.95	0.683	1.05	0.647	1.04	1.30	0.837	No
277	18.18	1.04	0.32	0.72	0.95	0.683	1.05	0.648	1.04	1.30	0.837	No
278	18.29	1.05	0.32	0.73	0.95	0.684	1.05	0.649	1.04	1.30	0.838	No
279	18.32	1.05	0.32	0.73	0.95	0.685	1.05	0.649	1.04	1.30	0.838	No
280	18.38	1.05	0.32	0.73	0.95	0.685	1.05	0.650	1.04	1.30	0.838	No
281	18.44	1.06	0.33	0.73	0.95	0.686	1.05	0.650	1.04	1.30	0.839	No
282	18.53	1.06	0.33	0.73	0.95	0.686	1.05	0.651	1.04	1.30	0.839	No
283	18.58	1.06	0.33	0.73	0.95	0.687	1.05	0.651	1.04	1.30	0.840	No
284	18.66	1.07	0.33	0.74	0.95	0.687	1.05	0.652	1.04	1.30	0.842	No
285	18.71	1.07	0.33	0.74	0.95	0.688	1.05	0.652	1.04	1.30	0.841	No
286	18.81	1.08	0.34	0.74	0.95	0.689	1.05	0.653	1.04	1.30	0.841	No
287	18.85	1.08	0.34	0.74	0.95	0.689	1.05	0.654	1.04	1.30	0.841	No
288	18.90	1.08	0.34	0.74	0.95	0.690	1.05	0.654	1.04	1.30	0.841	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	19.01	1.09	0.34	0.75	0.94	0.690	1.05	0.655	1.04	1.30	0.842	No
290	19.06	1.09	0.35	0.75	0.94	0.691	1.05	0.655	1.04	1.30	0.843	No
291	19.11	1.10	0.35	0.75	0.94	0.691	1.05	0.656	1.04	1.30	0.844	No
292	19.16	1.10	0.35	0.75	0.94	0.692	1.05	0.656	1.04	1.30	0.845	No
293	19.26	1.10	0.35	0.75	0.94	0.693	1.05	0.657	1.04	1.30	0.847	No
294	19.30	1.11	0.35	0.75	0.94	0.693	1.05	0.657	1.04	1.30	0.847	No
295	19.36	1.11	0.35	0.76	0.94	0.693	1.05	0.658	1.04	1.30	0.849	No
296	19.45	1.12	0.36	0.76	0.94	0.694	1.05	0.658	1.04	1.30	0.850	No
297	19.50	1.12	0.36	0.76	0.94	0.695	1.05	0.659	1.04	1.30	0.852	No
298	19.58	1.12	0.36	0.76	0.94	0.695	1.05	0.659	1.04	1.30	0.854	No
299	19.64	1.13	0.36	0.76	0.94	0.696	1.05	0.660	1.04	1.30	0.855	No
300	19.69	1.13	0.36	0.77	0.94	0.696	1.05	0.660	1.04	1.30	0.857	No
301	19.78	1.14	0.37	0.77	0.94	0.697	1.05	0.661	1.04	1.30	0.859	No
302	19.84	1.14	0.37	0.77	0.94	0.697	1.05	0.661	1.03	1.30	0.859	No
303	19.90	1.14	0.37	0.77	0.94	0.698	1.05	0.662	1.03	1.30	0.861	No
304	19.95	1.15	0.37	0.77	0.94	0.698	1.05	0.662	1.03	1.30	0.862	No
305	20.03	1.15	0.38	0.77	0.94	0.699	1.05	0.663	1.03	1.30	0.863	No
306	20.08	1.15	0.38	0.78	0.94	0.699	1.05	0.663	1.03	1.30	0.865	No
307	20.16	1.16	0.38	0.78	0.94	0.700	1.05	0.664	1.03	1.30	0.866	No
308	20.25	1.16	0.38	0.78	0.94	0.700	1.05	0.664	1.03	1.30	0.868	No
309	20.30	1.17	0.38	0.78	0.94	0.701	1.05	0.664	1.03	1.30	0.869	No
310	20.35	1.17	0.39	0.78	0.94	0.701	1.05	0.665	1.03	1.30	0.869	No
311	20.45	1.18	0.39	0.79	0.94	0.702	1.05	0.665	1.03	1.30	0.869	No
312	20.50	1.18	0.39	0.79	0.94	0.702	1.05	0.666	1.03	1.30	0.869	No
313	20.54	1.18	0.39	0.79	0.94	0.702	1.05	0.666	1.03	1.30	0.870	No
314	20.62	1.19	0.39	0.79	0.94	0.703	1.05	0.667	1.03	1.30	0.869	No
315	20.69	1.19	0.40	0.79	0.94	0.703	1.05	0.667	1.03	1.30	0.870	No
316	20.74	1.19	0.40	0.80	0.94	0.704	1.05	0.667	1.03	1.30	0.870	No
317	20.83	1.20	0.40	0.80	0.94	0.704	1.05	0.668	1.03	1.30	0.871	No
318	20.88	1.20	0.40	0.80	0.94	0.704	1.05	0.668	1.03	1.30	0.871	No
319	20.94	1.21	0.40	0.80	0.94	0.705	1.05	0.668	1.03	1.30	0.871	No
320	21.04	1.21	0.41	0.80	0.94	0.705	1.05	0.669	1.03	1.30	0.873	No
321	21.08	1.21	0.41	0.81	0.94	0.706	1.05	0.669	1.03	1.30	0.873	No
322	21.14	1.22	0.41	0.81	0.94	0.706	1.05	0.670	1.03	1.30	0.874	No
323	21.23	1.22	0.41	0.81	0.94	0.707	1.05	0.670	1.03	1.30	0.875	No
324	21.28	1.23	0.41	0.81	0.94	0.707	1.05	0.671	1.03	1.30	0.876	No
325	21.33	1.23	0.42	0.81	0.93	0.707	1.05	0.671	1.03	1.30	0.876	No
326	21.42	1.23	0.42	0.82	0.93	0.708	1.05	0.671	1.03	1.30	0.877	No
327	21.48	1.24	0.42	0.82	0.93	0.708	1.05	0.672	1.03	1.30	0.878	No
328	21.53	1.24	0.42	0.82	0.93	0.709	1.05	0.672	1.03	1.30	0.878	No
329	21.62	1.25	0.43	0.82	0.93	0.709	1.05	0.672	1.03	1.30	0.878	No
330	21.68	1.25	0.43	0.82	0.93	0.709	1.05	0.673	1.03	1.30	0.879	No
331	21.73	1.25	0.43	0.82	0.93	0.710	1.05	0.673	1.03	1.30	0.878	No
332	21.79	1.26	0.43	0.83	0.93	0.710	1.05	0.673	1.03	1.30	0.877	No
333	21.86	1.26	0.43	0.83	0.93	0.710	1.05	0.674	1.03	1.30	0.876	No
334	21.92	1.26	0.43	0.83	0.93	0.711	1.05	0.674	1.03	1.30	0.875	No
335	22.00	1.27	0.44	0.83	0.93	0.711	1.05	0.674	1.03	1.30	0.874	No
336	22.05	1.27	0.44	0.83	0.93	0.711	1.05	0.675	1.03	1.30	0.872	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	22.12	1.28	0.44	0.84	0.93	0.712	1.05	0.675	1.03	1.30	0.872	No
338	22.22	1.28	0.44	0.84	0.93	0.712	1.05	0.675	1.03	1.30	0.869	No
339	22.27	1.29	0.45	0.84	0.93	0.712	1.05	0.676	1.03	1.30	0.869	No
340	22.32	1.29	0.45	0.84	0.93	0.713	1.05	0.676	1.03	1.30	0.867	No
341	22.38	1.29	0.45	0.85	0.93	0.713	1.05	0.676	1.03	1.30	0.865	No
342	22.47	1.30	0.45	0.85	0.93	0.713	1.05	0.677	1.03	1.30	0.863	No
343	22.52	1.30	0.45	0.85	0.93	0.714	1.05	0.677	1.03	1.30	0.862	No
344	22.59	1.31	0.46	0.85	0.93	0.714	1.05	0.677	1.03	1.30	0.860	No
345	22.65	1.31	0.46	0.85	0.93	0.714	1.05	0.677	1.03	1.30	0.860	No
346	22.71	1.31	0.46	0.86	0.93	0.714	1.05	0.678	1.03	1.30	0.860	No
347	22.77	1.32	0.46	0.86	0.93	0.715	1.05	0.678	1.03	1.30	0.862	No
348	22.85	1.32	0.46	0.86	0.93	0.715	1.05	0.678	1.03	1.30	0.865	No
349	22.90	1.33	0.47	0.86	0.93	0.715	1.05	0.678	1.03	1.30	0.867	No
350	22.98	1.33	0.47	0.86	0.93	0.716	1.05	0.679	1.03	1.30	0.870	No
351	23.06	1.34	0.47	0.87	0.93	0.716	1.05	0.679	1.03	1.30	0.870	No
352	23.10	1.34	0.47	0.87	0.93	0.716	1.05	0.679	1.03	1.30	0.870	No
353	23.17	1.34	0.47	0.87	0.93	0.716	1.05	0.679	1.03	1.30	0.870	No
354	23.24	1.35	0.48	0.87	0.93	0.717	1.05	0.680	1.03	1.30	0.870	No
355	23.32	1.35	0.48	0.87	0.93	0.717	1.05	0.680	1.03	1.30	0.870	No
356	23.37	1.36	0.48	0.88	0.93	0.717	1.05	0.680	1.03	1.30	0.871	No
357	23.45	1.36	0.48	0.88	0.93	0.717	1.05	0.680	1.03	1.30	0.870	No
358	23.51	1.37	0.48	0.88	0.93	0.718	1.05	0.681	1.03	1.30	0.871	No
359	23.56	1.37	0.49	0.88	0.93	0.718	1.05	0.681	1.03	1.30	0.871	No
360	23.63	1.37	0.49	0.89	0.92	0.718	1.05	0.681	1.03	1.30	0.869	No
361	23.71	1.38	0.49	0.89	0.92	0.718	1.05	0.681	1.03	1.30	0.867	No
362	23.77	1.38	0.49	0.89	0.92	0.718	1.05	0.681	1.03	1.30	0.863	No
363	23.84	1.39	0.49	0.89	0.92	0.719	1.05	0.682	1.03	1.30	0.861	No
364	23.89	1.39	0.50	0.89	0.92	0.719	1.05	0.682	1.03	1.30	0.859	No
365	23.95	1.39	0.50	0.90	0.92	0.719	1.05	0.682	1.03	1.30	0.858	No
366	24.05	1.40	0.50	0.90	0.92	0.719	1.05	0.682	1.03	1.30	0.860	No
367	24.09	1.40	0.50	0.90	0.92	0.720	1.05	0.682	1.03	1.30	0.861	No
368	24.15	1.41	0.50	0.90	0.92	0.720	1.05	0.683	1.03	1.30	0.863	No
369	24.24	1.41	0.51	0.91	0.92	0.720	1.05	0.683	1.03	1.30	0.866	No
370	24.30	1.42	0.51	0.91	0.92	0.720	1.05	0.683	1.03	1.30	0.869	No
371	24.37	1.42	0.51	0.91	0.92	0.720	1.05	0.683	1.02	1.30	0.872	No
372	24.42	1.42	0.51	0.91	0.92	0.721	1.05	0.683	1.02	1.30	0.874	No
373	24.48	1.43	0.51	0.91	0.92	0.721	1.05	0.684	1.02	1.30	0.876	No
374	24.54	1.43	0.52	0.91	0.92	0.721	1.05	0.684	1.02	1.30	0.877	No
375	24.61	1.44	0.52	0.92	0.92	0.721	1.05	0.684	1.02	1.30	0.880	No
376	24.71	1.44	0.52	0.92	0.92	0.721	1.05	0.684	1.02	1.30	0.886	No
377	24.76	1.44	0.52	0.92	0.92	0.722	1.05	0.684	1.02	1.30	0.890	No
378	24.81	1.45	0.52	0.92	0.92	0.722	1.05	0.685	1.02	1.30	0.895	No
379	24.90	1.45	0.53	0.93	0.92	0.722	1.05	0.685	1.02	1.30	0.901	No
380	24.96	1.46	0.53	0.93	0.92	0.722	1.05	0.685	1.02	1.30	0.904	No
381	25.00	1.46	0.53	0.93	0.92	0.723	1.05	0.685	1.01	1.30	0.908	No
382	25.09	1.46	0.53	0.93	0.92	0.723	1.05	0.686	1.01	1.30	0.911	No
383	25.16	1.47	0.54	0.93	0.92	0.723	1.05	0.686	1.01	1.30	0.913	No
384	25.20	1.47	0.54	0.93	0.92	0.723	1.05	0.686	1.01	1.30	0.915	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	25.30	1.48	0.54	0.94	0.92	0.724	1.05	0.686	1.01	1.30	0.917	No
386	25.36	1.48	0.54	0.94	0.92	0.724	1.05	0.686	1.01	1.30	0.918	No
387	25.40	1.48	0.54	0.94	0.92	0.724	1.05	0.687	1.01	1.30	0.919	No
388	25.48	1.49	0.55	0.94	0.92	0.724	1.05	0.687	1.01	1.30	0.919	No
389	25.53	1.49	0.55	0.94	0.92	0.724	1.05	0.687	1.01	1.30	0.919	No
390	25.59	1.50	0.55	0.95	0.92	0.725	1.05	0.687	1.01	1.30	0.918	No
391	25.67	1.50	0.55	0.95	0.92	0.725	1.05	0.687	1.01	1.30	0.918	No
392	25.75	1.50	0.55	0.95	0.92	0.725	1.05	0.688	1.01	1.30	0.919	No
393	25.80	1.51	0.56	0.95	0.92	0.725	1.05	0.688	1.01	1.30	0.920	No
394	25.87	1.51	0.56	0.95	0.92	0.725	1.05	0.688	1.01	1.30	0.920	No
395	25.95	1.52	0.56	0.96	0.91	0.726	1.05	0.688	1.01	1.30	0.920	No
396	25.99	1.52	0.56	0.96	0.91	0.726	1.05	0.688	1.01	1.30	0.920	No
397	26.09	1.53	0.56	0.96	0.91	0.726	1.05	0.689	1.01	1.30	0.915	No
398	26.14	1.53	0.57	0.96	0.91	0.726	1.05	0.689	1.01	1.30	0.912	No
399	26.19	1.53	0.57	0.96	0.91	0.726	1.05	0.689	1.01	1.30	0.910	No
400	26.27	1.54	0.57	0.97	0.91	0.727	1.05	0.689	1.01	1.30	0.904	No
401	26.33	1.54	0.57	0.97	0.91	0.727	1.05	0.689	1.01	1.30	0.902	No
402	26.39	1.54	0.57	0.97	0.91	0.727	1.05	0.689	1.01	1.30	0.899	No
403	26.45	1.55	0.58	0.97	0.91	0.727	1.05	0.689	1.01	1.30	0.896	No
404	26.53	1.55	0.58	0.98	0.91	0.727	1.05	0.690	1.01	1.30	0.894	No
405	26.59	1.56	0.58	0.98	0.91	0.727	1.05	0.690	1.01	1.30	0.894	No
406	26.64	1.56	0.58	0.98	0.91	0.727	1.05	0.690	1.01	1.30	0.898	No
407	26.73	1.57	0.58	0.98	0.91	0.727	1.05	0.690	1.01	1.30	0.903	No
408	26.79	1.57	0.59	0.98	0.91	0.728	1.05	0.690	1.01	1.30	0.906	No
409	26.86	1.57	0.59	0.99	0.91	0.728	1.05	0.690	1.01	1.30	0.911	No
410	26.93	1.58	0.59	0.99	0.91	0.728	1.05	0.690	1.01	1.30	0.915	No
411	26.99	1.58	0.59	0.99	0.91	0.728	1.05	0.690	1.01	1.30	0.918	No
412	27.08	1.59	0.60	0.99	0.91	0.728	1.05	0.691	1.01	1.30	0.922	No
413	27.13	1.59	0.60	0.99	0.91	0.728	1.05	0.691	1.01	1.30	0.924	No
414	27.17	1.59	0.60	1.00	0.91	0.728	1.05	0.691	1.01	1.30	0.925	No
415	27.25	1.60	0.60	1.00	0.91	0.729	1.05	0.691	1.01	1.30	0.927	No
416	27.32	1.60	0.60	1.00	0.91	0.729	1.05	0.691	1.01	1.30	0.928	No
417	27.38	1.61	0.60	1.00	0.91	0.729	1.05	0.691	1.01	1.30	0.930	No
418	27.44	1.61	0.61	1.00	0.91	0.729	1.05	0.691	1.00	1.30	0.931	No
419	27.53	1.62	0.61	1.01	0.91	0.729	1.05	0.692	1.00	1.30	0.932	No
420	27.58	1.62	0.61	1.01	0.91	0.729	1.05	0.692	1.00	1.30	0.932	No
421	27.63	1.62	0.61	1.01	0.91	0.729	1.05	0.692	1.00	1.30	0.933	No
422	27.71	1.63	0.61	1.01	0.91	0.730	1.05	0.692	1.00	1.30	0.933	No
423	27.77	1.63	0.62	1.01	0.91	0.730	1.05	0.692	1.00	1.30	0.933	No
424	27.82	1.63	0.62	1.01	0.91	0.730	1.05	0.692	1.00	1.30	0.934	No
425	27.90	1.64	0.62	1.02	0.91	0.730	1.05	0.692	1.00	1.30	0.929	No
426	27.97	1.64	0.62	1.02	0.91	0.730	1.05	0.693	1.00	1.30	0.926	No
427	28.02	1.65	0.62	1.02	0.91	0.730	1.05	0.693	1.00	1.30	0.922	No
428	28.12	1.65	0.63	1.02	0.90	0.730	1.05	0.693	1.00	1.30	0.913	No
429	28.17	1.65	0.63	1.03	0.90	0.731	1.05	0.693	1.00	1.30	0.909	No
430	28.23	1.66	0.63	1.03	0.90	0.731	1.05	0.693	1.00	1.30	0.908	No
431	28.31	1.66	0.63	1.03	0.90	0.731	1.05	0.693	1.00	1.30	0.908	No
432	28.37	1.67	0.64	1.03	0.90	0.731	1.05	0.693	1.00	1.30	0.910	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	28.42	1.67	0.64	1.03	0.90	0.731	1.05	0.693	1.00	1.30	0.912	No
434	28.51	1.68	0.64	1.04	0.90	0.731	1.05	0.693	1.00	1.30	0.916	No
435	28.55	1.68	0.64	1.04	0.90	0.731	1.05	0.693	1.00	1.30	0.919	No
436	28.61	1.68	0.64	1.04	0.90	0.731	1.05	0.693	1.00	1.30	0.923	No
437	28.71	1.69	0.65	1.04	0.90	0.731	1.05	0.694	1.00	1.30	0.927	No
438	28.76	1.69	0.65	1.04	0.90	0.731	1.05	0.694	1.00	1.30	0.931	No
439	28.81	1.69	0.65	1.05	0.90	0.731	1.05	0.694	1.00	1.30	0.933	No
440	28.91	1.70	0.65	1.05	0.90	0.732	1.05	0.694	1.00	1.30	0.937	No
441	28.95	1.70	0.65	1.05	0.90	0.732	1.05	0.694	1.00	1.30	0.937	No
442	29.00	1.71	0.66	1.05	0.90	0.732	1.05	0.694	1.00	1.30	0.938	No
443	29.07	1.71	0.66	1.05	0.90	0.732	1.05	0.694	1.00	1.30	0.938	No
444	29.16	1.72	0.66	1.06	0.90	0.732	1.05	0.694	1.00	1.30	0.938	No
445	29.21	1.72	0.66	1.06	0.90	0.732	1.05	0.694	1.00	1.30	0.937	No
446	29.30	1.72	0.66	1.06	0.90	0.732	1.05	0.694	1.00	1.30	0.936	No
447	29.36	1.73	0.67	1.06	0.90	0.732	1.05	0.695	1.00	1.30	0.936	No
448	29.41	1.73	0.67	1.06	0.90	0.732	1.05	0.695	1.00	1.30	0.934	No
449	29.50	1.74	0.67	1.07	0.90	0.732	1.05	0.695	1.00	1.30	0.931	No
450	29.56	1.74	0.67	1.07	0.90	0.733	1.05	0.695	1.00	1.30	0.929	No
451	29.61	1.74	0.67	1.07	0.90	0.733	1.05	0.695	1.00	1.30	0.928	No
452	29.69	1.75	0.68	1.07	0.90	0.733	1.05	0.695	1.00	1.30	0.928	No
453	29.76	1.75	0.68	1.07	0.90	0.733	1.05	0.695	1.00	1.30	0.929	No
454	29.80	1.76	0.68	1.08	0.90	0.733	1.05	0.695	1.00	1.30	0.931	No
455	29.89	1.76	0.68	1.08	0.90	0.733	1.05	0.695	1.00	1.30	0.935	No
456	29.93	1.76	0.68	1.08	0.90	0.733	1.05	0.695	1.00	1.30	0.938	No
457	30.00	1.77	0.69	1.08	0.90	0.733	1.05	0.695	1.00	1.30	0.940	No
458	30.06	1.77	0.69	1.08	0.90	0.733	1.05	0.695	1.00	1.30	0.943	No
459	30.13	1.78	0.69	1.08	0.90	0.733	1.05	0.695	1.00	1.30	0.943	No
460	30.21	1.78	0.69	1.09	0.89	0.733	1.05	0.696	1.00	1.30	0.944	No
461	30.27	1.78	0.69	1.09	0.89	0.733	1.05	0.696	1.00	1.30	0.945	No
462	30.36	1.79	0.70	1.09	0.89	0.734	1.05	0.696	1.00	1.30	0.946	No
463	30.41	1.79	0.70	1.09	0.89	0.734	1.05	0.696	1.00	1.30	0.946	No
464	30.46	1.79	0.70	1.09	0.89	0.734	1.05	0.696	1.00	1.30	0.946	No
465	30.55	1.80	0.70	1.10	0.89	0.734	1.05	0.696	1.00	1.30	0.947	No
466	30.60	1.80	0.71	1.10	0.89	0.734	1.05	0.696	1.00	1.30	0.947	No
467	30.65	1.81	0.71	1.10	0.89	0.734	1.05	0.696	1.00	1.30	0.947	No
468	30.73	1.81	0.71	1.10	0.89	0.734	1.05	0.696	1.00	1.30	0.948	No
469	30.80	1.81	0.71	1.10	0.89	0.735	1.05	0.697	1.00	1.30	0.948	No
470	30.85	1.82	0.71	1.10	0.89	0.735	1.05	0.697	1.00	1.30	0.948	No
471	30.95	1.82	0.72	1.11	0.89	0.735	1.05	0.697	1.00	1.30	0.949	No
472	30.99	1.82	0.72	1.11	0.89	0.735	1.05	0.697	1.00	1.30	0.949	No
473	31.05	1.83	0.72	1.11	0.89	0.735	1.05	0.697	1.00	1.30	0.949	No
474	31.15	1.83	0.72	1.11	0.89	0.735	1.05	0.697	1.00	1.30	0.950	No
475	31.18	1.84	0.72	1.11	0.89	0.735	1.05	0.697	1.00	1.30	0.950	No
476	31.23	1.84	0.72	1.11	0.89	0.735	1.05	0.697	1.00	1.30	0.950	No
477	31.30	1.84	0.73	1.12	0.89	0.735	1.05	0.697	1.00	1.30	0.950	No
478	31.39	1.85	0.73	1.12	0.89	0.736	1.05	0.698	1.00	1.30	0.951	No
479	31.45	1.85	0.73	1.12	0.89	0.736	1.05	0.698	1.00	1.30	0.951	No
480	31.50	1.85	0.73	1.12	0.89	0.736	1.05	0.698	1.00	1.30	0.951	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	31.58	1.86	0.74	1.12	0.89	0.736	1.05	0.698	0.99	1.30	0.952	No
482	31.64	1.86	0.74	1.12	0.89	0.736	1.05	0.698	0.99	1.30	0.952	No
483	31.70	1.87	0.74	1.13	0.89	0.736	1.05	0.698	0.99	1.30	0.952	No
484	31.78	1.87	0.74	1.13	0.89	0.736	1.05	0.698	0.99	1.30	0.952	No
485	31.84	1.87	0.74	1.13	0.89	0.736	1.05	0.698	0.99	1.30	0.953	No
486	31.90	1.88	0.75	1.13	0.89	0.736	1.05	0.698	0.99	1.30	0.953	No
487	31.96	1.88	0.75	1.13	0.89	0.736	1.05	0.698	0.99	1.30	0.953	No
488	32.03	1.89	0.75	1.14	0.89	0.736	1.05	0.698	0.99	1.30	0.953	No
489	32.09	1.89	0.75	1.14	0.89	0.737	1.05	0.699	0.99	1.30	0.953	No
490	32.19	1.89	0.75	1.14	0.89	0.737	1.05	0.699	0.99	1.30	0.954	No
491	32.24	1.90	0.76	1.14	0.89	0.737	1.05	0.699	0.99	1.30	0.954	No
492	32.32	1.90	0.76	1.14	0.88	0.737	1.05	0.699	0.99	1.30	0.954	No
493	32.39	1.91	0.76	1.15	0.88	0.737	1.05	0.699	0.99	1.30	0.955	No
494	32.43	1.91	0.76	1.15	0.88	0.737	1.05	0.699	0.99	1.30	0.955	No
495	32.48	1.91	0.76	1.15	0.88	0.737	1.05	0.699	0.99	1.30	0.955	No
496	32.55	1.92	0.77	1.15	0.88	0.737	1.05	0.699	0.99	1.30	0.955	No
497	32.62	1.92	0.77	1.15	0.88	0.737	1.05	0.699	0.99	1.30	0.955	No
498	32.69	1.92	0.77	1.15	0.88	0.737	1.05	0.699	0.99	1.30	0.956	No
499	32.78	1.93	0.77	1.16	0.88	0.737	1.05	0.699	0.99	1.30	0.956	No
500	32.82	1.93	0.77	1.16	0.88	0.737	1.05	0.699	0.99	1.30	0.956	No
501	32.88	1.93	0.78	1.16	0.88	0.738	1.05	0.699	0.99	1.30	0.956	No
502	32.97	1.94	0.78	1.16	0.88	0.738	1.05	0.700	0.99	1.30	0.957	No
503	33.02	1.94	0.78	1.16	0.88	0.738	1.05	0.700	0.99	1.30	0.957	No
504	33.08	1.95	0.78	1.16	0.88	0.738	1.05	0.700	0.99	1.30	0.957	No
505	33.17	1.95	0.79	1.17	0.88	0.738	1.05	0.700	0.99	1.30	0.957	No
506	33.21	1.95	0.79	1.17	0.88	0.738	1.05	0.700	0.99	1.30	0.957	No
507	33.29	1.96	0.79	1.17	0.88	0.738	1.05	0.700	0.99	1.30	0.957	No
508	33.37	1.96	0.79	1.17	0.88	0.738	1.05	0.700	0.99	1.30	0.957	No
509	33.41	1.97	0.79	1.17	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
510	33.47	1.97	0.79	1.17	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
511	33.56	1.97	0.80	1.18	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
512	33.61	1.98	0.80	1.18	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
513	33.68	1.98	0.80	1.18	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
514	33.77	1.99	0.80	1.18	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
515	33.82	1.99	0.81	1.18	0.88	0.738	1.05	0.700	0.99	1.30	0.959	No
516	33.87	1.99	0.81	1.18	0.88	0.738	1.05	0.700	0.99	1.30	0.959	No
517	33.97	2.00	0.81	1.19	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
518	34.01	2.00	0.81	1.19	0.88	0.738	1.05	0.700	0.99	1.30	0.958	No
519	34.08	2.00	0.81	1.19	0.88	0.738	1.05	0.700	0.99	1.30	0.959	No
520	34.13	2.01	0.82	1.19	0.88	0.738	1.05	0.700	0.99	1.30	0.959	No
521	34.19	2.01	0.82	1.19	0.88	0.738	1.05	0.700	0.99	1.30	0.959	No
522	34.27	2.02	0.82	1.20	0.88	0.738	1.05	0.700	0.99	1.30	0.960	No
523	34.36	2.02	0.82	1.20	0.88	0.738	1.05	0.700	0.99	1.30	0.960	No
524	34.41	2.02	0.82	1.20	0.87	0.738	1.05	0.700	0.99	1.30	0.960	No
525	34.46	2.03	0.83	1.20	0.87	0.738	1.05	0.700	0.99	1.30	0.961	No
526	34.54	2.03	0.83	1.20	0.87	0.739	1.05	0.700	0.99	1.30	0.961	No
527	34.60	2.04	0.83	1.21	0.87	0.739	1.05	0.700	0.99	1.30	0.961	No
528	34.65	2.04	0.83	1.21	0.87	0.739	1.05	0.700	0.99	1.30	0.961	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
529	34.73	2.04	0.83	1.21	0.87	0.739	1.05	0.700	0.99	1.30	0.961	No
530	34.80	2.05	0.84	1.21	0.87	0.739	1.05	0.701	0.99	1.30	0.962	No
531	34.85	2.05	0.84	1.21	0.87	0.739	1.05	0.701	0.99	1.30	0.962	No
532	34.92	2.05	0.84	1.21	0.87	0.739	1.05	0.701	0.99	1.30	0.962	No
533	34.98	2.06	0.84	1.22	0.87	0.739	1.05	0.701	0.99	1.30	0.962	No
534	35.04	2.06	0.84	1.22	0.87	0.739	1.05	0.701	0.99	1.30	0.962	No
535	35.12	2.07	0.85	1.22	0.87	0.739	1.05	0.701	0.99	1.30	0.962	No
536	35.17	2.07	0.85	1.22	0.87	0.739	1.05	0.701	0.99	1.30	0.962	No
537	35.25	2.07	0.85	1.22	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
538	35.32	2.08	0.85	1.22	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
539	35.37	2.08	0.85	1.23	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
540	35.44	2.08	0.86	1.23	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
541	35.50	2.09	0.86	1.23	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
542	35.60	2.09	0.86	1.23	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
543	35.65	2.10	0.86	1.23	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
544	35.70	2.10	0.86	1.24	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
545	35.79	2.10	0.87	1.24	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
546	35.85	2.11	0.87	1.24	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
547	35.90	2.11	0.87	1.24	0.87	0.739	1.05	0.701	0.99	1.30	0.963	No
548	35.98	2.12	0.87	1.24	0.87	0.739	1.05	0.701	0.99	1.30	0.964	No
549	36.03	2.12	0.87	1.24	0.87	0.739	1.05	0.701	0.99	1.30	0.964	No
550	36.09	2.12	0.88	1.25	0.87	0.739	1.05	0.701	0.99	1.30	0.964	No
551	36.18	2.13	0.88	1.25	0.87	0.739	1.05	0.701	0.99	1.30	0.964	No
552	36.24	2.13	0.88	1.25	0.87	0.739	1.05	0.701	0.99	1.30	0.964	No
553	36.29	2.13	0.88	1.25	0.87	0.739	1.05	0.701	0.99	1.30	0.964	No
554	36.38	2.14	0.89	1.25	0.87	0.739	1.05	0.701	0.98	1.30	0.964	No
555	36.44	2.14	0.89	1.26	0.86	0.739	1.05	0.701	0.98	1.30	0.964	No
556	36.49	2.15	0.89	1.26	0.86	0.739	1.05	0.701	0.98	1.30	0.964	No
557	36.57	2.15	0.89	1.26	0.86	0.739	1.05	0.701	0.98	1.30	0.964	No
558	36.63	2.15	0.89	1.26	0.86	0.739	1.05	0.701	0.98	1.30	0.964	No
559	36.69	2.16	0.90	1.26	0.86	0.739	1.05	0.701	0.98	1.30	0.965	No
560	36.77	2.16	0.90	1.27	0.86	0.739	1.05	0.700	0.98	1.30	0.965	No
561	36.83	2.17	0.90	1.27	0.86	0.739	1.05	0.700	0.98	1.30	0.965	No
562	36.88	2.17	0.90	1.27	0.86	0.739	1.05	0.700	0.98	1.30	0.965	No
563	36.96	2.17	0.90	1.27	0.86	0.739	1.05	0.700	0.98	1.30	0.965	No
564	37.03	2.18	0.91	1.27	0.86	0.739	1.05	0.700	0.98	1.30	0.965	No
565	37.08	2.18	0.91	1.27	0.86	0.739	1.05	0.700	0.98	1.30	0.965	No
566	37.14	2.18	0.91	1.28	0.86	0.738	1.05	0.700	0.98	1.30	0.965	No
567	37.23	2.19	0.91	1.28	0.86	0.738	1.05	0.700	0.98	1.30	0.963	No
568	37.28	2.19	0.91	1.28	0.86	0.738	1.05	0.700	0.98	1.30	0.962	No
569	37.36	2.20	0.92	1.28	0.86	0.738	1.05	0.700	0.98	1.30	0.963	No
570	37.41	2.20	0.92	1.28	0.86	0.738	1.05	0.700	0.98	1.30	0.964	No
571	37.48	2.21	0.92	1.29	0.86	0.738	1.05	0.700	0.98	1.30	0.965	No
572	37.57	2.21	0.92	1.29	0.86	0.738	1.05	0.700	0.98	1.30	0.965	No
573	37.63	2.21	0.92	1.29	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
574	37.66	2.22	0.93	1.29	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
575	37.77	2.22	0.93	1.29	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
576	37.82	2.23	0.93	1.30	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
577	37.88	2.23	0.93	1.30	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
578	37.96	2.23	0.93	1.30	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
579	38.01	2.24	0.94	1.30	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
580	38.06	2.24	0.94	1.30	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
581	38.13	2.24	0.94	1.30	0.86	0.738	1.05	0.700	0.98	1.30	0.966	No
582	38.19	2.25	0.94	1.31	0.86	0.738	1.05	0.700	0.98	1.30	0.967	No
583	38.26	2.25	0.94	1.31	0.86	0.738	1.05	0.700	0.98	1.30	0.967	No
584	38.32	2.25	0.95	1.31	0.86	0.738	1.05	0.700	0.98	1.30	0.967	No
585	38.41	2.26	0.95	1.31	0.86	0.738	1.05	0.700	0.98	1.30	0.967	No
586	38.46	2.26	0.95	1.31	0.85	0.738	1.05	0.700	0.98	1.30	0.967	No
587	38.52	2.27	0.95	1.31	0.85	0.738	1.05	0.700	0.98	1.30	0.967	No
588	38.59	2.27	0.95	1.32	0.85	0.738	1.05	0.700	0.98	1.30	0.967	No
589	38.65	2.27	0.96	1.32	0.85	0.738	1.05	0.700	0.98	1.30	0.967	No
590	38.73	2.28	0.96	1.32	0.85	0.738	1.05	0.699	0.98	1.30	0.967	No
591	38.79	2.28	0.96	1.32	0.85	0.737	1.05	0.699	0.98	1.30	0.967	No
592	38.86	2.29	0.96	1.32	0.85	0.737	1.05	0.699	0.98	1.30	0.966	No
593	38.92	2.29	0.96	1.33	0.85	0.737	1.05	0.699	0.98	1.30	0.966	No
594	38.98	2.29	0.97	1.33	0.85	0.737	1.05	0.699	0.98	1.30	0.965	No
595	39.06	2.30	0.97	1.33	0.85	0.737	1.05	0.699	0.97	1.30	0.963	No
596	39.12	2.30	0.97	1.33	0.85	0.737	1.05	0.699	0.97	1.30	0.962	No
597	39.18	2.31	0.97	1.33	0.85	0.737	1.05	0.699	0.97	1.30	0.960	No
598	39.28	2.31	0.98	1.34	0.85	0.737	1.05	0.699	0.97	1.30	0.957	No
599	39.32	2.32	0.98	1.34	0.85	0.737	1.05	0.699	0.97	1.30	0.956	No
600	39.37	2.32	0.98	1.34	0.85	0.737	1.05	0.699	0.96	1.30	0.954	No
601	39.48	2.33	0.98	1.34	0.85	0.736	1.05	0.698	0.96	1.30	0.950	No
602	39.52	2.33	0.98	1.34	0.85	0.736	1.05	0.698	0.96	1.30	0.949	No
603	39.57	2.33	0.99	1.35	0.85	0.736	1.05	0.698	0.96	1.30	0.947	No
604	39.66	2.34	0.99	1.35	0.85	0.736	1.05	0.698	0.96	1.30	0.947	No
605	39.70	2.34	0.99	1.35	0.85	0.736	1.05	0.698	0.96	1.30	0.949	No
606	39.77	2.34	0.99	1.35	0.85	0.736	1.05	0.698	0.95	1.30	0.946	No
607	39.87	2.35	0.99	1.36	0.85	0.736	1.05	0.698	0.95	1.30	0.944	No
608	39.92	2.35	1.00	1.36	0.85	0.735	1.05	0.697	0.95	1.30	0.943	No
609	39.98	2.36	1.00	1.36	0.85	0.735	1.05	0.697	0.95	1.30	0.941	No
610	40.06	2.36	1.00	1.36	0.85	0.735	1.05	0.697	0.96	1.30	0.952	No
611	40.12	2.37	1.00	1.36	0.85	0.735	1.05	0.697	0.94	1.30	0.938	No
612	40.16	2.37	1.00	1.37	0.85	0.735	1.05	0.697	0.94	1.30	0.941	No
613	40.25	2.38	1.01	1.37	0.85	0.735	1.05	0.697	0.93	1.30	0.946	No
614	40.31	2.38	1.01	1.37	0.85	0.734	1.05	0.697	0.93	1.30	0.947	No
615	40.37	2.38	1.01	1.37	0.85	0.734	1.05	0.696	0.93	1.30	0.947	No
616	40.44	2.39	1.01	1.38	0.85	0.734	1.05	0.696	0.93	1.30	0.946	No
617	40.50	2.39	1.01	1.38	0.84	0.734	1.05	0.696	0.93	1.30	0.945	No
618	40.56	2.40	1.02	1.38	0.84	0.734	1.05	0.696	0.94	1.30	0.943	No
619	40.63	2.40	1.02	1.38	0.84	0.734	1.05	0.696	0.94	1.30	0.941	No
620	40.71	2.41	1.02	1.39	0.84	0.733	1.05	0.696	0.94	1.30	0.940	No
621	40.77	2.41	1.02	1.39	0.84	0.733	1.05	0.695	0.94	1.30	0.939	No
622	40.86	2.42	1.03	1.39	0.84	0.733	1.05	0.695	0.94	1.30	0.941	No
623	40.90	2.42	1.03	1.39	0.84	0.733	1.05	0.695	0.94	1.30	0.942	No
624	40.96	2.42	1.03	1.39	0.84	0.733	1.05	0.695	0.94	1.30	0.943	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
625	41.03	2.43	1.03	1.40	0.84	0.733	1.05	0.695	0.95	1.30	0.946	No
626	41.09	2.43	1.03	1.40	0.84	0.732	1.05	0.695	0.95	1.30	0.947	No
627	41.15	2.43	1.03	1.40	0.84	0.732	1.05	0.695	0.95	1.30	0.948	No
628	41.24	2.44	1.04	1.40	0.84	0.732	1.05	0.694	0.95	1.30	0.950	No
629	41.28	2.44	1.04	1.41	0.84	0.732	1.05	0.694	0.95	1.30	0.951	No
630	41.35	2.45	1.04	1.41	0.84	0.732	1.05	0.694	0.95	1.30	0.952	No
631	41.41	2.45	1.04	1.41	0.84	0.732	1.05	0.694	0.95	1.30	0.953	No
632	41.50	2.46	1.05	1.41	0.84	0.731	1.05	0.694	0.95	1.30	0.954	No
633	41.55	2.46	1.05	1.41	0.84	0.731	1.05	0.694	0.95	1.30	0.954	No
634	41.61	2.46	1.05	1.42	0.84	0.731	1.05	0.693	0.96	1.30	0.955	No
635	41.71	2.47	1.05	1.42	0.84	0.731	1.05	0.693	0.96	1.30	0.956	No
636	41.75	2.47	1.05	1.42	0.84	0.731	1.05	0.693	0.96	1.30	0.956	No
637	41.80	2.48	1.05	1.42	0.84	0.731	1.05	0.693	0.96	1.30	0.957	No
638	41.87	2.48	1.06	1.42	0.84	0.731	1.05	0.693	0.96	1.30	0.957	No
639	41.93	2.49	1.06	1.43	0.84	0.730	1.05	0.693	0.96	1.30	0.957	No
640	42.00	2.49	1.06	1.43	0.84	0.730	1.05	0.693	0.96	1.30	0.958	No
641	42.09	2.50	1.06	1.43	0.84	0.730	1.05	0.692	0.96	1.30	0.958	No
642	42.14	2.50	1.07	1.43	0.84	0.730	1.05	0.692	0.96	1.30	0.959	No
643	42.20	2.50	1.07	1.44	0.84	0.730	1.05	0.692	0.96	1.30	0.959	No
644	42.29	2.51	1.07	1.44	0.84	0.730	1.05	0.692	0.96	1.30	0.959	No
645	42.34	2.51	1.07	1.44	0.84	0.729	1.05	0.692	0.96	1.30	0.959	No
646	42.39	2.51	1.07	1.44	0.84	0.729	1.05	0.692	0.96	1.30	0.960	No
647	42.48	2.52	1.08	1.44	0.84	0.729	1.05	0.692	0.96	1.30	0.960	No
648	42.54	2.52	1.08	1.45	0.83	0.729	1.05	0.691	0.96	1.30	0.960	No
649	42.59	2.53	1.08	1.45	0.83	0.729	1.05	0.691	0.96	1.30	0.960	No
650	42.68	2.53	1.08	1.45	0.83	0.729	1.05	0.691	0.96	1.30	0.960	No
651	42.73	2.54	1.08	1.45	0.83	0.729	1.05	0.691	0.96	1.30	0.960	No
652	42.79	2.54	1.09	1.45	0.83	0.728	1.05	0.691	0.96	1.30	0.960	No
653	42.88	2.55	1.09	1.46	0.83	0.728	1.05	0.691	0.96	1.30	0.960	No
654	42.93	2.55	1.09	1.46	0.83	0.728	1.05	0.691	0.96	1.30	0.960	No
655	42.99	2.55	1.09	1.46	0.83	0.728	1.05	0.690	0.96	1.30	0.960	No
656	43.06	2.56	1.09	1.46	0.83	0.728	1.05	0.690	0.96	1.30	0.960	No
657	43.14	2.56	1.10	1.47	0.83	0.728	1.05	0.690	0.96	1.30	0.961	No
658	43.18	2.56	1.10	1.47	0.83	0.728	1.05	0.690	0.96	1.30	0.961	No
659	43.28	2.57	1.10	1.47	0.83	0.727	1.05	0.690	0.96	1.30	0.962	No
660	43.33	2.57	1.10	1.47	0.83	0.727	1.05	0.690	0.96	1.30	0.962	No
661	43.42	2.58	1.10	1.47	0.83	0.727	1.05	0.690	0.96	1.30	0.962	No
662	43.44	2.58	1.11	1.48	0.83	0.727	1.05	0.689	0.96	1.30	0.963	No
663	43.53	2.59	1.11	1.48	0.83	0.727	1.05	0.689	0.97	1.30	0.963	No
664	43.58	2.59	1.11	1.48	0.83	0.727	1.05	0.689	0.97	1.30	0.963	No
665	43.67	2.60	1.11	1.48	0.83	0.727	1.05	0.689	0.97	1.30	0.963	No
666	43.73	2.60	1.11	1.48	0.83	0.726	1.05	0.689	0.97	1.30	0.963	No
667	43.78	2.60	1.12	1.49	0.83	0.726	1.05	0.689	0.97	1.30	0.963	No
668	43.86	2.61	1.12	1.49	0.83	0.726	1.05	0.689	0.97	1.30	0.963	No
669	43.92	2.61	1.12	1.49	0.83	0.726	1.05	0.689	0.97	1.30	0.963	No
670	43.97	2.61	1.12	1.49	0.83	0.726	1.05	0.689	0.97	1.30	0.963	No
671	44.06	2.62	1.13	1.49	0.83	0.726	1.05	0.688	0.97	1.30	0.963	No
672	44.12	2.62	1.13	1.50	0.83	0.726	1.05	0.688	0.97	1.30	0.963	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
673	44.17	2.63	1.13	1.50	0.83	0.726	1.05	0.688	0.97	1.30	0.963	No
674	44.26	2.63	1.13	1.50	0.83	0.725	1.05	0.688	0.97	1.30	0.962	No
675	44.30	2.63	1.13	1.50	0.83	0.725	1.05	0.688	0.97	1.30	0.962	No
676	44.37	2.64	1.13	1.50	0.83	0.725	1.05	0.688	0.97	1.30	0.962	No
677	44.44	2.64	1.14	1.50	0.83	0.725	1.05	0.688	0.97	1.30	0.962	No
678	44.50	2.64	1.14	1.51	0.83	0.725	1.05	0.688	0.97	1.30	0.962	No
679	44.59	2.65	1.14	1.51	0.82	0.725	1.05	0.688	0.97	1.30	0.962	No
680	44.64	2.65	1.14	1.51	0.82	0.725	1.05	0.688	0.97	1.30	0.962	No
681	44.73	2.66	1.15	1.51	0.82	0.725	1.05	0.687	0.97	1.30	0.962	No
682	44.77	2.66	1.15	1.51	0.82	0.725	1.05	0.687	0.97	1.30	0.962	No
683	44.83	2.66	1.15	1.52	0.82	0.725	1.05	0.687	0.97	1.30	0.962	No
684	44.88	2.67	1.15	1.52	0.82	0.725	1.05	0.687	0.97	1.30	0.962	No
685	44.96	2.67	1.15	1.52	0.82	0.724	1.05	0.687	0.97	1.30	0.962	No
686	45.03	2.68	1.16	1.52	0.82	0.724	1.05	0.687	0.97	1.30	0.962	No
687	45.08	2.68	1.16	1.52	0.82	0.724	1.05	0.687	0.97	1.30	0.962	No
688	45.17	2.68	1.16	1.52	0.82	0.724	1.05	0.687	0.97	1.30	0.962	No
689	45.22	2.69	1.16	1.53	0.82	0.724	1.05	0.687	0.97	1.30	0.961	No
690	45.28	2.69	1.16	1.53	0.82	0.724	1.05	0.687	0.97	1.30	0.962	No
691	45.36	2.70	1.17	1.53	0.82	0.724	1.05	0.686	0.97	1.30	0.961	No
692	45.41	2.70	1.17	1.53	0.82	0.724	1.05	0.686	0.97	1.30	0.961	No
693	45.48	2.70	1.17	1.53	0.82	0.724	1.05	0.686	0.97	1.30	0.961	No
694	45.54	2.71	1.17	1.53	0.82	0.724	1.05	0.686	0.97	1.30	0.961	No
695	45.63	2.71	1.17	1.54	0.82	0.723	1.05	0.686	0.97	1.30	0.961	No
696	45.67	2.71	1.18	1.54	0.82	0.723	1.05	0.686	0.97	1.30	0.961	No
697	45.74	2.72	1.18	1.54	0.82	0.723	1.05	0.686	0.97	1.30	0.962	No
698	45.83	2.72	1.18	1.54	0.82	0.723	1.05	0.686	0.96	1.30	0.962	No
699	45.88	2.73	1.18	1.54	0.82	0.723	1.05	0.686	0.95	1.30	0.961	No
700	45.97	2.73	1.18	1.55	0.82	0.723	1.05	0.685	0.95	1.30	0.959	No
701	46.03	2.74	1.19	1.55	0.82	0.722	1.05	0.685	0.94	1.30	0.958	No
702	46.07	2.74	1.19	1.55	0.82	0.722	1.05	0.685	0.94	1.30	0.958	No
703	46.17	2.74	1.19	1.55	0.82	0.722	1.05	0.685	0.94	1.30	0.956	No
704	46.22	2.75	1.19	1.56	0.82	0.722	1.05	0.685	0.93	1.30	0.955	No
705	46.27	2.75	1.19	1.56	0.82	0.722	1.05	0.685	0.93	1.30	0.955	No
706	46.36	2.76	1.20	1.56	0.82	0.721	1.05	0.684	0.93	1.30	0.954	No
707	46.41	2.76	1.20	1.56	0.82	0.721	1.05	0.684	0.92	1.30	0.953	No
708	46.49	2.77	1.20	1.56	0.82	0.721	1.05	0.684	0.92	1.30	0.952	No
709	46.54	2.77	1.20	1.57	0.81	0.721	1.05	0.684	0.91	1.30	0.951	No
710	46.62	2.77	1.21	1.57	0.81	0.721	1.05	0.683	0.90	1.30	0.961	No
711	46.66	2.78	1.21	1.57	0.81	0.721	1.05	0.683	0.90	1.30	0.964	No
712	46.73	2.78	1.21	1.57	0.81	0.720	1.05	0.683	0.89	1.30	0.970	No
713	46.82	2.79	1.21	1.58	0.81	0.720	1.05	0.683	0.89	1.30	0.970	No
714	46.85	2.79	1.21	1.58	0.81	0.720	1.05	0.683	0.89	1.30	0.969	No
715	46.92	2.79	1.21	1.58	0.81	0.720	1.05	0.683	0.90	1.30	0.966	No
716	47.01	2.80	1.22	1.58	0.81	0.719	1.05	0.682	0.90	1.30	0.963	No
717	47.06	2.80	1.22	1.58	0.81	0.719	1.05	0.682	0.90	1.30	0.961	No
718	47.15	2.81	1.22	1.59	0.81	0.719	1.05	0.682	0.90	1.30	0.957	No
719	47.21	2.81	1.22	1.59	0.81	0.719	1.05	0.682	0.90	1.30	0.957	No
720	47.25	2.82	1.22	1.59	0.81	0.719	1.05	0.682	0.90	1.30	0.956	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
721	47.31	2.82	1.23	1.59	0.81	0.719	1.05	0.681	0.91	1.30	0.952	No
722	47.41	2.83	1.23	1.60	0.81	0.718	1.05	0.681	0.91	1.30	0.953	No
723	47.46	2.83	1.23	1.60	0.81	0.718	1.05	0.681	0.90	1.30	0.956	No
724	47.54	2.83	1.23	1.60	0.81	0.718	1.05	0.681	0.90	1.30	0.961	No
725	47.58	2.84	1.24	1.60	0.81	0.718	1.05	0.681	0.90	1.30	0.962	No
726	47.67	2.84	1.24	1.61	0.81	0.717	1.05	0.680	0.89	1.30	0.968	No
727	47.71	2.85	1.24	1.61	0.81	0.717	1.05	0.680	0.89	1.30	0.968	No
728	47.77	2.85	1.24	1.61	0.81	0.717	1.05	0.680	0.89	1.30	0.965	No
729	47.85	2.85	1.24	1.61	0.81	0.717	1.05	0.680	0.89	1.30	0.964	No
730	47.92	2.86	1.25	1.61	0.81	0.717	1.05	0.680	0.89	1.30	0.963	No
731	47.97	2.86	1.25	1.62	0.81	0.716	1.05	0.679	0.89	1.30	0.963	No
732	48.06	2.87	1.25	1.62	0.81	0.716	1.05	0.679	0.89	1.30	0.965	No
733	48.12	2.87	1.25	1.62	0.81	0.716	1.05	0.679	0.89	1.30	0.967	No
734	48.17	2.88	1.25	1.62	0.81	0.716	1.05	0.679	0.89	1.30	0.970	No
735	48.25	2.88	1.26	1.63	0.81	0.716	1.05	0.679	0.88	1.30	0.973	No
736	48.31	2.88	1.26	1.63	0.81	0.715	1.05	0.678	0.88	1.30	0.974	No
737	48.36	2.89	1.26	1.63	0.81	0.715	1.05	0.678	0.88	1.30	0.975	No
738	48.45	2.89	1.26	1.63	0.81	0.715	1.05	0.678	0.88	1.30	0.972	No
739	48.50	2.90	1.26	1.63	0.81	0.715	1.05	0.678	0.89	1.30	0.970	No
740	48.57	2.90	1.27	1.64	0.80	0.714	1.05	0.678	0.89	1.30	0.969	No
741	48.63	2.91	1.27	1.64	0.80	0.714	1.05	0.677	0.89	1.30	0.966	No
742	48.72	2.91	1.27	1.64	0.80	0.714	1.05	0.677	0.89	1.30	0.964	No
743	48.77	2.91	1.27	1.64	0.80	0.714	1.05	0.677	0.89	1.30	0.961	No
744	48.85	2.92	1.27	1.65	0.80	0.714	1.05	0.677	0.90	1.30	0.957	No
745	48.91	2.92	1.28	1.65	0.80	0.713	1.05	0.677	0.90	1.30	0.953	No
746	48.97	2.93	1.28	1.65	0.80	0.713	1.05	0.676	0.90	1.30	0.953	No
747	49.05	2.93	1.28	1.65	0.80	0.713	1.05	0.676	0.90	1.30	0.953	No
748	49.11	2.94	1.28	1.65	0.80	0.713	1.05	0.676	0.90	1.30	0.953	No
749	49.16	2.94	1.28	1.66	0.80	0.713	1.05	0.676	0.91	1.30	0.953	No
750	49.21	2.94	1.29	1.66	0.80	0.712	1.05	0.676	0.91	1.30	0.953	No
751	49.28	2.95	1.29	1.66	0.80	0.712	1.05	0.675	0.91	1.30	0.953	No
752	49.35	2.95	1.29	1.66	0.80	0.712	1.05	0.675	0.91	1.30	0.953	No
753	49.42	2.96	1.29	1.66	0.80	0.712	1.05	0.675	0.91	1.30	0.953	No
754	49.48	2.96	1.29	1.67	0.80	0.712	1.05	0.675	0.91	1.30	0.953	No
755	49.54	2.96	1.30	1.67	0.80	0.711	1.05	0.675	0.91	1.30	0.953	No
756	49.61	2.97	1.30	1.67	0.80	0.711	1.05	0.674	0.91	1.30	0.953	No
757	49.68	2.97	1.30	1.67	0.80	0.711	1.05	0.674	0.91	1.30	0.953	No
758	49.76	2.98	1.30	1.68	0.80	0.711	1.05	0.674	0.91	1.30	0.953	No
759	49.81	2.98	1.30	1.68	0.80	0.711	1.05	0.674	0.91	1.30	0.953	No
760	49.88	2.99	1.31	1.68	0.80	0.710	1.05	0.674	0.91	1.30	0.953	No
761	49.95	2.99	1.31	1.68	0.80	0.710	1.05	0.674	0.91	1.30	0.953	No
762	50.02	3.00	1.31	1.68	0.80	0.710	1.05	0.673	0.90	1.30	2.000	No
763	50.10	3.00	1.31	1.69	0.80	0.710	1.05	0.673	0.90	1.30	2.000	No
764	50.15	3.00	1.31	1.69	0.80	0.709	1.05	0.673	0.90	1.30	2.000	No
765	50.20	3.01	1.32	1.69	0.80	0.709	1.05	0.673	0.90	1.30	2.000	No
766	50.28	3.01	1.32	1.69	0.80	0.709	1.05	0.672	0.89	1.30	2.000	No
767	50.34	3.02	1.32	1.70	0.80	0.709	1.05	0.672	0.89	1.30	2.000	No
768	50.44	3.02	1.32	1.70	0.80	0.709	1.05	0.672	0.89	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
769	50.47	3.03	1.33	1.70	0.80	0.708	1.05	0.672	0.89	1.30	2.000	No
770	50.54	3.03	1.33	1.70	0.80	0.708	1.05	0.672	0.88	1.30	2.000	No
771	50.59	3.03	1.33	1.70	0.79	0.708	1.05	0.671	0.88	1.30	2.000	No
772	50.69	3.04	1.33	1.71	0.79	0.708	1.05	0.671	0.88	1.30	2.000	No
773	50.73	3.04	1.33	1.71	0.79	0.708	1.05	0.671	0.88	1.30	2.000	No
774	50.84	3.05	1.34	1.71	0.79	0.707	1.05	0.671	0.89	1.30	2.000	No
775	50.86	3.05	1.34	1.71	0.79	0.707	1.05	0.671	0.89	1.30	2.000	No
776	50.93	3.06	1.34	1.72	0.79	0.707	1.05	0.670	0.89	1.30	2.000	No
777	50.99	3.06	1.34	1.72	0.79	0.707	1.05	0.670	0.89	1.30	2.000	No
778	51.05	3.06	1.34	1.72	0.79	0.706	1.05	0.670	0.89	1.30	2.000	No
779	51.13	3.07	1.35	1.72	0.79	0.706	1.05	0.670	0.89	1.30	2.000	No
780	51.20	3.07	1.35	1.72	0.79	0.706	1.05	0.670	0.89	1.30	2.000	No
781	51.25	3.08	1.35	1.73	0.79	0.706	1.05	0.669	0.89	1.30	2.000	No
782	51.34	3.08	1.35	1.73	0.79	0.706	1.05	0.669	0.89	1.30	2.000	No
783	51.38	3.09	1.35	1.73	0.79	0.705	1.05	0.669	0.89	1.30	2.000	No
784	51.48	3.09	1.36	1.73	0.79	0.705	1.05	0.669	0.89	1.30	2.000	No
785	51.53	3.09	1.36	1.74	0.79	0.705	1.05	0.668	0.89	1.30	2.000	No
786	51.58	3.10	1.36	1.74	0.79	0.705	1.05	0.668	0.89	1.30	2.000	No
787	51.67	3.10	1.36	1.74	0.79	0.704	1.05	0.668	0.89	1.30	2.000	No
788	51.72	3.11	1.36	1.74	0.79	0.704	1.05	0.668	0.89	1.30	2.000	No
789	51.78	3.11	1.37	1.75	0.79	0.704	1.05	0.668	0.89	1.30	2.000	No
790	51.86	3.12	1.37	1.75	0.79	0.704	1.05	0.667	0.89	1.30	2.000	No
791	51.93	3.12	1.37	1.75	0.79	0.704	1.05	0.667	0.89	1.30	2.000	No
792	51.97	3.12	1.37	1.75	0.79	0.703	1.05	0.667	0.89	1.30	2.000	No
793	52.06	3.13	1.37	1.75	0.79	0.703	1.05	0.667	0.89	1.30	2.000	No
794	52.11	3.13	1.38	1.76	0.79	0.703	1.05	0.667	0.88	1.30	2.000	No
795	52.17	3.14	1.38	1.76	0.79	0.703	1.05	0.666	0.88	1.30	2.000	No
796	52.24	3.14	1.38	1.76	0.79	0.702	1.05	0.666	0.88	1.30	2.000	No
797	52.31	3.15	1.38	1.76	0.79	0.702	1.05	0.666	0.88	1.30	2.000	No
798	52.37	3.15	1.38	1.77	0.79	0.702	1.05	0.666	0.88	1.30	2.000	No
799	52.47	3.16	1.39	1.77	0.79	0.702	1.05	0.666	0.88	1.30	2.000	No
800	52.52	3.16	1.39	1.77	0.79	0.702	1.05	0.665	0.89	1.30	2.000	No
801	52.57	3.16	1.39	1.77	0.79	0.701	1.05	0.665	0.89	1.30	2.000	No
802	52.67	3.17	1.39	1.78	0.78	0.701	1.05	0.665	0.89	1.30	2.000	No
803	52.72	3.17	1.40	1.78	0.78	0.701	1.05	0.665	0.90	1.30	2.000	No
804	52.77	3.18	1.40	1.78	0.78	0.701	1.05	0.665	0.90	1.30	2.000	No
805	52.86	3.18	1.40	1.78	0.78	0.700	1.05	0.664	0.91	1.30	2.000	No
806	52.91	3.18	1.40	1.78	0.78	0.700	1.05	0.664	0.91	1.30	2.000	No
807	52.96	3.19	1.40	1.79	0.78	0.700	1.05	0.664	0.91	1.30	2.000	No
808	53.02	3.19	1.40	1.79	0.78	0.700	1.05	0.664	0.91	1.30	2.000	No
809	53.10	3.20	1.41	1.79	0.78	0.700	1.05	0.664	0.92	1.30	2.000	No
810	53.16	3.20	1.41	1.79	0.78	0.699	1.05	0.663	0.92	1.30	2.000	No
811	53.24	3.21	1.41	1.79	0.78	0.699	1.05	0.663	0.92	1.30	2.000	No
812	53.30	3.21	1.41	1.80	0.78	0.699	1.05	0.663	0.92	1.30	2.000	No
813	53.36	3.21	1.42	1.80	0.78	0.699	1.05	0.663	0.92	1.30	2.000	No
814	53.42	3.22	1.42	1.80	0.78	0.699	1.05	0.663	0.92	1.30	2.000	No
815	53.48	3.22	1.42	1.80	0.78	0.698	1.05	0.662	0.93	1.30	2.000	No
816	53.56	3.23	1.42	1.80	0.78	0.698	1.05	0.662	0.92	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
817	53.61	3.23	1.42	1.81	0.78	0.698	1.05	0.662	0.92	1.30	2.000	No
818	53.69	3.23	1.43	1.81	0.78	0.698	1.05	0.662	0.92	1.30	2.000	No
819	53.75	3.24	1.43	1.81	0.78	0.698	1.05	0.662	0.92	1.30	2.000	No
820	53.82	3.24	1.43	1.81	0.78	0.697	1.05	0.661	0.92	1.30	2.000	No
821	53.88	3.25	1.43	1.82	0.78	0.697	1.05	0.661	0.92	1.30	2.000	No
822	53.97	3.25	1.43	1.82	0.78	0.697	1.05	0.661	0.92	1.30	2.000	No
823	54.02	3.26	1.44	1.82	0.78	0.697	1.05	0.661	0.92	1.30	2.000	No
824	54.09	3.26	1.44	1.82	0.78	0.696	1.05	0.661	0.92	1.30	2.000	No
825	54.14	3.26	1.44	1.82	0.78	0.696	1.05	0.660	0.92	1.30	2.000	No
826	54.21	3.27	1.44	1.83	0.78	0.696	1.05	0.660	0.93	1.30	2.000	No
827	54.28	3.27	1.44	1.83	0.78	0.696	1.05	0.660	0.93	1.30	2.000	No
828	54.33	3.28	1.45	1.83	0.78	0.696	1.05	0.660	0.93	1.30	2.000	No
829	54.43	3.28	1.45	1.83	0.78	0.695	1.05	0.660	0.93	1.30	2.000	No
830	54.48	3.28	1.45	1.83	0.78	0.695	1.05	0.659	0.93	1.30	2.000	No
831	54.53	3.29	1.45	1.84	0.78	0.695	1.05	0.659	0.93	1.30	2.000	No
832	54.62	3.29	1.45	1.84	0.78	0.695	1.05	0.659	0.93	1.30	2.000	No
833	54.67	3.30	1.46	1.84	0.77	0.695	1.05	0.659	0.93	1.30	2.000	No
834	54.73	3.30	1.46	1.84	0.77	0.695	1.05	0.659	0.93	1.30	2.000	No
835	54.82	3.31	1.46	1.85	0.77	0.694	1.05	0.658	0.93	1.30	2.000	No
836	54.87	3.31	1.46	1.85	0.77	0.694	1.05	0.658	0.93	1.30	2.000	No
837	54.95	3.31	1.46	1.85	0.77	0.694	1.05	0.658	0.93	1.30	2.000	No
838	55.01	3.32	1.47	1.85	0.77	0.694	1.05	0.658	0.93	1.30	2.000	No
839	55.06	3.32	1.47	1.85	0.77	0.694	1.05	0.658	0.93	1.30	2.000	No
840	55.12	3.32	1.47	1.85	0.77	0.693	1.05	0.658	0.93	1.30	2.000	No
841	55.20	3.33	1.47	1.86	0.77	0.693	1.05	0.657	0.93	1.30	2.000	No
842	55.26	3.33	1.47	1.86	0.77	0.693	1.05	0.657	0.94	1.30	2.000	No
843	55.32	3.34	1.48	1.86	0.77	0.693	1.05	0.657	0.94	1.30	2.000	No
844	55.41	3.34	1.48	1.86	0.77	0.693	1.05	0.657	0.94	1.30	2.000	No
845	55.47	3.35	1.48	1.87	0.77	0.692	1.05	0.657	0.93	1.30	2.000	No
846	55.51	3.35	1.48	1.87	0.77	0.692	1.05	0.657	0.93	1.30	2.000	No
847	55.59	3.35	1.48	1.87	0.77	0.692	1.05	0.656	0.93	1.30	2.000	No
848	55.67	3.36	1.49	1.87	0.77	0.692	1.05	0.656	0.93	1.30	2.000	No
849	55.72	3.36	1.49	1.87	0.77	0.692	1.05	0.656	0.92	1.30	2.000	No
850	55.81	3.37	1.49	1.88	0.77	0.691	1.05	0.656	0.91	1.30	2.000	No
851	55.86	3.37	1.49	1.88	0.77	0.691	1.05	0.656	0.91	1.30	2.000	No
852	55.92	3.37	1.49	1.88	0.77	0.691	1.05	0.655	0.91	1.30	2.000	No
853	56.01	3.38	1.50	1.88	0.77	0.691	1.05	0.655	0.90	1.30	2.000	No
854	56.06	3.38	1.50	1.88	0.77	0.691	1.05	0.655	0.90	1.30	2.000	No
855	56.11	3.39	1.50	1.89	0.77	0.690	1.05	0.655	0.90	1.30	2.000	No
856	56.21	3.39	1.50	1.89	0.77	0.690	1.05	0.655	0.89	1.30	2.000	No
857	56.25	3.40	1.51	1.89	0.77	0.690	1.05	0.654	0.89	1.30	2.000	No
858	56.31	3.40	1.51	1.89	0.77	0.690	1.05	0.654	0.88	1.30	2.000	No
859	56.38	3.40	1.51	1.89	0.77	0.690	1.05	0.654	0.90	1.30	2.000	No
860	56.44	3.41	1.51	1.90	0.77	0.689	1.05	0.654	0.90	1.30	2.000	No
861	56.50	3.41	1.51	1.90	0.77	0.689	1.05	0.654	0.89	1.30	2.000	No
862	56.58	3.42	1.52	1.90	0.77	0.689	1.05	0.653	0.89	1.30	2.000	No
863	56.65	3.42	1.52	1.90	0.77	0.689	1.05	0.653	0.89	1.30	2.000	No
864	56.73	3.43	1.52	1.91	0.77	0.688	1.05	0.653	0.88	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
865	56.76	3.43	1.52	1.91	0.76	0.688	1.05	0.653	0.87	1.30	2.000	No
866	56.84	3.43	1.52	1.91	0.76	0.688	1.05	0.653	0.87	1.30	2.000	No
867	56.92	3.44	1.53	1.91	0.76	0.688	1.05	0.652	0.86	1.30	2.000	No
868	56.98	3.44	1.53	1.91	0.76	0.688	1.05	0.652	0.86	1.30	2.000	No
869	57.02	3.45	1.53	1.92	0.76	0.687	1.05	0.652	0.86	1.30	2.000	No
870	57.12	3.45	1.53	1.92	0.76	0.687	1.05	0.652	0.85	1.30	2.000	No
871	57.17	3.46	1.53	1.92	0.76	0.687	1.05	0.651	0.85	1.30	2.000	No
872	57.23	3.46	1.54	1.92	0.76	0.687	1.05	0.651	0.85	1.30	2.000	No
873	57.32	3.47	1.54	1.93	0.76	0.686	1.05	0.651	0.85	1.30	2.000	No
874	57.36	3.47	1.54	1.93	0.76	0.686	1.05	0.651	0.85	1.30	2.000	No
875	57.42	3.47	1.54	1.93	0.76	0.686	1.05	0.651	0.84	1.30	2.000	No
876	57.50	3.48	1.54	1.93	0.76	0.686	1.05	0.650	0.84	1.30	2.000	No
877	57.55	3.48	1.55	1.93	0.76	0.686	1.05	0.650	0.84	1.30	2.000	No
878	57.62	3.48	1.55	1.94	0.76	0.685	1.05	0.650	0.84	1.30	2.000	No
879	57.69	3.49	1.55	1.94	0.76	0.685	1.05	0.650	0.83	1.30	2.000	No
880	57.77	3.49	1.55	1.94	0.76	0.685	1.05	0.649	0.83	1.30	2.000	No
881	57.83	3.50	1.55	1.94	0.76	0.685	1.05	0.649	0.83	1.30	2.000	No
882	57.91	3.50	1.56	1.95	0.76	0.684	1.05	0.649	0.83	1.30	2.000	No
883	57.97	3.51	1.56	1.95	0.76	0.684	1.05	0.649	0.83	1.30	2.000	No
884	58.01	3.51	1.56	1.95	0.76	0.684	1.05	0.649	0.83	1.30	2.000	No
885	58.11	3.52	1.56	1.95	0.76	0.684	1.05	0.648	0.82	1.30	2.000	No
886	58.16	3.52	1.56	1.96	0.76	0.683	1.05	0.648	0.82	1.30	2.000	No
887	58.22	3.52	1.57	1.96	0.76	0.683	1.05	0.648	0.82	1.30	2.000	No
888	58.31	3.53	1.57	1.96	0.76	0.683	1.05	0.648	0.83	1.30	2.000	No
889	58.36	3.53	1.57	1.96	0.76	0.683	1.05	0.647	0.83	1.30	2.000	No
890	58.41	3.54	1.57	1.96	0.76	0.682	1.05	0.647	0.83	1.30	2.000	No
891	58.51	3.54	1.58	1.97	0.76	0.682	1.05	0.647	0.82	1.30	2.000	No
892	58.55	3.55	1.58	1.97	0.76	0.682	1.05	0.647	0.81	1.30	2.000	No
893	58.60	3.55	1.58	1.97	0.76	0.682	1.05	0.647	0.81	1.30	2.000	No
894	58.67	3.55	1.58	1.97	0.76	0.682	1.05	0.646	0.82	1.30	2.000	No
895	58.76	3.56	1.58	1.98	0.76	0.681	1.05	0.646	0.82	1.30	2.000	No
896	58.80	3.56	1.58	1.98	0.76	0.681	1.05	0.646	0.82	1.30	2.000	No
897	58.88	3.57	1.59	1.98	0.75	0.681	1.05	0.646	0.83	1.30	2.000	No
898	58.94	3.57	1.59	1.98	0.75	0.681	1.05	0.645	0.82	1.30	2.000	No
899	59.01	3.58	1.59	1.98	0.75	0.680	1.05	0.645	0.82	1.30	2.000	No
900	59.06	3.58	1.59	1.99	0.75	0.680	1.05	0.645	0.81	1.30	2.000	No
901	59.15	3.59	1.60	1.99	0.75	0.680	1.05	0.645	0.82	1.30	2.000	No
902	59.20	3.59	1.60	1.99	0.75	0.680	1.05	0.645	0.82	1.30	2.000	No
903	59.25	3.59	1.60	1.99	0.75	0.679	1.05	0.644	0.82	1.30	2.000	No
904	59.34	3.60	1.60	2.00	0.75	0.679	1.05	0.644	0.81	1.30	2.000	No
905	59.40	3.60	1.60	2.00	0.75	0.679	1.05	0.644	0.82	1.30	2.000	No
906	59.45	3.61	1.61	2.00	0.75	0.679	1.05	0.644	0.85	1.30	2.000	No
907	59.54	3.61	1.61	2.00	0.75	0.678	1.05	0.643	0.84	1.30	2.000	No
908	59.60	3.62	1.61	2.01	0.75	0.678	1.05	0.643	0.83	1.30	2.000	No
909	59.65	3.62	1.61	2.01	0.75	0.678	1.05	0.643	0.83	1.30	2.000	No
910	59.74	3.62	1.61	2.01	0.75	0.678	1.05	0.643	0.82	1.30	2.000	No
911	59.78	3.63	1.62	2.01	0.75	0.678	1.05	0.643	0.83	1.30	2.000	No
912	59.87	3.63	1.62	2.01	0.75	0.677	1.05	0.642	0.85	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
913	59.94	3.64	1.62	2.02	0.75	0.677	1.05	0.642	0.85	1.30	2.000	No
914	59.99	3.64	1.62	2.02	0.75	0.677	1.05	0.642	0.84	1.30	2.000	No
915	60.05	3.64	1.62	2.02	0.75	0.677	1.05	0.642	0.84	1.30	2.000	No
916	60.14	3.65	1.63	2.02	0.75	0.676	1.05	0.641	0.82	1.30	2.000	No
917	60.19	3.65	1.63	2.03	0.75	0.676	1.05	0.641	0.82	1.30	2.000	No
918	60.24	3.66	1.63	2.03	0.75	0.676	1.05	0.641	0.82	1.30	2.000	No
919	60.34	3.66	1.63	2.03	0.75	0.676	1.05	0.641	0.82	1.30	2.000	No
920	60.38	3.67	1.63	2.03	0.75	0.675	1.05	0.641	0.82	1.30	2.000	No
921	60.44	3.67	1.64	2.03	0.75	0.675	1.05	0.640	0.81	1.30	2.000	No
922	60.53	3.68	1.64	2.04	0.75	0.675	1.05	0.640	0.80	1.30	2.000	No
923	60.58	3.68	1.64	2.04	0.75	0.675	1.05	0.640	0.80	1.30	2.000	No
924	60.63	3.68	1.64	2.04	0.75	0.675	1.05	0.640	0.80	1.30	2.000	No
925	60.71	3.69	1.64	2.04	0.75	0.674	1.05	0.639	0.80	1.30	2.000	No
926	60.78	3.69	1.65	2.05	0.75	0.674	1.05	0.639	0.80	1.30	2.000	No
927	60.83	3.70	1.65	2.05	0.75	0.674	1.05	0.639	0.80	1.30	2.000	No
928	60.91	3.70	1.65	2.05	0.75	0.674	1.05	0.639	0.80	1.30	2.000	No
929	60.97	3.71	1.65	2.05	0.75	0.673	1.05	0.639	0.80	1.30	2.000	No
930	61.03	3.71	1.65	2.05	0.74	0.673	1.05	0.638	0.80	1.30	2.000	No
931	61.10	3.71	1.66	2.06	0.74	0.673	1.05	0.638	0.80	1.30	2.000	No
932	61.16	3.72	1.66	2.06	0.74	0.673	1.05	0.638	0.80	1.30	2.000	No
933	61.23	3.72	1.66	2.06	0.74	0.672	1.05	0.638	0.80	1.30	2.000	No
934	61.32	3.73	1.66	2.06	0.74	0.672	1.05	0.637	0.80	1.30	2.000	No
935	61.38	3.73	1.67	2.07	0.74	0.672	1.05	0.637	0.80	1.30	2.000	No
936	61.43	3.74	1.67	2.07	0.74	0.672	1.05	0.637	0.80	1.30	2.000	No
937	61.52	3.74	1.67	2.07	0.74	0.671	1.05	0.637	0.80	1.30	2.000	No
938	61.56	3.74	1.67	2.07	0.74	0.671	1.05	0.637	0.80	1.30	2.000	No
939	61.62	3.75	1.67	2.08	0.74	0.671	1.05	0.636	0.80	1.30	2.000	No
940	61.71	3.75	1.68	2.08	0.74	0.671	1.05	0.636	0.80	1.30	2.000	No
941	61.77	3.76	1.68	2.08	0.74	0.670	1.05	0.636	0.80	1.30	2.000	No
942	61.84	3.76	1.68	2.08	0.74	0.670	1.05	0.636	0.80	1.30	2.000	No
943	61.92	3.77	1.68	2.09	0.74	0.670	1.05	0.635	0.80	1.30	2.000	No
944	61.94	3.77	1.68	2.09	0.74	0.670	1.05	0.635	0.80	1.30	2.000	No
945	62.02	3.78	1.69	2.09	0.74	0.669	1.05	0.635	0.80	1.30	2.000	No
946	62.12	3.78	1.69	2.09	0.74	0.669	1.05	0.635	0.80	1.30	2.000	No
947	62.15	3.78	1.69	2.09	0.74	0.669	1.05	0.635	0.80	1.30	2.000	No
948	62.22	3.79	1.69	2.10	0.74	0.669	1.05	0.634	0.79	1.30	2.000	No
949	62.27	3.79	1.69	2.10	0.74	0.669	1.05	0.634	0.79	1.30	2.000	No
950	62.36	3.80	1.70	2.10	0.74	0.668	1.05	0.634	0.80	1.30	2.000	No
951	62.41	3.80	1.70	2.10	0.74	0.668	1.05	0.634	0.80	1.30	2.000	No
952	62.48	3.81	1.70	2.11	0.74	0.668	1.05	0.633	0.80	1.30	2.000	No
953	62.55	3.81	1.70	2.11	0.74	0.668	1.05	0.633	0.80	1.30	2.000	No
954	62.61	3.81	1.70	2.11	0.74	0.667	1.05	0.633	0.81	1.30	2.000	No
955	62.69	3.82	1.71	2.11	0.74	0.667	1.05	0.633	0.81	1.30	2.000	No
956	62.74	3.82	1.71	2.11	0.74	0.667	1.05	0.633	0.81	1.30	2.000	No
957	62.81	3.83	1.71	2.12	0.74	0.667	1.05	0.632	0.81	1.30	2.000	No
958	62.87	3.83	1.71	2.12	0.74	0.666	1.05	0.632	0.81	1.30	2.000	No
959	62.95	3.84	1.71	2.12	0.74	0.666	1.05	0.632	0.81	1.30	2.000	No
960	63.00	3.84	1.72	2.12	0.74	0.666	1.05	0.632	0.81	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
961	63.10	3.85	1.72	2.13	0.74	0.666	1.05	0.631	0.80	1.30	2.000	No
962	63.13	3.85	1.72	2.13	0.74	0.666	1.05	0.631	0.80	1.30	2.000	No
963	63.19	3.85	1.72	2.13	0.74	0.665	1.05	0.631	0.80	1.30	2.000	No
964	63.26	3.86	1.72	2.13	0.73	0.665	1.05	0.631	0.80	1.30	2.000	No
965	63.32	3.86	1.73	2.13	0.73	0.665	1.05	0.631	0.81	1.30	2.000	No
966	63.39	3.86	1.73	2.14	0.73	0.665	1.05	0.630	0.82	1.30	2.000	No
967	63.49	3.87	1.73	2.14	0.73	0.664	1.05	0.630	0.82	1.30	2.000	No
968	63.52	3.87	1.73	2.14	0.73	0.664	1.05	0.630	0.83	1.30	2.000	No
969	63.60	3.88	1.73	2.14	0.73	0.664	1.05	0.630	0.84	1.30	2.000	No
970	63.69	3.88	1.74	2.15	0.73	0.664	1.05	0.629	0.84	1.30	2.000	No
971	63.74	3.89	1.74	2.15	0.73	0.663	1.05	0.629	0.84	1.30	2.000	No
972	63.79	3.89	1.74	2.15	0.73	0.663	1.05	0.629	0.84	1.30	2.000	No
973	63.85	3.89	1.74	2.15	0.73	0.663	1.05	0.629	0.84	1.30	2.000	No
974	63.92	3.90	1.74	2.15	0.73	0.663	1.05	0.629	0.85	1.30	2.000	No
975	63.99	3.90	1.75	2.16	0.73	0.663	1.05	0.628	0.86	1.30	2.000	No
976	64.05	3.91	1.75	2.16	0.73	0.662	1.05	0.628	0.86	1.30	2.000	No
977	64.13	3.91	1.75	2.16	0.73	0.662	1.05	0.628	0.87	1.30	2.000	No
978	64.18	3.92	1.75	2.16	0.73	0.662	1.05	0.628	0.87	1.30	2.000	No
979	64.24	3.92	1.75	2.17	0.73	0.662	1.05	0.628	0.87	1.30	2.000	No
980	64.34	3.93	1.76	2.17	0.73	0.661	1.05	0.627	0.87	1.30	2.000	No
981	64.39	3.93	1.76	2.17	0.73	0.661	1.05	0.627	0.87	1.30	2.000	No
982	64.45	3.93	1.76	2.17	0.73	0.661	1.05	0.627	0.87	1.30	2.000	No
983	64.51	3.94	1.76	2.17	0.73	0.661	1.05	0.627	0.87	1.30	2.000	No
984	64.59	3.94	1.77	2.18	0.73	0.661	1.05	0.627	0.87	1.30	2.000	No
985	64.64	3.95	1.77	2.18	0.73	0.660	1.05	0.626	0.87	1.30	2.000	No
986	64.73	3.95	1.77	2.18	0.73	0.660	1.05	0.626	0.86	1.30	2.000	No
987	64.78	3.95	1.77	2.18	0.73	0.660	1.05	0.626	0.86	1.30	2.000	No
988	64.83	3.96	1.77	2.18	0.73	0.660	1.05	0.626	0.85	1.30	2.000	No
989	64.93	3.96	1.78	2.19	0.73	0.660	1.05	0.625	0.84	1.30	2.000	No
990	64.98	3.97	1.78	2.19	0.73	0.659	1.05	0.625	0.84	1.30	2.000	No
991	65.03	3.97	1.78	2.19	0.73	0.659	1.05	0.625	0.83	1.30	2.000	No
992	65.12	3.98	1.78	2.19	0.73	0.659	1.05	0.625	0.82	1.30	2.000	No
993	65.17	3.98	1.78	2.20	0.73	0.659	1.05	0.625	0.81	1.30	2.000	No
994	65.23	3.98	1.79	2.20	0.73	0.658	1.05	0.624	0.81	1.30	2.000	No
995	65.31	3.99	1.79	2.20	0.73	0.658	1.05	0.624	0.80	1.30	2.000	No
996	65.36	3.99	1.79	2.20	0.73	0.658	1.05	0.624	0.80	1.30	2.000	No
997	65.42	4.00	1.79	2.21	0.73	0.658	1.05	0.624	0.80	1.30	2.000	No
998	65.50	4.00	1.79	2.21	0.72	0.658	1.05	0.624	0.81	1.30	2.000	No
999	65.58	4.01	1.80	2.21	0.72	0.657	1.05	0.623	0.82	1.30	2.000	No
1000	65.63	4.01	1.80	2.21	0.72	0.657	1.05	0.623	0.82	1.30	2.000	No
1001	65.72	4.02	1.80	2.22	0.72	0.657	1.05	0.623	0.82	1.30	2.000	No
1002	65.77	4.02	1.80	2.22	0.72	0.657	1.05	0.623	0.81	1.30	2.000	No
1003	65.83	4.02	1.80	2.22	0.72	0.656	1.05	0.623	0.81	1.30	2.000	No
1004	65.92	4.03	1.81	2.22	0.72	0.656	1.05	0.622	0.81	1.30	2.000	No
1005	65.97	4.03	1.81	2.22	0.72	0.656	1.05	0.622	0.81	1.30	2.000	No
1006	66.02	4.04	1.81	2.23	0.72	0.656	1.05	0.622	0.81	1.30	2.000	No
1007	66.11	4.04	1.81	2.23	0.72	0.655	1.05	0.622	0.81	1.30	2.000	No
1008	66.16	4.04	1.81	2.23	0.72	0.655	1.05	0.621	0.80	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1009	66.22	4.05	1.82	2.23	0.72	0.655	1.05	0.621	0.79	1.30	2.000	No
1010	66.30	4.05	1.82	2.24	0.72	0.655	1.05	0.621	0.78	1.30	2.000	No
1011	66.35	4.06	1.82	2.24	0.72	0.655	1.05	0.621	0.78	1.30	2.000	No
1012	66.42	4.06	1.82	2.24	0.72	0.654	1.05	0.621	0.78	1.30	2.000	No
1013	66.50	4.07	1.83	2.24	0.72	0.654	1.05	0.620	0.77	1.30	2.000	No
1014	66.55	4.07	1.83	2.24	0.72	0.654	1.05	0.620	0.78	1.30	2.000	No
1015	66.61	4.07	1.83	2.25	0.72	0.654	1.05	0.620	0.77	1.30	2.000	No
1016	66.70	4.08	1.83	2.25	0.72	0.653	1.05	0.620	0.78	1.30	2.000	No
1017	66.76	4.08	1.83	2.25	0.72	0.653	1.05	0.620	0.80	1.30	2.000	No
1018	66.80	4.09	1.83	2.25	0.72	0.653	1.05	0.619	0.81	1.30	2.000	No
1019	66.88	4.09	1.84	2.25	0.72	0.653	1.05	0.619	0.83	1.30	2.000	No
1020	66.96	4.10	1.84	2.26	0.72	0.653	1.05	0.619	0.85	1.30	2.000	No
1021	67.01	4.10	1.84	2.26	0.72	0.652	1.05	0.619	0.87	1.30	2.000	No
1022	67.06	4.10	1.84	2.26	0.72	0.652	1.05	0.619	0.88	1.30	2.000	No
1023	67.13	4.11	1.84	2.26	0.72	0.652	1.05	0.618	0.89	1.30	2.000	No
1024	67.19	4.11	1.85	2.26	0.72	0.652	1.05	0.618	0.90	1.30	2.000	No
1025	67.29	4.12	1.85	2.27	0.72	0.652	1.05	0.618	0.90	1.30	2.000	No
1026	67.35	4.12	1.85	2.27	0.72	0.651	1.05	0.618	0.90	1.30	2.000	No
1027	67.40	4.12	1.85	2.27	0.72	0.651	1.05	0.618	0.90	1.30	2.000	No
1028	67.50	4.13	1.86	2.27	0.72	0.651	1.05	0.617	0.91	1.30	2.000	No
1029	67.55	4.13	1.86	2.27	0.72	0.651	1.05	0.617	0.91	1.30	2.000	No
1030	67.60	4.14	1.86	2.28	0.72	0.651	1.05	0.617	0.91	1.30	2.000	No
1031	67.68	4.14	1.86	2.28	0.72	0.651	1.05	0.617	0.92	1.30	2.000	No
1032	67.73	4.14	1.86	2.28	0.72	0.650	1.05	0.617	0.92	1.30	2.000	No
1033	67.79	4.15	1.87	2.28	0.71	0.650	1.05	0.617	0.92	1.30	2.000	No
1034	67.87	4.15	1.87	2.28	0.71	0.650	1.05	0.617	0.92	1.30	2.000	No
1035	67.93	4.16	1.87	2.29	0.71	0.650	1.05	0.616	0.92	1.30	2.000	No
1036	67.98	4.16	1.87	2.29	0.71	0.650	1.05	0.616	0.92	1.30	2.000	No
1037	68.05	4.16	1.87	2.29	0.71	0.650	1.05	0.616	0.92	1.30	2.000	No
1038	68.11	4.17	1.88	2.29	0.71	0.649	1.05	0.616	0.91	1.30	2.000	No
1039	68.19	4.17	1.88	2.29	0.71	0.649	1.05	0.616	0.90	1.30	2.000	No
1040	68.25	4.17	1.88	2.30	0.71	0.649	1.05	0.615	0.89	1.30	2.000	No
1041	68.34	4.18	1.88	2.30	0.71	0.649	1.05	0.615	0.91	1.30	2.000	No
1042	68.39	4.18	1.88	2.30	0.71	0.649	1.05	0.615	0.88	1.30	2.000	No
1043	68.44	4.19	1.89	2.30	0.71	0.648	1.05	0.615	0.86	1.30	2.000	No
1044	68.54	4.19	1.89	2.30	0.71	0.648	1.05	0.615	0.80	1.30	2.000	No
1045	68.59	4.20	1.89	2.31	0.71	0.648	1.05	0.615	0.78	1.30	2.000	No
1046	68.64	4.20	1.89	2.31	0.71	0.648	1.05	0.614	0.77	1.30	2.000	No
1047	68.71	4.20	1.89	2.31	0.71	0.648	1.05	0.614	0.79	1.30	2.000	No
1048	68.77	4.21	1.90	2.31	0.71	0.647	1.05	0.614	0.83	1.30	2.000	No
1049	68.84	4.21	1.90	2.31	0.71	0.647	1.05	0.614	0.77	1.30	2.000	No
1050	68.91	4.22	1.90	2.32	0.71	0.647	1.05	0.614	0.77	1.30	2.000	No
1051	68.97	4.22	1.90	2.32	0.71	0.647	1.05	0.613	0.76	1.30	2.000	No
1052	69.04	4.22	1.90	2.32	0.71	0.647	1.05	0.613	0.76	1.30	2.000	No
1053	69.12	4.23	1.91	2.32	0.71	0.646	1.05	0.613	0.76	1.30	2.000	No
1054	69.17	4.23	1.91	2.32	0.71	0.646	1.05	0.613	0.76	1.30	2.000	No
1055	69.27	4.24	1.91	2.33	0.71	0.646	1.05	0.613	0.76	1.30	2.000	No
1056	69.29	4.24	1.91	2.33	0.71	0.646	1.05	0.612	0.76	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1057	69.37	4.25	1.91	2.33	0.71	0.646	1.05	0.612	0.79	1.30	2.000	No
1058	69.42	4.25	1.92	2.33	0.71	0.645	1.05	0.612	0.80	1.30	2.000	No
1059	69.52	4.25	1.92	2.34	0.71	0.645	1.05	0.612	0.82	1.30	2.000	No
1060	69.57	4.26	1.92	2.34	0.71	0.645	1.05	0.612	0.83	1.30	2.000	No
1061	69.65	4.26	1.92	2.34	0.71	0.645	1.05	0.611	0.84	1.30	2.000	No
1062	69.71	4.27	1.93	2.34	0.71	0.645	1.05	0.611	0.85	1.30	2.000	No
1063	69.77	4.27	1.93	2.34	0.71	0.644	1.05	0.611	0.85	1.30	2.000	No
1064	69.85	4.28	1.93	2.35	0.71	0.644	1.05	0.611	0.85	1.30	2.000	No
1065	69.89	4.28	1.93	2.35	0.71	0.644	1.05	0.611	0.85	1.30	2.000	No
1066	69.96	4.28	1.93	2.35	0.71	0.644	1.05	0.611	0.85	1.30	2.000	No
1067	70.02	4.29	1.93	2.35	0.71	0.644	1.05	0.610	0.84	1.30	2.000	No
1068	70.09	4.29	1.94	2.35	0.71	0.643	1.05	0.610	0.84	1.30	2.000	No
1069	70.15	4.29	1.94	2.36	0.70	0.643	1.05	0.610	0.84	1.30	2.000	No
1070	70.24	4.30	1.94	2.36	0.70	0.643	1.05	0.610	0.84	1.30	2.000	No
1071	70.30	4.30	1.94	2.36	0.70	0.643	1.05	0.610	0.83	1.30	2.000	No
1072	70.36	4.31	1.95	2.36	0.70	0.642	1.05	0.609	0.83	1.30	2.000	No
1073	70.44	4.31	1.95	2.37	0.70	0.642	1.05	0.609	0.83	1.30	2.000	No
1074	70.48	4.32	1.95	2.37	0.70	0.642	1.05	0.609	0.84	1.30	2.000	No
1075	70.55	4.32	1.95	2.37	0.70	0.642	1.05	0.609	0.84	1.30	2.000	No
1076	70.60	4.32	1.95	2.37	0.70	0.642	1.05	0.609	0.84	1.30	2.000	No
1077	70.69	4.33	1.96	2.37	0.70	0.641	1.05	0.608	0.83	1.30	2.000	No
1078	70.74	4.33	1.96	2.38	0.70	0.641	1.05	0.608	0.83	1.30	2.000	No
1079	70.83	4.34	1.96	2.38	0.70	0.641	1.05	0.608	0.83	1.30	2.000	No
1080	70.89	4.34	1.96	2.38	0.70	0.641	1.05	0.608	0.83	1.30	2.000	No
1081	70.94	4.35	1.96	2.38	0.70	0.641	1.05	0.608	0.83	1.30	2.000	No
1082	71.02	4.35	1.97	2.38	0.70	0.640	1.05	0.607	0.83	1.30	2.000	No
1083	71.08	4.35	1.97	2.39	0.70	0.640	1.05	0.607	0.83	1.30	2.000	No
1084	71.14	4.36	1.97	2.39	0.70	0.640	1.05	0.607	0.83	1.30	2.000	No
1085	71.22	4.36	1.97	2.39	0.70	0.640	1.05	0.607	0.84	1.30	2.000	No
1086	71.27	4.37	1.97	2.39	0.70	0.640	1.05	0.607	0.84	1.30	2.000	No
1087	71.33	4.37	1.98	2.40	0.70	0.639	1.05	0.606	0.85	1.30	2.000	No
1088	71.40	4.38	1.98	2.40	0.70	0.639	1.05	0.606	0.85	1.30	2.000	No
1089	71.47	4.38	1.98	2.40	0.70	0.639	1.05	0.606	0.85	1.30	2.000	No
1090	71.53	4.38	1.98	2.40	0.70	0.639	1.05	0.606	0.85	1.30	2.000	No
1091	71.63	4.39	1.99	2.40	0.70	0.638	1.05	0.605	0.86	1.30	2.000	No
1092	71.67	4.39	1.99	2.41	0.70	0.638	1.05	0.605	0.86	1.30	2.000	No
1093	71.73	4.40	1.99	2.41	0.70	0.638	1.05	0.605	0.86	1.30	2.000	No
1094	71.81	4.40	1.99	2.41	0.70	0.638	1.05	0.605	0.86	1.30	2.000	No
1095	71.88	4.41	1.99	2.41	0.70	0.638	1.05	0.605	0.84	1.30	2.000	No
1096	71.93	4.41	1.99	2.41	0.70	0.637	1.05	0.605	0.82	1.30	2.000	No
1097	71.99	4.41	2.00	2.42	0.70	0.637	1.05	0.604	0.80	1.30	2.000	No
1098	72.05	4.42	2.00	2.42	0.70	0.637	1.05	0.604	0.78	1.30	2.000	No
1099	72.13	4.42	2.00	2.42	0.70	0.637	1.05	0.604	0.76	1.30	2.000	No
1100	72.18	4.43	2.00	2.42	0.70	0.637	1.05	0.604	0.75	1.30	2.000	No
1101	72.27	4.43	2.01	2.43	0.70	0.636	1.05	0.603	0.75	1.30	2.000	No
1102	72.32	4.43	2.01	2.43	0.70	0.636	1.05	0.603	0.75	1.30	2.000	No
1103	72.38	4.44	2.01	2.43	0.70	0.636	1.05	0.603	0.75	1.30	2.000	No
1104	72.46	4.44	2.01	2.43	0.70	0.636	1.05	0.603	0.75	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1105	72.52	4.45	2.01	2.43	0.70	0.636	1.05	0.603	0.75	1.30	2.000	No
1106	72.62	4.45	2.02	2.44	0.69	0.635	1.05	0.602	0.76	1.30	2.000	No
1107	72.66	4.46	2.02	2.44	0.69	0.635	1.05	0.602	0.75	1.30	2.000	No
1108	72.71	4.46	2.02	2.44	0.69	0.635	1.05	0.602	0.75	1.30	2.000	No
1109	72.82	4.47	2.02	2.44	0.69	0.635	1.05	0.602	0.75	1.30	2.000	No
1110	72.85	4.47	2.02	2.45	0.69	0.634	1.05	0.602	0.75	1.30	2.000	No
1111	72.91	4.47	2.03	2.45	0.69	0.634	1.05	0.602	0.75	1.30	2.000	No
1112	72.97	4.48	2.03	2.45	0.69	0.634	1.05	0.601	0.75	1.30	2.000	No
1113	73.06	4.48	2.03	2.45	0.69	0.634	1.05	0.601	0.75	1.30	2.000	No
1114	73.11	4.49	2.03	2.45	0.69	0.634	1.05	0.601	0.75	1.30	2.000	No
1115	73.17	4.49	2.03	2.46	0.69	0.633	1.05	0.601	0.75	1.30	2.000	No
1116	73.24	4.49	2.04	2.46	0.69	0.633	1.05	0.601	0.75	1.30	2.000	No
1117	73.31	4.50	2.04	2.46	0.69	0.633	1.05	0.600	0.75	1.30	2.000	No
1118	73.37	4.50	2.04	2.46	0.69	0.633	1.05	0.600	0.75	1.30	2.000	No
1119	73.43	4.51	2.04	2.46	0.69	0.633	1.05	0.600	0.75	1.30	2.000	No
1120	73.51	4.51	2.04	2.47	0.69	0.632	1.05	0.600	0.75	1.30	2.000	No
1121	73.56	4.51	2.05	2.47	0.69	0.632	1.05	0.600	0.75	1.30	2.000	No
1122	73.65	4.52	2.05	2.47	0.69	0.632	1.05	0.599	0.75	1.30	2.000	No
1123	73.71	4.52	2.05	2.47	0.69	0.632	1.05	0.599	0.75	1.30	2.000	No
1124	73.76	4.53	2.05	2.48	0.69	0.632	1.05	0.599	0.74	1.30	2.000	No
1125	73.84	4.53	2.05	2.48	0.69	0.631	1.05	0.599	0.74	1.30	2.000	No
1126	73.90	4.54	2.06	2.48	0.69	0.631	1.05	0.599	0.74	1.30	2.000	No
1127	73.95	4.54	2.06	2.48	0.69	0.631	1.05	0.598	0.74	1.30	2.000	No
1128	74.06	4.55	2.06	2.49	0.69	0.631	1.05	0.598	0.74	1.30	2.000	No
1129	74.10	4.55	2.06	2.49	0.69	0.630	1.05	0.598	0.74	1.30	2.000	No
1130	74.15	4.55	2.06	2.49	0.69	0.630	1.05	0.598	0.74	1.30	2.000	No
1131	74.22	4.56	2.07	2.49	0.69	0.630	1.05	0.598	0.74	1.30	2.000	No
1132	74.29	4.56	2.07	2.49	0.69	0.630	1.05	0.597	0.74	1.30	2.000	No
1133	74.35	4.57	2.07	2.50	0.69	0.630	1.05	0.597	0.74	1.30	2.000	No
1134	74.43	4.57	2.07	2.50	0.69	0.629	1.05	0.597	0.74	1.30	2.000	No
1135	74.48	4.57	2.07	2.50	0.69	0.629	1.05	0.597	0.74	1.30	2.000	No
1136	74.54	4.58	2.08	2.50	0.69	0.629	1.05	0.597	0.83	1.30	2.000	No
1137	74.64	4.58	2.08	2.51	0.69	0.629	1.05	0.596	0.77	1.30	2.000	No
1138	74.69	4.59	2.08	2.51	0.69	0.629	1.05	0.596	0.79	1.30	2.000	No
1139	74.75	4.59	2.08	2.51	0.69	0.628	1.05	0.596	0.80	1.30	2.000	No
1140	74.83	4.60	2.09	2.51	0.69	0.628	1.05	0.596	0.82	1.30	2.000	No
1141	74.87	4.60	2.09	2.51	0.69	0.628	1.05	0.596	0.83	1.30	2.000	No
1142	74.94	4.60	2.09	2.52	0.69	0.628	1.05	0.596	0.84	1.30	2.000	No
1143	75.02	4.61	2.09	2.52	0.69	0.628	1.05	0.595	0.84	1.30	2.000	No
1144	75.08	4.61	2.09	2.52	0.68	0.627	1.05	0.595	0.84	1.30	2.000	No
1145	75.13	4.62	2.09	2.52	0.68	0.627	1.05	0.595	0.84	1.30	2.000	No
1146	75.22	4.62	2.10	2.52	0.68	0.627	1.05	0.595	0.84	1.30	2.000	No
1147	75.28	4.62	2.10	2.53	0.68	0.627	1.05	0.595	0.74	1.30	2.000	No
1148	75.33	4.63	2.10	2.53	0.68	0.627	1.05	0.595	0.74	1.30	2.000	No
1149	75.42	4.63	2.10	2.53	0.68	0.627	1.05	0.595	0.74	1.30	2.000	No
1150	75.47	4.63	2.11	2.53	0.68	0.627	1.05	0.595	0.74	1.30	2.000	No
1151	75.53	4.64	2.11	2.53	0.68	0.627	1.05	0.594	0.74	1.30	2.000	No
1152	75.62	4.64	2.11	2.53	0.68	0.627	1.05	0.594	0.74	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR_{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	7.73	99.61	2.96	0.57	1.70	12.42	0.00	12.42	4.000	No	Yes	2.00
2	0.16	10.44	97.13	2.93	0.56	1.70	16.77	0.00	16.77	4.000	No	Yes	2.00
3	0.20	10.04	100.00	3.05	0.56	1.70	16.13	0.00	16.13	4.000	No	Yes	2.00
4	0.28	15.86	79.78	2.71	0.53	1.70	25.48	0.00	25.48	4.000	No	Yes	2.00
5	0.34	25.10	54.87	2.40	0.50	1.70	40.33	58.47	98.80	4.000	No	No	2.00
6	0.41	44.98	26.65	2.05	0.46	1.70	72.27	45.39	117.66	4.000	No	No	2.00
7	0.48	52.61	21.86	1.99	0.45	1.70	84.53	38.99	123.51	4.000	No	No	2.00
8	0.55	50.55	26.77	2.05	0.44	1.70	81.22	47.23	128.45	4.000	No	No	2.00
9	0.60	32.73	49.97	2.34	0.47	1.70	52.59	59.92	112.51	4.000	No	No	2.00
10	0.67	48.49	34.15	2.14	0.43	1.70	77.91	55.71	133.61	4.000	No	No	2.00
11	0.74	58.13	27.00	2.05	0.41	1.70	93.39	49.86	143.25	4.000	No	No	2.00
12	0.79	70.38	18.44	1.94	0.41	1.70	113.08	34.58	147.65	4.000	No	No	2.00
13	0.89	78.81	16.37	1.92	0.39	1.70	126.62	29.83	156.45	4.000	No	No	2.00
14	0.94	84.53	14.63	1.90	0.39	1.70	135.83	24.77	160.59	4.000	No	No	2.00
15	0.98	88.14	13.83	1.89	0.38	1.70	141.63	22.34	163.97	4.000	No	No	2.00
16	1.06	86.53	18.89	1.95	0.36	1.70	139.04	39.07	178.11	4.000	No	No	2.00
17	1.12	81.61	23.84	2.01	0.35	1.70	131.13	50.62	181.76	4.000	No	No	2.00
18	1.20	76.99	28.46	2.07	0.35	1.70	123.73	57.98	181.71	4.000	No	No	2.00
19	1.25	68.35	35.49	2.16	0.37	1.70	109.85	64.22	174.07	4.000	No	No	2.00
20	1.34	62.52	39.92	2.21	0.38	1.70	100.50	66.11	166.60	4.000	No	No	2.00
21	1.38	56.80	44.41	2.27	0.39	1.70	91.31	67.05	158.35	4.000	No	No	2.00
22	1.46	49.87	50.02	2.34	0.41	1.70	80.17	67.25	147.42	4.000	No	No	2.00
23	1.54	45.55	52.94	2.37	0.42	1.70	73.23	66.69	139.92	4.000	No	No	2.00
24	1.60	38.81	59.65	2.46	0.44	1.70	62.42	66.11	128.52	4.000	No	No	2.00
25	1.66	34.80	63.55	2.51	0.45	1.70	55.98	65.40	121.37	4.000	No	No	2.00
26	1.75	28.97	70.79	2.60	0.47	1.70	46.61	64.35	110.96	4.000	No	No	2.00
27	1.80	26.36	74.34	2.64	0.48	1.70	42.42	0.00	42.42	4.000	No	Yes	2.00
28	1.86	23.45	78.67	2.70	0.50	1.70	37.74	0.00	37.74	4.000	No	Yes	2.00
29	1.91	21.04	82.99	2.75	0.51	1.70	33.87	0.00	33.87	4.000	No	Yes	2.00
30	1.98	18.94	86.16	2.79	0.52	1.70	30.49	0.00	30.49	4.000	No	Yes	2.00
31	2.04	17.33	88.04	2.81	0.52	1.70	27.91	0.00	27.91	4.000	No	Yes	2.00
32	2.14	15.52	89.71	2.83	0.53	1.70	25.00	0.00	25.00	4.000	No	Yes	2.00
33	2.17	14.42	92.28	2.87	0.54	1.70	23.23	0.00	23.23	4.000	No	Yes	2.00
34	2.24	13.61	92.91	2.87	0.54	1.70	21.93	0.00	21.93	4.000	No	Yes	2.00
35	2.32	12.91	93.36	2.88	0.54	1.70	20.81	0.00	20.81	4.000	No	Yes	2.00
36	2.37	12.61	93.23	2.88	0.55	1.70	20.32	0.00	20.32	4.000	No	Yes	2.00
37	2.43	11.91	94.43	2.89	0.55	1.70	19.20	0.00	19.20	4.000	No	Yes	2.00
38	2.53	11.81	93.31	2.88	0.55	1.70	19.04	0.00	19.04	4.000	No	Yes	2.00
39	2.58	11.41	94.88	2.90	0.55	1.70	18.40	0.00	18.40	4.000	No	Yes	2.00
40	2.64	11.41	94.99	2.90	0.55	1.70	18.40	0.00	18.40	4.000	No	Yes	2.00
41	2.70	11.42	95.67	2.91	0.55	1.70	18.40	0.00	18.40	4.000	No	Yes	2.00
42	2.78	12.52	93.03	2.88	0.55	1.70	20.16	0.00	20.16	4.000	No	Yes	2.00
43	2.82	13.32	91.10	2.85	0.54	1.70	21.45	0.00	21.45	4.000	No	Yes	2.00
44	2.89	18.04	77.42	2.68	0.52	1.70	29.03	0.00	29.03	4.000	No	Yes	2.00
45	2.96	21.66	68.74	2.57	0.51	1.70	34.85	60.52	95.37	4.000	No	No	2.00
46	3.03	24.27	63.15	2.50	0.50	1.70	39.04	60.48	99.52	4.000	No	No	2.00
47	3.12	23.36	63.64	2.51	0.50	1.70	37.58	60.18	97.76	4.000	No	No	2.00
48	3.17	22.06	65.61	2.53	0.51	1.70	35.49	60.04	95.53	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	3.23	20.95	66.84	2.55	0.51	1.70	33.71	59.80	93.50	4.000	No	No	2.00
50	3.28	19.95	66.29	2.54	0.52	1.70	32.10	59.22	91.32	4.000	No	No	2.00
51	3.35	19.35	63.72	2.51	0.52	1.70	31.14	58.37	89.50	4.000	No	No	2.00
52	3.43	18.24	62.52	2.49	0.53	1.70	29.35	57.57	86.93	4.000	No	No	2.00
53	3.48	17.24	62.37	2.49	0.53	1.70	27.75	57.08	84.83	4.000	No	No	2.00
54	3.56	16.54	60.38	2.47	0.54	1.70	26.62	56.28	82.90	4.000	No	No	2.00
55	3.61	16.23	59.35	2.45	0.54	1.70	26.12	55.87	81.99	4.000	No	No	2.00
56	3.68	16.95	57.26	2.43	0.54	1.70	27.26	55.61	82.88	4.000	No	No	2.00
57	3.77	18.75	52.35	2.37	0.53	1.70	30.16	54.86	85.01	4.000	No	No	2.00
58	3.82	20.47	48.25	2.32	0.53	1.70	32.90	54.02	86.92	4.000	No	No	2.00
59	3.87	22.38	44.64	2.27	0.52	1.70	35.97	53.17	89.14	4.000	No	No	2.00
60	3.96	23.98	41.36	2.23	0.52	1.70	38.54	52.05	90.59	4.000	No	No	2.00
61	4.02	24.49	39.86	2.21	0.52	1.70	39.36	51.33	90.70	4.000	No	No	2.00
62	4.11	24.89	39.36	2.20	0.52	1.70	40.01	51.17	91.17	4.000	No	No	2.00
63	4.16	25.49	38.43	2.19	0.52	1.70	40.97	50.78	91.75	4.000	No	No	2.00
64	4.21	25.90	37.88	2.19	0.52	1.70	41.61	50.55	92.16	4.000	No	No	2.00
65	4.27	27.71	35.02	2.15	0.51	1.70	44.52	49.05	93.57	4.000	No	No	2.00
66	4.35	24.80	40.90	2.22	0.52	1.70	39.84	52.09	91.94	4.000	No	No	2.00
67	4.40	29.82	32.23	2.12	0.51	1.70	47.91	47.29	95.20	4.000	No	No	2.00
68	4.47	33.93	27.64	2.06	0.50	1.70	54.51	43.44	97.96	4.000	No	No	2.00
69	4.55	35.54	26.94	2.05	0.50	1.70	57.10	43.00	100.10	4.000	No	No	2.00
70	4.61	37.05	25.94	2.04	0.49	1.70	59.53	42.02	101.55	4.000	No	No	2.00
71	4.68	38.35	25.84	2.04	0.49	1.70	61.61	42.25	103.86	4.000	No	No	2.00
72	4.75	38.85	26.68	2.05	0.49	1.70	62.42	43.63	106.05	4.000	No	No	2.00
73	4.80	38.95	27.35	2.05	0.48	1.70	62.58	44.59	107.17	4.000	No	No	2.00
74	4.86	38.45	29.09	2.08	0.48	1.70	61.78	46.70	108.47	4.000	No	No	2.00
75	4.93	37.85	30.36	2.09	0.48	1.70	60.81	48.01	108.83	4.000	No	No	2.00
76	5.00	36.85	31.67	2.11	0.48	1.70	59.20	49.12	108.33	4.000	No	No	2.00
77	5.05	35.14	33.72	2.13	0.48	1.70	56.46	50.56	107.02	4.000	No	No	2.00
78	5.14	32.43	37.25	2.18	0.49	1.70	52.10	52.54	104.65	4.000	No	No	2.00
79	5.19	32.33	36.93	2.17	0.49	1.70	51.94	52.26	104.20	4.000	No	No	2.00
80	5.28	32.93	35.57	2.16	0.49	1.70	52.91	51.40	104.31	4.000	No	No	2.00
81	5.34	34.14	33.75	2.13	0.49	1.70	54.85	50.23	105.08	4.000	No	No	2.00
82	5.38	35.74	31.52	2.11	0.49	1.70	57.42	48.59	106.01	4.000	No	No	2.00
83	5.45	37.75	29.10	2.08	0.48	1.70	60.65	46.49	107.14	4.000	No	No	2.00
84	5.54	41.56	25.23	2.03	0.48	1.70	66.77	42.23	109.01	4.000	No	No	2.00
85	5.59	43.77	23.06	2.00	0.48	1.70	70.32	39.13	109.46	4.000	No	No	2.00
86	5.65	45.28	21.96	1.99	0.48	1.70	72.75	37.41	110.16	4.000	No	No	2.00
87	5.73	45.88	21.88	1.99	0.47	1.70	73.71	37.41	111.13	4.000	No	No	2.00
88	5.79	45.28	22.91	2.00	0.47	1.70	72.75	39.23	111.98	4.000	No	No	2.00
89	5.84	43.47	24.91	2.02	0.47	1.70	69.84	42.25	112.09	4.000	No	No	2.00
90	5.94	39.56	29.47	2.08	0.47	1.70	63.56	47.52	111.08	4.000	No	No	2.00
91	5.99	36.85	32.63	2.12	0.48	1.70	59.20	50.10	109.31	4.000	No	No	2.00
92	6.04	35.34	34.63	2.15	0.48	1.70	56.78	51.46	108.24	4.000	No	No	2.00
93	6.12	29.82	44.29	2.27	0.49	1.70	47.91	56.01	103.92	4.000	No	No	2.00
94	6.19	26.81	51.00	2.35	0.50	1.70	43.07	57.81	100.89	4.000	No	No	2.00
95	6.24	24.60	56.40	2.42	0.50	1.70	39.52	58.74	98.26	4.000	No	No	2.00
96	6.31	21.08	64.57	2.52	0.51	1.70	33.87	59.34	93.21	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	6.37	20.08	66.64	2.55	0.52	1.70	32.26	59.34	91.60	4.000	No	No	2.00
98	6.44	18.37	71.52	2.61	0.52	1.70	29.51	0.00	29.51	4.000	No	Yes	2.00
99	6.52	17.07	77.43	2.68	0.53	1.70	27.43	0.00	27.43	4.000	No	Yes	2.00
100	6.58	16.77	79.92	2.71	0.53	1.70	26.94	0.00	26.94	4.000	No	Yes	2.00
101	6.64	16.77	80.90	2.72	0.53	1.70	26.94	0.00	26.94	4.000	No	Yes	2.00
102	6.72	17.87	80.91	2.72	0.52	1.70	28.71	0.00	28.71	4.000	No	Yes	2.00
103	6.78	19.68	77.58	2.68	0.52	1.68	31.32	0.00	31.32	4.000	No	Yes	2.00
104	6.84	22.19	72.67	2.62	0.51	1.66	34.89	0.00	34.89	4.000	No	Yes	2.00
105	6.92	24.60	67.97	2.56	0.50	1.64	38.12	61.31	99.43	4.000	No	No	2.00
106	6.98	26.81	63.97	2.51	0.49	1.62	41.07	61.25	102.32	4.000	No	No	2.00
107	7.03	28.41	61.60	2.48	0.49	1.61	43.22	61.27	104.49	4.000	No	No	2.00
108	7.09	37.65	48.00	2.31	0.47	1.57	55.80	59.89	115.68	4.000	No	No	2.00
109	7.18	49.60	34.63	2.15	0.44	1.53	71.57	54.76	126.34	4.000	No	No	2.00
110	7.22	52.11	32.19	2.11	0.44	1.52	74.81	52.99	127.80	4.000	No	No	2.00
111	7.33	56.11	27.31	2.05	0.44	1.51	80.00	47.82	127.82	4.000	No	No	2.00
112	7.38	56.42	26.42	2.04	0.44	1.51	80.31	46.53	126.84	4.000	No	No	2.00
113	7.43	56.01	26.41	2.04	0.45	1.50	79.61	46.38	126.00	4.000	No	No	2.00
114	7.52	54.82	27.56	2.06	0.45	1.50	77.68	47.75	125.43	4.000	No	No	2.00
115	7.58	54.42	28.05	2.06	0.45	1.49	76.88	48.29	125.16	4.000	No	No	2.00
116	7.62	54.32	28.28	2.07	0.45	1.49	76.53	48.54	125.08	4.000	No	No	2.00
117	7.72	55.32	27.93	2.06	0.45	1.48	77.42	48.22	125.64	4.000	No	No	2.00
118	7.76	56.72	27.26	2.05	0.45	1.47	79.03	47.56	126.59	4.000	No	No	2.00
119	7.82	58.43	26.95	2.05	0.44	1.46	80.80	47.43	128.23	4.000	No	No	2.00
120	7.90	61.04	23.39	2.00	0.44	1.46	84.30	42.00	126.30	4.000	No	No	2.00
121	7.97	62.75	21.21	1.98	0.45	1.46	86.66	37.93	124.60	4.000	No	No	2.00
122	8.02	64.56	20.50	1.97	0.45	1.46	88.79	36.65	125.44	0.185	No	No	0.33
123	8.07	65.96	20.03	1.96	0.45	1.45	90.22	35.74	125.96	0.186	No	No	0.33
124	8.16	67.17	19.96	1.96	0.44	1.44	91.25	35.73	126.98	0.189	No	No	0.33
125	8.21	65.26	21.48	1.98	0.44	1.43	88.41	38.77	127.19	0.189	No	No	0.33
126	8.27	64.56	22.16	1.99	0.44	1.43	87.25	40.04	127.29	0.190	No	No	0.33
127	8.35	68.07	19.71	1.96	0.44	1.42	91.55	35.16	126.71	0.188	No	No	0.33
128	8.41	68.57	19.25	1.95	0.45	1.42	92.12	34.10	126.22	0.187	No	No	0.32
129	8.49	67.47	20.16	1.96	0.45	1.42	90.24	36.05	126.29	0.187	No	No	0.32
130	8.55	65.06	21.84	1.99	0.45	1.41	86.74	39.29	126.02	0.186	No	No	0.32
131	8.62	61.54	24.44	2.02	0.45	1.41	81.83	43.51	125.34	0.184	No	No	0.31
132	8.67	57.63	27.63	2.06	0.45	1.41	76.54	47.63	124.16	0.181	No	No	0.31
133	8.76	51.50	33.57	2.13	0.45	1.40	68.33	53.02	121.35	0.174	No	No	0.29
134	8.80	47.99	37.38	2.18	0.46	1.40	63.71	55.35	119.06	0.169	No	No	0.28
135	8.86	44.17	41.72	2.23	0.47	1.41	58.73	57.22	115.95	0.163	No	No	0.27
136	8.95	37.55	49.63	2.33	0.48	1.41	50.16	59.14	109.29	0.151	No	No	0.25
137	8.99	33.33	55.33	2.40	0.49	1.42	44.73	59.83	104.56	0.144	No	No	0.23
138	9.06	30.22	59.57	2.46	0.50	1.42	40.65	59.99	100.64	0.138	No	No	0.22
139	9.15	28.21	61.16	2.48	0.50	1.42	37.94	59.66	97.60	0.134	No	No	0.22
140	9.22	26.91	61.90	2.49	0.51	1.42	36.19	59.36	95.55	0.132	No	No	0.21
141	9.26	26.10	62.26	2.49	0.51	1.42	35.07	59.13	94.21	0.130	No	No	0.21
142	9.35	26.20	60.27	2.47	0.51	1.42	35.07	58.62	93.69	0.130	No	No	0.21
143	9.40	27.21	57.60	2.43	0.51	1.41	36.28	58.21	94.48	0.131	No	No	0.21
144	9.46	27.81	55.34	2.40	0.51	1.41	36.95	57.70	94.64	0.131	No	No	0.21

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	9.54	26.71	55.73	2.41	0.51	1.40	35.43	57.40	92.83	0.129	No	No	0.20
146	9.60	25.40	58.14	2.44	0.52	1.40	33.66	57.64	91.29	0.127	No	No	0.20
147	9.66	24.70	59.00	2.45	0.52	1.40	32.68	57.61	90.29	0.126	No	No	0.20
148	9.72	22.69	60.01	2.46	0.53	1.40	30.06	57.15	87.21	0.123	No	No	0.19
149	9.80	20.68	61.43	2.48	0.54	1.40	27.42	56.76	84.18	0.120	No	No	0.18
150	9.85	18.57	66.94	2.55	0.54	1.40	24.65	57.21	81.86	0.118	No	No	0.18
151	9.96	15.26	78.65	2.70	0.55	1.40	20.26	0.00	20.26	4.000	No	Yes	2.00
152	10.00	14.56	81.59	2.73	0.55	1.40	19.31	0.00	19.31	4.000	No	Yes	2.00
153	10.05	12.95	88.00	2.81	0.56	1.40	17.18	0.00	17.18	4.000	No	Yes	2.00
154	10.12	13.35	86.98	2.80	0.56	1.40	17.64	0.00	17.64	4.000	No	Yes	2.00
155	10.18	13.05	88.36	2.82	0.56	1.39	17.20	0.00	17.20	4.000	No	Yes	2.00
156	10.27	13.15	88.28	2.82	0.56	1.39	17.25	0.00	17.25	4.000	No	Yes	2.00
157	10.33	13.65	86.75	2.80	0.56	1.38	17.83	0.00	17.83	4.000	No	Yes	2.00
158	10.37	13.96	86.44	2.79	0.56	1.38	18.18	0.00	18.18	4.000	No	Yes	2.00
159	10.47	15.36	83.51	2.76	0.55	1.37	19.85	0.00	19.85	4.000	No	Yes	2.00
160	10.53	16.36	80.90	2.72	0.55	1.36	21.04	0.00	21.04	4.000	No	Yes	2.00
161	10.57	17.37	78.56	2.69	0.54	1.36	22.25	0.00	22.25	4.000	No	Yes	2.00
162	10.67	18.98	75.41	2.66	0.54	1.34	24.12	0.00	24.12	4.000	No	Yes	2.00
163	10.70	20.08	72.68	2.62	0.54	1.34	25.44	0.00	25.44	4.000	No	Yes	2.00
164	10.78	21.79	68.46	2.57	0.53	1.33	27.43	58.31	85.74	0.121	No	No	0.18
165	10.83	23.29	64.95	2.52	0.53	1.33	29.19	58.09	87.28	0.123	No	No	0.18
166	10.91	25.40	60.01	2.46	0.52	1.32	31.63	57.59	89.21	0.125	No	No	0.18
167	10.97	27.41	55.86	2.41	0.52	1.31	33.96	57.04	91.00	0.127	No	No	0.18
168	11.03	28.71	52.70	2.37	0.52	1.31	35.44	56.40	91.84	0.128	No	No	0.19
169	11.10	30.02	49.86	2.34	0.51	1.30	36.90	55.73	92.63	0.129	No	No	0.19
170	11.17	31.73	46.91	2.30	0.51	1.29	38.83	54.98	93.80	0.130	No	No	0.19
171	11.26	32.92	45.35	2.28	0.51	1.29	40.09	54.56	94.65	0.131	No	No	0.19
172	11.31	33.62	44.46	2.27	0.51	1.28	40.83	54.31	95.14	0.131	No	No	0.19
173	11.36	34.13	43.91	2.26	0.51	1.28	41.34	54.15	95.49	0.132	No	No	0.19
174	11.44	34.43	43.81	2.26	0.51	1.28	41.55	54.15	95.71	0.132	No	No	0.19
175	11.50	34.53	43.88	2.26	0.51	1.27	41.56	54.19	95.75	0.132	No	No	0.19
176	11.56	34.63	44.08	2.26	0.51	1.27	41.56	54.29	95.85	0.132	No	No	0.19
177	11.63	34.53	44.50	2.27	0.51	1.27	41.33	54.45	95.78	0.132	No	No	0.19
178	11.69	34.33	44.97	2.27	0.51	1.26	40.98	54.60	95.59	0.132	No	No	0.19
179	11.76	34.13	45.31	2.28	0.51	1.26	40.64	54.68	95.33	0.132	No	No	0.19
180	11.86	33.22	47.01	2.30	0.51	1.25	39.41	55.17	94.58	0.131	No	No	0.18
181	11.89	33.02	47.49	2.31	0.51	1.25	39.13	55.31	94.44	0.131	No	No	0.18
182	11.95	32.42	48.95	2.32	0.51	1.25	38.33	55.73	94.06	0.130	No	No	0.18
183	12.01	31.52	50.84	2.35	0.51	1.25	37.20	56.19	93.38	0.129	No	No	0.18
184	12.10	31.21	50.96	2.35	0.51	1.24	36.71	56.10	92.82	0.129	No	No	0.18
185	12.15	31.11	51.05	2.35	0.51	1.24	36.53	56.09	92.62	0.129	No	No	0.18
186	12.21	31.41	50.49	2.34	0.51	1.24	36.79	55.94	92.73	0.129	No	No	0.18
187	12.28	31.92	49.73	2.33	0.51	1.23	37.26	55.77	93.02	0.129	No	No	0.18
188	12.36	33.52	47.28	2.30	0.51	1.23	38.96	55.18	94.14	0.130	No	No	0.18
189	12.40	34.73	45.47	2.28	0.51	1.23	40.26	54.66	94.92	0.131	No	No	0.18
190	12.47	35.93	43.38	2.25	0.51	1.22	41.52	53.92	95.44	0.132	No	No	0.18
191	12.55	38.04	40.10	2.21	0.51	1.22	43.79	52.55	96.34	0.133	No	No	0.18
192	12.60	39.25	38.33	2.19	0.51	1.21	45.07	51.69	96.76	0.133	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	12.69	41.06	36.29	2.17	0.50	1.21	46.94	50.61	97.55	0.134	No	No	0.18
194	12.74	42.27	35.09	2.15	0.50	1.21	48.19	49.93	98.13	0.135	No	No	0.18
195	12.82	44.07	33.72	2.13	0.50	1.20	50.06	49.15	99.21	0.136	No	No	0.19
196	12.88	45.18	33.16	2.13	0.50	1.20	51.15	48.88	100.03	0.137	No	No	0.19
197	12.94	46.08	32.65	2.12	0.50	1.19	52.03	48.58	100.62	0.138	No	No	0.19
198	13.00	46.68	32.56	2.12	0.50	1.19	52.57	48.61	101.18	0.139	No	No	0.19
199	13.09	46.99	33.17	2.13	0.49	1.19	52.71	49.22	101.93	0.140	No	No	0.19
200	13.14	46.89	33.55	2.13	0.49	1.18	52.49	49.54	102.03	0.140	No	No	0.19
201	13.20	46.89	33.81	2.14	0.49	1.18	52.37	49.75	102.12	0.140	No	No	0.19
202	13.27	46.89	35.08	2.15	0.49	1.18	52.19	50.82	103.01	0.142	No	No	0.19
203	13.34	46.89	35.77	2.16	0.49	1.17	52.04	51.37	103.41	0.142	No	No	0.19
204	13.39	46.79	36.22	2.17	0.49	1.17	51.85	51.69	103.53	0.142	No	No	0.19
205	13.47	46.58	37.24	2.18	0.49	1.17	51.44	52.38	103.82	0.143	No	No	0.19
206	13.54	46.38	38.13	2.19	0.49	1.17	51.09	52.96	104.05	0.143	No	No	0.19
207	13.59	45.98	39.19	2.20	0.49	1.16	50.54	53.57	104.11	0.143	No	No	0.19
208	13.65	45.67	40.27	2.22	0.49	1.16	50.10	54.19	104.29	0.143	No	No	0.19
209	13.72	45.37	41.35	2.23	0.49	1.16	49.64	54.76	104.40	0.143	No	No	0.19
210	13.79	45.27	42.21	2.24	0.49	1.15	49.41	55.22	104.63	0.144	No	No	0.19
211	13.85	45.17	40.97	2.22	0.49	1.15	49.21	54.42	103.63	0.142	No	No	0.19
212	13.94	45.57	36.22	2.17	0.50	1.15	49.59	51.17	100.76	0.138	No	No	0.18
213	13.98	45.77	36.65	2.17	0.50	1.15	49.70	51.53	101.24	0.139	No	No	0.18
214	14.08	46.06	37.70	2.18	0.49	1.14	49.83	52.35	102.18	0.140	No	No	0.18
215	14.13	46.06	37.86	2.19	0.49	1.14	49.74	52.45	102.19	0.140	No	No	0.18
216	14.18	45.96	38.16	2.19	0.49	1.14	49.55	52.62	102.17	0.140	No	No	0.18
217	14.27	44.75	38.80	2.20	0.50	1.14	48.13	52.73	100.87	0.139	No	No	0.18
218	14.33	44.45	38.63	2.20	0.50	1.14	47.73	52.52	100.25	0.138	No	No	0.18
219	14.39	43.02	39.95	2.21	0.50	1.13	46.16	53.03	99.19	0.136	No	No	0.18
220	14.44	41.21	42.15	2.24	0.50	1.13	44.16	53.89	98.05	0.135	No	No	0.17
221	14.53	38.00	46.18	2.29	0.51	1.13	40.65	55.11	95.76	0.132	No	No	0.17
222	14.59	35.39	49.79	2.33	0.51	1.13	37.83	55.94	93.78	0.130	No	No	0.17
223	14.64	32.78	54.19	2.39	0.52	1.13	35.02	56.80	91.81	0.128	No	No	0.16
224	14.73	28.16	63.58	2.51	0.53	1.13	30.05	58.03	88.08	0.124	No	No	0.16
225	14.77	26.76	66.77	2.55	0.53	1.13	28.54	58.29	86.83	0.122	No	No	0.16
226	14.83	21.74	77.79	2.68	0.54	1.13	23.21	0.00	23.21	4.000	No	Yes	2.00
227	14.93	18.02	87.04	2.80	0.55	1.13	19.23	0.00	19.23	4.000	No	Yes	2.00
228	14.98	16.52	90.96	2.85	0.56	1.12	17.61	0.00	17.61	4.000	No	Yes	2.00
229	15.03	15.31	94.49	2.89	0.56	1.12	16.31	0.00	16.31	4.000	No	Yes	2.00
230	15.10	14.11	98.68	2.95	0.56	1.12	15.01	0.00	15.01	4.000	No	Yes	2.00
231	15.17	13.20	100.00	2.99	0.57	1.12	14.02	0.00	14.02	4.000	No	Yes	2.00
232	15.22	12.40	100.00	3.03	0.57	1.12	13.15	0.00	13.15	4.000	No	Yes	2.00
233	15.29	11.50	100.00	3.08	0.57	1.12	12.18	0.00	12.18	4.000	No	Yes	2.00
234	15.37	11.60	100.00	3.08	0.57	1.11	12.25	0.00	12.25	4.000	No	Yes	2.00
235	15.44	11.60	100.00	3.09	0.57	1.11	12.22	0.00	12.22	4.000	No	Yes	2.00
236	15.52	11.70	100.00	3.10	0.57	1.11	12.29	0.00	12.29	4.000	No	Yes	2.00
237	15.56	11.90	100.00	3.10	0.57	1.10	12.48	0.00	12.48	4.000	No	Yes	2.00
238	15.62	12.00	100.00	3.09	0.57	1.10	12.55	0.00	12.55	4.000	No	Yes	2.00
239	15.70	12.20	100.00	3.07	0.57	1.10	12.72	0.00	12.72	4.000	No	Yes	2.00
240	15.76	12.20	100.00	3.06	0.57	1.10	12.69	0.00	12.69	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	15.82	12.30	100.00	3.05	0.57	1.09	12.77	0.00	12.77	4.000	No	Yes	2.00
242	15.91	12.40	100.00	3.04	0.57	1.09	12.83	0.00	12.83	4.000	No	Yes	2.00
243	15.95	12.60	100.00	3.02	0.57	1.09	13.02	0.00	13.02	4.000	No	Yes	2.00
244	16.01	12.60	100.00	3.01	0.57	1.09	12.99	0.00	12.99	4.000	No	Yes	2.00
245	16.08	12.70	100.00	3.01	0.57	1.08	13.06	0.00	13.06	4.000	No	Yes	2.00
246	16.14	12.80	100.00	3.01	0.57	1.08	13.14	0.00	13.14	4.000	No	Yes	2.00
247	16.22	13.20	100.00	3.01	0.57	1.08	13.51	0.00	13.51	4.000	No	Yes	2.00
248	16.31	14.01	100.00	2.99	0.57	1.07	14.28	0.00	14.28	4.000	No	Yes	2.00
249	16.36	14.91	99.98	2.96	0.56	1.07	15.16	0.00	15.16	4.000	No	Yes	2.00
250	16.41	16.01	96.87	2.92	0.56	1.07	16.24	0.00	16.24	4.000	No	Yes	2.00
251	16.50	18.12	91.85	2.86	0.55	1.07	18.31	0.00	18.31	4.000	No	Yes	2.00
252	16.55	19.63	88.47	2.82	0.55	1.06	19.79	0.00	19.79	4.000	No	Yes	2.00
253	16.61	21.13	84.74	2.77	0.55	1.06	21.25	0.00	21.25	4.000	No	Yes	2.00
254	16.69	23.64	78.59	2.69	0.54	1.06	23.69	0.00	23.69	4.000	No	Yes	2.00
255	16.74	25.15	75.21	2.65	0.54	1.06	25.15	0.00	25.15	4.000	No	Yes	2.00
256	16.80	27.26	70.97	2.60	0.53	1.05	27.18	58.71	85.90	0.122	No	No	0.15
257	16.88	29.37	66.85	2.55	0.53	1.05	29.20	58.50	87.70	0.123	No	No	0.15
258	16.95	31.78	62.76	2.50	0.52	1.05	31.51	58.25	89.76	0.125	No	No	0.15
259	17.00	33.48	60.09	2.46	0.52	1.05	33.13	58.03	91.16	0.127	No	No	0.15
260	17.07	35.29	57.27	2.43	0.52	1.04	34.83	57.71	92.54	0.128	No	No	0.16
261	17.15	36.00	56.45	2.42	0.51	1.04	35.44	57.63	93.07	0.129	No	No	0.16
262	17.20	36.50	55.79	2.41	0.51	1.04	35.87	57.55	93.42	0.129	No	No	0.16
263	17.26	37.11	54.95	2.40	0.51	1.04	36.40	57.42	93.83	0.130	No	No	0.16
264	17.33	37.31	55.30	2.40	0.51	1.03	36.52	57.57	94.09	0.130	No	No	0.16
265	17.41	37.51	55.71	2.41	0.51	1.03	36.63	57.73	94.36	0.131	No	No	0.16
266	17.46	37.61	55.94	2.41	0.51	1.03	36.67	57.81	94.48	0.131	No	No	0.16
267	17.52	37.61	56.35	2.42	0.51	1.03	36.60	57.92	94.52	0.131	No	No	0.16
268	17.60	37.31	57.23	2.43	0.51	1.03	36.22	58.08	94.31	0.130	No	No	0.16
269	17.65	37.42	57.35	2.43	0.51	1.02	36.27	58.13	94.40	0.131	No	No	0.16
270	17.74	38.22	56.75	2.42	0.51	1.02	36.94	58.14	95.08	0.131	No	No	0.16
271	17.80	38.72	56.42	2.42	0.51	1.02	37.36	58.15	95.52	0.132	No	No	0.16
272	17.85	39.53	55.81	2.41	0.51	1.02	38.08	58.16	96.24	0.133	No	No	0.16
273	17.93	40.83	54.91	2.40	0.50	1.02	39.24	58.18	97.42	0.134	No	No	0.16
274	17.99	41.84	54.62	2.40	0.50	1.01	40.13	58.33	98.46	0.135	No	No	0.16
275	18.07	43.44	53.68	2.38	0.50	1.01	41.57	58.40	99.98	0.137	No	No	0.16
276	18.13	44.85	52.95	2.37	0.50	1.01	42.85	58.49	101.33	0.139	No	No	0.17
277	18.18	45.85	52.65	2.37	0.49	1.01	43.73	58.62	102.35	0.141	No	No	0.17
278	18.29	47.16	51.64	2.36	0.49	1.01	44.85	58.54	103.38	0.142	No	No	0.17
279	18.32	48.06	51.29	2.35	0.49	1.00	45.66	58.62	104.28	0.143	No	No	0.17
280	18.38	49.17	51.49	2.36	0.49	1.00	46.64	58.96	105.60	0.145	No	No	0.17
281	18.44	50.17	51.21	2.35	0.48	1.00	47.51	59.08	106.59	0.147	No	No	0.17
282	18.53	51.27	51.18	2.35	0.48	1.00	48.42	59.31	107.74	0.149	No	No	0.18
283	18.58	51.99	50.94	2.35	0.48	1.00	49.03	59.38	108.41	0.150	No	No	0.18
284	18.66	49.48	53.98	2.39	0.48	1.00	46.57	59.86	106.43	0.146	No	No	0.17
285	18.71	53.80	49.73	2.33	0.48	0.99	50.55	59.28	109.83	0.152	No	No	0.18
286	18.81	55.51	48.28	2.32	0.47	0.99	52.03	59.03	111.06	0.154	No	No	0.18
287	18.85	56.82	47.17	2.30	0.47	0.99	53.19	58.82	112.01	0.156	No	No	0.18
288	18.90	58.02	46.18	2.29	0.47	0.99	54.25	58.60	112.85	0.157	No	No	0.19

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	19.01	60.13	44.00	2.26	0.47	0.99	56.07	57.91	113.98	0.159	No	No	0.19
290	19.06	61.03	42.76	2.25	0.47	0.99	56.83	57.39	114.22	0.160	No	No	0.19
291	19.11	61.33	42.05	2.24	0.47	0.98	57.04	57.01	114.04	0.159	No	No	0.19
292	19.16	61.53	41.27	2.23	0.47	0.98	57.14	56.54	113.69	0.159	No	No	0.19
293	19.26	61.73	39.52	2.21	0.47	0.98	57.18	55.39	112.57	0.157	No	No	0.18
294	19.30	61.73	38.93	2.20	0.47	0.98	57.13	54.97	112.10	0.156	No	No	0.18
295	19.36	61.73	38.37	2.19	0.47	0.98	57.03	54.54	111.57	0.155	No	No	0.18
296	19.45	60.53	39.37	2.20	0.48	0.98	55.79	54.95	110.74	0.153	No	No	0.18
297	19.50	59.02	40.62	2.22	0.48	0.97	54.32	55.44	109.76	0.152	No	No	0.18
298	19.58	56.21	42.79	2.25	0.48	0.97	51.62	56.11	107.72	0.148	No	No	0.17
299	19.64	54.51	44.18	2.26	0.48	0.97	49.98	56.47	106.45	0.147	No	No	0.17
300	19.69	53.30	45.34	2.28	0.49	0.97	48.80	56.78	105.58	0.145	No	No	0.17
301	19.78	50.69	48.07	2.31	0.49	0.97	46.30	57.44	103.73	0.143	No	No	0.17
302	19.84	50.29	50.01	2.34	0.49	0.96	45.85	58.16	104.01	0.143	No	No	0.17
303	19.90	47.48	55.26	2.40	0.49	0.96	43.22	59.39	102.61	0.141	No	No	0.16
304	19.95	46.47	58.68	2.45	0.49	0.96	42.24	60.18	102.42	0.141	No	No	0.16
305	20.03	45.07	61.83	2.49	0.49	0.96	40.88	60.67	101.55	0.140	No	No	0.16
306	20.08	41.86	66.52	2.54	0.50	0.96	37.90	60.93	98.83	0.136	No	No	0.16
307	20.16	40.85	68.90	2.57	0.50	0.96	36.91	61.15	98.05	0.135	No	No	0.16
308	20.25	40.04	71.33	2.60	0.50	0.95	36.09	0.00	36.09	4.000	No	Yes	2.00
309	20.30	39.34	72.73	2.62	0.51	0.95	35.41	0.00	35.41	4.000	No	Yes	2.00
310	20.35	39.14	73.33	2.63	0.51	0.95	35.18	0.00	35.18	4.000	No	Yes	2.00
311	20.45	42.05	70.22	2.59	0.50	0.95	37.73	61.65	99.38	0.137	No	No	0.16
312	20.50	43.05	69.19	2.58	0.50	0.95	38.58	61.69	100.27	0.138	No	No	0.16
313	20.54	42.85	69.50	2.58	0.50	0.95	38.36	61.69	100.05	0.138	No	No	0.16
314	20.62	46.16	65.80	2.54	0.49	0.95	41.26	61.74	103.00	0.141	No	No	0.16
315	20.69	47.37	64.47	2.52	0.49	0.94	42.28	61.72	104.00	0.143	No	No	0.16
316	20.74	47.37	63.65	2.51	0.49	0.94	42.22	61.51	103.73	0.143	No	No	0.16
317	20.83	48.77	61.48	2.48	0.49	0.94	43.39	61.28	104.67	0.144	No	No	0.17
318	20.88	49.88	60.09	2.46	0.49	0.94	44.33	61.17	105.50	0.145	No	No	0.17
319	20.94	50.88	57.51	2.43	0.49	0.94	45.16	60.64	105.80	0.146	No	No	0.17
320	21.04	50.98	55.76	2.41	0.49	0.94	45.13	60.08	105.21	0.145	No	No	0.17
321	21.08	51.89	54.92	2.40	0.49	0.94	45.90	60.01	105.90	0.146	No	No	0.17
322	21.14	51.38	55.51	2.41	0.49	0.93	45.37	60.06	105.43	0.145	No	No	0.17
323	21.23	50.69	57.42	2.43	0.49	0.93	44.66	60.48	105.13	0.145	No	No	0.17
324	21.28	50.49	58.71	2.45	0.49	0.93	44.42	60.80	105.22	0.145	No	No	0.17
325	21.33	50.59	59.36	2.45	0.49	0.93	44.46	61.00	105.46	0.145	No	No	0.17
326	21.42	50.59	59.92	2.46	0.49	0.93	44.37	61.13	105.50	0.145	No	No	0.17
327	21.48	50.69	60.06	2.46	0.49	0.93	44.40	61.18	105.58	0.145	No	No	0.17
328	21.53	51.69	59.43	2.46	0.48	0.93	45.23	61.23	106.46	0.147	No	No	0.17
329	21.62	52.19	59.94	2.46	0.48	0.92	45.58	61.48	107.06	0.147	No	No	0.17
330	21.68	52.49	60.37	2.47	0.48	0.92	45.80	61.66	107.46	0.148	No	No	0.17
331	21.73	54.50	59.36	2.45	0.48	0.92	47.52	61.85	109.38	0.151	No	No	0.17
332	21.79	58.41	56.86	2.42	0.47	0.92	50.92	62.03	112.95	0.157	No	No	0.18
333	21.86	61.72	55.01	2.40	0.46	0.92	53.77	62.19	115.96	0.163	No	No	0.19
334	21.92	63.73	54.43	2.39	0.46	0.92	55.49	62.45	117.95	0.167	No	No	0.19
335	22.00	67.85	52.44	2.37	0.45	0.92	59.06	62.66	121.72	0.175	No	No	0.20
336	22.05	71.06	50.53	2.34	0.45	0.92	61.84	62.62	124.45	0.182	No	No	0.21

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	22.12	72.77	49.66	2.33	0.45	0.92	63.25	62.61	125.86	0.186	No	No	0.21
338	22.22	79.90	45.19	2.28	0.44	0.92	69.44	61.97	131.41	0.202	No	No	0.23
339	22.27	81.40	44.55	2.27	0.43	0.92	70.69	61.92	132.61	0.206	No	No	0.24
340	22.32	85.72	42.19	2.24	0.43	0.92	74.45	61.40	135.85	0.218	No	No	0.25
341	22.38	89.84	40.20	2.21	0.42	0.92	78.02	60.89	138.91	0.230	No	No	0.27
342	22.47	95.06	38.01	2.19	0.42	0.92	82.51	60.26	142.77	0.248	No	No	0.29
343	22.52	97.97	36.83	2.17	0.41	0.92	85.02	59.83	144.85	0.258	No	No	0.30
344	22.59	101.78	35.31	2.15	0.41	0.92	88.27	59.16	147.43	0.273	No	No	0.32
345	22.65	103.99	34.37	2.14	0.41	0.92	90.13	58.63	148.76	0.281	No	No	0.33
346	22.71	104.80	34.04	2.14	0.40	0.92	90.73	58.43	149.16	0.283	No	No	0.33
347	22.77	102.59	35.20	2.15	0.41	0.91	88.68	59.15	147.82	0.275	No	No	0.32
348	22.85	98.17	37.29	2.18	0.41	0.91	84.63	60.15	144.78	0.258	No	No	0.30
349	22.90	94.96	39.10	2.20	0.42	0.91	81.71	60.95	142.66	0.247	No	No	0.28
350	22.98	91.84	41.42	2.23	0.42	0.91	78.85	61.97	140.82	0.238	No	No	0.27
351	23.06	91.74	41.66	2.23	0.42	0.91	78.64	62.08	140.72	0.238	No	No	0.27
352	23.10	92.45	41.41	2.23	0.42	0.91	79.19	62.04	141.24	0.240	No	No	0.28
353	23.17	94.15	41.72	2.23	0.41	0.91	80.61	62.61	143.21	0.250	No	No	0.29
354	23.24	94.15	43.11	2.25	0.41	0.90	80.52	63.51	144.03	0.254	No	No	0.29
355	23.32	92.75	45.43	2.28	0.41	0.90	79.20	64.59	143.79	0.253	No	No	0.29
356	23.37	92.60	46.60	2.29	0.41	0.90	79.01	65.20	144.21	0.255	No	No	0.29
357	23.45	92.60	49.03	2.33	0.41	0.90	78.92	66.44	145.36	0.261	No	No	0.30
358	23.51	92.45	49.60	2.33	0.41	0.90	78.70	66.66	145.36	0.261	No	No	0.30
359	23.56	93.46	49.21	2.33	0.41	0.90	79.50	66.68	146.18	0.266	No	No	0.30
360	23.63	97.17	47.39	2.30	0.40	0.90	82.65	66.57	149.22	0.284	No	No	0.33
361	23.71	101.08	45.37	2.28	0.40	0.90	85.97	66.28	152.25	0.304	No	No	0.35
362	23.77	107.81	41.80	2.23	0.39	0.90	91.78	65.41	157.19	0.345	No	No	0.40
363	23.84	112.43	39.38	2.20	0.39	0.90	95.73	64.53	160.26	0.374	No	No	0.43
364	23.89	116.75	37.16	2.18	0.38	0.90	99.42	63.47	162.89	0.403	No	No	0.47
365	23.95	119.66	34.98	2.15	0.38	0.90	101.82	61.88	163.70	0.413	No	No	0.48
366	24.05	122.88	31.85	2.11	0.38	0.90	104.36	58.87	163.23	0.408	No	No	0.47
367	24.09	123.08	31.18	2.10	0.38	0.90	104.41	58.03	162.44	0.398	No	No	0.46
368	24.15	122.98	30.59	2.09	0.39	0.90	104.16	57.20	161.37	0.386	No	No	0.45
369	24.24	120.67	30.56	2.09	0.39	0.89	101.93	56.70	158.63	0.358	No	No	0.41
370	24.30	118.06	31.03	2.10	0.39	0.89	99.51	56.81	156.31	0.337	No	No	0.39
371	24.37	113.74	32.28	2.12	0.40	0.89	95.62	57.53	153.14	0.311	No	No	0.36
372	24.42	111.63	32.36	2.12	0.40	0.89	93.65	57.20	150.85	0.295	No	No	0.34
373	24.48	110.93	31.99	2.11	0.40	0.89	92.91	56.60	149.51	0.286	No	No	0.33
374	24.54	110.33	31.81	2.11	0.41	0.88	92.25	56.26	148.51	0.279	No	No	0.32
375	24.61	106.41	33.34	2.13	0.41	0.88	88.75	57.25	146.00	0.264	No	No	0.30
376	24.71	96.77	37.45	2.18	0.42	0.88	80.31	59.27	139.58	0.233	No	No	0.26
377	24.76	88.74	41.27	2.23	0.43	0.87	73.34	60.51	133.85	0.210	No	No	0.24
378	24.81	80.91	45.20	2.28	0.44	0.87	66.58	61.24	127.81	0.191	No	No	0.21
379	24.90	69.26	51.62	2.36	0.46	0.86	56.57	61.67	118.24	0.168	No	No	0.19
380	24.96	62.04	56.29	2.42	0.47	0.86	50.42	61.71	112.12	0.156	No	No	0.17
381	25.00	55.21	61.60	2.48	0.48	0.86	44.66	61.67	106.33	0.146	No	No	0.16
382	25.09	46.78	69.44	2.58	0.50	0.85	37.58	61.45	99.04	0.136	No	No	0.15
383	25.16	42.06	75.04	2.65	0.51	0.85	33.64	0.00	33.64	4.000	No	Yes	2.00
384	25.20	38.04	80.74	2.72	0.52	0.84	30.31	0.00	30.31	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	25.30	32.42	90.11	2.84	0.53	0.84	25.69	0.00	25.69	4.000	No	Yes	2.00
386	25.36	30.51	93.57	2.88	0.53	0.84	24.11	0.00	24.11	4.000	No	Yes	2.00
387	25.40	29.91	94.78	2.90	0.53	0.83	23.60	0.00	23.60	4.000	No	Yes	2.00
388	25.48	31.52	91.63	2.86	0.53	0.83	24.85	0.00	24.85	4.000	No	Yes	2.00
389	25.53	33.42	88.18	2.81	0.53	0.83	26.36	0.00	26.36	4.000	No	Yes	2.00
390	25.59	36.03	83.56	2.76	0.52	0.83	28.43	0.00	28.43	4.000	No	Yes	2.00
391	25.67	38.84	79.96	2.71	0.52	0.84	30.66	0.00	30.66	4.000	No	Yes	2.00
392	25.75	38.54	80.97	2.72	0.52	0.83	30.36	0.00	30.36	4.000	No	Yes	2.00
393	25.80	36.94	83.60	2.76	0.52	0.83	29.04	0.00	29.04	4.000	No	Yes	2.00
394	25.87	36.99	84.58	2.77	0.52	0.83	29.04	0.00	29.04	4.000	No	Yes	2.00
395	25.95	37.04	86.52	2.79	0.52	0.83	29.04	0.00	29.04	4.000	No	Yes	2.00
396	25.99	41.15	82.03	2.74	0.51	0.83	32.33	0.00	32.33	4.000	No	Yes	2.00
397	26.09	54.31	70.48	2.59	0.48	0.84	43.00	63.24	106.23	0.146	No	No	0.16
398	26.14	64.75	62.08	2.49	0.47	0.84	51.56	63.75	115.31	0.162	No	No	0.18
399	26.19	69.06	59.17	2.45	0.46	0.84	55.08	63.91	118.99	0.169	No	No	0.19
400	26.27	83.02	49.52	2.33	0.44	0.85	66.64	63.44	130.07	0.198	No	No	0.22
401	26.33	89.65	45.88	2.29	0.43	0.85	72.13	63.03	135.16	0.215	No	No	0.24
402	26.39	95.27	43.53	2.26	0.42	0.85	76.80	62.84	139.64	0.233	No	No	0.26
403	26.45	102.09	41.08	2.23	0.41	0.85	82.50	62.62	145.12	0.260	No	No	0.29
404	26.53	105.21	40.21	2.22	0.41	0.86	85.04	62.60	147.64	0.274	No	No	0.31
405	26.59	105.81	40.06	2.21	0.41	0.85	85.46	62.59	148.05	0.276	No	No	0.31
406	26.64	100.69	42.45	2.24	0.41	0.85	81.06	63.21	144.26	0.255	No	No	0.28
407	26.73	91.95	46.77	2.30	0.42	0.85	73.57	63.89	137.46	0.224	No	No	0.25
408	26.79	85.43	50.50	2.34	0.43	0.84	68.04	64.25	132.30	0.205	No	No	0.23
409	26.86	76.09	56.42	2.42	0.45	0.84	60.19	64.44	124.63	0.182	No	No	0.20
410	26.93	69.77	60.61	2.47	0.46	0.83	54.90	64.28	119.18	0.170	No	No	0.19
411	26.99	63.04	65.42	2.53	0.47	0.83	49.32	63.96	113.28	0.158	No	No	0.17
412	27.08	53.50	73.23	2.63	0.49	0.82	41.49	0.00	41.49	4.000	No	Yes	2.00
413	27.13	49.08	77.72	2.68	0.50	0.82	37.89	0.00	37.89	4.000	No	Yes	2.00
414	27.17	45.77	81.38	2.73	0.50	0.81	35.22	0.00	35.22	4.000	No	Yes	2.00
415	27.25	42.66	84.79	2.77	0.51	0.81	32.69	0.00	32.69	4.000	No	Yes	2.00
416	27.32	40.05	87.17	2.80	0.51	0.81	30.57	0.00	30.57	4.000	No	Yes	2.00
417	27.38	34.13	94.16	2.89	0.53	0.80	25.88	0.00	25.88	4.000	No	Yes	2.00
418	27.44	31.31	95.84	2.91	0.53	0.80	23.65	0.00	23.65	4.000	No	Yes	2.00
419	27.53	28.90	95.63	2.91	0.54	0.80	21.73	0.00	21.73	4.000	No	Yes	2.00
420	27.58	28.20	96.09	2.91	0.54	0.79	21.17	0.00	21.17	4.000	No	Yes	2.00
421	27.63	27.80	96.73	2.92	0.54	0.79	20.84	0.00	20.84	4.000	No	Yes	2.00
422	27.71	29.21	95.09	2.90	0.54	0.79	21.89	0.00	21.89	4.000	No	Yes	2.00
423	27.77	32.12	91.17	2.85	0.53	0.79	24.11	0.00	24.11	4.000	No	Yes	2.00
424	27.82	25.69	100.00	3.01	0.55	0.79	19.14	0.00	19.14	4.000	No	Yes	2.00
425	27.90	50.39	69.54	2.58	0.50	0.80	38.31	61.69	100.00	0.137	No	No	0.15
426	27.97	60.63	60.94	2.47	0.48	0.81	46.41	61.99	108.40	0.150	No	No	0.16
427	28.02	73.18	52.02	2.36	0.46	0.82	56.46	61.80	118.25	0.168	No	No	0.18
428	28.12	99.79	37.23	2.18	0.43	0.83	78.01	58.56	136.56	0.220	No	No	0.24
429	28.17	109.42	32.87	2.12	0.42	0.83	85.82	56.10	141.92	0.243	No	No	0.27
430	28.23	115.25	30.75	2.10	0.41	0.83	90.53	54.60	145.13	0.260	No	No	0.29
431	28.31	116.15	30.41	2.09	0.41	0.83	91.14	54.29	145.42	0.261	No	No	0.29
432	28.37	112.74	31.74	2.11	0.41	0.83	88.26	55.33	143.59	0.252	No	No	0.28

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	28.42	106.61	34.47	2.14	0.42	0.83	83.19	57.20	140.39	0.236	No	No	0.26
434	28.51	95.57	40.55	2.22	0.43	0.82	74.11	60.20	134.31	0.212	No	No	0.23
435	28.55	87.24	45.29	2.28	0.44	0.82	67.29	61.47	128.77	0.194	No	No	0.21
436	28.61	78.70	51.46	2.36	0.45	0.81	60.34	62.61	122.96	0.178	No	No	0.19
437	28.71	65.95	63.70	2.51	0.47	0.80	50.07	63.75	113.82	0.159	No	No	0.17
438	28.76	57.32	71.30	2.60	0.48	0.80	43.18	0.00	43.18	4.000	No	Yes	2.00
439	28.81	49.29	79.53	2.71	0.50	0.79	36.85	0.00	36.85	4.000	No	Yes	2.00
440	28.91	36.94	92.53	2.87	0.52	0.78	27.24	0.00	27.24	4.000	No	Yes	2.00
441	28.95	35.83	93.31	2.88	0.53	0.78	26.37	0.00	26.37	4.000	No	Yes	2.00
442	29.00	35.78	93.03	2.88	0.53	0.78	26.30	0.00	26.30	4.000	No	Yes	2.00
443	29.07	35.73	92.97	2.87	0.53	0.78	26.23	0.00	26.23	4.000	No	Yes	2.00
444	29.16	39.15	88.36	2.82	0.52	0.78	28.78	0.00	28.78	4.000	No	Yes	2.00
445	29.21	43.16	83.16	2.75	0.51	0.78	31.82	0.00	31.82	4.000	No	Yes	2.00
446	29.30	49.39	75.95	2.66	0.50	0.78	36.56	0.00	36.56	4.000	No	Yes	2.00
447	29.36	51.29	73.85	2.64	0.50	0.78	37.99	0.00	37.99	4.000	No	Yes	2.00
448	29.41	57.22	67.61	2.56	0.49	0.79	42.55	62.52	105.07	0.144	No	No	0.15
449	29.50	69.16	57.64	2.43	0.47	0.79	51.84	62.53	114.38	0.160	No	No	0.17
450	29.56	75.79	52.27	2.37	0.46	0.80	57.02	62.05	119.07	0.169	No	No	0.18
451	29.61	82.52	47.41	2.31	0.45	0.80	62.29	61.29	123.59	0.180	No	No	0.19
452	29.69	86.73	40.96	2.22	0.45	0.80	65.39	58.36	123.76	0.180	No	No	0.19
453	29.76	83.12	43.55	2.26	0.45	0.80	62.49	59.26	121.75	0.175	No	No	0.19
454	29.80	76.59	48.28	2.32	0.46	0.79	57.31	60.41	117.73	0.167	No	No	0.18
455	29.89	64.14	57.73	2.43	0.48	0.78	47.50	61.36	108.86	0.150	No	No	0.16
456	29.93	54.71	66.31	2.54	0.49	0.78	40.17	61.54	101.71	0.140	No	No	0.15
457	30.00	46.07	75.61	2.66	0.51	0.77	33.54	0.00	33.54	4.000	No	Yes	2.00
458	30.06	34.33	91.26	2.85	0.53	0.76	24.67	0.00	24.67	4.000	No	Yes	2.00
459	30.13	31.62	94.59	2.89	0.54	0.76	22.62	0.00	22.62	4.000	No	Yes	2.00
460	30.21	28.19	99.45	2.96	0.55	0.75	20.07	0.00	20.07	4.000	No	Yes	2.00
461	30.27	24.68	100.00	3.03	0.55	0.75	17.47	0.00	17.47	4.000	No	Yes	2.00
462	30.36	23.67	100.00	3.02	0.56	0.75	16.71	0.00	16.71	4.000	No	Yes	2.00
463	30.41	23.47	100.00	3.01	0.56	0.75	16.55	0.00	16.55	4.000	No	Yes	2.00
464	30.46	22.77	100.00	3.00	0.56	0.74	16.02	0.00	16.02	4.000	No	Yes	2.00
465	30.55	21.77	100.00	3.00	0.56	0.74	15.27	0.00	15.27	4.000	No	Yes	2.00
466	30.60	21.67	100.00	2.99	0.56	0.74	15.19	0.00	15.19	4.000	No	Yes	2.00
467	30.65	21.47	100.00	2.99	0.56	0.74	15.03	0.00	15.03	4.000	No	Yes	2.00
468	30.73	21.06	100.00	3.01	0.56	0.74	14.71	0.00	14.71	4.000	No	Yes	2.00
469	30.80	20.96	100.00	3.01	0.56	0.74	14.62	0.00	14.62	4.000	No	Yes	2.00
470	30.85	20.76	100.00	3.01	0.57	0.74	14.46	0.00	14.46	4.000	No	Yes	2.00
471	30.95	20.56	100.00	3.02	0.57	0.74	14.30	0.00	14.30	4.000	No	Yes	2.00
472	30.99	20.36	100.00	3.03	0.57	0.73	14.14	0.00	14.14	4.000	No	Yes	2.00
473	31.05	20.46	100.00	3.03	0.57	0.73	14.20	0.00	14.20	4.000	No	Yes	2.00
474	31.15	20.46	100.00	3.03	0.57	0.73	14.17	0.00	14.17	4.000	No	Yes	2.00
475	31.18	20.46	100.00	3.03	0.57	0.73	14.17	0.00	14.17	4.000	No	Yes	2.00
476	31.23	20.46	100.00	3.04	0.57	0.73	14.15	0.00	14.15	4.000	No	Yes	2.00
477	31.30	20.76	100.00	3.03	0.57	0.73	14.35	0.00	14.35	4.000	No	Yes	2.00
478	31.39	20.76	100.00	3.04	0.57	0.73	14.32	0.00	14.32	4.000	No	Yes	2.00
479	31.45	20.76	100.00	3.05	0.57	0.73	14.31	0.00	14.31	4.000	No	Yes	2.00
480	31.50	20.67	100.00	3.06	0.57	0.73	14.22	0.00	14.22	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	31.58	20.67	100.00	3.06	0.57	0.73	14.20	0.00	14.20	4.000	No	Yes	2.00
482	31.64	20.67	100.00	3.06	0.57	0.73	14.19	0.00	14.19	4.000	No	Yes	2.00
483	31.70	20.67	100.00	3.06	0.57	0.73	14.17	0.00	14.17	4.000	No	Yes	2.00
484	31.78	20.47	100.00	3.08	0.57	0.72	14.01	0.00	14.01	4.000	No	Yes	2.00
485	31.84	20.27	100.00	3.09	0.57	0.72	13.86	0.00	13.86	4.000	No	Yes	2.00
486	31.90	20.07	100.00	3.11	0.57	0.72	13.70	0.00	13.70	4.000	No	Yes	2.00
487	31.96	20.57	100.00	3.10	0.57	0.72	14.04	0.00	14.04	4.000	No	Yes	2.00
488	32.03	21.17	100.00	3.10	0.57	0.72	14.44	0.00	14.44	4.000	No	Yes	2.00
489	32.09	21.17	100.00	3.10	0.57	0.72	14.42	0.00	14.42	4.000	No	Yes	2.00
490	32.19	22.58	100.00	3.04	0.56	0.72	15.39	0.00	15.39	4.000	No	Yes	2.00
491	32.24	23.48	100.00	3.01	0.56	0.72	16.01	0.00	16.01	4.000	No	Yes	2.00
492	32.32	22.09	100.00	3.05	0.56	0.72	15.00	0.00	15.00	4.000	No	Yes	2.00
493	32.39	20.09	100.00	3.12	0.57	0.72	13.58	0.00	13.58	4.000	No	Yes	2.00
494	32.43	19.59	100.00	3.13	0.57	0.71	13.22	0.00	13.22	4.000	No	Yes	2.00
495	32.48	19.49	100.00	3.13	0.57	0.71	13.14	0.00	13.14	4.000	No	Yes	2.00
496	32.55	19.79	100.00	3.11	0.57	0.71	13.33	0.00	13.33	4.000	No	Yes	2.00
497	32.62	19.79	100.00	3.09	0.57	0.71	13.32	0.00	13.32	4.000	No	Yes	2.00
498	32.69	19.39	100.00	3.09	0.57	0.71	13.02	0.00	13.02	4.000	No	Yes	2.00
499	32.78	19.39	100.00	3.10	0.57	0.71	13.00	0.00	13.00	4.000	No	Yes	2.00
500	32.82	19.39	100.00	3.10	0.57	0.71	12.99	0.00	12.99	4.000	No	Yes	2.00
501	32.88	19.59	100.00	3.08	0.57	0.71	13.12	0.00	13.12	4.000	No	Yes	2.00
502	32.97	19.99	100.00	3.08	0.57	0.71	13.37	0.00	13.37	4.000	No	Yes	2.00
503	33.02	20.19	100.00	3.08	0.57	0.71	13.50	0.00	13.50	4.000	No	Yes	2.00
504	33.08	20.69	100.00	3.08	0.57	0.71	13.83	0.00	13.83	4.000	No	Yes	2.00
505	33.17	21.50	100.00	3.05	0.57	0.71	14.37	0.00	14.37	4.000	No	Yes	2.00
506	33.21	21.80	100.00	3.05	0.56	0.71	14.56	0.00	14.56	4.000	No	Yes	2.00
507	33.29	22.50	100.00	3.05	0.56	0.71	15.03	0.00	15.03	4.000	No	Yes	2.00
508	33.37	23.40	100.00	3.04	0.56	0.71	15.63	0.00	15.63	4.000	No	Yes	2.00
509	33.41	23.30	100.00	3.05	0.56	0.71	15.55	0.00	15.55	4.000	No	Yes	2.00
510	33.47	23.50	100.00	3.06	0.56	0.71	15.67	0.00	15.67	4.000	No	Yes	2.00
511	33.56	23.50	100.00	3.06	0.56	0.70	15.65	0.00	15.65	4.000	No	Yes	2.00
512	33.61	24.31	100.00	3.05	0.56	0.71	16.19	0.00	16.19	4.000	No	Yes	2.00
513	33.68	24.11	100.00	3.06	0.56	0.70	16.04	0.00	16.04	4.000	No	Yes	2.00
514	33.77	24.91	100.00	3.05	0.56	0.70	16.56	0.00	16.56	4.000	No	Yes	2.00
515	33.82	25.21	100.00	3.05	0.56	0.70	16.76	0.00	16.76	4.000	No	Yes	2.00
516	33.87	26.51	100.00	3.02	0.55	0.70	17.64	0.00	17.64	4.000	No	Yes	2.00
517	33.97	29.63	99.92	2.96	0.55	0.71	19.78	0.00	19.78	4.000	No	Yes	2.00
518	34.01	31.23	97.59	2.93	0.54	0.71	20.88	0.00	20.88	4.000	No	Yes	2.00
519	34.08	31.43	97.68	2.93	0.54	0.71	20.99	0.00	20.99	4.000	No	Yes	2.00
520	34.13	29.33	100.00	2.97	0.55	0.70	19.52	0.00	19.52	4.000	No	Yes	2.00
521	34.19	26.11	100.00	3.05	0.56	0.70	17.27	0.00	17.27	4.000	No	Yes	2.00
522	34.27	22.40	100.00	3.15	0.56	0.70	14.71	0.00	14.71	4.000	No	Yes	2.00
523	34.36	20.59	100.00	3.18	0.57	0.69	13.46	0.00	13.46	4.000	No	Yes	2.00
524	34.41	19.39	100.00	3.20	0.57	0.69	12.64	0.00	12.64	4.000	No	Yes	2.00
525	34.46	15.37	100.00	3.35	0.58	0.68	9.94	0.00	9.94	4.000	No	Yes	2.00
526	34.54	18.58	100.00	3.21	0.57	0.69	12.07	0.00	12.07	4.000	No	Yes	2.00
527	34.60	18.38	100.00	3.21	0.57	0.69	11.92	0.00	11.92	4.000	No	Yes	2.00
528	34.65	18.38	100.00	3.21	0.57	0.69	11.91	0.00	11.91	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	34.73	18.38	100.00	3.21	0.57	0.69	11.89	0.00	11.89	4.000	No	Yes	2.00
530	34.80	18.28	100.00	3.21	0.58	0.68	11.81	0.00	11.81	4.000	No	Yes	2.00
531	34.85	18.09	100.00	3.21	0.58	0.68	11.67	0.00	11.67	4.000	No	Yes	2.00
532	34.92	17.89	100.00	3.22	0.58	0.68	11.52	0.00	11.52	4.000	No	Yes	2.00
533	34.98	18.09	100.00	3.21	0.58	0.68	11.65	0.00	11.65	4.000	No	Yes	2.00
534	35.04	17.89	100.00	3.22	0.58	0.68	11.50	0.00	11.50	4.000	No	Yes	2.00
535	35.12	18.09	100.00	3.21	0.58	0.68	11.62	0.00	11.62	4.000	No	Yes	2.00
536	35.17	18.39	100.00	3.20	0.58	0.68	11.81	0.00	11.81	4.000	No	Yes	2.00
537	35.25	18.39	100.00	3.19	0.58	0.68	11.79	0.00	11.79	4.000	No	Yes	2.00
538	35.32	18.59	100.00	3.19	0.57	0.68	11.91	0.00	11.91	4.000	No	Yes	2.00
539	35.37	18.69	100.00	3.20	0.57	0.68	11.97	0.00	11.97	4.000	No	Yes	2.00
540	35.44	19.20	100.00	3.19	0.57	0.68	12.29	0.00	12.29	4.000	No	Yes	2.00
541	35.50	20.60	100.00	3.16	0.57	0.68	13.20	0.00	13.20	4.000	No	Yes	2.00
542	35.60	23.61	100.00	3.09	0.56	0.68	15.19	0.00	15.19	4.000	No	Yes	2.00
543	35.65	24.62	100.00	3.08	0.56	0.68	15.85	0.00	15.85	4.000	No	Yes	2.00
544	35.70	26.22	100.00	3.04	0.56	0.68	16.91	0.00	16.91	4.000	No	Yes	2.00
545	35.79	28.03	100.00	3.01	0.55	0.68	18.11	0.00	18.11	4.000	No	Yes	2.00
546	35.85	27.83	100.00	3.01	0.55	0.68	17.96	0.00	17.96	4.000	No	Yes	2.00
547	35.90	26.73	100.00	3.03	0.56	0.68	17.20	0.00	17.20	4.000	No	Yes	2.00
548	35.98	24.52	100.00	3.08	0.56	0.68	15.70	0.00	15.70	4.000	No	Yes	2.00
549	36.03	24.01	100.00	3.09	0.56	0.68	15.34	0.00	15.34	4.000	No	Yes	2.00
550	36.09	24.57	100.00	3.08	0.56	0.68	15.70	0.00	15.70	4.000	No	Yes	2.00
551	36.18	23.21	100.00	3.12	0.56	0.67	14.78	0.00	14.78	4.000	No	Yes	2.00
552	36.24	24.62	100.00	3.08	0.56	0.68	15.70	0.00	15.70	4.000	No	Yes	2.00
553	36.29	25.62	100.00	3.06	0.56	0.68	16.35	0.00	16.35	4.000	No	Yes	2.00
554	36.38	30.74	100.00	2.97	0.55	0.68	19.76	0.00	19.76	4.000	No	Yes	2.00
555	36.44	33.95	96.58	2.92	0.54	0.68	21.90	0.00	21.90	4.000	No	Yes	2.00
556	36.49	35.56	95.00	2.90	0.54	0.68	22.98	0.00	22.98	4.000	No	Yes	2.00
557	36.57	33.15	98.55	2.94	0.54	0.68	21.32	0.00	21.32	4.000	No	Yes	2.00
558	36.63	29.84	100.00	3.01	0.55	0.68	19.07	0.00	19.07	4.000	No	Yes	2.00
559	36.69	27.53	100.00	3.07	0.55	0.67	17.51	0.00	17.51	4.000	No	Yes	2.00
560	36.77	25.92	100.00	3.08	0.56	0.67	16.42	0.00	16.42	4.000	No	Yes	2.00
561	36.83	24.92	100.00	3.09	0.56	0.67	15.75	0.00	15.75	4.000	No	Yes	2.00
562	36.88	23.41	100.00	3.12	0.56	0.67	14.74	0.00	14.74	4.000	No	Yes	2.00
563	36.96	22.71	100.00	3.14	0.57	0.67	14.26	0.00	14.26	4.000	No	Yes	2.00
564	37.03	22.51	100.00	3.15	0.57	0.66	14.12	0.00	14.12	4.000	No	Yes	2.00
565	37.08	27.33	100.00	3.02	0.56	0.67	17.27	0.00	17.27	4.000	No	Yes	2.00
566	37.14	36.56	89.92	2.84	0.54	0.68	23.40	0.00	23.40	4.000	No	Yes	2.00
567	37.23	54.64	70.73	2.60	0.50	0.69	35.76	61.17	96.93	0.134	No	No	0.14
568	37.28	61.16	66.62	2.55	0.49	0.70	40.30	61.65	101.95	0.140	No	No	0.15
569	37.36	56.34	73.58	2.63	0.50	0.69	36.92	0.00	36.92	4.000	No	Yes	2.00
570	37.41	48.31	83.36	2.75	0.51	0.69	31.33	0.00	31.33	4.000	No	Yes	2.00
571	37.48	41.07	91.63	2.86	0.53	0.68	26.36	0.00	26.36	4.000	No	Yes	2.00
572	37.57	32.84	100.00	2.99	0.54	0.67	20.80	0.00	20.80	4.000	No	Yes	2.00
573	37.63	28.12	100.00	3.07	0.55	0.66	17.65	0.00	17.65	4.000	No	Yes	2.00
574	37.66	26.21	100.00	3.11	0.56	0.66	16.38	0.00	16.38	4.000	No	Yes	2.00
575	37.77	23.30	100.00	3.15	0.57	0.66	14.47	0.00	14.47	4.000	No	Yes	2.00
576	37.82	22.30	100.00	3.16	0.57	0.66	13.81	0.00	13.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
577	37.88	21.90	100.00	3.16	0.57	0.65	13.54	0.00	13.54	4.000	No	Yes	2.00
578	37.96	22.00	100.00	3.13	0.57	0.65	13.59	0.00	13.59	4.000	No	Yes	2.00
579	38.01	22.60	100.00	3.10	0.57	0.65	13.96	0.00	13.96	4.000	No	Yes	2.00
580	38.06	22.50	100.00	3.09	0.57	0.65	13.89	0.00	13.89	4.000	No	Yes	2.00
581	38.13	22.90	100.00	3.04	0.57	0.65	14.13	0.00	14.13	4.000	No	Yes	2.00
582	38.19	23.40	100.00	3.02	0.57	0.65	14.44	0.00	14.44	4.000	No	Yes	2.00
583	38.26	23.60	100.00	3.04	0.56	0.65	14.55	0.00	14.55	4.000	No	Yes	2.00
584	38.32	23.31	100.00	3.05	0.57	0.65	14.35	0.00	14.35	4.000	No	Yes	2.00
585	38.41	22.61	100.00	3.08	0.57	0.65	13.88	0.00	13.88	4.000	No	Yes	2.00
586	38.46	19.60	100.00	3.20	0.57	0.65	11.96	0.00	11.96	4.000	No	Yes	2.00
587	38.52	24.82	100.00	3.06	0.56	0.65	15.27	0.00	15.27	4.000	No	Yes	2.00
588	38.59	25.72	100.00	3.07	0.56	0.65	15.83	0.00	15.83	4.000	No	Yes	2.00
589	38.65	26.83	100.00	3.07	0.56	0.65	16.54	0.00	16.54	4.000	No	Yes	2.00
590	38.73	30.04	100.00	3.02	0.55	0.66	18.60	0.00	18.60	4.000	No	Yes	2.00
591	38.79	33.95	99.25	2.95	0.54	0.66	21.14	0.00	21.14	4.000	No	Yes	2.00
592	38.86	42.79	88.69	2.82	0.53	0.67	26.96	0.00	26.96	4.000	No	Yes	2.00
593	38.92	51.32	80.56	2.72	0.51	0.67	32.71	0.00	32.71	4.000	No	Yes	2.00
594	38.98	59.96	73.31	2.63	0.50	0.68	38.59	0.00	38.59	4.000	No	Yes	2.00
595	39.06	72.71	64.63	2.52	0.48	0.69	47.50	63.25	110.75	0.153	No	No	0.16
596	39.12	81.14	59.93	2.46	0.46	0.70	53.50	63.70	117.20	0.165	No	No	0.17
597	39.18	89.98	55.09	2.40	0.45	0.70	59.87	63.88	123.75	0.180	No	No	0.19
598	39.28	106.24	47.80	2.31	0.43	0.72	71.80	63.96	135.76	0.217	No	No	0.23
599	39.32	110.56	46.31	2.29	0.42	0.72	75.02	64.01	139.03	0.230	No	No	0.24
600	39.37	119.29	43.45	2.26	0.41	0.72	81.67	64.02	145.69	0.263	No	No	0.28
601	39.48	132.55	40.35	2.22	0.39	0.73	91.89	64.37	156.25	0.336	No	No	0.35
602	39.52	135.05	40.40	2.22	0.39	0.74	93.87	64.89	158.76	0.359	No	No	0.38
603	39.57	138.77	40.31	2.22	0.38	0.74	96.82	65.53	162.36	0.397	No	No	0.42
604	39.66	143.59	36.20	2.17	0.38	0.74	100.16	62.74	162.90	0.404	No	No	0.43
605	39.70	144.79	32.44	2.12	0.39	0.73	100.50	58.76	159.27	0.364	No	No	0.38
606	39.77	148.71	34.13	2.14	0.38	0.74	103.92	61.44	165.36	0.435	No	No	0.46
607	39.87	152.72	34.58	2.14	0.37	0.74	107.20	62.66	169.86	0.502	No	No	0.53
608	39.92	156.74	34.21	2.14	0.37	0.75	110.42	62.97	173.40	0.567	No	No	0.60
609	39.98	161.86	33.35	2.13	0.36	0.75	114.49	62.87	177.36	0.656	No	No	0.70
610	40.06	119.99	52.03	2.36	0.40	0.72	82.07	68.68	150.75	0.294	No	No	0.31
611	40.12	171.18	33.73	2.13	0.35	0.76	122.31	65.04	187.35	0.995	No	No	1.06
612	40.16	175.99	33.17	2.13	0.34	0.76	126.28	65.22	191.49	1.210	No	No	1.29
613	40.25	182.11	33.34	2.13	0.33	0.76	131.51	66.58	198.08	1.701	No	No	1.80
614	40.31	182.30	34.39	2.14	0.33	0.76	131.80	67.92	199.73	1.863	No	No	1.97
615	40.37	181.40	35.13	2.15	0.33	0.76	131.09	68.63	199.72	1.862	No	No	1.97
616	40.44	178.39	36.20	2.17	0.33	0.76	128.56	69.24	197.81	1.675	No	No	1.77
617	40.50	175.48	37.05	2.18	0.34	0.76	126.10	69.56	195.66	1.494	No	No	1.58
618	40.56	172.97	37.66	2.18	0.34	0.76	123.95	69.67	193.61	1.345	No	No	1.43
619	40.63	169.15	38.50	2.19	0.34	0.75	120.70	69.70	190.41	1.148	No	No	1.22
620	40.71	166.94	38.60	2.19	0.35	0.75	118.71	69.33	188.04	1.027	No	No	1.09
621	40.77	163.53	39.38	2.20	0.35	0.75	115.85	69.34	185.19	0.903	No	No	0.96
622	40.86	159.61	40.40	2.22	0.35	0.75	112.55	69.41	181.97	0.787	No	No	0.84
623	40.90	156.50	41.30	2.23	0.36	0.74	110.00	69.51	179.51	0.713	No	No	0.76
624	40.96	152.79	42.22	2.24	0.36	0.74	106.93	69.46	176.39	0.632	No	No	0.67

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	41.03	146.66	43.93	2.26	0.37	0.74	101.94	69.42	171.36	0.528	No	No	0.56
626	41.09	142.95	44.90	2.27	0.37	0.73	98.91	69.29	168.20	0.475	No	No	0.50
627	41.15	139.23	46.00	2.29	0.38	0.73	95.91	69.20	165.11	0.431	No	No	0.45
628	41.24	134.91	46.40	2.29	0.39	0.72	92.34	68.52	160.87	0.381	No	No	0.40
629	41.28	131.60	47.37	2.30	0.39	0.72	89.71	68.39	158.11	0.353	No	No	0.37
630	41.35	129.19	47.95	2.31	0.39	0.72	87.76	68.20	155.96	0.334	No	No	0.35
631	41.41	124.99	49.27	2.33	0.40	0.71	84.44	68.01	152.45	0.306	No	No	0.32
632	41.50	122.48	49.92	2.34	0.40	0.71	82.42	67.80	150.21	0.290	No	No	0.30
633	41.55	119.87	50.81	2.35	0.41	0.71	80.38	67.68	148.06	0.277	No	No	0.29
634	41.61	116.86	51.67	2.36	0.41	0.71	78.02	67.43	145.45	0.261	No	No	0.27
635	41.71	114.25	52.20	2.36	0.42	0.70	75.93	67.10	143.04	0.249	No	No	0.26
636	41.75	112.95	52.63	2.37	0.42	0.70	74.83	66.99	141.82	0.243	No	No	0.25
637	41.80	111.44	53.26	2.38	0.42	0.70	73.66	66.93	140.59	0.237	No	No	0.25
638	41.87	109.94	53.88	2.39	0.42	0.70	72.48	66.87	139.34	0.232	No	No	0.24
639	41.93	108.23	54.73	2.40	0.42	0.70	71.17	66.84	138.01	0.226	No	No	0.24
640	42.00	105.32	56.14	2.41	0.43	0.69	68.97	66.76	135.73	0.217	No	No	0.23
641	42.09	102.51	57.41	2.43	0.43	0.69	66.84	66.61	133.45	0.209	No	No	0.22
642	42.14	100.60	58.29	2.44	0.44	0.69	65.40	66.51	131.91	0.204	No	No	0.21
643	42.20	99.09	58.97	2.45	0.44	0.69	64.26	66.41	130.67	0.200	No	No	0.21
644	42.29	96.98	59.87	2.46	0.44	0.68	62.65	66.24	128.89	0.194	No	No	0.20
645	42.34	96.18	60.23	2.47	0.44	0.68	62.03	66.18	128.21	0.192	No	No	0.20
646	42.39	95.28	60.73	2.47	0.44	0.68	61.35	66.13	127.48	0.190	No	No	0.20
647	42.48	94.47	61.21	2.48	0.44	0.68	60.70	66.09	126.79	0.188	No	No	0.20
648	42.54	94.37	61.22	2.48	0.44	0.68	60.58	66.06	126.63	0.188	No	No	0.20
649	42.59	94.57	60.87	2.47	0.44	0.68	60.67	65.98	126.65	0.188	No	No	0.20
650	42.68	95.47	59.59	2.46	0.44	0.68	61.23	65.76	126.99	0.189	No	No	0.20
651	42.73	95.87	59.34	2.45	0.44	0.68	61.47	65.75	127.22	0.189	No	No	0.20
652	42.79	96.16	59.43	2.46	0.44	0.68	61.65	65.82	127.48	0.190	No	No	0.20
653	42.88	94.55	60.14	2.46	0.45	0.68	60.42	65.70	126.12	0.186	No	No	0.19
654	42.93	92.84	61.58	2.48	0.45	0.67	59.20	65.77	124.97	0.183	No	No	0.19
655	42.99	90.33	63.55	2.51	0.45	0.67	57.39	65.80	123.19	0.179	No	No	0.19
656	43.06	89.11	64.00	2.51	0.45	0.67	56.48	65.66	122.14	0.176	No	No	0.18
657	43.14	87.40	62.97	2.50	0.46	0.67	55.17	65.02	120.19	0.172	No	No	0.18
658	43.18	85.19	63.22	2.50	0.46	0.66	53.57	64.63	118.20	0.168	No	No	0.17
659	43.28	79.26	66.34	2.54	0.47	0.66	49.39	64.20	113.60	0.158	No	No	0.16
660	43.33	73.93	69.97	2.59	0.48	0.65	45.73	63.93	109.66	0.152	No	No	0.16
661	43.42	65.90	76.46	2.67	0.49	0.65	40.25	0.00	40.25	4.000	No	Yes	2.00
662	43.44	63.39	78.34	2.69	0.49	0.64	38.58	0.00	38.58	4.000	No	Yes	2.00
663	43.53	57.16	81.68	2.73	0.50	0.64	34.46	0.00	34.46	4.000	No	Yes	2.00
664	43.58	55.15	82.34	2.74	0.51	0.63	33.13	0.00	33.13	4.000	No	Yes	2.00
665	43.67	48.42	88.26	2.82	0.52	0.63	28.74	0.00	28.74	4.000	No	Yes	2.00
666	43.73	46.01	90.42	2.84	0.52	0.62	27.19	0.00	27.19	4.000	No	Yes	2.00
667	43.78	44.61	91.58	2.86	0.53	0.62	26.28	0.00	26.28	4.000	No	Yes	2.00
668	43.86	45.96	89.58	2.83	0.52	0.62	27.10	0.00	27.10	4.000	No	Yes	2.00
669	43.92	45.51	89.43	2.83	0.53	0.62	26.79	0.00	26.79	4.000	No	Yes	2.00
670	43.97	45.91	87.28	2.80	0.53	0.62	27.01	0.00	27.01	4.000	No	Yes	2.00
671	44.06	45.81	82.79	2.75	0.53	0.62	26.88	0.00	26.88	4.000	No	Yes	2.00
672	44.12	43.50	85.94	2.79	0.53	0.62	25.43	0.00	25.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
673	44.17	39.19	92.12	2.86	0.54	0.61	22.75	0.00	22.75	4.000	No	Yes	2.00
674	44.26	32.16	100.00	2.98	0.55	0.61	18.44	0.00	18.44	4.000	No	Yes	2.00
675	44.30	28.45	100.00	3.05	0.56	0.60	16.18	0.00	16.18	4.000	No	Yes	2.00
676	44.37	23.53	100.00	3.18	0.57	0.59	13.25	0.00	13.25	4.000	No	Yes	2.00
677	44.44	20.72	100.00	3.27	0.58	0.59	11.60	0.00	11.60	4.000	No	Yes	2.00
678	44.50	21.43	100.00	3.25	0.57	0.59	12.00	0.00	12.00	4.000	No	Yes	2.00
679	44.59	20.33	100.00	3.29	0.58	0.59	11.34	0.00	11.34	4.000	No	Yes	2.00
680	44.64	20.43	100.00	3.28	0.58	0.59	11.39	0.00	11.39	4.000	No	Yes	2.00
681	44.73	22.34	100.00	3.22	0.57	0.59	12.49	0.00	12.49	4.000	No	Yes	2.00
682	44.77	23.74	100.00	3.17	0.57	0.59	13.30	0.00	13.30	4.000	No	Yes	2.00
683	44.83	24.65	100.00	3.14	0.57	0.59	13.82	0.00	13.82	4.000	No	Yes	2.00
684	44.88	26.35	100.00	3.09	0.56	0.59	14.81	0.00	14.81	4.000	No	Yes	2.00
685	44.96	27.66	100.00	3.06	0.56	0.59	15.57	0.00	15.57	4.000	No	Yes	2.00
686	45.03	26.15	100.00	3.11	0.56	0.59	14.66	0.00	14.66	4.000	No	Yes	2.00
687	45.08	25.05	100.00	3.15	0.57	0.59	14.01	0.00	14.01	4.000	No	Yes	2.00
688	45.17	26.15	100.00	3.13	0.56	0.59	14.64	0.00	14.64	4.000	No	Yes	2.00
689	45.22	25.15	100.00	3.15	0.57	0.59	14.04	0.00	14.04	4.000	No	Yes	2.00
690	45.28	26.15	100.00	3.11	0.56	0.59	14.62	0.00	14.62	4.000	No	Yes	2.00
691	45.36	25.15	100.00	3.07	0.57	0.59	14.02	0.00	14.02	4.000	No	Yes	2.00
692	45.41	23.14	100.00	3.10	0.57	0.59	12.84	0.00	12.84	4.000	No	Yes	2.00
693	45.48	21.33	100.00	3.17	0.58	0.58	11.78	0.00	11.78	4.000	No	Yes	2.00
694	45.54	20.23	100.00	3.25	0.58	0.58	11.14	0.00	11.14	4.000	No	Yes	2.00
695	45.63	19.83	100.00	3.30	0.58	0.58	10.90	0.00	10.90	4.000	No	Yes	2.00
696	45.67	20.33	100.00	3.30	0.58	0.58	11.18	0.00	11.18	4.000	No	Yes	2.00
697	45.74	30.97	100.00	3.06	0.55	0.59	17.37	0.00	17.37	4.000	No	Yes	2.00
698	45.83	65.52	72.65	2.62	0.50	0.63	38.77	0.00	38.77	4.000	No	Yes	2.00
699	45.88	92.92	54.91	2.40	0.46	0.65	57.00	63.04	120.03	0.171	No	No	0.18
700	45.97	112.09	48.65	2.32	0.43	0.66	70.40	64.02	134.42	0.212	No	No	0.22
701	46.03	116.71	49.28	2.33	0.42	0.67	73.92	65.25	139.17	0.231	No	No	0.24
702	46.07	121.93	49.25	2.33	0.41	0.67	77.80	66.25	144.05	0.254	No	No	0.27
703	46.17	131.37	48.18	2.31	0.40	0.68	84.85	67.56	152.41	0.306	No	No	0.32
704	46.22	136.49	47.10	2.30	0.39	0.69	88.69	67.98	156.67	0.340	No	No	0.36
705	46.27	142.11	45.87	2.29	0.39	0.69	92.94	68.36	161.31	0.386	No	No	0.40
706	46.36	149.14	44.42	2.27	0.38	0.70	98.28	68.82	167.11	0.459	No	No	0.48
707	46.41	154.16	42.81	2.25	0.37	0.70	102.08	68.68	170.76	0.517	No	No	0.54
708	46.49	164.80	39.24	2.20	0.36	0.71	110.16	67.87	178.03	0.673	No	No	0.71
709	46.54	175.75	35.97	2.16	0.35	0.71	118.59	66.72	185.31	0.908	No	No	0.95
710	46.62	193.62	30.63	2.10	0.34	0.72	132.28	63.04	195.32	1.468	No	No	1.53
711	46.66	199.73	28.82	2.07	0.33	0.73	136.90	61.15	198.05	1.698	No	No	1.76
712	46.73	215.70	24.02	2.01	0.33	0.73	148.57	53.93	202.50	2.185	No	No	2.00
713	46.82	223.21	21.60	1.98	0.33	0.73	153.61	48.75	202.35	2.166	No	No	2.00
714	46.85	223.42	21.26	1.98	0.33	0.73	153.51	47.80	201.30	2.037	No	No	2.00
715	46.92	218.99	21.90	1.99	0.33	0.72	149.93	48.98	198.90	1.779	No	No	1.84
716	47.01	210.36	24.13	2.01	0.34	0.72	143.55	53.32	196.87	1.593	No	No	1.65
717	47.06	202.83	26.35	2.04	0.34	0.72	138.02	56.95	194.98	1.442	No	No	1.50
718	47.15	191.79	30.00	2.09	0.34	0.72	129.82	61.60	191.42	1.205	No	No	1.26
719	47.21	187.27	32.51	2.12	0.34	0.72	126.66	64.46	191.12	1.188	No	No	1.24
720	47.25	186.27	32.65	2.12	0.34	0.71	125.80	64.45	190.25	1.139	No	No	1.19

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	47.31	187.87	28.06	2.06	0.35	0.71	125.62	57.69	183.31	0.833	No	No	0.88
722	47.41	204.54	23.10	2.00	0.35	0.71	137.40	49.98	187.38	0.997	No	No	1.05
723	47.46	214.18	21.15	1.98	0.34	0.71	144.43	46.19	190.61	1.159	No	No	1.21
724	47.54	226.23	18.98	1.95	0.34	0.72	153.19	41.10	194.30	1.392	No	No	1.45
725	47.58	214.88	22.45	1.99	0.34	0.72	145.69	49.73	195.42	1.475	No	No	1.53
726	47.67	232.45	18.77	1.95	0.33	0.72	158.29	41.10	199.38	1.827	No	No	1.89
727	47.71	235.87	18.04	1.94	0.33	0.72	160.60	38.98	199.58	1.848	No	No	1.91
728	47.77	245.30	15.62	1.91	0.33	0.72	166.46	31.00	197.45	1.644	No	No	1.70
729	47.85	252.84	14.00	1.89	0.34	0.72	171.19	25.11	196.30	1.546	No	No	1.60
730	47.92	254.95	13.51	1.88	0.34	0.72	172.35	23.21	195.56	1.486	No	No	1.54
731	47.97	254.36	13.61	1.88	0.34	0.71	171.86	23.62	195.48	1.480	No	No	1.54
732	48.06	251.65	14.48	1.89	0.33	0.72	170.32	26.96	197.28	1.628	No	No	1.69
733	48.12	249.45	15.18	1.90	0.33	0.72	169.05	29.57	198.62	1.752	No	No	1.81
734	48.17	246.14	16.21	1.92	0.33	0.72	167.15	33.26	200.41	1.936	No	No	2.00
735	48.25	241.12	17.71	1.93	0.33	0.72	164.06	38.28	202.34	2.164	No	No	2.00
736	48.31	237.91	18.64	1.95	0.33	0.72	161.96	41.11	203.07	2.259	No	No	2.00
737	48.36	235.40	19.38	1.95	0.33	0.72	160.30	43.26	203.56	2.325	No	No	2.00
738	48.45	234.00	19.32	1.95	0.33	0.72	158.87	42.90	201.77	2.093	No	No	2.00
739	48.50	233.09	19.14	1.95	0.33	0.72	157.83	42.20	200.02	1.894	No	No	1.95
740	48.57	234.00	18.72	1.95	0.33	0.72	158.16	40.90	199.06	1.795	No	No	1.85
741	48.63	233.29	18.52	1.94	0.33	0.71	157.25	40.15	197.39	1.638	No	No	1.70
742	48.72	234.00	17.91	1.94	0.34	0.71	157.19	38.15	195.33	1.469	No	No	1.52
743	48.77	235.10	17.24	1.93	0.34	0.71	157.43	35.92	193.35	1.327	No	No	1.38
744	48.85	238.92	15.68	1.91	0.35	0.70	159.05	30.56	189.61	1.105	No	No	1.16
745	48.91	242.93	14.28	1.89	0.35	0.70	160.90	25.43	186.33	0.950	No	No	1.00
746	48.97	246.85	13.44	1.88	0.35	0.70	163.26	22.37	185.63	0.921	No	No	0.97
747	49.05	253.58	11.90	1.86	0.35	0.70	167.11	16.55	183.66	0.846	No	No	0.89
748	49.11	257.09	10.91	1.85	0.36	0.69	168.88	12.86	181.74	0.780	No	No	0.82
749	49.16	258.89	10.21	1.84	0.36	0.69	169.54	10.37	179.91	0.724	No	No	0.76
750	49.21	258.79	9.56	1.83	0.36	0.69	168.64	8.18	176.82	0.642	No	No	0.67
751	49.28	255.97	8.85	1.82	0.37	0.68	165.34	5.98	171.32	0.527	No	No	0.55
752	49.35	249.45	10.01	1.84	0.37	0.68	160.78	9.43	170.21	0.508	No	No	0.53
753	49.42	233.79	13.52	1.88	0.37	0.68	151.29	21.84	173.14	0.561	No	No	0.59
754	49.48	220.33	16.21	1.92	0.37	0.68	142.60	30.85	173.46	0.568	No	No	0.60
755	49.54	207.28	20.28	1.97	0.36	0.69	134.90	42.49	177.39	0.656	No	No	0.69
756	49.61	193.23	22.62	2.00	0.37	0.68	124.57	46.82	171.39	0.528	No	No	0.55
757	49.68	187.50	25.76	2.03	0.37	0.68	121.33	52.82	174.15	0.582	No	No	0.61
758	49.76	182.48	25.29	2.03	0.38	0.68	116.92	51.15	168.07	0.473	No	No	0.50
759	49.81	180.38	26.55	2.04	0.37	0.68	115.67	53.23	168.90	0.486	No	No	0.51
760	49.88	179.97	28.40	2.07	0.37	0.68	115.97	56.38	172.35	0.546	No	No	0.57
761	49.95	179.57	30.24	2.09	0.36	0.68	116.18	59.17	175.35	0.608	No	No	0.64
762	50.02	179.92	31.56	2.11	0.36	0.69	116.78	61.11	177.89	4.000	No	No	2.00
763	50.10	179.92	32.89	2.12	0.36	0.69	117.07	62.88	179.95	4.000	No	No	2.00
764	50.15	180.27	33.49	2.13	0.36	0.69	117.46	63.68	181.14	4.000	No	No	2.00
765	50.20	183.88	32.73	2.12	0.35	0.69	120.19	63.35	183.54	4.000	No	No	2.00
766	50.28	185.99	32.96	2.12	0.35	0.69	121.91	64.01	185.92	4.000	No	No	2.00
767	50.34	187.89	33.07	2.13	0.35	0.70	123.46	64.48	187.95	4.000	No	No	2.00
768	50.44	190.71	33.19	2.13	0.34	0.70	125.75	65.12	190.87	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
769	50.47	191.91	33.05	2.13	0.34	0.70	126.68	65.16	191.84	4.000	No	No	2.00
770	50.54	192.61	33.27	2.13	0.34	0.70	127.25	65.55	192.81	4.000	No	No	2.00
771	50.59	192.41	33.53	2.13	0.34	0.70	127.10	65.84	192.94	4.000	No	No	2.00
772	50.69	191.11	34.23	2.14	0.34	0.70	126.08	66.47	192.54	4.000	No	No	2.00
773	50.73	190.51	34.44	2.14	0.34	0.70	125.58	66.60	192.18	4.000	No	No	2.00
774	50.84	188.60	34.66	2.15	0.34	0.69	123.90	66.48	190.39	4.000	No	No	2.00
775	50.86	188.00	34.76	2.15	0.34	0.69	123.40	66.48	189.88	4.000	No	No	2.00
776	50.93	186.09	35.20	2.15	0.35	0.69	121.83	66.62	188.45	4.000	No	No	2.00
777	50.99	184.38	35.69	2.16	0.35	0.69	120.46	66.84	187.30	4.000	No	No	2.00
778	51.05	182.07	36.35	2.17	0.35	0.69	118.62	67.11	185.73	4.000	No	No	2.00
779	51.13	181.67	36.39	2.17	0.35	0.69	118.21	67.07	185.28	4.000	No	No	2.00
780	51.20	181.97	36.16	2.16	0.35	0.69	118.33	66.86	185.19	4.000	No	No	2.00
781	51.25	181.77	36.19	2.16	0.35	0.69	118.11	66.83	184.94	4.000	No	No	2.00
782	51.34	181.87	36.21	2.17	0.35	0.69	118.10	66.86	184.95	4.000	No	No	2.00
783	51.38	181.97	36.21	2.17	0.35	0.69	118.13	66.86	184.99	4.000	No	No	2.00
784	51.48	183.58	35.79	2.16	0.35	0.69	119.25	66.68	185.93	4.000	No	No	2.00
785	51.53	185.08	35.36	2.15	0.35	0.69	120.33	66.46	186.79	4.000	No	No	2.00
786	51.58	186.19	35.00	2.15	0.35	0.69	121.11	66.23	187.34	4.000	No	No	2.00
787	51.67	187.69	34.17	2.14	0.35	0.69	122.03	65.49	187.52	4.000	No	No	2.00
788	51.72	187.39	34.10	2.14	0.35	0.69	121.71	65.34	187.05	4.000	No	No	2.00
789	51.78	186.99	34.19	2.14	0.35	0.69	121.33	65.36	186.69	4.000	No	No	2.00
790	51.86	185.59	34.79	2.15	0.35	0.69	120.24	65.81	186.04	4.000	No	No	2.00
791	51.93	185.08	35.13	2.15	0.35	0.68	119.82	66.09	185.91	4.000	No	No	2.00
792	51.97	184.68	35.41	2.16	0.35	0.68	119.51	66.32	185.83	4.000	No	No	2.00
793	52.06	185.79	35.39	2.15	0.35	0.69	120.33	66.49	186.82	4.000	No	No	2.00
794	52.11	186.99	35.22	2.15	0.35	0.69	121.22	66.50	187.73	4.000	No	No	2.00
795	52.17	187.79	35.26	2.15	0.35	0.69	121.84	66.69	188.53	4.000	No	No	2.00
796	52.24	189.60	35.03	2.15	0.34	0.69	123.20	66.74	189.94	4.000	No	No	2.00
797	52.31	190.51	34.98	2.15	0.34	0.69	123.88	66.83	190.71	4.000	No	No	2.00
798	52.37	189.70	35.10	2.15	0.34	0.69	123.16	66.81	189.97	4.000	No	No	2.00
799	52.47	186.09	35.76	2.16	0.35	0.68	120.21	66.86	187.07	4.000	No	No	2.00
800	52.52	182.07	36.80	2.17	0.35	0.68	117.07	67.22	184.29	4.000	No	No	2.00
801	52.57	180.06	37.12	2.18	0.35	0.68	115.44	67.15	182.60	4.000	No	No	2.00
802	52.67	171.73	38.87	2.20	0.36	0.67	108.93	67.25	176.18	4.000	No	No	2.00
803	52.72	166.71	39.90	2.21	0.37	0.67	105.04	67.19	172.23	4.000	No	No	2.00
804	52.77	161.29	41.24	2.23	0.38	0.66	100.93	67.25	168.18	4.000	No	No	2.00
805	52.86	153.76	43.31	2.25	0.38	0.66	95.26	67.33	162.59	4.000	No	No	2.00
806	52.91	149.04	44.80	2.27	0.39	0.65	91.77	67.41	159.19	4.000	No	No	2.00
807	52.96	144.82	46.06	2.29	0.39	0.65	88.67	67.38	156.05	4.000	No	No	2.00
808	53.02	140.51	47.47	2.31	0.40	0.64	85.54	67.36	152.90	4.000	No	No	2.00
809	53.10	134.28	49.94	2.34	0.41	0.64	81.09	67.46	148.54	4.000	No	No	2.00
810	53.16	130.37	51.54	2.36	0.41	0.64	78.31	67.45	145.76	4.000	No	No	2.00
811	53.24	125.65	53.42	2.38	0.42	0.63	74.97	67.36	142.32	4.000	No	No	2.00
812	53.30	122.64	53.63	2.38	0.42	0.63	72.78	66.85	139.63	4.000	No	No	2.00
813	53.36	118.92	54.53	2.39	0.43	0.62	70.15	66.49	136.64	4.000	No	No	2.00
814	53.42	117.01	55.95	2.41	0.43	0.62	68.86	66.66	135.52	4.000	No	No	2.00
815	53.48	115.71	56.95	2.42	0.43	0.62	67.85	66.74	134.58	4.000	No	No	2.00
816	53.56	115.91	57.36	2.43	0.43	0.62	67.98	66.92	134.90	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
817	53.61	115.31	58.00	2.44	0.43	0.62	67.58	67.02	134.59	4.000	No	No	2.00
818	53.69	120.63	55.35	2.40	0.42	0.63	71.31	67.11	138.42	4.000	No	No	2.00
819	53.75	126.75	52.02	2.36	0.42	0.63	75.47	66.90	142.37	4.000	No	No	2.00
820	53.82	130.37	49.71	2.33	0.41	0.63	77.89	66.50	144.39	4.000	No	No	2.00
821	53.88	131.17	48.88	2.32	0.41	0.63	78.38	66.22	144.60	4.000	No	No	2.00
822	53.97	130.07	48.27	2.32	0.42	0.63	77.49	65.68	143.17	4.000	No	No	2.00
823	54.02	129.16	47.82	2.31	0.42	0.63	76.76	65.26	142.02	4.000	No	No	2.00
824	54.09	123.94	49.24	2.33	0.42	0.62	73.09	65.00	138.09	4.000	No	No	2.00
825	54.14	119.22	51.12	2.35	0.43	0.62	69.85	65.01	134.86	4.000	No	No	2.00
826	54.21	114.50	53.09	2.38	0.44	0.61	66.52	64.94	131.46	4.000	No	No	2.00
827	54.28	107.38	57.01	2.43	0.44	0.61	61.80	65.09	126.89	4.000	No	No	2.00
828	54.33	103.46	59.33	2.45	0.45	0.61	59.23	65.12	124.35	4.000	No	No	2.00
829	54.43	101.75	60.44	2.47	0.45	0.60	58.09	65.13	123.22	4.000	No	No	2.00
830	54.48	101.95	60.40	2.47	0.45	0.60	58.21	65.16	123.37	4.000	No	No	2.00
831	54.53	102.86	59.79	2.46	0.45	0.60	58.78	65.13	123.91	4.000	No	No	2.00
832	54.62	102.76	59.29	2.45	0.45	0.60	58.66	64.95	123.61	4.000	No	No	2.00
833	54.67	101.75	59.33	2.45	0.45	0.60	57.97	64.77	122.74	4.000	No	No	2.00
834	54.73	101.15	59.05	2.45	0.45	0.60	57.54	64.56	122.09	4.000	No	No	2.00
835	54.82	98.54	59.56	2.46	0.46	0.60	55.79	64.23	120.01	4.000	No	No	2.00
836	54.87	96.83	59.97	2.46	0.46	0.60	54.65	64.03	118.68	4.000	No	No	2.00
837	54.95	94.73	60.12	2.46	0.46	0.59	53.25	63.68	116.92	4.000	No	No	2.00
838	55.01	93.52	60.60	2.47	0.47	0.59	52.45	63.59	116.05	4.000	No	No	2.00
839	55.06	91.11	61.94	2.49	0.47	0.59	50.91	63.53	114.44	4.000	No	No	2.00
840	55.12	88.50	63.29	2.50	0.47	0.59	49.25	63.42	112.66	4.000	No	No	2.00
841	55.20	85.89	64.80	2.52	0.48	0.59	47.59	63.32	110.91	4.000	No	No	2.00
842	55.26	84.59	65.57	2.53	0.48	0.58	46.76	63.27	110.03	4.000	No	No	2.00
843	55.32	83.28	66.35	2.54	0.48	0.58	45.93	63.21	109.14	4.000	No	No	2.00
844	55.41	83.28	66.28	2.54	0.48	0.58	45.91	63.19	109.10	4.000	No	No	2.00
845	55.47	85.19	64.97	2.52	0.48	0.58	47.08	63.21	110.29	4.000	No	No	2.00
846	55.51	88.20	63.12	2.50	0.47	0.59	48.95	63.29	112.23	4.000	No	No	2.00
847	55.59	96.23	58.26	2.44	0.46	0.59	53.98	63.32	117.31	4.000	No	No	2.00
848	55.67	110.69	50.31	2.34	0.45	0.60	63.23	62.89	126.12	4.000	No	No	2.00
849	55.72	122.74	44.44	2.27	0.43	0.61	71.06	61.94	133.00	4.000	No	No	2.00
850	55.81	138.40	38.36	2.19	0.42	0.62	81.65	60.35	142.00	4.000	No	No	2.00
851	55.86	145.33	36.07	2.16	0.41	0.63	86.34	59.45	145.78	4.000	No	No	2.00
852	55.92	150.75	34.84	2.15	0.41	0.63	90.11	59.12	149.22	4.000	No	No	2.00
853	56.01	159.08	33.87	2.14	0.39	0.64	96.16	59.45	155.60	4.000	No	No	2.00
854	56.06	163.80	33.18	2.13	0.39	0.64	99.60	59.43	159.03	4.000	No	No	2.00
855	56.11	168.62	32.36	2.12	0.38	0.65	103.10	59.23	162.33	4.000	No	No	2.00
856	56.21	181.07	29.42	2.08	0.37	0.65	111.94	57.14	169.08	4.000	No	No	2.00
857	56.25	191.51	26.41	2.04	0.37	0.66	119.09	53.61	172.69	4.000	No	No	2.00
858	56.31	203.05	22.83	2.00	0.37	0.66	126.51	47.61	174.12	4.000	No	No	2.00
859	56.38	216.71	15.50	1.91	0.39	0.64	131.48	27.40	158.88	4.000	No	No	2.00
860	56.44	224.14	14.82	1.90	0.39	0.65	136.76	25.51	162.27	4.000	No	No	2.00
861	56.50	231.67	13.83	1.89	0.38	0.65	141.75	22.34	164.09	4.000	No	No	2.00
862	56.58	241.41	12.36	1.87	0.38	0.65	147.95	17.31	165.26	4.000	No	No	2.00
863	56.65	246.12	12.23	1.87	0.38	0.65	151.68	17.03	168.72	4.000	No	No	2.00
864	56.73	236.78	16.14	1.91	0.36	0.66	148.61	31.20	179.81	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
865	56.76	242.80	15.35	1.90	0.36	0.67	152.79	28.77	181.56	4.000	No	No	2.00
866	56.84	244.11	15.87	1.91	0.35	0.67	154.49	30.81	185.30	4.000	No	No	2.00
867	56.92	241.60	17.35	1.93	0.35	0.67	153.98	35.93	189.91	4.000	No	No	2.00
868	56.98	239.49	18.40	1.94	0.34	0.68	153.22	39.28	192.50	4.000	No	No	2.00
869	57.02	236.78	19.22	1.95	0.34	0.68	151.66	41.67	193.33	4.000	No	No	2.00
870	57.12	234.17	20.17	1.96	0.34	0.68	150.22	44.29	194.52	4.000	No	No	2.00
871	57.17	234.17	20.33	1.97	0.34	0.68	150.33	44.77	195.09	4.000	No	No	2.00
872	57.23	234.17	20.48	1.97	0.34	0.68	150.42	45.19	195.61	4.000	No	No	2.00
873	57.32	234.17	20.95	1.97	0.34	0.68	150.76	46.55	197.31	4.000	No	No	2.00
874	57.36	234.47	21.08	1.98	0.33	0.68	151.10	46.96	198.07	4.000	No	No	2.00
875	57.42	235.47	21.15	1.98	0.33	0.68	151.99	47.27	199.26	4.000	No	No	2.00
876	57.50	237.18	21.04	1.98	0.33	0.68	153.33	47.17	200.50	4.000	No	No	2.00
877	57.55	240.69	20.34	1.97	0.33	0.68	155.75	45.54	201.29	4.000	No	No	2.00
878	57.62	245.91	19.49	1.96	0.33	0.69	159.48	43.48	202.96	4.000	No	No	2.00
879	57.69	254.05	17.73	1.93	0.33	0.69	164.74	38.42	203.15	4.000	No	No	2.00
880	57.77	262.58	16.07	1.91	0.33	0.69	170.23	33.05	203.27	4.000	No	No	2.00
881	57.83	267.29	15.32	1.90	0.33	0.69	173.39	30.46	203.84	4.000	No	No	2.00
882	57.91	271.61	14.60	1.90	0.32	0.69	176.77	27.94	204.71	4.000	No	No	2.00
883	57.97	273.92	14.29	1.89	0.32	0.69	178.36	26.81	205.17	4.000	No	No	2.00
884	58.01	274.92	14.33	1.89	0.32	0.69	179.29	27.02	206.31	4.000	No	No	2.00
885	58.11	278.22	14.05	1.89	0.32	0.69	181.82	26.11	207.93	4.000	No	No	2.00
886	58.16	282.64	13.28	1.88	0.32	0.69	184.61	23.09	207.71	4.000	No	No	2.00
887	58.22	289.97	11.92	1.86	0.32	0.69	189.10	17.70	206.79	4.000	No	No	2.00
888	58.31	301.11	9.50	1.83	0.33	0.69	195.49	8.61	204.10	4.000	No	No	2.00
889	58.36	307.44	8.16	1.81	0.33	0.69	199.58	4.61	204.19	4.000	No	No	2.00
890	58.41	313.26	6.95	1.80	0.32	0.69	203.84	2.06	205.90	4.000	No	No	2.00
891	58.51	318.78	5.80	1.78	0.32	0.69	208.31	0.67	208.97	4.000	No	No	2.00
892	58.55	320.68	5.46	1.78	0.32	0.69	209.97	0.44	210.41	4.000	No	No	2.00
893	58.60	320.98	5.43	1.78	0.32	0.69	210.20	0.42	210.61	4.000	No	No	2.00
894	58.67	318.47	6.00	1.79	0.32	0.69	207.94	0.84	208.78	4.000	No	No	2.00
895	58.76	314.36	6.96	1.80	0.32	0.69	204.54	2.07	206.61	4.000	No	No	2.00
896	58.80	312.75	7.28	1.80	0.32	0.69	203.25	2.65	205.90	4.000	No	No	2.00
897	58.88	307.13	8.43	1.82	0.32	0.69	199.12	5.34	204.46	4.000	No	No	2.00
898	58.94	303.81	9.46	1.83	0.32	0.69	197.36	8.52	205.88	4.000	No	No	2.00
899	59.01	301.81	10.41	1.84	0.32	0.69	196.90	11.98	208.88	4.000	No	No	2.00
900	59.06	301.00	10.73	1.85	0.32	0.69	196.60	13.18	209.78	4.000	No	No	2.00
901	59.15	300.80	10.35	1.84	0.32	0.69	195.72	11.71	207.43	4.000	No	No	2.00
902	59.20	300.00	10.32	1.84	0.32	0.69	194.88	11.56	206.44	4.000	No	No	2.00
903	59.25	297.99	10.63	1.85	0.32	0.69	193.46	12.69	206.14	4.000	No	No	2.00
904	59.34	290.26	12.62	1.87	0.32	0.69	189.54	20.64	210.17	4.000	No	No	2.00
905	59.40	286.04	12.55	1.87	0.32	0.69	185.47	20.11	205.58	4.000	No	No	2.00
906	59.45	283.13	10.76	1.85	0.34	0.67	179.29	12.69	191.98	4.000	No	No	2.00
907	59.54	279.61	12.32	1.87	0.34	0.68	178.50	18.81	197.31	4.000	No	No	2.00
908	59.60	278.50	12.76	1.87	0.33	0.68	178.76	20.60	199.37	4.000	No	No	2.00
909	59.65	278.60	13.14	1.88	0.33	0.68	179.42	22.21	201.63	4.000	No	No	2.00
910	59.74	255.71	17.98	1.94	0.33	0.68	164.95	39.30	204.24	4.000	No	No	2.00
911	59.78	261.34	15.85	1.91	0.33	0.68	167.23	31.93	199.16	4.000	No	No	2.00
912	59.87	285.73	9.78	1.83	0.35	0.67	179.81	9.19	189.00	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
913	59.94	291.15	9.13	1.83	0.34	0.67	183.70	7.16	190.86	4.000	No	No	2.00
914	59.99	291.96	9.38	1.83	0.34	0.67	185.37	7.98	193.35	4.000	No	No	2.00
915	60.05	294.07	9.73	1.83	0.33	0.68	187.75	9.23	196.97	4.000	No	No	2.00
916	60.14	287.14	11.98	1.86	0.33	0.68	184.90	17.74	202.64	4.000	No	No	2.00
917	60.19	293.21	10.99	1.85	0.33	0.68	188.79	13.93	202.72	4.000	No	No	2.00
918	60.24	287.94	11.98	1.86	0.33	0.68	185.55	17.78	203.33	4.000	No	No	2.00
919	60.34	292.36	11.36	1.85	0.33	0.68	188.49	15.40	203.89	4.000	No	No	2.00
920	60.38	292.86	11.65	1.86	0.32	0.68	189.39	16.60	205.99	4.000	No	No	2.00
921	60.44	291.36	12.42	1.87	0.32	0.69	189.27	19.79	209.05	4.000	No	No	2.00
922	60.53	288.23	13.61	1.88	0.31	0.69	188.32	24.74	213.07	4.000	No	No	2.00
923	60.58	285.32	14.49	1.89	0.31	0.69	187.02	28.29	215.31	4.000	No	No	2.00
924	60.63	283.41	15.15	1.90	0.31	0.70	186.24	30.91	217.15	4.000	No	No	2.00
925	60.71	280.90	15.84	1.91	0.31	0.70	184.90	33.55	218.45	4.000	No	No	2.00
926	60.78	281.41	15.87	1.91	0.31	0.70	185.37	33.72	219.09	4.000	No	No	2.00
927	60.83	281.61	15.80	1.91	0.31	0.70	185.41	33.45	218.86	4.000	No	No	2.00
928	60.91	279.60	15.99	1.91	0.31	0.70	183.75	34.02	217.77	4.000	No	No	2.00
929	60.97	276.59	16.40	1.92	0.31	0.69	181.51	35.40	216.92	4.000	No	No	2.00
930	61.03	276.64	16.58	1.92	0.31	0.69	181.78	36.12	217.90	4.000	No	No	2.00
931	61.10	276.69	16.58	1.92	0.31	0.69	181.77	36.12	217.89	4.000	No	No	2.00
932	61.16	279.50	15.82	1.91	0.31	0.69	183.20	33.32	216.53	4.000	No	No	2.00
933	61.23	286.43	14.57	1.89	0.31	0.69	187.64	28.68	216.32	4.000	No	No	2.00
934	61.32	290.24	13.80	1.89	0.31	0.69	189.83	25.64	215.47	4.000	No	No	2.00
935	61.38	290.94	13.89	1.89	0.31	0.69	190.58	26.05	216.63	4.000	No	No	2.00
936	61.43	291.04	14.23	1.89	0.31	0.69	191.22	27.54	218.76	4.000	No	No	2.00
937	61.52	292.95	13.94	1.89	0.31	0.69	192.43	26.38	218.81	4.000	No	No	2.00
938	61.56	294.86	13.44	1.88	0.31	0.69	193.33	24.34	217.68	4.000	No	No	2.00
939	61.62	296.06	13.18	1.88	0.31	0.69	193.96	23.29	217.25	4.000	No	No	2.00
940	61.71	293.75	13.66	1.88	0.31	0.69	192.54	25.24	217.78	4.000	No	No	2.00
941	61.77	290.95	14.25	1.89	0.31	0.69	190.85	27.57	218.43	4.000	No	No	2.00
942	61.84	290.24	14.21	1.89	0.31	0.69	190.08	27.35	217.43	4.000	No	No	2.00
943	61.92	290.25	13.62	1.88	0.31	0.69	189.01	24.82	213.83	4.000	No	No	2.00
944	61.94	290.24	13.51	1.88	0.31	0.69	188.79	24.34	213.13	4.000	No	No	2.00
945	62.02	290.25	13.23	1.88	0.32	0.69	188.24	23.13	211.37	4.000	No	No	2.00
946	62.12	289.95	13.32	1.88	0.32	0.69	188.05	23.51	211.56	4.000	No	No	2.00
947	62.15	289.24	13.41	1.88	0.32	0.69	187.53	23.85	211.38	4.000	No	No	2.00
948	62.22	286.54	13.81	1.89	0.32	0.69	185.63	25.37	211.00	4.000	No	No	2.00
949	62.27	283.41	14.36	1.89	0.32	0.69	183.60	27.49	211.09	4.000	No	No	2.00
950	62.36	277.40	15.26	1.90	0.32	0.68	179.41	30.77	210.18	4.000	No	No	2.00
951	62.41	275.58	15.58	1.91	0.32	0.68	178.20	31.91	210.11	4.000	No	No	2.00
952	62.48	274.99	15.53	1.91	0.32	0.68	177.51	31.64	209.15	4.000	No	No	2.00
953	62.55	275.39	15.16	1.90	0.32	0.68	177.26	30.18	207.44	4.000	No	No	2.00
954	62.61	278.60	14.36	1.89	0.32	0.68	178.90	27.14	206.03	4.000	No	No	2.00
955	62.69	281.21	13.60	1.88	0.33	0.68	179.97	24.11	204.08	4.000	No	No	2.00
956	62.74	282.62	13.13	1.88	0.33	0.68	180.45	22.23	202.67	4.000	No	No	2.00
957	62.81	283.52	13.10	1.88	0.33	0.68	181.16	22.14	203.30	4.000	No	No	2.00
958	62.87	284.63	12.97	1.87	0.33	0.68	181.89	21.64	203.53	4.000	No	No	2.00
959	62.95	285.23	12.86	1.87	0.33	0.68	182.20	21.23	203.43	4.000	No	No	2.00
960	63.00	284.03	13.23	1.88	0.32	0.68	181.68	22.70	204.38	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
961	63.10	277.80	14.76	1.90	0.32	0.68	178.40	28.69	207.09	4.000	No	No	2.00
962	63.13	272.78	15.87	1.91	0.32	0.68	175.49	32.78	208.27	4.000	No	No	2.00
963	63.19	277.75	14.79	1.90	0.32	0.68	178.33	28.80	207.13	4.000	No	No	2.00
964	63.26	273.89	15.40	1.91	0.32	0.68	175.70	30.99	206.69	4.000	No	No	2.00
965	63.32	277.70	14.15	1.89	0.33	0.67	177.15	26.14	203.28	4.000	No	No	2.00
966	63.39	279.71	13.15	1.88	0.33	0.67	177.29	22.11	199.40	4.000	No	No	2.00
967	63.49	278.70	12.82	1.87	0.34	0.67	175.74	20.67	196.42	4.000	No	No	2.00
968	63.52	277.50	12.64	1.87	0.34	0.66	174.35	19.87	194.22	4.000	No	No	2.00
969	63.60	274.99	11.99	1.86	0.35	0.66	170.39	17.07	187.46	4.000	No	No	2.00
970	63.69	270.37	12.11	1.86	0.35	0.65	166.47	17.34	183.81	4.000	No	No	2.00
971	63.74	266.46	12.98	1.87	0.35	0.65	164.37	20.61	184.98	4.000	No	No	2.00
972	63.79	266.31	13.04	1.88	0.35	0.65	164.30	20.86	185.16	4.000	No	No	2.00
973	63.85	266.31	12.90	1.87	0.35	0.65	164.04	20.30	184.34	4.000	No	No	2.00
974	63.92	266.16	12.16	1.86	0.36	0.65	162.71	17.33	180.04	4.000	No	No	2.00
975	63.99	270.37	10.23	1.84	0.37	0.64	163.42	10.26	173.68	4.000	No	No	2.00
976	64.05	273.58	8.75	1.82	0.37	0.63	164.20	5.67	169.87	4.000	No	No	2.00
977	64.13	277.70	6.41	1.79	0.38	0.63	165.71	1.14	166.86	4.000	No	No	2.00
978	64.18	279.71	2.85	1.75	0.38	0.63	166.88	0.00	166.88	4.000	No	No	2.00
979	64.24	281.01	0.00	1.67	0.38	0.63	167.94	0.00	167.94	4.000	No	No	2.00
980	64.34	278.10	0.00	1.68	0.38	0.63	165.38	0.00	165.38	4.000	No	No	2.00
981	64.39	276.50	0.00	1.69	0.38	0.63	163.98	0.00	163.98	4.000	No	No	2.00
982	64.45	277.90	0.00	1.71	0.38	0.63	165.12	0.00	165.12	4.000	No	No	2.00
983	64.51	271.18	2.89	1.75	0.39	0.62	159.41	0.00	159.41	4.000	No	No	2.00
984	64.59	274.99	4.16	1.76	0.39	0.63	162.56	0.04	162.60	4.000	No	No	2.00
985	64.64	279.51	4.41	1.77	0.38	0.63	166.36	0.06	166.42	4.000	No	No	2.00
986	64.73	282.02	5.70	1.78	0.38	0.63	168.62	0.53	169.15	4.000	No	No	2.00
987	64.78	283.12	6.54	1.79	0.37	0.63	169.87	1.31	171.18	4.000	No	No	2.00
988	64.83	285.53	7.52	1.81	0.37	0.64	172.58	2.88	175.46	4.000	No	No	2.00
989	64.93	287.34	9.13	1.83	0.36	0.65	175.84	6.98	182.82	4.000	No	No	2.00
990	64.98	288.95	9.58	1.83	0.35	0.65	177.83	8.46	186.29	4.000	No	No	2.00
991	65.03	289.65	10.12	1.84	0.34	0.66	179.90	10.36	190.26	4.000	No	No	2.00
992	65.12	292.16	10.63	1.85	0.34	0.66	182.92	12.34	195.26	4.000	No	No	2.00
993	65.17	294.87	10.73	1.85	0.33	0.67	185.50	12.81	198.31	4.000	No	No	2.00
994	65.23	299.19	10.42	1.84	0.33	0.67	188.89	11.74	200.64	4.000	No	No	2.00
995	65.31	304.81	9.85	1.84	0.33	0.67	193.06	9.77	202.83	4.000	No	No	2.00
996	65.36	307.12	9.36	1.83	0.33	0.67	194.38	8.12	202.50	4.000	No	No	2.00
997	65.42	308.32	9.04	1.83	0.33	0.67	194.97	7.10	202.06	4.000	No	No	2.00
998	65.50	307.62	8.49	1.82	0.33	0.67	193.48	5.42	198.90	4.000	No	No	2.00
999	65.58	305.71	8.10	1.81	0.34	0.66	191.17	4.35	195.52	4.000	No	No	2.00
1000	65.63	306.72	7.36	1.80	0.34	0.66	191.29	2.72	194.02	4.000	No	No	2.00
1001	65.72	311.13	4.71	1.77	0.34	0.66	194.02	0.13	194.15	4.000	No	No	2.00
1002	65.77	313.04	3.37	1.75	0.34	0.66	195.68	0.00	195.68	4.000	No	No	2.00
1003	65.83	316.45	1.41	1.73	0.33	0.66	198.77	0.00	198.77	4.000	No	No	2.00
1004	65.92	314.75	1.52	1.73	0.33	0.66	197.11	0.00	197.11	4.000	No	No	2.00
1005	65.97	313.54	1.95	1.74	0.34	0.66	195.95	0.00	195.95	4.000	No	No	2.00
1006	66.02	314.04	2.05	1.74	0.34	0.66	196.36	0.00	196.36	4.000	No	No	2.00
1007	66.11	317.56	1.51	1.73	0.33	0.66	199.55	0.00	199.55	4.000	No	No	2.00
1008	66.16	322.18	0.47	1.72	0.33	0.67	203.81	0.00	203.81	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1009	66.22	325.69	0.00	1.71	0.32	0.67	207.06	0.00	207.06	4.000	No	No	2.00
1010	66.30	329.31	0.00	1.71	0.32	0.68	210.41	0.00	210.41	4.000	No	No	2.00
1011	66.35	331.01	0.00	1.71	0.32	0.68	211.98	0.00	211.98	4.000	No	No	2.00
1012	66.42	331.21	0.00	1.70	0.32	0.68	212.12	0.00	212.12	4.000	No	No	2.00
1013	66.50	330.11	0.00	1.67	0.32	0.68	210.99	0.00	210.99	4.000	No	No	2.00
1014	66.55	329.51	0.00	1.65	0.32	0.68	210.37	0.00	210.37	4.000	No	No	2.00
1015	66.61	329.91	0.00	1.63	0.32	0.68	210.70	0.00	210.70	4.000	No	No	2.00
1016	66.70	325.99	0.00	1.63	0.32	0.67	206.90	0.00	206.90	4.000	No	No	2.00
1017	66.76	321.07	0.00	1.64	0.33	0.67	202.22	0.00	202.22	4.000	No	No	2.00
1018	66.80	315.35	0.00	1.65	0.33	0.66	196.86	0.00	196.86	4.000	No	No	2.00
1019	66.88	303.40	0.00	1.65	0.35	0.65	185.90	0.00	185.90	4.000	No	No	2.00
1020	66.96	288.44	0.00	1.64	0.37	0.63	171.96	0.00	171.96	4.000	No	No	2.00
1021	67.01	276.50	0.00	1.66	0.39	0.62	161.76	0.00	161.76	4.000	No	No	2.00
1022	67.06	260.53	0.00	1.69	0.41	0.60	148.53	0.00	148.53	4.000	No	No	2.00
1023	67.13	249.89	0.37	1.72	0.42	0.59	139.94	0.00	139.94	4.000	No	No	2.00
1024	67.19	226.70	4.61	1.77	0.46	0.57	121.59	0.08	121.68	4.000	No	No	2.00
1025	67.29	189.95	13.62	1.88	0.46	0.57	101.63	18.83	120.46	4.000	No	No	2.00
1026	67.35	175.19	18.17	1.94	0.44	0.58	95.39	31.75	127.14	4.000	No	No	2.00
1027	67.40	157.93	22.22	1.99	0.45	0.57	85.46	39.88	125.34	4.000	No	No	2.00
1028	67.50	133.13	28.86	2.07	0.46	0.56	71.07	48.24	119.31	4.000	No	No	2.00
1029	67.55	117.47	36.82	2.17	0.46	0.56	62.37	54.59	116.96	4.000	No	No	2.00
1030	67.60	102.31	45.92	2.29	0.47	0.55	53.68	58.32	112.00	4.000	No	No	2.00
1031	67.68	83.63	58.97	2.45	0.49	0.54	42.86	60.44	103.29	4.000	No	No	2.00
1032	67.73	73.59	69.31	2.58	0.50	0.54	37.29	61.34	98.63	4.000	No	No	2.00
1033	67.79	67.47	75.11	2.65	0.51	0.53	33.90	0.00	33.90	4.000	No	Yes	2.00
1034	67.87	62.85	78.94	2.70	0.52	0.53	31.29	0.00	31.29	4.000	No	Yes	2.00
1035	67.93	62.45	80.17	2.71	0.52	0.53	31.07	0.00	31.07	4.000	No	Yes	2.00
1036	67.98	65.06	79.31	2.70	0.51	0.53	32.58	0.00	32.58	4.000	No	Yes	2.00
1037	68.05	71.18	75.45	2.66	0.50	0.53	35.97	0.00	35.97	4.000	No	Yes	2.00
1038	68.11	88.45	63.68	2.51	0.48	0.55	45.92	62.57	108.48	4.000	No	No	2.00
1039	68.19	125.20	41.27	2.23	0.45	0.57	67.88	59.17	127.05	4.000	No	No	2.00
1040	68.25	162.24	23.65	2.01	0.43	0.58	89.13	43.28	132.41	4.000	No	No	2.00
1041	68.34	218.57	5.40	1.78	0.47	0.56	115.06	0.30	115.36	4.000	No	No	2.00
1042	68.39	253.30	0.00	1.62	0.42	0.59	141.79	0.00	141.79	4.000	No	No	2.00
1043	68.44	284.03	0.00	1.51	0.38	0.62	167.06	0.00	167.06	4.000	No	No	2.00
1044	68.54	316.15	0.00	1.46	0.34	0.66	196.19	0.00	196.19	4.000	No	No	2.00
1045	68.59	328.60	0.00	1.45	0.32	0.67	207.80	0.00	207.80	4.000	No	No	2.00
1046	68.64	335.53	0.00	1.45	0.31	0.68	214.37	0.00	214.37	4.000	No	No	2.00
1047	68.71	322.88	0.00	1.51	0.33	0.66	202.31	0.00	202.31	4.000	No	No	2.00
1048	68.77	301.40	0.00	1.58	0.35	0.64	182.61	0.00	182.61	4.000	No	No	2.00
1049	68.84	344.67	0.00	1.50	0.30	0.68	223.06	0.00	223.06	4.000	No	No	2.00
1050	68.91	350.09	0.00	1.50	0.30	0.69	228.33	0.00	228.33	4.000	No	No	2.00
1051	68.97	355.41	0.00	1.51	0.29	0.70	233.57	0.00	233.57	4.000	No	No	2.00
1052	69.04	361.93	0.00	1.52	0.28	0.70	240.08	0.00	240.08	4.000	No	No	2.00
1053	69.12	363.54	0.00	1.52	0.28	0.70	241.63	0.00	241.63	4.000	No	No	2.00
1054	69.17	359.53	0.00	1.54	0.28	0.70	237.53	0.00	237.53	4.000	No	No	2.00
1055	69.27	344.16	0.00	1.56	0.30	0.68	222.17	0.00	222.17	4.000	No	No	2.00
1056	69.29	338.54	0.00	1.57	0.31	0.68	216.69	0.00	216.69	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1057	69.37	322.18	0.00	1.61	0.33	0.66	201.08	0.00	201.08	4.000	No	No	2.00
1058	69.42	316.55	0.00	1.62	0.34	0.65	195.81	0.00	195.81	4.000	No	No	2.00
1059	69.52	308.22	0.00	1.63	0.35	0.65	188.11	0.00	188.11	4.000	No	No	2.00
1060	69.57	303.20	0.00	1.63	0.35	0.64	183.54	0.00	183.54	4.000	No	No	2.00
1061	69.65	292.76	0.00	1.64	0.37	0.63	173.57	0.00	173.57	4.000	No	No	2.00
1062	69.71	284.93	0.00	1.66	0.38	0.62	166.81	0.00	166.81	4.000	No	No	2.00
1063	69.77	285.13	0.00	1.61	0.38	0.62	166.93	0.00	166.93	4.000	No	No	2.00
1064	69.85	283.83	0.00	1.63	0.38	0.62	165.77	0.00	165.77	4.000	No	No	2.00
1065	69.89	285.33	0.00	1.66	0.38	0.62	167.00	0.00	167.00	4.000	No	No	2.00
1066	69.96	288.34	0.00	1.63	0.38	0.62	169.52	0.00	169.52	4.000	No	No	2.00
1067	70.02	293.06	0.00	1.64	0.37	0.63	173.53	0.00	173.53	4.000	No	No	2.00
1068	70.09	297.38	0.00	1.67	0.36	0.63	177.22	0.00	177.22	4.000	No	No	2.00
1069	70.15	296.12	0.00	1.69	0.37	0.63	176.08	0.00	176.08	4.000	No	No	2.00
1070	70.24	294.87	0.40	1.72	0.37	0.63	174.92	0.00	174.92	4.000	No	No	2.00
1071	70.30	298.68	1.00	1.72	0.36	0.63	178.18	0.00	178.18	4.000	No	No	2.00
1072	70.36	300.39	1.94	1.74	0.36	0.64	180.38	0.00	180.38	4.000	No	No	2.00
1073	70.44	297.68	4.12	1.76	0.36	0.63	177.20	0.03	177.23	4.000	No	No	2.00
1074	70.48	296.58	5.20	1.78	0.37	0.63	176.32	0.27	176.59	4.000	No	No	2.00
1075	70.55	289.65	7.58	1.81	0.37	0.63	171.53	2.98	174.51	4.000	No	No	2.00
1076	70.60	286.64	8.81	1.82	0.37	0.63	170.26	5.95	176.21	4.000	No	No	2.00
1077	70.69	284.63	9.88	1.84	0.36	0.63	169.94	9.26	179.20	4.000	No	No	2.00
1078	70.74	286.59	9.63	1.83	0.36	0.63	171.22	8.46	179.68	4.000	No	No	2.00
1079	70.83	284.83	10.01	1.84	0.36	0.63	170.19	9.71	179.90	4.000	No	No	2.00
1080	70.89	286.54	9.73	1.83	0.36	0.63	171.20	8.79	179.99	4.000	No	No	2.00
1081	70.94	287.44	9.67	1.83	0.36	0.63	171.86	8.61	180.47	4.000	No	No	2.00
1082	71.02	291.66	8.78	1.82	0.36	0.63	174.22	5.93	180.15	4.000	No	No	2.00
1083	71.08	292.86	8.29	1.82	0.36	0.63	174.61	4.63	179.24	4.000	No	No	2.00
1084	71.14	291.25	8.33	1.82	0.36	0.63	173.21	4.71	177.92	4.000	No	No	2.00
1085	71.22	287.54	8.41	1.82	0.37	0.63	170.03	4.87	174.90	4.000	No	No	2.00
1086	71.27	283.62	8.65	1.82	0.37	0.62	166.91	5.44	172.35	4.000	No	No	2.00
1087	71.33	279.61	8.25	1.82	0.38	0.62	162.98	4.37	167.35	4.000	No	No	2.00
1088	71.40	275.79	8.82	1.82	0.38	0.62	160.37	5.80	166.17	4.000	No	No	2.00
1089	71.47	272.68	9.37	1.83	0.38	0.61	158.41	7.34	165.75	4.000	No	No	2.00
1090	71.53	270.87	9.03	1.83	0.39	0.61	156.41	6.30	162.71	4.000	No	No	2.00
1091	71.63	266.46	8.97	1.82	0.39	0.61	152.60	6.06	158.67	4.000	No	No	2.00
1092	71.67	266.56	8.87	1.82	0.39	0.61	152.53	5.79	158.32	4.000	No	No	2.00
1093	71.73	267.56	8.29	1.82	0.39	0.60	152.67	4.33	156.99	4.000	No	No	2.00
1094	71.81	275.69	5.86	1.79	0.39	0.60	157.64	0.62	158.26	4.000	No	No	2.00
1095	71.88	288.44	3.08	1.75	0.38	0.62	168.01	0.00	168.01	4.000	No	No	2.00
1096	71.93	306.72	0.00	1.71	0.35	0.64	184.69	0.00	184.69	4.000	No	No	2.00
1097	71.99	317.26	0.00	1.68	0.34	0.65	194.23	0.00	194.23	4.000	No	No	2.00
1098	72.05	324.89	0.00	1.67	0.33	0.66	201.25	0.00	201.25	4.000	No	No	2.00
1099	72.13	332.72	0.00	1.66	0.32	0.66	208.56	0.00	208.56	4.000	No	No	2.00
1100	72.18	336.53	0.00	1.66	0.32	0.67	212.15	0.00	212.15	4.000	No	No	2.00
1101	72.27	341.55	0.00	1.65	0.31	0.67	216.90	0.00	216.90	4.000	No	No	2.00
1102	72.32	343.16	0.00	1.65	0.31	0.67	218.42	0.00	218.42	4.000	No	No	2.00
1103	72.38	342.66	0.00	1.66	0.31	0.67	217.88	0.00	217.88	4.000	No	No	2.00
1104	72.46	339.85	0.00	1.68	0.31	0.67	215.08	0.00	215.08	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1105	72.52	335.63	0.00	1.70	0.32	0.66	210.98	0.00	210.98	4.000	No	No	2.00
1106	72.62	333.22	0.00	1.71	0.32	0.66	208.59	0.00	208.59	4.000	No	No	2.00
1107	72.66	334.12	0.00	1.70	0.32	0.66	209.41	0.00	209.41	4.000	No	No	2.00
1108	72.71	336.43	0.00	1.70	0.32	0.67	211.57	0.00	211.57	4.000	No	No	2.00
1109	72.82	342.46	0.00	1.67	0.31	0.67	217.28	0.00	217.28	4.000	No	No	2.00
1110	72.85	346.07	0.00	1.67	0.30	0.67	220.76	0.00	220.76	4.000	No	No	2.00
1111	72.91	349.08	0.00	1.66	0.30	0.68	223.66	0.00	223.66	4.000	No	No	2.00
1112	72.97	354.00	0.00	1.65	0.30	0.68	228.47	0.00	228.47	4.000	No	No	2.00
1113	73.06	362.84	0.00	1.61	0.29	0.69	237.25	0.00	237.25	4.000	No	No	2.00
1114	73.11	368.16	0.00	1.60	0.28	0.70	242.61	0.00	242.61	4.000	No	No	2.00
1115	73.17	378.00	0.00	1.57	0.27	0.71	252.72	0.00	252.72	4.000	No	No	2.00
1116	73.24	383.33	0.00	1.56	0.26	0.71	257.50	0.00	257.50	4.000	No	No	2.00
1117	73.31	388.25	0.00	1.55	0.26	0.71	260.76	0.00	260.76	4.000	No	No	2.00
1118	73.37	392.06	0.00	1.55	0.26	0.71	263.29	0.00	263.29	4.000	No	No	2.00
1119	73.43	394.67	0.00	1.55	0.26	0.71	265.00	0.00	265.00	4.000	No	No	2.00
1120	73.51	398.99	0.00	1.55	0.26	0.71	267.85	0.00	267.85	4.000	No	No	2.00
1121	73.56	400.40	0.00	1.55	0.26	0.71	268.77	0.00	268.77	4.000	No	No	2.00
1122	73.65	404.41	0.00	1.55	0.26	0.71	271.40	0.00	271.40	4.000	No	No	2.00
1123	73.71	404.71	0.00	1.56	0.26	0.71	271.56	0.00	271.56	4.000	No	No	2.00
1124	73.76	405.22	0.00	1.56	0.26	0.71	271.88	0.00	271.88	4.000	No	No	2.00
1125	73.84	404.91	0.00	1.57	0.26	0.71	271.61	0.00	271.61	4.000	No	No	2.00
1126	73.90	403.41	0.00	1.58	0.26	0.71	270.57	0.00	270.57	4.000	No	No	2.00
1127	73.95	401.20	0.00	1.57	0.26	0.71	269.06	0.00	269.06	4.000	No	No	2.00
1128	74.06	396.88	0.00	1.57	0.26	0.71	266.10	0.00	266.10	4.000	No	No	2.00
1129	74.10	391.36	0.00	1.58	0.26	0.71	262.37	0.00	262.37	4.000	No	No	2.00
1130	74.15	385.64	0.00	1.57	0.26	0.71	258.51	0.00	258.51	4.000	No	No	2.00
1131	74.22	376.40	0.00	1.57	0.27	0.70	250.05	0.00	250.05	4.000	No	No	2.00
1132	74.29	371.48	0.00	1.58	0.28	0.70	244.89	0.00	244.89	4.000	No	No	2.00
1133	74.35	364.56	0.00	1.59	0.28	0.69	237.77	0.00	237.77	4.000	No	No	2.00
1134	74.43	355.32	0.00	1.61	0.30	0.68	228.42	0.00	228.42	4.000	No	No	2.00
1135	74.48	349.39	0.00	1.63	0.30	0.67	222.52	0.00	222.52	4.000	No	No	2.00
1136	74.54	295.08	3.61	1.76	0.37	0.61	171.47	0.01	171.47	4.000	No	No	2.00
1137	74.64	326.91	0.00	1.69	0.33	0.65	200.83	0.00	200.83	4.000	No	No	2.00
1138	74.69	319.78	0.00	1.71	0.34	0.64	194.17	0.00	194.17	4.000	No	No	2.00
1139	74.75	312.75	0.00	1.71	0.35	0.63	187.70	0.00	187.70	4.000	No	No	2.00
1140	74.83	303.61	0.00	1.71	0.36	0.63	179.44	0.00	179.44	4.000	No	No	2.00
1141	74.87	297.59	1.70	1.73	0.37	0.62	173.35	0.00	173.35	4.000	No	No	2.00
1142	74.94	291.67	3.86	1.76	0.38	0.61	168.24	0.02	168.25	4.000	No	No	2.00
1143	75.02	285.34	6.29	1.79	0.38	0.61	163.29	1.01	164.30	4.000	No	No	2.00
1144	75.08	276.81	8.75	1.82	0.38	0.60	158.26	5.57	163.83	4.000	No	No	2.00
1145	75.13	267.07	11.10	1.85	0.38	0.61	153.49	12.99	166.48	4.000	No	No	2.00
1146	75.22	278.61	8.11	1.81	0.39	0.60	158.93	4.00	162.93	4.000	No	No	2.00
1147	75.28	280.32	100.00	4.06	0.26	0.71	187.47	0.00	187.47	4.000	No	Yes	2.00
1148	75.33	282.33	100.00	4.06	0.26	0.71	188.80	0.00	188.80	4.000	No	Yes	2.00
1149	75.42	284.64	100.00	4.06	0.26	0.71	190.33	0.00	190.33	4.000	No	Yes	2.00
1150	75.47	286.45	100.00	4.06	0.26	0.71	191.54	0.00	191.54	4.000	No	Yes	2.00
1151	75.53	288.15	100.00	4.06	0.26	0.71	192.66	0.00	192.66	4.000	No	Yes	2.00
1152	75.62	289.46	100.00	4.06	0.26	0.71	193.52	0.00	193.52	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
$CRR_{7.5}$:	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.10	2.00	0.00	0.00	0.06	0.00	0.16	2.00	0.00	0.00	0.06	0.00
0.20	2.00	0.00	0.00	0.04	0.00	0.28	2.00	0.00	0.00	0.08	0.00
0.34	2.00	0.00	0.00	0.06	0.00	0.41	2.00	0.00	0.00	0.06	0.00
0.48	2.00	0.00	0.00	0.07	0.00	0.55	2.00	0.00	0.00	0.07	0.00
0.60	2.00	0.00	0.00	0.06	0.00	0.67	2.00	0.00	0.00	0.07	0.00
0.74	2.00	0.00	0.00	0.06	0.00	0.79	2.00	0.00	0.00	0.06	0.00
0.89	2.00	0.00	0.00	0.09	0.00	0.94	2.00	0.00	0.00	0.05	0.00
0.98	2.00	0.00	0.00	0.04	0.00	1.06	2.00	0.00	0.00	0.08	0.00
1.12	2.00	0.00	0.00	0.06	0.00	1.20	2.00	0.00	0.00	0.08	0.00
1.25	2.00	0.00	0.00	0.05	0.00	1.34	2.00	0.00	0.00	0.09	0.00
1.38	2.00	0.00	0.00	0.04	0.00	1.46	2.00	0.00	0.00	0.07	0.00
1.54	2.00	0.00	0.00	0.09	0.00	1.60	2.00	0.00	0.00	0.05	0.00
1.66	2.00	0.00	0.00	0.06	0.00	1.75	2.00	0.00	0.00	0.09	0.00
1.80	2.00	0.00	0.00	0.05	0.00	1.86	2.00	0.00	0.00	0.06	0.00
1.91	2.00	0.00	0.00	0.05	0.00	1.98	2.00	0.00	0.00	0.07	0.00
2.04	2.00	0.00	0.00	0.06	0.00	2.14	2.00	0.00	0.00	0.10	0.00
2.17	2.00	0.00	0.00	0.04	0.00	2.24	2.00	0.00	0.00	0.06	0.00
2.32	2.00	0.00	0.00	0.08	0.00	2.37	2.00	0.00	0.00	0.05	0.00
2.43	2.00	0.00	0.00	0.06	0.00	2.53	2.00	0.00	0.00	0.10	0.00
2.58	2.00	0.00	0.00	0.05	0.00	2.64	2.00	0.00	0.00	0.05	0.00
2.70	2.00	0.00	0.00	0.06	0.00	2.78	2.00	0.00	0.00	0.08	0.00
2.82	2.00	0.00	0.00	0.04	0.00	2.89	2.00	0.00	0.00	0.07	0.00
2.96	2.00	0.00	0.00	0.07	0.00	3.03	2.00	0.00	0.00	0.07	0.00
3.12	2.00	0.00	0.00	0.09	0.00	3.17	2.00	0.00	0.00	0.05	0.00
3.23	2.00	0.00	0.00	0.05	0.00	3.28	2.00	0.00	0.00	0.06	0.00
3.35	2.00	0.00	0.00	0.07	0.00	3.43	2.00	0.00	0.00	0.08	0.00
3.48	2.00	0.00	0.00	0.05	0.00	3.56	2.00	0.00	0.00	0.08	0.00
3.61	2.00	0.00	0.00	0.05	0.00	3.68	2.00	0.00	0.00	0.06	0.00
3.77	2.00	0.00	0.00	0.09	0.00	3.82	2.00	0.00	0.00	0.05	0.00
3.87	2.00	0.00	0.00	0.06	0.00	3.96	2.00	0.00	0.00	0.09	0.00
4.02	2.00	0.00	0.00	0.05	0.00	4.11	2.00	0.00	0.00	0.09	0.00
4.16	2.00	0.00	0.00	0.05	0.00	4.21	2.00	0.00	0.00	0.04	0.00
4.27	2.00	0.00	0.00	0.06	0.00	4.35	2.00	0.00	0.00	0.08	0.00
4.40	2.00	0.00	0.00	0.05	0.00	4.47	2.00	0.00	0.00	0.07	0.00
4.55	2.00	0.00	0.00	0.08	0.00	4.61	2.00	0.00	0.00	0.06	0.00
4.68	2.00	0.00	0.00	0.07	0.00	4.75	2.00	0.00	0.00	0.08	0.00
4.80	2.00	0.00	0.00	0.04	0.00	4.86	2.00	0.00	0.00	0.07	0.00
4.93	2.00	0.00	0.00	0.07	0.00	5.00	2.00	0.00	0.00	0.06	0.00
5.05	2.00	0.00	0.00	0.06	0.00	5.14	2.00	0.00	0.00	0.08	0.00
5.19	2.00	0.00	0.00	0.06	0.00	5.28	2.00	0.00	0.00	0.08	0.00
5.34	2.00	0.00	0.00	0.06	0.00	5.38	2.00	0.00	0.00	0.05	0.00
5.45	2.00	0.00	0.00	0.06	0.00	5.54	2.00	0.00	0.00	0.09	0.00
5.59	2.00	0.00	0.00	0.05	0.00	5.65	2.00	0.00	0.00	0.06	0.00
5.73	2.00	0.00	0.00	0.09	0.00	5.79	2.00	0.00	0.00	0.06	0.00
5.84	2.00	0.00	0.00	0.05	0.00	5.94	2.00	0.00	0.00	0.10	0.00
5.99	2.00	0.00	0.00	0.05	0.00	6.04	2.00	0.00	0.00	0.04	0.00
6.12	2.00	0.00	0.00	0.09	0.00	6.19	2.00	0.00	0.00	0.06	0.00
6.24	2.00	0.00	0.00	0.05	0.00	6.31	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
6.37	2.00	0.00	0.00	0.06	0.00	6.44	2.00	0.00	0.00	0.07	0.00
6.52	2.00	0.00	0.00	0.09	0.00	6.58	2.00	0.00	0.00	0.06	0.00
6.64	2.00	0.00	0.00	0.05	0.00	6.72	2.00	0.00	0.00	0.09	0.00
6.78	2.00	0.00	0.00	0.06	0.00	6.84	2.00	0.00	0.00	0.06	0.00
6.92	2.00	0.00	0.00	0.09	0.00	6.98	2.00	0.00	0.00	0.06	0.00
7.03	2.00	0.00	0.00	0.04	0.00	7.09	2.00	0.00	0.00	0.06	0.00
7.18	2.00	0.00	0.00	0.09	0.00	7.22	2.00	0.00	0.00	0.04	0.00
7.33	2.00	0.00	0.00	0.11	0.00	7.38	2.00	0.00	0.00	0.05	0.00
7.43	2.00	0.00	0.00	0.05	0.00	7.52	2.00	0.00	0.00	0.09	0.00
7.58	2.00	0.00	0.00	0.06	0.00	7.62	2.00	0.00	0.00	0.05	0.00
7.72	2.00	0.00	0.00	0.09	0.00	7.76	2.00	0.00	0.00	0.05	0.00
7.82	2.00	0.00	0.00	0.06	0.00	7.90	2.00	0.00	0.00	0.08	0.00
7.97	2.00	0.00	0.00	0.07	0.00	8.02	0.33	0.67	0.34	0.05	0.09
8.07	0.33	0.67	0.34	0.05	0.10	8.16	0.33	0.67	0.34	0.09	0.17
8.21	0.33	0.67	0.34	0.04	0.08	8.27	0.33	0.67	0.34	0.06	0.12
8.35	0.33	0.67	0.34	0.08	0.14	8.41	0.32	0.68	0.33	0.06	0.11
8.49	0.32	0.68	0.33	0.08	0.14	8.55	0.32	0.68	0.33	0.06	0.12
8.62	0.31	0.69	0.33	0.06	0.12	8.67	0.31	0.69	0.33	0.05	0.09
8.76	0.29	0.71	0.32	0.09	0.17	8.80	0.28	0.72	0.31	0.05	0.09
8.86	0.27	0.73	0.31	0.05	0.10	8.95	0.25	0.75	0.30	0.09	0.18
8.99	0.23	0.77	0.29	0.04	0.08	9.06	0.22	0.78	0.29	0.07	0.14
9.15	0.22	0.78	0.28	0.09	0.19	9.22	0.21	0.79	0.28	0.06	0.13
9.26	0.21	0.79	0.28	0.04	0.09	9.35	0.21	0.79	0.28	0.09	0.18
9.40	0.21	0.79	0.28	0.05	0.11	9.46	0.21	0.79	0.28	0.06	0.12
9.54	0.20	0.80	0.28	0.08	0.17	9.60	0.20	0.80	0.28	0.06	0.13
9.66	0.20	0.80	0.28	0.06	0.12	9.72	0.19	0.81	0.27	0.07	0.14
9.80	0.18	0.82	0.27	0.08	0.16	9.85	0.18	0.82	0.27	0.05	0.10
9.96	2.00	0.00	0.00	0.11	0.00	10.00	2.00	0.00	0.00	0.05	0.00
10.05	2.00	0.00	0.00	0.05	0.00	10.12	2.00	0.00	0.00	0.06	0.00
10.18	2.00	0.00	0.00	0.06	0.00	10.27	2.00	0.00	0.00	0.09	0.00
10.33	2.00	0.00	0.00	0.06	0.00	10.37	2.00	0.00	0.00	0.05	0.00
10.47	2.00	0.00	0.00	0.10	0.00	10.53	2.00	0.00	0.00	0.05	0.00
10.57	2.00	0.00	0.00	0.04	0.00	10.67	2.00	0.00	0.00	0.10	0.00
10.70	2.00	0.00	0.00	0.03	0.00	10.78	0.18	0.82	0.27	0.08	0.17
10.83	0.18	0.82	0.27	0.04	0.09	10.91	0.18	0.82	0.27	0.08	0.17
10.97	0.18	0.82	0.27	0.06	0.12	11.03	0.19	0.81	0.27	0.06	0.12
11.10	0.19	0.81	0.27	0.07	0.14	11.17	0.19	0.81	0.27	0.07	0.14
11.26	0.19	0.81	0.27	0.09	0.19	11.31	0.19	0.81	0.27	0.05	0.11
11.36	0.19	0.81	0.27	0.05	0.10	11.44	0.19	0.81	0.27	0.08	0.16
11.50	0.19	0.81	0.27	0.06	0.12	11.56	0.19	0.81	0.27	0.06	0.13
11.63	0.19	0.81	0.27	0.06	0.13	11.69	0.19	0.81	0.27	0.07	0.13
11.76	0.19	0.81	0.27	0.06	0.13	11.86	0.18	0.82	0.27	0.10	0.20
11.89	0.18	0.82	0.27	0.03	0.06	11.95	0.18	0.82	0.27	0.06	0.13
12.01	0.18	0.82	0.27	0.06	0.12	12.10	0.18	0.82	0.27	0.09	0.18
12.15	0.18	0.82	0.27	0.04	0.09	12.21	0.18	0.82	0.27	0.06	0.13
12.28	0.18	0.82	0.27	0.07	0.15	12.36	0.18	0.82	0.27	0.07	0.15
12.40	0.18	0.82	0.27	0.05	0.10	12.47	0.18	0.82	0.27	0.07	0.14
12.55	0.18	0.82	0.27	0.08	0.16	12.60	0.18	0.82	0.27	0.05	0.10

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
12.69	0.18	0.82	0.27	0.09	0.18	12.74	0.18	0.82	0.27	0.05	0.11
12.82	0.19	0.81	0.27	0.07	0.14	12.88	0.19	0.81	0.27	0.07	0.13
12.94	0.19	0.81	0.27	0.06	0.11	13.00	0.19	0.81	0.27	0.06	0.11
13.09	0.19	0.81	0.27	0.09	0.18	13.14	0.19	0.81	0.27	0.05	0.10
13.20	0.19	0.81	0.27	0.06	0.11	13.27	0.19	0.81	0.27	0.08	0.15
13.34	0.19	0.81	0.27	0.07	0.13	13.39	0.19	0.81	0.27	0.05	0.09
13.47	0.19	0.81	0.27	0.09	0.17	13.54	0.19	0.81	0.27	0.07	0.13
13.59	0.19	0.81	0.27	0.06	0.11	13.65	0.19	0.81	0.27	0.06	0.11
13.72	0.19	0.81	0.27	0.07	0.14	13.79	0.19	0.81	0.27	0.07	0.13
13.85	0.19	0.81	0.27	0.07	0.13	13.94	0.18	0.82	0.27	0.08	0.16
13.98	0.18	0.82	0.27	0.05	0.10	14.08	0.18	0.82	0.27	0.10	0.19
14.13	0.18	0.82	0.27	0.05	0.09	14.18	0.18	0.82	0.27	0.05	0.10
14.27	0.18	0.82	0.27	0.09	0.19	14.33	0.18	0.82	0.27	0.06	0.12
14.39	0.18	0.82	0.27	0.05	0.10	14.44	0.17	0.83	0.27	0.06	0.11
14.53	0.17	0.83	0.27	0.09	0.17	14.59	0.17	0.83	0.26	0.05	0.11
14.64	0.16	0.84	0.26	0.05	0.10	14.73	0.16	0.84	0.26	0.09	0.18
14.77	0.16	0.84	0.26	0.04	0.08	14.83	2.00	0.00	0.00	0.06	0.00
14.93	2.00	0.00	0.00	0.10	0.00	14.98	2.00	0.00	0.00	0.05	0.00
15.03	2.00	0.00	0.00	0.05	0.00	15.10	2.00	0.00	0.00	0.07	0.00
15.17	2.00	0.00	0.00	0.07	0.00	15.22	2.00	0.00	0.00	0.05	0.00
15.29	2.00	0.00	0.00	0.07	0.00	15.37	2.00	0.00	0.00	0.07	0.00
15.44	2.00	0.00	0.00	0.07	0.00	15.52	2.00	0.00	0.00	0.09	0.00
15.56	2.00	0.00	0.00	0.04	0.00	15.62	2.00	0.00	0.00	0.06	0.00
15.70	2.00	0.00	0.00	0.08	0.00	15.76	2.00	0.00	0.00	0.06	0.00
15.82	2.00	0.00	0.00	0.06	0.00	15.91	2.00	0.00	0.00	0.09	0.00
15.95	2.00	0.00	0.00	0.03	0.00	16.01	2.00	0.00	0.00	0.06	0.00
16.08	2.00	0.00	0.00	0.07	0.00	16.14	2.00	0.00	0.00	0.07	0.00
16.22	2.00	0.00	0.00	0.07	0.00	16.31	2.00	0.00	0.00	0.09	0.00
16.36	2.00	0.00	0.00	0.05	0.00	16.41	2.00	0.00	0.00	0.05	0.00
16.50	2.00	0.00	0.00	0.08	0.00	16.55	2.00	0.00	0.00	0.06	0.00
16.61	2.00	0.00	0.00	0.05	0.00	16.69	2.00	0.00	0.00	0.08	0.00
16.74	2.00	0.00	0.00	0.05	0.00	16.80	0.15	0.85	0.26	0.07	0.13
16.88	0.15	0.85	0.26	0.07	0.14	16.95	0.15	0.85	0.26	0.07	0.13
17.00	0.15	0.85	0.26	0.06	0.11	17.07	0.16	0.84	0.26	0.07	0.14
17.15	0.16	0.84	0.26	0.08	0.15	17.20	0.16	0.84	0.26	0.05	0.09
17.26	0.16	0.84	0.26	0.06	0.12	17.33	0.16	0.84	0.26	0.07	0.13
17.41	0.16	0.84	0.26	0.08	0.15	17.46	0.16	0.84	0.26	0.05	0.10
17.52	0.16	0.84	0.26	0.06	0.11	17.60	0.16	0.84	0.26	0.08	0.15
17.65	0.16	0.84	0.26	0.05	0.09	17.74	0.16	0.84	0.26	0.09	0.17
17.80	0.16	0.84	0.26	0.05	0.10	17.85	0.16	0.84	0.26	0.05	0.10
17.93	0.16	0.84	0.26	0.08	0.15	17.99	0.16	0.84	0.26	0.06	0.12
18.07	0.16	0.84	0.26	0.07	0.14	18.13	0.17	0.83	0.26	0.06	0.11
18.18	0.17	0.83	0.27	0.06	0.10	18.29	0.17	0.83	0.27	0.10	0.19
18.32	0.17	0.83	0.27	0.03	0.06	18.38	0.17	0.83	0.27	0.06	0.10
18.44	0.17	0.83	0.27	0.06	0.11	18.53	0.18	0.82	0.27	0.09	0.17
18.58	0.18	0.82	0.27	0.05	0.09	18.66	0.17	0.83	0.27	0.07	0.13
18.71	0.18	0.82	0.27	0.05	0.10	18.81	0.18	0.82	0.27	0.10	0.17
18.85	0.18	0.82	0.27	0.05	0.08	18.90	0.19	0.81	0.27	0.05	0.09

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
19.01	0.19	0.81	0.27	0.10	0.18	19.06	0.19	0.81	0.27	0.05	0.10
19.11	0.19	0.81	0.27	0.05	0.09	19.16	0.19	0.81	0.27	0.05	0.09
19.26	0.18	0.82	0.27	0.10	0.17	19.30	0.18	0.82	0.27	0.04	0.06
19.36	0.18	0.82	0.27	0.07	0.11	19.45	0.18	0.82	0.27	0.09	0.16
19.50	0.18	0.82	0.27	0.05	0.09	19.58	0.17	0.83	0.27	0.08	0.14
19.64	0.17	0.83	0.27	0.05	0.09	19.69	0.17	0.83	0.27	0.06	0.10
19.78	0.17	0.83	0.26	0.08	0.15	19.84	0.17	0.83	0.26	0.07	0.12
19.90	0.16	0.84	0.26	0.06	0.10	19.95	0.16	0.84	0.26	0.05	0.09
20.03	0.16	0.84	0.26	0.07	0.13	20.08	0.16	0.84	0.26	0.06	0.10
20.16	0.16	0.84	0.26	0.07	0.13	20.25	2.00	0.00	0.00	0.09	0.00
20.30	2.00	0.00	0.00	0.05	0.00	20.35	2.00	0.00	0.00	0.05	0.00
20.45	0.16	0.84	0.26	0.10	0.17	20.50	0.16	0.84	0.26	0.05	0.09
20.54	0.16	0.84	0.26	0.04	0.07	20.62	0.16	0.84	0.26	0.09	0.15
20.69	0.16	0.84	0.26	0.07	0.11	20.74	0.16	0.84	0.26	0.05	0.10
20.83	0.17	0.83	0.26	0.09	0.15	20.88	0.17	0.83	0.26	0.05	0.08
20.94	0.17	0.83	0.26	0.06	0.11	21.04	0.17	0.83	0.26	0.10	0.17
21.08	0.17	0.83	0.26	0.05	0.08	21.14	0.17	0.83	0.26	0.06	0.10
21.23	0.17	0.83	0.26	0.09	0.15	21.28	0.17	0.83	0.26	0.05	0.09
21.33	0.17	0.83	0.26	0.05	0.09	21.42	0.17	0.83	0.26	0.09	0.15
21.48	0.17	0.83	0.26	0.06	0.10	21.53	0.17	0.83	0.26	0.05	0.09
21.62	0.17	0.83	0.27	0.09	0.16	21.68	0.17	0.83	0.27	0.05	0.09
21.73	0.17	0.83	0.27	0.05	0.09	21.79	0.18	0.82	0.27	0.06	0.11
21.86	0.19	0.81	0.27	0.07	0.12	21.92	0.19	0.81	0.27	0.05	0.09
22.00	0.20	0.80	0.28	0.08	0.13	22.05	0.21	0.79	0.28	0.05	0.08
22.12	0.21	0.79	0.28	0.08	0.12	22.22	0.23	0.77	0.29	0.09	0.14
22.27	0.24	0.76	0.29	0.06	0.09	22.32	0.25	0.75	0.30	0.05	0.08
22.38	0.27	0.73	0.31	0.06	0.09	22.47	0.29	0.71	0.32	0.09	0.13
22.52	0.30	0.70	0.32	0.05	0.07	22.59	0.32	0.68	0.33	0.08	0.10
22.65	0.33	0.67	0.34	0.06	0.08	22.71	0.33	0.67	0.34	0.06	0.08
22.77	0.32	0.68	0.33	0.06	0.08	22.85	0.30	0.70	0.32	0.08	0.11
22.90	0.28	0.72	0.31	0.05	0.08	22.98	0.27	0.73	0.31	0.08	0.11
23.06	0.27	0.73	0.31	0.08	0.11	23.10	0.28	0.72	0.31	0.04	0.06
23.17	0.29	0.71	0.32	0.07	0.10	23.24	0.29	0.71	0.32	0.07	0.10
23.32	0.29	0.71	0.32	0.07	0.10	23.37	0.29	0.71	0.32	0.05	0.07
23.45	0.30	0.70	0.32	0.08	0.11	23.51	0.30	0.70	0.32	0.06	0.08
23.56	0.30	0.70	0.33	0.05	0.07	23.63	0.33	0.67	0.34	0.07	0.09
23.71	0.35	0.65	0.35	0.08	0.10	23.77	0.40	0.60	0.38	0.06	0.07
23.84	0.43	0.57	0.41	0.06	0.07	23.89	0.47	0.53	0.45	0.05	0.05
23.95	0.48	0.52	0.46	0.06	0.06	24.05	0.47	0.53	0.45	0.09	0.10
24.09	0.46	0.54	0.44	0.05	0.05	24.15	0.45	0.55	0.43	0.06	0.06
24.24	0.41	0.59	0.40	0.09	0.10	24.30	0.39	0.61	0.38	0.06	0.08
24.37	0.36	0.64	0.36	0.06	0.08	24.42	0.34	0.66	0.34	0.05	0.07
24.48	0.33	0.67	0.34	0.06	0.07	24.54	0.32	0.68	0.33	0.06	0.08
24.61	0.30	0.70	0.32	0.07	0.10	24.71	0.26	0.74	0.30	0.09	0.13
24.76	0.24	0.76	0.29	0.05	0.08	24.81	0.21	0.79	0.28	0.05	0.08
24.90	0.19	0.81	0.27	0.09	0.13	24.96	0.17	0.83	0.27	0.06	0.09
25.00	0.16	0.84	0.26	0.05	0.07	25.09	0.15	0.85	0.26	0.08	0.13
25.16	2.00	0.00	0.00	0.07	0.00	25.20	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
25.30	2.00	0.00	0.00	0.09	0.00	25.36	2.00	0.00	0.00	0.06	0.00
25.40	2.00	0.00	0.00	0.04	0.00	25.48	2.00	0.00	0.00	0.08	0.00
25.53	2.00	0.00	0.00	0.05	0.00	25.59	2.00	0.00	0.00	0.06	0.00
25.67	2.00	0.00	0.00	0.08	0.00	25.75	2.00	0.00	0.00	0.08	0.00
25.80	2.00	0.00	0.00	0.05	0.00	25.87	2.00	0.00	0.00	0.07	0.00
25.95	2.00	0.00	0.00	0.08	0.00	25.99	2.00	0.00	0.00	0.05	0.00
26.09	0.16	0.84	0.26	0.10	0.15	26.14	0.18	0.82	0.27	0.06	0.08
26.19	0.19	0.81	0.27	0.05	0.07	26.27	0.22	0.78	0.28	0.08	0.11
26.33	0.24	0.76	0.29	0.06	0.08	26.39	0.26	0.74	0.30	0.06	0.08
26.45	0.29	0.71	0.32	0.06	0.08	26.53	0.31	0.69	0.33	0.08	0.10
26.59	0.31	0.69	0.33	0.06	0.08	26.64	0.28	0.72	0.31	0.05	0.07
26.73	0.25	0.75	0.30	0.09	0.12	26.79	0.23	0.77	0.29	0.06	0.08
26.86	0.20	0.80	0.28	0.08	0.11	26.93	0.19	0.81	0.27	0.07	0.10
26.99	0.17	0.83	0.27	0.05	0.08	27.08	2.00	0.00	0.00	0.09	0.00
27.13	2.00	0.00	0.00	0.05	0.00	27.17	2.00	0.00	0.00	0.04	0.00
27.25	2.00	0.00	0.00	0.08	0.00	27.32	2.00	0.00	0.00	0.07	0.00
27.38	2.00	0.00	0.00	0.06	0.00	27.44	2.00	0.00	0.00	0.06	0.00
27.53	2.00	0.00	0.00	0.09	0.00	27.58	2.00	0.00	0.00	0.05	0.00
27.63	2.00	0.00	0.00	0.05	0.00	27.71	2.00	0.00	0.00	0.08	0.00
27.77	2.00	0.00	0.00	0.06	0.00	27.82	2.00	0.00	0.00	0.05	0.00
27.90	0.15	0.85	0.26	0.08	0.12	27.97	0.16	0.84	0.26	0.06	0.10
28.02	0.18	0.82	0.27	0.05	0.08	28.12	0.24	0.76	0.29	0.10	0.14
28.17	0.27	0.73	0.31	0.05	0.06	28.23	0.29	0.71	0.32	0.05	0.07
28.31	0.29	0.71	0.32	0.09	0.11	28.37	0.28	0.72	0.31	0.06	0.07
28.42	0.26	0.74	0.30	0.05	0.06	28.51	0.23	0.77	0.29	0.09	0.12
28.55	0.21	0.79	0.28	0.05	0.06	28.61	0.19	0.81	0.27	0.06	0.08
28.71	0.17	0.83	0.27	0.10	0.14	28.76	2.00	0.00	0.00	0.04	0.00
28.81	2.00	0.00	0.00	0.05	0.00	28.91	2.00	0.00	0.00	0.10	0.00
28.95	2.00	0.00	0.00	0.04	0.00	29.00	2.00	0.00	0.00	0.05	0.00
29.07	2.00	0.00	0.00	0.06	0.00	29.16	2.00	0.00	0.00	0.10	0.00
29.21	2.00	0.00	0.00	0.05	0.00	29.30	2.00	0.00	0.00	0.09	0.00
29.36	2.00	0.00	0.00	0.05	0.00	29.41	0.15	0.85	0.26	0.05	0.08
29.50	0.17	0.83	0.27	0.09	0.12	29.56	0.18	0.82	0.27	0.06	0.08
29.61	0.19	0.81	0.27	0.05	0.07	29.69	0.19	0.81	0.27	0.08	0.11
29.76	0.19	0.81	0.27	0.07	0.09	29.80	0.18	0.82	0.27	0.04	0.06
29.89	0.16	0.84	0.26	0.08	0.12	29.93	0.15	0.85	0.26	0.05	0.06
30.00	2.00	0.00	0.00	0.06	0.00	30.06	2.00	0.00	0.00	0.06	0.00
30.13	2.00	0.00	0.00	0.08	0.00	30.21	2.00	0.00	0.00	0.08	0.00
30.27	2.00	0.00	0.00	0.05	0.00	30.36	2.00	0.00	0.00	0.09	0.00
30.41	2.00	0.00	0.00	0.05	0.00	30.46	2.00	0.00	0.00	0.05	0.00
30.55	2.00	0.00	0.00	0.09	0.00	30.60	2.00	0.00	0.00	0.05	0.00
30.65	2.00	0.00	0.00	0.05	0.00	30.73	2.00	0.00	0.00	0.08	0.00
30.80	2.00	0.00	0.00	0.07	0.00	30.85	2.00	0.00	0.00	0.05	0.00
30.95	2.00	0.00	0.00	0.09	0.00	30.99	2.00	0.00	0.00	0.04	0.00
31.05	2.00	0.00	0.00	0.06	0.00	31.15	2.00	0.00	0.00	0.10	0.00
31.18	2.00	0.00	0.00	0.03	0.00	31.23	2.00	0.00	0.00	0.06	0.00
31.30	2.00	0.00	0.00	0.07	0.00	31.39	2.00	0.00	0.00	0.09	0.00
31.45	2.00	0.00	0.00	0.05	0.00	31.50	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
31.58	2.00	0.00	0.00	0.08	0.00	31.64	2.00	0.00	0.00	0.05	0.00
31.70	2.00	0.00	0.00	0.06	0.00	31.78	2.00	0.00	0.00	0.09	0.00
31.84	2.00	0.00	0.00	0.05	0.00	31.90	2.00	0.00	0.00	0.06	0.00
31.96	2.00	0.00	0.00	0.06	0.00	32.03	2.00	0.00	0.00	0.07	0.00
32.09	2.00	0.00	0.00	0.06	0.00	32.19	2.00	0.00	0.00	0.10	0.00
32.24	2.00	0.00	0.00	0.05	0.00	32.32	2.00	0.00	0.00	0.08	0.00
32.39	2.00	0.00	0.00	0.06	0.00	32.43	2.00	0.00	0.00	0.04	0.00
32.48	2.00	0.00	0.00	0.06	0.00	32.55	2.00	0.00	0.00	0.07	0.00
32.62	2.00	0.00	0.00	0.06	0.00	32.69	2.00	0.00	0.00	0.07	0.00
32.78	2.00	0.00	0.00	0.09	0.00	32.82	2.00	0.00	0.00	0.04	0.00
32.88	2.00	0.00	0.00	0.06	0.00	32.97	2.00	0.00	0.00	0.09	0.00
33.02	2.00	0.00	0.00	0.05	0.00	33.08	2.00	0.00	0.00	0.05	0.00
33.17	2.00	0.00	0.00	0.09	0.00	33.21	2.00	0.00	0.00	0.04	0.00
33.29	2.00	0.00	0.00	0.08	0.00	33.37	2.00	0.00	0.00	0.08	0.00
33.41	2.00	0.00	0.00	0.05	0.00	33.47	2.00	0.00	0.00	0.06	0.00
33.56	2.00	0.00	0.00	0.09	0.00	33.61	2.00	0.00	0.00	0.05	0.00
33.68	2.00	0.00	0.00	0.06	0.00	33.77	2.00	0.00	0.00	0.09	0.00
33.82	2.00	0.00	0.00	0.05	0.00	33.87	2.00	0.00	0.00	0.05	0.00
33.97	2.00	0.00	0.00	0.10	0.00	34.01	2.00	0.00	0.00	0.03	0.00
34.08	2.00	0.00	0.00	0.08	0.00	34.13	2.00	0.00	0.00	0.05	0.00
34.19	2.00	0.00	0.00	0.06	0.00	34.27	2.00	0.00	0.00	0.08	0.00
34.36	2.00	0.00	0.00	0.09	0.00	34.41	2.00	0.00	0.00	0.05	0.00
34.46	2.00	0.00	0.00	0.05	0.00	34.54	2.00	0.00	0.00	0.09	0.00
34.60	2.00	0.00	0.00	0.06	0.00	34.65	2.00	0.00	0.00	0.05	0.00
34.73	2.00	0.00	0.00	0.08	0.00	34.80	2.00	0.00	0.00	0.07	0.00
34.85	2.00	0.00	0.00	0.05	0.00	34.92	2.00	0.00	0.00	0.07	0.00
34.98	2.00	0.00	0.00	0.05	0.00	35.04	2.00	0.00	0.00	0.06	0.00
35.12	2.00	0.00	0.00	0.08	0.00	35.17	2.00	0.00	0.00	0.05	0.00
35.25	2.00	0.00	0.00	0.07	0.00	35.32	2.00	0.00	0.00	0.07	0.00
35.37	2.00	0.00	0.00	0.06	0.00	35.44	2.00	0.00	0.00	0.07	0.00
35.50	2.00	0.00	0.00	0.06	0.00	35.60	2.00	0.00	0.00	0.10	0.00
35.65	2.00	0.00	0.00	0.05	0.00	35.70	2.00	0.00	0.00	0.06	0.00
35.79	2.00	0.00	0.00	0.09	0.00	35.85	2.00	0.00	0.00	0.06	0.00
35.90	2.00	0.00	0.00	0.05	0.00	35.98	2.00	0.00	0.00	0.08	0.00
36.03	2.00	0.00	0.00	0.06	0.00	36.09	2.00	0.00	0.00	0.06	0.00
36.18	2.00	0.00	0.00	0.09	0.00	36.24	2.00	0.00	0.00	0.06	0.00
36.29	2.00	0.00	0.00	0.05	0.00	36.38	2.00	0.00	0.00	0.09	0.00
36.44	2.00	0.00	0.00	0.06	0.00	36.49	2.00	0.00	0.00	0.05	0.00
36.57	2.00	0.00	0.00	0.09	0.00	36.63	2.00	0.00	0.00	0.06	0.00
36.69	2.00	0.00	0.00	0.05	0.00	36.77	2.00	0.00	0.00	0.09	0.00
36.83	2.00	0.00	0.00	0.05	0.00	36.88	2.00	0.00	0.00	0.06	0.00
36.96	2.00	0.00	0.00	0.08	0.00	37.03	2.00	0.00	0.00	0.07	0.00
37.08	2.00	0.00	0.00	0.05	0.00	37.14	2.00	0.00	0.00	0.06	0.00
37.23	0.14	0.86	0.25	0.09	0.11	37.28	0.15	0.85	0.26	0.05	0.05
37.36	2.00	0.00	0.00	0.08	0.00	37.41	2.00	0.00	0.00	0.05	0.00
37.48	2.00	0.00	0.00	0.07	0.00	37.57	2.00	0.00	0.00	0.09	0.00
37.63	2.00	0.00	0.00	0.06	0.00	37.66	2.00	0.00	0.00	0.04	0.00
37.77	2.00	0.00	0.00	0.11	0.00	37.82	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
37.88	2.00	0.00	0.00	0.05	0.00	37.96	2.00	0.00	0.00	0.09	0.00
38.01	2.00	0.00	0.00	0.05	0.00	38.06	2.00	0.00	0.00	0.05	0.00
38.13	2.00	0.00	0.00	0.07	0.00	38.19	2.00	0.00	0.00	0.06	0.00
38.26	2.00	0.00	0.00	0.06	0.00	38.32	2.00	0.00	0.00	0.07	0.00
38.41	2.00	0.00	0.00	0.09	0.00	38.46	2.00	0.00	0.00	0.05	0.00
38.52	2.00	0.00	0.00	0.06	0.00	38.59	2.00	0.00	0.00	0.08	0.00
38.65	2.00	0.00	0.00	0.06	0.00	38.73	2.00	0.00	0.00	0.08	0.00
38.79	2.00	0.00	0.00	0.05	0.00	38.86	2.00	0.00	0.00	0.08	0.00
38.92	2.00	0.00	0.00	0.06	0.00	38.98	2.00	0.00	0.00	0.06	0.00
39.06	0.16	0.84	0.26	0.08	0.08	39.12	0.17	0.83	0.27	0.05	0.06
39.18	0.19	0.81	0.27	0.06	0.06	39.28	0.23	0.77	0.29	0.10	0.10
39.32	0.24	0.76	0.29	0.04	0.03	39.37	0.28	0.72	0.31	0.06	0.05
39.48	0.35	0.65	0.35	0.10	0.08	39.52	0.38	0.62	0.37	0.04	0.03
39.57	0.42	0.58	0.40	0.06	0.04	39.66	0.43	0.57	0.41	0.09	0.06
39.70	0.38	0.62	0.37	0.04	0.03	39.77	0.46	0.54	0.44	0.07	0.05
39.87	0.53	0.47	0.52	0.09	0.05	39.92	0.60	0.40	0.63	0.05	0.02
39.98	0.70	0.30	0.91	0.06	0.02	40.06	0.31	0.69	0.33	0.09	0.07
40.12	1.06	0.00	0.00	0.06	0.00	40.16	1.29	0.00	0.00	0.05	0.00
40.25	1.80	0.00	0.00	0.08	0.00	40.31	1.97	0.00	0.00	0.07	0.00
40.37	1.97	0.00	0.00	0.05	0.00	40.44	1.77	0.00	0.00	0.07	0.00
40.50	1.58	0.00	0.00	0.06	0.00	40.56	1.43	0.00	0.00	0.06	0.00
40.63	1.22	0.00	0.00	0.07	0.00	40.71	1.09	0.00	0.00	0.08	0.00
40.77	0.96	0.00	0.00	0.06	0.00	40.86	0.84	0.00	0.00	0.09	0.02
40.90	0.76	0.00	0.00	0.04	0.01	40.96	0.67	0.33	0.81	0.06	0.02
41.03	0.56	0.44	0.56	0.07	0.04	41.09	0.50	0.50	0.48	0.06	0.03
41.15	0.45	0.55	0.43	0.05	0.03	41.24	0.40	0.60	0.39	0.09	0.06
41.28	0.37	0.63	0.36	0.04	0.03	41.35	0.35	0.65	0.35	0.07	0.05
41.41	0.32	0.68	0.33	0.07	0.05	41.50	0.30	0.70	0.32	0.09	0.07
41.55	0.29	0.71	0.32	0.05	0.04	41.61	0.27	0.73	0.31	0.06	0.05
41.71	0.26	0.74	0.30	0.10	0.08	41.75	0.25	0.75	0.30	0.05	0.04
41.80	0.25	0.75	0.30	0.05	0.04	41.87	0.24	0.76	0.29	0.07	0.06
41.93	0.24	0.76	0.29	0.05	0.05	42.00	0.23	0.77	0.29	0.07	0.06
42.09	0.22	0.78	0.28	0.08	0.07	42.14	0.21	0.79	0.28	0.06	0.05
42.20	0.21	0.79	0.28	0.05	0.05	42.29	0.20	0.80	0.28	0.09	0.08
42.34	0.20	0.80	0.28	0.05	0.05	42.39	0.20	0.80	0.28	0.05	0.04
42.48	0.20	0.80	0.28	0.09	0.07	42.54	0.20	0.80	0.28	0.07	0.06
42.59	0.20	0.80	0.28	0.05	0.04	42.68	0.20	0.80	0.28	0.08	0.07
42.73	0.20	0.80	0.28	0.05	0.05	42.79	0.20	0.80	0.28	0.05	0.05
42.88	0.19	0.81	0.27	0.10	0.08	42.93	0.19	0.81	0.27	0.05	0.04
42.99	0.19	0.81	0.27	0.06	0.05	43.06	0.18	0.82	0.27	0.07	0.06
43.14	0.18	0.82	0.27	0.08	0.07	43.18	0.17	0.83	0.27	0.05	0.04
43.28	0.16	0.84	0.26	0.10	0.08	43.33	0.16	0.84	0.26	0.05	0.05
43.42	2.00	0.00	0.00	0.09	0.00	43.44	2.00	0.00	0.00	0.02	0.00
43.53	2.00	0.00	0.00	0.09	0.00	43.58	2.00	0.00	0.00	0.05	0.00
43.67	2.00	0.00	0.00	0.09	0.00	43.73	2.00	0.00	0.00	0.06	0.00
43.78	2.00	0.00	0.00	0.05	0.00	43.86	2.00	0.00	0.00	0.08	0.00
43.92	2.00	0.00	0.00	0.06	0.00	43.97	2.00	0.00	0.00	0.05	0.00
44.06	2.00	0.00	0.00	0.09	0.00	44.12	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
44.17	2.00	0.00	0.00	0.05	0.00	44.26	2.00	0.00	0.00	0.09	0.00
44.30	2.00	0.00	0.00	0.04	0.00	44.37	2.00	0.00	0.00	0.07	0.00
44.44	2.00	0.00	0.00	0.06	0.00	44.50	2.00	0.00	0.00	0.06	0.00
44.59	2.00	0.00	0.00	0.09	0.00	44.64	2.00	0.00	0.00	0.05	0.00
44.73	2.00	0.00	0.00	0.09	0.00	44.77	2.00	0.00	0.00	0.05	0.00
44.83	2.00	0.00	0.00	0.06	0.00	44.88	2.00	0.00	0.00	0.05	0.00
44.96	2.00	0.00	0.00	0.08	0.00	45.03	2.00	0.00	0.00	0.07	0.00
45.08	2.00	0.00	0.00	0.05	0.00	45.17	2.00	0.00	0.00	0.08	0.00
45.22	2.00	0.00	0.00	0.06	0.00	45.28	2.00	0.00	0.00	0.06	0.00
45.36	2.00	0.00	0.00	0.08	0.00	45.41	2.00	0.00	0.00	0.05	0.00
45.48	2.00	0.00	0.00	0.06	0.00	45.54	2.00	0.00	0.00	0.07	0.00
45.63	2.00	0.00	0.00	0.08	0.00	45.67	2.00	0.00	0.00	0.05	0.00
45.74	2.00	0.00	0.00	0.07	0.00	45.83	2.00	0.00	0.00	0.09	0.00
45.88	0.18	0.82	0.27	0.05	0.04	45.97	0.22	0.78	0.29	0.09	0.06
46.03	0.24	0.76	0.29	0.06	0.04	46.07	0.27	0.73	0.31	0.05	0.03
46.17	0.32	0.68	0.33	0.10	0.06	46.22	0.36	0.64	0.35	0.05	0.03
46.27	0.40	0.60	0.39	0.05	0.03	46.36	0.48	0.52	0.46	0.09	0.04
46.41	0.54	0.46	0.53	0.05	0.02	46.49	0.71	0.29	0.95	0.07	0.02
46.54	0.95	0.00	0.00	0.05	0.00	46.62	1.53	0.00	0.00	0.08	0.00
46.66	1.76	0.00	0.00	0.03	0.00	46.73	2.00	0.00	0.00	0.08	0.00
46.82	2.00	0.00	0.00	0.08	0.00	46.85	2.00	0.00	0.00	0.03	0.00
46.92	1.84	0.00	0.00	0.07	0.00	47.01	1.65	0.00	0.00	0.09	0.00
47.06	1.50	0.00	0.00	0.05	0.00	47.15	1.26	0.00	0.00	0.09	0.00
47.21	1.24	0.00	0.00	0.06	0.00	47.25	1.19	0.00	0.00	0.04	0.00
47.31	0.88	0.00	0.00	0.06	0.01	47.41	1.05	0.00	0.00	0.09	0.00
47.46	1.21	0.00	0.00	0.05	0.00	47.54	1.45	0.00	0.00	0.08	0.00
47.58	1.53	0.00	0.00	0.05	0.00	47.67	1.89	0.00	0.00	0.09	0.00
47.71	1.91	0.00	0.00	0.04	0.00	47.77	1.70	0.00	0.00	0.06	0.00
47.85	1.60	0.00	0.00	0.08	0.00	47.92	1.54	0.00	0.00	0.07	0.00
47.97	1.54	0.00	0.00	0.05	0.00	48.06	1.69	0.00	0.00	0.09	0.00
48.12	1.81	0.00	0.00	0.06	0.00	48.17	2.00	0.00	0.00	0.05	0.00
48.25	2.00	0.00	0.00	0.08	0.00	48.31	2.00	0.00	0.00	0.06	0.00
48.36	2.00	0.00	0.00	0.05	0.00	48.45	2.00	0.00	0.00	0.08	0.00
48.50	1.95	0.00	0.00	0.05	0.00	48.57	1.85	0.00	0.00	0.07	0.00
48.63	1.70	0.00	0.00	0.07	0.00	48.72	1.52	0.00	0.00	0.08	0.00
48.77	1.38	0.00	0.00	0.06	0.00	48.85	1.16	0.00	0.00	0.08	0.00
48.91	1.00	0.00	0.00	0.06	0.00	48.97	0.97	0.00	0.00	0.05	0.00
49.05	0.89	0.00	0.00	0.09	0.01	49.11	0.82	0.00	0.00	0.05	0.01
49.16	0.76	0.00	0.00	0.05	0.01	49.21	0.67	0.33	0.82	0.05	0.01
49.28	0.55	0.45	0.55	0.07	0.02	49.35	0.53	0.47	0.52	0.07	0.02
49.42	0.59	0.41	0.61	0.07	0.02	49.48	0.60	0.40	0.62	0.06	0.02
49.54	0.69	0.31	0.87	0.06	0.01	49.61	0.55	0.45	0.55	0.07	0.02
49.68	0.61	0.39	0.65	0.07	0.02	49.76	0.50	0.50	0.47	0.08	0.03
49.81	0.51	0.49	0.49	0.06	0.02	49.88	0.57	0.43	0.58	0.07	0.02
49.95	0.64	0.36	0.72	0.07	0.02	50.02	2.00	0.00	0.00	0.07	0.00
50.10	2.00	0.00	0.00	0.08	0.00	50.15	2.00	0.00	0.00	0.05	0.00
50.20	2.00	0.00	0.00	0.05	0.00	50.28	2.00	0.00	0.00	0.08	0.00
50.34	2.00	0.00	0.00	0.06	0.00	50.44	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
50.47	2.00	0.00	0.00	0.03	0.00	50.54	2.00	0.00	0.00	0.07	0.00
50.59	2.00	0.00	0.00	0.05	0.00	50.69	2.00	0.00	0.00	0.10	0.00
50.73	2.00	0.00	0.00	0.04	0.00	50.84	2.00	0.00	0.00	0.11	0.00
50.86	2.00	0.00	0.00	0.02	0.00	50.93	2.00	0.00	0.00	0.07	0.00
50.99	2.00	0.00	0.00	0.06	0.00	51.05	2.00	0.00	0.00	0.07	0.00
51.13	2.00	0.00	0.00	0.07	0.00	51.20	2.00	0.00	0.00	0.07	0.00
51.25	2.00	0.00	0.00	0.05	0.00	51.34	2.00	0.00	0.00	0.09	0.00
51.38	2.00	0.00	0.00	0.05	0.00	51.48	2.00	0.00	0.00	0.09	0.00
51.53	2.00	0.00	0.00	0.05	0.00	51.58	2.00	0.00	0.00	0.05	0.00
51.67	2.00	0.00	0.00	0.09	0.00	51.72	2.00	0.00	0.00	0.05	0.00
51.78	2.00	0.00	0.00	0.06	0.00	51.86	2.00	0.00	0.00	0.08	0.00
51.93	2.00	0.00	0.00	0.07	0.00	51.97	2.00	0.00	0.00	0.05	0.00
52.06	2.00	0.00	0.00	0.08	0.00	52.11	2.00	0.00	0.00	0.05	0.00
52.17	2.00	0.00	0.00	0.06	0.00	52.24	2.00	0.00	0.00	0.08	0.00
52.31	2.00	0.00	0.00	0.06	0.00	52.37	2.00	0.00	0.00	0.06	0.00
52.47	2.00	0.00	0.00	0.10	0.00	52.52	2.00	0.00	0.00	0.05	0.00
52.57	2.00	0.00	0.00	0.05	0.00	52.67	2.00	0.00	0.00	0.10	0.00
52.72	2.00	0.00	0.00	0.05	0.00	52.77	2.00	0.00	0.00	0.05	0.00
52.86	2.00	0.00	0.00	0.09	0.00	52.91	2.00	0.00	0.00	0.05	0.00
52.96	2.00	0.00	0.00	0.06	0.00	53.02	2.00	0.00	0.00	0.05	0.00
53.10	2.00	0.00	0.00	0.08	0.00	53.16	2.00	0.00	0.00	0.05	0.00
53.24	2.00	0.00	0.00	0.08	0.00	53.30	2.00	0.00	0.00	0.06	0.00
53.36	2.00	0.00	0.00	0.07	0.00	53.42	2.00	0.00	0.00	0.06	0.00
53.48	2.00	0.00	0.00	0.06	0.00	53.56	2.00	0.00	0.00	0.08	0.00
53.61	2.00	0.00	0.00	0.05	0.00	53.69	2.00	0.00	0.00	0.07	0.00
53.75	2.00	0.00	0.00	0.06	0.00	53.82	2.00	0.00	0.00	0.08	0.00
53.88	2.00	0.00	0.00	0.05	0.00	53.97	2.00	0.00	0.00	0.09	0.00
54.02	2.00	0.00	0.00	0.06	0.00	54.09	2.00	0.00	0.00	0.07	0.00
54.14	2.00	0.00	0.00	0.05	0.00	54.21	2.00	0.00	0.00	0.07	0.00
54.28	2.00	0.00	0.00	0.07	0.00	54.33	2.00	0.00	0.00	0.05	0.00
54.43	2.00	0.00	0.00	0.09	0.00	54.48	2.00	0.00	0.00	0.05	0.00
54.53	2.00	0.00	0.00	0.05	0.00	54.62	2.00	0.00	0.00	0.09	0.00
54.67	2.00	0.00	0.00	0.05	0.00	54.73	2.00	0.00	0.00	0.06	0.00
54.82	2.00	0.00	0.00	0.09	0.00	54.87	2.00	0.00	0.00	0.05	0.00
54.95	2.00	0.00	0.00	0.09	0.00	55.01	2.00	0.00	0.00	0.05	0.00
55.06	2.00	0.00	0.00	0.05	0.00	55.12	2.00	0.00	0.00	0.06	0.00
55.20	2.00	0.00	0.00	0.09	0.00	55.26	2.00	0.00	0.00	0.05	0.00
55.32	2.00	0.00	0.00	0.06	0.00	55.41	2.00	0.00	0.00	0.09	0.00
55.47	2.00	0.00	0.00	0.06	0.00	55.51	2.00	0.00	0.00	0.04	0.00
55.59	2.00	0.00	0.00	0.08	0.00	55.67	2.00	0.00	0.00	0.08	0.00
55.72	2.00	0.00	0.00	0.05	0.00	55.81	2.00	0.00	0.00	0.09	0.00
55.86	2.00	0.00	0.00	0.05	0.00	55.92	2.00	0.00	0.00	0.05	0.00
56.01	2.00	0.00	0.00	0.09	0.00	56.06	2.00	0.00	0.00	0.05	0.00
56.11	2.00	0.00	0.00	0.05	0.00	56.21	2.00	0.00	0.00	0.10	0.00
56.25	2.00	0.00	0.00	0.04	0.00	56.31	2.00	0.00	0.00	0.06	0.00
56.38	2.00	0.00	0.00	0.08	0.00	56.44	2.00	0.00	0.00	0.06	0.00
56.50	2.00	0.00	0.00	0.06	0.00	56.58	2.00	0.00	0.00	0.08	0.00
56.65	2.00	0.00	0.00	0.07	0.00	56.73	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
56.76	2.00	0.00	0.00	0.03	0.00	56.84	2.00	0.00	0.00	0.07	0.00
56.92	2.00	0.00	0.00	0.08	0.00	56.98	2.00	0.00	0.00	0.06	0.00
57.02	2.00	0.00	0.00	0.05	0.00	57.12	2.00	0.00	0.00	0.09	0.00
57.17	2.00	0.00	0.00	0.06	0.00	57.23	2.00	0.00	0.00	0.05	0.00
57.32	2.00	0.00	0.00	0.10	0.00	57.36	2.00	0.00	0.00	0.04	0.00
57.42	2.00	0.00	0.00	0.06	0.00	57.50	2.00	0.00	0.00	0.09	0.00
57.55	2.00	0.00	0.00	0.05	0.00	57.62	2.00	0.00	0.00	0.06	0.00
57.69	2.00	0.00	0.00	0.07	0.00	57.77	2.00	0.00	0.00	0.08	0.00
57.83	2.00	0.00	0.00	0.06	0.00	57.91	2.00	0.00	0.00	0.08	0.00
57.97	2.00	0.00	0.00	0.06	0.00	58.01	2.00	0.00	0.00	0.04	0.00
58.11	2.00	0.00	0.00	0.10	0.00	58.16	2.00	0.00	0.00	0.05	0.00
58.22	2.00	0.00	0.00	0.06	0.00	58.31	2.00	0.00	0.00	0.09	0.00
58.36	2.00	0.00	0.00	0.05	0.00	58.41	2.00	0.00	0.00	0.05	0.00
58.51	2.00	0.00	0.00	0.10	0.00	58.55	2.00	0.00	0.00	0.03	0.00
58.60	2.00	0.00	0.00	0.05	0.00	58.67	2.00	0.00	0.00	0.07	0.00
58.76	2.00	0.00	0.00	0.09	0.00	58.80	2.00	0.00	0.00	0.04	0.00
58.88	2.00	0.00	0.00	0.08	0.00	58.94	2.00	0.00	0.00	0.06	0.00
59.01	2.00	0.00	0.00	0.07	0.00	59.06	2.00	0.00	0.00	0.05	0.00
59.15	2.00	0.00	0.00	0.09	0.00	59.20	2.00	0.00	0.00	0.04	0.00
59.25	2.00	0.00	0.00	0.06	0.00	59.34	2.00	0.00	0.00	0.09	0.00
59.40	2.00	0.00	0.00	0.06	0.00	59.45	2.00	0.00	0.00	0.05	0.00
59.54	2.00	0.00	0.00	0.08	0.00	59.60	2.00	0.00	0.00	0.06	0.00
59.65	2.00	0.00	0.00	0.05	0.00	59.74	2.00	0.00	0.00	0.09	0.00
59.78	2.00	0.00	0.00	0.05	0.00	59.87	2.00	0.00	0.00	0.09	0.00
59.94	2.00	0.00	0.00	0.07	0.00	59.99	2.00	0.00	0.00	0.05	0.00
60.05	2.00	0.00	0.00	0.05	0.00	60.14	2.00	0.00	0.00	0.09	0.00
60.19	2.00	0.00	0.00	0.05	0.00	60.24	2.00	0.00	0.00	0.05	0.00
60.34	2.00	0.00	0.00	0.10	0.00	60.38	2.00	0.00	0.00	0.05	0.00
60.44	2.00	0.00	0.00	0.05	0.00	60.53	2.00	0.00	0.00	0.09	0.00
60.58	2.00	0.00	0.00	0.05	0.00	60.63	2.00	0.00	0.00	0.06	0.00
60.71	2.00	0.00	0.00	0.08	0.00	60.78	2.00	0.00	0.00	0.07	0.00
60.83	2.00	0.00	0.00	0.05	0.00	60.91	2.00	0.00	0.00	0.08	0.00
60.97	2.00	0.00	0.00	0.06	0.00	61.03	2.00	0.00	0.00	0.06	0.00
61.10	2.00	0.00	0.00	0.07	0.00	61.16	2.00	0.00	0.00	0.07	0.00
61.23	2.00	0.00	0.00	0.06	0.00	61.32	2.00	0.00	0.00	0.10	0.00
61.38	2.00	0.00	0.00	0.05	0.00	61.43	2.00	0.00	0.00	0.05	0.00
61.52	2.00	0.00	0.00	0.10	0.00	61.56	2.00	0.00	0.00	0.03	0.00
61.62	2.00	0.00	0.00	0.06	0.00	61.71	2.00	0.00	0.00	0.09	0.00
61.77	2.00	0.00	0.00	0.06	0.00	61.84	2.00	0.00	0.00	0.06	0.00
61.92	2.00	0.00	0.00	0.08	0.00	61.94	2.00	0.00	0.00	0.03	0.00
62.02	2.00	0.00	0.00	0.08	0.00	62.12	2.00	0.00	0.00	0.09	0.00
62.15	2.00	0.00	0.00	0.03	0.00	62.22	2.00	0.00	0.00	0.07	0.00
62.27	2.00	0.00	0.00	0.05	0.00	62.36	2.00	0.00	0.00	0.09	0.00
62.41	2.00	0.00	0.00	0.05	0.00	62.48	2.00	0.00	0.00	0.07	0.00
62.55	2.00	0.00	0.00	0.07	0.00	62.61	2.00	0.00	0.00	0.06	0.00
62.69	2.00	0.00	0.00	0.08	0.00	62.74	2.00	0.00	0.00	0.05	0.00
62.81	2.00	0.00	0.00	0.07	0.00	62.87	2.00	0.00	0.00	0.06	0.00
62.95	2.00	0.00	0.00	0.08	0.00	63.00	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
63.10	2.00	0.00	0.00	0.11	0.00	63.13	2.00	0.00	0.00	0.02	0.00
63.19	2.00	0.00	0.00	0.06	0.00	63.26	2.00	0.00	0.00	0.07	0.00
63.32	2.00	0.00	0.00	0.07	0.00	63.39	2.00	0.00	0.00	0.06	0.00
63.49	2.00	0.00	0.00	0.11	0.00	63.52	2.00	0.00	0.00	0.03	0.00
63.60	2.00	0.00	0.00	0.08	0.00	63.69	2.00	0.00	0.00	0.09	0.00
63.74	2.00	0.00	0.00	0.05	0.00	63.79	2.00	0.00	0.00	0.06	0.00
63.85	2.00	0.00	0.00	0.05	0.00	63.92	2.00	0.00	0.00	0.08	0.00
63.99	2.00	0.00	0.00	0.07	0.00	64.05	2.00	0.00	0.00	0.05	0.00
64.13	2.00	0.00	0.00	0.08	0.00	64.18	2.00	0.00	0.00	0.05	0.00
64.24	2.00	0.00	0.00	0.06	0.00	64.34	2.00	0.00	0.00	0.09	0.00
64.39	2.00	0.00	0.00	0.06	0.00	64.45	2.00	0.00	0.00	0.05	0.00
64.51	2.00	0.00	0.00	0.06	0.00	64.59	2.00	0.00	0.00	0.08	0.00
64.64	2.00	0.00	0.00	0.05	0.00	64.73	2.00	0.00	0.00	0.09	0.00
64.78	2.00	0.00	0.00	0.05	0.00	64.83	2.00	0.00	0.00	0.06	0.00
64.93	2.00	0.00	0.00	0.09	0.00	64.98	2.00	0.00	0.00	0.05	0.00
65.03	2.00	0.00	0.00	0.05	0.00	65.12	2.00	0.00	0.00	0.09	0.00
65.17	2.00	0.00	0.00	0.06	0.00	65.23	2.00	0.00	0.00	0.05	0.00
65.31	2.00	0.00	0.00	0.08	0.00	65.36	2.00	0.00	0.00	0.06	0.00
65.42	2.00	0.00	0.00	0.06	0.00	65.50	2.00	0.00	0.00	0.08	0.00
65.58	2.00	0.00	0.00	0.08	0.00	65.63	2.00	0.00	0.00	0.05	0.00
65.72	2.00	0.00	0.00	0.09	0.00	65.77	2.00	0.00	0.00	0.04	0.00
65.83	2.00	0.00	0.00	0.06	0.00	65.92	2.00	0.00	0.00	0.09	0.00
65.97	2.00	0.00	0.00	0.05	0.00	66.02	2.00	0.00	0.00	0.05	0.00
66.11	2.00	0.00	0.00	0.08	0.00	66.16	2.00	0.00	0.00	0.06	0.00
66.22	2.00	0.00	0.00	0.06	0.00	66.30	2.00	0.00	0.00	0.08	0.00
66.35	2.00	0.00	0.00	0.05	0.00	66.42	2.00	0.00	0.00	0.06	0.00
66.50	2.00	0.00	0.00	0.08	0.00	66.55	2.00	0.00	0.00	0.05	0.00
66.61	2.00	0.00	0.00	0.06	0.00	66.70	2.00	0.00	0.00	0.09	0.00
66.76	2.00	0.00	0.00	0.06	0.00	66.80	2.00	0.00	0.00	0.05	0.00
66.88	2.00	0.00	0.00	0.07	0.00	66.96	2.00	0.00	0.00	0.08	0.00
67.01	2.00	0.00	0.00	0.05	0.00	67.06	2.00	0.00	0.00	0.05	0.00
67.13	2.00	0.00	0.00	0.07	0.00	67.19	2.00	0.00	0.00	0.06	0.00
67.29	2.00	0.00	0.00	0.10	0.00	67.35	2.00	0.00	0.00	0.06	0.00
67.40	2.00	0.00	0.00	0.05	0.00	67.50	2.00	0.00	0.00	0.09	0.00
67.55	2.00	0.00	0.00	0.05	0.00	67.60	2.00	0.00	0.00	0.05	0.00
67.68	2.00	0.00	0.00	0.09	0.00	67.73	2.00	0.00	0.00	0.05	0.00
67.79	2.00	0.00	0.00	0.06	0.00	67.87	2.00	0.00	0.00	0.08	0.00
67.93	2.00	0.00	0.00	0.05	0.00	67.98	2.00	0.00	0.00	0.05	0.00
68.05	2.00	0.00	0.00	0.06	0.00	68.11	2.00	0.00	0.00	0.07	0.00
68.19	2.00	0.00	0.00	0.07	0.00	68.25	2.00	0.00	0.00	0.06	0.00
68.34	2.00	0.00	0.00	0.09	0.00	68.39	2.00	0.00	0.00	0.05	0.00
68.44	2.00	0.00	0.00	0.05	0.00	68.54	2.00	0.00	0.00	0.10	0.00
68.59	2.00	0.00	0.00	0.05	0.00	68.64	2.00	0.00	0.00	0.05	0.00
68.71	2.00	0.00	0.00	0.06	0.00	68.77	2.00	0.00	0.00	0.06	0.00
68.84	2.00	0.00	0.00	0.07	0.00	68.91	2.00	0.00	0.00	0.07	0.00
68.97	2.00	0.00	0.00	0.06	0.00	69.04	2.00	0.00	0.00	0.06	0.00
69.12	2.00	0.00	0.00	0.08	0.00	69.17	2.00	0.00	0.00	0.05	0.00
69.27	2.00	0.00	0.00	0.10	0.00	69.29	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
69.37	2.00	0.00	0.00	0.08	0.00	69.42	2.00	0.00	0.00	0.05	0.00
69.52	2.00	0.00	0.00	0.09	0.00	69.57	2.00	0.00	0.00	0.05	0.00
69.65	2.00	0.00	0.00	0.08	0.00	69.71	2.00	0.00	0.00	0.06	0.00
69.77	2.00	0.00	0.00	0.06	0.00	69.85	2.00	0.00	0.00	0.08	0.00
69.89	2.00	0.00	0.00	0.05	0.00	69.96	2.00	0.00	0.00	0.06	0.00
70.02	2.00	0.00	0.00	0.06	0.00	70.09	2.00	0.00	0.00	0.07	0.00
70.15	2.00	0.00	0.00	0.06	0.00	70.24	2.00	0.00	0.00	0.09	0.00
70.30	2.00	0.00	0.00	0.06	0.00	70.36	2.00	0.00	0.00	0.06	0.00
70.44	2.00	0.00	0.00	0.08	0.00	70.48	2.00	0.00	0.00	0.04	0.00
70.55	2.00	0.00	0.00	0.07	0.00	70.60	2.00	0.00	0.00	0.05	0.00
70.69	2.00	0.00	0.00	0.09	0.00	70.74	2.00	0.00	0.00	0.05	0.00
70.83	2.00	0.00	0.00	0.09	0.00	70.89	2.00	0.00	0.00	0.06	0.00
70.94	2.00	0.00	0.00	0.05	0.00	71.02	2.00	0.00	0.00	0.08	0.00
71.08	2.00	0.00	0.00	0.06	0.00	71.14	2.00	0.00	0.00	0.05	0.00
71.22	2.00	0.00	0.00	0.09	0.00	71.27	2.00	0.00	0.00	0.05	0.00
71.33	2.00	0.00	0.00	0.06	0.00	71.40	2.00	0.00	0.00	0.06	0.00
71.47	2.00	0.00	0.00	0.07	0.00	71.53	2.00	0.00	0.00	0.07	0.00
71.63	2.00	0.00	0.00	0.10	0.00	71.67	2.00	0.00	0.00	0.05	0.00
71.73	2.00	0.00	0.00	0.05	0.00	71.81	2.00	0.00	0.00	0.08	0.00
71.88	2.00	0.00	0.00	0.07	0.00	71.93	2.00	0.00	0.00	0.05	0.00
71.99	2.00	0.00	0.00	0.06	0.00	72.05	2.00	0.00	0.00	0.07	0.00
72.13	2.00	0.00	0.00	0.08	0.00	72.18	2.00	0.00	0.00	0.06	0.00
72.27	2.00	0.00	0.00	0.09	0.00	72.32	2.00	0.00	0.00	0.05	0.00
72.38	2.00	0.00	0.00	0.05	0.00	72.46	2.00	0.00	0.00	0.09	0.00
72.52	2.00	0.00	0.00	0.05	0.00	72.62	2.00	0.00	0.00	0.10	0.00
72.66	2.00	0.00	0.00	0.04	0.00	72.71	2.00	0.00	0.00	0.05	0.00
72.82	2.00	0.00	0.00	0.10	0.00	72.85	2.00	0.00	0.00	0.03	0.00
72.91	2.00	0.00	0.00	0.06	0.00	72.97	2.00	0.00	0.00	0.06	0.00
73.06	2.00	0.00	0.00	0.09	0.00	73.11	2.00	0.00	0.00	0.05	0.00
73.17	2.00	0.00	0.00	0.06	0.00	73.24	2.00	0.00	0.00	0.07	0.00
73.31	2.00	0.00	0.00	0.07	0.00	73.37	2.00	0.00	0.00	0.06	0.00
73.43	2.00	0.00	0.00	0.06	0.00	73.51	2.00	0.00	0.00	0.08	0.00
73.56	2.00	0.00	0.00	0.05	0.00	73.65	2.00	0.00	0.00	0.10	0.00
73.71	2.00	0.00	0.00	0.06	0.00	73.76	2.00	0.00	0.00	0.05	0.00
73.84	2.00	0.00	0.00	0.08	0.00	73.90	2.00	0.00	0.00	0.06	0.00
73.95	2.00	0.00	0.00	0.05	0.00	74.06	2.00	0.00	0.00	0.11	0.00
74.10	2.00	0.00	0.00	0.04	0.00	74.15	2.00	0.00	0.00	0.05	0.00
74.22	2.00	0.00	0.00	0.07	0.00	74.29	2.00	0.00	0.00	0.07	0.00
74.35	2.00	0.00	0.00	0.06	0.00	74.43	2.00	0.00	0.00	0.08	0.00
74.48	2.00	0.00	0.00	0.05	0.00	74.54	2.00	0.00	0.00	0.07	0.00
74.64	2.00	0.00	0.00	0.09	0.00	74.69	2.00	0.00	0.00	0.05	0.00
74.75	2.00	0.00	0.00	0.05	0.00	74.83	2.00	0.00	0.00	0.08	0.00
74.87	2.00	0.00	0.00	0.05	0.00	74.94	2.00	0.00	0.00	0.06	0.00
75.02	2.00	0.00	0.00	0.08	0.00	75.08	2.00	0.00	0.00	0.06	0.00
75.13	2.00	0.00	0.00	0.06	0.00	75.22	2.00	0.00	0.00	0.08	0.00
75.28	2.00	0.00	0.00	0.06	0.00	75.33	2.00	0.00	0.00	0.05	0.00
75.42	2.00	0.00	0.00	0.09	0.00	75.47	2.00	0.00	0.00	0.05	0.00
75.53	2.00	0.00	0.00	0.06	0.00	75.62	2.00	0.00	0.00	0.09	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}	Depth (ft)	FS	m(FS)	$H_1 * m(FS)$	d_z	LPI_{ISH}

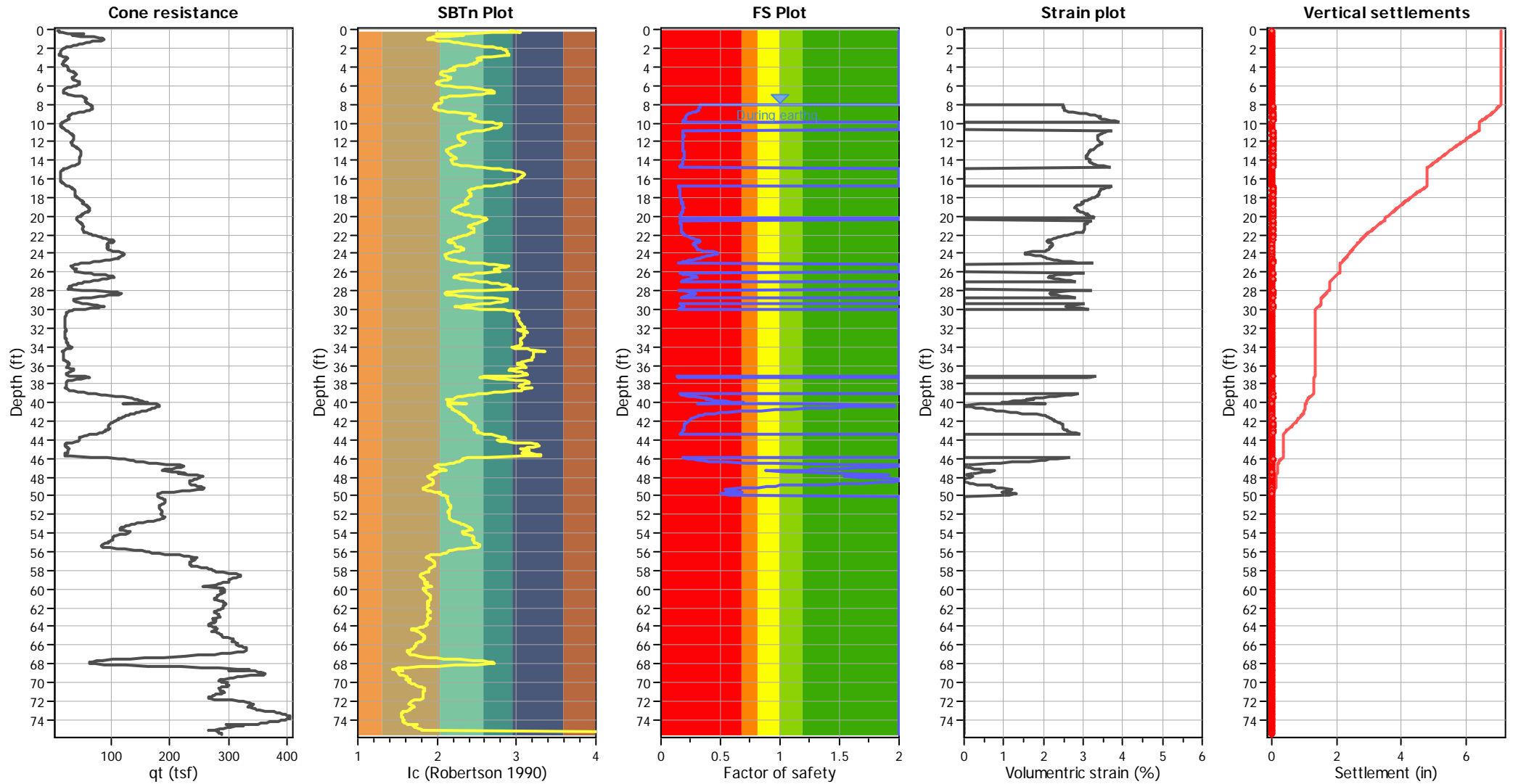
Overall liquefaction potential: 32.07

$LPI_{ISH} > 5.0$ - Liquefaction manifestation is expected

Abbreviations

- FS: Calculated factor of safety for test point
- d_z : Layer thickness (ft)
- LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- qt: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement due to soil liquefaction ::											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.02	125.44	0.33	2.53	1.00	0.02	8.07	125.96	0.33	2.52	1.00	0.02
8.16	126.98	0.33	2.50	1.00	0.03	8.21	127.19	0.33	2.49	1.00	0.01
8.27	127.29	0.33	2.49	1.00	0.02	8.35	126.71	0.33	2.50	1.00	0.02
8.41	126.22	0.32	2.51	1.00	0.02	8.49	126.29	0.32	2.51	1.00	0.02
8.55	126.02	0.32	2.52	1.00	0.02	8.62	125.34	0.31	2.53	1.00	0.02
8.67	124.16	0.31	2.56	1.00	0.02	8.76	121.35	0.29	2.62	1.00	0.03
8.80	119.06	0.28	2.68	1.00	0.02	8.86	115.95	0.27	2.75	1.00	0.02
8.95	109.29	0.25	2.93	1.00	0.03	8.99	104.56	0.23	3.07	1.00	0.02
9.06	100.64	0.22	3.19	1.00	0.03	9.15	97.60	0.22	3.29	1.00	0.04
9.22	95.55	0.21	3.37	1.00	0.03	9.26	94.21	0.21	3.41	1.00	0.02
9.35	93.69	0.21	3.43	1.00	0.04	9.40	94.48	0.21	3.40	1.00	0.02
9.46	94.64	0.21	3.40	1.00	0.02	9.54	92.83	0.20	3.46	1.00	0.03
9.60	91.29	0.20	3.52	1.00	0.03	9.66	90.29	0.20	3.56	1.00	0.02
9.72	87.21	0.19	3.69	1.00	0.03	9.80	84.18	0.18	3.82	1.00	0.03
9.85	81.86	0.18	3.92	1.00	0.02	9.96	20.26	2.00	0.00	1.00	0.00
10.00	19.31	2.00	0.00	1.00	0.00	10.05	17.18	2.00	0.00	1.00	0.00
10.12	17.64	2.00	0.00	1.00	0.00	10.18	17.20	2.00	0.00	1.00	0.00
10.27	17.25	2.00	0.00	1.00	0.00	10.33	17.83	2.00	0.00	1.00	0.00
10.37	18.18	2.00	0.00	1.00	0.00	10.47	19.85	2.00	0.00	1.00	0.00
10.53	21.04	2.00	0.00	1.00	0.00	10.57	22.25	2.00	0.00	1.00	0.00
10.67	24.12	2.00	0.00	1.00	0.00	10.70	25.44	2.00	0.00	1.00	0.00
10.78	85.74	0.18	3.75	1.00	0.04	10.83	87.28	0.18	3.68	1.00	0.02
10.91	89.21	0.18	3.60	1.00	0.04	10.97	91.00	0.18	3.53	1.00	0.03
11.03	91.84	0.19	3.50	1.00	0.02	11.10	92.63	0.19	3.47	1.00	0.03
11.17	93.80	0.19	3.43	1.00	0.03	11.26	94.65	0.19	3.40	1.00	0.04
11.31	95.14	0.19	3.38	1.00	0.02	11.36	95.49	0.19	3.37	1.00	0.02
11.44	95.71	0.19	3.36	1.00	0.03	11.50	95.75	0.19	3.36	1.00	0.02
11.56	95.85	0.19	3.35	1.00	0.03	11.63	95.78	0.19	3.36	1.00	0.03
11.69	95.59	0.19	3.36	1.00	0.03	11.76	95.33	0.19	3.37	1.00	0.03
11.86	94.58	0.18	3.40	1.00	0.04	11.89	94.44	0.18	3.40	1.00	0.01
11.95	94.06	0.18	3.42	1.00	0.03	12.01	93.38	0.18	3.44	1.00	0.02
12.10	92.82	0.18	3.46	1.00	0.04	12.15	92.62	0.18	3.47	1.00	0.02
12.21	92.73	0.18	3.47	1.00	0.03	12.28	93.02	0.18	3.46	1.00	0.03
12.36	94.14	0.18	3.42	1.00	0.03	12.40	94.92	0.18	3.39	1.00	0.02
12.47	95.44	0.18	3.37	1.00	0.03	12.55	96.34	0.18	3.34	1.00	0.03
12.60	96.76	0.18	3.32	1.00	0.02	12.69	97.55	0.18	3.30	1.00	0.04
12.74	98.13	0.18	3.28	1.00	0.02	12.82	99.21	0.19	3.24	1.00	0.03
12.88	100.03	0.19	3.21	1.00	0.03	12.94	100.62	0.19	3.19	1.00	0.02
13.00	101.18	0.19	3.17	1.00	0.02	13.09	101.93	0.19	3.15	1.00	0.03
13.14	102.03	0.19	3.15	1.00	0.02	13.20	102.12	0.19	3.14	1.00	0.02
13.27	103.01	0.19	3.12	1.00	0.03	13.34	103.41	0.19	3.10	1.00	0.02
13.39	103.53	0.19	3.10	1.00	0.02	13.47	103.82	0.19	3.09	1.00	0.03
13.54	104.05	0.19	3.08	1.00	0.02	13.59	104.11	0.19	3.08	1.00	0.02
13.65	104.29	0.19	3.08	1.00	0.02	13.72	104.40	0.19	3.07	1.00	0.03
13.79	104.63	0.19	3.07	1.00	0.02	13.85	103.63	0.19	3.10	1.00	0.02
13.94	100.76	0.18	3.19	1.00	0.03	13.98	101.24	0.18	3.17	1.00	0.02
14.08	102.18	0.18	3.14	1.00	0.04	14.13	102.19	0.18	3.14	1.00	0.02
14.18	102.17	0.18	3.14	1.00	0.02	14.27	100.87	0.18	3.18	1.00	0.04

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
14.33	100.25	0.18	3.20	1.00	0.02	14.39	99.19	0.18	3.24	1.00	0.02
14.44	98.05	0.17	3.28	1.00	0.02	14.53	95.76	0.17	3.36	1.00	0.04
14.59	93.78	0.17	3.43	1.00	0.02	14.64	91.81	0.16	3.50	1.00	0.02
14.73	88.08	0.16	3.65	1.00	0.04	14.77	86.83	0.16	3.70	1.00	0.02
14.83	23.21	2.00	0.00	1.00	0.00	14.93	19.23	2.00	0.00	1.00	0.00
14.98	17.61	2.00	0.00	1.00	0.00	15.03	16.31	2.00	0.00	1.00	0.00
15.10	15.01	2.00	0.00	1.00	0.00	15.17	14.02	2.00	0.00	1.00	0.00
15.22	13.15	2.00	0.00	1.00	0.00	15.29	12.18	2.00	0.00	1.00	0.00
15.37	12.25	2.00	0.00	1.00	0.00	15.44	12.22	2.00	0.00	1.00	0.00
15.52	12.29	2.00	0.00	1.00	0.00	15.56	12.48	2.00	0.00	1.00	0.00
15.62	12.55	2.00	0.00	1.00	0.00	15.70	12.72	2.00	0.00	1.00	0.00
15.76	12.69	2.00	0.00	1.00	0.00	15.82	12.77	2.00	0.00	1.00	0.00
15.91	12.83	2.00	0.00	1.00	0.00	15.95	13.02	2.00	0.00	1.00	0.00
16.01	12.99	2.00	0.00	1.00	0.00	16.08	13.06	2.00	0.00	1.00	0.00
16.14	13.14	2.00	0.00	1.00	0.00	16.22	13.51	2.00	0.00	1.00	0.00
16.31	14.28	2.00	0.00	1.00	0.00	16.36	15.16	2.00	0.00	1.00	0.00
16.41	16.24	2.00	0.00	1.00	0.00	16.50	18.31	2.00	0.00	1.00	0.00
16.55	19.79	2.00	0.00	1.00	0.00	16.61	21.25	2.00	0.00	1.00	0.00
16.69	23.69	2.00	0.00	1.00	0.00	16.74	25.15	2.00	0.00	1.00	0.00
16.80	85.90	0.15	3.74	1.00	0.03	16.88	87.70	0.15	3.67	1.00	0.03
16.95	89.76	0.15	3.58	1.00	0.03	17.00	91.16	0.15	3.53	1.00	0.02
17.07	92.54	0.16	3.47	1.00	0.03	17.15	93.07	0.16	3.46	1.00	0.03
17.20	93.42	0.16	3.44	1.00	0.02	17.26	93.83	0.16	3.43	1.00	0.03
17.33	94.09	0.16	3.42	1.00	0.03	17.41	94.36	0.16	3.41	1.00	0.03
17.46	94.48	0.16	3.40	1.00	0.02	17.52	94.52	0.16	3.40	1.00	0.02
17.60	94.31	0.16	3.41	1.00	0.03	17.65	94.40	0.16	3.41	1.00	0.02
17.74	95.08	0.16	3.38	1.00	0.04	17.80	95.52	0.16	3.37	1.00	0.02
17.85	96.24	0.16	3.34	1.00	0.02	17.93	97.42	0.16	3.30	1.00	0.03
17.99	98.46	0.16	3.26	1.00	0.02	18.07	99.98	0.16	3.21	1.00	0.03
18.13	101.33	0.17	3.17	1.00	0.02	18.18	102.35	0.17	3.14	1.00	0.02
18.29	103.38	0.17	3.11	1.00	0.04	18.32	104.28	0.17	3.08	1.00	0.01
18.38	105.60	0.17	3.04	1.00	0.02	18.44	106.59	0.17	3.01	1.00	0.02
18.53	107.74	0.18	2.98	1.00	0.03	18.58	108.41	0.18	2.96	1.00	0.02
18.66	106.43	0.17	3.01	1.00	0.03	18.71	109.83	0.18	2.92	1.00	0.02
18.81	111.06	0.18	2.88	1.00	0.03	18.85	112.01	0.18	2.86	1.00	0.02
18.90	112.85	0.19	2.83	1.00	0.02	19.01	113.98	0.19	2.80	1.00	0.04
19.06	114.22	0.19	2.80	1.00	0.02	19.11	114.04	0.19	2.80	1.00	0.02
19.16	113.69	0.19	2.81	1.00	0.02	19.26	112.57	0.18	2.84	1.00	0.03
19.30	112.10	0.18	2.85	1.00	0.01	19.36	111.57	0.18	2.87	1.00	0.02
19.45	110.74	0.18	2.89	1.00	0.03	19.50	109.76	0.18	2.92	1.00	0.02
19.58	107.72	0.17	2.98	1.00	0.03	19.64	106.45	0.17	3.01	1.00	0.02
19.69	105.58	0.17	3.04	1.00	0.02	19.78	103.73	0.17	3.09	1.00	0.03
19.84	104.01	0.17	3.09	1.00	0.02	19.90	102.61	0.16	3.13	1.00	0.02
19.95	102.42	0.16	3.14	1.00	0.02	20.03	101.55	0.16	3.16	1.00	0.03
20.08	98.83	0.16	3.25	1.00	0.02	20.16	98.05	0.16	3.28	1.00	0.03
20.25	36.09	2.00	0.00	1.00	0.00	20.30	35.41	2.00	0.00	1.00	0.00
20.35	35.18	2.00	0.00	1.00	0.00	20.45	99.38	0.16	3.23	1.00	0.04
20.50	100.27	0.16	3.20	1.00	0.02	20.54	100.05	0.16	3.21	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
20.62	103.00	0.16	3.12	1.00	0.03	20.69	104.00	0.16	3.09	1.00	0.02
20.74	103.73	0.16	3.09	1.00	0.02	20.83	104.67	0.17	3.07	1.00	0.03
20.88	105.50	0.17	3.04	1.00	0.02	20.94	105.80	0.17	3.03	1.00	0.02
21.04	105.21	0.17	3.05	1.00	0.04	21.08	105.90	0.17	3.03	1.00	0.02
21.14	105.43	0.17	3.04	1.00	0.02	21.23	105.13	0.17	3.05	1.00	0.03
21.28	105.22	0.17	3.05	1.00	0.02	21.33	105.46	0.17	3.04	1.00	0.02
21.42	105.50	0.17	3.04	1.00	0.03	21.48	105.58	0.17	3.04	1.00	0.02
21.53	106.46	0.17	3.01	1.00	0.02	21.62	107.06	0.17	2.99	1.00	0.03
21.68	107.46	0.17	2.98	1.00	0.02	21.73	109.38	0.17	2.93	1.00	0.02
21.79	112.95	0.18	2.83	1.00	0.02	21.86	115.96	0.19	2.75	1.00	0.02
21.92	117.95	0.19	2.70	1.00	0.02	22.00	121.72	0.20	2.61	1.00	0.02
22.05	124.45	0.21	2.55	1.00	0.02	22.12	125.86	0.21	2.52	1.00	0.02
22.22	131.41	0.23	2.41	1.00	0.03	22.27	132.61	0.24	2.38	1.00	0.02
22.32	135.85	0.25	2.32	1.00	0.01	22.38	138.91	0.27	2.26	1.00	0.02
22.47	142.77	0.29	2.19	1.00	0.02	22.52	144.85	0.30	2.16	1.00	0.01
22.59	147.43	0.32	2.12	1.00	0.02	22.65	148.76	0.33	2.09	1.00	0.01
22.71	149.16	0.33	2.09	1.00	0.02	22.77	147.82	0.32	2.11	1.00	0.01
22.85	144.78	0.30	2.16	1.00	0.02	22.90	142.66	0.28	2.20	1.00	0.01
22.98	140.82	0.27	2.23	1.00	0.02	23.06	140.72	0.27	2.23	1.00	0.02
23.10	141.24	0.28	2.22	1.00	0.01	23.17	143.21	0.29	2.19	1.00	0.02
23.24	144.03	0.29	2.17	1.00	0.02	23.32	143.79	0.29	2.18	1.00	0.02
23.37	144.21	0.29	2.17	1.00	0.01	23.45	145.36	0.30	2.15	1.00	0.02
23.51	145.36	0.30	2.15	1.00	0.02	23.56	146.18	0.30	2.14	1.00	0.01
23.63	149.22	0.33	2.09	1.00	0.02	23.71	152.25	0.35	2.04	1.00	0.02
23.77	157.19	0.40	1.90	1.00	0.01	23.84	160.26	0.43	1.71	1.00	0.01
23.89	162.89	0.47	1.56	1.00	0.01	23.95	163.70	0.48	1.52	1.00	0.01
24.05	163.23	0.47	1.55	1.00	0.02	24.09	162.44	0.46	1.59	1.00	0.01
24.15	161.37	0.45	1.65	1.00	0.01	24.24	158.63	0.41	1.81	1.00	0.02
24.30	156.31	0.39	1.96	1.00	0.02	24.37	153.14	0.36	2.03	1.00	0.02
24.42	150.85	0.34	2.06	1.00	0.01	24.48	149.51	0.33	2.08	1.00	0.01
24.54	148.51	0.32	2.10	1.00	0.02	24.61	146.00	0.30	2.14	1.00	0.02
24.71	139.58	0.26	2.25	1.00	0.03	24.76	133.85	0.24	2.36	1.00	0.01
24.81	127.81	0.21	2.48	1.00	0.02	24.90	118.24	0.19	2.70	1.00	0.03
24.96	112.12	0.17	2.85	1.00	0.02	25.00	106.33	0.16	3.02	1.00	0.02
25.09	99.04	0.15	3.24	1.00	0.03	25.16	33.64	2.00	0.00	1.00	0.00
25.20	30.31	2.00	0.00	1.00	0.00	25.30	25.69	2.00	0.00	1.00	0.00
25.36	24.11	2.00	0.00	1.00	0.00	25.40	23.60	2.00	0.00	1.00	0.00
25.48	24.85	2.00	0.00	1.00	0.00	25.53	26.36	2.00	0.00	1.00	0.00
25.59	28.43	2.00	0.00	1.00	0.00	25.67	30.66	2.00	0.00	1.00	0.00
25.75	30.36	2.00	0.00	1.00	0.00	25.80	29.04	2.00	0.00	1.00	0.00
25.87	29.04	2.00	0.00	1.00	0.00	25.95	29.04	2.00	0.00	1.00	0.00
25.99	32.33	2.00	0.00	1.00	0.00	26.09	106.23	0.16	3.02	1.00	0.03
26.14	115.31	0.18	2.77	1.00	0.02	26.19	118.99	0.19	2.68	1.00	0.02
26.27	130.07	0.22	2.43	1.00	0.02	26.33	135.16	0.24	2.33	1.00	0.02
26.39	139.64	0.26	2.25	1.00	0.02	26.45	145.12	0.29	2.15	1.00	0.02
26.53	147.64	0.31	2.11	1.00	0.02	26.59	148.05	0.31	2.11	1.00	0.02
26.64	144.26	0.28	2.17	1.00	0.01	26.73	137.46	0.25	2.29	1.00	0.02
26.79	132.30	0.23	2.39	1.00	0.02	26.86	124.63	0.20	2.55	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
26.93	119.18	0.19	2.67	1.00	0.02	26.99	113.28	0.17	2.82	1.00	0.02
27.08	41.49	2.00	0.00	1.00	0.00	27.13	37.89	2.00	0.00	1.00	0.00
27.17	35.22	2.00	0.00	1.00	0.00	27.25	32.69	2.00	0.00	1.00	0.00
27.32	30.57	2.00	0.00	1.00	0.00	27.38	25.88	2.00	0.00	1.00	0.00
27.44	23.65	2.00	0.00	1.00	0.00	27.53	21.73	2.00	0.00	1.00	0.00
27.58	21.17	2.00	0.00	1.00	0.00	27.63	20.84	2.00	0.00	1.00	0.00
27.71	21.89	2.00	0.00	1.00	0.00	27.77	24.11	2.00	0.00	1.00	0.00
27.82	19.14	2.00	0.00	1.00	0.00	27.90	100.00	0.15	3.21	1.00	0.03
27.97	108.40	0.16	2.96	1.00	0.02	28.02	118.25	0.18	2.70	1.00	0.02
28.12	136.56	0.24	2.31	1.00	0.03	28.17	141.92	0.27	2.21	1.00	0.01
28.23	145.13	0.29	2.15	1.00	0.01	28.31	145.42	0.29	2.15	1.00	0.02
28.37	143.59	0.28	2.18	1.00	0.01	28.42	140.39	0.26	2.24	1.00	0.01
28.51	134.31	0.23	2.35	1.00	0.03	28.55	128.77	0.21	2.46	1.00	0.01
28.61	122.96	0.19	2.59	1.00	0.02	28.71	113.82	0.17	2.81	1.00	0.03
28.76	43.18	2.00	0.00	1.00	0.00	28.81	36.85	2.00	0.00	1.00	0.00
28.91	27.24	2.00	0.00	1.00	0.00	28.95	26.37	2.00	0.00	1.00	0.00
29.00	26.30	2.00	0.00	1.00	0.00	29.07	26.23	2.00	0.00	1.00	0.00
29.16	28.78	2.00	0.00	1.00	0.00	29.21	31.82	2.00	0.00	1.00	0.00
29.30	36.56	2.00	0.00	1.00	0.00	29.36	37.99	2.00	0.00	1.00	0.00
29.41	105.07	0.15	3.05	1.00	0.02	29.50	114.38	0.17	2.79	1.00	0.03
29.56	119.07	0.18	2.68	1.00	0.02	29.61	123.59	0.19	2.57	1.00	0.02
29.69	123.76	0.19	2.57	1.00	0.03	29.76	121.75	0.19	2.61	1.00	0.02
29.80	117.73	0.18	2.71	1.00	0.01	29.89	108.86	0.16	2.94	1.00	0.03
29.93	101.71	0.15	3.16	1.00	0.02	30.00	33.54	2.00	0.00	1.00	0.00
30.06	24.67	2.00	0.00	1.00	0.00	30.13	22.62	2.00	0.00	1.00	0.00
30.21	20.07	2.00	0.00	1.00	0.00	30.27	17.47	2.00	0.00	1.00	0.00
30.36	16.71	2.00	0.00	1.00	0.00	30.41	16.55	2.00	0.00	1.00	0.00
30.46	16.02	2.00	0.00	1.00	0.00	30.55	15.27	2.00	0.00	1.00	0.00
30.60	15.19	2.00	0.00	1.00	0.00	30.65	15.03	2.00	0.00	1.00	0.00
30.73	14.71	2.00	0.00	1.00	0.00	30.80	14.62	2.00	0.00	1.00	0.00
30.85	14.46	2.00	0.00	1.00	0.00	30.95	14.30	2.00	0.00	1.00	0.00
30.99	14.14	2.00	0.00	1.00	0.00	31.05	14.20	2.00	0.00	1.00	0.00
31.15	14.17	2.00	0.00	1.00	0.00	31.18	14.17	2.00	0.00	1.00	0.00
31.23	14.15	2.00	0.00	1.00	0.00	31.30	14.35	2.00	0.00	1.00	0.00
31.39	14.32	2.00	0.00	1.00	0.00	31.45	14.31	2.00	0.00	1.00	0.00
31.50	14.22	2.00	0.00	1.00	0.00	31.58	14.20	2.00	0.00	1.00	0.00
31.64	14.19	2.00	0.00	1.00	0.00	31.70	14.17	2.00	0.00	1.00	0.00
31.78	14.01	2.00	0.00	1.00	0.00	31.84	13.86	2.00	0.00	1.00	0.00
31.90	13.70	2.00	0.00	1.00	0.00	31.96	14.04	2.00	0.00	1.00	0.00
32.03	14.44	2.00	0.00	1.00	0.00	32.09	14.42	2.00	0.00	1.00	0.00
32.19	15.39	2.00	0.00	1.00	0.00	32.24	16.01	2.00	0.00	1.00	0.00
32.32	15.00	2.00	0.00	1.00	0.00	32.39	13.58	2.00	0.00	1.00	0.00
32.43	13.22	2.00	0.00	1.00	0.00	32.48	13.14	2.00	0.00	1.00	0.00
32.55	13.33	2.00	0.00	1.00	0.00	32.62	13.32	2.00	0.00	1.00	0.00
32.69	13.02	2.00	0.00	1.00	0.00	32.78	13.00	2.00	0.00	1.00	0.00
32.82	12.99	2.00	0.00	1.00	0.00	32.88	13.12	2.00	0.00	1.00	0.00
32.97	13.37	2.00	0.00	1.00	0.00	33.02	13.50	2.00	0.00	1.00	0.00
33.08	13.83	2.00	0.00	1.00	0.00	33.17	14.37	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
33.21	14.56	2.00	0.00	1.00	0.00	33.29	15.03	2.00	0.00	1.00	0.00
33.37	15.63	2.00	0.00	1.00	0.00	33.41	15.55	2.00	0.00	1.00	0.00
33.47	15.67	2.00	0.00	1.00	0.00	33.56	15.65	2.00	0.00	1.00	0.00
33.61	16.19	2.00	0.00	1.00	0.00	33.68	16.04	2.00	0.00	1.00	0.00
33.77	16.56	2.00	0.00	1.00	0.00	33.82	16.76	2.00	0.00	1.00	0.00
33.87	17.64	2.00	0.00	1.00	0.00	33.97	19.78	2.00	0.00	1.00	0.00
34.01	20.88	2.00	0.00	1.00	0.00	34.08	20.99	2.00	0.00	1.00	0.00
34.13	19.52	2.00	0.00	1.00	0.00	34.19	17.27	2.00	0.00	1.00	0.00
34.27	14.71	2.00	0.00	1.00	0.00	34.36	13.46	2.00	0.00	1.00	0.00
34.41	12.64	2.00	0.00	1.00	0.00	34.46	9.94	2.00	0.00	1.00	0.00
34.54	12.07	2.00	0.00	1.00	0.00	34.60	11.92	2.00	0.00	1.00	0.00
34.65	11.91	2.00	0.00	1.00	0.00	34.73	11.89	2.00	0.00	1.00	0.00
34.80	11.81	2.00	0.00	1.00	0.00	34.85	11.67	2.00	0.00	1.00	0.00
34.92	11.52	2.00	0.00	1.00	0.00	34.98	11.65	2.00	0.00	1.00	0.00
35.04	11.50	2.00	0.00	1.00	0.00	35.12	11.62	2.00	0.00	1.00	0.00
35.17	11.81	2.00	0.00	1.00	0.00	35.25	11.79	2.00	0.00	1.00	0.00
35.32	11.91	2.00	0.00	1.00	0.00	35.37	11.97	2.00	0.00	1.00	0.00
35.44	12.29	2.00	0.00	1.00	0.00	35.50	13.20	2.00	0.00	1.00	0.00
35.60	15.19	2.00	0.00	1.00	0.00	35.65	15.85	2.00	0.00	1.00	0.00
35.70	16.91	2.00	0.00	1.00	0.00	35.79	18.11	2.00	0.00	1.00	0.00
35.85	17.96	2.00	0.00	1.00	0.00	35.90	17.20	2.00	0.00	1.00	0.00
35.98	15.70	2.00	0.00	1.00	0.00	36.03	15.34	2.00	0.00	1.00	0.00
36.09	15.70	2.00	0.00	1.00	0.00	36.18	14.78	2.00	0.00	1.00	0.00
36.24	15.70	2.00	0.00	1.00	0.00	36.29	16.35	2.00	0.00	1.00	0.00
36.38	19.76	2.00	0.00	1.00	0.00	36.44	21.90	2.00	0.00	1.00	0.00
36.49	22.98	2.00	0.00	1.00	0.00	36.57	21.32	2.00	0.00	1.00	0.00
36.63	19.07	2.00	0.00	1.00	0.00	36.69	17.51	2.00	0.00	1.00	0.00
36.77	16.42	2.00	0.00	1.00	0.00	36.83	15.75	2.00	0.00	1.00	0.00
36.88	14.74	2.00	0.00	1.00	0.00	36.96	14.26	2.00	0.00	1.00	0.00
37.03	14.12	2.00	0.00	1.00	0.00	37.08	17.27	2.00	0.00	1.00	0.00
37.14	23.40	2.00	0.00	1.00	0.00	37.23	96.93	0.14	3.32	1.00	0.04
37.28	101.95	0.15	3.15	1.00	0.02	37.36	36.92	2.00	0.00	1.00	0.00
37.41	31.33	2.00	0.00	1.00	0.00	37.48	26.36	2.00	0.00	1.00	0.00
37.57	20.80	2.00	0.00	1.00	0.00	37.63	17.65	2.00	0.00	1.00	0.00
37.66	16.38	2.00	0.00	1.00	0.00	37.77	14.47	2.00	0.00	1.00	0.00
37.82	13.81	2.00	0.00	1.00	0.00	37.88	13.54	2.00	0.00	1.00	0.00
37.96	13.59	2.00	0.00	1.00	0.00	38.01	13.96	2.00	0.00	1.00	0.00
38.06	13.89	2.00	0.00	1.00	0.00	38.13	14.13	2.00	0.00	1.00	0.00
38.19	14.44	2.00	0.00	1.00	0.00	38.26	14.55	2.00	0.00	1.00	0.00
38.32	14.35	2.00	0.00	1.00	0.00	38.41	13.88	2.00	0.00	1.00	0.00
38.46	11.96	2.00	0.00	1.00	0.00	38.52	15.27	2.00	0.00	1.00	0.00
38.59	15.83	2.00	0.00	1.00	0.00	38.65	16.54	2.00	0.00	1.00	0.00
38.73	18.60	2.00	0.00	1.00	0.00	38.79	21.14	2.00	0.00	1.00	0.00
38.86	26.96	2.00	0.00	1.00	0.00	38.92	32.71	2.00	0.00	1.00	0.00
38.98	38.59	2.00	0.00	1.00	0.00	39.06	110.75	0.16	2.89	1.00	0.03
39.12	117.20	0.17	2.72	1.00	0.02	39.18	123.75	0.19	2.57	1.00	0.02
39.28	135.76	0.23	2.32	1.00	0.03	39.32	139.03	0.24	2.26	1.00	0.01
39.37	145.69	0.28	2.15	1.00	0.01	39.48	156.25	0.35	1.96	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
39.52	158.76	0.38	1.80	1.00	0.01	39.57	162.36	0.42	1.59	1.00	0.01
39.66	162.90	0.43	1.56	1.00	0.02	39.70	159.27	0.38	1.77	1.00	0.01
39.77	165.36	0.46	1.44	1.00	0.01	39.87	169.86	0.53	1.23	1.00	0.01
39.92	173.40	0.60	1.09	1.00	0.01	39.98	177.36	0.70	0.94	1.00	0.01
40.06	150.75	0.31	2.06	1.00	0.02	40.12	187.35	1.06	0.63	1.00	0.00
40.16	191.49	1.29	0.40	1.00	0.00	40.25	198.08	1.80	0.08	1.00	0.00
40.31	199.73	1.97	0.01	1.00	0.00	40.37	199.72	1.97	0.01	1.00	0.00
40.44	197.81	1.77	0.10	1.00	0.00	40.50	195.66	1.58	0.20	1.00	0.00
40.56	193.61	1.43	0.29	1.00	0.00	40.63	190.41	1.22	0.46	1.00	0.00
40.71	188.04	1.09	0.59	1.00	0.01	40.77	185.19	0.96	0.71	1.00	0.00
40.86	181.97	0.84	0.80	1.00	0.01	40.90	179.51	0.76	0.87	1.00	0.00
40.96	176.39	0.67	0.98	1.00	0.01	41.03	171.36	0.56	1.17	1.00	0.01
41.09	168.20	0.50	1.30	1.00	0.01	41.15	165.11	0.45	1.45	1.00	0.01
41.24	160.87	0.40	1.68	1.00	0.02	41.28	158.11	0.37	1.84	1.00	0.01
41.35	155.96	0.35	1.98	1.00	0.02	41.41	152.45	0.32	2.04	1.00	0.02
41.50	150.21	0.30	2.07	1.00	0.02	41.55	148.06	0.29	2.11	1.00	0.01
41.61	145.45	0.27	2.15	1.00	0.02	41.71	143.04	0.26	2.19	1.00	0.03
41.75	141.82	0.25	2.21	1.00	0.01	41.80	140.59	0.25	2.23	1.00	0.01
41.87	139.34	0.24	2.25	1.00	0.02	41.93	138.01	0.24	2.28	1.00	0.02
42.00	135.73	0.23	2.32	1.00	0.02	42.09	133.45	0.22	2.37	1.00	0.02
42.14	131.91	0.21	2.40	1.00	0.02	42.20	130.67	0.21	2.42	1.00	0.02
42.29	128.89	0.20	2.46	1.00	0.03	42.34	128.21	0.20	2.47	1.00	0.02
42.39	127.48	0.20	2.49	1.00	0.01	42.48	126.79	0.20	2.50	1.00	0.03
42.54	126.63	0.20	2.51	1.00	0.02	42.59	126.65	0.20	2.50	1.00	0.02
42.68	126.99	0.20	2.50	1.00	0.02	42.73	127.22	0.20	2.49	1.00	0.02
42.79	127.48	0.20	2.49	1.00	0.02	42.88	126.12	0.19	2.52	1.00	0.03
42.93	124.97	0.19	2.54	1.00	0.01	42.99	123.19	0.19	2.58	1.00	0.02
43.06	122.14	0.18	2.61	1.00	0.02	43.14	120.19	0.18	2.65	1.00	0.03
43.18	118.20	0.17	2.70	1.00	0.01	43.28	113.60	0.16	2.81	1.00	0.03
43.33	109.66	0.16	2.92	1.00	0.02	43.42	40.25	2.00	0.00	1.00	0.00
43.44	38.58	2.00	0.00	1.00	0.00	43.53	34.46	2.00	0.00	1.00	0.00
43.58	33.13	2.00	0.00	1.00	0.00	43.67	28.74	2.00	0.00	1.00	0.00
43.73	27.19	2.00	0.00	1.00	0.00	43.78	26.28	2.00	0.00	1.00	0.00
43.86	27.10	2.00	0.00	1.00	0.00	43.92	26.79	2.00	0.00	1.00	0.00
43.97	27.01	2.00	0.00	1.00	0.00	44.06	26.88	2.00	0.00	1.00	0.00
44.12	25.43	2.00	0.00	1.00	0.00	44.17	22.75	2.00	0.00	1.00	0.00
44.26	18.44	2.00	0.00	1.00	0.00	44.30	16.18	2.00	0.00	1.00	0.00
44.37	13.25	2.00	0.00	1.00	0.00	44.44	11.60	2.00	0.00	1.00	0.00
44.50	12.00	2.00	0.00	1.00	0.00	44.59	11.34	2.00	0.00	1.00	0.00
44.64	11.39	2.00	0.00	1.00	0.00	44.73	12.49	2.00	0.00	1.00	0.00
44.77	13.30	2.00	0.00	1.00	0.00	44.83	13.82	2.00	0.00	1.00	0.00
44.88	14.81	2.00	0.00	1.00	0.00	44.96	15.57	2.00	0.00	1.00	0.00
45.03	14.66	2.00	0.00	1.00	0.00	45.08	14.01	2.00	0.00	1.00	0.00
45.17	14.64	2.00	0.00	1.00	0.00	45.22	14.04	2.00	0.00	1.00	0.00
45.28	14.62	2.00	0.00	1.00	0.00	45.36	14.02	2.00	0.00	1.00	0.00
45.41	12.84	2.00	0.00	1.00	0.00	45.48	11.78	2.00	0.00	1.00	0.00
45.54	11.14	2.00	0.00	1.00	0.00	45.63	10.90	2.00	0.00	1.00	0.00
45.67	11.18	2.00	0.00	1.00	0.00	45.74	17.37	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
45.83	38.77	2.00	0.00	1.00	0.00	45.88	120.03	0.18	2.65	1.00	0.02
45.97	134.42	0.22	2.35	1.00	0.03	46.03	139.17	0.24	2.26	1.00	0.02
46.07	144.05	0.27	2.17	1.00	0.01	46.17	152.41	0.32	2.04	1.00	0.02
46.22	156.67	0.36	1.93	1.00	0.01	46.27	161.31	0.40	1.65	1.00	0.01
46.36	167.11	0.48	1.35	1.00	0.02	46.41	170.76	0.54	1.19	1.00	0.01
46.49	178.03	0.71	0.92	1.00	0.01	46.54	185.31	0.95	0.71	1.00	0.00
46.62	195.32	1.53	0.23	1.00	0.00	46.66	198.05	1.76	0.10	1.00	0.00
46.73	202.50	2.00	0.00	1.00	0.00	46.82	202.35	2.00	0.00	1.00	0.00
46.85	201.30	2.00	0.00	1.00	0.00	46.92	198.90	1.84	0.06	1.00	0.00
47.01	196.87	1.65	0.16	1.00	0.00	47.06	194.98	1.50	0.24	1.00	0.00
47.15	191.42	1.26	0.42	1.00	0.00	47.21	191.12	1.24	0.44	1.00	0.00
47.25	190.25	1.19	0.48	1.00	0.00	47.31	183.31	0.88	0.76	1.00	0.01
47.41	187.38	1.05	0.64	1.00	0.01	47.46	190.61	1.21	0.46	1.00	0.00
47.54	194.30	1.45	0.28	1.00	0.00	47.58	195.42	1.53	0.22	1.00	0.00
47.67	199.38	1.89	0.04	1.00	0.00	47.71	199.58	1.91	0.04	1.00	0.00
47.77	197.45	1.70	0.13	1.00	0.00	47.85	196.30	1.60	0.18	1.00	0.00
47.92	195.56	1.54	0.22	1.00	0.00	47.97	195.48	1.54	0.22	1.00	0.00
48.06	197.28	1.69	0.14	1.00	0.00	48.12	198.62	1.81	0.08	1.00	0.00
48.17	200.41	2.00	0.00	1.00	0.00	48.25	202.34	2.00	0.00	1.00	0.00
48.31	203.07	2.00	0.00	1.00	0.00	48.36	203.56	2.00	0.00	1.00	0.00
48.45	201.77	2.00	0.00	1.00	0.00	48.50	200.02	1.95	0.02	1.00	0.00
48.57	199.06	1.85	0.06	1.00	0.00	48.63	197.39	1.70	0.13	1.00	0.00
48.72	195.33	1.52	0.23	1.00	0.00	48.77	193.35	1.38	0.33	1.00	0.00
48.85	189.61	1.16	0.52	1.00	0.01	48.91	186.33	1.00	0.68	1.00	0.00
48.97	185.63	0.97	0.70	1.00	0.00	49.05	183.66	0.89	0.75	1.00	0.01
49.11	181.74	0.82	0.80	1.00	0.01	49.16	179.91	0.76	0.86	1.00	0.01
49.21	176.82	0.67	0.96	1.00	0.01	49.28	171.32	0.55	1.17	1.00	0.01
49.35	170.21	0.53	1.21	1.00	0.01	49.42	173.14	0.59	1.10	1.00	0.01
49.48	173.46	0.60	1.08	1.00	0.01	49.54	177.39	0.69	0.94	1.00	0.01
49.61	171.39	0.55	1.16	1.00	0.01	49.68	174.15	0.61	1.06	1.00	0.01
49.76	168.07	0.50	1.31	1.00	0.01	49.81	168.90	0.51	1.27	1.00	0.01
49.88	172.35	0.57	1.13	1.00	0.01	49.95	175.35	0.64	1.01	1.00	0.01
50.02	177.89	2.00	0.00	1.00	0.00	50.10	179.95	2.00	0.00	1.00	0.00
50.15	181.14	2.00	0.00	1.00	0.00	50.20	183.54	2.00	0.00	1.00	0.00
50.28	185.92	2.00	0.00	1.00	0.00	50.34	187.95	2.00	0.00	1.00	0.00
50.44	190.87	2.00	0.00	1.00	0.00	50.47	191.84	2.00	0.00	1.00	0.00
50.54	192.81	2.00	0.00	1.00	0.00	50.59	192.94	2.00	0.00	1.00	0.00
50.69	192.54	2.00	0.00	1.00	0.00	50.73	192.18	2.00	0.00	1.00	0.00
50.84	190.39	2.00	0.00	1.00	0.00	50.86	189.88	2.00	0.00	1.00	0.00
50.93	188.45	2.00	0.00	1.00	0.00	50.99	187.30	2.00	0.00	1.00	0.00
51.05	185.73	2.00	0.00	1.00	0.00	51.13	185.28	2.00	0.00	1.00	0.00
51.20	185.19	2.00	0.00	1.00	0.00	51.25	184.94	2.00	0.00	1.00	0.00
51.34	184.95	2.00	0.00	1.00	0.00	51.38	184.99	2.00	0.00	1.00	0.00
51.48	185.93	2.00	0.00	1.00	0.00	51.53	186.79	2.00	0.00	1.00	0.00
51.58	187.34	2.00	0.00	1.00	0.00	51.67	187.52	2.00	0.00	1.00	0.00
51.72	187.05	2.00	0.00	1.00	0.00	51.78	186.69	2.00	0.00	1.00	0.00
51.86	186.04	2.00	0.00	1.00	0.00	51.93	185.91	2.00	0.00	1.00	0.00
51.97	185.83	2.00	0.00	1.00	0.00	52.06	186.82	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
52.11	187.73	2.00	0.00	1.00	0.00	52.17	188.53	2.00	0.00	1.00	0.00
52.24	189.94	2.00	0.00	1.00	0.00	52.31	190.71	2.00	0.00	1.00	0.00
52.37	189.97	2.00	0.00	1.00	0.00	52.47	187.07	2.00	0.00	1.00	0.00
52.52	184.29	2.00	0.00	1.00	0.00	52.57	182.60	2.00	0.00	1.00	0.00
52.67	176.18	2.00	0.00	1.00	0.00	52.72	172.23	2.00	0.00	1.00	0.00
52.77	168.18	2.00	0.00	1.00	0.00	52.86	162.59	2.00	0.00	1.00	0.00
52.91	159.19	2.00	0.00	1.00	0.00	52.96	156.05	2.00	0.00	1.00	0.00
53.02	152.90	2.00	0.00	1.00	0.00	53.10	148.54	2.00	0.00	1.00	0.00
53.16	145.76	2.00	0.00	1.00	0.00	53.24	142.32	2.00	0.00	1.00	0.00
53.30	139.63	2.00	0.00	1.00	0.00	53.36	136.64	2.00	0.00	1.00	0.00
53.42	135.52	2.00	0.00	1.00	0.00	53.48	134.58	2.00	0.00	1.00	0.00
53.56	134.90	2.00	0.00	1.00	0.00	53.61	134.59	2.00	0.00	1.00	0.00
53.69	138.42	2.00	0.00	1.00	0.00	53.75	142.37	2.00	0.00	1.00	0.00
53.82	144.39	2.00	0.00	1.00	0.00	53.88	144.60	2.00	0.00	1.00	0.00
53.97	143.17	2.00	0.00	1.00	0.00	54.02	142.02	2.00	0.00	1.00	0.00
54.09	138.09	2.00	0.00	1.00	0.00	54.14	134.86	2.00	0.00	1.00	0.00
54.21	131.46	2.00	0.00	1.00	0.00	54.28	126.89	2.00	0.00	1.00	0.00
54.33	124.35	2.00	0.00	1.00	0.00	54.43	123.22	2.00	0.00	1.00	0.00
54.48	123.37	2.00	0.00	1.00	0.00	54.53	123.91	2.00	0.00	1.00	0.00
54.62	123.61	2.00	0.00	1.00	0.00	54.67	122.74	2.00	0.00	1.00	0.00
54.73	122.09	2.00	0.00	1.00	0.00	54.82	120.01	2.00	0.00	1.00	0.00
54.87	118.68	2.00	0.00	1.00	0.00	54.95	116.92	2.00	0.00	1.00	0.00
55.01	116.05	2.00	0.00	1.00	0.00	55.06	114.44	2.00	0.00	1.00	0.00
55.12	112.66	2.00	0.00	1.00	0.00	55.20	110.91	2.00	0.00	1.00	0.00
55.26	110.03	2.00	0.00	1.00	0.00	55.32	109.14	2.00	0.00	1.00	0.00
55.41	109.10	2.00	0.00	1.00	0.00	55.47	110.29	2.00	0.00	1.00	0.00
55.51	112.23	2.00	0.00	1.00	0.00	55.59	117.31	2.00	0.00	1.00	0.00
55.67	126.12	2.00	0.00	1.00	0.00	55.72	133.00	2.00	0.00	1.00	0.00
55.81	142.00	2.00	0.00	1.00	0.00	55.86	145.78	2.00	0.00	1.00	0.00
55.92	149.22	2.00	0.00	1.00	0.00	56.01	155.60	2.00	0.00	1.00	0.00
56.06	159.03	2.00	0.00	1.00	0.00	56.11	162.33	2.00	0.00	1.00	0.00
56.21	169.08	2.00	0.00	1.00	0.00	56.25	172.69	2.00	0.00	1.00	0.00
56.31	174.12	2.00	0.00	1.00	0.00	56.38	158.88	2.00	0.00	1.00	0.00
56.44	162.27	2.00	0.00	1.00	0.00	56.50	164.09	2.00	0.00	1.00	0.00
56.58	165.26	2.00	0.00	1.00	0.00	56.65	168.72	2.00	0.00	1.00	0.00
56.73	179.81	2.00	0.00	1.00	0.00	56.76	181.56	2.00	0.00	1.00	0.00
56.84	185.30	2.00	0.00	1.00	0.00	56.92	189.91	2.00	0.00	1.00	0.00
56.98	192.50	2.00	0.00	1.00	0.00	57.02	193.33	2.00	0.00	1.00	0.00
57.12	194.52	2.00	0.00	1.00	0.00	57.17	195.09	2.00	0.00	1.00	0.00
57.23	195.61	2.00	0.00	1.00	0.00	57.32	197.31	2.00	0.00	1.00	0.00
57.36	198.07	2.00	0.00	1.00	0.00	57.42	199.26	2.00	0.00	1.00	0.00
57.50	200.50	2.00	0.00	1.00	0.00	57.55	201.29	2.00	0.00	1.00	0.00
57.62	202.96	2.00	0.00	1.00	0.00	57.69	203.15	2.00	0.00	1.00	0.00
57.77	203.27	2.00	0.00	1.00	0.00	57.83	203.84	2.00	0.00	1.00	0.00
57.91	204.71	2.00	0.00	1.00	0.00	57.97	205.17	2.00	0.00	1.00	0.00
58.01	206.31	2.00	0.00	1.00	0.00	58.11	207.93	2.00	0.00	1.00	0.00
58.16	207.71	2.00	0.00	1.00	0.00	58.22	206.79	2.00	0.00	1.00	0.00
58.31	204.10	2.00	0.00	1.00	0.00	58.36	204.19	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
58.41	205.90	2.00	0.00	1.00	0.00	58.51	208.97	2.00	0.00	1.00	0.00
58.55	210.41	2.00	0.00	1.00	0.00	58.60	210.61	2.00	0.00	1.00	0.00
58.67	208.78	2.00	0.00	1.00	0.00	58.76	206.61	2.00	0.00	1.00	0.00
58.80	205.90	2.00	0.00	1.00	0.00	58.88	204.46	2.00	0.00	1.00	0.00
58.94	205.88	2.00	0.00	1.00	0.00	59.01	208.88	2.00	0.00	1.00	0.00
59.06	209.78	2.00	0.00	1.00	0.00	59.15	207.43	2.00	0.00	1.00	0.00
59.20	206.44	2.00	0.00	1.00	0.00	59.25	206.14	2.00	0.00	1.00	0.00
59.34	210.17	2.00	0.00	1.00	0.00	59.40	205.58	2.00	0.00	1.00	0.00
59.45	191.98	2.00	0.00	1.00	0.00	59.54	197.31	2.00	0.00	1.00	0.00
59.60	199.37	2.00	0.00	1.00	0.00	59.65	201.63	2.00	0.00	1.00	0.00
59.74	204.24	2.00	0.00	1.00	0.00	59.78	199.16	2.00	0.00	1.00	0.00
59.87	189.00	2.00	0.00	1.00	0.00	59.94	190.86	2.00	0.00	1.00	0.00
59.99	193.35	2.00	0.00	1.00	0.00	60.05	196.97	2.00	0.00	1.00	0.00
60.14	202.64	2.00	0.00	1.00	0.00	60.19	202.72	2.00	0.00	1.00	0.00
60.24	203.33	2.00	0.00	1.00	0.00	60.34	203.89	2.00	0.00	1.00	0.00
60.38	205.99	2.00	0.00	1.00	0.00	60.44	209.05	2.00	0.00	1.00	0.00
60.53	213.07	2.00	0.00	1.00	0.00	60.58	215.31	2.00	0.00	1.00	0.00
60.63	217.15	2.00	0.00	1.00	0.00	60.71	218.45	2.00	0.00	1.00	0.00
60.78	219.09	2.00	0.00	1.00	0.00	60.83	218.86	2.00	0.00	1.00	0.00
60.91	217.77	2.00	0.00	1.00	0.00	60.97	216.92	2.00	0.00	1.00	0.00
61.03	217.90	2.00	0.00	1.00	0.00	61.10	217.89	2.00	0.00	1.00	0.00
61.16	216.53	2.00	0.00	1.00	0.00	61.23	216.32	2.00	0.00	1.00	0.00
61.32	215.47	2.00	0.00	1.00	0.00	61.38	216.63	2.00	0.00	1.00	0.00
61.43	218.76	2.00	0.00	1.00	0.00	61.52	218.81	2.00	0.00	1.00	0.00
61.56	217.68	2.00	0.00	1.00	0.00	61.62	217.25	2.00	0.00	1.00	0.00
61.71	217.78	2.00	0.00	1.00	0.00	61.77	218.43	2.00	0.00	1.00	0.00
61.84	217.43	2.00	0.00	1.00	0.00	61.92	213.83	2.00	0.00	1.00	0.00
61.94	213.13	2.00	0.00	1.00	0.00	62.02	211.37	2.00	0.00	1.00	0.00
62.12	211.56	2.00	0.00	1.00	0.00	62.15	211.38	2.00	0.00	1.00	0.00
62.22	211.00	2.00	0.00	1.00	0.00	62.27	211.09	2.00	0.00	1.00	0.00
62.36	210.18	2.00	0.00	1.00	0.00	62.41	210.11	2.00	0.00	1.00	0.00
62.48	209.15	2.00	0.00	1.00	0.00	62.55	207.44	2.00	0.00	1.00	0.00
62.61	206.03	2.00	0.00	1.00	0.00	62.69	204.08	2.00	0.00	1.00	0.00
62.74	202.67	2.00	0.00	1.00	0.00	62.81	203.30	2.00	0.00	1.00	0.00
62.87	203.53	2.00	0.00	1.00	0.00	62.95	203.43	2.00	0.00	1.00	0.00
63.00	204.38	2.00	0.00	1.00	0.00	63.10	207.09	2.00	0.00	1.00	0.00
63.13	208.27	2.00	0.00	1.00	0.00	63.19	207.13	2.00	0.00	1.00	0.00
63.26	206.69	2.00	0.00	1.00	0.00	63.32	203.28	2.00	0.00	1.00	0.00
63.39	199.40	2.00	0.00	1.00	0.00	63.49	196.42	2.00	0.00	1.00	0.00
63.52	194.22	2.00	0.00	1.00	0.00	63.60	187.46	2.00	0.00	1.00	0.00
63.69	183.81	2.00	0.00	1.00	0.00	63.74	184.98	2.00	0.00	1.00	0.00
63.79	185.16	2.00	0.00	1.00	0.00	63.85	184.34	2.00	0.00	1.00	0.00
63.92	180.04	2.00	0.00	1.00	0.00	63.99	173.68	2.00	0.00	1.00	0.00
64.05	169.87	2.00	0.00	1.00	0.00	64.13	166.86	2.00	0.00	1.00	0.00
64.18	166.88	2.00	0.00	1.00	0.00	64.24	167.94	2.00	0.00	1.00	0.00
64.34	165.38	2.00	0.00	1.00	0.00	64.39	163.98	2.00	0.00	1.00	0.00
64.45	165.12	2.00	0.00	1.00	0.00	64.51	159.41	2.00	0.00	1.00	0.00
64.59	162.60	2.00	0.00	1.00	0.00	64.64	166.42	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
64.73	169.15	2.00	0.00	1.00	0.00	64.78	171.18	2.00	0.00	1.00	0.00
64.83	175.46	2.00	0.00	1.00	0.00	64.93	182.82	2.00	0.00	1.00	0.00
64.98	186.29	2.00	0.00	1.00	0.00	65.03	190.26	2.00	0.00	1.00	0.00
65.12	195.26	2.00	0.00	1.00	0.00	65.17	198.31	2.00	0.00	1.00	0.00
65.23	200.64	2.00	0.00	1.00	0.00	65.31	202.83	2.00	0.00	1.00	0.00
65.36	202.50	2.00	0.00	1.00	0.00	65.42	202.06	2.00	0.00	1.00	0.00
65.50	198.90	2.00	0.00	1.00	0.00	65.58	195.52	2.00	0.00	1.00	0.00
65.63	194.02	2.00	0.00	1.00	0.00	65.72	194.15	2.00	0.00	1.00	0.00
65.77	195.68	2.00	0.00	1.00	0.00	65.83	198.77	2.00	0.00	1.00	0.00
65.92	197.11	2.00	0.00	1.00	0.00	65.97	195.95	2.00	0.00	1.00	0.00
66.02	196.36	2.00	0.00	1.00	0.00	66.11	199.55	2.00	0.00	1.00	0.00
66.16	203.81	2.00	0.00	1.00	0.00	66.22	207.06	2.00	0.00	1.00	0.00
66.30	210.41	2.00	0.00	1.00	0.00	66.35	211.98	2.00	0.00	1.00	0.00
66.42	212.12	2.00	0.00	1.00	0.00	66.50	210.99	2.00	0.00	1.00	0.00
66.55	210.37	2.00	0.00	1.00	0.00	66.61	210.70	2.00	0.00	1.00	0.00
66.70	206.90	2.00	0.00	1.00	0.00	66.76	202.22	2.00	0.00	1.00	0.00
66.80	196.86	2.00	0.00	1.00	0.00	66.88	185.90	2.00	0.00	1.00	0.00
66.96	171.96	2.00	0.00	1.00	0.00	67.01	161.76	2.00	0.00	1.00	0.00
67.06	148.53	2.00	0.00	1.00	0.00	67.13	139.94	2.00	0.00	1.00	0.00
67.19	121.68	2.00	0.00	1.00	0.00	67.29	120.46	2.00	0.00	1.00	0.00
67.35	127.14	2.00	0.00	1.00	0.00	67.40	125.34	2.00	0.00	1.00	0.00
67.50	119.31	2.00	0.00	1.00	0.00	67.55	116.96	2.00	0.00	1.00	0.00
67.60	112.00	2.00	0.00	1.00	0.00	67.68	103.29	2.00	0.00	1.00	0.00
67.73	98.63	2.00	0.00	1.00	0.00	67.79	33.90	2.00	0.00	1.00	0.00
67.87	31.29	2.00	0.00	1.00	0.00	67.93	31.07	2.00	0.00	1.00	0.00
67.98	32.58	2.00	0.00	1.00	0.00	68.05	35.97	2.00	0.00	1.00	0.00
68.11	108.48	2.00	0.00	1.00	0.00	68.19	127.05	2.00	0.00	1.00	0.00
68.25	132.41	2.00	0.00	1.00	0.00	68.34	115.36	2.00	0.00	1.00	0.00
68.39	141.79	2.00	0.00	1.00	0.00	68.44	167.06	2.00	0.00	1.00	0.00
68.54	196.19	2.00	0.00	1.00	0.00	68.59	207.80	2.00	0.00	1.00	0.00
68.64	214.37	2.00	0.00	1.00	0.00	68.71	202.31	2.00	0.00	1.00	0.00
68.77	182.61	2.00	0.00	1.00	0.00	68.84	223.06	2.00	0.00	1.00	0.00
68.91	228.33	2.00	0.00	1.00	0.00	68.97	233.57	2.00	0.00	1.00	0.00
69.04	240.08	2.00	0.00	1.00	0.00	69.12	241.63	2.00	0.00	1.00	0.00
69.17	237.53	2.00	0.00	1.00	0.00	69.27	222.17	2.00	0.00	1.00	0.00
69.29	216.69	2.00	0.00	1.00	0.00	69.37	201.08	2.00	0.00	1.00	0.00
69.42	195.81	2.00	0.00	1.00	0.00	69.52	188.11	2.00	0.00	1.00	0.00
69.57	183.54	2.00	0.00	1.00	0.00	69.65	173.57	2.00	0.00	1.00	0.00
69.71	166.81	2.00	0.00	1.00	0.00	69.77	166.93	2.00	0.00	1.00	0.00
69.85	165.77	2.00	0.00	1.00	0.00	69.89	167.00	2.00	0.00	1.00	0.00
69.96	169.52	2.00	0.00	1.00	0.00	70.02	173.53	2.00	0.00	1.00	0.00
70.09	177.22	2.00	0.00	1.00	0.00	70.15	176.08	2.00	0.00	1.00	0.00
70.24	174.92	2.00	0.00	1.00	0.00	70.30	178.18	2.00	0.00	1.00	0.00
70.36	180.38	2.00	0.00	1.00	0.00	70.44	177.23	2.00	0.00	1.00	0.00
70.48	176.59	2.00	0.00	1.00	0.00	70.55	174.51	2.00	0.00	1.00	0.00
70.60	176.21	2.00	0.00	1.00	0.00	70.69	179.20	2.00	0.00	1.00	0.00
70.74	179.68	2.00	0.00	1.00	0.00	70.83	179.90	2.00	0.00	1.00	0.00
70.89	179.99	2.00	0.00	1.00	0.00	70.94	180.47	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
71.02	180.15	2.00	0.00	1.00	0.00	71.08	179.24	2.00	0.00	1.00	0.00
71.14	177.92	2.00	0.00	1.00	0.00	71.22	174.90	2.00	0.00	1.00	0.00
71.27	172.35	2.00	0.00	1.00	0.00	71.33	167.35	2.00	0.00	1.00	0.00
71.40	166.17	2.00	0.00	1.00	0.00	71.47	165.75	2.00	0.00	1.00	0.00
71.53	162.71	2.00	0.00	1.00	0.00	71.63	158.67	2.00	0.00	1.00	0.00
71.67	158.32	2.00	0.00	1.00	0.00	71.73	156.99	2.00	0.00	1.00	0.00
71.81	158.26	2.00	0.00	1.00	0.00	71.88	168.01	2.00	0.00	1.00	0.00
71.93	184.69	2.00	0.00	1.00	0.00	71.99	194.23	2.00	0.00	1.00	0.00
72.05	201.25	2.00	0.00	1.00	0.00	72.13	208.56	2.00	0.00	1.00	0.00
72.18	212.15	2.00	0.00	1.00	0.00	72.27	216.90	2.00	0.00	1.00	0.00
72.32	218.42	2.00	0.00	1.00	0.00	72.38	217.88	2.00	0.00	1.00	0.00
72.46	215.08	2.00	0.00	1.00	0.00	72.52	210.98	2.00	0.00	1.00	0.00
72.62	208.59	2.00	0.00	1.00	0.00	72.66	209.41	2.00	0.00	1.00	0.00
72.71	211.57	2.00	0.00	1.00	0.00	72.82	217.28	2.00	0.00	1.00	0.00
72.85	220.76	2.00	0.00	1.00	0.00	72.91	223.66	2.00	0.00	1.00	0.00
72.97	228.47	2.00	0.00	1.00	0.00	73.06	237.25	2.00	0.00	1.00	0.00
73.11	242.61	2.00	0.00	1.00	0.00	73.17	252.72	2.00	0.00	1.00	0.00
73.24	257.50	2.00	0.00	1.00	0.00	73.31	260.76	2.00	0.00	1.00	0.00
73.37	263.29	2.00	0.00	1.00	0.00	73.43	265.00	2.00	0.00	1.00	0.00
73.51	267.85	2.00	0.00	1.00	0.00	73.56	268.77	2.00	0.00	1.00	0.00
73.65	271.40	2.00	0.00	1.00	0.00	73.71	271.56	2.00	0.00	1.00	0.00
73.76	271.88	2.00	0.00	1.00	0.00	73.84	271.61	2.00	0.00	1.00	0.00
73.90	270.57	2.00	0.00	1.00	0.00	73.95	269.06	2.00	0.00	1.00	0.00
74.06	266.10	2.00	0.00	1.00	0.00	74.10	262.37	2.00	0.00	1.00	0.00
74.15	258.51	2.00	0.00	1.00	0.00	74.22	250.05	2.00	0.00	1.00	0.00
74.29	244.89	2.00	0.00	1.00	0.00	74.35	237.77	2.00	0.00	1.00	0.00
74.43	228.42	2.00	0.00	1.00	0.00	74.48	222.52	2.00	0.00	1.00	0.00
74.54	171.47	2.00	0.00	1.00	0.00	74.64	200.83	2.00	0.00	1.00	0.00
74.69	194.17	2.00	0.00	1.00	0.00	74.75	187.70	2.00	0.00	1.00	0.00
74.83	179.44	2.00	0.00	1.00	0.00	74.87	173.35	2.00	0.00	1.00	0.00
74.94	168.25	2.00	0.00	1.00	0.00	75.02	164.30	2.00	0.00	1.00	0.00
75.08	163.83	2.00	0.00	1.00	0.00	75.13	166.48	2.00	0.00	1.00	0.00
75.22	162.93	2.00	0.00	1.00	0.00	75.28	187.47	2.00	0.00	1.00	0.00
75.33	188.80	2.00	0.00	1.00	0.00	75.42	190.33	2.00	0.00	1.00	0.00
75.47	191.54	2.00	0.00	1.00	0.00	75.53	192.66	2.00	0.00	1.00	0.00
75.62	193.52	2.00	0.00	1.00	0.00						

Total estimated settlement: 7.09

Abbreviations

- Q_{tn,cs}: Equivalent clean sand normalized cone resistance
- FS: Factor of safety against liquefaction
- e_v (%): Post-liquefaction volumetric strain
- DF: e_v depth weighting factor
- Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
0.10	7.73	12.41	8.09	100.36	2.96	0.08	0.62
0.16	10.44	16.76	7.60	127.40	2.93	0.09	0.62
0.20	10.04	16.11	9.68	155.94	3.05	0.09	66.28
0.28	15.86	25.46	4.81	122.43	2.71	0.09	0.62
0.34	25.10	40.30	2.37	95.32	2.40	0.10	0.75
0.41	44.98	72.23	1.35	97.52	2.05	0.12	0.78
0.48	52.61	84.48	1.30	109.47	1.99	0.13	0.79
0.55	50.55	81.17	1.35	109.72	2.05	0.13	0.80
0.60	32.73	52.53	2.07	108.94	2.34	0.12	0.77
0.67	48.49	77.84	1.48	115.49	2.14	0.14	0.80
0.74	58.13	93.32	1.35	126.44	2.05	0.16	0.82
0.79	70.38	113.00	1.27	142.97	1.94	0.18	0.82
0.89	78.81	126.53	1.25	157.94	1.92	0.22	0.84
0.94	84.53	135.73	1.23	167.47	1.90	0.25	0.84
0.98	88.14	141.52	1.23	173.65	1.89	0.28	0.85
1.06	86.53	138.93	1.27	176.31	1.95	0.29	0.86
1.12	81.61	131.01	1.32	172.43	2.01	0.28	0.87
1.20	76.99	123.59	1.38	170.07	2.07	0.26	0.87
1.25	68.35	109.69	1.52	166.27	2.16	0.23	0.86
1.34	62.52	100.32	1.64	164.85	2.21	0.21	0.85
1.38	56.80	91.12	1.81	164.91	2.27	0.19	0.84
1.46	49.87	79.98	2.08	166.10	2.34	0.17	0.82
1.54	45.55	73.03	2.24	163.86	2.37	0.16	0.81
1.60	38.81	62.21	2.71	168.27	2.46	0.14	0.80
1.66	34.80	55.76	3.03	168.75	2.51	0.13	0.79
1.75	28.97	46.38	3.73	172.96	2.60	0.12	0.77
1.80	26.36	42.18	4.13	174.11	2.64	0.11	0.62
1.86	23.45	37.50	4.66	174.87	2.70	0.11	0.62
1.91	21.04	33.62	5.25	176.64	2.75	0.11	0.62
1.98	18.94	30.24	5.72	173.08	2.79	0.10	0.62
2.04	17.33	27.65	6.02	166.37	2.81	0.10	0.62
2.14	15.52	24.74	6.29	155.51	2.83	0.09	0.62
2.17	14.42	22.97	6.72	154.37	2.87	0.09	0.62
2.24	13.61	21.66	6.83	147.93	2.87	0.09	0.62
2.32	12.91	20.53	6.91	141.84	2.88	0.09	0.62
2.37	12.61	20.04	6.89	138.01	2.88	0.09	0.62
2.43	11.91	18.91	7.10	134.31	2.89	0.09	0.62
2.53	11.81	18.74	6.90	129.36	2.88	0.09	0.62
2.58	11.41	18.09	7.18	129.97	2.90	0.09	0.62
2.64	11.41	18.09	7.20	130.30	2.90	0.09	0.62
2.70	11.42	18.09	7.33	132.55	2.91	0.09	0.62
2.78	12.52	19.85	6.85	136.01	2.88	0.09	0.62
2.82	13.32	21.13	6.52	137.74	2.85	0.09	0.62
2.89	18.04	28.71	4.50	129.27	2.68	0.10	0.62
2.96	21.66	34.52	3.52	121.35	2.57	0.10	0.74
3.03	24.27	38.70	2.99	115.77	2.50	0.10	0.75
3.12	23.36	37.23	3.03	112.96	2.51	0.10	0.74
3.17	22.06	35.14	3.21	112.87	2.53	0.10	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
3.23	20.95	33.35	3.33	110.99	2.55	0.10	0.74
3.28	19.95	31.74	3.28	103.97	2.54	0.10	0.73
3.35	19.35	30.77	3.04	93.59	2.51	0.09	0.73
3.43	18.24	28.98	2.94	85.12	2.49	0.09	0.72
3.48	17.24	27.37	2.92	80.05	2.49	0.09	0.72
3.56	16.54	26.24	2.76	72.49	2.47	0.09	0.71
3.61	16.23	25.74	2.68	69.06	2.45	0.08	0.71
3.68	16.95	26.89	2.53	67.98	2.43	0.08	0.71
3.77	18.75	29.78	2.21	65.78	2.37	0.09	0.72
3.82	20.47	32.53	1.99	64.57	2.32	0.09	0.72
3.87	22.38	35.59	1.82	64.77	2.27	0.09	0.73
3.96	23.98	38.16	1.69	64.59	2.23	0.09	0.73
4.02	24.49	38.98	1.64	63.98	2.21	0.09	0.73
4.11	24.89	39.62	1.63	64.38	2.20	0.09	0.73
4.16	25.49	40.58	1.60	64.78	2.19	0.09	0.73
4.21	25.90	41.22	1.58	65.14	2.19	0.09	0.73
4.27	27.71	44.12	1.50	66.37	2.15	0.09	0.74
4.35	24.80	39.44	1.68	66.12	2.22	0.09	0.73
4.40	29.82	47.50	1.44	68.53	2.12	0.09	0.74
4.47	33.93	54.10	1.36	73.79	2.06	0.09	0.74
4.55	35.54	56.68	1.35	76.75	2.05	0.10	0.75
4.61	37.05	59.10	1.34	79.25	2.04	0.10	0.75
4.68	38.35	61.18	1.34	81.96	2.04	0.10	0.76
4.75	38.85	61.98	1.35	83.71	2.05	0.10	0.76
4.80	38.95	62.14	1.36	84.50	2.05	0.10	0.76
4.86	38.45	61.33	1.39	85.00	2.08	0.11	0.76
4.93	37.85	60.36	1.41	84.94	2.09	0.11	0.76
5.00	36.85	58.75	1.43	84.10	2.11	0.11	0.76
5.05	35.14	55.99	1.47	82.54	2.13	0.10	0.76
5.14	32.43	51.63	1.56	80.67	2.18	0.10	0.76
5.19	32.33	51.47	1.55	79.95	2.17	0.10	0.76
5.28	32.93	52.42	1.52	79.57	2.16	0.10	0.76
5.34	34.14	54.36	1.47	80.16	2.13	0.10	0.76
5.38	35.74	56.93	1.43	81.33	2.11	0.10	0.76
5.45	37.75	60.15	1.39	83.38	2.08	0.10	0.76
5.54	41.56	66.26	1.33	88.28	2.03	0.11	0.76
5.59	43.77	69.81	1.31	91.30	2.00	0.11	0.77
5.65	45.28	72.23	1.30	93.67	1.99	0.11	0.77
5.73	45.88	73.19	1.30	94.86	1.99	0.11	0.77
5.79	45.28	72.22	1.31	94.34	2.00	0.11	0.77
5.84	43.47	69.31	1.33	92.06	2.02	0.11	0.77
5.94	39.56	63.02	1.39	87.72	2.08	0.11	0.77
5.99	36.85	58.66	1.45	85.09	2.12	0.11	0.76
6.04	35.34	56.23	1.49	84.06	2.15	0.11	0.76
6.12	29.82	47.35	1.80	85.46	2.27	0.10	0.76
6.19	26.81	42.51	2.13	90.56	2.35	0.10	0.75
6.24	24.60	38.95	2.47	96.13	2.42	0.10	0.74
6.31	21.08	33.29	3.12	103.75	2.52	0.10	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
6.37	20.08	31.68	3.31	104.85	2.55	0.10	0.73
6.44	18.37	28.93	3.81	110.19	2.61	0.09	0.62
6.52	17.07	26.83	4.50	120.86	2.68	0.09	0.62
6.58	16.77	26.34	4.83	127.18	2.71	0.09	0.62
6.64	16.77	26.34	4.96	130.67	2.72	0.09	0.62
6.72	17.87	28.10	4.96	139.43	2.72	0.10	0.62
6.78	19.68	31.00	4.52	140.25	2.68	0.10	0.62
6.84	22.19	35.03	3.94	137.88	2.62	0.10	0.62
6.92	24.60	38.90	3.44	133.73	2.56	0.11	0.75
6.98	26.81	42.43	3.06	129.98	2.51	0.11	0.75
7.03	28.41	45.00	2.86	128.75	2.48	0.11	0.76
7.09	37.65	59.84	1.97	118.04	2.31	0.12	0.78
7.18	49.60	79.03	1.49	118.14	2.15	0.13	0.79
7.22	52.11	83.06	1.44	119.74	2.11	0.13	0.80
7.33	56.11	89.48	1.36	121.62	2.05	0.13	0.80
7.38	56.42	89.97	1.35	121.20	2.04	0.13	0.79
7.43	56.01	89.31	1.35	120.30	2.04	0.13	0.79
7.52	54.82	87.38	1.36	119.09	2.06	0.13	0.79
7.58	54.42	86.74	1.37	118.82	2.06	0.13	0.79
7.62	54.32	86.57	1.37	118.90	2.07	0.13	0.79
7.72	55.32	88.17	1.37	120.62	2.06	0.13	0.79
7.76	56.72	90.41	1.36	122.82	2.05	0.13	0.79
7.82	58.43	93.16	1.35	126.16	2.05	0.13	0.80
7.90	61.04	97.34	1.31	127.65	2.00	0.13	0.79
7.97	62.75	99.77	1.29	128.67	1.98	0.13	0.79
8.02	64.56	101.98	1.28	130.85	1.97	0.13	0.79
8.07	65.96	103.58	1.28	132.47	1.96	0.14	0.79
8.16	67.17	104.71	1.28	133.86	1.96	0.14	0.79
8.21	65.26	101.97	1.29	131.76	1.98	0.14	0.79
8.27	64.56	100.63	1.30	130.69	1.99	0.14	0.79
8.35	68.07	104.53	1.28	133.39	1.96	0.14	0.79
8.41	68.57	104.66	1.27	133.14	1.95	0.14	0.79
8.49	67.47	102.73	1.28	131.50	1.96	0.14	0.79
8.55	65.06	99.16	1.30	128.47	1.99	0.13	0.79
8.62	61.54	94.18	1.32	124.59	2.02	0.13	0.79
8.67	57.63	88.81	1.36	121.12	2.06	0.13	0.79
8.76	51.50	80.40	1.47	118.24	2.13	0.12	0.78
8.80	47.99	75.58	1.57	118.37	2.18	0.12	0.78
8.86	44.17	70.15	1.71	119.62	2.23	0.12	0.78
8.95	37.55	59.50	2.06	122.35	2.33	0.11	0.76
8.99	33.33	52.72	2.40	126.30	2.40	0.11	0.76
9.06	30.22	47.72	2.70	128.80	2.46	0.10	0.75
9.15	28.21	44.48	2.83	125.65	2.48	0.10	0.74
9.22	26.91	42.38	2.89	122.32	2.49	0.10	0.74
9.26	26.10	41.08	2.92	119.79	2.49	0.10	0.74
9.35	26.20	41.24	2.75	113.56	2.47	0.10	0.74
9.40	27.21	42.85	2.55	109.39	2.43	0.10	0.74
9.46	27.81	43.72	2.40	104.74	2.40	0.10	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
9.54	26.71	41.72	2.42	101.05	2.41	0.09	0.73
9.60	25.40	39.72	2.59	102.93	2.44	0.09	0.73
9.66	24.70	38.52	2.66	102.31	2.45	0.09	0.73
9.72	22.69	35.23	2.73	96.30	2.46	0.09	0.72
9.80	20.68	31.97	2.85	91.01	2.48	0.09	0.72
9.85	18.57	28.93	3.34	96.56	2.55	0.09	0.71
9.96	15.26	23.60	4.66	110.00	2.70	0.09	0.62
10.00	14.56	22.47	5.06	113.61	2.73	0.08	0.62
10.05	12.95	19.88	6.01	119.49	2.81	0.08	0.62
10.12	13.35	20.52	5.85	120.03	2.80	0.08	0.62
10.18	13.05	20.03	6.07	121.55	2.82	0.08	0.62
10.27	13.15	20.19	6.06	122.24	2.82	0.08	0.62
10.33	13.65	20.98	5.81	121.99	2.80	0.08	0.62
10.37	13.96	21.48	5.77	123.85	2.79	0.08	0.62
10.47	15.36	23.64	5.33	125.96	2.76	0.09	0.62
10.53	16.36	24.95	4.96	123.81	2.72	0.09	0.62
10.57	17.37	26.29	4.65	122.24	2.69	0.09	0.62
10.67	18.98	28.33	4.25	120.52	2.66	0.09	0.62
10.70	20.08	29.74	3.94	117.09	2.62	0.09	0.62
10.78	21.79	31.79	3.49	110.86	2.57	0.09	0.72
10.83	23.29	33.60	3.15	105.90	2.52	0.09	0.72
10.91	25.40	36.04	2.73	98.53	2.46	0.09	0.73
10.97	27.41	38.40	2.43	93.34	2.41	0.09	0.73
11.03	28.71	39.78	2.23	88.69	2.37	0.09	0.73
11.10	30.02	41.14	2.07	85.09	2.34	0.09	0.73
11.17	31.73	43.02	1.92	82.61	2.30	0.09	0.74
11.26	32.92	44.24	1.85	81.83	2.28	0.09	0.74
11.31	33.62	44.95	1.81	81.45	2.27	0.09	0.74
11.36	34.13	45.43	1.79	81.29	2.26	0.09	0.74
11.44	34.43	45.60	1.79	81.41	2.26	0.09	0.74
11.50	34.53	45.57	1.79	81.48	2.26	0.09	0.74
11.56	34.63	45.53	1.80	81.78	2.26	0.09	0.74
11.63	34.53	45.25	1.81	82.06	2.27	0.09	0.74
11.69	34.33	44.85	1.83	82.23	2.27	0.09	0.74
11.76	34.13	44.43	1.85	82.10	2.28	0.09	0.74
11.86	33.22	43.10	1.92	82.98	2.30	0.09	0.74
11.89	33.02	42.80	1.95	83.36	2.31	0.09	0.74
11.95	32.42	41.96	2.02	84.78	2.32	0.09	0.74
12.01	31.52	40.77	2.12	86.49	2.35	0.09	0.74
12.10	31.21	40.13	2.13	85.42	2.35	0.09	0.73
12.15	31.11	39.89	2.13	85.12	2.35	0.09	0.73
12.21	31.41	40.08	2.10	84.26	2.34	0.09	0.73
12.28	31.92	40.50	2.06	83.47	2.33	0.09	0.73
12.36	33.52	42.18	1.94	81.73	2.30	0.09	0.74
12.40	34.73	43.45	1.85	80.59	2.28	0.09	0.74
12.47	35.93	44.63	1.77	78.91	2.25	0.09	0.74
12.55	38.04	46.80	1.65	77.18	2.21	0.09	0.74
12.60	39.25	48.02	1.59	76.54	2.19	0.09	0.74

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
12.69	41.06	49.83	1.54	76.55	2.17	0.09	0.74
12.74	42.27	51.06	1.51	76.90	2.15	0.09	0.74
12.82	44.07	52.94	1.47	78.03	2.13	0.09	0.75
12.88	45.18	54.04	1.46	79.00	2.13	0.10	0.75
12.94	46.08	54.92	1.45	79.70	2.12	0.10	0.75
13.00	46.68	55.47	1.45	80.39	2.12	0.10	0.75
13.09	46.99	55.64	1.46	81.34	2.13	0.10	0.75
13.14	46.89	55.39	1.47	81.45	2.13	0.10	0.75
13.20	46.89	55.25	1.48	81.55	2.14	0.10	0.75
13.27	46.89	55.13	1.51	83.01	2.15	0.10	0.75
13.34	46.89	55.00	1.52	83.76	2.16	0.10	0.75
13.39	46.79	54.78	1.53	84.06	2.17	0.10	0.75
13.47	46.58	54.36	1.56	84.92	2.18	0.10	0.76
13.54	46.38	54.00	1.59	85.74	2.19	0.10	0.76
13.59	45.98	53.45	1.62	86.58	2.20	0.10	0.76
13.65	45.67	53.01	1.65	87.73	2.22	0.10	0.76
13.72	45.37	52.53	1.69	88.88	2.23	0.10	0.76
13.79	45.27	52.28	1.72	90.10	2.24	0.10	0.76
13.85	45.17	51.88	1.68	87.10	2.22	0.10	0.75
13.94	45.57	51.79	1.53	79.47	2.17	0.10	0.75
13.98	45.77	51.92	1.55	80.27	2.17	0.10	0.75
14.08	46.06	52.07	1.58	82.01	2.18	0.10	0.75
14.13	46.06	51.95	1.58	82.06	2.19	0.10	0.75
14.18	45.96	51.72	1.59	82.15	2.19	0.10	0.75
14.27	44.75	50.13	1.61	80.59	2.20	0.10	0.75
14.33	44.45	49.62	1.60	79.53	2.20	0.10	0.75
14.39	43.02	47.95	1.64	78.83	2.21	0.10	0.75
14.44	41.21	45.87	1.72	78.95	2.24	0.10	0.74
14.53	38.00	42.23	1.89	79.66	2.29	0.09	0.74
14.59	35.39	39.31	2.06	81.14	2.33	0.09	0.74
14.64	32.78	36.41	2.32	84.52	2.39	0.09	0.73
14.73	28.16	31.30	3.03	94.81	2.51	0.09	0.72
14.77	26.76	29.72	3.32	98.74	2.55	0.09	0.72
14.83	21.74	24.16	4.55	109.95	2.68	0.09	0.62
14.93	18.02	19.92	5.86	116.74	2.80	0.09	0.62
14.98	16.52	18.19	6.49	118.16	2.85	0.09	0.62
15.03	15.31	16.79	7.11	119.42	2.89	0.08	0.62
15.10	14.11	15.34	7.90	121.21	2.95	0.08	0.62
15.17	13.20	14.22	8.64	122.91	2.99	0.08	0.62
15.22	12.40	13.25	9.34	123.67	3.03	0.08	0.95
15.29	11.50	12.16	10.26	124.68	3.08	0.08	0.87
15.37	11.60	12.21	10.25	125.14	3.08	0.08	0.87
15.44	11.60	12.15	10.51	127.73	3.09	0.08	0.87
15.52	11.70	12.19	10.65	129.82	3.10	0.08	0.87
15.56	11.90	12.38	10.52	130.29	3.10	0.08	0.88
15.62	12.00	12.45	10.38	129.24	3.09	0.08	0.89
15.70	12.20	12.60	10.05	126.60	3.07	0.08	0.90
15.76	12.20	12.55	9.92	124.49	3.06	0.08	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
15.82	12.30	12.61	9.68	122.09	3.05	0.08	0.90
15.91	12.40	12.64	9.42	119.11	3.04	0.08	0.90
15.95	12.60	12.83	9.20	118.01	3.02	0.08	0.92
16.01	12.60	12.78	9.00	115.06	3.01	0.08	0.91
16.08	12.70	12.83	9.02	115.73	3.01	0.08	0.92
16.14	12.80	12.88	9.01	116.13	3.01	0.08	0.92
16.22	13.20	13.25	8.98	119.09	3.01	0.08	0.95
16.31	14.01	14.05	8.66	121.63	2.99	0.08	0.62
16.36	14.91	14.96	8.16	122.10	2.96	0.08	0.62
16.41	16.01	16.09	7.55	121.50	2.92	0.08	0.62
16.50	18.12	18.21	6.65	121.01	2.86	0.09	0.62
16.55	19.63	19.70	6.08	119.86	2.82	0.09	0.62
16.61	21.13	21.17	5.51	116.60	2.77	0.09	0.62
16.69	23.64	23.62	4.65	109.88	2.69	0.09	0.62
16.74	25.15	25.07	4.23	106.09	2.65	0.09	0.62
16.80	27.26	27.10	3.75	101.61	2.60	0.09	0.72
16.88	29.37	29.11	3.33	96.89	2.55	0.09	0.72
16.95	31.78	31.41	2.96	92.91	2.50	0.09	0.73
17.00	33.48	33.01	2.74	90.42	2.46	0.09	0.73
17.07	35.29	34.68	2.53	87.70	2.43	0.09	0.73
17.15	36.00	35.25	2.47	87.11	2.42	0.10	0.73
17.20	36.50	35.65	2.43	86.50	2.41	0.10	0.74
17.26	37.11	36.15	2.37	85.69	2.40	0.10	0.74
17.33	37.31	36.23	2.39	86.71	2.40	0.10	0.74
17.41	37.51	36.30	2.42	87.88	2.41	0.10	0.74
17.46	37.61	36.30	2.44	88.45	2.41	0.10	0.74
17.52	37.61	36.20	2.46	89.22	2.42	0.10	0.74
17.60	37.31	35.77	2.53	90.35	2.43	0.10	0.74
17.65	37.42	35.79	2.53	90.71	2.43	0.10	0.74
17.74	38.22	36.41	2.49	90.73	2.42	0.10	0.74
17.80	38.72	36.80	2.47	90.87	2.42	0.10	0.74
17.85	39.53	37.49	2.43	90.99	2.41	0.10	0.74
17.93	40.83	38.60	2.37	91.39	2.40	0.10	0.74
17.99	41.84	39.46	2.35	92.69	2.40	0.10	0.75
18.07	43.44	40.86	2.29	93.53	2.38	0.10	0.75
18.13	44.85	42.09	2.24	94.47	2.37	0.10	0.75
18.18	45.85	42.94	2.23	95.59	2.37	0.10	0.75
18.29	47.16	43.98	2.17	95.29	2.36	0.11	0.75
18.32	48.06	44.77	2.15	96.12	2.35	0.11	0.76
18.38	49.17	45.71	2.16	98.65	2.36	0.11	0.76
18.44	50.17	46.52	2.14	99.66	2.35	0.11	0.76
18.53	51.27	47.36	2.14	101.38	2.35	0.11	0.76
18.58	51.99	47.93	2.13	101.94	2.35	0.11	0.76
18.66	49.48	45.40	2.31	104.79	2.39	0.11	0.76
18.71	53.80	49.34	2.06	101.71	2.33	0.11	0.77
18.81	55.51	50.73	1.99	100.78	2.32	0.11	0.77
18.85	56.82	51.85	1.93	100.20	2.30	0.11	0.77
18.90	58.02	52.85	1.89	99.73	2.29	0.11	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
19.01	60.13	54.58	1.79	97.85	2.26	0.12	0.77
19.06	61.03	55.29	1.74	96.43	2.25	0.12	0.77
19.11	61.33	55.45	1.72	95.24	2.24	0.11	0.77
19.16	61.53	55.52	1.69	93.79	2.23	0.11	0.77
19.26	61.73	55.50	1.63	90.48	2.21	0.11	0.77
19.30	61.73	55.43	1.61	89.35	2.20	0.11	0.77
19.36	61.73	55.29	1.59	88.18	2.19	0.11	0.77
19.45	60.53	53.97	1.63	87.74	2.20	0.11	0.77
19.50	59.02	52.48	1.67	87.48	2.22	0.11	0.77
19.58	56.21	49.74	1.75	86.81	2.25	0.11	0.76
19.64	54.51	48.08	1.80	86.56	2.26	0.11	0.76
19.69	53.30	46.86	1.85	86.67	2.28	0.11	0.76
19.78	50.69	44.33	1.98	87.59	2.31	0.10	0.75
19.84	50.29	43.81	2.08	90.98	2.34	0.11	0.76
19.90	47.48	41.13	2.39	98.33	2.40	0.11	0.75
19.95	46.47	40.08	2.63	105.48	2.45	0.11	0.75
20.03	45.07	38.67	2.88	111.34	2.49	0.11	0.75
20.08	41.86	35.68	3.30	117.65	2.54	0.10	0.75
20.16	40.85	34.63	3.53	122.33	2.57	0.10	0.74
20.25	40.04	33.75	3.79	127.85	2.60	0.10	0.62
20.30	39.34	33.04	3.94	130.29	2.62	0.10	0.62
20.35	39.14	32.77	4.01	131.47	2.63	0.10	0.62
20.45	42.05	35.17	3.67	129.06	2.59	0.11	0.75
20.50	43.05	35.96	3.56	128.09	2.58	0.11	0.75
20.54	42.85	35.72	3.59	128.35	2.58	0.11	0.75
20.62	46.16	38.47	3.23	124.26	2.54	0.11	0.75
20.69	47.37	39.42	3.11	122.50	2.52	0.11	0.76
20.74	47.37	39.34	3.03	119.38	2.51	0.11	0.75
20.83	48.77	40.43	2.85	115.27	2.48	0.11	0.76
20.88	49.88	41.32	2.74	113.20	2.46	0.11	0.76
20.94	50.88	42.12	2.55	107.23	2.43	0.11	0.76
21.04	50.98	42.07	2.42	101.99	2.41	0.11	0.76
21.08	51.89	42.78	2.37	101.35	2.40	0.11	0.76
21.14	51.38	42.23	2.41	101.68	2.41	0.11	0.76
21.23	50.69	41.43	2.54	105.23	2.43	0.11	0.76
21.28	50.49	41.14	2.63	108.34	2.45	0.11	0.76
21.33	50.59	41.11	2.68	110.30	2.45	0.11	0.76
21.42	50.59	40.94	2.73	111.62	2.46	0.11	0.76
21.48	50.69	40.92	2.74	112.01	2.46	0.11	0.76
21.53	51.69	41.67	2.69	112.02	2.46	0.11	0.76
21.62	52.19	41.90	2.73	114.31	2.46	0.11	0.76
21.68	52.49	42.04	2.76	116.10	2.47	0.11	0.76
21.73	54.50	43.62	2.68	117.05	2.45	0.11	0.77
21.79	58.41	46.79	2.50	116.97	2.42	0.12	0.77
21.86	61.72	49.43	2.37	117.38	2.40	0.12	0.78
21.92	63.73	50.99	2.34	119.14	2.39	0.12	0.78
22.00	67.85	54.27	2.21	120.13	2.37	0.13	0.79
22.05	71.06	56.85	2.10	119.65	2.34	0.13	0.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
22.12	72.77	58.12	2.06	119.59	2.33	0.13	0.79
22.22	79.90	63.93	1.84	117.83	2.28	0.14	0.80
22.27	81.40	65.05	1.82	118.12	2.27	0.14	0.80
22.32	85.72	68.57	1.72	118.13	2.24	0.15	0.81
22.38	89.84	71.90	1.65	118.81	2.21	0.15	0.81
22.47	95.06	76.04	1.58	120.46	2.19	0.16	0.82
22.52	97.97	78.36	1.55	121.52	2.17	0.16	0.82
22.59	101.78	81.35	1.51	122.93	2.15	0.16	0.82
22.65	103.99	83.03	1.49	123.61	2.14	0.17	0.83
22.71	104.80	83.53	1.48	123.73	2.14	0.17	0.83
22.77	102.59	81.48	1.51	122.91	2.15	0.16	0.82
22.85	98.17	77.52	1.56	121.21	2.18	0.16	0.82
22.90	94.96	74.66	1.62	120.73	2.20	0.16	0.82
22.98	91.84	71.79	1.69	121.64	2.23	0.15	0.81
23.06	91.74	71.48	1.70	121.74	2.23	0.15	0.81
23.10	92.45	71.94	1.69	121.87	2.23	0.15	0.81
23.17	94.15	73.07	1.71	124.61	2.23	0.16	0.82
23.24	94.15	72.76	1.76	127.88	2.25	0.16	0.82
23.32	92.75	71.27	1.85	132.08	2.28	0.16	0.82
23.37	92.60	70.92	1.91	135.15	2.29	0.16	0.82
23.45	92.60	70.49	2.02	142.70	2.33	0.16	0.82
23.51	92.45	70.15	2.05	144.11	2.33	0.16	0.82
23.56	93.46	70.81	2.03	144.02	2.33	0.17	0.82
23.63	97.17	73.63	1.94	143.06	2.30	0.17	0.83
23.71	101.08	76.60	1.85	141.78	2.28	0.18	0.83
23.77	107.81	81.95	1.71	139.98	2.23	0.19	0.84
23.84	112.43	85.58	1.63	139.15	2.20	0.19	0.84
23.89	116.75	88.99	1.56	138.81	2.18	0.20	0.84
23.95	119.66	91.29	1.50	137.24	2.15	0.20	0.84
24.05	122.88	93.86	1.44	134.69	2.11	0.20	0.84
24.09	123.08	93.94	1.42	133.60	2.10	0.20	0.84
24.15	122.98	93.75	1.41	132.32	2.09	0.19	0.84
24.24	120.67	91.71	1.41	129.39	2.09	0.19	0.84
24.30	118.06	89.45	1.42	126.95	2.10	0.18	0.84
24.37	113.74	85.81	1.44	123.86	2.12	0.17	0.83
24.42	111.63	84.03	1.45	121.43	2.12	0.17	0.83
24.48	110.93	83.38	1.44	119.86	2.11	0.17	0.83
24.54	110.33	82.77	1.43	118.70	2.11	0.17	0.82
24.61	106.41	79.42	1.47	116.41	2.13	0.16	0.82
24.71	96.77	71.47	1.57	112.07	2.18	0.15	0.81
24.76	88.74	64.97	1.69	109.74	2.23	0.14	0.80
24.81	80.91	58.68	1.84	108.17	2.28	0.13	0.80
24.90	69.26	49.44	2.17	107.09	2.36	0.12	0.78
24.96	62.04	43.77	2.46	107.69	2.42	0.12	0.77
25.00	55.21	38.46	2.86	110.01	2.48	0.11	0.76
25.09	46.78	31.94	3.59	114.57	2.58	0.11	0.75
25.16	42.06	28.28	4.21	119.09	2.65	0.10	0.62
25.20	38.04	25.20	4.94	124.47	2.72	0.10	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
25.30	32.42	20.94	6.35	133.05	2.84	0.10	0.62
25.36	30.51	19.60	6.95	136.17	2.88	0.09	0.62
25.40	29.91	19.16	7.16	137.28	2.90	0.09	0.62
25.48	31.52	20.18	6.61	133.36	2.86	0.09	0.62
25.53	33.42	21.46	6.04	129.56	2.81	0.10	0.62
25.59	36.03	23.33	5.34	124.47	2.76	0.10	0.62
25.67	38.84	25.30	4.83	122.27	2.71	0.10	0.62
25.75	38.54	24.97	4.97	124.10	2.72	0.10	0.62
25.80	36.94	23.74	5.34	126.78	2.76	0.10	0.62
25.87	36.99	23.66	5.48	129.79	2.77	0.10	0.62
25.95	37.04	23.54	5.78	136.00	2.79	0.10	0.62
25.99	41.15	26.41	5.12	135.18	2.74	0.10	0.62
26.09	54.31	35.76	3.70	132.19	2.59	0.11	0.76
26.14	64.75	43.37	2.90	125.80	2.49	0.12	0.78
26.19	69.06	46.48	2.67	124.03	2.45	0.13	0.78
26.27	83.02	56.89	2.05	116.63	2.33	0.14	0.80
26.33	89.65	61.80	1.87	115.76	2.29	0.15	0.81
26.39	95.27	65.88	1.77	116.88	2.26	0.15	0.81
26.45	102.09	70.85	1.68	119.22	2.23	0.16	0.82
26.53	105.21	72.97	1.65	120.61	2.22	0.17	0.82
26.59	105.81	73.26	1.65	120.74	2.21	0.17	0.82
26.64	100.69	69.23	1.73	119.91	2.24	0.16	0.82
26.73	91.95	62.43	1.91	119.47	2.30	0.15	0.81
26.79	85.43	57.41	2.10	120.72	2.34	0.14	0.80
26.86	76.09	50.32	2.47	124.26	2.42	0.13	0.79
26.93	69.77	45.57	2.78	126.74	2.47	0.13	0.78
26.99	63.04	40.62	3.19	129.75	2.53	0.12	0.77
27.08	53.50	33.68	4.00	134.73	2.63	0.11	0.62
27.13	49.08	30.49	4.54	138.48	2.68	0.11	0.62
27.17	45.77	28.12	5.03	141.34	2.73	0.11	0.62
27.25	42.66	25.88	5.52	142.78	2.77	0.10	0.62
27.32	40.05	24.05	5.88	141.39	2.80	0.10	0.62
27.38	34.13	20.24	7.05	142.78	2.89	0.10	0.62
27.44	31.31	18.45	7.36	135.75	2.91	0.09	0.62
27.53	28.90	16.89	7.32	123.65	2.91	0.09	0.62
27.58	28.20	16.43	7.41	121.67	2.91	0.09	0.62
27.63	27.80	16.15	7.53	121.53	2.92	0.09	0.62
27.71	29.21	16.96	7.22	122.49	2.90	0.09	0.62
27.77	32.12	18.71	6.53	122.17	2.85	0.09	0.62
27.82	25.69	14.73	8.95	131.86	3.01	0.09	1.05
27.90	50.39	30.94	3.60	111.33	2.58	0.11	0.75
27.97	60.63	38.03	2.81	106.74	2.47	0.11	0.76
28.02	73.18	46.90	2.19	102.67	2.36	0.12	0.78
28.12	99.79	66.19	1.56	103.38	2.18	0.14	0.81
28.17	109.42	73.25	1.46	106.63	2.12	0.15	0.82
28.23	115.25	77.44	1.41	109.52	2.10	0.16	0.82
28.31	116.15	77.91	1.41	109.71	2.09	0.16	0.82
28.37	112.74	75.25	1.43	107.81	2.11	0.16	0.82

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
28.42	106.61	70.57	1.49	105.24	2.14	0.15	0.81
28.51	95.57	62.14	1.66	103.43	2.22	0.14	0.80
28.55	87.24	55.96	1.85	103.39	2.28	0.14	0.80
28.61	78.70	49.59	2.16	106.96	2.36	0.13	0.79
28.71	65.95	40.14	3.04	122.00	2.51	0.12	0.77
28.76	57.32	34.11	3.79	129.14	2.60	0.11	0.62
28.81	49.29	28.61	4.78	136.64	2.71	0.11	0.62
28.91	36.94	20.72	6.76	140.17	2.87	0.10	0.62
28.95	35.83	20.04	6.90	138.28	2.88	0.10	0.62
29.00	35.78	19.97	6.85	136.80	2.88	0.10	0.62
29.07	35.73	19.89	6.84	136.07	2.87	0.10	0.62
29.16	39.15	21.81	6.07	132.34	2.82	0.10	0.62
29.21	43.16	24.34	5.28	128.47	2.75	0.10	0.62
29.30	49.39	28.38	4.32	122.62	2.66	0.11	0.62
29.36	51.29	29.60	4.07	120.49	2.64	0.11	0.62
29.41	57.22	33.56	3.40	114.22	2.56	0.11	0.76
29.50	69.16	41.62	2.56	106.35	2.43	0.12	0.77
29.56	75.79	46.21	2.20	101.84	2.37	0.12	0.78
29.61	82.52	50.92	1.94	98.99	2.31	0.13	0.79
29.69	86.73	54.27	1.68	91.09	2.22	0.13	0.79
29.76	83.12	51.54	1.77	91.47	2.26	0.13	0.79
29.80	76.59	46.80	1.99	92.98	2.32	0.12	0.78
29.89	64.14	38.02	2.56	97.42	2.43	0.11	0.76
29.93	54.71	31.57	3.28	103.45	2.54	0.11	0.75
30.00	46.07	25.77	4.28	110.28	2.66	0.10	0.62
30.06	34.33	18.38	6.55	120.35	2.85	0.09	0.62
30.13	31.62	16.81	7.13	119.85	2.89	0.09	0.62
30.21	28.19	14.84	8.05	119.49	2.96	0.09	0.62
30.27	24.68	12.84	9.31	119.50	3.03	0.09	0.92
30.36	23.67	12.23	9.15	111.91	3.02	0.09	0.87
30.41	23.47	12.10	8.87	107.33	3.01	0.09	0.86
30.46	22.77	11.69	8.81	103.00	3.00	0.08	0.83
30.55	21.77	11.10	8.70	96.58	3.00	0.08	0.62
30.60	21.67	11.02	8.62	94.96	2.99	0.08	0.62
30.65	21.47	10.89	8.67	94.37	2.99	0.08	0.62
30.73	21.06	10.63	8.90	94.64	3.01	0.08	0.76
30.80	20.96	10.55	8.93	94.26	3.01	0.08	0.75
30.85	20.76	10.42	8.99	93.67	3.01	0.08	0.74
30.95	20.56	10.28	9.06	93.11	3.02	0.08	0.73
30.99	20.36	10.16	9.22	93.69	3.03	0.08	0.73
31.05	20.46	10.19	9.25	94.31	3.03	0.08	0.73
31.15	20.46	10.16	9.33	94.74	3.03	0.08	0.73
31.18	20.46	10.15	9.36	94.97	3.03	0.08	0.72
31.23	20.46	10.13	9.42	95.44	3.04	0.08	0.72
31.30	20.76	10.27	9.39	96.38	3.03	0.08	0.73
31.39	20.76	10.23	9.54	97.61	3.04	0.08	0.73
31.45	20.76	10.22	9.63	98.37	3.05	0.08	0.73
31.50	20.67	10.14	9.79	99.27	3.06	0.08	0.72

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
31.58	20.67	10.12	9.83	99.40	3.06	0.08	0.72
31.64	20.67	10.10	9.83	99.29	3.06	0.08	0.72
31.70	20.67	10.08	9.88	99.53	3.06	0.08	0.72
31.78	20.47	9.94	10.15	100.90	3.08	0.08	0.71
31.84	20.27	9.82	10.36	101.71	3.09	0.08	0.70
31.90	20.07	9.69	10.77	104.34	3.11	0.08	0.69
31.96	20.57	9.94	10.70	106.35	3.10	0.08	0.71
32.03	21.17	10.23	10.63	108.74	3.10	0.08	0.73
32.09	21.17	10.21	10.61	108.35	3.10	0.08	0.73
32.19	22.58	10.92	9.51	103.86	3.04	0.08	0.78
32.24	23.48	11.38	9.00	102.38	3.01	0.08	0.81
32.32	22.09	10.61	9.67	102.68	3.05	0.08	0.76
32.39	20.09	9.54	10.93	104.23	3.12	0.08	0.68
32.43	19.59	9.27	11.30	104.74	3.13	0.08	0.66
32.48	19.49	9.20	11.26	103.53	3.13	0.08	0.66
32.55	19.79	9.33	10.73	100.11	3.11	0.08	0.67
32.62	19.79	9.31	10.37	96.52	3.09	0.08	0.67
32.69	19.39	9.08	10.50	95.39	3.09	0.08	0.65
32.78	19.39	9.05	10.53	95.33	3.10	0.08	0.65
32.82	19.39	9.04	10.54	95.33	3.10	0.08	0.65
32.88	19.59	9.13	10.31	94.16	3.08	0.08	0.65
32.97	19.99	9.31	10.28	95.67	3.08	0.08	0.66
33.02	20.19	9.39	10.30	96.77	3.08	0.08	0.67
33.08	20.69	9.63	10.13	97.64	3.08	0.08	0.69
33.17	21.50	10.02	9.75	97.70	3.05	0.08	0.72
33.21	21.80	10.16	9.63	97.83	3.05	0.08	0.73
33.29	22.50	10.49	9.66	101.37	3.05	0.08	0.75
33.37	23.40	10.92	9.53	104.13	3.04	0.08	0.78
33.41	23.30	10.86	9.71	105.43	3.05	0.08	0.78
33.47	23.50	10.94	9.76	106.79	3.06	0.08	0.78
33.56	23.50	10.91	9.93	108.26	3.06	0.08	0.78
33.61	24.31	11.30	9.63	108.76	3.05	0.09	0.81
33.68	24.11	11.17	9.85	110.07	3.06	0.08	0.80
33.77	24.91	11.54	9.71	112.13	3.05	0.09	0.82
33.82	25.21	11.67	9.68	112.96	3.05	0.09	0.83
33.87	26.51	12.31	9.16	112.71	3.02	0.09	0.88
33.97	29.63	13.83	8.15	112.67	2.96	0.09	0.62
34.01	31.23	14.62	7.69	112.39	2.93	0.09	0.62
34.08	31.43	14.68	7.71	113.16	2.93	0.09	0.62
34.13	29.33	13.61	8.32	113.30	2.97	0.09	0.62
34.19	26.11	11.98	9.67	115.89	3.05	0.09	0.86
34.27	22.40	10.11	11.54	116.71	3.15	0.08	0.72
34.36	20.59	9.19	12.21	112.15	3.18	0.08	0.66
34.41	19.39	8.58	12.84	110.13	3.20	0.08	0.61
34.46	15.37	6.58	16.65	109.64	3.35	0.08	0.47
34.54	18.58	8.15	12.92	105.27	3.21	0.08	0.58
34.60	18.38	8.03	13.03	104.67	3.21	0.08	0.57
34.65	18.38	8.02	13.07	104.80	3.21	0.08	0.57

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
34.73	18.38	8.00	13.00	104.02	3.21	0.08	0.57
34.80	18.28	7.93	12.89	102.27	3.21	0.08	0.57
34.85	18.09	7.82	12.99	101.65	3.21	0.08	0.56
34.92	17.89	7.71	13.10	100.97	3.22	0.08	0.55
34.98	18.09	7.79	12.86	100.20	3.21	0.08	0.56
35.04	17.89	7.68	13.09	100.55	3.22	0.08	0.55
35.12	18.09	7.76	12.92	100.20	3.21	0.08	0.55
35.17	18.39	7.89	12.65	99.78	3.20	0.08	0.56
35.25	18.39	7.87	12.61	99.28	3.19	0.08	0.56
35.32	18.59	7.95	12.58	99.97	3.19	0.08	0.57
35.37	18.69	7.98	12.70	101.35	3.20	0.08	0.57
35.44	19.20	8.21	12.61	103.56	3.19	0.08	0.59
35.50	20.60	8.87	11.85	105.09	3.16	0.08	0.63
35.60	23.61	10.28	10.50	107.93	3.09	0.08	0.73
35.65	24.62	10.74	10.15	109.04	3.08	0.08	0.77
35.70	26.22	11.49	9.52	109.30	3.04	0.09	0.82
35.79	28.03	12.32	8.88	109.41	3.01	0.09	0.88
35.85	27.83	12.20	8.98	109.60	3.01	0.09	0.87
35.90	26.73	11.66	9.31	108.54	3.03	0.09	0.83
35.98	24.52	10.59	10.29	108.96	3.08	0.08	0.76
36.03	24.01	10.33	10.51	108.54	3.09	0.08	0.74
36.09	24.57	10.57	10.24	108.32	3.08	0.08	0.76
36.18	23.21	9.91	11.02	109.14	3.12	0.08	0.71
36.24	24.62	10.55	10.26	108.19	3.08	0.08	0.75
36.29	25.62	11.00	9.84	108.28	3.06	0.09	0.79
36.38	30.74	13.37	8.23	110.01	2.97	0.09	0.62
36.44	33.95	14.84	7.50	111.29	2.92	0.09	0.62
36.49	35.56	15.57	7.21	112.19	2.90	0.09	0.62
36.57	33.15	14.41	7.88	113.50	2.94	0.09	0.62
36.63	29.84	12.85	9.02	115.95	3.01	0.09	0.92
36.69	27.53	11.76	9.97	117.21	3.07	0.09	0.84
36.77	25.92	10.98	10.20	111.95	3.08	0.09	0.78
36.83	24.92	10.50	10.45	109.72	3.09	0.08	0.75
36.88	23.41	9.79	11.01	107.78	3.12	0.08	0.70
36.96	22.71	9.44	11.34	107.12	3.14	0.08	0.67
37.03	22.51	9.33	11.53	107.64	3.15	0.08	0.67
37.08	27.33	11.53	9.05	104.30	3.02	0.09	0.82
37.14	36.56	15.73	6.32	99.47	2.84	0.09	0.62
37.23	54.64	24.95	3.72	92.91	2.60	0.10	0.74
37.28	61.16	28.42	3.31	93.97	2.55	0.11	0.75
37.36	56.34	25.41	4.04	102.67	2.63	0.11	0.62
37.41	48.31	20.94	5.31	111.15	2.75	0.10	0.62
37.48	41.07	17.63	6.61	116.50	2.86	0.10	0.62
37.57	32.84	13.86	8.57	118.72	2.99	0.09	0.62
37.63	28.12	11.70	10.13	118.51	3.07	0.09	0.84
37.66	26.21	10.83	10.84	117.31	3.11	0.09	0.77
37.77	23.30	9.48	11.73	111.23	3.15	0.08	0.68
37.82	22.30	9.02	11.91	107.38	3.16	0.08	0.64

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
37.88	21.90	8.83	11.76	103.78	3.16	0.08	0.63
37.96	22.00	8.85	11.23	99.34	3.13	0.08	0.63
38.01	22.60	9.11	10.67	97.19	3.10	0.08	0.65
38.06	22.50	9.05	10.50	95.04	3.09	0.08	0.65
38.13	22.90	9.21	9.53	87.70	3.04	0.08	0.66
38.19	23.40	9.41	9.17	86.35	3.02	0.08	0.67
38.26	23.60	9.49	9.51	90.21	3.04	0.08	0.68
38.32	23.31	9.33	9.61	89.73	3.05	0.08	0.67
38.41	22.61	9.00	10.31	92.86	3.08	0.08	0.64
38.46	19.60	7.66	12.76	97.76	3.20	0.08	0.55
38.52	24.82	9.95	9.92	98.73	3.06	0.08	0.71
38.59	25.72	10.33	10.06	103.83	3.07	0.08	0.74
38.65	26.83	10.80	10.02	108.18	3.07	0.09	0.77
38.73	30.04	12.18	9.19	111.98	3.02	0.09	0.87
38.79	33.95	13.87	8.01	111.20	2.95	0.09	0.62
38.86	42.79	17.71	6.12	108.39	2.82	0.10	0.62
38.92	51.32	21.49	4.91	105.62	2.72	0.10	0.62
38.98	59.96	25.92	4.01	103.91	2.63	0.11	0.62
39.06	72.71	32.59	3.12	101.77	2.52	0.12	0.77
39.12	81.14	37.08	2.73	101.11	2.46	0.12	0.78
39.18	89.98	41.94	2.38	99.78	2.40	0.13	0.79
39.28	106.24	50.94	1.96	99.99	2.31	0.15	0.81
39.32	110.56	53.30	1.89	100.88	2.29	0.15	0.81
39.37	119.29	58.13	1.77	102.95	2.26	0.16	0.82
39.48	132.55	65.31	1.66	108.26	2.22	0.18	0.84
39.52	135.05	66.48	1.66	110.31	2.22	0.19	0.84
39.57	138.77	68.27	1.66	113.07	2.22	0.20	0.84
39.66	143.59	71.63	1.53	109.88	2.17	0.20	0.84
39.70	144.79	73.20	1.45	105.90	2.12	0.19	0.84
39.77	148.71	74.60	1.48	110.66	2.14	0.20	0.85
39.87	152.72	76.35	1.49	114.04	2.14	0.22	0.85
39.92	156.74	78.40	1.49	116.44	2.14	0.23	0.86
39.98	161.86	81.15	1.47	118.96	2.13	0.24	0.86
40.06	119.99	55.61	2.19	121.76	2.36	0.18	0.83
40.12	171.18	85.48	1.47	126.01	2.13	0.28	0.87
40.16	175.99	88.00	1.46	128.65	2.13	0.30	0.88
40.25	182.11	90.86	1.47	133.17	2.13	0.34	0.88
40.31	182.30	90.44	1.49	134.69	2.14	0.35	0.89
40.37	181.40	89.62	1.51	135.06	2.15	0.35	0.89
40.44	178.39	87.59	1.53	134.37	2.17	0.34	0.88
40.50	175.48	85.72	1.56	133.47	2.18	0.32	0.88
40.56	172.97	84.16	1.57	132.47	2.18	0.31	0.88
40.63	169.15	81.87	1.60	130.89	2.19	0.30	0.88
40.71	166.94	80.59	1.60	129.08	2.19	0.28	0.87
40.77	163.53	78.56	1.63	127.74	2.20	0.27	0.87
40.86	159.61	76.18	1.66	126.39	2.22	0.26	0.87
40.90	156.50	74.33	1.69	125.64	2.23	0.25	0.86
40.96	152.79	72.16	1.72	124.39	2.24	0.24	0.86

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
41.03	146.66	68.63	1.79	122.86	2.26	0.22	0.85
41.09	142.95	66.50	1.83	121.75	2.27	0.22	0.85
41.15	139.23	64.38	1.88	120.92	2.29	0.21	0.85
41.24	134.91	62.10	1.90	117.79	2.29	0.20	0.84
41.28	131.60	60.25	1.94	117.01	2.30	0.19	0.84
41.35	129.19	58.89	1.97	116.02	2.31	0.19	0.83
41.41	124.99	56.54	2.04	115.17	2.33	0.18	0.83
41.50	122.48	55.11	2.07	114.17	2.34	0.17	0.83
41.55	119.87	53.66	2.12	113.77	2.35	0.17	0.82
41.61	116.86	52.02	2.17	112.81	2.36	0.17	0.82
41.71	114.25	50.60	2.20	111.29	2.36	0.16	0.82
41.75	112.95	49.86	2.23	110.96	2.37	0.16	0.82
41.80	111.44	49.00	2.26	110.89	2.38	0.16	0.81
41.87	109.94	48.11	2.30	110.76	2.39	0.16	0.81
41.93	108.23	47.12	2.36	111.01	2.40	0.15	0.81
42.00	105.32	45.47	2.45	111.40	2.41	0.15	0.81
42.09	102.51	43.91	2.54	111.46	2.43	0.15	0.80
42.14	100.60	42.81	2.60	111.44	2.44	0.15	0.80
42.20	99.09	41.98	2.65	111.39	2.45	0.14	0.80
42.29	96.98	40.81	2.72	111.12	2.46	0.14	0.80
42.34	96.18	40.35	2.75	110.99	2.47	0.14	0.80
42.39	95.28	39.83	2.79	111.14	2.47	0.14	0.79
42.48	94.47	39.32	2.83	111.23	2.48	0.14	0.79
42.54	94.37	39.20	2.83	110.92	2.48	0.14	0.79
42.59	94.57	39.29	2.80	110.06	2.47	0.14	0.79
42.68	95.47	39.80	2.70	107.49	2.46	0.14	0.79
42.73	95.87	39.95	2.68	107.14	2.45	0.14	0.79
42.79	96.16	40.01	2.69	107.54	2.46	0.14	0.79
42.88	94.55	39.10	2.74	107.28	2.46	0.14	0.79
42.93	92.84	38.10	2.86	108.93	2.48	0.14	0.79
42.99	90.33	36.68	3.03	111.01	2.51	0.13	0.79
43.06	89.11	36.04	3.07	110.51	2.51	0.13	0.79
43.14	87.40	35.41	2.98	105.37	2.50	0.13	0.78
43.18	85.19	34.41	3.00	103.13	2.50	0.13	0.78
43.28	79.26	31.44	3.28	103.14	2.54	0.12	0.77
43.33	73.93	28.78	3.64	104.85	2.59	0.12	0.77
43.42	65.90	24.80	4.38	108.69	2.67	0.11	0.62
43.44	63.39	23.61	4.62	109.06	2.69	0.11	0.62
43.53	57.16	21.10	5.07	106.94	2.73	0.11	0.62
43.58	55.15	20.30	5.16	104.75	2.74	0.10	0.62
43.67	48.42	17.66	6.05	106.86	2.82	0.10	0.62
43.73	46.01	16.71	6.40	106.99	2.84	0.10	0.62
43.78	44.61	16.15	6.60	106.59	2.86	0.10	0.62
43.86	45.96	16.63	6.27	104.21	2.83	0.10	0.62
43.92	45.51	16.43	6.24	102.55	2.83	0.10	0.62
43.97	45.91	16.57	5.90	97.69	2.80	0.10	0.62
44.06	45.81	16.49	5.22	86.16	2.75	0.10	0.62
44.12	43.50	15.59	5.69	88.70	2.79	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
44.17	39.19	13.93	6.69	93.22	2.86	0.09	0.62
44.26	32.16	11.23	8.43	94.63	2.98	0.09	0.62
44.30	28.45	9.80	9.73	95.36	3.05	0.09	0.70
44.37	23.53	7.92	12.17	96.43	3.18	0.08	0.57
44.44	20.72	6.85	14.53	99.48	3.27	0.08	0.49
44.50	21.43	7.10	13.98	99.33	3.25	0.08	0.51
44.59	20.33	6.67	14.85	99.02	3.29	0.08	0.48
44.64	20.43	6.70	14.75	98.87	3.28	0.08	0.48
44.73	22.34	7.40	13.13	97.26	3.22	0.08	0.53
44.77	23.74	7.92	12.10	95.90	3.17	0.08	0.57
44.83	24.65	8.25	11.48	94.72	3.14	0.08	0.59
44.88	26.35	8.88	10.51	93.32	3.09	0.08	0.63
44.96	27.66	9.35	9.78	91.47	3.06	0.08	0.67
45.03	26.15	8.77	10.76	94.42	3.11	0.08	0.63
45.08	25.05	8.35	11.67	97.46	3.15	0.08	0.60
45.17	26.15	8.74	11.26	98.45	3.13	0.08	0.62
45.22	25.15	8.36	11.70	97.82	3.15	0.08	0.60
45.28	26.15	8.72	10.82	94.36	3.11	0.08	0.62
45.36	25.15	8.33	9.97	83.11	3.07	0.08	0.60
45.41	23.14	7.58	10.71	81.17	3.10	0.08	0.54
45.48	21.33	6.90	12.05	83.11	3.17	0.08	0.49
45.54	20.23	6.48	13.81	89.46	3.25	0.08	0.46
45.63	19.83	6.32	15.15	95.68	3.30	0.08	0.45
45.67	20.33	6.49	15.29	99.29	3.30	0.08	0.46
45.74	30.97	10.40	9.93	103.22	3.06	0.09	0.74
45.83	65.52	23.56	3.93	92.69	2.62	0.11	0.62
45.88	92.92	36.62	2.37	86.70	2.40	0.13	0.78
45.97	112.09	45.57	2.01	91.38	2.32	0.15	0.81
46.03	116.71	47.29	2.04	96.38	2.33	0.15	0.81
46.07	121.93	49.41	2.04	100.60	2.33	0.16	0.82
46.17	131.37	53.46	1.98	105.93	2.31	0.18	0.83
46.22	136.49	55.80	1.93	107.64	2.30	0.19	0.84
46.27	142.11	58.40	1.87	109.37	2.29	0.20	0.84
46.36	149.14	61.62	1.81	111.54	2.27	0.21	0.85
46.41	154.16	64.12	1.75	111.96	2.25	0.22	0.85
46.49	164.80	69.64	1.62	112.93	2.20	0.24	0.86
46.54	175.75	75.37	1.53	115.17	2.16	0.27	0.87
46.62	193.62	85.06	1.41	120.11	2.10	0.33	0.88
46.66	199.73	88.46	1.38	122.22	2.07	0.35	0.88
46.73	215.70	97.59	1.32	128.64	2.01	0.41	0.89
46.82	223.21	101.99	1.29	131.91	1.98	0.44	0.89
46.85	223.42	102.18	1.29	131.82	1.98	0.44	0.89
46.92	218.99	99.68	1.30	129.20	1.99	0.40	0.89
47.01	210.36	94.55	1.32	124.74	2.01	0.37	0.88
47.06	202.83	90.09	1.35	121.27	2.04	0.34	0.88
47.15	191.79	83.53	1.40	117.02	2.09	0.31	0.88
47.21	187.27	80.49	1.45	116.56	2.12	0.30	0.88
47.25	186.27	79.93	1.45	115.98	2.12	0.30	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
47.31	187.87	82.26	1.37	112.70	2.06	0.27	0.87
47.41	204.54	91.58	1.31	119.82	2.00	0.31	0.87
47.46	214.18	96.73	1.29	124.70	1.98	0.35	0.88
47.54	226.23	103.13	1.27	130.95	1.95	0.41	0.88
47.58	214.88	96.22	1.30	125.24	1.99	0.37	0.88
47.67	232.45	105.82	1.27	134.18	1.95	0.46	0.89
47.71	235.87	107.68	1.26	135.89	1.94	0.48	0.89
47.77	245.30	113.18	1.24	140.58	1.91	0.53	0.88
47.85	252.84	117.42	1.23	144.25	1.89	0.58	0.88
47.92	254.95	118.52	1.22	145.08	1.88	0.59	0.88
47.97	254.36	118.06	1.23	144.64	1.88	0.58	0.88
48.06	251.65	116.11	1.23	143.12	1.89	0.57	0.88
48.12	249.45	114.56	1.24	141.88	1.90	0.56	0.89
48.17	246.14	112.37	1.25	140.12	1.92	0.55	0.89
48.25	241.12	109.10	1.26	137.38	1.93	0.52	0.89
48.31	237.91	107.02	1.27	135.59	1.95	0.51	0.89
48.36	235.40	105.40	1.27	134.20	1.95	0.49	0.89
48.45	234.00	104.62	1.27	133.15	1.95	0.48	0.89
48.50	233.09	104.19	1.27	132.44	1.95	0.46	0.89
48.57	234.00	104.67	1.27	132.68	1.95	0.46	0.89
48.63	233.29	104.31	1.27	132.05	1.94	0.44	0.88
48.72	234.00	104.77	1.26	132.10	1.94	0.44	0.88
48.77	235.10	105.49	1.26	132.43	1.93	0.43	0.88
48.85	238.92	107.85	1.24	134.02	1.91	0.43	0.88
48.91	242.93	110.31	1.23	135.78	1.89	0.44	0.87
48.97	246.85	112.45	1.22	137.60	1.88	0.46	0.87
49.05	253.58	116.22	1.21	140.57	1.86	0.49	0.87
49.11	257.09	118.30	1.20	141.92	1.85	0.50	0.87
49.16	258.89	119.42	1.19	142.40	1.84	0.50	0.86
49.21	258.79	119.63	1.19	141.80	1.83	0.48	0.86
49.28	255.97	118.57	1.18	139.55	1.82	0.43	0.85
49.35	249.45	114.72	1.19	136.54	1.84	0.40	0.85
49.42	233.79	105.47	1.22	129.12	1.88	0.34	0.86
49.48	220.33	97.91	1.25	122.08	1.92	0.30	0.86
49.54	207.28	90.11	1.28	115.45	1.97	0.28	0.86
49.61	193.23	82.84	1.30	107.97	2.00	0.24	0.85
49.68	187.50	79.01	1.34	105.77	2.03	0.24	0.86
49.76	182.48	76.92	1.33	102.53	2.03	0.22	0.85
49.81	180.38	75.47	1.35	101.79	2.04	0.22	0.85
49.88	179.97	74.51	1.38	102.47	2.07	0.23	0.86
49.95	179.57	73.57	1.41	103.38	2.09	0.24	0.86
50.02	179.92	73.12	1.43	104.51	2.11	0.24	0.86
50.10	179.92	72.53	1.46	105.60	2.12	0.25	0.86
50.15	180.27	72.38	1.47	106.32	2.13	0.26	0.87
50.20	183.88	74.05	1.45	107.58	2.12	0.27	0.87
50.28	185.99	74.70	1.46	108.88	2.12	0.28	0.87
50.34	187.89	75.34	1.46	109.99	2.13	0.29	0.87
50.44	190.71	76.28	1.46	111.55	2.13	0.30	0.88

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
50.47	191.91	76.77	1.46	112.05	2.13	0.31	0.88
50.54	192.61	76.87	1.46	112.54	2.13	0.31	0.88
50.59	192.41	76.60	1.47	112.59	2.13	0.31	0.88
50.69	191.11	75.65	1.49	112.39	2.14	0.31	0.88
50.73	190.51	75.27	1.49	112.19	2.14	0.31	0.88
50.84	188.60	74.25	1.50	111.05	2.15	0.30	0.88
50.86	188.00	73.94	1.50	110.76	2.15	0.29	0.88
50.93	186.09	72.91	1.51	109.99	2.15	0.29	0.87
50.99	184.38	71.96	1.52	109.44	2.16	0.28	0.87
51.05	182.07	70.70	1.54	108.74	2.17	0.27	0.87
51.13	181.67	70.42	1.54	108.39	2.17	0.27	0.87
51.20	181.97	70.52	1.53	108.11	2.16	0.27	0.87
51.25	181.77	70.35	1.53	107.90	2.16	0.27	0.87
51.34	181.87	70.25	1.53	107.79	2.17	0.27	0.87
51.38	181.97	70.22	1.53	107.74	2.17	0.27	0.87
51.48	183.58	70.87	1.52	107.96	2.16	0.28	0.87
51.53	185.08	71.53	1.51	108.20	2.15	0.28	0.87
51.58	186.19	72.03	1.50	108.31	2.15	0.28	0.87
51.67	187.69	72.79	1.48	108.03	2.14	0.28	0.87
51.72	187.39	72.62	1.48	107.67	2.14	0.28	0.87
51.78	186.99	72.34	1.48	107.40	2.14	0.28	0.87
51.86	185.59	71.45	1.50	107.09	2.15	0.28	0.87
51.93	185.08	71.03	1.51	107.03	2.15	0.28	0.87
51.97	184.68	70.70	1.51	107.02	2.16	0.27	0.87
52.06	185.79	71.02	1.51	107.47	2.15	0.28	0.87
52.11	186.99	71.47	1.51	107.85	2.15	0.28	0.87
52.17	187.79	71.68	1.51	108.25	2.15	0.29	0.87
52.24	189.60	72.35	1.50	108.85	2.15	0.29	0.88
52.31	190.51	72.63	1.50	109.18	2.15	0.30	0.88
52.37	189.70	72.17	1.51	108.71	2.15	0.29	0.88
52.47	186.09	70.39	1.52	107.18	2.16	0.28	0.87
52.52	182.07	68.39	1.55	106.01	2.17	0.27	0.87
52.57	180.06	67.45	1.56	105.14	2.18	0.26	0.87
52.67	171.73	63.56	1.61	102.34	2.20	0.24	0.86
52.72	166.71	61.27	1.64	100.65	2.21	0.22	0.86
52.77	161.29	58.76	1.69	99.21	2.23	0.21	0.85
52.86	153.76	55.26	1.77	97.55	2.25	0.20	0.84
52.91	149.04	53.06	1.83	96.90	2.27	0.19	0.84
52.96	144.82	51.15	1.88	96.23	2.29	0.18	0.83
53.02	140.51	49.20	1.95	95.78	2.31	0.18	0.83
53.10	134.28	46.32	2.07	96.00	2.34	0.17	0.82
53.16	130.37	44.53	2.16	96.24	2.36	0.17	0.82
53.24	125.65	42.42	2.27	96.43	2.38	0.16	0.82
53.30	122.64	41.30	2.29	94.42	2.38	0.16	0.81
53.36	118.92	39.80	2.34	93.25	2.39	0.15	0.81
53.42	117.01	38.77	2.44	94.48	2.41	0.15	0.81
53.48	115.71	38.10	2.51	95.50	2.42	0.15	0.81
53.56	115.91	38.05	2.54	96.49	2.43	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
53.61	115.31	37.70	2.58	97.32	2.44	0.15	0.81
53.69	120.63	40.06	2.40	96.01	2.40	0.15	0.81
53.75	126.75	42.87	2.19	93.83	2.36	0.16	0.82
53.82	130.37	44.62	2.06	91.94	2.33	0.16	0.82
53.88	131.17	45.08	2.02	90.90	2.32	0.16	0.82
53.97	130.07	44.79	1.99	88.95	2.32	0.16	0.82
54.02	129.16	44.54	1.96	87.48	2.31	0.16	0.82
54.09	123.94	42.34	2.04	86.18	2.33	0.15	0.81
54.14	119.22	40.26	2.14	86.06	2.35	0.15	0.81
54.21	114.50	38.19	2.25	86.06	2.38	0.14	0.80
54.28	107.38	34.94	2.51	87.71	2.43	0.14	0.79
54.33	103.46	33.20	2.68	89.01	2.45	0.13	0.79
54.43	101.75	32.41	2.77	89.68	2.47	0.13	0.79
54.48	101.95	32.46	2.76	89.74	2.47	0.13	0.79
54.53	102.86	32.85	2.72	89.22	2.46	0.13	0.79
54.62	102.76	32.86	2.68	88.01	2.45	0.13	0.79
54.67	101.75	32.50	2.68	87.15	2.45	0.13	0.79
54.73	101.15	32.33	2.66	85.99	2.45	0.13	0.79
54.82	98.54	31.36	2.70	84.62	2.46	0.13	0.78
54.87	96.83	30.71	2.73	83.84	2.46	0.13	0.78
54.95	94.73	29.97	2.74	82.17	2.46	0.12	0.78
55.01	93.52	29.48	2.78	81.94	2.47	0.12	0.78
55.06	91.11	28.47	2.89	82.25	2.49	0.12	0.77
55.12	88.50	27.41	3.00	82.34	2.50	0.12	0.77
55.20	85.89	26.34	3.14	82.63	2.52	0.12	0.77
55.26	84.59	25.80	3.21	82.76	2.53	0.12	0.77
55.32	83.28	25.26	3.28	82.89	2.54	0.12	0.76
55.41	83.28	25.25	3.27	82.68	2.54	0.12	0.76
55.47	85.19	26.01	3.15	82.02	2.52	0.12	0.77
55.51	88.20	27.22	2.99	81.35	2.50	0.12	0.77
55.59	96.23	30.54	2.60	79.43	2.44	0.12	0.78
55.67	110.69	36.84	2.09	77.09	2.34	0.13	0.79
55.72	122.74	42.27	1.81	76.55	2.27	0.14	0.80
55.81	138.40	49.35	1.59	78.69	2.19	0.15	0.82
55.86	145.33	52.50	1.53	80.36	2.16	0.16	0.82
55.92	150.75	54.83	1.50	82.25	2.15	0.17	0.83
56.01	159.08	58.18	1.48	85.95	2.14	0.18	0.83
56.06	163.80	60.14	1.46	87.94	2.13	0.19	0.84
56.11	168.62	62.19	1.45	89.87	2.12	0.20	0.84
56.21	181.07	67.87	1.39	94.43	2.08	0.22	0.85
56.25	191.51	73.01	1.35	98.34	2.04	0.23	0.86
56.31	203.05	78.95	1.31	103.06	2.00	0.25	0.86
56.38	216.71	87.68	1.24	108.82	1.91	0.24	0.84
56.44	224.14	91.02	1.24	112.45	1.90	0.26	0.84
56.50	231.67	94.58	1.23	116.04	1.89	0.28	0.85
56.58	241.41	99.33	1.21	120.57	1.87	0.31	0.85
56.65	246.12	101.30	1.21	122.84	1.87	0.33	0.85
56.73	236.78	95.30	1.25	118.77	1.91	0.34	0.86

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
56.76	242.80	98.14	1.24	121.68	1.90	0.37	0.87
56.84	244.11	98.33	1.24	122.34	1.91	0.39	0.87
56.92	241.60	96.45	1.26	121.17	1.93	0.40	0.88
56.98	239.49	95.01	1.26	120.17	1.94	0.40	0.88
57.02	236.78	93.45	1.27	118.86	1.95	0.39	0.88
57.12	234.17	91.85	1.28	117.58	1.96	0.39	0.88
57.17	234.17	91.71	1.28	117.54	1.97	0.39	0.88
57.23	234.17	91.59	1.28	117.51	1.97	0.39	0.88
57.32	234.17	91.27	1.29	117.49	1.97	0.40	0.88
57.36	234.47	91.29	1.29	117.62	1.98	0.41	0.88
57.42	235.47	91.60	1.29	118.08	1.98	0.42	0.89
57.50	237.18	92.25	1.29	118.82	1.98	0.43	0.89
57.55	240.69	93.95	1.28	120.41	1.97	0.45	0.89
57.62	245.91	96.41	1.27	122.84	1.96	0.49	0.89
57.69	254.05	100.53	1.26	126.61	1.93	0.53	0.89
57.77	262.58	104.81	1.25	130.58	1.91	0.60	0.89
57.83	267.29	107.11	1.24	132.76	1.90	0.64	0.89
57.91	271.61	109.19	1.23	134.70	1.90	0.70	0.89
57.97	273.92	110.26	1.23	135.73	1.89	0.73	0.89
58.01	274.92	110.60	1.23	136.18	1.89	0.75	0.89
58.11	278.22	112.01	1.23	137.65	1.89	0.81	0.90
58.16	282.64	114.24	1.22	139.62	1.88	0.85	0.89
58.22	289.97	118.06	1.21	142.81	1.86	0.85	0.89
58.31	301.11	124.17	1.18	147.09	1.83	0.86	0.89
58.36	307.44	127.69	1.17	149.20	1.81	0.86	0.89
58.41	313.26	130.94	1.15	150.88	1.80	0.87	0.89
58.51	318.78	133.99	1.13	152.08	1.78	0.87	0.90
58.55	320.68	135.01	1.13	152.51	1.78	0.87	0.90
58.60	320.98	135.10	1.13	152.53	1.78	0.87	0.90
58.67	318.47	133.52	1.14	151.96	1.79	0.87	0.90
58.76	314.36	130.98	1.15	150.92	1.80	0.87	0.89
58.80	312.75	130.02	1.16	150.41	1.80	0.86	0.89
58.88	307.13	126.75	1.17	148.54	1.82	0.86	0.89
58.94	303.81	124.58	1.18	147.52	1.83	0.86	0.89
59.01	301.81	123.02	1.19	146.96	1.84	0.86	0.90
59.06	301.00	122.42	1.20	146.64	1.85	0.86	0.90
59.15	300.80	122.48	1.19	146.23	1.84	0.86	0.89
59.20	300.00	122.12	1.19	145.76	1.84	0.86	0.89
59.25	297.99	121.02	1.20	144.84	1.85	0.85	0.89
59.34	290.26	116.45	1.22	141.63	1.87	0.85	0.90
59.40	286.04	114.72	1.22	139.45	1.87	0.85	0.89
59.45	283.13	114.61	1.20	137.32	1.85	0.68	0.88
59.54	279.61	112.10	1.21	136.03	1.87	0.69	0.88
59.60	278.50	111.32	1.22	135.53	1.87	0.70	0.89
59.65	278.60	111.06	1.22	135.60	1.88	0.73	0.89
59.74	255.71	99.04	1.26	124.93	1.94	0.54	0.89
59.78	261.34	102.41	1.24	127.39	1.91	0.54	0.89
59.87	285.73	115.85	1.19	137.60	1.83	0.67	0.87

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
59.94	291.15	118.42	1.18	139.78	1.83	0.75	0.88
59.99	291.96	118.54	1.18	140.26	1.83	0.80	0.88
60.05	294.07	119.12	1.19	141.41	1.83	0.85	0.88
60.14	287.14	114.73	1.21	138.85	1.86	0.85	0.89
60.19	293.21	117.78	1.20	141.39	1.85	0.85	0.89
60.24	287.94	114.94	1.21	139.11	1.86	0.85	0.89
60.34	292.36	117.02	1.20	140.93	1.85	0.85	0.89
60.38	292.86	116.99	1.21	141.21	1.86	0.85	0.89
60.44	291.36	115.82	1.21	140.65	1.87	0.85	0.90
60.53	288.23	113.70	1.23	139.30	1.88	0.85	0.90
60.58	285.32	111.94	1.23	137.98	1.89	0.84	0.90
60.63	283.41	110.71	1.24	137.08	1.90	0.84	0.90
60.71	280.90	109.21	1.24	135.84	1.91	0.84	0.91
60.78	281.41	109.31	1.24	136.00	1.91	0.84	0.91
60.83	281.61	109.38	1.24	136.02	1.91	0.84	0.91
60.91	279.60	108.39	1.25	134.96	1.91	0.84	0.91
60.97	276.59	106.90	1.25	133.46	1.92	0.84	0.90
61.03	276.64	106.75	1.25	133.44	1.92	0.84	0.91
61.10	276.69	106.70	1.25	133.37	1.92	0.84	0.91
61.16	279.50	108.19	1.24	134.56	1.91	0.84	0.90
61.23	286.43	111.62	1.23	137.67	1.89	0.84	0.90
61.32	290.24	113.52	1.23	139.26	1.89	0.85	0.90
61.38	290.94	113.68	1.23	139.54	1.89	0.85	0.90
61.43	291.04	113.44	1.23	139.59	1.89	0.85	0.91
61.52	292.95	114.28	1.23	140.33	1.89	0.85	0.91
61.56	294.86	115.32	1.22	141.11	1.88	0.85	0.91
61.62	296.06	115.90	1.22	141.55	1.88	0.85	0.90
61.71	293.75	114.57	1.23	140.41	1.88	0.85	0.91
61.77	290.95	113.02	1.23	139.08	1.89	0.84	0.91
61.84	290.24	112.70	1.23	138.65	1.89	0.84	0.90
61.92	290.25	112.98	1.23	138.43	1.88	0.84	0.90
61.94	290.24	113.03	1.22	138.37	1.88	0.84	0.90
62.02	290.25	113.12	1.22	138.20	1.88	0.84	0.90
62.12	289.95	112.84	1.22	137.96	1.88	0.84	0.90
62.15	289.24	112.48	1.22	137.60	1.88	0.84	0.90
62.22	286.54	111.08	1.23	136.28	1.89	0.84	0.90
62.27	283.41	109.46	1.23	134.80	1.89	0.84	0.90
62.36	277.40	106.46	1.24	131.92	1.90	0.78	0.90
62.41	275.58	105.52	1.24	131.02	1.91	0.76	0.90
62.48	274.99	105.24	1.24	130.64	1.91	0.74	0.90
62.55	275.39	105.55	1.24	130.70	1.90	0.72	0.89
62.61	278.60	107.22	1.23	132.05	1.89	0.74	0.89
62.69	281.21	108.63	1.22	133.07	1.88	0.75	0.89
62.74	282.62	109.43	1.22	133.60	1.88	0.75	0.89
62.81	283.52	109.73	1.22	133.93	1.88	0.77	0.89
62.87	284.63	110.18	1.22	134.35	1.87	0.79	0.89
62.95	285.23	110.40	1.22	134.52	1.87	0.79	0.89
63.00	284.03	109.65	1.22	133.96	1.88	0.79	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
63.10	277.80	106.17	1.23	131.11	1.90	0.74	0.89
63.13	272.78	103.54	1.24	128.82	1.91	0.70	0.90
63.19	277.75	106.05	1.24	130.99	1.90	0.74	0.89
63.26	273.89	104.12	1.24	129.14	1.91	0.69	0.89
63.32	277.70	106.28	1.23	130.70	1.89	0.70	0.89
63.39	279.71	107.61	1.22	131.40	1.88	0.68	0.89
63.49	278.70	107.31	1.22	130.72	1.87	0.64	0.88
63.52	277.50	106.93	1.22	130.07	1.87	0.61	0.88
63.60	274.99	106.27	1.21	128.62	1.86	0.53	0.87
63.69	270.37	104.30	1.21	126.36	1.86	0.48	0.87
63.74	266.46	102.21	1.22	124.64	1.87	0.46	0.87
63.79	266.31	102.06	1.22	124.52	1.88	0.46	0.87
63.85	266.31	102.09	1.22	124.43	1.87	0.46	0.87
63.92	266.16	102.40	1.21	124.10	1.86	0.43	0.86
63.99	270.37	105.14	1.19	125.39	1.84	0.42	0.86
64.05	273.58	107.26	1.18	126.11	1.82	0.42	0.85
64.13	277.70	110.30	1.14	126.21	1.79	0.42	0.85
64.18	279.71	113.34	1.08	122.58	1.75	0.41	0.85
64.24	281.01	118.10	1.00	118.10	1.67	0.42	0.85
64.34	278.10	116.00	1.00	116.00	1.68	0.39	0.85
64.39	276.50	114.66	1.00	114.66	1.69	0.38	0.85
64.45	277.90	114.55	1.00	114.55	1.71	0.39	0.85
64.51	271.18	109.51	1.08	118.52	1.75	0.35	0.84
64.59	274.99	110.20	1.11	121.99	1.76	0.38	0.84
64.64	279.51	111.82	1.11	124.30	1.77	0.41	0.85
64.73	282.02	111.92	1.13	126.85	1.78	0.45	0.85
64.78	283.12	111.77	1.15	128.12	1.79	0.47	0.85
64.83	285.53	112.04	1.16	129.98	1.81	0.51	0.86
64.93	287.34	111.63	1.18	131.75	1.83	0.58	0.87
64.98	288.95	111.92	1.19	132.68	1.83	0.63	0.87
65.03	289.65	111.79	1.19	133.19	1.84	0.68	0.88
65.12	292.16	112.35	1.20	134.47	1.85	0.76	0.88
65.17	294.87	113.28	1.20	135.70	1.85	0.83	0.89
65.23	299.19	115.12	1.19	137.53	1.84	0.85	0.89
65.31	304.81	117.62	1.19	139.79	1.84	0.85	0.89
65.36	307.12	118.79	1.18	140.53	1.83	0.85	0.89
65.42	308.32	119.42	1.18	140.83	1.83	0.85	0.89
65.50	307.62	119.45	1.17	140.06	1.82	0.85	0.89
65.58	305.71	118.88	1.17	138.81	1.81	0.85	0.88
65.63	306.72	119.73	1.16	138.65	1.80	0.85	0.88
65.72	311.13	123.26	1.12	137.69	1.77	0.86	0.88
65.77	313.04	124.96	1.09	136.45	1.75	0.86	0.88
65.83	316.45	127.71	1.05	134.02	1.73	0.86	0.89
65.92	314.75	126.84	1.05	133.44	1.73	0.86	0.88
65.97	313.54	125.98	1.06	133.77	1.74	0.86	0.88
66.02	314.04	126.05	1.06	134.13	1.74	0.86	0.88
66.11	317.56	127.79	1.05	134.41	1.73	0.86	0.89
66.16	322.18	130.41	1.03	133.78	1.72	0.87	0.89

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
66.22	325.69	132.30	1.01	133.35	1.71	0.87	0.89
66.30	329.31	133.76	1.01	134.49	1.71	0.87	0.90
66.35	331.01	134.36	1.01	135.33	1.71	0.87	0.90
66.42	331.21	134.87	1.00	134.87	1.70	0.87	0.90
66.50	330.11	136.18	1.00	136.18	1.67	0.87	0.90
66.55	329.51	137.12	1.00	137.12	1.65	0.87	0.90
66.61	329.91	138.78	1.00	138.78	1.63	0.87	0.90
66.70	325.99	137.21	1.00	137.21	1.63	0.87	0.89
66.76	321.07	133.94	1.00	133.94	1.64	0.87	0.89
66.80	315.35	131.07	1.00	131.07	1.65	0.87	0.88
66.88	303.40	126.14	1.00	126.14	1.65	0.70	0.87
66.96	288.44	119.86	1.00	119.86	1.64	0.47	0.85
67.01	276.50	114.07	1.00	114.07	1.66	0.36	0.84
67.06	260.53	105.76	1.00	105.76	1.69	0.27	0.82
67.13	249.89	99.99	1.00	99.99	1.72	0.23	0.81
67.19	226.70	88.28	1.00	88.28	1.77	0.18	0.79
67.29	189.95	69.84	1.23	85.56	1.88	0.15	0.78
67.35	175.19	62.55	1.26	79.01	1.94	0.14	0.79
67.40	157.93	54.89	1.30	71.32	1.99	0.13	0.79
67.50	133.13	44.24	1.38	61.15	2.07	0.12	0.78
67.55	117.47	37.07	1.55	57.48	2.17	0.12	0.78
67.60	102.31	30.42	1.87	57.03	2.29	0.11	0.77
67.68	83.63	22.76	2.65	60.39	2.45	0.11	0.75
67.73	73.59	18.87	3.57	67.44	2.58	0.11	0.75
67.79	67.47	17.20	4.22	72.56	2.65	0.10	0.62
67.87	62.85	15.93	4.70	74.84	2.70	0.10	0.62
67.93	62.45	15.81	4.86	76.89	2.71	0.10	0.62
67.98	65.06	16.51	4.75	78.39	2.70	0.10	0.62
68.05	71.18	18.16	4.26	77.37	2.66	0.11	0.62
68.11	88.45	23.39	3.04	71.04	2.51	0.12	0.76
68.19	125.20	38.35	1.69	64.77	2.23	0.13	0.79
68.25	162.24	55.56	1.31	73.01	2.01	0.14	0.80
68.34	218.57	83.91	1.00	83.91	1.78	0.16	0.78
68.39	253.30	105.25	1.00	105.25	1.62	0.24	0.82
68.44	284.03	124.76	1.00	124.76	1.51	0.41	0.85
68.54	316.15	142.14	1.00	142.14	1.46	0.88	0.88
68.59	328.60	148.75	1.00	148.75	1.45	0.88	0.90
68.64	335.53	151.42	1.00	151.42	1.45	0.89	0.90
68.71	322.88	141.75	1.00	141.75	1.51	0.88	0.89
68.77	301.40	128.06	1.00	128.06	1.58	0.63	0.87
68.84	344.67	151.77	1.00	151.77	1.50	0.89	0.91
68.91	350.09	154.00	1.00	154.00	1.50	0.89	0.92
68.97	355.41	155.72	1.00	155.72	1.51	0.89	0.92
69.04	361.93	158.29	1.00	158.29	1.52	0.89	0.93
69.12	363.54	158.46	1.00	158.46	1.52	0.89	0.93
69.17	359.53	155.25	1.00	155.25	1.54	0.89	0.92
69.27	344.16	146.40	1.00	146.40	1.56	0.88	0.91
69.29	338.54	143.29	1.00	143.29	1.57	0.88	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
69.37	322.18	133.96	1.00	133.96	1.61	0.87	0.89
69.42	316.55	130.98	1.00	130.98	1.62	0.87	0.88
69.52	308.22	126.82	1.00	126.82	1.63	0.76	0.87
69.57	303.20	124.55	1.00	124.55	1.63	0.65	0.87
69.65	292.76	119.66	1.00	119.66	1.64	0.49	0.86
69.71	284.93	114.84	1.00	114.84	1.66	0.41	0.85
69.77	285.13	117.89	1.00	117.89	1.61	0.41	0.85
69.85	283.83	116.00	1.00	116.00	1.63	0.40	0.85
69.89	285.33	115.21	1.00	115.21	1.66	0.41	0.85
69.96	288.34	117.70	1.00	117.70	1.63	0.44	0.85
70.02	293.06	119.07	1.00	119.07	1.64	0.49	0.86
70.09	297.38	119.53	1.00	119.53	1.67	0.54	0.86
70.15	296.12	117.83	1.00	117.83	1.69	0.52	0.86
70.24	294.87	115.48	1.02	118.27	1.72	0.51	0.86
70.30	298.68	116.52	1.04	121.11	1.72	0.56	0.86
70.36	300.39	116.48	1.06	123.65	1.74	0.60	0.86
70.44	297.68	113.83	1.11	125.93	1.76	0.55	0.86
70.48	296.58	112.63	1.13	126.74	1.78	0.55	0.86
70.55	289.65	108.34	1.16	125.76	1.81	0.50	0.86
70.60	286.64	106.35	1.18	125.12	1.82	0.49	0.86
70.69	284.63	104.83	1.19	124.63	1.84	0.50	0.86
70.74	286.59	105.68	1.19	125.34	1.83	0.52	0.86
70.83	284.83	104.69	1.19	124.61	1.84	0.51	0.86
70.89	286.54	105.46	1.19	125.20	1.83	0.52	0.86
70.94	287.44	105.79	1.19	125.52	1.83	0.53	0.87
71.02	291.66	107.87	1.18	126.87	1.82	0.55	0.86
71.08	292.86	108.58	1.17	127.05	1.82	0.55	0.86
71.14	291.25	107.90	1.17	126.31	1.82	0.53	0.86
71.22	287.54	106.37	1.17	124.63	1.82	0.49	0.86
71.27	283.62	104.70	1.17	122.98	1.82	0.45	0.86
71.33	279.61	103.39	1.17	120.92	1.82	0.40	0.85
71.40	275.79	101.55	1.18	119.48	1.82	0.38	0.85
71.47	272.68	99.99	1.18	118.29	1.83	0.37	0.85
71.53	270.87	99.46	1.18	117.28	1.83	0.35	0.84
71.63	266.46	97.77	1.18	115.21	1.82	0.32	0.84
71.67	266.56	97.83	1.18	115.16	1.82	0.32	0.84
71.73	267.56	98.50	1.17	115.25	1.82	0.32	0.84
71.81	275.69	102.98	1.14	116.98	1.79	0.34	0.84
71.88	288.44	109.60	1.09	119.04	1.75	0.43	0.85
71.93	306.72	119.21	1.00	119.21	1.71	0.68	0.87
71.99	317.26	124.82	1.00	124.82	1.68	0.86	0.88
72.05	324.89	128.59	1.00	128.59	1.67	0.86	0.89
72.13	332.72	132.01	1.00	132.01	1.66	0.87	0.90
72.18	336.53	133.71	1.00	133.71	1.66	0.87	0.90
72.27	341.55	136.29	1.00	136.29	1.65	0.87	0.90
72.32	343.16	136.95	1.00	136.95	1.65	0.87	0.91
72.38	342.66	135.98	1.00	135.98	1.66	0.87	0.91
72.46	339.85	133.38	1.00	133.38	1.68	0.87	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
72.52	335.63	130.35	1.00	130.35	1.70	0.87	0.90
72.62	333.22	128.82	1.00	129.12	1.71	0.86	0.90
72.66	334.12	129.36	1.00	129.36	1.70	0.86	0.90
72.71	336.43	130.69	1.00	130.69	1.70	0.87	0.90
72.82	342.46	134.40	1.00	134.40	1.67	0.87	0.90
72.85	346.07	136.36	1.00	136.36	1.67	0.87	0.91
72.91	349.08	137.97	1.00	137.97	1.66	0.87	0.91
72.97	354.00	140.66	1.00	140.66	1.65	0.88	0.92
73.06	362.84	146.50	1.00	146.50	1.61	0.88	0.92
73.11	368.16	149.84	1.00	149.84	1.60	0.89	0.93
73.17	378.00	155.57	1.00	155.57	1.57	0.89	0.94
73.24	383.33	158.62	1.00	158.62	1.56	0.89	0.94
73.31	388.25	161.49	1.00	161.49	1.55	0.90	0.95
73.37	392.06	163.03	1.00	163.03	1.55	0.90	0.95
73.43	394.67	163.70	1.00	163.70	1.55	0.90	0.95
73.51	398.99	165.69	1.00	165.69	1.55	0.90	0.95
73.56	400.40	166.38	1.00	166.38	1.55	0.90	0.95
73.65	404.41	167.72	1.00	167.72	1.55	0.90	0.95
73.71	404.71	167.52	1.00	167.52	1.56	0.90	0.95
73.76	405.22	167.10	1.00	167.10	1.56	0.90	0.95
73.84	404.91	165.94	1.00	165.94	1.57	0.90	0.95
73.90	403.41	165.12	1.00	165.12	1.58	0.90	0.95
73.95	401.20	164.20	1.00	164.20	1.57	0.90	0.95
74.06	396.88	162.69	1.00	162.69	1.57	0.90	0.95
74.10	391.36	159.62	1.00	159.62	1.58	0.90	0.95
74.15	385.64	157.47	1.00	157.47	1.57	0.89	0.94
74.22	376.40	154.10	1.00	154.10	1.57	0.89	0.94
74.29	371.48	151.34	1.00	151.34	1.58	0.89	0.93
74.35	364.56	147.22	1.00	147.22	1.59	0.88	0.92
74.43	355.32	142.05	1.00	142.05	1.61	0.88	0.92
74.48	349.39	138.59	1.00	138.59	1.63	0.87	0.91
74.54	295.08	109.32	1.10	119.89	1.76	0.47	0.85
74.64	326.91	125.30	1.00	125.30	1.69	0.86	0.89
74.69	319.78	121.16	1.01	122.74	1.71	0.85	0.88
74.75	312.75	118.47	1.01	119.70	1.71	0.75	0.87
74.83	303.61	115.04	1.00	115.51	1.71	0.58	0.86
74.87	297.59	111.27	1.06	117.52	1.73	0.49	0.86
74.94	291.67	107.51	1.10	118.43	1.76	0.43	0.85
75.02	285.34	103.50	1.14	118.26	1.79	0.39	0.85
75.08	276.81	98.79	1.18	116.15	1.82	0.36	0.84
75.13	267.07	93.83	1.20	112.75	1.85	0.34	0.85
75.22	278.61	99.72	1.17	116.46	1.81	0.36	0.84
75.28	280.32	70.21	54.25	3809.10	4.06	0.78	5.02
75.33	282.33	70.72	54.25	3836.24	4.06	0.78	5.05
75.42	284.64	71.28	54.25	3866.95	4.06	0.78	5.09
75.47	286.45	71.73	54.25	3891.34	4.06	0.78	5.12
75.53	288.15	72.15	54.25	3914.06	4.06	0.78	5.15
75.62	289.46	72.46	54.25	3930.92	4.06	0.78	5.18

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
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Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

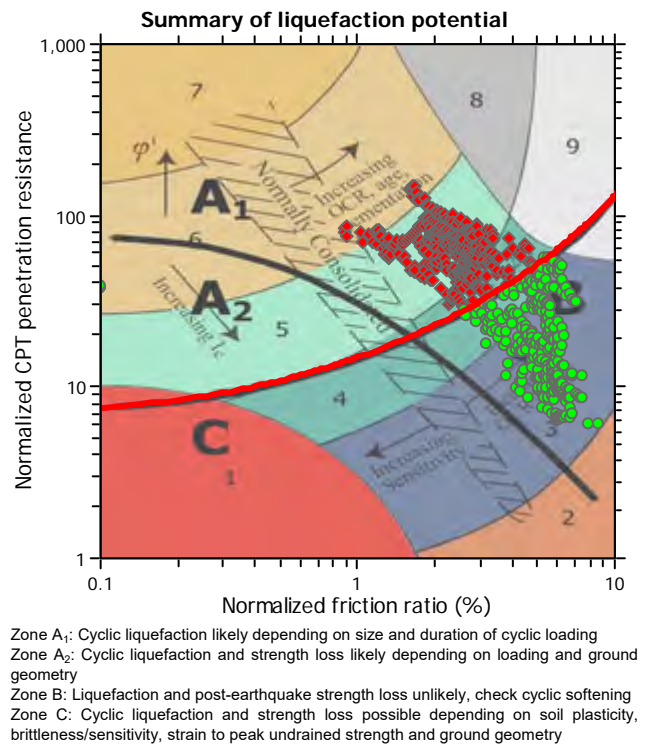
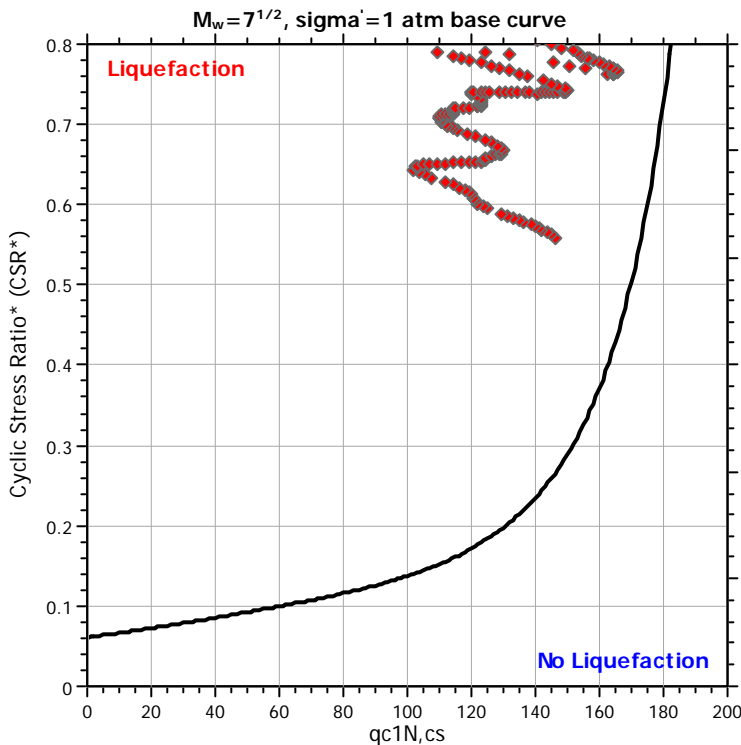
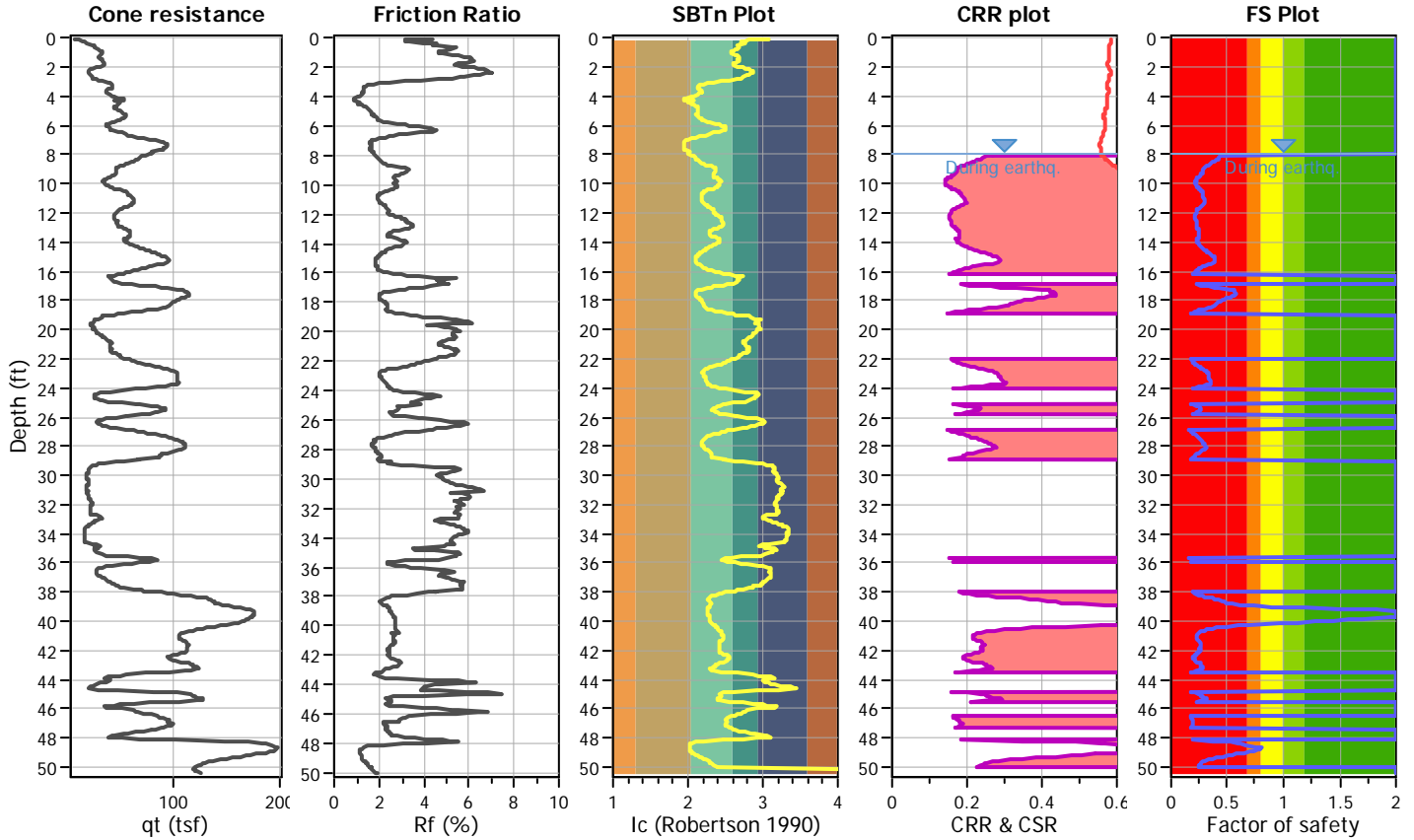
LIQUEFACTION ANALYSIS REPORT

Project title : Universal Engineering Services / Compton
CPT file : CPT-6

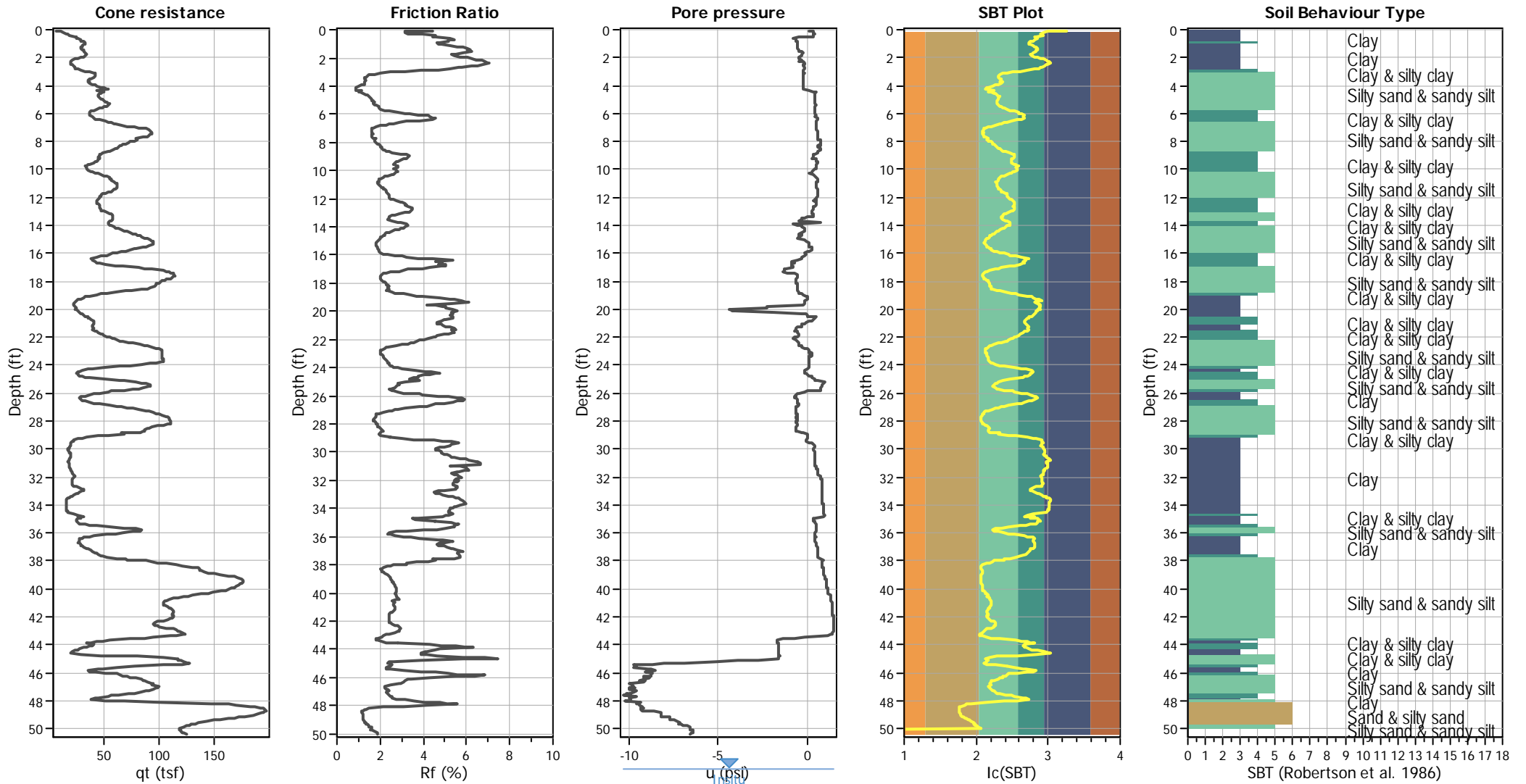
Location : 1111 E. Artesia Blvd, Compton, CA

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	52.90 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	8.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	1	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w :	7.30	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method
Peak ground acceleration:	0.77	Unit weight calculation:	Based on SBT	K_G applied:	Yes		



CPT basic interpretation plots



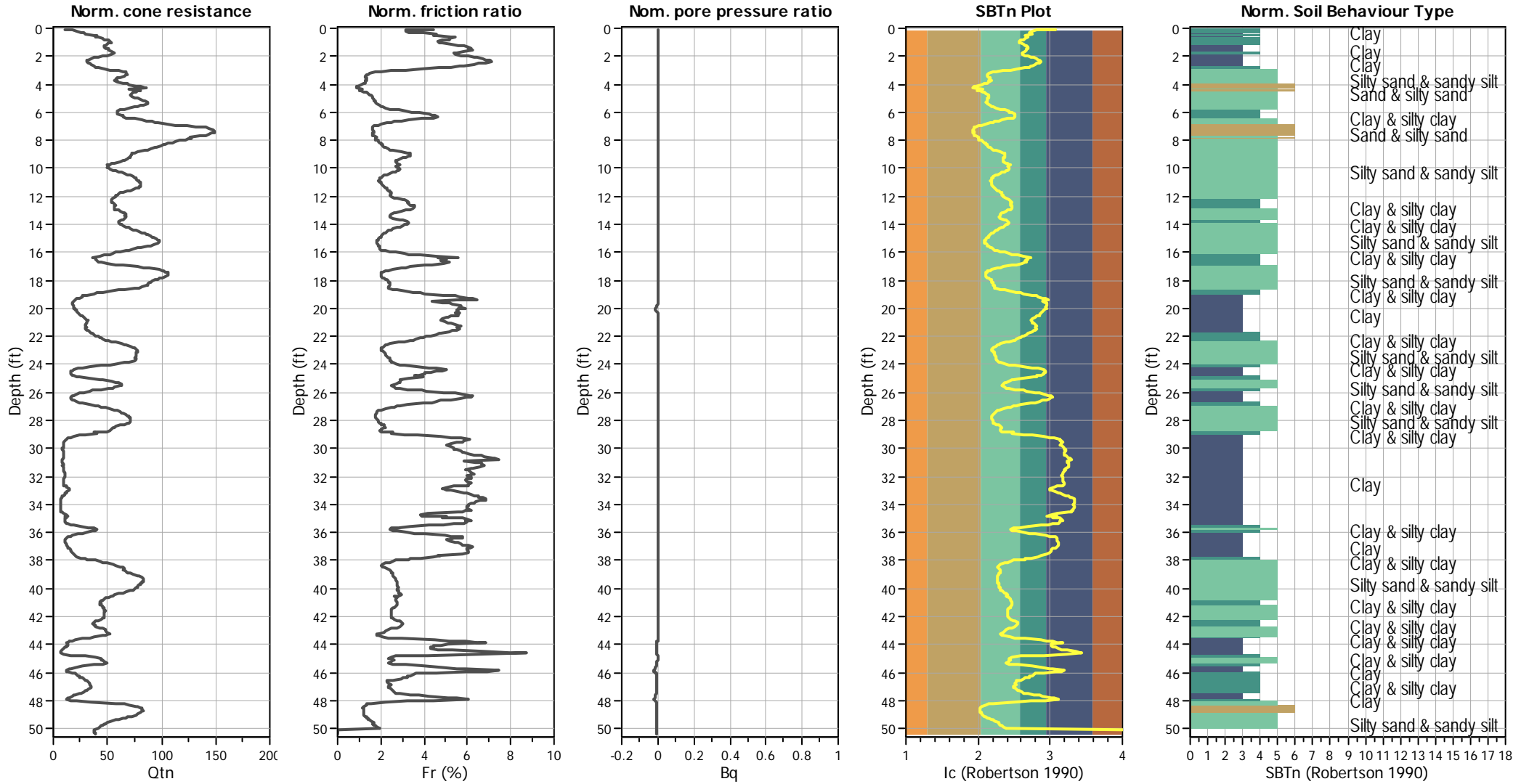
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

■ 1. Sensitive fine grained	■ 4. Clayey silt to silty	■ 7. Gravely sand to sand
■ 2. Organic material	■ 5. Silty sand to sandy silt	■ 8. Very stiff sand to
■ 3. Clay to silty clay	■ 6. Clean sand to silty sand	■ 9. Very stiff fine grained

CPT basic interpretation plots (normalized)



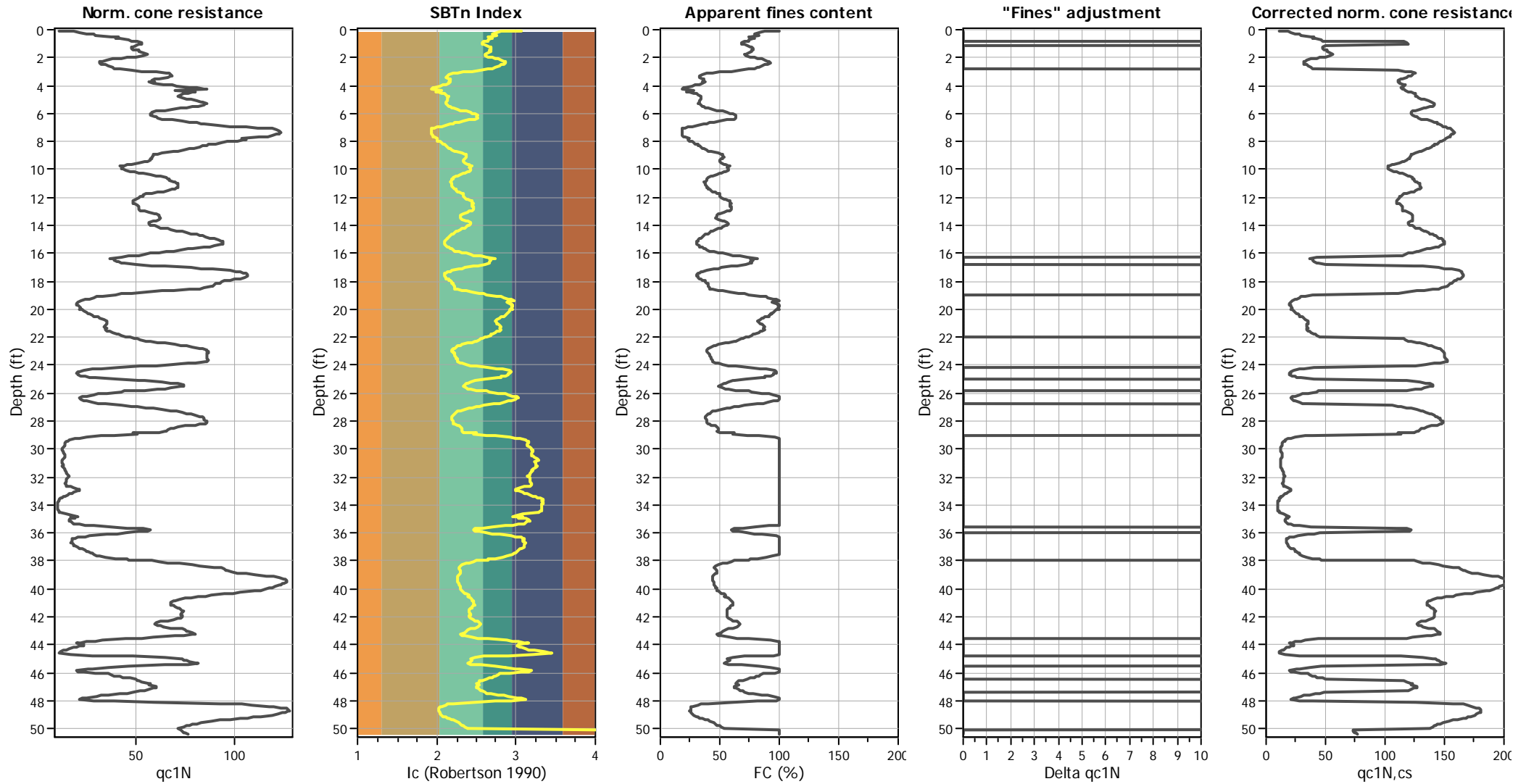
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

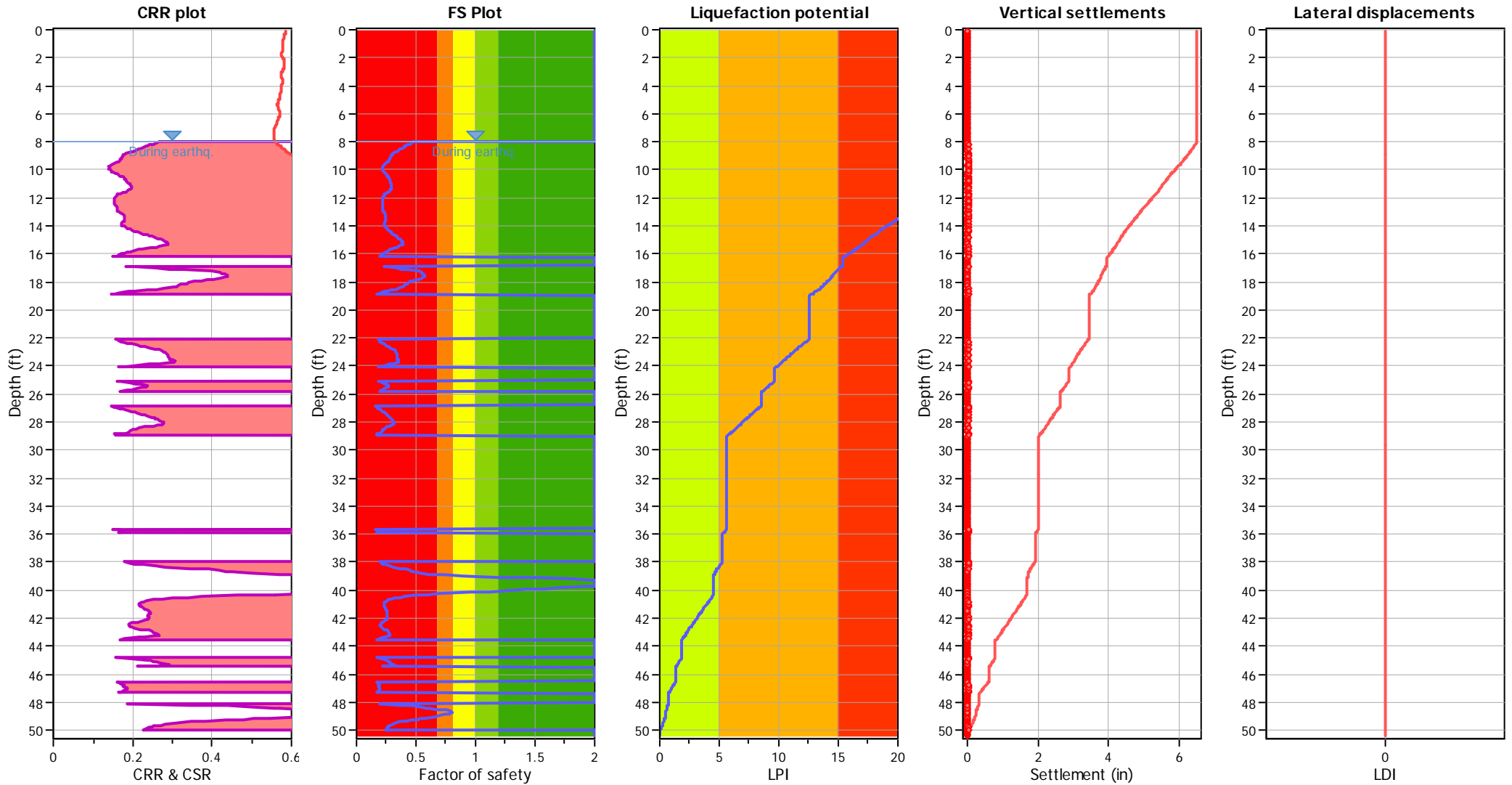
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

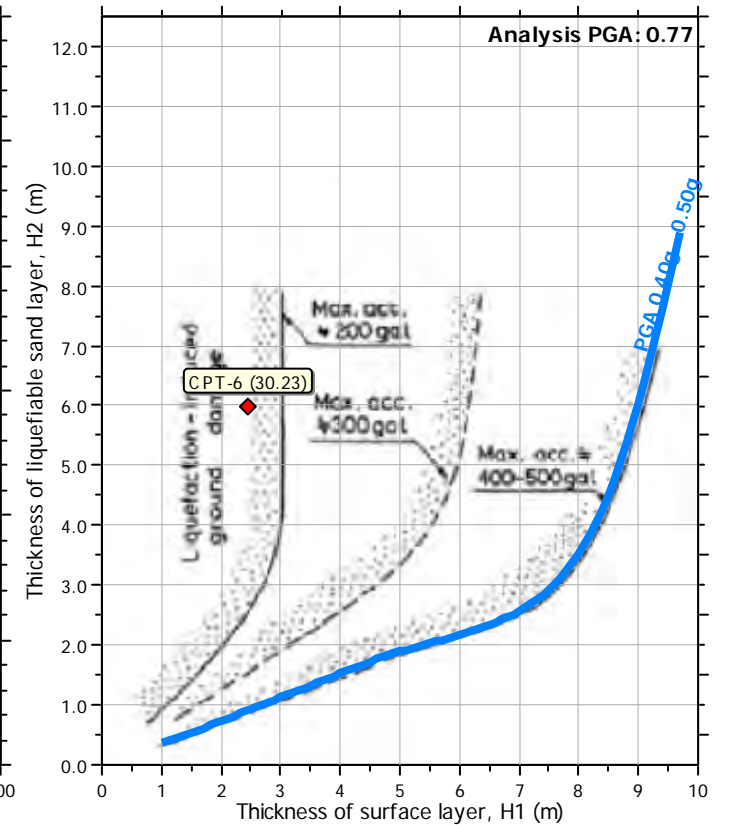
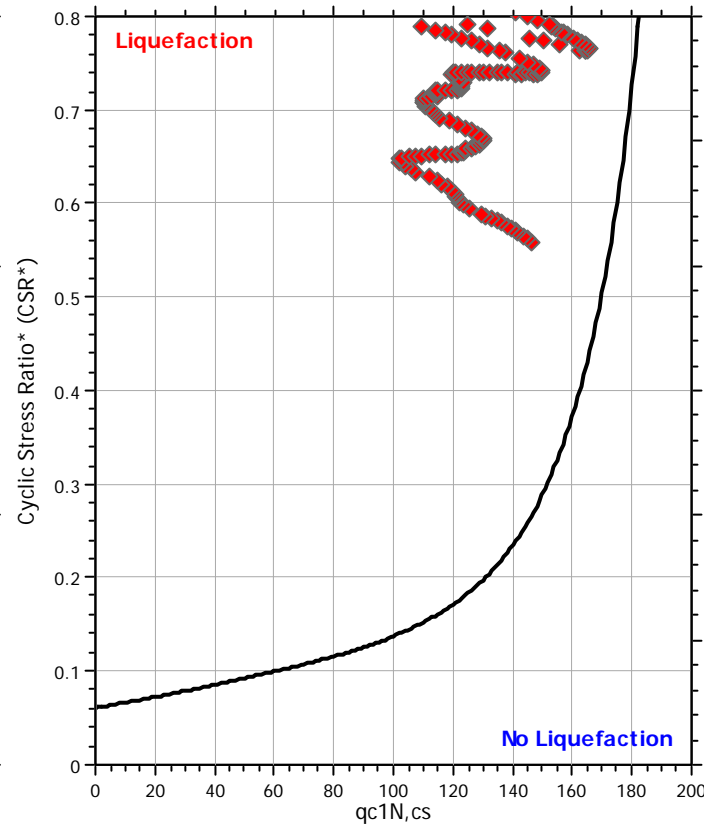
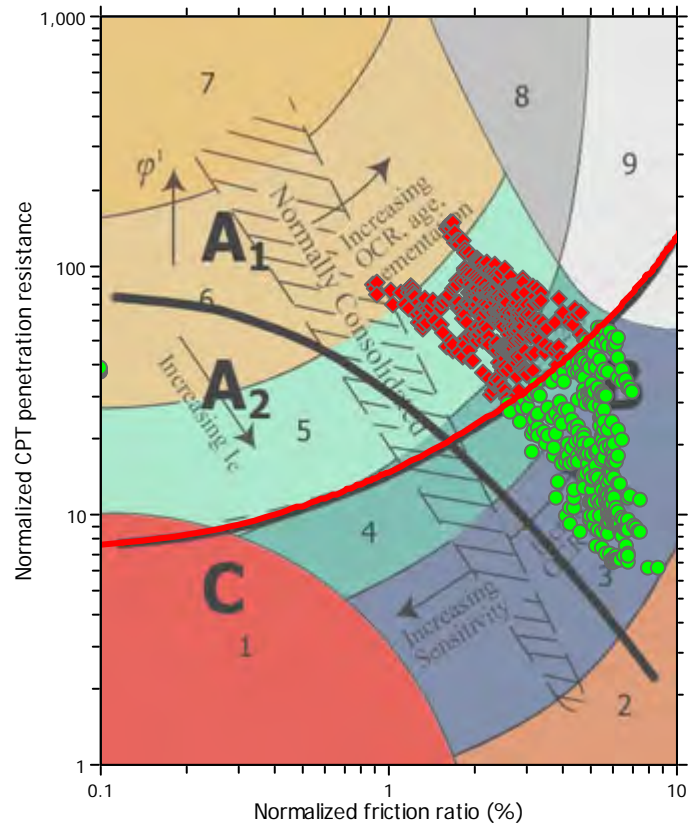
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

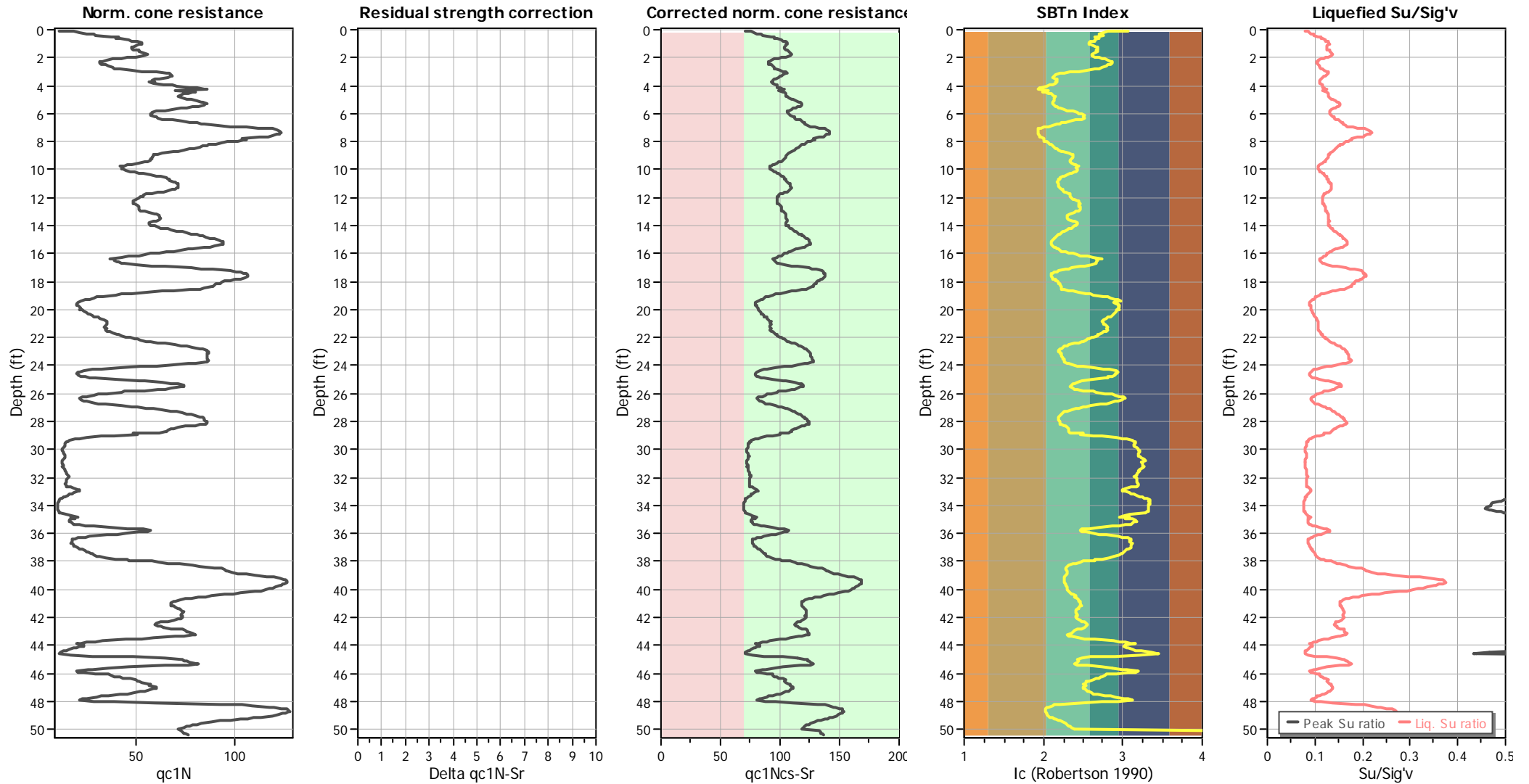
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on I_c value	I_c cut-off value:	2.60	K_G applied:	Yes
Earthquake magnitude M_w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	8.00 ft	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	1	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K _σ applied:	Yes
Earthquake magnitude M _w :	7.30	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.77	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	52.90 ft	Fill height:	N/A	Limit depth:	50.00 ft

:: Field input data ::						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.10	6.64	0.29	0.10	63.48	105.89
2	0.14	11.06	0.35	0.29	46.60	108.49
3	0.21	13.17	0.42	0.29	43.19	110.18
4	0.26	15.48	0.51	0.38	40.81	112.03
5	0.34	17.50	0.69	0.29	41.50	114.59
6	0.40	18.00	0.82	0.29	43.28	115.90
7	0.49	23.33	1.03	0.29	38.36	118.16
8	0.53	25.34	1.16	-0.48	37.63	119.23
9	0.59	24.63	1.29	-0.86	40.28	119.95
10	0.66	25.94	1.41	-0.67	40.02	120.70
11	0.73	28.76	1.48	-0.67	37.60	121.34
12	0.81	29.56	1.52	-0.67	37.22	121.62
13	0.87	31.57	1.51	-0.57	35.11	121.72
14	0.92	32.88	1.53	-0.57	34.02	121.88
15	0.99	33.08	1.54	-0.57	34.03	121.98
16	1.05	32.17	1.55	-0.57	34.88	121.93
17	1.15	30.97	1.62	-0.57	36.76	122.17
18	1.20	29.96	1.67	-0.57	38.27	122.30
19	1.26	29.56	1.72	-0.57	39.23	122.50
20	1.32	29.56	1.79	-0.57	39.91	122.79
21	1.39	30.16	1.86	-0.48	39.89	123.11
22	1.46	31.77	1.92	-0.48	38.77	123.47
23	1.51	32.07	1.96	-0.48	38.87	123.66
24	1.58	31.97	1.99	-0.38	39.23	123.77
25	1.66	33.58	1.96	-0.29	37.42	123.78
26	1.71	34.89	1.92	-0.38	35.90	123.71
27	1.79	34.79	1.85	-0.38	35.43	123.45
28	1.84	33.58	1.83	-0.38	36.25	123.25
29	1.93	31.07	1.76	-0.48	38.09	122.80
30	1.98	28.45	1.72	-0.48	40.50	122.40
31	2.04	26.34	1.65	-0.48	42.37	121.92
32	2.11	23.83	1.53	-0.48	44.44	121.11
33	2.17	21.62	1.44	-0.38	46.86	120.45
34	2.24	20.31	1.39	-0.48	48.40	120.01
35	2.32	19.61	1.37	-0.29	49.42	119.81
36	2.38	19.41	1.37	-0.19	49.81	119.78
37	2.43	20.11	1.37	-0.29	48.50	119.87
38	2.52	21.42	1.39	-0.19	46.51	120.15
39	2.56	22.22	1.39	-0.29	45.24	120.25
40	2.64	23.53	1.36	-0.19	42.90	120.24
41	2.69	23.73	1.33	-0.19	42.23	120.09
42	2.78	24.23	1.27	-0.19	40.69	119.78
43	2.83	26.14	1.22	-0.19	37.68	119.70
44	2.89	29.66	1.15	-0.29	32.89	119.53
45	2.95	33.08	1.05	-0.29	28.66	119.15
46	3.02	37.40	0.92	-0.29	24.04	118.53
47	3.09	40.62	0.82	-0.29	20.85	117.86
48	3.15	41.83	0.73	-0.19	19.01	117.04

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.22	42.33	0.63	-0.29	17.49	116.07
50	3.29	42.73	0.59	-0.29	16.75	115.63
51	3.35	41.93	0.56	-0.29	16.61	115.16
52	3.41	41.02	0.53	-0.29	16.52	114.67
53	3.52	38.51	0.50	-0.29	17.28	114.11
54	3.55	36.90	0.50	-0.29	18.03	113.93
55	3.61	36.10	0.47	-0.29	18.07	113.55
56	3.71	36.85	0.47	-0.29	17.54	113.49
57	3.75	35.39	0.46	-0.29	18.27	113.33
58	3.81	36.80	0.47	-0.29	17.59	113.51
59	3.90	40.02	0.50	-0.29	16.51	114.18
60	3.95	42.53	0.50	-0.29	15.39	114.33
61	4.01	44.04	0.46	-0.29	14.07	113.75
62	4.09	47.96	0.43	-0.29	12.28	113.58
63	4.15	50.57	0.45	-0.29	11.70	114.00
64	4.21	52.79	0.46	-0.29	11.25	114.34
65	4.29	53.49	0.48	-0.29	11.27	114.62
66	4.34	43.54	0.49	0.05	14.85	114.28
67	4.41	49.97	0.51	0.29	12.75	114.87
68	4.46	48.97	0.53	0.48	13.45	115.18
69	4.55	47.56	0.59	0.38	14.67	115.78
70	4.61	46.45	0.61	0.38	15.49	116.07
71	4.67	45.25	0.64	0.38	16.28	116.27
72	4.75	44.54	0.67	0.38	16.98	116.56
73	4.79	44.54	0.68	0.38	17.19	116.73
74	4.87	45.75	0.72	0.38	17.14	117.18
75	4.93	47.06	0.75	0.38	17.00	117.57
76	4.99	48.46	0.78	0.38	16.81	117.94
77	5.06	50.37	0.83	0.38	16.60	118.47
78	5.14	51.88	0.88	0.38	16.54	118.94
79	5.19	52.69	0.90	0.38	16.51	119.19
80	5.25	54.39	0.93	0.38	16.17	119.48
81	5.33	54.70	0.96	0.38	16.40	119.76
82	5.38	54.39	0.99	0.48	16.81	119.98
83	5.45	52.38	1.01	0.38	17.66	119.97
84	5.52	50.57	0.98	0.38	18.12	119.70
85	5.59	48.46	0.96	0.38	18.73	119.40
86	5.64	46.75	0.96	0.38	19.48	119.32
87	5.72	43.74	0.96	0.38	20.92	119.16
88	5.78	41.22	0.99	0.38	22.58	119.23
89	5.85	38.41	1.08	0.38	25.34	119.74
90	5.92	37.10	1.17	0.38	27.23	120.24
91	5.98	37.15	1.25	0.38	28.05	120.73
92	6.04	37.15	1.39	0.38	29.51	121.52
93	6.11	37.20	1.57	0.48	31.12	122.37
94	6.17	39.21	1.68	0.38	30.70	123.03
95	6.24	40.12	1.78	0.38	30.87	123.49
96	6.32	40.82	1.87	0.57	31.15	123.91

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.38	42.53	1.88	0.57	30.03	124.02
98	6.44	46.75	1.80	0.57	26.99	123.96
99	6.51	50.98	1.65	0.48	23.74	123.54
100	6.58	54.19	1.57	0.48	21.75	123.33
101	6.66	57.21	1.50	0.48	20.02	123.11
102	6.71	58.72	1.43	0.48	18.99	122.84
103	6.77	60.43	1.37	0.48	17.93	122.58
104	6.83	65.66	1.33	0.48	16.03	122.57
105	6.92	70.68	1.30	0.48	14.46	122.57
106	6.97	77.12	1.31	0.48	13.02	122.84
107	7.03	82.15	1.34	0.48	12.18	123.17
108	7.10	87.98	1.40	0.48	11.42	123.63
109	7.16	90.19	1.46	0.48	11.38	124.00
110	7.22	92.00	1.49	0.57	11.28	124.23
111	7.31	93.00	1.52	0.57	11.28	124.41
112	7.36	93.00	1.54	0.57	11.36	124.49
113	7.42	93.00	1.53	0.57	11.30	124.43
114	7.49	91.90	1.48	0.57	11.28	124.18
115	7.55	90.39	1.47	0.57	11.46	124.05
116	7.62	89.08	1.46	0.57	11.66	123.97
117	7.71	85.77	1.44	0.57	12.17	123.78
118	7.75	79.33	1.43	0.57	13.31	123.54
119	7.83	80.84	1.39	0.57	12.88	123.40
120	7.88	79.73	1.38	0.67	13.04	123.29
121	7.95	77.82	1.35	0.67	13.28	123.07
122	8.01	74.00	1.36	0.67	14.19	123.02
123	8.09	71.79	1.36	0.67	14.72	122.92
124	8.14	69.68	1.35	0.67	15.22	122.83
125	8.24	67.16	1.35	0.67	15.89	122.72
126	8.29	66.26	1.34	0.57	16.13	122.66
127	8.34	64.95	1.34	0.67	16.48	122.59
128	8.41	63.65	1.33	0.57	16.86	122.51
129	8.49	61.33	1.32	0.67	17.52	122.36
130	8.53	60.03	1.32	0.67	17.92	122.29
131	8.60	57.51	1.33	0.67	18.85	122.24
132	8.67	55.50	1.33	0.57	19.59	122.15
133	8.73	53.69	1.37	0.57	20.60	122.29
134	8.80	48.97	1.44	0.57	23.13	122.44
135	8.87	47.36	1.51	0.38	24.49	122.72
136	8.93	45.85	1.52	0.29	25.36	122.68
137	9.02	45.75	1.50	0.29	25.33	122.58
138	9.07	45.25	1.49	0.29	25.51	122.47
139	9.13	45.45	1.47	0.29	25.33	122.40
140	9.20	45.55	1.41	0.19	24.90	122.12
141	9.25	45.35	1.35	0.48	24.52	121.78
142	9.32	44.94	1.28	0.48	24.18	121.37
143	9.39	43.84	1.21	0.48	24.12	120.86
144	9.46	42.73	1.14	0.57	24.13	120.38

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.52	40.82	1.07	0.57	24.55	119.83
146	9.61	37.40	1.01	0.48	25.94	119.15
147	9.66	36.20	0.99	0.48	26.56	118.94
148	9.71	34.49	0.97	0.48	27.53	118.67
149	9.78	33.28	0.94	0.48	28.09	118.34
150	9.86	34.44	0.91	0.48	27.01	118.22
151	9.91	33.83	0.91	0.48	27.46	118.15
152	9.97	34.39	0.95	0.38	27.63	118.51
153	10.06	36.00	1.02	0.29	27.48	119.17
154	10.11	37.81	1.05	0.19	26.64	119.48
155	10.17	39.92	1.08	0.19	25.78	119.85
156	10.25	42.33	1.11	0.19	24.77	120.17
157	10.31	44.34	1.13	0.10	23.93	120.39
158	10.37	47.46	1.13	0.29	22.50	120.57
159	10.44	50.07	1.12	0.38	21.34	120.66
160	10.50	52.38	1.12	0.38	20.45	120.76
161	10.57	54.70	1.11	0.48	19.53	120.80
162	10.64	55.90	1.11	0.57	19.11	120.82
163	10.70	56.81	1.11	0.57	18.87	120.89
164	10.77	57.01	1.11	0.57	18.82	120.87
165	10.85	59.12	1.12	0.57	18.28	121.06
166	10.90	59.82	1.13	0.48	18.16	121.14
167	10.97	60.53	1.17	0.48	18.33	121.44
168	11.03	61.53	1.21	0.48	18.35	121.71
169	11.09	61.74	1.24	0.48	18.56	121.91
170	11.17	61.94	1.27	0.48	18.79	122.10
171	11.26	61.94	1.32	0.48	19.19	122.36
172	11.30	61.84	1.33	0.48	19.32	122.41
173	11.36	61.13	1.34	0.57	19.68	122.45
174	11.42	59.72	1.34	0.57	20.22	122.41
175	11.50	57.91	1.32	0.57	20.75	122.22
176	11.56	56.10	1.29	0.57	21.24	121.98
177	11.62	53.59	1.27	0.57	22.08	121.74
178	11.69	50.98	1.23	0.57	22.87	121.37
179	11.76	48.36	1.18	0.57	23.69	120.97
180	11.83	47.36	1.15	0.57	23.87	120.68
181	11.88	46.95	1.12	0.57	23.86	120.49
182	11.95	46.25	1.11	0.57	24.20	120.42
183	12.01	45.55	1.12	0.48	24.64	120.41
184	12.08	44.44	1.15	0.48	25.60	120.55
185	12.14	44.24	1.20	0.38	26.28	120.87
186	12.23	42.93	1.27	0.48	27.76	121.20
187	12.28	43.13	1.30	0.29	27.97	121.39
188	12.35	43.13	1.36	0.48	28.57	121.70
189	12.40	43.13	1.39	0.48	28.92	121.88
190	12.47	44.44	1.42	0.48	28.42	122.07
191	12.54	45.45	1.48	0.48	28.47	122.45
192	12.60	46.75	1.54	0.38	28.29	122.81

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.70	46.35	1.61	0.29	29.18	123.12
194	12.75	46.55	1.62	0.29	29.19	123.18
195	12.80	46.65	1.62	0.29	29.17	123.17
196	12.87	46.85	1.60	0.29	28.95	123.09
197	12.93	47.46	1.58	0.19	28.53	123.04
198	12.99	50.27	1.57	0.19	27.03	123.13
199	13.06	52.38	1.53	0.19	25.74	123.03
200	13.14	55.30	1.47	0.19	24.08	122.89
201	13.19	56.10	1.44	0.29	23.53	122.76
202	13.26	57.71	1.39	0.29	22.58	122.60
203	13.32	57.61	1.39	0.29	22.61	122.56
204	13.40	58.12	1.39	0.00	22.51	122.61
205	13.46	58.42	1.38	-0.19	22.33	122.55
206	13.53	58.52	1.38	-0.38	22.32	122.54
207	13.58	58.12	1.46	-0.38	23.18	122.97
208	13.68	56.81	1.62	-0.48	24.93	123.65
209	13.73	55.90	1.67	-0.51	25.69	123.82
210	13.79	53.39	1.71	0.67	27.16	123.88
211	13.88	53.49	1.75	-0.51	27.50	124.06
212	13.92	53.59	1.74	-0.86	27.46	124.05
213	13.98	54.70	1.74	-0.57	26.95	124.08
214	14.05	57.01	1.75	-0.38	26.06	124.24
215	14.13	58.82	1.74	-0.38	25.25	124.25
216	14.17	60.33	1.72	-0.19	24.58	124.25
217	14.24	63.65	1.71	-0.19	23.28	124.33
218	14.33	65.86	1.67	-0.19	22.33	124.26
219	14.37	68.47	1.66	-0.19	21.38	124.28
220	14.45	71.39	1.64	-0.19	20.43	124.31
221	14.53	73.90	1.66	-0.38	19.83	124.46
222	14.57	76.11	1.67	-0.48	19.34	124.60
223	14.64	79.23	1.68	-0.38	18.59	124.71
224	14.72	80.94	1.68	-0.48	18.22	124.78
225	14.76	82.55	1.68	-0.38	17.88	124.85
226	14.85	84.86	1.69	-0.48	17.42	124.95
227	14.90	86.67	1.70	-0.57	17.08	125.03
228	14.96	88.98	1.71	-0.57	16.67	125.14
229	15.03	91.80	1.70	-0.19	16.07	125.19
230	15.10	93.00	1.71	-0.10	15.90	125.25
231	15.16	94.21	1.71	-0.10	15.69	125.28
232	15.24	94.81	1.71	0.10	15.62	125.31
233	15.31	94.61	1.71	0.10	15.70	125.31
234	15.36	94.21	1.71	0.10	15.76	125.26
235	15.45	90.59	1.68	0.10	16.38	125.06
236	15.50	88.38	1.65	0.10	16.73	124.88
237	15.55	85.26	1.63	0.19	17.29	124.67
238	15.66	79.63	1.54	0.19	18.14	124.09
239	15.69	77.32	1.50	0.19	18.51	123.84
240	15.75	73.90	1.42	0.19	18.95	123.34

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.82	69.98	1.39	0.10	19.92	123.06
242	15.91	66.46	1.45	0.00	21.48	123.21
243	15.96	62.44	1.48	-0.19	23.21	123.25
244	16.02	58.01	1.54	-0.19	25.42	123.33
245	16.08	55.00	1.65	-0.10	27.70	123.73
246	16.14	52.18	1.68	-0.19	29.34	123.71
247	16.22	47.16	1.78	-0.19	33.00	123.88
248	16.30	43.64	1.95	-0.38	36.76	124.36
249	16.34	37.60	2.03	-0.38	42.34	124.30
250	16.42	39.82	1.81	-0.38	38.61	123.59
251	16.50	40.12	1.96	-0.56	39.75	124.20
252	16.54	41.73	2.02	-0.95	39.00	124.52
253	16.62	42.13	1.97	-0.74	38.34	124.35
254	16.70	43.94	2.21	-0.76	38.91	125.30
255	16.74	45.75	2.31	-0.92	38.38	125.73
256	16.80	51.78	2.49	-0.92	35.72	126.57
257	16.87	60.73	2.59	-0.92	31.68	127.25
258	16.94	67.77	2.67	-0.86	29.10	127.73
259	17.01	81.74	2.71	-0.86	24.59	128.31
260	17.09	87.37	2.72	-1.24	23.10	128.51
261	17.14	93.41	2.70	-1.33	21.49	128.59
262	17.23	103.36	2.58	-1.33	18.84	128.51
263	17.28	106.98	2.47	-1.33	17.73	128.28
264	17.34	109.09	2.37	-1.43	16.94	128.02
265	17.39	110.80	2.29	-1.14	16.35	127.82
266	17.46	112.81	2.27	-0.76	15.94	127.80
267	17.52	113.82	2.27	-0.57	15.79	127.82
268	17.60	114.02	2.27	-0.57	15.79	127.82
269	17.66	113.72	2.27	-0.57	15.86	127.81
270	17.73	112.31	2.25	-0.57	16.06	127.73
271	17.79	109.90	2.26	-0.67	16.53	127.70
272	17.86	107.18	2.30	-0.67	17.20	127.76
273	17.92	105.07	2.31	-0.67	17.68	127.75
274	17.98	102.36	2.33	-0.67	18.31	127.74
275	18.07	100.75	2.33	-0.67	18.66	127.70
276	18.11	99.84	2.33	-0.67	18.87	127.68
277	18.18	97.83	2.34	-0.57	19.40	127.67
278	18.27	97.23	2.30	-0.57	19.40	127.54
279	18.32	96.42	2.29	-0.57	19.56	127.49
280	18.37	95.52	2.28	-0.57	19.72	127.43
281	18.46	92.00	2.15	-0.57	19.94	126.91
282	18.52	89.28	2.05	-0.57	20.09	126.48
283	18.57	84.56	1.97	-0.57	20.90	126.07
284	18.66	75.21	1.90	-0.57	23.21	125.51
285	18.71	69.58	1.88	-0.57	25.00	125.24
286	18.77	60.23	1.84	-0.48	28.53	124.74
287	18.84	52.38	1.78	-0.48	32.03	124.15
288	18.91	46.85	1.74	-0.38	35.07	123.70

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.97	43.74	1.73	-0.29	37.17	123.48
290	19.05	36.30	1.73	-0.10	43.58	123.03
291	19.10	32.98	1.72	0.00	47.11	122.78
292	19.16	31.87	1.72	0.00	48.46	122.69
293	19.26	28.86	1.67	0.00	51.88	122.22
294	19.30	26.85	1.60	0.00	54.09	121.75
295	19.36	24.53	1.50	-0.19	56.72	121.07
296	19.43	24.73	1.30	-0.19	53.70	120.03
297	19.51	23.13	0.96	-0.19	50.98	117.61
298	19.55	22.12	1.01	-0.19	53.76	117.88
299	19.63	22.12	1.08	-0.19	55.05	118.37
300	19.69	22.12	1.11	-0.29	55.74	118.61
301	19.75	22.92	1.16	-0.29	55.02	118.97
302	19.84	23.63	1.27	-2.27	55.71	119.76
303	19.89	24.63	1.32	-2.27	54.62	120.09
304	19.96	24.23	1.35	-4.38	55.95	120.25
305	20.02	25.64	1.36	-4.29	53.74	120.42
306	20.09	26.14	1.38	-4.19	53.32	120.58
307	20.14	26.85	1.41	-4.10	52.74	120.83
308	20.22	27.95	1.49	-1.91	52.16	121.33
309	20.28	29.46	1.54	-0.38	50.66	121.68
310	20.36	30.26	1.63	-0.10	50.78	122.18
311	20.41	31.77	1.70	0.00	49.59	122.57
312	20.48	32.88	1.76	0.00	48.99	122.92
313	20.55	35.29	1.78	0.48	46.55	123.18
314	20.61	36.10	1.78	0.38	45.78	123.25
315	20.68	36.70	1.78	0.38	45.20	123.27
316	20.74	38.61	1.80	0.29	43.56	123.47
317	20.81	40.32	1.86	0.19	42.65	123.82
318	20.88	41.12	1.91	0.10	42.47	124.07
319	20.93	40.62	1.96	-0.10	43.44	124.25
320	21.00	40.72	2.00	-0.19	43.76	124.40
321	21.07	40.52	2.05	-0.38	44.42	124.56
322	21.13	39.92	2.10	-0.38	45.42	124.68
323	21.22	39.51	2.16	-0.38	46.39	124.86
324	21.27	39.62	2.18	-0.57	46.50	124.94
325	21.34	41.02	2.19	-0.67	45.34	125.05
326	21.41	40.52	2.19	-0.67	45.86	125.02
327	21.46	40.12	2.19	-0.67	46.34	125.02
328	21.55	41.73	2.23	-0.76	45.25	125.24
329	21.59	43.54	2.25	-0.62	43.87	125.41
330	21.66	44.84	2.24	-0.62	42.80	125.45
331	21.76	47.76	2.22	-0.55	40.50	125.53
332	21.80	48.66	2.22	-0.48	39.92	125.59
333	21.86	49.97	2.23	-0.48	39.15	125.69
334	21.95	53.29	2.25	-0.57	37.17	125.89
335	22.01	55.60	2.24	-0.76	35.78	125.96
336	22.06	57.91	2.23	-0.86	34.47	126.03

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.12	59.82	2.22	-0.86	33.47	126.09
338	22.18	62.14	2.22	-0.67	32.36	126.18
339	22.26	65.15	2.22	-0.57	31.01	126.30
340	22.31	67.77	2.22	-0.57	29.91	126.39
341	22.38	72.59	2.20	-0.48	27.91	126.49
342	22.44	76.62	2.12	-0.48	26.05	126.36
343	22.53	83.25	1.97	-0.48	23.09	126.02
344	22.59	86.67	1.97	-0.48	22.15	126.12
345	22.65	89.69	1.97	-0.38	21.39	126.21
346	22.71	93.61	1.97	-0.38	20.45	126.32
347	22.78	97.73	1.99	-0.19	19.60	126.48
348	22.86	99.94	2.01	0.00	19.28	126.63
349	22.92	102.15	2.03	0.10	18.90	126.73
350	22.98	102.66	2.05	0.10	18.91	126.81
351	23.04	103.16	2.09	0.10	19.03	126.96
352	23.10	103.26	2.15	0.19	19.37	127.20
353	23.16	102.86	2.18	0.10	19.63	127.29
354	23.25	102.86	2.22	0.19	19.83	127.40
355	23.30	102.86	2.24	0.10	19.96	127.48
356	23.36	102.86	2.27	0.19	20.14	127.58
357	23.43	102.96	2.33	0.10	20.42	127.76
358	23.49	102.96	2.38	0.10	20.67	127.91
359	23.56	103.66	2.44	0.10	20.83	128.11
360	23.65	104.37	2.48	0.10	20.89	128.25
361	23.71	103.76	2.50	0.10	21.13	128.28
362	23.76	102.56	2.48	0.10	21.34	128.21
363	23.83	97.33	2.41	0.10	22.26	127.86
364	23.89	92.40	2.33	0.10	23.16	127.50
365	23.95	83.65	2.21	0.10	25.03	126.87
366	24.02	74.10	2.09	0.10	27.59	126.18
367	24.09	64.15	1.95	0.10	30.78	125.32
368	24.15	50.68	1.83	0.10	37.24	124.27
369	24.24	40.12	1.63	0.00	43.67	122.87
370	24.29	35.29	1.54	0.00	47.56	122.11
371	24.35	29.86	1.43	-0.19	52.87	121.16
372	24.42	27.15	1.25	-0.19	54.38	119.93
373	24.49	26.04	1.12	-0.19	54.21	119.02
374	24.54	25.44	1.03	-0.19	53.86	118.40
375	24.62	25.94	0.98	-0.10	52.20	118.05
376	24.69	25.84	0.98	0.00	52.41	118.04
377	24.75	27.55	0.98	0.10	49.87	118.18
378	24.81	30.67	1.04	0.19	46.74	118.88
379	24.88	33.38	1.22	0.19	46.23	120.28
380	24.94	37.50	1.43	0.19	44.53	121.74
381	25.00	51.18	1.62	0.38	35.64	123.41
382	25.07	64.75	1.83	0.38	30.15	124.86
383	25.13	68.07	1.97	0.57	29.77	125.54
384	25.22	79.33	2.27	0.95	27.39	126.94

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.27	84.56	2.38	0.86	26.32	127.45
386	25.33	88.78	2.46	0.86	25.50	127.81
387	25.40	92.70	2.46	0.76	24.39	127.90
388	25.48	92.70	2.29	0.76	23.57	127.39
389	25.53	90.69	2.20	0.76	23.63	127.03
390	25.60	84.96	2.19	0.67	25.27	126.83
391	25.67	81.74	2.16	0.67	26.17	126.65
392	25.73	76.92	2.15	0.67	27.80	126.47
393	25.79	68.67	2.14	0.67	31.02	126.16
394	25.87	56.71	2.15	0.00	37.18	125.73
395	25.92	54.29	2.15	-0.19	38.72	125.63
396	26.00	45.65	2.15	-0.48	45.02	125.19
397	26.07	40.32	2.09	-0.57	49.37	124.70
398	26.12	36.80	2.04	-0.67	52.52	124.27
399	26.19	32.68	1.89	-0.76	56.08	123.44
400	26.25	29.46	1.74	-0.67	59.02	122.59
401	26.33	27.65	1.61	-0.76	60.37	121.87
402	26.39	27.65	1.55	-0.67	59.61	121.57
403	26.45	28.76	1.54	-0.57	57.77	121.60
404	26.52	30.57	1.52	-0.57	54.99	121.65
405	26.58	32.78	1.49	-0.57	51.89	121.71
406	26.66	36.90	1.62	-0.57	48.70	122.58
407	26.72	40.52	1.69	-0.57	45.96	123.15
408	26.78	45.65	1.74	-0.48	41.97	123.64
409	26.84	55.70	1.76	-0.48	35.31	124.21
410	26.91	61.84	1.75	-0.57	32.00	124.44
411	26.97	65.76	1.77	-0.67	30.36	124.68
412	27.05	71.39	1.83	-0.67	28.41	125.09
413	27.10	75.91	1.85	-0.67	26.90	125.34
414	27.17	81.94	1.78	-0.67	24.43	125.24
415	27.24	87.57	1.70	-0.67	22.26	125.07
416	27.30	91.19	1.68	-0.67	21.17	125.07
417	27.37	94.81	1.69	-0.67	20.34	125.20
418	27.46	98.03	1.76	-0.67	20.07	125.61
419	27.51	100.24	1.78	-0.57	19.70	125.74
420	27.57	103.16	1.80	-0.57	19.17	125.88
421	27.64	106.38	1.82	-0.67	18.62	126.03
422	27.70	108.09	1.83	-0.57	18.37	126.12
423	27.76	108.69	1.86	-0.67	18.40	126.23
424	27.82	109.59	1.90	-0.57	18.48	126.42
425	27.91	109.69	1.97	-0.57	18.88	126.70
426	27.96	110.40	2.01	-0.67	18.97	126.87
427	28.03	111.20	2.06	-0.57	19.06	127.04
428	28.09	111.00	2.08	-0.67	19.22	127.11
429	28.16	110.20	2.10	-0.57	19.51	127.16
430	28.23	107.28	2.10	-0.57	20.14	127.09
431	28.29	103.96	2.08	-0.57	20.83	126.97
432	28.36	98.33	2.06	-0.57	22.06	126.75

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	28.45	94.11	1.98	-0.67	22.74	126.37
434	28.48	91.09	1.95	-0.67	23.36	126.16
435	28.55	88.98	1.85	-0.67	23.34	125.70
436	28.61	87.27	1.75	-0.67	23.22	125.25
437	28.68	86.67	1.71	-0.67	23.15	125.06
438	28.74	86.17	1.66	-0.57	23.03	124.86
439	28.81	82.45	1.63	-0.32	23.98	124.63
440	28.87	65.47	1.64	-0.26	30.47	124.09
441	28.94	67.97	1.64	0.00	29.38	124.18
442	29.03	53.59	1.61	0.00	36.67	123.46
443	29.08	44.74	1.59	0.00	42.94	122.92
444	29.16	34.39	1.55	0.00	52.73	122.09
445	29.22	29.76	1.47	0.00	57.89	121.35
446	29.27	26.44	1.40	0.00	62.39	120.74
447	29.35	22.82	1.28	-0.10	67.68	119.72
448	29.43	21.82	1.16	-0.10	67.94	118.89
449	29.47	20.81	1.10	-0.10	69.29	118.40
450	29.53	19.91	1.04	0.10	70.42	117.88
451	29.60	19.61	0.97	0.19	69.84	117.34
452	29.67	19.71	0.93	0.29	68.79	117.04
453	29.73	19.81	0.91	0.38	68.04	116.85
454	29.80	19.30	0.88	0.38	68.79	116.55
455	29.87	18.40	0.86	0.38	70.95	116.31
456	29.93	17.90	0.86	0.29	72.36	116.21
457	30.00	17.80	0.86	0.29	72.64	116.17
458	30.07	17.70	0.85	0.29	72.91	116.12
459	30.12	17.70	0.88	0.29	73.55	116.33
460	30.20	18.20	0.93	0.38	73.38	116.83
461	30.27	18.80	0.98	0.38	72.83	117.29
462	30.32	19.20	1.01	0.38	72.48	117.59
463	30.40	20.01	1.09	0.38	71.96	118.23
464	30.46	20.21	1.15	0.38	72.67	118.66
465	30.52	19.81	1.19	0.38	74.41	118.82
466	30.59	19.71	1.21	0.38	75.09	118.92
467	30.65	18.80	1.21	0.38	77.81	118.84
468	30.71	18.50	1.21	0.38	78.64	118.76
469	30.79	18.00	1.20	0.38	80.18	118.67
470	30.85	17.90	1.19	0.38	80.28	118.56
471	30.96	17.80	0.93	0.38	75.23	116.73
472	31.00	18.20	1.04	0.38	76.55	117.63
473	31.04	18.40	1.10	0.38	77.21	118.07
474	31.11	18.70	1.12	0.38	76.77	118.23
475	31.18	18.60	1.13	0.38	77.35	118.29
476	31.25	18.40	1.12	0.48	77.80	118.19
477	31.30	18.70	1.11	0.48	76.80	118.18
478	31.38	19.61	1.10	0.48	74.20	118.26
479	31.44	19.66	1.10	0.57	74.07	118.24
480	31.50	19.91	1.06	0.57	72.62	117.99

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	31.57	19.71	1.08	0.57	73.55	118.08
482	31.63	20.91	1.16	0.57	72.12	118.77
483	31.70	21.62	1.22	0.57	71.44	119.20
484	31.79	21.92	1.26	0.57	71.60	119.50
485	31.83	22.47	1.28	0.57	70.62	119.65
486	31.90	23.33	1.29	0.67	68.92	119.79
487	31.97	23.13	1.26	0.67	69.06	119.65
488	32.03	22.02	1.24	0.67	71.17	119.37
489	32.10	21.62	1.21	0.67	71.70	119.16
490	32.16	21.52	1.17	0.76	71.38	118.94
491	32.23	21.62	1.17	0.76	71.06	118.90
492	32.30	21.72	1.17	0.76	70.92	118.92
493	32.36	21.62	1.17	0.76	71.20	118.90
494	32.46	20.91	1.17	0.76	73.01	118.82
495	32.51	20.91	1.17	0.76	73.08	118.82
496	32.56	21.42	1.18	0.76	72.03	118.94
497	32.65	21.92	1.21	0.76	71.51	119.20
498	32.68	24.83	1.23	0.76	65.69	119.64
499	32.76	27.15	1.28	0.76	62.30	120.15
500	32.84	30.77	1.38	0.76	58.16	121.00
501	32.89	31.37	1.44	0.76	58.08	121.34
502	32.95	31.67	1.50	0.76	58.49	121.67
503	33.01	30.67	1.50	0.76	60.01	121.61
504	33.10	27.65	1.43	0.76	63.81	120.97
505	33.15	26.04	1.40	0.76	66.40	120.71
506	33.24	24.53	1.35	0.76	68.53	120.25
507	33.29	22.92	1.29	0.76	71.09	119.76
508	33.35	20.71	1.18	0.76	74.69	118.90
509	33.40	19.51	1.13	0.76	77.01	118.43
510	33.47	18.80	1.09	0.76	78.34	118.08
511	33.55	17.50	1.04	0.76	81.36	117.54
512	33.65	16.39	0.98	0.76	84.00	116.95
513	33.66	16.19	0.97	0.76	84.49	116.84
514	33.74	16.09	0.92	0.76	83.75	116.45
515	33.84	15.69	0.87	0.76	84.04	115.96
516	33.88	15.69	0.86	0.76	83.80	115.86
517	33.93	15.69	0.84	0.86	83.42	115.73
518	33.99	15.69	0.83	0.86	83.10	115.60
519	34.07	15.48	0.81	0.86	83.56	115.43
520	34.12	15.48	0.80	0.86	83.43	115.37
521	34.19	15.48	0.80	0.86	83.46	115.35
522	34.28	15.79	0.82	0.86	82.83	115.55
523	34.32	15.89	0.83	0.86	82.87	115.69
524	34.40	16.29	0.87	0.86	82.53	116.10
525	34.48	16.59	0.86	0.86	81.19	116.02
526	34.52	16.79	0.84	0.86	80.10	115.91
527	34.58	17.70	0.87	0.86	77.74	116.23
528	34.68	22.82	0.86	0.86	64.59	116.84

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	34.72	26.64	0.93	0.95	58.85	117.78
530	34.81	30.97	1.13	0.86	55.60	119.51
531	34.85	26.04	1.20	0.86	64.57	119.53
532	34.92	29.26	1.31	0.38	60.93	120.48
533	34.98	26.04	1.37	0.29	67.43	120.55
534	35.05	25.04	1.37	0.29	69.44	120.45
535	35.12	24.43	1.37	0.29	70.77	120.40
536	35.18	25.54	1.38	0.38	68.71	120.55
537	35.26	26.64	1.46	0.38	67.72	121.02
538	35.31	27.85	1.50	0.48	66.23	121.36
539	35.41	32.48	1.64	0.48	60.80	122.36
540	35.47	36.80	1.70	0.48	56.09	122.96
541	35.51	43.54	1.75	0.48	49.72	123.56
542	35.58	56.91	1.82	0.48	40.43	124.52
543	35.63	68.37	1.87	0.48	34.40	125.15
544	35.71	78.93	1.90	0.48	30.12	125.64
545	35.78	83.96	1.97	0.48	28.77	126.05
546	35.84	82.45	2.03	0.48	29.70	126.20
547	35.90	76.72	2.06	0.48	32.20	126.14
548	35.98	67.37	2.10	0.38	36.88	125.97
549	36.05	60.53	2.08	0.38	40.63	125.64
550	36.10	53.19	2.05	0.38	45.17	125.21
551	36.20	40.92	1.92	0.38	54.37	124.11
552	36.25	37.00	1.82	0.48	57.66	123.46
553	36.30	31.77	1.70	0.38	63.27	122.60
554	36.35	29.76	1.59	0.38	64.96	121.92
555	36.45	27.65	1.37	0.38	65.58	120.65
556	36.48	27.35	1.30	0.38	65.19	120.27
557	36.55	27.25	1.26	0.38	64.75	120.01
558	36.63	27.40	1.29	0.38	65.08	120.22
559	36.69	26.85	1.33	0.48	66.70	120.39
560	36.75	27.45	1.40	0.48	66.61	120.79
561	36.84	28.45	1.50	0.48	66.37	121.40
562	36.89	29.36	1.57	0.48	65.84	121.82
563	36.95	30.06	1.68	0.48	66.12	122.38
564	37.05	32.07	1.86	0.57	65.18	123.29
565	37.08	33.98	1.93	0.57	63.23	123.70
566	37.14	36.00	2.01	0.57	61.42	124.13
567	37.23	38.21	2.15	0.57	60.08	124.75
568	37.28	39.31	2.23	0.57	59.55	125.08
569	37.34	40.12	2.29	0.57	59.28	125.35
570	37.43	42.23	2.42	0.57	58.10	125.85
571	37.48	43.44	2.47	0.57	57.38	126.10
572	37.53	44.74	2.44	0.57	55.90	126.07
573	37.61	47.66	2.12	0.57	50.76	125.18
574	37.67	48.87	2.23	0.57	50.72	125.63
575	37.73	53.29	2.25	0.57	47.55	125.89
576	37.82	61.33	2.26	0.67	42.61	126.29

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	37.88	69.48	2.26	0.67	38.02	126.58
578	37.93	70.58	2.26	0.86	37.48	126.62
579	38.00	87.78	2.27	0.76	30.34	127.18
580	38.08	93.00	2.29	0.76	28.73	127.38
581	38.12	98.63	2.30	0.76	27.06	127.55
582	38.20	106.78	2.32	0.76	24.98	127.81
583	38.29	115.73	2.37	0.76	23.13	128.17
584	38.33	120.55	2.41	0.76	22.31	128.40
585	38.43	130.01	2.69	0.76	21.72	129.39
586	38.48	132.72	2.78	0.86	21.60	129.67
587	38.52	134.93	2.86	0.86	21.55	129.93
588	38.59	136.64	3.03	0.86	21.95	130.38
589	38.68	137.24	3.21	0.86	22.58	130.82
590	38.72	138.25	3.29	0.86	22.71	131.02
591	38.79	141.27	3.44	0.86	22.72	131.38
592	38.87	145.39	3.60	0.86	22.57	131.78
593	38.92	150.42	3.73	0.86	22.19	132.14
594	38.98	155.84	3.87	0.86	21.75	132.48
595	39.05	162.88	4.08	0.95	21.35	132.98
596	39.12	167.91	4.24	0.95	21.09	133.34
597	39.17	171.43	4.40	0.95	21.04	133.65
598	39.26	174.45	4.56	0.95	21.11	133.97
599	39.32	175.35	4.63	1.05	21.18	134.09
600	39.37	175.75	4.68	1.05	21.27	134.17
601	39.46	175.75	4.72	1.05	21.41	134.24
602	39.52	175.75	4.73	1.05	21.45	134.25
603	39.57	174.65	4.72	1.05	21.61	134.22
604	39.63	173.44	4.72	1.05	21.78	134.20
605	39.72	172.54	4.70	1.05	21.89	134.15
606	39.77	172.03	4.68	1.05	21.92	134.12
607	39.85	169.22	4.64	1.05	22.27	134.02
608	39.91	167.81	4.61	1.05	22.41	133.95
609	39.96	165.80	4.56	1.14	22.58	133.83
610	40.06	163.79	4.43	1.14	22.58	133.61
611	40.11	160.87	4.38	1.14	22.89	133.47
612	40.16	157.15	4.31	1.14	23.32	133.30
613	40.26	148.51	4.10	1.14	24.19	132.80
614	40.30	144.18	4.03	1.14	24.78	132.60
615	40.36	138.15	3.92	1.14	25.59	132.29
616	40.44	130.11	3.74	1.24	26.65	131.79
617	40.50	126.89	3.52	1.24	26.58	131.30
618	40.55	122.26	3.13	1.24	26.03	130.33
619	40.62	117.03	3.16	1.24	27.44	130.30
620	40.68	113.11	3.02	1.24	27.86	129.89
621	40.75	109.19	2.88	1.24	28.28	129.46
622	40.84	106.68	2.80	1.24	28.61	129.19
623	40.90	105.52	2.78	1.24	28.87	129.11
624	40.96	103.86	2.77	1.33	29.34	129.06

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	41.04	104.37	2.78	1.33	29.26	129.09
626	41.09	104.16	2.80	1.33	29.44	129.13
627	41.15	104.27	2.82	1.33	29.54	129.19
628	41.22	105.77	2.83	1.33	29.16	129.24
629	41.30	107.58	2.80	1.33	28.57	129.23
630	41.35	109.09	2.78	1.33	28.06	129.20
631	41.41	110.30	2.75	1.33	27.62	129.16
632	41.48	111.91	2.74	1.33	27.14	129.15
633	41.55	112.91	2.74	1.33	26.90	129.17
634	41.62	113.42	2.73	1.33	26.79	129.17
635	41.68	113.11	2.73	1.33	26.85	129.14
636	41.74	112.61	2.72	1.33	26.97	129.11
637	41.80	112.21	2.73	1.33	27.14	129.13
638	41.88	112.21	2.73	1.33	27.16	129.12
639	41.95	112.71	2.72	1.43	27.05	129.13
640	42.00	113.01	2.72	1.43	26.97	129.13
641	42.08	112.11	2.73	1.43	27.29	129.14
642	42.15	110.70	2.74	1.43	27.74	129.12
643	42.22	107.28	2.74	1.43	28.73	129.06
644	42.28	103.46	2.75	1.43	29.90	128.98
645	42.34	98.43	2.75	1.43	31.53	128.88
646	42.39	95.42	2.77	1.43	32.63	128.83
647	42.48	94.21	2.78	1.43	33.15	128.83
648	42.53	94.61	2.77	1.43	33.02	128.83
649	42.59	96.42	2.78	1.43	32.48	128.91
650	42.68	98.74	2.84	1.43	32.03	129.11
651	42.72	100.44	2.84	1.43	31.51	129.16
652	42.79	106.18	2.83	1.43	29.70	129.25
653	42.87	113.62	2.76	1.43	27.33	129.23
654	42.92	116.33	2.68	1.43	26.29	129.08
655	43.00	117.64	2.56	1.43	25.38	128.77
656	43.05	118.14	2.55	1.43	25.26	128.76
657	43.13	121.36	2.53	1.33	24.45	128.78
658	43.22	123.87	2.31	1.33	22.80	128.15
659	43.27	122.16	2.19	1.24	22.53	127.71
660	43.33	116.33	2.08	1.14	23.28	127.24
661	43.37	110.70	2.05	1.14	24.44	127.00
662	43.47	94.71	1.94	-0.19	28.35	126.23
663	43.52	86.27	1.94	-0.76	31.28	126.00
664	43.57	73.40	2.07	-1.43	37.84	126.07
665	43.66	55.20	2.38	-1.72	50.49	126.39
666	43.72	49.37	2.40	-1.72	55.21	126.18
667	43.77	43.03	2.38	-1.72	61.13	125.79
668	43.83	38.61	2.30	-1.72	65.53	125.28
669	43.90	33.98	2.14	-1.68	70.31	124.43
670	43.97	40.32	1.92	-1.68	60.04	124.07
671	44.03	40.02	1.79	-1.68	59.03	123.51
672	44.13	37.00	1.53	-1.62	59.69	122.17

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	44.17	34.69	1.41	-1.62	61.22	121.45
674	44.23	31.57	1.23	-1.62	63.11	120.22
675	44.33	27.85	1.08	-1.62	66.74	118.94
676	44.37	26.14	1.08	-1.62	70.01	118.81
677	44.43	23.33	1.08	-1.62	76.16	118.54
678	44.52	20.61	1.21	-1.62	85.80	119.03
679	44.57	19.41	1.33	-1.62	91.84	119.58
680	44.62	19.61	1.46	-1.62	93.65	120.32
681	44.72	29.66	1.73	-1.62	73.38	122.57
682	44.76	47.96	1.87	-1.52	52.55	124.30
683	44.83	80.94	2.11	-1.62	35.30	126.47
684	44.92	103.66	2.49	-1.62	29.51	128.25
685	44.97	115.33	2.67	-1.62	27.27	129.04
686	45.02	116.83	2.82	-1.62	27.67	129.48
687	45.09	117.34	2.98	-2.76	28.33	129.89
688	45.16	119.35	3.00	-3.91	27.93	129.97
689	45.22	121.86	2.98	-5.15	27.24	129.98
690	45.29	126.89	2.93	-6.86	25.87	129.96
691	45.37	127.49	2.93	-8.01	25.76	129.97
692	45.41	121.16	2.99	-8.67	27.53	129.98
693	45.47	104.57	3.24	-9.72	33.41	130.20
694	45.56	77.42	3.02	-9.53	42.84	128.97
695	45.62	62.14	2.82	-9.72	49.83	127.92
696	45.70	49.17	2.55	-8.96	57.71	126.61
697	45.75	44.64	2.47	-8.77	61.42	126.14
698	45.81	35.39	2.42	-8.48	72.27	125.42
699	45.90	36.50	2.32	-8.96	69.84	125.18
700	45.95	41.73	2.28	-9.05	63.07	125.40
701	46.01	51.68	2.21	-8.67	53.17	125.71
702	46.10	61.84	2.13	-8.77	45.55	125.85
703	46.15	64.05	2.12	-8.77	44.25	125.91
704	46.21	66.66	2.12	-8.77	42.84	126.00
705	46.29	71.09	2.20	-9.15	41.18	126.42
706	46.33	73.20	2.25	-9.15	40.57	126.67
707	46.41	79.53	2.33	-8.86	38.30	127.13
708	46.47	83.96	2.41	-9.05	36.90	127.51
709	46.53	85.16	2.12	-9.43	34.44	126.61
710	46.59	86.57	1.90	-9.10	32.27	125.84
711	46.66	89.28	1.99	-9.15	31.93	126.25
712	46.75	93.81	2.10	-10.01	31.15	126.78
713	46.79	95.22	2.15	-9.91	31.03	127.00
714	46.85	94.01	2.24	-9.78	32.01	127.24
715	46.92	94.21	2.27	-9.78	32.17	127.35
716	47.00	99.64	2.28	-9.70	30.46	127.52
717	47.05	99.44	2.28	-10.01	30.56	127.53
718	47.12	97.63	2.28	-9.63	31.14	127.46
719	47.20	94.31	2.26	-10.01	32.21	127.32
720	47.26	90.99	2.22	-9.58	33.19	127.11

:: Field input data :: (continued)						
Point ID	Depth (ft)	q _c (tsf)	f _s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	47.32	87.78	2.18	-9.53	34.16	126.88
722	47.39	83.15	2.10	-9.72	35.52	126.47
723	47.47	78.22	2.01	-10.01	37.12	126.00
724	47.51	72.39	2.00	-10.10	39.77	125.80
725	47.59	63.65	2.02	-9.91	44.43	125.56
726	47.65	57.21	2.04	-10.29	48.58	125.36
727	47.71	53.49	2.13	-9.53	52.00	125.52
728	47.79	44.64	2.13	-10.01	59.75	125.07
729	47.85	41.83	2.14	-10.01	62.83	124.94
730	47.91	38.91	2.15	-9.91	66.43	124.81
731	48.00	50.88	2.11	-10.01	53.96	125.30
732	48.05	68.47	2.10	-10.20	42.61	126.02
733	48.10	100.44	2.16	-9.34	29.88	127.14
734	48.19	147.70	2.20	-9.53	19.32	128.21
735	48.25	163.18	2.20	-9.39	17.02	128.47
736	48.30	170.22	2.21	-9.43	16.13	128.61
737	48.39	182.99	2.17	-9.24	14.43	128.64
738	48.43	186.51	2.16	-9.29	14.02	128.66
739	48.50	192.14	2.21	-9.15	13.64	128.90
740	48.59	195.46	2.30	-9.34	13.66	129.22
741	48.64	196.57	2.32	-9.34	13.66	129.32
742	48.70	197.47	2.33	-9.24	13.62	129.36
743	48.79	196.16	2.33	-8.58	13.75	129.33
744	48.83	194.86	2.32	-8.20	13.88	129.30
745	48.89	193.05	2.30	-8.20	13.97	129.19
746	48.95	189.33	2.27	-8.20	14.29	129.07
747	49.02	185.61	2.25	-8.20	14.62	128.95
748	49.11	177.76	2.22	-8.20	15.44	128.75
749	49.19	172.43	2.23	-7.72	16.14	128.69
750	49.22	168.61	2.23	-7.72	16.66	128.65
751	49.28	162.78	2.23	-7.72	17.48	128.57
752	49.35	155.74	2.20	-7.72	18.39	128.36
753	49.42	149.51	2.18	-7.43	19.27	128.18
754	49.48	143.38	2.16	-7.34	20.24	128.01
755	49.56	135.84	2.19	-7.15	21.82	127.99
756	49.63	132.42	2.17	-7.24	22.41	127.86
757	49.68	129.40	2.01	-7.05	22.16	127.25
758	49.74	127.49	2.08	-6.96	22.95	127.44
759	49.83	125.28	2.14	-6.77	23.84	127.64
760	49.87	122.87	2.16	-6.58	24.51	127.66
761	49.97	119.05	2.23	-6.58	25.83	127.79
762	50.03	119.15	2.26	-6.58	25.99	127.89
763	50.08	118.64	0.00	-6.58	100.00	87.36
764	50.14	119.25	0.00	-6.38	100.00	87.36
765	50.23	120.25	0.00	-6.38	100.00	87.36
766	50.27	121.06	0.00	-6.38	100.00	87.36
767	50.33	122.26	0.00	-6.48	100.00	87.36
768	50.41	124.48	0.00	-6.58	100.00	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c :	Measured cone resistance (tsf)
f_s :	Sleeve friction resistance (tsf)
u :	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
1	0.10	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
2	0.14	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
3	0.21	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
4	0.26	0.01	0.00	0.01	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
5	0.34	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
6	0.40	0.02	0.00	0.02	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
7	0.49	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
8	0.53	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
9	0.59	0.03	0.00	0.03	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
10	0.66	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
11	0.73	0.04	0.00	0.04	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
12	0.81	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
13	0.87	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
14	0.92	0.05	0.00	0.05	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
15	0.99	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
16	1.05	0.06	0.00	0.06	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
17	1.15	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
18	1.20	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
19	1.26	0.07	0.00	0.07	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
20	1.32	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
21	1.39	0.08	0.00	0.08	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
22	1.46	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
23	1.51	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
24	1.58	0.09	0.00	0.09	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
25	1.66	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
26	1.71	0.10	0.00	0.10	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
27	1.79	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
28	1.84	0.11	0.00	0.11	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
29	1.93	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
30	1.98	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
31	2.04	0.12	0.00	0.12	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
32	2.11	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
33	2.17	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
34	2.24	0.13	0.00	0.13	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
35	2.32	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
36	2.38	0.14	0.00	0.14	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
37	2.43	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
38	2.52	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
39	2.56	0.15	0.00	0.15	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
40	2.64	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
41	2.69	0.16	0.00	0.16	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
42	2.78	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
43	2.83	0.17	0.00	0.17	1.00	0.500	1.05	0.475	1.10	1.30	2.000	No
44	2.89	0.17	0.00	0.17	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
45	2.95	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
46	3.02	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
47	3.09	0.18	0.00	0.18	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
48	3.15	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
49	3.22	0.19	0.00	0.19	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
50	3.29	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
51	3.35	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
52	3.41	0.20	0.00	0.20	1.00	0.500	1.05	0.474	1.10	1.30	2.000	No
53	3.52	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
54	3.55	0.21	0.00	0.21	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
55	3.61	0.22	0.00	0.22	1.00	0.499	1.05	0.474	1.10	1.30	2.000	No
56	3.71	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
57	3.75	0.22	0.00	0.22	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
58	3.81	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
59	3.90	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
60	3.95	0.23	0.00	0.23	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
61	4.01	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
62	4.09	0.24	0.00	0.24	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
63	4.15	0.25	0.00	0.25	1.00	0.499	1.05	0.473	1.10	1.30	2.000	No
64	4.21	0.25	0.00	0.25	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
65	4.29	0.25	0.00	0.25	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
66	4.34	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
67	4.41	0.26	0.00	0.26	1.00	0.498	1.05	0.473	1.10	1.30	2.000	No
68	4.46	0.26	0.00	0.26	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
69	4.55	0.27	0.00	0.27	1.00	0.498	1.05	0.472	1.10	1.30	2.000	No
70	4.61	0.27	0.00	0.27	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
71	4.67	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
72	4.75	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
73	4.79	0.28	0.00	0.28	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
74	4.87	0.29	0.00	0.29	0.99	0.498	1.05	0.472	1.10	1.30	2.000	No
75	4.93	0.29	0.00	0.29	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
76	4.99	0.29	0.00	0.29	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
77	5.06	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
78	5.14	0.30	0.00	0.30	0.99	0.497	1.05	0.472	1.10	1.30	2.000	No
79	5.19	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
80	5.25	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
81	5.33	0.31	0.00	0.31	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
82	5.38	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
83	5.45	0.32	0.00	0.32	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
84	5.52	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
85	5.59	0.33	0.00	0.33	0.99	0.497	1.05	0.471	1.10	1.30	2.000	No
86	5.64	0.33	0.00	0.33	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
87	5.72	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
88	5.78	0.34	0.00	0.34	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
89	5.85	0.35	0.00	0.35	0.99	0.496	1.05	0.471	1.10	1.30	2.000	No
90	5.92	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
91	5.98	0.35	0.00	0.35	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
92	6.04	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
93	6.11	0.36	0.00	0.36	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
94	6.17	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
95	6.24	0.37	0.00	0.37	0.99	0.496	1.05	0.470	1.10	1.30	2.000	No
96	6.32	0.37	0.00	0.37	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
97	6.38	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
98	6.44	0.38	0.00	0.38	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
99	6.51	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
100	6.58	0.39	0.00	0.39	0.99	0.495	1.05	0.470	1.10	1.30	2.000	No
101	6.66	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
102	6.71	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
103	6.77	0.40	0.00	0.40	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
104	6.83	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
105	6.92	0.41	0.00	0.41	0.99	0.495	1.05	0.469	1.10	1.30	2.000	No
106	6.97	0.41	0.00	0.41	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
107	7.03	0.42	0.00	0.42	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
108	7.10	0.42	0.00	0.42	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
109	7.16	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
110	7.22	0.43	0.00	0.43	0.99	0.494	1.05	0.469	1.10	1.30	2.000	No
111	7.31	0.44	0.00	0.44	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
112	7.36	0.44	0.00	0.44	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
113	7.42	0.44	0.00	0.44	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
114	7.49	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
115	7.55	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
116	7.62	0.45	0.00	0.45	0.99	0.494	1.05	0.468	1.10	1.30	2.000	No
117	7.71	0.46	0.00	0.46	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
118	7.75	0.46	0.00	0.46	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
119	7.83	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
120	7.88	0.47	0.00	0.47	0.99	0.493	1.05	0.468	1.10	1.30	2.000	No
121	7.95	0.48	0.00	0.48	0.98	0.493	1.05	0.468	1.10	1.30	2.000	No
122	8.01	0.48	0.00	0.48	0.98	0.493	1.05	0.468	1.10	1.30	0.559	No
123	8.09	0.48	0.00	0.48	0.98	0.496	1.05	0.470	1.10	1.30	0.562	No
124	8.14	0.49	0.00	0.48	0.98	0.497	1.05	0.472	1.10	1.30	0.565	No
125	8.24	0.49	0.01	0.49	0.98	0.500	1.05	0.474	1.10	1.30	0.569	No
126	8.29	0.50	0.01	0.49	0.98	0.501	1.05	0.476	1.10	1.30	0.571	No
127	8.34	0.50	0.01	0.49	0.98	0.503	1.05	0.477	1.10	1.30	0.573	No
128	8.41	0.50	0.01	0.49	0.98	0.505	1.05	0.479	1.10	1.30	0.575	No
129	8.49	0.51	0.02	0.49	0.98	0.507	1.05	0.481	1.10	1.30	0.579	No
130	8.53	0.51	0.02	0.49	0.98	0.509	1.05	0.482	1.10	1.30	0.581	No
131	8.60	0.52	0.02	0.50	0.98	0.511	1.05	0.484	1.10	1.30	0.584	No
132	8.67	0.52	0.02	0.50	0.98	0.512	1.05	0.486	1.10	1.30	0.587	No
133	8.73	0.52	0.02	0.50	0.98	0.514	1.05	0.488	1.10	1.30	0.589	No
134	8.80	0.53	0.02	0.50	0.98	0.516	1.05	0.489	1.10	1.30	0.594	No
135	8.87	0.53	0.03	0.50	0.98	0.518	1.05	0.491	1.09	1.30	0.598	No
136	8.93	0.54	0.03	0.51	0.98	0.519	1.05	0.493	1.09	1.30	0.601	No
137	9.02	0.54	0.03	0.51	0.98	0.522	1.05	0.495	1.09	1.30	0.605	No
138	9.07	0.54	0.03	0.51	0.98	0.523	1.05	0.496	1.09	1.30	0.608	No
139	9.13	0.55	0.04	0.51	0.98	0.525	1.05	0.498	1.09	1.30	0.609	No
140	9.20	0.55	0.04	0.51	0.98	0.527	1.05	0.500	1.09	1.30	0.612	No
141	9.25	0.56	0.04	0.52	0.98	0.528	1.05	0.501	1.09	1.30	0.614	No
142	9.32	0.56	0.04	0.52	0.98	0.530	1.05	0.502	1.09	1.30	0.618	No
143	9.39	0.56	0.04	0.52	0.98	0.532	1.05	0.504	1.09	1.30	0.621	No
144	9.46	0.57	0.05	0.52	0.98	0.533	1.05	0.506	1.08	1.30	0.625	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
145	9.52	0.57	0.05	0.52	0.98	0.535	1.05	0.507	1.08	1.30	0.629	No
146	9.61	0.58	0.05	0.53	0.98	0.537	1.05	0.509	1.08	1.30	0.634	No
147	9.66	0.58	0.05	0.53	0.98	0.538	1.05	0.511	1.08	1.30	0.637	No
148	9.71	0.58	0.05	0.53	0.98	0.540	1.05	0.512	1.08	1.30	0.640	No
149	9.78	0.59	0.06	0.53	0.98	0.541	1.05	0.513	1.07	1.30	0.643	No
150	9.86	0.59	0.06	0.53	0.98	0.543	1.05	0.515	1.07	1.30	0.645	No
151	9.91	0.59	0.06	0.53	0.98	0.544	1.05	0.516	1.07	1.30	0.647	No
152	9.97	0.60	0.06	0.54	0.98	0.546	1.05	0.518	1.07	1.30	0.649	No
153	10.06	0.60	0.06	0.54	0.98	0.548	1.05	0.520	1.07	1.30	0.650	No
154	10.11	0.61	0.07	0.54	0.98	0.549	1.05	0.521	1.08	1.30	0.650	No
155	10.17	0.61	0.07	0.54	0.98	0.551	1.05	0.522	1.08	1.30	0.651	No
156	10.25	0.61	0.07	0.54	0.98	0.552	1.05	0.524	1.08	1.30	0.652	No
157	10.31	0.62	0.07	0.55	0.98	0.554	1.05	0.525	1.08	1.30	0.652	No
158	10.37	0.62	0.07	0.55	0.98	0.555	1.05	0.526	1.08	1.30	0.652	No
159	10.44	0.63	0.08	0.55	0.98	0.557	1.05	0.528	1.08	1.30	0.652	No
160	10.50	0.63	0.08	0.55	0.98	0.558	1.05	0.529	1.08	1.30	0.653	No
161	10.57	0.63	0.08	0.55	0.98	0.559	1.05	0.531	1.08	1.30	0.654	No
162	10.64	0.64	0.08	0.56	0.98	0.561	1.05	0.532	1.08	1.30	0.655	No
163	10.70	0.64	0.08	0.56	0.98	0.562	1.05	0.533	1.08	1.30	0.656	No
164	10.77	0.65	0.09	0.56	0.98	0.564	1.05	0.535	1.08	1.30	0.659	No
165	10.85	0.65	0.09	0.56	0.98	0.565	1.05	0.536	1.08	1.30	0.659	No
166	10.90	0.65	0.09	0.56	0.98	0.566	1.05	0.537	1.08	1.30	0.660	No
167	10.97	0.66	0.09	0.57	0.98	0.568	1.05	0.539	1.08	1.30	0.662	No
168	11.03	0.66	0.09	0.57	0.97	0.569	1.05	0.540	1.08	1.30	0.663	No
169	11.09	0.67	0.10	0.57	0.97	0.571	1.05	0.541	1.08	1.30	0.664	No
170	11.17	0.67	0.10	0.57	0.97	0.572	1.05	0.543	1.08	1.30	0.666	No
171	11.26	0.68	0.10	0.57	0.97	0.574	1.05	0.544	1.08	1.30	0.668	No
172	11.30	0.68	0.10	0.58	0.97	0.575	1.05	0.545	1.08	1.30	0.669	No
173	11.36	0.68	0.10	0.58	0.97	0.576	1.05	0.546	1.08	1.30	0.671	No
174	11.42	0.69	0.11	0.58	0.97	0.577	1.05	0.547	1.08	1.30	0.674	No
175	11.50	0.69	0.11	0.58	0.97	0.579	1.05	0.549	1.08	1.30	0.677	No
176	11.56	0.69	0.11	0.58	0.97	0.580	1.05	0.550	1.08	1.30	0.681	No
177	11.62	0.70	0.11	0.58	0.97	0.581	1.05	0.551	1.07	1.30	0.684	No
178	11.69	0.70	0.12	0.59	0.97	0.582	1.05	0.552	1.07	1.30	0.688	No
179	11.76	0.71	0.12	0.59	0.97	0.583	1.05	0.553	1.07	1.30	0.692	No
180	11.83	0.71	0.12	0.59	0.97	0.585	1.05	0.555	1.07	1.30	0.695	No
181	11.88	0.71	0.12	0.59	0.97	0.586	1.05	0.556	1.07	1.30	0.697	No
182	11.95	0.72	0.12	0.59	0.97	0.587	1.05	0.557	1.07	1.30	0.699	No
183	12.01	0.72	0.13	0.60	0.97	0.588	1.05	0.558	1.07	1.30	0.701	No
184	12.08	0.73	0.13	0.60	0.97	0.590	1.05	0.559	1.07	1.30	0.703	No
185	12.14	0.73	0.13	0.60	0.97	0.591	1.05	0.560	1.07	1.30	0.705	No
186	12.23	0.73	0.13	0.60	0.97	0.592	1.05	0.562	1.06	1.30	0.708	No
187	12.28	0.74	0.13	0.60	0.97	0.593	1.05	0.562	1.06	1.30	0.709	No
188	12.35	0.74	0.14	0.61	0.97	0.594	1.05	0.564	1.06	1.30	0.711	No
189	12.40	0.75	0.14	0.61	0.97	0.595	1.05	0.564	1.06	1.30	0.712	No
190	12.47	0.75	0.14	0.61	0.97	0.596	1.05	0.566	1.06	1.30	0.713	No
191	12.54	0.75	0.14	0.61	0.97	0.598	1.05	0.567	1.06	1.30	0.714	No
192	12.60	0.76	0.14	0.61	0.97	0.599	1.05	0.568	1.06	1.30	0.714	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR _{eq}	K_σ	User FS	CSR*	Belongs to transition
193	12.70	0.76	0.15	0.62	0.97	0.600	1.05	0.569	1.06	1.30	0.716	No
194	12.75	0.77	0.15	0.62	0.97	0.601	1.05	0.570	1.06	1.30	0.718	No
195	12.80	0.77	0.15	0.62	0.97	0.602	1.05	0.571	1.06	1.30	0.719	No
196	12.87	0.77	0.15	0.62	0.97	0.603	1.05	0.572	1.06	1.30	0.720	No
197	12.93	0.78	0.15	0.62	0.97	0.604	1.05	0.573	1.06	1.30	0.721	No
198	12.99	0.78	0.16	0.63	0.97	0.605	1.05	0.574	1.06	1.30	0.721	No
199	13.06	0.79	0.16	0.63	0.97	0.606	1.05	0.575	1.06	1.30	0.721	No
200	13.14	0.79	0.16	0.63	0.97	0.607	1.05	0.576	1.07	1.30	0.722	No
201	13.19	0.79	0.16	0.63	0.97	0.608	1.05	0.577	1.07	1.30	0.722	No
202	13.26	0.80	0.16	0.63	0.97	0.609	1.05	0.578	1.07	1.30	0.723	No
203	13.32	0.80	0.17	0.64	0.97	0.610	1.05	0.579	1.06	1.30	0.725	No
204	13.40	0.81	0.17	0.64	0.97	0.611	1.05	0.580	1.06	1.30	0.726	No
205	13.46	0.81	0.17	0.64	0.97	0.612	1.05	0.581	1.06	1.30	0.728	No
206	13.53	0.81	0.17	0.64	0.97	0.613	1.05	0.582	1.06	1.30	0.729	No
207	13.58	0.82	0.17	0.64	0.97	0.614	1.05	0.583	1.06	1.30	0.730	No
208	13.68	0.82	0.18	0.65	0.97	0.616	1.05	0.584	1.06	1.30	0.733	No
209	13.73	0.83	0.18	0.65	0.97	0.616	1.05	0.585	1.06	1.30	0.734	No
210	13.79	0.83	0.18	0.65	0.97	0.617	1.05	0.585	1.06	1.30	0.737	No
211	13.88	0.84	0.18	0.65	0.96	0.619	1.05	0.587	1.06	1.30	0.739	No
212	13.92	0.84	0.18	0.65	0.96	0.619	1.05	0.587	1.06	1.30	0.740	No
213	13.98	0.84	0.19	0.66	0.96	0.620	1.05	0.588	1.06	1.30	0.741	No
214	14.05	0.85	0.19	0.66	0.96	0.621	1.05	0.589	1.06	1.30	0.740	No
215	14.13	0.85	0.19	0.66	0.96	0.622	1.05	0.590	1.06	1.30	0.741	No
216	14.17	0.85	0.19	0.66	0.96	0.623	1.05	0.591	1.06	1.30	0.741	No
217	14.24	0.86	0.19	0.66	0.96	0.624	1.05	0.591	1.06	1.30	0.740	No
218	14.33	0.86	0.20	0.67	0.96	0.625	1.05	0.593	1.06	1.30	0.741	No
219	14.37	0.87	0.20	0.67	0.96	0.625	1.05	0.593	1.06	1.30	0.740	No
220	14.45	0.87	0.20	0.67	0.96	0.626	1.05	0.594	1.06	1.30	0.740	No
221	14.53	0.88	0.20	0.67	0.96	0.627	1.05	0.595	1.06	1.30	0.740	No
222	14.57	0.88	0.21	0.67	0.96	0.628	1.05	0.596	1.07	1.30	0.739	No
223	14.64	0.88	0.21	0.68	0.96	0.629	1.05	0.597	1.07	1.30	0.739	No
224	14.72	0.89	0.21	0.68	0.96	0.630	1.05	0.597	1.07	1.30	0.739	No
225	14.76	0.89	0.21	0.68	0.96	0.630	1.05	0.598	1.07	1.30	0.739	No
226	14.85	0.90	0.21	0.68	0.96	0.632	1.05	0.599	1.07	1.30	0.739	No
227	14.90	0.90	0.22	0.68	0.96	0.632	1.05	0.600	1.07	1.30	0.739	No
228	14.96	0.90	0.22	0.69	0.96	0.633	1.05	0.600	1.07	1.30	0.739	No
229	15.03	0.91	0.22	0.69	0.96	0.634	1.05	0.601	1.07	1.30	0.739	No
230	15.10	0.91	0.22	0.69	0.96	0.635	1.05	0.602	1.07	1.30	0.740	No
231	15.16	0.92	0.22	0.69	0.96	0.635	1.05	0.603	1.07	1.30	0.740	No
232	15.24	0.92	0.23	0.70	0.96	0.636	1.05	0.604	1.07	1.30	0.742	No
233	15.31	0.93	0.23	0.70	0.96	0.637	1.05	0.604	1.07	1.30	0.743	No
234	15.36	0.93	0.23	0.70	0.96	0.638	1.05	0.605	1.07	1.30	0.744	No
235	15.45	0.93	0.23	0.70	0.96	0.639	1.05	0.606	1.06	1.30	0.748	No
236	15.50	0.94	0.23	0.70	0.96	0.639	1.05	0.606	1.06	1.30	0.751	No
237	15.55	0.94	0.24	0.70	0.96	0.640	1.05	0.607	1.06	1.30	0.754	No
238	15.66	0.95	0.24	0.71	0.96	0.641	1.05	0.608	1.06	1.30	0.761	No
239	15.69	0.95	0.24	0.71	0.96	0.642	1.05	0.608	1.06	1.30	0.763	No
240	15.75	0.95	0.24	0.71	0.96	0.642	1.05	0.609	1.05	1.30	0.767	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
241	15.82	0.96	0.24	0.71	0.96	0.643	1.05	0.610	1.05	1.30	0.770	No
242	15.91	0.96	0.25	0.72	0.96	0.644	1.05	0.611	1.05	1.30	0.774	No
243	15.96	0.97	0.25	0.72	0.96	0.645	1.05	0.611	1.05	1.30	0.777	No
244	16.02	0.97	0.25	0.72	0.96	0.645	1.05	0.612	1.05	1.30	0.780	No
245	16.08	0.97	0.25	0.72	0.96	0.646	1.05	0.613	1.05	1.30	0.783	No
246	16.14	0.98	0.25	0.72	0.96	0.647	1.05	0.613	1.05	1.30	0.786	No
247	16.22	0.98	0.26	0.73	0.96	0.648	1.05	0.614	1.04	1.30	0.790	No
248	16.30	0.99	0.26	0.73	0.96	0.648	1.05	0.615	1.04	1.30	0.793	No
249	16.34	0.99	0.26	0.73	0.96	0.649	1.05	0.615	1.04	1.30	0.797	No
250	16.42	0.99	0.26	0.73	0.96	0.650	1.05	0.616	1.04	1.30	0.797	No
251	16.50	1.00	0.27	0.73	0.95	0.651	1.05	0.617	1.04	1.30	0.799	No
252	16.54	1.00	0.27	0.74	0.95	0.651	1.05	0.617	1.04	1.30	0.798	No
253	16.62	1.01	0.27	0.74	0.95	0.652	1.05	0.618	1.04	1.30	0.799	No
254	16.70	1.01	0.27	0.74	0.95	0.653	1.05	0.619	1.04	1.30	0.799	No
255	16.74	1.01	0.27	0.74	0.95	0.653	1.05	0.619	1.04	1.30	0.799	No
256	16.80	1.02	0.27	0.74	0.95	0.654	1.05	0.620	1.04	1.30	0.796	No
257	16.87	1.02	0.28	0.75	0.95	0.654	1.05	0.620	1.05	1.30	0.791	No
258	16.94	1.03	0.28	0.75	0.95	0.655	1.05	0.621	1.05	1.30	0.787	No
259	17.01	1.03	0.28	0.75	0.95	0.655	1.05	0.622	1.05	1.30	0.777	No
260	17.09	1.04	0.28	0.75	0.95	0.656	1.05	0.622	1.05	1.30	0.773	No
261	17.14	1.04	0.29	0.75	0.95	0.657	1.05	0.623	1.06	1.30	0.769	No
262	17.23	1.05	0.29	0.76	0.95	0.657	1.05	0.624	1.06	1.30	0.764	No
263	17.28	1.05	0.29	0.76	0.95	0.658	1.05	0.624	1.06	1.30	0.763	No
264	17.34	1.05	0.29	0.76	0.95	0.658	1.05	0.625	1.06	1.30	0.763	No
265	17.39	1.06	0.29	0.76	0.95	0.659	1.05	0.625	1.06	1.30	0.764	No
266	17.46	1.06	0.30	0.76	0.95	0.660	1.05	0.626	1.06	1.30	0.764	No
267	17.52	1.06	0.30	0.77	0.95	0.660	1.05	0.626	1.06	1.30	0.765	No
268	17.60	1.07	0.30	0.77	0.95	0.661	1.05	0.627	1.06	1.30	0.766	No
269	17.66	1.07	0.30	0.77	0.95	0.661	1.05	0.627	1.06	1.30	0.767	No
270	17.73	1.08	0.30	0.77	0.95	0.662	1.05	0.628	1.06	1.30	0.770	No
271	17.79	1.08	0.31	0.78	0.95	0.662	1.05	0.628	1.06	1.30	0.772	No
272	17.86	1.09	0.31	0.78	0.95	0.663	1.05	0.629	1.05	1.30	0.775	No
273	17.92	1.09	0.31	0.78	0.95	0.663	1.05	0.629	1.05	1.30	0.777	No
274	17.98	1.09	0.31	0.78	0.95	0.664	1.05	0.630	1.05	1.30	0.780	No
275	18.07	1.10	0.31	0.78	0.95	0.665	1.05	0.630	1.05	1.30	0.782	No
276	18.11	1.10	0.32	0.79	0.95	0.665	1.05	0.631	1.05	1.30	0.784	No
277	18.18	1.11	0.32	0.79	0.95	0.666	1.05	0.631	1.05	1.30	0.786	No
278	18.27	1.11	0.32	0.79	0.95	0.666	1.05	0.632	1.05	1.30	0.788	No
279	18.32	1.12	0.32	0.79	0.95	0.667	1.05	0.632	1.05	1.30	0.790	No
280	18.37	1.12	0.32	0.79	0.95	0.667	1.05	0.633	1.05	1.30	0.791	No
281	18.46	1.12	0.33	0.80	0.95	0.668	1.05	0.633	1.04	1.30	0.796	No
282	18.52	1.13	0.33	0.80	0.95	0.668	1.05	0.634	1.04	1.30	0.800	No
283	18.57	1.13	0.33	0.80	0.95	0.669	1.05	0.634	1.04	1.30	0.804	No
284	18.66	1.14	0.33	0.80	0.95	0.669	1.05	0.635	1.04	1.30	0.812	No
285	18.71	1.14	0.33	0.81	0.95	0.670	1.05	0.635	1.04	1.30	0.816	No
286	18.77	1.14	0.34	0.81	0.95	0.670	1.05	0.636	1.03	1.30	0.822	No
287	18.84	1.15	0.34	0.81	0.95	0.671	1.05	0.636	1.03	1.30	0.828	No
288	18.91	1.15	0.34	0.81	0.95	0.671	1.05	0.637	1.03	1.30	0.831	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
289	18.97	1.16	0.34	0.81	0.94	0.672	1.05	0.637	1.03	1.30	0.834	No
290	19.05	1.16	0.34	0.82	0.94	0.672	1.05	0.638	1.03	1.30	0.838	No
291	19.10	1.16	0.35	0.82	0.94	0.673	1.05	0.638	1.03	1.30	0.840	No
292	19.16	1.17	0.35	0.82	0.94	0.673	1.05	0.639	1.03	1.30	0.841	No
293	19.26	1.17	0.35	0.82	0.94	0.674	1.05	0.639	1.02	1.30	0.844	No
294	19.30	1.18	0.35	0.82	0.94	0.674	1.05	0.640	1.02	1.30	0.845	No
295	19.36	1.18	0.35	0.83	0.94	0.675	1.05	0.640	1.02	1.30	0.847	No
296	19.43	1.18	0.36	0.83	0.94	0.675	1.05	0.641	1.02	1.30	0.848	No
297	19.51	1.19	0.36	0.83	0.94	0.676	1.05	0.641	1.02	1.30	0.849	No
298	19.55	1.19	0.36	0.83	0.94	0.676	1.05	0.641	1.02	1.30	0.850	No
299	19.63	1.20	0.36	0.83	0.94	0.677	1.05	0.642	1.02	1.30	0.851	No
300	19.69	1.20	0.36	0.83	0.94	0.677	1.05	0.642	1.02	1.30	0.852	No
301	19.75	1.20	0.37	0.84	0.94	0.678	1.05	0.643	1.02	1.30	0.852	No
302	19.84	1.21	0.37	0.84	0.94	0.679	1.05	0.644	1.02	1.30	0.853	No
303	19.89	1.21	0.37	0.84	0.94	0.679	1.05	0.644	1.02	1.30	0.853	No
304	19.96	1.22	0.37	0.84	0.94	0.679	1.05	0.644	1.02	1.30	0.854	No
305	20.02	1.22	0.37	0.84	0.94	0.680	1.05	0.645	1.02	1.30	0.855	No
306	20.09	1.22	0.38	0.85	0.94	0.680	1.05	0.645	1.02	1.30	0.855	No
307	20.14	1.23	0.38	0.85	0.94	0.681	1.05	0.646	1.02	1.30	0.856	No
308	20.22	1.23	0.38	0.85	0.94	0.681	1.05	0.646	1.02	1.30	0.856	No
309	20.28	1.23	0.38	0.85	0.94	0.682	1.05	0.647	1.02	1.30	0.856	No
310	20.36	1.24	0.39	0.85	0.94	0.682	1.05	0.647	1.02	1.30	0.857	No
311	20.41	1.24	0.39	0.86	0.94	0.683	1.05	0.647	1.02	1.30	0.857	No
312	20.48	1.25	0.39	0.86	0.94	0.683	1.05	0.648	1.02	1.30	0.857	No
313	20.55	1.25	0.39	0.86	0.94	0.683	1.05	0.648	1.02	1.30	0.857	No
314	20.61	1.26	0.39	0.86	0.94	0.684	1.05	0.649	1.02	1.30	0.858	No
315	20.68	1.26	0.40	0.86	0.94	0.684	1.05	0.649	1.02	1.30	0.858	No
316	20.74	1.26	0.40	0.87	0.94	0.685	1.05	0.649	1.02	1.30	0.858	No
317	20.81	1.27	0.40	0.87	0.94	0.685	1.05	0.650	1.02	1.30	0.858	No
318	20.88	1.27	0.40	0.87	0.94	0.686	1.05	0.650	1.02	1.30	0.858	No
319	20.93	1.27	0.40	0.87	0.94	0.686	1.05	0.650	1.02	1.30	0.859	No
320	21.00	1.28	0.41	0.87	0.94	0.686	1.05	0.651	1.02	1.30	0.860	No
321	21.07	1.28	0.41	0.88	0.94	0.687	1.05	0.651	1.02	1.30	0.861	No
322	21.13	1.29	0.41	0.88	0.94	0.687	1.05	0.652	1.02	1.30	0.862	No
323	21.22	1.29	0.41	0.88	0.94	0.688	1.05	0.652	1.02	1.30	0.863	No
324	21.27	1.30	0.41	0.88	0.94	0.688	1.05	0.652	1.02	1.30	0.863	No
325	21.34	1.30	0.42	0.88	0.93	0.688	1.05	0.653	1.02	1.30	0.863	No
326	21.41	1.30	0.42	0.89	0.93	0.689	1.05	0.653	1.02	1.30	0.864	No
327	21.46	1.31	0.42	0.89	0.93	0.689	1.05	0.653	1.02	1.30	0.865	No
328	21.55	1.31	0.42	0.89	0.93	0.689	1.05	0.654	1.02	1.30	0.865	No
329	21.59	1.32	0.42	0.89	0.93	0.690	1.05	0.654	1.02	1.30	0.865	No
330	21.66	1.32	0.43	0.89	0.93	0.690	1.05	0.654	1.02	1.30	0.865	No
331	21.76	1.33	0.43	0.90	0.93	0.690	1.05	0.655	1.02	1.30	0.865	No
332	21.80	1.33	0.43	0.90	0.93	0.691	1.05	0.655	1.02	1.30	0.865	No
333	21.86	1.33	0.43	0.90	0.93	0.691	1.05	0.655	1.02	1.30	0.865	No
334	21.95	1.34	0.44	0.90	0.93	0.691	1.05	0.656	1.02	1.30	0.864	No
335	22.01	1.34	0.44	0.91	0.93	0.692	1.05	0.656	1.02	1.30	0.864	No
336	22.06	1.35	0.44	0.91	0.93	0.692	1.05	0.656	1.02	1.30	0.863	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
337	22.12	1.35	0.44	0.91	0.93	0.692	1.05	0.657	1.02	1.30	0.863	No
338	22.18	1.35	0.44	0.91	0.93	0.693	1.05	0.657	1.02	1.30	0.863	No
339	22.26	1.36	0.44	0.91	0.93	0.693	1.05	0.657	1.02	1.30	0.862	No
340	22.31	1.36	0.45	0.91	0.93	0.693	1.05	0.657	1.02	1.30	0.861	No
341	22.38	1.37	0.45	0.92	0.93	0.694	1.05	0.658	1.02	1.30	0.859	No
342	22.44	1.37	0.45	0.92	0.93	0.694	1.05	0.658	1.02	1.30	0.858	No
343	22.53	1.38	0.45	0.92	0.93	0.694	1.05	0.658	1.02	1.30	0.856	No
344	22.59	1.38	0.46	0.92	0.93	0.694	1.05	0.659	1.02	1.30	0.855	No
345	22.65	1.38	0.46	0.93	0.93	0.695	1.05	0.659	1.02	1.30	0.854	No
346	22.71	1.39	0.46	0.93	0.93	0.695	1.05	0.659	1.02	1.30	0.853	No
347	22.78	1.39	0.46	0.93	0.93	0.695	1.05	0.659	1.02	1.30	0.851	No
348	22.86	1.40	0.46	0.93	0.93	0.696	1.05	0.660	1.02	1.30	0.851	No
349	22.92	1.40	0.47	0.93	0.93	0.696	1.05	0.660	1.02	1.30	0.850	No
350	22.98	1.40	0.47	0.94	0.93	0.696	1.05	0.660	1.02	1.30	0.850	No
351	23.04	1.41	0.47	0.94	0.93	0.696	1.05	0.661	1.02	1.30	0.850	No
352	23.10	1.41	0.47	0.94	0.93	0.697	1.05	0.661	1.02	1.30	0.851	No
353	23.16	1.42	0.47	0.94	0.93	0.697	1.05	0.661	1.02	1.30	0.851	No
354	23.25	1.42	0.48	0.95	0.93	0.697	1.05	0.661	1.02	1.30	0.852	No
355	23.30	1.42	0.48	0.95	0.93	0.698	1.05	0.662	1.02	1.30	0.852	No
356	23.36	1.43	0.48	0.95	0.93	0.698	1.05	0.662	1.02	1.30	0.853	No
357	23.43	1.43	0.48	0.95	0.93	0.698	1.05	0.662	1.02	1.30	0.853	No
358	23.49	1.44	0.48	0.95	0.93	0.698	1.05	0.662	1.02	1.30	0.853	No
359	23.56	1.44	0.49	0.96	0.93	0.699	1.05	0.662	1.02	1.30	0.853	No
360	23.65	1.45	0.49	0.96	0.92	0.699	1.05	0.663	1.02	1.30	0.854	No
361	23.71	1.45	0.49	0.96	0.92	0.699	1.05	0.663	1.02	1.30	0.854	No
362	23.76	1.45	0.49	0.96	0.92	0.699	1.05	0.663	1.02	1.30	0.856	No
363	23.83	1.46	0.49	0.96	0.92	0.699	1.05	0.663	1.01	1.30	0.860	No
364	23.89	1.46	0.50	0.97	0.92	0.700	1.05	0.664	1.01	1.30	0.864	No
365	23.95	1.47	0.50	0.97	0.92	0.700	1.05	0.664	1.01	1.30	0.869	No
366	24.02	1.47	0.50	0.97	0.92	0.700	1.05	0.664	1.01	1.30	0.875	No
367	24.09	1.47	0.50	0.97	0.92	0.700	1.05	0.664	1.01	1.30	0.880	No
368	24.15	1.48	0.50	0.97	0.92	0.701	1.05	0.665	1.01	1.30	0.886	No
369	24.24	1.48	0.51	0.98	0.92	0.701	1.05	0.665	1.01	1.30	0.890	No
370	24.29	1.49	0.51	0.98	0.92	0.701	1.05	0.665	1.01	1.30	0.892	No
371	24.35	1.49	0.51	0.98	0.92	0.701	1.05	0.665	1.01	1.30	0.894	No
372	24.42	1.49	0.51	0.98	0.92	0.702	1.05	0.666	1.01	1.30	0.895	No
373	24.49	1.50	0.51	0.98	0.92	0.702	1.05	0.666	1.01	1.30	0.896	No
374	24.54	1.50	0.52	0.99	0.92	0.702	1.05	0.666	1.01	1.30	0.896	No
375	24.62	1.51	0.52	0.99	0.92	0.703	1.05	0.666	1.01	1.30	0.897	No
376	24.69	1.51	0.52	0.99	0.92	0.703	1.05	0.667	1.01	1.30	0.898	No
377	24.75	1.51	0.52	0.99	0.92	0.703	1.05	0.667	1.01	1.30	0.898	No
378	24.81	1.52	0.52	0.99	0.92	0.703	1.05	0.667	1.01	1.30	0.897	No
379	24.88	1.52	0.53	1.00	0.92	0.704	1.05	0.667	1.01	1.30	0.897	No
380	24.94	1.53	0.53	1.00	0.92	0.704	1.05	0.668	1.01	1.30	0.896	No
381	25.00	1.53	0.53	1.00	0.92	0.704	1.05	0.668	1.01	1.30	0.893	No
382	25.07	1.53	0.53	1.00	0.92	0.704	1.05	0.668	1.01	1.30	0.888	No
383	25.13	1.54	0.53	1.00	0.92	0.705	1.05	0.668	1.01	1.30	0.887	No
384	25.22	1.54	0.54	1.01	0.92	0.705	1.05	0.668	1.01	1.30	0.883	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
385	25.27	1.55	0.54	1.01	0.92	0.705	1.05	0.669	1.01	1.30	0.880	No
386	25.33	1.55	0.54	1.01	0.92	0.705	1.05	0.669	1.01	1.30	0.878	No
387	25.40	1.55	0.54	1.01	0.92	0.705	1.05	0.669	1.01	1.30	0.877	No
388	25.48	1.56	0.55	1.01	0.92	0.706	1.05	0.669	1.01	1.30	0.878	No
389	25.53	1.56	0.55	1.02	0.92	0.706	1.05	0.669	1.01	1.30	0.880	No
390	25.60	1.57	0.55	1.02	0.92	0.706	1.05	0.669	1.01	1.30	0.883	No
391	25.67	1.57	0.55	1.02	0.92	0.706	1.05	0.670	1.00	1.30	0.885	No
392	25.73	1.58	0.55	1.02	0.92	0.706	1.05	0.670	1.00	1.30	0.888	No
393	25.79	1.58	0.56	1.02	0.92	0.706	1.05	0.670	1.00	1.30	0.892	No
394	25.87	1.58	0.56	1.03	0.91	0.707	1.05	0.670	1.00	1.30	0.897	No
395	25.92	1.59	0.56	1.03	0.91	0.707	1.05	0.670	1.00	1.30	0.898	No
396	26.00	1.59	0.56	1.03	0.91	0.707	1.05	0.671	1.00	1.30	0.901	No
397	26.07	1.60	0.56	1.03	0.91	0.707	1.05	0.671	1.00	1.30	0.903	No
398	26.12	1.60	0.57	1.03	0.91	0.707	1.05	0.671	1.00	1.30	0.904	No
399	26.19	1.60	0.57	1.04	0.91	0.708	1.05	0.671	1.00	1.30	0.906	No
400	26.25	1.61	0.57	1.04	0.91	0.708	1.05	0.671	1.00	1.30	0.907	No
401	26.33	1.61	0.57	1.04	0.91	0.708	1.05	0.671	1.00	1.30	0.908	No
402	26.39	1.62	0.57	1.04	0.91	0.708	1.05	0.672	1.00	1.30	0.908	No
403	26.45	1.62	0.58	1.04	0.91	0.708	1.05	0.672	1.00	1.30	0.908	No
404	26.52	1.62	0.58	1.05	0.91	0.709	1.05	0.672	1.00	1.30	0.908	No
405	26.58	1.63	0.58	1.05	0.91	0.709	1.05	0.672	1.00	1.30	0.908	No
406	26.66	1.63	0.58	1.05	0.91	0.709	1.05	0.672	1.00	1.30	0.908	No
407	26.72	1.64	0.58	1.05	0.91	0.709	1.05	0.673	1.00	1.30	0.907	No
408	26.78	1.64	0.59	1.05	0.91	0.709	1.05	0.673	1.00	1.30	0.906	No
409	26.84	1.64	0.59	1.06	0.91	0.709	1.05	0.673	1.00	1.30	0.904	No
410	26.91	1.65	0.59	1.06	0.91	0.710	1.05	0.673	1.00	1.30	0.903	No
411	26.97	1.65	0.59	1.06	0.91	0.710	1.05	0.673	1.00	1.30	0.902	No
412	27.05	1.66	0.59	1.06	0.91	0.710	1.05	0.673	1.00	1.30	0.900	No
413	27.10	1.66	0.60	1.06	0.91	0.710	1.05	0.673	1.00	1.30	0.899	No
414	27.17	1.66	0.60	1.07	0.91	0.710	1.05	0.674	1.00	1.30	0.897	No
415	27.24	1.67	0.60	1.07	0.91	0.710	1.05	0.674	1.00	1.30	0.896	No
416	27.30	1.67	0.60	1.07	0.91	0.710	1.05	0.674	1.00	1.30	0.895	No
417	27.37	1.68	0.60	1.07	0.91	0.711	1.05	0.674	1.00	1.30	0.895	No
418	27.46	1.68	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.894	No
419	27.51	1.69	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.893	No
420	27.57	1.69	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.892	No
421	27.64	1.69	0.61	1.08	0.91	0.711	1.05	0.674	1.00	1.30	0.892	No
422	27.70	1.70	0.61	1.08	0.91	0.711	1.05	0.675	1.00	1.30	0.891	No
423	27.76	1.70	0.62	1.09	0.91	0.711	1.05	0.675	1.00	1.30	0.891	No
424	27.82	1.71	0.62	1.09	0.91	0.711	1.05	0.675	1.00	1.30	0.891	No
425	27.91	1.71	0.62	1.09	0.91	0.712	1.05	0.675	1.00	1.30	0.891	No
426	27.96	1.71	0.62	1.09	0.91	0.712	1.05	0.675	1.00	1.30	0.891	No
427	28.03	1.72	0.62	1.09	0.91	0.712	1.05	0.675	0.99	1.30	0.891	No
428	28.09	1.72	0.63	1.10	0.90	0.712	1.05	0.675	0.99	1.30	0.891	No
429	28.16	1.73	0.63	1.10	0.90	0.712	1.05	0.675	0.99	1.30	0.892	No
430	28.23	1.73	0.63	1.10	0.90	0.712	1.05	0.675	0.99	1.30	0.894	No
431	28.29	1.74	0.63	1.10	0.90	0.712	1.05	0.675	0.99	1.30	0.895	No
432	28.36	1.74	0.64	1.10	0.90	0.712	1.05	0.676	0.99	1.30	0.898	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
433	28.45	1.75	0.64	1.11	0.90	0.712	1.05	0.676	0.99	1.30	0.901	No
434	28.48	1.75	0.64	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.902	No
435	28.55	1.75	0.64	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.904	No
436	28.61	1.76	0.64	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.905	No
437	28.68	1.76	0.65	1.11	0.90	0.713	1.05	0.676	0.99	1.30	0.905	No
438	28.74	1.76	0.65	1.12	0.90	0.713	1.05	0.676	0.99	1.30	0.906	No
439	28.81	1.77	0.65	1.12	0.90	0.713	1.05	0.676	0.99	1.30	0.908	No
440	28.87	1.77	0.65	1.12	0.90	0.713	1.05	0.676	0.99	1.30	0.913	No
441	28.94	1.78	0.65	1.12	0.90	0.713	1.05	0.676	0.99	1.30	0.913	No
442	29.03	1.78	0.66	1.13	0.90	0.713	1.05	0.677	0.99	1.30	0.917	No
443	29.08	1.78	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.919	No
444	29.16	1.79	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.921	No
445	29.22	1.79	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.922	No
446	29.27	1.80	0.66	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.923	No
447	29.35	1.80	0.67	1.13	0.90	0.714	1.05	0.677	0.99	1.30	0.924	No
448	29.43	1.81	0.67	1.14	0.90	0.714	1.05	0.677	0.99	1.30	0.924	No
449	29.47	1.81	0.67	1.14	0.90	0.714	1.05	0.677	0.99	1.30	0.925	No
450	29.53	1.81	0.67	1.14	0.90	0.714	1.05	0.678	0.99	1.30	0.925	No
451	29.60	1.82	0.67	1.14	0.90	0.715	1.05	0.678	0.99	1.30	0.925	No
452	29.67	1.82	0.68	1.14	0.90	0.715	1.05	0.678	0.99	1.30	0.926	No
453	29.73	1.82	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.926	No
454	29.80	1.83	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.926	No
455	29.87	1.83	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.927	No
456	29.93	1.83	0.68	1.15	0.90	0.715	1.05	0.678	0.99	1.30	0.927	No
457	30.00	1.84	0.69	1.15	0.90	0.715	1.05	0.679	0.99	1.30	0.927	No
458	30.07	1.84	0.69	1.15	0.90	0.716	1.05	0.679	0.99	1.30	0.928	No
459	30.12	1.85	0.69	1.16	0.90	0.716	1.05	0.679	0.99	1.30	0.928	No
460	30.20	1.85	0.69	1.16	0.89	0.716	1.05	0.679	0.99	1.30	0.928	No
461	30.27	1.85	0.69	1.16	0.89	0.716	1.05	0.679	0.99	1.30	0.929	No
462	30.32	1.86	0.70	1.16	0.89	0.716	1.05	0.679	0.99	1.30	0.929	No
463	30.40	1.86	0.70	1.16	0.89	0.716	1.05	0.679	0.99	1.30	0.929	No
464	30.46	1.87	0.70	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.929	No
465	30.52	1.87	0.70	1.17	0.89	0.716	1.05	0.679	0.99	1.30	0.929	No
466	30.59	1.87	0.70	1.17	0.89	0.717	1.05	0.680	0.99	1.30	0.930	No
467	30.65	1.88	0.71	1.17	0.89	0.717	1.05	0.680	0.99	1.30	0.930	No
468	30.71	1.88	0.71	1.17	0.89	0.717	1.05	0.680	0.99	1.30	0.930	No
469	30.79	1.89	0.71	1.17	0.89	0.717	1.05	0.680	0.99	1.30	0.931	No
470	30.85	1.89	0.71	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.931	No
471	30.96	1.90	0.72	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.931	No
472	31.00	1.90	0.72	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.932	No
473	31.04	1.90	0.72	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.932	No
474	31.11	1.90	0.72	1.18	0.89	0.717	1.05	0.680	0.99	1.30	0.932	No
475	31.18	1.91	0.72	1.19	0.89	0.717	1.05	0.680	0.99	1.30	0.932	No
476	31.25	1.91	0.73	1.19	0.89	0.718	1.05	0.681	0.99	1.30	0.933	No
477	31.30	1.92	0.73	1.19	0.89	0.718	1.05	0.681	0.99	1.30	0.933	No
478	31.38	1.92	0.73	1.19	0.89	0.718	1.05	0.681	0.99	1.30	0.933	No
479	31.44	1.92	0.73	1.19	0.89	0.718	1.05	0.681	0.99	1.30	0.933	No
480	31.50	1.93	0.73	1.19	0.89	0.718	1.05	0.681	0.99	1.30	0.933	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
481	31.57	1.93	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
482	31.63	1.94	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
483	31.70	1.94	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
484	31.79	1.94	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
485	31.83	1.95	0.74	1.20	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
486	31.90	1.95	0.75	1.21	0.89	0.718	1.05	0.681	0.99	1.30	0.934	No
487	31.97	1.96	0.75	1.21	0.89	0.719	1.05	0.681	0.99	1.30	0.935	No
488	32.03	1.96	0.75	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.935	No
489	32.10	1.96	0.75	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.935	No
490	32.16	1.97	0.75	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.936	No
491	32.23	1.97	0.76	1.21	0.89	0.719	1.05	0.682	0.99	1.30	0.936	No
492	32.30	1.98	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.936	No
493	32.36	1.98	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.936	No
494	32.46	1.98	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
495	32.51	1.99	0.76	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
496	32.56	1.99	0.77	1.22	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
497	32.65	2.00	0.77	1.23	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
498	32.68	2.00	0.77	1.23	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
499	32.76	2.00	0.77	1.23	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
500	32.84	2.01	0.78	1.23	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
501	32.89	2.01	0.78	1.23	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
502	32.95	2.01	0.78	1.24	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
503	33.01	2.02	0.78	1.24	0.88	0.719	1.05	0.682	0.99	1.30	0.937	No
504	33.10	2.02	0.78	1.24	0.88	0.720	1.05	0.682	0.99	1.30	0.938	No
505	33.15	2.03	0.78	1.24	0.88	0.720	1.05	0.682	0.99	1.30	0.938	No
506	33.24	2.03	0.79	1.24	0.88	0.720	1.05	0.682	0.99	1.30	0.939	No
507	33.29	2.03	0.79	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
508	33.35	2.04	0.79	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
509	33.40	2.04	0.79	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.939	No
510	33.47	2.05	0.79	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
511	33.55	2.05	0.80	1.25	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
512	33.65	2.06	0.80	1.26	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
513	33.66	2.06	0.80	1.26	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
514	33.74	2.06	0.80	1.26	0.88	0.720	1.05	0.683	0.99	1.30	0.940	No
515	33.84	2.07	0.81	1.26	0.88	0.720	1.05	0.683	0.99	1.30	0.941	No
516	33.88	2.07	0.81	1.26	0.88	0.720	1.05	0.683	0.99	1.30	0.941	No
517	33.93	2.07	0.81	1.26	0.88	0.720	1.05	0.683	0.99	1.30	0.941	No
518	33.99	2.08	0.81	1.26	0.88	0.720	1.05	0.683	0.99	1.30	0.941	No
519	34.07	2.08	0.81	1.27	0.88	0.720	1.05	0.683	0.99	1.30	0.941	No
520	34.12	2.08	0.81	1.27	0.88	0.720	1.05	0.683	0.99	1.30	0.942	No
521	34.19	2.09	0.82	1.27	0.88	0.720	1.05	0.683	0.99	1.30	0.942	No
522	34.28	2.09	0.82	1.27	0.88	0.721	1.05	0.683	0.98	1.30	0.942	No
523	34.32	2.09	0.82	1.27	0.88	0.721	1.05	0.683	0.98	1.30	0.942	No
524	34.40	2.10	0.82	1.28	0.87	0.721	1.05	0.683	0.98	1.30	0.942	No
525	34.48	2.10	0.83	1.28	0.87	0.721	1.05	0.683	0.98	1.30	0.942	No
526	34.52	2.11	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
527	34.58	2.11	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
528	34.68	2.12	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
529	34.72	2.12	0.83	1.28	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
530	34.81	2.12	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
531	34.85	2.13	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
532	34.92	2.13	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
533	34.98	2.13	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
534	35.05	2.14	0.84	1.29	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
535	35.12	2.14	0.85	1.30	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
536	35.18	2.15	0.85	1.30	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
537	35.26	2.15	0.85	1.30	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
538	35.31	2.15	0.85	1.30	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
539	35.41	2.16	0.86	1.30	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
540	35.47	2.16	0.86	1.31	0.87	0.721	1.05	0.684	0.98	1.30	0.944	No
541	35.51	2.17	0.86	1.31	0.87	0.721	1.05	0.684	0.98	1.30	0.943	No
542	35.58	2.17	0.86	1.31	0.87	0.721	1.05	0.684	0.98	1.30	0.942	No
543	35.63	2.17	0.86	1.31	0.87	0.721	1.05	0.684	0.98	1.30	0.940	No
544	35.71	2.18	0.86	1.31	0.87	0.721	1.05	0.684	0.97	1.30	0.939	No
545	35.78	2.18	0.87	1.32	0.87	0.721	1.05	0.684	0.97	1.30	0.938	No
546	35.84	2.19	0.87	1.32	0.87	0.721	1.05	0.683	0.97	1.30	0.938	No
547	35.90	2.19	0.87	1.32	0.87	0.721	1.05	0.683	0.97	1.30	0.940	No
548	35.98	2.20	0.87	1.32	0.87	0.721	1.05	0.683	0.97	1.30	0.941	No
549	36.05	2.20	0.88	1.32	0.87	0.721	1.05	0.683	0.98	1.30	0.942	No
550	36.10	2.20	0.88	1.33	0.87	0.720	1.05	0.683	0.98	1.30	0.943	No
551	36.20	2.21	0.88	1.33	0.87	0.720	1.05	0.683	0.98	1.30	0.944	No
552	36.25	2.21	0.88	1.33	0.87	0.720	1.05	0.683	0.98	1.30	0.945	No
553	36.30	2.22	0.88	1.33	0.87	0.720	1.05	0.683	0.98	1.30	0.945	No
554	36.35	2.22	0.88	1.33	0.87	0.720	1.05	0.683	0.98	1.30	0.945	No
555	36.45	2.22	0.89	1.34	0.86	0.720	1.05	0.683	0.98	1.30	0.945	No
556	36.48	2.23	0.89	1.34	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
557	36.55	2.23	0.89	1.34	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
558	36.63	2.23	0.89	1.34	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
559	36.69	2.24	0.90	1.34	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
560	36.75	2.24	0.90	1.35	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
561	36.84	2.25	0.90	1.35	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
562	36.89	2.25	0.90	1.35	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
563	36.95	2.25	0.90	1.35	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
564	37.05	2.26	0.91	1.35	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
565	37.08	2.26	0.91	1.36	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
566	37.14	2.27	0.91	1.36	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
567	37.23	2.27	0.91	1.36	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
568	37.28	2.28	0.91	1.36	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
569	37.34	2.28	0.92	1.36	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
570	37.43	2.28	0.92	1.37	0.86	0.720	1.05	0.683	0.98	1.30	0.946	No
571	37.48	2.29	0.92	1.37	0.86	0.720	1.05	0.683	0.97	1.30	0.946	No
572	37.53	2.29	0.92	1.37	0.86	0.720	1.05	0.683	0.97	1.30	0.946	No
573	37.61	2.30	0.92	1.37	0.86	0.720	1.05	0.682	0.97	1.30	0.946	No
574	37.67	2.30	0.93	1.37	0.86	0.720	1.05	0.682	0.97	1.30	0.946	No
575	37.73	2.30	0.93	1.38	0.86	0.719	1.05	0.682	0.97	1.30	0.946	No
576	37.82	2.31	0.93	1.38	0.86	0.719	1.05	0.682	0.97	1.30	0.945	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
577	37.88	2.31	0.93	1.38	0.86	0.719	1.05	0.682	0.97	1.30	0.944	No
578	37.93	2.32	0.93	1.38	0.86	0.719	1.05	0.682	0.97	1.30	0.944	No
579	38.00	2.32	0.94	1.38	0.86	0.719	1.05	0.682	0.97	1.30	0.942	No
580	38.08	2.33	0.94	1.39	0.86	0.719	1.05	0.682	0.96	1.30	0.941	No
581	38.12	2.33	0.94	1.39	0.86	0.719	1.05	0.682	0.96	1.30	0.940	No
582	38.20	2.33	0.94	1.39	0.86	0.719	1.05	0.682	0.96	1.30	0.938	No
583	38.29	2.34	0.94	1.39	0.86	0.719	1.05	0.682	0.96	1.30	0.937	No
584	38.33	2.34	0.95	1.40	0.86	0.719	1.05	0.682	0.96	1.30	0.936	No
585	38.43	2.35	0.95	1.40	0.86	0.719	1.05	0.681	0.95	1.30	0.933	No
586	38.48	2.35	0.95	1.40	0.85	0.718	1.05	0.681	0.95	1.30	0.932	No
587	38.52	2.35	0.95	1.40	0.85	0.718	1.05	0.681	0.95	1.30	0.931	No
588	38.59	2.36	0.95	1.40	0.85	0.718	1.05	0.681	0.95	1.30	0.931	No
589	38.68	2.36	0.96	1.41	0.85	0.718	1.05	0.681	0.95	1.30	0.930	No
590	38.72	2.37	0.96	1.41	0.85	0.718	1.05	0.681	0.95	1.30	0.930	No
591	38.79	2.37	0.96	1.41	0.85	0.718	1.05	0.681	0.95	1.30	0.929	No
592	38.87	2.38	0.96	1.41	0.85	0.718	1.05	0.681	0.94	1.30	0.928	No
593	38.92	2.38	0.96	1.42	0.85	0.718	1.05	0.681	0.94	1.30	0.926	No
594	38.98	2.38	0.97	1.42	0.85	0.718	1.05	0.681	0.94	1.30	0.925	No
595	39.05	2.39	0.97	1.42	0.85	0.717	1.05	0.680	0.93	1.30	0.926	No
596	39.12	2.39	0.97	1.42	0.85	0.717	1.05	0.680	0.93	1.30	0.930	No
597	39.17	2.40	0.97	1.42	0.85	0.717	1.05	0.680	0.92	1.30	0.933	No
598	39.26	2.40	0.98	1.43	0.85	0.717	1.05	0.680	0.92	1.30	0.937	No
599	39.32	2.41	0.98	1.43	0.85	0.717	1.05	0.680	0.92	1.30	0.938	No
600	39.37	2.41	0.98	1.43	0.85	0.717	1.05	0.680	0.92	1.30	0.939	No
601	39.46	2.42	0.98	1.43	0.85	0.717	1.05	0.680	0.92	1.30	0.939	No
602	39.52	2.42	0.98	1.44	0.85	0.716	1.05	0.679	0.92	1.30	0.939	No
603	39.57	2.42	0.98	1.44	0.85	0.716	1.05	0.679	0.92	1.30	0.939	No
604	39.63	2.43	0.99	1.44	0.85	0.716	1.05	0.679	0.92	1.30	0.938	No
605	39.72	2.43	0.99	1.44	0.85	0.716	1.05	0.679	0.92	1.30	0.937	No
606	39.77	2.44	0.99	1.45	0.85	0.716	1.05	0.679	0.92	1.30	0.937	No
607	39.85	2.44	0.99	1.45	0.85	0.716	1.05	0.679	0.92	1.30	0.935	No
608	39.91	2.45	1.00	1.45	0.85	0.716	1.05	0.679	0.92	1.30	0.934	No
609	39.96	2.45	1.00	1.45	0.85	0.715	1.05	0.679	0.92	1.30	0.932	No
610	40.06	2.46	1.00	1.46	0.85	0.715	1.05	0.678	0.92	1.30	0.930	No
611	40.11	2.46	1.00	1.46	0.85	0.715	1.05	0.678	0.93	1.30	0.928	No
612	40.16	2.46	1.00	1.46	0.85	0.715	1.05	0.678	0.93	1.30	0.927	No
613	40.26	2.47	1.01	1.46	0.85	0.715	1.05	0.678	0.93	1.30	0.930	No
614	40.30	2.47	1.01	1.46	0.85	0.715	1.05	0.678	0.94	1.30	0.931	No
615	40.36	2.48	1.01	1.47	0.85	0.715	1.05	0.678	0.94	1.30	0.933	No
616	40.44	2.48	1.01	1.47	0.85	0.714	1.05	0.678	0.94	1.30	0.935	No
617	40.50	2.49	1.01	1.47	0.84	0.714	1.05	0.677	0.94	1.30	0.936	No
618	40.55	2.49	1.02	1.47	0.84	0.714	1.05	0.677	0.95	1.30	0.937	No
619	40.62	2.49	1.02	1.48	0.84	0.714	1.05	0.677	0.95	1.30	0.938	No
620	40.68	2.50	1.02	1.48	0.84	0.714	1.05	0.677	0.95	1.30	0.939	No
621	40.75	2.50	1.02	1.48	0.84	0.714	1.05	0.677	0.95	1.30	0.940	No
622	40.84	2.51	1.02	1.48	0.84	0.714	1.05	0.677	0.95	1.30	0.941	No
623	40.90	2.51	1.03	1.48	0.84	0.714	1.05	0.677	0.95	1.30	0.941	No
624	40.96	2.52	1.03	1.49	0.84	0.713	1.05	0.677	0.95	1.30	0.941	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
625	41.04	2.52	1.03	1.49	0.84	0.713	1.05	0.676	0.95	1.30	0.941	No
626	41.09	2.52	1.03	1.49	0.84	0.713	1.05	0.676	0.95	1.30	0.941	No
627	41.15	2.53	1.03	1.49	0.84	0.713	1.05	0.676	0.95	1.30	0.941	No
628	41.22	2.53	1.04	1.50	0.84	0.713	1.05	0.676	0.95	1.30	0.941	No
629	41.30	2.54	1.04	1.50	0.84	0.713	1.05	0.676	0.95	1.30	0.941	No
630	41.35	2.54	1.04	1.50	0.84	0.713	1.05	0.676	0.95	1.30	0.941	No
631	41.41	2.54	1.04	1.50	0.84	0.713	1.05	0.676	0.95	1.30	0.941	No
632	41.48	2.55	1.04	1.50	0.84	0.712	1.05	0.676	0.95	1.30	0.940	No
633	41.55	2.55	1.05	1.51	0.84	0.712	1.05	0.676	0.95	1.30	0.940	No
634	41.62	2.56	1.05	1.51	0.84	0.712	1.05	0.675	0.95	1.30	0.940	No
635	41.68	2.56	1.05	1.51	0.84	0.712	1.05	0.675	0.95	1.30	0.940	No
636	41.74	2.57	1.05	1.51	0.84	0.712	1.05	0.675	0.95	1.30	0.941	No
637	41.80	2.57	1.05	1.51	0.84	0.712	1.05	0.675	0.95	1.30	0.941	No
638	41.88	2.57	1.06	1.52	0.84	0.712	1.05	0.675	0.95	1.30	0.941	No
639	41.95	2.58	1.06	1.52	0.84	0.711	1.05	0.675	0.95	1.30	0.941	No
640	42.00	2.58	1.06	1.52	0.84	0.711	1.05	0.675	0.95	1.30	0.941	No
641	42.08	2.59	1.06	1.52	0.84	0.711	1.05	0.675	0.95	1.30	0.941	No
642	42.15	2.59	1.07	1.53	0.84	0.711	1.05	0.674	0.95	1.30	0.941	No
643	42.22	2.60	1.07	1.53	0.84	0.711	1.05	0.674	0.95	1.30	0.942	No
644	42.28	2.60	1.07	1.53	0.84	0.711	1.05	0.674	0.95	1.30	0.942	No
645	42.34	2.60	1.07	1.53	0.84	0.711	1.05	0.674	0.95	1.30	0.943	No
646	42.39	2.61	1.07	1.53	0.84	0.711	1.05	0.674	0.95	1.30	0.943	No
647	42.48	2.61	1.08	1.54	0.84	0.710	1.05	0.674	0.95	1.30	0.943	No
648	42.53	2.62	1.08	1.54	0.83	0.710	1.05	0.674	0.95	1.30	0.943	No
649	42.59	2.62	1.08	1.54	0.83	0.710	1.05	0.674	0.95	1.30	0.943	No
650	42.68	2.63	1.08	1.54	0.83	0.710	1.05	0.673	0.95	1.30	0.943	No
651	42.72	2.63	1.08	1.55	0.83	0.710	1.05	0.673	0.95	1.30	0.942	No
652	42.79	2.63	1.09	1.55	0.83	0.710	1.05	0.673	0.95	1.30	0.942	No
653	42.87	2.64	1.09	1.55	0.83	0.710	1.05	0.673	0.94	1.30	0.941	No
654	42.92	2.64	1.09	1.55	0.83	0.709	1.05	0.673	0.94	1.30	0.941	No
655	43.00	2.65	1.09	1.55	0.83	0.709	1.05	0.673	0.94	1.30	0.941	No
656	43.05	2.65	1.09	1.56	0.83	0.709	1.05	0.673	0.94	1.30	0.941	No
657	43.13	2.66	1.10	1.56	0.83	0.709	1.05	0.672	0.94	1.30	0.941	No
658	43.22	2.66	1.10	1.56	0.83	0.709	1.05	0.672	0.94	1.30	0.941	No
659	43.27	2.66	1.10	1.56	0.83	0.709	1.05	0.672	0.94	1.30	0.941	No
660	43.33	2.67	1.10	1.57	0.83	0.709	1.05	0.672	0.94	1.30	0.942	No
661	43.37	2.67	1.10	1.57	0.83	0.709	1.05	0.672	0.94	1.30	0.942	No
662	43.47	2.68	1.11	1.57	0.83	0.708	1.05	0.672	0.95	1.30	0.943	No
663	43.52	2.68	1.11	1.57	0.83	0.708	1.05	0.672	0.95	1.30	0.944	No
664	43.57	2.68	1.11	1.57	0.83	0.708	1.05	0.672	0.95	1.30	0.944	No
665	43.66	2.69	1.11	1.58	0.83	0.708	1.05	0.671	0.96	1.30	0.944	No
666	43.72	2.69	1.11	1.58	0.83	0.708	1.05	0.671	0.96	1.30	0.944	No
667	43.77	2.70	1.12	1.58	0.83	0.708	1.05	0.671	0.96	1.30	0.944	No
668	43.83	2.70	1.12	1.58	0.83	0.708	1.05	0.671	0.96	1.30	0.944	No
669	43.90	2.70	1.12	1.58	0.83	0.707	1.05	0.671	0.96	1.30	0.943	No
670	43.97	2.71	1.12	1.59	0.83	0.707	1.05	0.671	0.96	1.30	0.944	No
671	44.03	2.71	1.12	1.59	0.83	0.707	1.05	0.671	0.96	1.30	0.944	No
672	44.13	2.72	1.13	1.59	0.83	0.707	1.05	0.671	0.96	1.30	0.943	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
673	44.17	2.72	1.13	1.59	0.83	0.707	1.05	0.671	0.96	1.30	0.943	No
674	44.23	2.72	1.13	1.59	0.83	0.707	1.05	0.670	0.96	1.30	0.943	No
675	44.33	2.73	1.13	1.60	0.83	0.707	1.05	0.670	0.96	1.30	0.943	No
676	44.37	2.73	1.13	1.60	0.83	0.707	1.05	0.670	0.96	1.30	0.942	No
677	44.43	2.74	1.14	1.60	0.83	0.707	1.05	0.670	0.97	1.30	0.942	No
678	44.52	2.74	1.14	1.60	0.82	0.707	1.05	0.670	0.97	1.30	0.942	No
679	44.57	2.74	1.14	1.60	0.82	0.706	1.05	0.670	0.97	1.30	0.942	No
680	44.62	2.75	1.14	1.60	0.82	0.706	1.05	0.670	0.97	1.30	0.942	No
681	44.72	2.75	1.15	1.61	0.82	0.706	1.05	0.670	0.96	1.30	0.943	No
682	44.76	2.76	1.15	1.61	0.82	0.706	1.05	0.670	0.96	1.30	0.944	No
683	44.83	2.76	1.15	1.61	0.82	0.706	1.05	0.670	0.95	1.30	0.944	No
684	44.92	2.77	1.15	1.61	0.82	0.706	1.05	0.669	0.94	1.30	0.943	No
685	44.97	2.77	1.15	1.62	0.82	0.706	1.05	0.669	0.94	1.30	0.942	No
686	45.02	2.77	1.16	1.62	0.82	0.706	1.05	0.669	0.94	1.30	0.942	No
687	45.09	2.78	1.16	1.62	0.82	0.705	1.05	0.669	0.94	1.30	0.942	No
688	45.16	2.78	1.16	1.62	0.82	0.705	1.05	0.669	0.93	1.30	0.942	No
689	45.22	2.79	1.16	1.62	0.82	0.705	1.05	0.669	0.93	1.30	0.942	No
690	45.29	2.79	1.16	1.63	0.82	0.705	1.05	0.669	0.93	1.30	0.941	No
691	45.37	2.79	1.17	1.63	0.82	0.705	1.05	0.668	0.93	1.30	0.941	No
692	45.41	2.80	1.17	1.63	0.82	0.705	1.05	0.668	0.93	1.30	0.942	No
693	45.47	2.80	1.17	1.63	0.82	0.704	1.05	0.668	0.94	1.30	0.943	No
694	45.56	2.81	1.17	1.64	0.82	0.704	1.05	0.668	0.95	1.30	0.943	No
695	45.62	2.81	1.17	1.64	0.82	0.704	1.05	0.668	0.95	1.30	0.943	No
696	45.70	2.82	1.18	1.64	0.82	0.704	1.05	0.668	0.96	1.30	0.943	No
697	45.75	2.82	1.18	1.64	0.82	0.704	1.05	0.667	0.96	1.30	0.942	No
698	45.81	2.82	1.18	1.64	0.82	0.704	1.05	0.667	0.96	1.30	0.941	No
699	45.90	2.83	1.18	1.65	0.82	0.703	1.05	0.667	0.96	1.30	0.941	No
700	45.95	2.83	1.18	1.65	0.82	0.703	1.05	0.667	0.96	1.30	0.942	No
701	46.01	2.84	1.19	1.65	0.82	0.703	1.05	0.667	0.96	1.30	0.942	No
702	46.10	2.84	1.19	1.65	0.82	0.703	1.05	0.667	0.95	1.30	0.943	No
703	46.15	2.84	1.19	1.65	0.82	0.703	1.05	0.667	0.95	1.30	0.943	No
704	46.21	2.85	1.19	1.66	0.82	0.703	1.05	0.667	0.95	1.30	0.943	No
705	46.29	2.85	1.19	1.66	0.82	0.703	1.05	0.666	0.95	1.30	0.943	No
706	46.33	2.86	1.20	1.66	0.82	0.703	1.05	0.666	0.95	1.30	0.943	No
707	46.41	2.86	1.20	1.66	0.82	0.702	1.05	0.666	0.95	1.30	0.943	No
708	46.47	2.87	1.20	1.66	0.82	0.702	1.05	0.666	0.95	1.30	0.943	No
709	46.53	2.87	1.20	1.67	0.81	0.702	1.05	0.666	0.95	1.30	0.943	No
710	46.59	2.87	1.20	1.67	0.81	0.702	1.05	0.666	0.95	1.30	0.943	No
711	46.66	2.88	1.21	1.67	0.81	0.702	1.05	0.666	0.94	1.30	0.943	No
712	46.75	2.88	1.21	1.67	0.81	0.702	1.05	0.665	0.94	1.30	0.943	No
713	46.79	2.89	1.21	1.67	0.81	0.701	1.05	0.665	0.94	1.30	0.942	No
714	46.85	2.89	1.21	1.68	0.81	0.701	1.05	0.665	0.94	1.30	0.942	No
715	46.92	2.89	1.21	1.68	0.81	0.701	1.05	0.665	0.94	1.30	0.942	No
716	47.00	2.90	1.22	1.68	0.81	0.701	1.05	0.665	0.94	1.30	0.942	No
717	47.05	2.90	1.22	1.68	0.81	0.701	1.05	0.665	0.94	1.30	0.942	No
718	47.12	2.91	1.22	1.69	0.81	0.701	1.05	0.665	0.94	1.30	0.942	No
719	47.20	2.91	1.22	1.69	0.81	0.700	1.05	0.664	0.94	1.30	0.942	No
720	47.26	2.92	1.22	1.69	0.81	0.700	1.05	0.664	0.94	1.30	0.942	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)												
Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ'_v (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
721	47.32	2.92	1.23	1.69	0.81	0.700	1.05	0.664	0.94	1.30	0.942	No
722	47.39	2.92	1.23	1.69	0.81	0.700	1.05	0.664	0.94	1.30	0.942	No
723	47.47	2.93	1.23	1.70	0.81	0.700	1.05	0.664	0.95	1.30	0.942	No
724	47.51	2.93	1.23	1.70	0.81	0.700	1.05	0.664	0.95	1.30	0.941	No
725	47.59	2.94	1.24	1.70	0.81	0.700	1.05	0.663	0.95	1.30	0.941	No
726	47.65	2.94	1.24	1.70	0.81	0.699	1.05	0.663	0.95	1.30	0.941	No
727	47.71	2.94	1.24	1.70	0.81	0.699	1.05	0.663	0.95	1.30	0.940	No
728	47.79	2.95	1.24	1.71	0.81	0.699	1.05	0.663	0.95	1.30	0.940	No
729	47.85	2.95	1.24	1.71	0.81	0.699	1.05	0.663	0.96	1.30	0.939	No
730	47.91	2.96	1.25	1.71	0.81	0.699	1.05	0.663	0.96	1.30	0.939	No
731	48.00	2.96	1.25	1.71	0.81	0.699	1.05	0.663	0.95	1.30	0.940	No
732	48.05	2.96	1.25	1.72	0.81	0.698	1.05	0.662	0.95	1.30	0.941	No
733	48.10	2.97	1.25	1.72	0.81	0.698	1.05	0.662	0.94	1.30	0.941	No
734	48.19	2.97	1.25	1.72	0.81	0.698	1.05	0.662	0.92	1.30	0.941	No
735	48.25	2.98	1.26	1.72	0.81	0.698	1.05	0.662	0.91	1.30	0.941	No
736	48.30	2.98	1.26	1.72	0.81	0.698	1.05	0.662	0.91	1.30	0.941	No
737	48.39	2.99	1.26	1.73	0.81	0.698	1.05	0.662	0.90	1.30	0.941	No
738	48.43	2.99	1.26	1.73	0.81	0.698	1.05	0.662	0.90	1.30	0.941	No
739	48.50	2.99	1.26	1.73	0.81	0.697	1.05	0.661	0.90	1.30	0.942	No
740	48.59	3.00	1.27	1.73	0.80	0.697	1.05	0.661	0.90	1.30	0.942	No
741	48.64	3.00	1.27	1.73	0.80	0.697	1.05	0.661	0.89	1.30	0.942	No
742	48.70	3.01	1.27	1.74	0.80	0.697	1.05	0.661	0.89	1.30	0.942	No
743	48.79	3.01	1.27	1.74	0.80	0.697	1.05	0.661	0.89	1.30	0.942	No
744	48.83	3.01	1.27	1.74	0.80	0.696	1.05	0.660	0.89	1.30	0.942	No
745	48.89	3.02	1.28	1.74	0.80	0.696	1.05	0.660	0.90	1.30	0.942	No
746	48.95	3.02	1.28	1.75	0.80	0.696	1.05	0.660	0.90	1.30	0.942	No
747	49.02	3.03	1.28	1.75	0.80	0.696	1.05	0.660	0.90	1.30	0.942	No
748	49.11	3.03	1.28	1.75	0.80	0.696	1.05	0.660	0.90	1.30	0.942	No
749	49.19	3.04	1.29	1.75	0.80	0.695	1.05	0.660	0.90	1.30	0.941	No
750	49.22	3.04	1.29	1.75	0.80	0.695	1.05	0.659	0.90	1.30	0.941	No
751	49.28	3.04	1.29	1.76	0.80	0.695	1.05	0.659	0.91	1.30	0.941	No
752	49.35	3.05	1.29	1.76	0.80	0.695	1.05	0.659	0.91	1.30	0.941	No
753	49.42	3.05	1.29	1.76	0.80	0.695	1.05	0.659	0.91	1.30	0.941	No
754	49.48	3.06	1.29	1.76	0.80	0.695	1.05	0.659	0.92	1.30	0.941	No
755	49.56	3.06	1.30	1.77	0.80	0.694	1.05	0.659	0.92	1.30	0.941	No
756	49.63	3.07	1.30	1.77	0.80	0.694	1.05	0.658	0.92	1.30	0.940	No
757	49.68	3.07	1.30	1.77	0.80	0.694	1.05	0.658	0.92	1.30	0.940	No
758	49.74	3.07	1.30	1.77	0.80	0.694	1.05	0.658	0.92	1.30	0.940	No
759	49.83	3.08	1.31	1.77	0.80	0.694	1.05	0.658	0.92	1.30	0.940	No
760	49.87	3.08	1.31	1.78	0.80	0.694	1.05	0.658	0.92	1.30	0.940	No
761	49.97	3.09	1.31	1.78	0.80	0.693	1.05	0.658	0.93	1.30	0.940	No
762	50.03	3.09	1.31	1.78	0.80	0.693	1.05	0.657	0.92	1.30	2.000	No
763	50.08	3.09	1.31	1.78	0.80	0.693	1.05	0.657	0.92	1.30	2.000	No
764	50.14	3.10	1.31	1.78	0.80	0.693	1.05	0.658	0.92	1.30	2.000	No
765	50.23	3.10	1.32	1.78	0.80	0.693	1.05	0.658	0.92	1.30	2.000	No
766	50.27	3.10	1.32	1.78	0.80	0.693	1.05	0.658	0.92	1.30	2.000	No
767	50.33	3.11	1.32	1.78	0.80	0.693	1.05	0.658	0.91	1.30	2.000	No
768	50.41	3.11	1.32	1.79	0.80	0.693	1.05	0.658	0.91	1.30	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR*	Belongs to transition
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
σ_v :	Total overburden pressure at test point (tsf)
u_0 :	Water pressure at test point (tsf)
σ_v' :	Effective overburden pressure based on GWT during earthquake (tsf)
r_d :	Nonlinear shear mass factor
CSR:	Cyclic Stress Ratio
MSF:	Magnitude Scaling Factor
CSR_{eq} :	CSR adjusted for M=7.5
K_σ :	Effective overburden stress factor
CSR*:	CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
1	0.10	6.64	100.00	3.07	0.58	1.70	10.67	0.00	10.67	4.000	No	Yes	2.00
2	0.14	11.06	87.83	2.81	0.56	1.70	17.77	0.00	17.77	4.000	No	Yes	2.00
3	0.21	13.17	83.03	2.75	0.55	1.70	21.16	0.00	21.16	4.000	No	Yes	2.00
4	0.26	15.48	79.53	2.71	0.54	1.70	24.87	0.00	24.87	4.000	No	Yes	2.00
5	0.34	17.50	80.56	2.72	0.52	1.70	28.12	0.00	28.12	4.000	No	Yes	2.00
6	0.40	18.00	83.16	2.75	0.52	1.70	28.92	0.00	28.92	4.000	No	Yes	2.00
7	0.49	23.33	75.79	2.66	0.50	1.70	37.48	0.00	37.48	4.000	No	Yes	2.00
8	0.53	25.33	74.65	2.65	0.49	1.70	40.71	0.00	40.71	4.000	No	Yes	2.00
9	0.59	24.62	78.74	2.70	0.49	1.70	39.57	0.00	39.57	4.000	No	Yes	2.00
10	0.66	25.93	78.35	2.69	0.49	1.70	41.68	0.00	41.68	4.000	No	Yes	2.00
11	0.73	28.75	74.60	2.65	0.47	1.70	46.21	0.00	46.21	4.000	No	Yes	2.00
12	0.81	29.55	74.01	2.64	0.47	1.70	47.49	0.00	47.49	4.000	No	Yes	2.00
13	0.87	31.56	70.59	2.59	0.46	1.70	50.72	65.51	116.24	4.000	No	No	2.00
14	0.92	32.87	68.79	2.57	0.46	1.70	52.83	65.75	118.57	4.000	No	No	2.00
15	0.99	33.07	68.79	2.57	0.46	1.70	53.15	65.84	118.99	4.000	No	No	2.00
16	1.05	32.16	70.22	2.59	0.46	1.70	51.69	65.72	117.41	4.000	No	No	2.00
17	1.15	30.96	73.27	2.63	0.47	1.70	49.76	0.00	49.76	4.000	No	Yes	2.00
18	1.20	29.95	75.66	2.66	0.47	1.70	48.13	0.00	48.13	4.000	No	Yes	2.00
19	1.26	29.55	77.13	2.68	0.47	1.70	47.49	0.00	47.49	4.000	No	Yes	2.00
20	1.32	29.55	78.17	2.69	0.47	1.70	47.49	0.00	47.49	4.000	No	Yes	2.00
21	1.39	30.15	78.14	2.69	0.47	1.70	48.46	0.00	48.46	4.000	No	Yes	2.00
22	1.46	31.76	76.43	2.67	0.46	1.70	51.04	0.00	51.04	4.000	No	Yes	2.00
23	1.51	32.06	76.58	2.67	0.46	1.70	51.52	0.00	51.52	4.000	No	Yes	2.00
24	1.58	31.97	77.13	2.68	0.46	1.70	51.36	0.00	51.36	4.000	No	Yes	2.00
25	1.66	33.58	74.32	2.64	0.45	1.70	53.95	0.00	53.95	4.000	No	Yes	2.00
26	1.71	34.89	71.89	2.61	0.45	1.70	56.06	0.00	56.06	4.000	No	Yes	2.00
27	1.79	34.79	71.11	2.60	0.45	1.70	55.90	0.00	55.90	4.000	No	Yes	2.00
28	1.84	33.58	72.46	2.62	0.46	1.70	53.95	0.00	53.95	4.000	No	Yes	2.00
29	1.93	31.06	75.37	2.65	0.46	1.70	49.92	0.00	49.92	4.000	No	Yes	2.00
30	1.98	28.44	79.07	2.70	0.47	1.70	45.71	0.00	45.71	4.000	No	Yes	2.00
31	2.04	26.33	81.84	2.74	0.48	1.70	42.32	0.00	42.32	4.000	No	Yes	2.00
32	2.11	23.82	84.83	2.77	0.49	1.70	38.29	0.00	38.29	4.000	No	Yes	2.00
33	2.17	21.62	88.20	2.81	0.50	1.70	34.74	0.00	34.74	4.000	No	Yes	2.00
34	2.24	20.30	90.28	2.84	0.51	1.70	32.63	0.00	32.63	4.000	No	Yes	2.00
35	2.32	19.61	91.64	2.86	0.51	1.70	31.51	0.00	31.51	4.000	No	Yes	2.00
36	2.38	19.41	92.15	2.86	0.51	1.70	31.18	0.00	31.18	4.000	No	Yes	2.00
37	2.43	20.11	90.41	2.84	0.51	1.70	32.31	0.00	32.31	4.000	No	Yes	2.00
38	2.52	21.42	87.72	2.81	0.50	1.70	34.41	0.00	34.41	4.000	No	Yes	2.00
39	2.56	22.22	85.95	2.79	0.50	1.70	35.70	0.00	35.70	4.000	No	Yes	2.00
40	2.64	23.53	82.62	2.75	0.49	1.70	37.80	0.00	37.80	4.000	No	Yes	2.00
41	2.69	23.73	81.63	2.73	0.49	1.70	38.13	0.00	38.13	4.000	No	Yes	2.00
42	2.78	24.23	79.35	2.70	0.49	1.70	38.93	0.00	38.93	4.000	No	Yes	2.00
43	2.83	26.14	74.73	2.65	0.49	1.70	42.00	0.00	42.00	4.000	No	Yes	2.00
44	2.89	29.66	66.87	2.55	0.47	1.70	47.65	63.82	111.48	4.000	No	No	2.00
45	2.95	33.08	59.29	2.45	0.46	1.70	53.15	63.41	116.55	4.000	No	No	2.00
46	3.02	37.40	50.21	2.34	0.45	1.70	60.09	62.02	122.10	4.000	No	No	2.00
47	3.09	40.62	43.30	2.25	0.45	1.70	65.26	59.81	125.07	4.000	No	No	2.00
48	3.15	41.83	39.03	2.20	0.45	1.70	67.21	57.44	124.64	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
49	3.22	42.33	35.32	2.15	0.45	1.70	68.01	54.60	122.61	4.000	No	No	2.00
50	3.29	42.73	33.45	2.13	0.45	1.70	68.65	52.98	121.63	4.000	No	No	2.00
51	3.35	41.93	33.10	2.13	0.46	1.70	67.37	52.34	119.71	4.000	No	No	2.00
52	3.41	41.02	32.87	2.12	0.46	1.70	65.90	51.79	117.70	4.000	No	No	2.00
53	3.52	38.51	34.80	2.15	0.47	1.70	61.87	52.75	114.62	4.000	No	No	2.00
54	3.55	36.90	36.67	2.17	0.47	1.70	59.29	53.75	113.04	4.000	No	No	2.00
55	3.61	36.10	36.77	2.17	0.47	1.70	58.00	53.54	111.54	4.000	No	No	2.00
56	3.71	36.85	35.46	2.16	0.47	1.70	59.20	52.73	111.94	4.000	No	No	2.00
57	3.75	35.39	37.25	2.18	0.48	1.70	56.86	53.66	110.51	4.000	No	No	2.00
58	3.81	36.80	35.59	2.16	0.47	1.70	59.12	52.82	111.94	4.000	No	No	2.00
59	3.90	40.02	32.84	2.12	0.47	1.70	64.30	51.41	115.71	4.000	No	No	2.00
60	3.95	42.53	29.87	2.09	0.46	1.70	68.33	48.97	117.30	4.000	No	No	2.00
61	4.01	44.04	26.24	2.04	0.47	1.70	70.76	44.51	115.27	4.000	No	No	2.00
62	4.09	47.96	21.00	1.98	0.47	1.70	77.05	36.09	113.14	4.000	No	No	2.00
63	4.15	50.57	19.22	1.95	0.47	1.70	81.25	32.64	113.89	4.000	No	No	2.00
64	4.21	52.79	17.80	1.93	0.47	1.70	84.81	29.53	114.34	4.000	No	No	2.00
65	4.29	53.49	17.87	1.94	0.47	1.70	85.94	29.83	115.77	4.000	No	No	2.00
66	4.34	43.54	28.42	2.07	0.46	1.70	69.95	47.45	117.40	4.000	No	No	2.00
67	4.41	49.97	22.41	1.99	0.46	1.70	80.28	39.47	119.75	4.000	No	No	2.00
68	4.46	48.98	24.46	2.02	0.45	1.70	78.68	43.02	121.69	4.000	No	No	2.00
69	4.55	47.56	27.93	2.06	0.45	1.70	76.41	48.02	124.44	4.000	No	No	2.00
70	4.61	46.45	30.14	2.09	0.45	1.70	74.63	50.58	125.21	4.000	No	No	2.00
71	4.67	45.25	32.24	2.12	0.45	1.70	72.70	52.59	125.29	4.000	No	No	2.00
72	4.75	44.54	34.04	2.14	0.45	1.70	71.56	54.19	125.75	4.000	No	No	2.00
73	4.79	44.54	34.57	2.14	0.44	1.70	71.56	54.70	126.26	4.000	No	No	2.00
74	4.87	45.75	34.45	2.14	0.44	1.70	73.50	55.02	128.52	4.000	No	No	2.00
75	4.93	47.06	34.08	2.14	0.44	1.70	75.61	55.13	130.74	4.000	No	No	2.00
76	4.99	48.46	33.61	2.13	0.43	1.70	77.86	55.15	133.00	4.000	No	No	2.00
77	5.06	50.37	33.07	2.13	0.43	1.70	80.93	55.25	136.18	4.000	No	No	2.00
78	5.14	51.88	32.90	2.12	0.42	1.70	83.14	55.55	138.70	4.000	No	No	2.00
79	5.19	52.69	32.83	2.12	0.42	1.69	83.94	55.65	139.59	4.000	No	No	2.00
80	5.25	54.39	31.96	2.11	0.42	1.67	85.97	55.10	141.07	4.000	No	No	2.00
81	5.33	54.70	32.56	2.12	0.42	1.66	85.87	55.76	141.63	4.000	No	No	2.00
82	5.38	54.40	33.61	2.13	0.42	1.65	85.02	56.72	141.73	4.000	No	No	2.00
83	5.45	52.38	35.76	2.16	0.42	1.65	81.74	58.11	139.86	4.000	No	No	2.00
84	5.52	50.57	36.88	2.17	0.43	1.65	78.90	58.46	137.36	4.000	No	No	2.00
85	5.59	48.46	38.37	2.19	0.43	1.65	75.62	58.93	134.54	4.000	No	No	2.00
86	5.64	46.75	40.16	2.21	0.43	1.65	72.95	59.64	132.59	4.000	No	No	2.00
87	5.72	43.74	43.47	2.26	0.44	1.65	68.36	60.69	129.05	4.000	No	No	2.00
88	5.78	41.22	47.13	2.30	0.45	1.66	64.49	61.72	126.21	4.000	No	No	2.00
89	5.85	38.41	52.87	2.37	0.45	1.66	60.14	63.13	123.27	4.000	No	No	2.00
90	5.92	37.10	56.59	2.42	0.45	1.65	57.94	63.88	121.82	4.000	No	No	2.00
91	5.98	37.15	58.16	2.44	0.45	1.64	57.71	64.33	122.04	4.000	No	No	2.00
92	6.04	37.15	60.88	2.47	0.45	1.63	57.39	65.06	122.45	4.000	No	No	2.00
93	6.11	37.21	63.77	2.51	0.45	1.62	57.13	65.78	122.91	4.000	No	No	2.00
94	6.17	39.21	63.03	2.50	0.45	1.61	59.60	66.29	125.89	4.000	No	No	2.00
95	6.24	40.12	63.34	2.50	0.44	1.59	60.42	66.60	127.02	4.000	No	No	2.00
96	6.32	40.83	63.83	2.51	0.44	1.58	61.00	66.90	127.91	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
97	6.38	42.54	61.83	2.49	0.44	1.57	63.05	66.93	129.99	4.000	No	No	2.00
98	6.44	46.76	56.13	2.41	0.43	1.55	68.39	66.59	134.98	4.000	No	No	2.00
99	6.51	50.99	49.60	2.33	0.42	1.53	73.65	65.32	138.97	4.000	No	No	2.00
100	6.58	54.20	45.32	2.28	0.42	1.51	77.58	64.11	141.69	4.000	No	No	2.00
101	6.66	57.22	41.42	2.23	0.41	1.50	81.21	62.55	143.75	4.000	No	No	2.00
102	6.71	58.73	38.98	2.20	0.41	1.50	83.01	61.17	144.17	4.000	No	No	2.00
103	6.77	60.44	36.42	2.17	0.41	1.49	85.04	59.47	144.51	4.000	No	No	2.00
104	6.83	65.67	31.59	2.11	0.41	1.48	91.64	55.86	147.50	4.000	No	No	2.00
105	6.92	70.69	27.34	2.05	0.40	1.46	97.82	51.22	149.04	4.000	No	No	2.00
106	6.97	77.13	23.21	2.00	0.40	1.46	106.06	45.17	151.23	4.000	No	No	2.00
107	7.03	82.16	20.69	1.97	0.40	1.45	112.34	40.40	152.75	4.000	No	No	2.00
108	7.10	87.99	18.33	1.94	0.39	1.44	119.49	35.05	154.54	4.000	No	No	2.00
109	7.16	90.20	18.21	1.94	0.39	1.43	121.65	34.94	156.59	4.000	No	No	2.00
110	7.22	92.01	17.87	1.94	0.39	1.42	123.51	34.16	157.67	4.000	No	No	2.00
111	7.31	93.01	17.88	1.94	0.39	1.41	124.09	34.25	158.34	4.000	No	No	2.00
112	7.36	93.01	18.14	1.94	0.39	1.41	123.71	35.00	158.71	4.000	No	No	2.00
113	7.42	93.01	17.94	1.94	0.39	1.40	123.46	34.37	157.83	4.000	No	No	2.00
114	7.49	91.91	17.88	1.94	0.39	1.40	121.86	34.01	155.87	4.000	No	No	2.00
115	7.55	90.40	18.47	1.94	0.39	1.40	119.61	35.45	155.06	4.000	No	No	2.00
116	7.62	89.09	19.09	1.95	0.40	1.40	117.55	36.94	154.49	4.000	No	No	2.00
117	7.71	85.78	20.65	1.97	0.40	1.39	112.81	40.36	153.18	4.000	No	No	2.00
118	7.75	79.34	24.07	2.01	0.40	1.39	104.45	46.65	151.10	4.000	No	No	2.00
119	7.83	80.85	22.79	2.00	0.40	1.39	106.06	44.29	150.35	4.000	No	No	2.00
120	7.88	79.74	23.27	2.00	0.40	1.39	104.47	45.04	149.51	4.000	No	No	2.00
121	7.95	77.83	23.96	2.01	0.41	1.38	101.84	46.00	147.83	4.000	No	No	2.00
122	8.01	74.01	26.58	2.04	0.41	1.38	96.69	49.80	146.49	0.267	No	No	0.48
123	8.09	71.80	28.04	2.06	0.41	1.38	93.60	51.50	145.09	0.260	No	No	0.46
124	8.14	69.69	29.43	2.08	0.41	1.38	90.76	52.92	143.68	0.252	No	No	0.45
125	8.24	67.17	31.22	2.10	0.42	1.37	87.27	54.50	141.77	0.243	No	No	0.43
126	8.29	66.27	31.84	2.11	0.42	1.37	85.98	54.97	140.95	0.239	No	No	0.42
127	8.34	64.96	32.76	2.12	0.42	1.37	84.18	55.62	139.80	0.234	No	No	0.41
128	8.41	63.66	33.73	2.13	0.42	1.37	82.33	56.25	138.59	0.229	No	No	0.40
129	8.49	61.34	35.39	2.15	0.43	1.37	79.23	57.20	136.43	0.220	No	No	0.38
130	8.53	60.04	36.40	2.17	0.43	1.37	77.48	57.72	135.20	0.215	No	No	0.37
131	8.60	57.52	38.65	2.20	0.43	1.37	74.24	58.83	133.07	0.208	No	No	0.36
132	8.67	55.51	40.40	2.22	0.44	1.36	71.58	59.48	131.07	0.201	No	No	0.34
133	8.73	53.70	42.74	2.25	0.44	1.36	69.16	60.44	129.60	0.196	No	No	0.33
134	8.80	48.98	48.30	2.32	0.45	1.37	63.21	61.96	125.17	0.184	No	No	0.31
135	8.87	47.36	51.15	2.35	0.45	1.36	61.01	62.66	123.67	0.180	No	No	0.30
136	8.93	45.85	52.92	2.37	0.45	1.36	59.03	62.85	121.88	0.176	No	No	0.29
137	9.02	45.75	52.85	2.37	0.45	1.36	58.66	62.72	121.38	0.175	No	No	0.29
138	9.07	45.25	53.21	2.38	0.46	1.35	57.91	62.66	120.57	0.173	No	No	0.28
139	9.13	45.45	52.84	2.37	0.46	1.35	58.02	62.54	120.56	0.173	No	No	0.28
140	9.20	45.55	51.98	2.36	0.46	1.35	57.96	62.19	120.14	0.172	No	No	0.28
141	9.25	45.36	51.21	2.35	0.46	1.34	57.60	61.78	119.38	0.170	No	No	0.28
142	9.32	44.95	50.52	2.34	0.46	1.34	56.97	61.32	118.28	0.168	No	No	0.27
143	9.39	43.85	50.38	2.34	0.46	1.34	55.51	60.87	116.38	0.164	No	No	0.26
144	9.46	42.74	50.40	2.34	0.47	1.34	54.05	60.49	114.54	0.160	No	No	0.26

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
145	9.52	40.83	51.26	2.35	0.47	1.34	51.64	60.20	111.84	0.155	No	No	0.25
146	9.61	37.41	54.07	2.39	0.48	1.34	47.37	60.11	107.48	0.148	No	No	0.23
147	9.66	36.21	55.29	2.40	0.49	1.34	45.81	60.11	105.92	0.146	No	No	0.23
148	9.71	34.50	57.17	2.43	0.49	1.34	43.66	60.12	103.78	0.143	No	No	0.22
149	9.78	33.29	58.23	2.44	0.49	1.34	42.07	60.00	102.07	0.140	No	No	0.22
150	9.86	34.45	56.17	2.41	0.49	1.33	43.31	59.71	103.02	0.142	No	No	0.22
151	9.91	33.84	57.04	2.43	0.49	1.33	42.48	59.75	102.23	0.140	No	No	0.22
152	9.97	34.39	57.35	2.43	0.49	1.32	43.01	60.00	103.00	0.141	No	No	0.22
153	10.06	36.00	57.07	2.43	0.49	1.31	44.74	60.39	105.13	0.145	No	No	0.22
154	10.11	37.81	55.45	2.41	0.48	1.31	46.76	60.42	107.18	0.148	No	No	0.23
155	10.17	39.92	53.76	2.38	0.48	1.30	49.08	60.47	109.55	0.151	No	No	0.23
156	10.25	42.33	51.73	2.36	0.47	1.29	51.71	60.41	112.12	0.156	No	No	0.24
157	10.31	44.34	49.98	2.34	0.47	1.29	53.90	60.28	114.18	0.160	No	No	0.24
158	10.37	47.46	46.96	2.30	0.46	1.28	57.35	59.79	117.14	0.165	No	No	0.25
159	10.44	50.07	44.42	2.27	0.46	1.27	60.19	59.18	119.37	0.170	No	No	0.26
160	10.50	52.38	42.40	2.24	0.45	1.27	62.68	58.62	121.30	0.174	No	No	0.27
161	10.57	54.71	40.28	2.22	0.45	1.26	65.15	57.84	122.98	0.178	No	No	0.27
162	10.64	55.91	39.27	2.20	0.45	1.26	66.32	57.40	123.73	0.180	No	No	0.28
163	10.70	56.82	38.71	2.20	0.45	1.25	67.20	57.20	124.40	0.182	No	No	0.28
164	10.77	57.02	38.58	2.19	0.45	1.25	67.22	57.11	124.33	0.182	No	No	0.28
165	10.85	59.13	37.28	2.18	0.45	1.24	69.40	56.60	125.99	0.186	No	No	0.28
166	10.90	59.83	36.99	2.17	0.44	1.24	70.03	56.51	126.54	0.188	No	No	0.28
167	10.97	60.54	37.40	2.18	0.44	1.23	70.59	56.97	127.56	0.190	No	No	0.29
168	11.03	61.54	37.44	2.18	0.44	1.23	71.51	57.22	128.73	0.194	No	No	0.29
169	11.09	61.75	37.96	2.19	0.44	1.23	71.54	57.64	129.18	0.195	No	No	0.29
170	11.17	61.95	38.50	2.19	0.44	1.22	71.53	58.07	129.59	0.196	No	No	0.29
171	11.26	61.95	39.47	2.21	0.44	1.22	71.24	58.73	129.97	0.198	No	No	0.30
172	11.30	61.85	39.77	2.21	0.44	1.22	71.03	58.90	129.92	0.197	No	No	0.30
173	11.36	61.14	40.62	2.22	0.44	1.21	70.08	59.27	129.35	0.196	No	No	0.29
174	11.42	59.73	41.88	2.24	0.44	1.21	68.35	59.69	128.05	0.192	No	No	0.28
175	11.50	57.92	43.09	2.25	0.45	1.21	66.19	59.92	126.11	0.186	No	No	0.28
176	11.56	56.11	44.19	2.26	0.45	1.21	64.07	60.04	124.10	0.181	No	No	0.27
177	11.62	53.60	46.03	2.29	0.45	1.21	61.18	60.31	121.48	0.175	No	No	0.26
178	11.69	50.99	47.75	2.31	0.46	1.21	58.18	60.39	118.57	0.168	No	No	0.24
179	11.76	48.37	49.49	2.33	0.47	1.21	55.17	60.40	115.57	0.162	No	No	0.23
180	11.83	47.37	49.86	2.34	0.47	1.21	53.94	60.23	114.17	0.160	No	No	0.23
181	11.88	46.96	49.85	2.34	0.47	1.20	53.38	60.08	113.46	0.158	No	No	0.23
182	11.95	46.26	50.55	2.34	0.47	1.20	52.48	60.14	112.62	0.157	No	No	0.22
183	12.01	45.56	51.46	2.36	0.47	1.20	51.60	60.27	111.88	0.155	No	No	0.22
184	12.08	44.45	53.39	2.38	0.48	1.20	50.24	60.64	110.88	0.154	No	No	0.22
185	12.14	44.24	54.73	2.40	0.47	1.19	49.89	61.03	110.92	0.154	No	No	0.22
186	12.23	42.94	57.60	2.43	0.48	1.19	48.28	61.53	109.82	0.152	No	No	0.21
187	12.28	43.13	58.01	2.44	0.48	1.19	48.41	61.70	110.11	0.152	No	No	0.21
188	12.35	43.14	59.13	2.45	0.48	1.18	48.26	61.99	110.25	0.153	No	No	0.21
189	12.40	43.14	59.78	2.46	0.48	1.18	48.17	62.16	110.32	0.153	No	No	0.21
190	12.47	44.45	58.86	2.45	0.47	1.18	49.45	62.24	111.70	0.155	No	No	0.22
191	12.54	45.46	58.95	2.45	0.47	1.17	50.39	62.53	112.92	0.157	No	No	0.22
192	12.60	46.75	58.60	2.45	0.47	1.17	51.66	62.78	114.45	0.160	No	No	0.22

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
193	12.70	46.35	60.27	2.47	0.47	1.17	51.05	63.11	114.16	0.160	No	No	0.22
194	12.75	46.55	60.29	2.47	0.47	1.16	51.17	63.14	114.31	0.160	No	No	0.22
195	12.80	46.65	60.25	2.47	0.47	1.16	51.17	63.13	114.30	0.160	No	No	0.22
196	12.87	46.85	59.85	2.46	0.47	1.16	51.25	63.04	114.30	0.160	No	No	0.22
197	12.93	47.46	59.05	2.45	0.47	1.15	51.80	62.96	114.76	0.161	No	No	0.22
198	12.99	50.27	56.20	2.42	0.46	1.15	54.64	62.84	117.48	0.166	No	No	0.23
199	13.06	52.38	53.68	2.38	0.46	1.15	56.75	62.52	119.26	0.170	No	No	0.24
200	13.14	55.30	50.30	2.34	0.45	1.14	59.66	61.94	121.60	0.175	No	No	0.24
201	13.19	56.10	49.14	2.33	0.45	1.14	60.40	61.62	122.02	0.176	No	No	0.24
202	13.26	57.71	47.13	2.30	0.45	1.14	61.94	61.06	123.00	0.178	No	No	0.25
203	13.32	57.61	47.20	2.30	0.45	1.13	61.71	61.04	122.75	0.178	No	No	0.25
204	13.40	58.12	46.97	2.30	0.45	1.13	62.09	61.02	123.11	0.179	No	No	0.25
205	13.46	58.42	46.58	2.29	0.45	1.13	62.28	60.87	123.15	0.179	No	No	0.25
206	13.53	58.52	46.57	2.29	0.45	1.13	62.24	60.86	123.10	0.179	No	No	0.24
207	13.58	58.12	48.40	2.32	0.45	1.12	61.69	61.62	123.31	0.179	No	No	0.25
208	13.68	56.80	52.05	2.36	0.45	1.12	60.11	62.79	122.91	0.178	No	No	0.24
209	13.73	55.89	53.58	2.38	0.45	1.12	59.07	63.11	122.18	0.176	No	No	0.24
210	13.79	53.40	56.47	2.42	0.46	1.12	56.37	63.40	119.78	0.171	No	No	0.23
211	13.88	53.48	57.10	2.43	0.46	1.11	56.30	63.60	119.90	0.171	No	No	0.23
212	13.92	53.58	57.03	2.43	0.46	1.11	56.32	63.58	119.90	0.171	No	No	0.23
213	13.98	54.69	56.06	2.41	0.46	1.11	57.34	63.53	120.88	0.173	No	No	0.23
214	14.05	57.01	54.31	2.39	0.45	1.11	59.59	63.52	123.11	0.179	No	No	0.24
215	14.13	58.82	52.70	2.37	0.45	1.10	61.28	63.36	124.64	0.183	No	No	0.25
216	14.17	60.33	51.33	2.35	0.45	1.10	62.72	63.19	125.91	0.186	No	No	0.25
217	14.24	63.65	48.63	2.32	0.44	1.10	65.95	62.84	128.79	0.194	No	No	0.26
218	14.33	65.86	46.59	2.29	0.44	1.09	68.02	62.36	130.37	0.199	No	No	0.27
219	14.37	68.47	44.50	2.27	0.43	1.09	70.56	61.86	132.41	0.205	No	No	0.28
220	14.45	71.39	42.36	2.24	0.43	1.09	73.33	61.24	134.57	0.213	No	No	0.29
221	14.53	73.90	40.97	2.22	0.43	1.08	75.69	60.88	136.58	0.220	No	No	0.30
222	14.57	76.10	39.83	2.21	0.42	1.08	77.80	60.57	138.37	0.228	No	No	0.31
223	14.64	79.23	38.02	2.19	0.42	1.08	80.75	59.86	140.61	0.237	No	No	0.32
224	14.72	80.93	37.14	2.18	0.42	1.08	82.29	59.48	141.76	0.243	No	No	0.33
225	14.76	82.55	36.29	2.17	0.42	1.07	83.79	59.06	142.85	0.248	No	No	0.34
226	14.85	84.85	35.16	2.15	0.41	1.07	85.89	58.48	144.36	0.256	No	No	0.35
227	14.90	86.66	34.29	2.14	0.41	1.07	87.56	57.99	145.55	0.262	No	No	0.35
228	14.96	88.97	33.24	2.13	0.41	1.07	89.70	57.34	147.04	0.270	No	No	0.37
229	15.03	91.80	31.70	2.11	0.41	1.06	92.32	56.13	148.45	0.279	No	No	0.38
230	15.10	93.00	31.24	2.10	0.40	1.06	93.34	55.79	149.13	0.283	No	No	0.38
231	15.16	94.21	30.68	2.10	0.40	1.06	94.38	55.30	149.68	0.287	No	No	0.39
232	15.24	94.81	30.50	2.09	0.40	1.06	94.76	55.15	149.91	0.288	No	No	0.39
233	15.31	94.61	30.72	2.10	0.40	1.06	94.40	55.36	149.75	0.287	No	No	0.39
234	15.36	94.21	30.87	2.10	0.40	1.05	93.87	55.43	149.30	0.284	No	No	0.38
235	15.45	90.59	32.51	2.12	0.41	1.05	90.10	56.61	146.72	0.269	No	No	0.36
236	15.50	88.38	33.40	2.13	0.41	1.05	87.81	57.11	144.92	0.259	No	No	0.34
237	15.55	85.26	34.82	2.15	0.42	1.05	84.63	57.86	142.49	0.246	No	No	0.33
238	15.66	79.63	36.93	2.17	0.42	1.05	78.89	58.50	137.39	0.224	No	No	0.29
239	15.69	77.32	37.85	2.19	0.43	1.05	76.57	58.73	135.30	0.216	No	No	0.28
240	15.75	73.90	38.90	2.20	0.43	1.05	73.10	58.74	131.84	0.203	No	No	0.27

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
241	15.82	69.98	41.18	2.23	0.44	1.05	69.13	59.42	128.56	0.193	No	No	0.25
242	15.91	66.46	44.71	2.27	0.44	1.04	65.52	60.70	126.22	0.187	No	No	0.24
243	15.96	62.44	48.46	2.32	0.45	1.04	61.50	61.60	123.10	0.179	No	No	0.23
244	16.02	58.01	53.03	2.38	0.46	1.04	57.08	62.36	119.44	0.170	No	No	0.22
245	16.08	55.00	57.49	2.43	0.46	1.04	54.03	63.09	117.12	0.165	No	No	0.21
246	16.14	52.18	60.56	2.47	0.47	1.04	51.19	63.23	114.42	0.160	No	No	0.20
247	16.22	47.16	67.05	2.55	0.48	1.04	46.20	63.44	109.64	0.152	No	No	0.19
248	16.30	43.64	73.27	2.63	0.48	1.03	42.66	0.00	42.66	4.000	No	Yes	2.00
249	16.34	37.60	81.80	2.73	0.50	1.03	36.75	0.00	36.75	4.000	No	Yes	2.00
250	16.42	39.82	76.19	2.66	0.49	1.03	38.82	0.00	38.82	4.000	No	Yes	2.00
251	16.50	40.11	77.93	2.69	0.49	1.03	39.01	0.00	39.01	4.000	No	Yes	2.00
252	16.54	41.72	76.79	2.67	0.49	1.03	40.51	0.00	40.51	4.000	No	Yes	2.00
253	16.62	42.12	75.76	2.66	0.49	1.02	40.80	0.00	40.80	4.000	No	Yes	2.00
254	16.70	43.93	76.65	2.67	0.48	1.02	42.45	0.00	42.45	4.000	No	Yes	2.00
255	16.74	45.74	75.83	2.66	0.48	1.02	44.13	0.00	44.13	4.000	No	Yes	2.00
256	16.80	51.77	71.59	2.61	0.47	1.02	49.83	0.00	49.83	4.000	No	Yes	2.00
257	16.87	60.72	64.76	2.52	0.45	1.02	58.28	66.37	124.65	0.183	No	No	0.23
258	16.94	67.76	60.12	2.46	0.43	1.01	64.89	66.95	131.83	0.203	No	No	0.26
259	17.01	81.73	51.34	2.35	0.41	1.01	78.08	67.31	145.38	0.261	No	No	0.34
260	17.09	87.35	48.25	2.32	0.40	1.01	83.27	67.18	150.46	0.292	No	No	0.38
261	17.14	93.39	44.73	2.27	0.39	1.01	88.90	66.64	155.54	0.330	No	No	0.43
262	17.23	103.34	38.64	2.20	0.38	1.00	98.15	64.49	162.63	0.401	No	No	0.52
263	17.28	106.96	35.93	2.16	0.38	1.00	101.45	62.76	164.21	0.420	No	No	0.55
264	17.34	109.07	33.94	2.14	0.38	1.00	103.32	61.10	164.42	0.422	No	No	0.55
265	17.39	110.79	32.41	2.12	0.38	1.00	104.81	59.65	164.46	0.423	No	No	0.55
266	17.46	112.80	31.34	2.10	0.38	1.00	106.54	58.67	165.21	0.433	No	No	0.57
267	17.52	113.81	30.95	2.10	0.38	1.00	107.34	58.34	165.68	0.439	No	No	0.57
268	17.60	114.01	30.94	2.10	0.38	1.00	107.33	58.32	165.66	0.438	No	No	0.57
269	17.66	113.71	31.12	2.10	0.38	0.99	106.92	58.48	165.40	0.435	No	No	0.57
270	17.73	112.30	31.66	2.11	0.38	0.99	105.41	58.85	164.26	0.420	No	No	0.55
271	17.79	109.89	32.88	2.12	0.38	0.99	103.01	59.82	162.83	0.403	No	No	0.52
272	17.86	107.17	34.60	2.14	0.38	0.99	100.31	61.14	161.45	0.387	No	No	0.50
273	17.92	105.06	35.79	2.16	0.39	0.99	98.19	61.88	160.07	0.372	No	No	0.48
274	17.98	102.35	37.35	2.18	0.39	0.99	95.51	62.73	158.24	0.354	No	No	0.45
275	18.07	100.74	38.21	2.19	0.39	0.99	93.82	63.09	156.91	0.342	No	No	0.44
276	18.11	99.83	38.72	2.20	0.39	0.98	92.87	63.30	156.16	0.335	No	No	0.43
277	18.18	97.82	39.96	2.21	0.40	0.98	90.84	63.81	154.65	0.323	No	No	0.41
278	18.27	97.22	39.97	2.21	0.40	0.98	90.11	63.64	153.75	0.316	No	No	0.40
279	18.32	96.41	40.34	2.22	0.40	0.98	89.24	63.71	152.96	0.310	No	No	0.39
280	18.37	95.51	40.71	2.22	0.40	0.98	88.30	63.77	152.06	0.303	No	No	0.38
281	18.46	91.99	41.21	2.23	0.41	0.98	84.84	63.29	148.13	0.277	No	No	0.35
282	18.52	89.27	41.58	2.23	0.41	0.97	82.20	62.90	145.10	0.260	No	No	0.32
283	18.57	84.55	43.42	2.26	0.42	0.97	77.72	63.00	140.73	0.238	No	No	0.30
284	18.66	75.20	48.48	2.32	0.43	0.97	68.91	63.54	132.45	0.205	No	No	0.25
285	18.71	69.57	52.19	2.36	0.44	0.97	63.63	63.80	127.43	0.190	No	No	0.23
286	18.77	60.22	59.05	2.45	0.46	0.97	54.93	63.83	118.76	0.169	No	No	0.21
287	18.84	52.37	65.38	2.53	0.47	0.96	47.63	63.47	111.09	0.154	No	No	0.19
288	18.91	46.85	70.53	2.59	0.49	0.96	42.48	63.10	105.58	0.145	No	No	0.17

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
289	18.97	43.74	73.92	2.64	0.49	0.96	39.58	0.00	39.58	4.000	No	Yes	2.00
290	19.05	36.30	83.59	2.76	0.51	0.95	32.73	0.00	32.73	4.000	No	Yes	2.00
291	19.10	32.98	88.54	2.82	0.52	0.95	29.67	0.00	29.67	4.000	No	Yes	2.00
292	19.16	31.87	90.36	2.84	0.52	0.95	28.62	0.00	28.62	4.000	No	Yes	2.00
293	19.26	28.86	94.85	2.90	0.53	0.95	25.83	0.00	25.83	4.000	No	Yes	2.00
294	19.30	26.85	97.65	2.93	0.53	0.95	23.99	0.00	23.99	4.000	No	Yes	2.00
295	19.36	24.53	100.00	2.97	0.54	0.94	21.86	0.00	21.86	4.000	No	Yes	2.00
296	19.43	24.73	97.16	2.93	0.54	0.94	22.00	0.00	22.00	4.000	No	Yes	2.00
297	19.51	23.13	93.69	2.88	0.55	0.94	20.52	0.00	20.52	4.000	No	Yes	2.00
298	19.55	22.12	97.23	2.93	0.55	0.94	19.59	0.00	19.59	4.000	No	Yes	2.00
299	19.63	22.12	98.84	2.95	0.55	0.94	19.55	0.00	19.55	4.000	No	Yes	2.00
300	19.69	22.12	99.69	2.96	0.55	0.93	19.52	0.00	19.52	4.000	No	Yes	2.00
301	19.75	22.92	98.80	2.95	0.55	0.93	20.20	0.00	20.20	4.000	No	Yes	2.00
302	19.84	23.60	99.65	2.96	0.54	0.93	20.78	0.00	20.78	4.000	No	Yes	2.00
303	19.89	24.60	98.31	2.94	0.54	0.93	21.64	0.00	21.64	4.000	No	Yes	2.00
304	19.96	24.18	99.95	2.96	0.54	0.93	21.24	0.00	21.24	4.000	No	Yes	2.00
305	20.02	25.59	97.21	2.93	0.54	0.93	22.46	0.00	22.46	4.000	No	Yes	2.00
306	20.09	26.09	96.68	2.92	0.54	0.93	22.86	0.00	22.86	4.000	No	Yes	2.00
307	20.14	26.80	95.95	2.91	0.54	0.92	23.45	0.00	23.45	4.000	No	Yes	2.00
308	20.22	27.93	95.21	2.90	0.53	0.92	24.37	0.00	24.37	4.000	No	Yes	2.00
309	20.28	29.46	93.27	2.88	0.53	0.92	25.66	0.00	25.66	4.000	No	Yes	2.00
310	20.36	30.26	93.43	2.88	0.53	0.92	26.31	0.00	26.31	4.000	No	Yes	2.00
311	20.41	31.77	91.86	2.86	0.52	0.92	27.61	0.00	27.61	4.000	No	Yes	2.00
312	20.48	32.88	91.08	2.85	0.52	0.92	28.53	0.00	28.53	4.000	No	Yes	2.00
313	20.55	35.30	87.77	2.81	0.51	0.92	30.60	0.00	30.60	4.000	No	Yes	2.00
314	20.61	36.10	86.70	2.80	0.51	0.92	31.26	0.00	31.26	4.000	No	Yes	2.00
315	20.68	36.70	85.89	2.79	0.51	0.91	31.73	0.00	31.73	4.000	No	Yes	2.00
316	20.74	38.61	83.56	2.76	0.51	0.91	33.36	0.00	33.36	4.000	No	Yes	2.00
317	20.81	40.32	82.25	2.74	0.50	0.91	34.79	0.00	34.79	4.000	No	Yes	2.00
318	20.88	41.12	81.99	2.74	0.50	0.91	35.44	0.00	35.44	4.000	No	Yes	2.00
319	20.93	40.62	83.40	2.75	0.50	0.91	34.95	0.00	34.95	4.000	No	Yes	2.00
320	21.00	40.72	83.85	2.76	0.50	0.91	34.99	0.00	34.99	4.000	No	Yes	2.00
321	21.07	40.52	84.79	2.77	0.50	0.91	34.75	0.00	34.75	4.000	No	Yes	2.00
322	21.13	39.92	86.20	2.79	0.50	0.91	34.18	0.00	34.18	4.000	No	Yes	2.00
323	21.22	39.51	87.55	2.81	0.51	0.90	33.75	0.00	33.75	4.000	No	Yes	2.00
324	21.27	39.61	87.71	2.81	0.50	0.90	33.80	0.00	33.80	4.000	No	Yes	2.00
325	21.34	41.01	86.08	2.79	0.50	0.90	34.96	0.00	34.96	4.000	No	Yes	2.00
326	21.41	40.51	86.81	2.80	0.50	0.90	34.47	0.00	34.47	4.000	No	Yes	2.00
327	21.46	40.11	87.48	2.81	0.50	0.90	34.08	0.00	34.08	4.000	No	Yes	2.00
328	21.55	41.72	85.96	2.79	0.50	0.90	35.39	0.00	35.39	4.000	No	Yes	2.00
329	21.59	43.53	84.02	2.76	0.50	0.90	36.92	0.00	36.92	4.000	No	Yes	2.00
330	21.66	44.83	82.47	2.74	0.49	0.90	37.99	0.00	37.99	4.000	No	Yes	2.00
331	21.76	47.75	79.07	2.70	0.49	0.90	40.42	0.00	40.42	4.000	No	Yes	2.00
332	21.80	48.65	78.19	2.69	0.49	0.90	41.16	0.00	41.16	4.000	No	Yes	2.00
333	21.86	49.96	77.02	2.68	0.48	0.89	42.23	0.00	42.23	4.000	No	Yes	2.00
334	21.95	53.28	73.92	2.64	0.48	0.89	45.02	0.00	45.02	4.000	No	Yes	2.00
335	22.01	55.59	71.68	2.61	0.47	0.89	46.95	0.00	46.95	4.000	No	Yes	2.00
336	22.06	57.90	69.53	2.58	0.47	0.89	48.89	64.76	113.66	0.159	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
337	22.12	59.81	67.85	2.56	0.47	0.89	50.48	64.86	115.35	0.162	No	No	0.19
338	22.18	62.13	65.95	2.54	0.46	0.89	52.42	64.98	117.40	0.166	No	No	0.19
339	22.26	65.14	63.59	2.51	0.46	0.89	54.94	65.11	120.05	0.172	No	No	0.20
340	22.31	67.76	61.60	2.48	0.45	0.89	57.15	65.20	122.35	0.177	No	No	0.21
341	22.38	72.58	57.90	2.44	0.44	0.89	61.25	65.23	126.48	0.187	No	No	0.22
342	22.44	76.61	54.29	2.39	0.44	0.89	64.66	64.90	129.55	0.196	No	No	0.23
343	22.53	83.24	48.23	2.32	0.43	0.89	70.28	63.78	134.05	0.211	No	No	0.25
344	22.59	86.66	46.20	2.29	0.43	0.89	73.18	63.48	136.66	0.221	No	No	0.26
345	22.65	89.69	44.53	2.27	0.42	0.89	75.71	63.18	138.89	0.230	No	No	0.27
346	22.71	93.61	42.41	2.24	0.42	0.89	79.04	62.68	141.72	0.242	No	No	0.28
347	22.78	97.73	40.44	2.22	0.41	0.89	82.51	62.16	144.68	0.257	No	No	0.30
348	22.86	99.94	39.68	2.21	0.41	0.89	84.31	62.02	146.33	0.266	No	No	0.31
349	22.92	102.15	38.79	2.20	0.41	0.89	86.15	61.76	147.91	0.276	No	No	0.32
350	22.98	102.66	38.80	2.20	0.41	0.89	86.50	61.86	148.36	0.278	No	No	0.33
351	23.04	103.16	39.08	2.20	0.41	0.89	86.86	62.17	149.03	0.283	No	No	0.33
352	23.10	103.26	39.90	2.21	0.40	0.89	86.87	62.81	149.68	0.287	No	No	0.34
353	23.16	102.86	40.51	2.22	0.40	0.89	86.43	63.16	149.59	0.286	No	No	0.34
354	23.25	102.86	40.98	2.22	0.40	0.89	86.29	63.48	149.77	0.287	No	No	0.34
355	23.30	102.86	41.28	2.23	0.40	0.89	86.23	63.68	149.90	0.288	No	No	0.34
356	23.36	102.86	41.69	2.23	0.40	0.89	86.14	63.95	150.09	0.289	No	No	0.34
357	23.43	102.96	42.32	2.24	0.40	0.89	86.13	64.38	150.51	0.292	No	No	0.34
358	23.49	102.96	42.90	2.25	0.40	0.88	86.05	64.75	150.80	0.294	No	No	0.34
359	23.56	103.66	43.26	2.25	0.40	0.88	86.57	65.12	151.68	0.300	No	No	0.35
360	23.65	104.37	43.40	2.26	0.40	0.88	87.06	65.33	152.39	0.306	No	No	0.36
361	23.71	103.76	43.94	2.26	0.40	0.88	86.44	65.52	151.97	0.302	No	No	0.35
362	23.76	102.56	44.41	2.27	0.40	0.88	85.32	65.54	150.85	0.295	No	No	0.34
363	23.83	97.33	46.44	2.29	0.41	0.88	80.67	65.54	146.21	0.266	No	No	0.31
364	23.89	92.40	48.36	2.32	0.42	0.87	76.31	65.42	141.73	0.242	No	No	0.28
365	23.95	83.65	52.26	2.37	0.43	0.87	68.69	65.18	133.88	0.210	No	No	0.24
366	24.02	74.10	57.28	2.43	0.45	0.86	60.46	64.81	125.27	0.184	No	No	0.21
367	24.09	64.15	63.17	2.50	0.46	0.86	51.98	64.16	116.14	0.163	No	No	0.19
368	24.15	50.68	74.03	2.64	0.49	0.85	40.66	0.00	40.66	4.000	No	Yes	2.00
369	24.24	40.12	83.72	2.76	0.51	0.84	31.89	0.00	31.89	4.000	No	Yes	2.00
370	24.29	35.29	89.15	2.83	0.52	0.84	27.92	0.00	27.92	4.000	No	Yes	2.00
371	24.35	29.86	96.11	2.91	0.53	0.83	23.50	0.00	23.50	4.000	No	Yes	2.00
372	24.42	27.15	98.02	2.94	0.54	0.83	21.28	0.00	21.28	4.000	No	Yes	2.00
373	24.49	26.04	97.79	2.93	0.55	0.83	20.36	0.00	20.36	4.000	No	Yes	2.00
374	24.54	25.44	97.36	2.93	0.55	0.83	19.85	0.00	19.85	4.000	No	Yes	2.00
375	24.62	25.94	95.26	2.90	0.55	0.82	20.21	0.00	20.21	4.000	No	Yes	2.00
376	24.69	25.84	95.52	2.91	0.55	0.82	20.10	0.00	20.10	4.000	No	Yes	2.00
377	24.75	27.55	92.24	2.87	0.54	0.82	21.44	0.00	21.44	4.000	No	Yes	2.00
378	24.81	30.67	88.02	2.81	0.54	0.82	23.90	0.00	23.90	4.000	No	Yes	2.00
379	24.88	33.38	87.33	2.80	0.53	0.83	26.03	0.00	26.03	4.000	No	Yes	2.00
380	24.94	37.50	84.94	2.77	0.52	0.83	29.31	0.00	29.31	4.000	No	Yes	2.00
381	25.00	51.18	71.46	2.61	0.49	0.83	40.35	0.00	40.35	4.000	No	Yes	2.00
382	25.07	64.75	62.04	2.49	0.47	0.84	51.47	63.72	115.19	0.161	No	No	0.18
383	25.13	68.08	61.35	2.48	0.46	0.84	54.18	64.29	118.47	0.168	No	No	0.19
384	25.22	79.34	56.90	2.42	0.44	0.85	63.51	65.52	129.03	0.195	No	No	0.22

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
385	25.27	84.57	54.83	2.40	0.43	0.85	67.87	65.97	133.84	0.210	No	No	0.24
386	25.33	88.79	53.20	2.38	0.42	0.85	71.35	66.29	137.64	0.225	No	No	0.26
387	25.40	92.71	50.94	2.35	0.42	0.85	74.57	66.19	140.76	0.238	No	No	0.27
388	25.48	92.71	49.23	2.33	0.42	0.85	74.41	65.35	139.76	0.234	No	No	0.27
389	25.53	90.70	49.36	2.33	0.42	0.85	72.63	64.95	137.58	0.224	No	No	0.25
390	25.60	84.97	52.74	2.37	0.43	0.84	67.73	65.12	132.86	0.207	No	No	0.23
391	25.67	81.75	54.53	2.39	0.44	0.84	64.96	65.07	130.03	0.198	No	No	0.22
392	25.73	76.93	57.68	2.43	0.45	0.84	60.88	65.06	125.94	0.186	No	No	0.21
393	25.79	68.68	63.61	2.51	0.46	0.83	54.00	64.85	118.85	0.169	No	No	0.19
394	25.87	56.71	73.94	2.64	0.48	0.82	44.15	0.00	44.15	4.000	No	Yes	2.00
395	25.92	54.29	76.35	2.67	0.48	0.82	42.15	0.00	42.15	4.000	No	Yes	2.00
396	26.00	45.64	85.63	2.78	0.50	0.81	35.15	0.00	35.15	4.000	No	Yes	2.00
397	26.07	40.31	91.58	2.86	0.51	0.81	30.85	0.00	30.85	4.000	No	Yes	2.00
398	26.12	36.79	95.66	2.91	0.52	0.81	28.05	0.00	28.05	4.000	No	Yes	2.00
399	26.19	32.67	100.00	2.96	0.53	0.80	24.77	0.00	24.77	4.000	No	Yes	2.00
400	26.25	29.45	100.00	3.01	0.54	0.80	22.23	0.00	22.23	4.000	No	Yes	2.00
401	26.33	27.64	100.00	3.03	0.54	0.80	20.79	0.00	20.79	4.000	No	Yes	2.00
402	26.39	27.64	100.00	3.02	0.54	0.79	20.76	0.00	20.76	4.000	No	Yes	2.00
403	26.45	28.75	100.00	2.99	0.54	0.79	21.59	0.00	21.59	4.000	No	Yes	2.00
404	26.52	30.56	98.76	2.95	0.54	0.79	22.96	0.00	22.96	4.000	No	Yes	2.00
405	26.58	32.77	94.86	2.90	0.53	0.80	24.64	0.00	24.64	4.000	No	Yes	2.00
406	26.66	36.89	90.69	2.85	0.52	0.80	27.80	0.00	27.80	4.000	No	Yes	2.00
407	26.72	40.51	86.95	2.80	0.51	0.80	30.59	0.00	30.59	4.000	No	Yes	2.00
408	26.78	45.64	81.26	2.73	0.50	0.80	34.59	0.00	34.59	4.000	No	Yes	2.00
409	26.84	55.69	70.92	2.60	0.49	0.81	42.50	63.18	105.67	0.145	No	No	0.16
410	26.91	61.83	65.33	2.53	0.48	0.81	47.34	63.37	110.71	0.153	No	No	0.17
411	26.97	65.75	62.42	2.49	0.47	0.81	50.43	63.53	113.96	0.159	No	No	0.18
412	27.05	71.38	58.83	2.45	0.46	0.81	54.91	63.76	118.66	0.169	No	No	0.19
413	27.10	75.90	55.96	2.41	0.45	0.82	58.51	63.82	122.33	0.177	No	No	0.20
414	27.17	81.93	51.02	2.35	0.44	0.82	63.32	63.22	126.53	0.188	No	No	0.21
415	27.24	87.56	46.42	2.29	0.44	0.82	67.78	62.21	129.99	0.198	No	No	0.22
416	27.30	91.18	44.02	2.26	0.43	0.82	70.64	61.59	132.23	0.205	No	No	0.23
417	27.37	94.80	42.14	2.24	0.43	0.82	73.51	61.14	134.65	0.213	No	No	0.24
418	27.46	98.02	41.52	2.23	0.43	0.82	76.06	61.35	137.42	0.224	No	No	0.25
419	27.51	100.23	40.66	2.22	0.42	0.82	77.82	61.18	139.00	0.230	No	No	0.26
420	27.57	103.15	39.41	2.21	0.42	0.82	80.14	60.82	140.96	0.239	No	No	0.27
421	27.64	106.37	38.10	2.19	0.42	0.82	82.68	60.37	143.05	0.249	No	No	0.28
422	27.70	108.08	37.49	2.18	0.41	0.82	84.01	60.18	144.18	0.255	No	No	0.29
423	27.76	108.68	37.57	2.18	0.41	0.82	84.44	60.34	144.78	0.258	No	No	0.29
424	27.82	109.58	37.76	2.18	0.41	0.82	85.12	60.66	145.79	0.263	No	No	0.30
425	27.91	109.68	38.73	2.20	0.41	0.82	85.15	61.47	146.62	0.268	No	No	0.30
426	27.96	110.39	38.94	2.20	0.41	0.82	85.69	61.77	147.46	0.273	No	No	0.31
427	28.03	111.19	39.15	2.20	0.41	0.82	86.29	62.08	148.37	0.278	No	No	0.31
428	28.09	110.99	39.55	2.21	0.41	0.82	86.05	62.34	148.38	0.279	No	No	0.31
429	28.16	110.19	40.21	2.22	0.41	0.82	85.32	62.67	147.99	0.276	No	No	0.31
430	28.23	107.27	41.69	2.23	0.41	0.82	82.82	63.13	145.95	0.264	No	No	0.30
431	28.29	103.95	43.27	2.25	0.41	0.81	80.03	63.49	143.52	0.251	No	No	0.28
432	28.36	98.32	46.01	2.29	0.42	0.81	75.35	63.93	139.28	0.231	No	No	0.26

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
433	28.45	94.10	47.48	2.31	0.43	0.81	71.78	63.79	135.57	0.217	No	No	0.24
434	28.48	91.08	48.80	2.32	0.43	0.80	69.29	63.80	133.09	0.208	No	No	0.23
435	28.55	88.97	48.75	2.32	0.44	0.80	67.47	63.30	130.77	0.200	No	No	0.22
436	28.61	87.26	48.50	2.32	0.44	0.80	65.99	62.79	128.77	0.194	No	No	0.21
437	28.68	86.66	48.35	2.32	0.44	0.80	65.42	62.57	127.99	0.192	No	No	0.21
438	28.74	86.16	48.09	2.31	0.44	0.80	64.93	62.32	127.25	0.190	No	No	0.21
439	28.81	82.45	50.10	2.34	0.45	0.79	61.89	62.44	124.33	0.182	No	No	0.20
440	28.87	65.47	62.62	2.50	0.47	0.78	48.46	63.02	111.48	0.155	No	No	0.17
441	28.94	67.97	60.64	2.47	0.47	0.78	50.36	63.02	113.38	0.158	No	No	0.17
442	29.03	53.59	73.12	2.63	0.49	0.77	39.14	0.00	39.14	4.000	No	Yes	2.00
443	29.08	44.74	82.66	2.75	0.51	0.77	32.38	0.00	32.38	4.000	No	Yes	2.00
444	29.16	34.39	95.93	2.91	0.53	0.76	24.59	0.00	24.59	4.000	No	Yes	2.00
445	29.22	29.76	100.00	2.99	0.54	0.75	21.13	0.00	21.13	4.000	No	Yes	2.00
446	29.27	26.44	100.00	3.06	0.55	0.75	18.68	0.00	18.68	4.000	No	Yes	2.00
447	29.35	22.82	100.00	3.13	0.56	0.74	16.01	0.00	16.01	4.000	No	Yes	2.00
448	29.43	21.82	100.00	3.13	0.56	0.74	15.27	0.00	15.27	4.000	No	Yes	2.00
449	29.47	20.81	100.00	3.15	0.57	0.74	14.53	0.00	14.53	4.000	No	Yes	2.00
450	29.53	19.91	100.00	3.17	0.57	0.74	13.87	0.00	13.87	4.000	No	Yes	2.00
451	29.60	19.61	100.00	3.16	0.57	0.74	13.64	0.00	13.64	4.000	No	Yes	2.00
452	29.67	19.71	100.00	3.14	0.57	0.73	13.69	0.00	13.69	4.000	No	Yes	2.00
453	29.73	19.81	100.00	3.13	0.57	0.73	13.75	0.00	13.75	4.000	No	Yes	2.00
454	29.80	19.30	100.00	3.14	0.57	0.73	13.36	0.00	13.36	4.000	No	Yes	2.00
455	29.87	18.40	100.00	3.17	0.57	0.73	12.71	0.00	12.71	4.000	No	Yes	2.00
456	29.93	17.90	100.00	3.19	0.57	0.73	12.34	0.00	12.34	4.000	No	Yes	2.00
457	30.00	17.80	100.00	3.20	0.57	0.73	12.25	0.00	12.25	4.000	No	Yes	2.00
458	30.07	17.70	100.00	3.20	0.57	0.73	12.17	0.00	12.17	4.000	No	Yes	2.00
459	30.12	17.70	100.00	3.21	0.57	0.73	12.15	0.00	12.15	4.000	No	Yes	2.00
460	30.20	18.20	100.00	3.20	0.57	0.73	12.49	0.00	12.49	4.000	No	Yes	2.00
461	30.27	18.80	100.00	3.20	0.57	0.73	12.89	0.00	12.89	4.000	No	Yes	2.00
462	30.32	19.20	100.00	3.19	0.57	0.73	13.16	0.00	13.16	4.000	No	Yes	2.00
463	30.40	20.01	100.00	3.19	0.57	0.73	13.72	0.00	13.72	4.000	No	Yes	2.00
464	30.46	20.21	100.00	3.20	0.57	0.72	13.84	0.00	13.84	4.000	No	Yes	2.00
465	30.52	19.81	100.00	3.22	0.57	0.72	13.55	0.00	13.55	4.000	No	Yes	2.00
466	30.59	19.71	100.00	3.23	0.57	0.72	13.46	0.00	13.46	4.000	No	Yes	2.00
467	30.65	18.80	100.00	3.26	0.57	0.72	12.80	0.00	12.80	4.000	No	Yes	2.00
468	30.71	18.50	100.00	3.27	0.57	0.72	12.58	0.00	12.58	4.000	No	Yes	2.00
469	30.79	18.00	100.00	3.29	0.57	0.72	12.21	0.00	12.21	4.000	No	Yes	2.00
470	30.85	17.90	100.00	3.29	0.57	0.72	12.13	0.00	12.13	4.000	No	Yes	2.00
471	30.96	17.80	100.00	3.23	0.57	0.72	12.04	0.00	12.04	4.000	No	Yes	2.00
472	31.00	18.20	100.00	3.24	0.57	0.72	12.30	0.00	12.30	4.000	No	Yes	2.00
473	31.04	18.40	100.00	3.25	0.57	0.71	12.43	0.00	12.43	4.000	No	Yes	2.00
474	31.11	18.70	100.00	3.25	0.57	0.71	12.63	0.00	12.63	4.000	No	Yes	2.00
475	31.18	18.60	100.00	3.25	0.57	0.71	12.54	0.00	12.54	4.000	No	Yes	2.00
476	31.25	18.41	100.00	3.26	0.57	0.71	12.39	0.00	12.39	4.000	No	Yes	2.00
477	31.30	18.71	100.00	3.25	0.57	0.71	12.58	0.00	12.58	4.000	No	Yes	2.00
478	31.38	19.62	100.00	3.22	0.57	0.71	13.20	0.00	13.20	4.000	No	Yes	2.00
479	31.44	19.67	100.00	3.21	0.57	0.71	13.21	0.00	13.21	4.000	No	Yes	2.00
480	31.50	19.92	100.00	3.20	0.57	0.71	13.37	0.00	13.37	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
481	31.57	19.72	100.00	3.21	0.57	0.71	13.22	0.00	13.22	4.000	No	Yes	2.00
482	31.63	20.92	100.00	3.19	0.57	0.71	14.03	0.00	14.03	4.000	No	Yes	2.00
483	31.70	21.63	100.00	3.18	0.57	0.71	14.51	0.00	14.51	4.000	No	Yes	2.00
484	31.79	21.93	100.00	3.18	0.56	0.71	14.69	0.00	14.69	4.000	No	Yes	2.00
485	31.83	22.48	100.00	3.17	0.56	0.71	15.06	0.00	15.06	4.000	No	Yes	2.00
486	31.90	23.34	100.00	3.15	0.56	0.71	15.64	0.00	15.64	4.000	No	Yes	2.00
487	31.97	23.14	100.00	3.15	0.56	0.71	15.48	0.00	15.48	4.000	No	Yes	2.00
488	32.03	22.03	100.00	3.18	0.56	0.71	14.70	0.00	14.70	4.000	No	Yes	2.00
489	32.10	21.63	100.00	3.18	0.57	0.70	14.40	0.00	14.40	4.000	No	Yes	2.00
490	32.16	21.53	100.00	3.18	0.57	0.70	14.32	0.00	14.32	4.000	No	Yes	2.00
491	32.23	21.63	100.00	3.17	0.57	0.70	14.37	0.00	14.37	4.000	No	Yes	2.00
492	32.30	21.73	100.00	3.17	0.57	0.70	14.42	0.00	14.42	4.000	No	Yes	2.00
493	32.36	21.63	100.00	3.18	0.57	0.70	14.34	0.00	14.34	4.000	No	Yes	2.00
494	32.46	20.92	100.00	3.20	0.57	0.70	13.83	0.00	13.83	4.000	No	Yes	2.00
495	32.51	20.92	100.00	3.20	0.57	0.70	13.82	0.00	13.82	4.000	No	Yes	2.00
496	32.56	21.43	100.00	3.19	0.57	0.70	14.15	0.00	14.15	4.000	No	Yes	2.00
497	32.65	21.93	100.00	3.18	0.57	0.70	14.47	0.00	14.47	4.000	No	Yes	2.00
498	32.68	24.84	100.00	3.10	0.56	0.70	16.46	0.00	16.46	4.000	No	Yes	2.00
499	32.76	27.16	100.00	3.06	0.55	0.70	18.04	0.00	18.04	4.000	No	Yes	2.00
500	32.84	30.78	100.00	3.00	0.54	0.71	20.53	0.00	20.53	4.000	No	Yes	2.00
501	32.89	31.38	100.00	2.99	0.54	0.71	20.93	0.00	20.93	4.000	No	Yes	2.00
502	32.95	31.68	100.00	3.00	0.54	0.71	21.12	0.00	21.12	4.000	No	Yes	2.00
503	33.01	30.68	100.00	3.02	0.54	0.70	20.40	0.00	20.40	4.000	No	Yes	2.00
504	33.10	27.66	100.00	3.08	0.55	0.70	18.27	0.00	18.27	4.000	No	Yes	2.00
505	33.15	26.05	100.00	3.11	0.56	0.70	17.15	0.00	17.15	4.000	No	Yes	2.00
506	33.24	24.54	100.00	3.14	0.56	0.69	16.10	0.00	16.10	4.000	No	Yes	2.00
507	33.29	22.93	100.00	3.18	0.56	0.69	14.99	0.00	14.99	4.000	No	Yes	2.00
508	33.35	20.72	100.00	3.22	0.57	0.69	13.48	0.00	13.48	4.000	No	Yes	2.00
509	33.40	19.52	100.00	3.25	0.57	0.69	12.66	0.00	12.66	4.000	No	Yes	2.00
510	33.47	18.81	100.00	3.27	0.57	0.69	12.17	0.00	12.17	4.000	No	Yes	2.00
511	33.55	17.51	100.00	3.30	0.58	0.68	11.29	0.00	11.29	4.000	No	Yes	2.00
512	33.65	16.40	100.00	3.33	0.58	0.68	10.54	0.00	10.54	4.000	No	Yes	2.00
513	33.66	16.20	100.00	3.34	0.58	0.68	10.40	0.00	10.40	4.000	No	Yes	2.00
514	33.74	16.10	100.00	3.33	0.58	0.68	10.32	0.00	10.32	4.000	No	Yes	2.00
515	33.84	15.70	100.00	3.34	0.58	0.68	10.04	0.00	10.04	4.000	No	Yes	2.00
516	33.88	15.70	100.00	3.33	0.58	0.68	10.04	0.00	10.04	4.000	No	Yes	2.00
517	33.93	15.70	100.00	3.33	0.58	0.68	10.03	0.00	10.03	4.000	No	Yes	2.00
518	33.99	15.70	100.00	3.32	0.58	0.68	10.02	0.00	10.02	4.000	No	Yes	2.00
519	34.07	15.49	100.00	3.33	0.58	0.67	9.87	0.00	9.87	4.000	No	Yes	2.00
520	34.12	15.49	100.00	3.33	0.58	0.67	9.86	0.00	9.86	4.000	No	Yes	2.00
521	34.19	15.49	100.00	3.33	0.58	0.67	9.85	0.00	9.85	4.000	No	Yes	2.00
522	34.28	15.80	100.00	3.32	0.58	0.67	10.03	0.00	10.03	4.000	No	Yes	2.00
523	34.32	15.90	100.00	3.32	0.58	0.67	10.09	0.00	10.09	4.000	No	Yes	2.00
524	34.40	16.30	100.00	3.32	0.58	0.67	10.34	0.00	10.34	4.000	No	Yes	2.00
525	34.48	16.60	100.00	3.30	0.58	0.67	10.52	0.00	10.52	4.000	No	Yes	2.00
526	34.52	16.80	100.00	3.29	0.58	0.67	10.65	0.00	10.65	4.000	No	Yes	2.00
527	34.58	17.71	100.00	3.26	0.58	0.67	11.23	0.00	11.23	4.000	No	Yes	2.00
528	34.68	22.83	100.00	3.09	0.56	0.68	14.58	0.00	14.58	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
529	34.72	26.65	100.00	3.01	0.56	0.68	17.12	0.00	17.12	4.000	No	Yes	2.00
530	34.81	30.98	99.52	2.96	0.55	0.68	20.01	0.00	20.01	4.000	No	Yes	2.00
531	34.85	26.05	100.00	3.09	0.56	0.68	16.68	0.00	16.68	4.000	No	Yes	2.00
532	34.92	29.26	100.00	3.04	0.55	0.68	18.82	0.00	18.82	4.000	No	Yes	2.00
533	34.98	26.04	100.00	3.13	0.56	0.68	16.65	0.00	16.65	4.000	No	Yes	2.00
534	35.05	25.04	100.00	3.15	0.56	0.67	15.96	0.00	15.96	4.000	No	Yes	2.00
535	35.12	24.43	100.00	3.17	0.56	0.67	15.54	0.00	15.54	4.000	No	Yes	2.00
536	35.18	25.54	100.00	3.14	0.56	0.67	16.26	0.00	16.26	4.000	No	Yes	2.00
537	35.26	26.64	100.00	3.13	0.56	0.67	16.97	0.00	16.97	4.000	No	Yes	2.00
538	35.31	27.86	100.00	3.11	0.55	0.67	17.76	0.00	17.76	4.000	No	Yes	2.00
539	35.41	32.49	100.00	3.03	0.54	0.68	20.84	0.00	20.84	4.000	No	Yes	2.00
540	35.47	36.81	100.00	2.96	0.53	0.68	23.76	0.00	23.76	4.000	No	Yes	2.00
541	35.51	43.55	92.03	2.86	0.52	0.69	28.35	0.00	28.35	4.000	No	Yes	2.00
542	35.58	56.92	78.96	2.70	0.50	0.70	37.65	0.00	37.65	4.000	No	Yes	2.00
543	35.63	68.38	69.43	2.58	0.48	0.71	45.82	63.85	109.66	0.152	No	No	0.16
544	35.71	78.94	61.98	2.49	0.46	0.72	53.46	64.26	117.72	0.167	No	No	0.18
545	35.78	83.97	59.51	2.46	0.45	0.72	57.13	64.58	121.71	0.175	No	No	0.19
546	35.84	82.46	61.23	2.48	0.46	0.72	55.98	64.77	120.75	0.173	No	No	0.18
547	35.90	76.73	65.68	2.53	0.46	0.71	51.73	64.72	116.45	0.164	No	No	0.17
548	35.98	67.37	73.46	2.63	0.48	0.71	44.91	0.00	44.91	4.000	No	Yes	2.00
549	36.05	60.53	79.26	2.70	0.49	0.70	39.95	0.00	39.95	4.000	No	Yes	2.00
550	36.10	53.19	85.85	2.79	0.50	0.69	34.78	0.00	34.78	4.000	No	Yes	2.00
551	36.20	40.92	98.00	2.94	0.53	0.68	26.27	0.00	26.27	4.000	No	Yes	2.00
552	36.25	37.01	100.00	2.99	0.53	0.67	23.59	0.00	23.59	4.000	No	Yes	2.00
553	36.30	31.77	100.00	3.07	0.55	0.67	20.06	0.00	20.06	4.000	No	Yes	2.00
554	36.35	29.76	100.00	3.09	0.55	0.67	18.72	0.00	18.72	4.000	No	Yes	2.00
555	36.45	27.65	100.00	3.10	0.56	0.66	17.30	0.00	17.30	4.000	No	Yes	2.00
556	36.48	27.35	100.00	3.10	0.56	0.66	17.10	0.00	17.10	4.000	No	Yes	2.00
557	36.55	27.25	100.00	3.09	0.56	0.66	17.01	0.00	17.01	4.000	No	Yes	2.00
558	36.63	27.40	100.00	3.09	0.56	0.66	17.09	0.00	17.09	4.000	No	Yes	2.00
559	36.69	26.86	100.00	3.12	0.56	0.66	16.71	0.00	16.71	4.000	No	Yes	2.00
560	36.75	27.46	100.00	3.12	0.56	0.66	17.09	0.00	17.09	4.000	No	Yes	2.00
561	36.84	28.46	100.00	3.11	0.55	0.66	17.72	0.00	17.72	4.000	No	Yes	2.00
562	36.89	29.37	100.00	3.10	0.55	0.66	18.30	0.00	18.30	4.000	No	Yes	2.00
563	36.95	30.07	100.00	3.11	0.55	0.66	18.74	0.00	18.74	4.000	No	Yes	2.00
564	37.05	32.08	100.00	3.10	0.55	0.66	20.03	0.00	20.03	4.000	No	Yes	2.00
565	37.08	33.99	100.00	3.07	0.54	0.66	21.28	0.00	21.28	4.000	No	Yes	2.00
566	37.14	36.01	100.00	3.04	0.54	0.66	22.60	0.00	22.60	4.000	No	Yes	2.00
567	37.23	38.22	100.00	3.02	0.53	0.67	24.04	0.00	24.04	4.000	No	Yes	2.00
568	37.28	39.32	100.00	3.02	0.53	0.67	24.76	0.00	24.76	4.000	No	Yes	2.00
569	37.34	40.13	100.00	3.01	0.53	0.67	25.29	0.00	25.29	4.000	No	Yes	2.00
570	37.43	42.24	100.00	2.99	0.52	0.67	26.67	0.00	26.67	4.000	No	Yes	2.00
571	37.48	43.45	100.00	2.98	0.52	0.67	27.47	0.00	27.47	4.000	No	Yes	2.00
572	37.53	44.75	99.89	2.96	0.52	0.67	28.33	0.00	28.33	4.000	No	Yes	2.00
573	37.61	47.67	93.40	2.88	0.51	0.67	30.25	0.00	30.25	4.000	No	Yes	2.00
574	37.67	48.88	93.36	2.88	0.51	0.67	31.05	0.00	31.05	4.000	No	Yes	2.00
575	37.73	53.30	89.14	2.83	0.50	0.68	34.04	0.00	34.04	4.000	No	Yes	2.00
576	37.82	61.34	82.19	2.74	0.49	0.68	39.52	0.00	39.52	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
577	37.88	69.49	75.26	2.65	0.48	0.69	45.22	0.00	45.22	4.000	No	Yes	2.00
578	37.93	70.59	74.41	2.64	0.48	0.69	45.97	0.00	45.97	4.000	No	Yes	2.00
579	38.00	87.79	62.38	2.49	0.45	0.70	58.28	65.74	124.02	0.181	No	No	0.19
580	38.08	93.01	59.44	2.46	0.44	0.71	62.04	65.94	127.98	0.192	No	No	0.20
581	38.12	98.64	56.27	2.42	0.43	0.71	66.16	66.03	132.19	0.205	No	No	0.22
582	38.20	106.79	52.15	2.36	0.42	0.71	72.15	66.07	138.22	0.227	No	No	0.24
583	38.29	115.74	48.31	2.32	0.41	0.72	78.90	66.07	144.97	0.259	No	No	0.28
584	38.33	120.56	46.54	2.29	0.41	0.72	82.54	66.08	148.62	0.280	No	No	0.30
585	38.43	130.02	45.26	2.28	0.39	0.73	89.89	67.22	157.11	0.344	No	No	0.37
586	38.48	132.73	44.99	2.27	0.39	0.73	92.01	67.59	159.61	0.368	No	No	0.39
587	38.52	134.94	44.88	2.27	0.38	0.74	93.75	67.96	161.71	0.390	No	No	0.42
588	38.59	136.65	45.75	2.28	0.38	0.74	95.13	68.85	163.98	0.417	No	No	0.45
589	38.68	137.25	47.13	2.30	0.38	0.74	95.63	69.79	165.42	0.435	No	No	0.47
590	38.72	138.26	47.41	2.31	0.38	0.74	96.43	70.16	166.59	0.451	No	No	0.49
591	38.79	141.28	47.43	2.31	0.37	0.74	98.82	70.79	169.61	0.498	No	No	0.54
592	38.87	145.40	47.11	2.30	0.37	0.74	102.11	71.46	173.57	0.570	No	No	0.61
593	38.92	150.43	46.29	2.29	0.36	0.75	106.15	72.01	178.16	0.676	No	No	0.73
594	38.98	155.85	45.32	2.28	0.35	0.75	110.54	72.52	183.07	0.825	No	No	0.89
595	39.05	162.89	44.43	2.27	0.34	0.76	116.33	73.39	189.72	1.111	No	No	1.20
596	39.12	167.92	43.86	2.26	0.34	0.76	120.48	74.04	194.52	1.408	No	No	1.51
597	39.17	171.44	43.75	2.26	0.33	0.76	123.43	74.70	198.13	1.705	No	No	1.83
598	39.26	174.46	43.89	2.26	0.33	0.76	125.95	75.44	201.38	2.047	No	No	2.00
599	39.32	175.36	44.06	2.26	0.33	0.76	126.67	75.74	202.41	2.173	No	No	2.00
600	39.37	175.76	44.25	2.27	0.33	0.76	126.97	75.95	202.92	2.239	No	No	2.00
601	39.46	175.76	44.57	2.27	0.33	0.76	126.88	76.16	203.04	2.255	No	No	2.00
602	39.52	175.76	44.65	2.27	0.33	0.76	126.81	76.21	203.02	2.252	No	No	2.00
603	39.57	174.66	45.00	2.27	0.33	0.76	125.82	76.20	202.02	2.124	No	No	2.00
604	39.63	173.45	45.38	2.28	0.33	0.76	124.73	76.18	200.91	1.992	No	No	2.00
605	39.72	172.55	45.62	2.28	0.33	0.76	123.86	76.12	199.98	1.890	No	No	2.00
606	39.77	172.04	45.70	2.28	0.33	0.76	123.36	76.05	199.41	1.830	No	No	1.95
607	39.85	169.23	46.45	2.29	0.33	0.76	120.90	75.91	196.81	1.588	No	No	1.70
608	39.91	167.82	46.75	2.30	0.34	0.75	119.65	75.78	195.42	1.476	No	No	1.58
609	39.96	165.81	47.14	2.30	0.34	0.75	117.89	75.56	193.45	1.333	No	No	1.43
610	40.06	163.80	47.12	2.30	0.34	0.75	116.05	75.07	191.12	1.188	No	No	1.28
611	40.11	160.88	47.79	2.31	0.35	0.75	113.57	74.84	188.40	1.044	No	No	1.12
612	40.16	157.16	48.70	2.32	0.35	0.74	110.44	74.54	184.98	0.895	No	No	0.97
613	40.26	148.52	50.54	2.34	0.36	0.74	103.26	73.63	176.89	0.644	No	No	0.69
614	40.30	144.19	51.73	2.36	0.37	0.73	99.73	73.28	173.00	0.559	No	No	0.60
615	40.36	138.16	53.37	2.38	0.38	0.73	94.85	72.71	167.56	0.465	No	No	0.50
616	40.44	130.13	55.47	2.41	0.39	0.72	88.40	71.84	160.24	0.374	No	No	0.40
617	40.50	126.91	55.33	2.40	0.39	0.72	85.77	71.07	156.83	0.341	No	No	0.36
618	40.55	122.28	54.24	2.39	0.40	0.71	82.00	69.60	151.60	0.300	No	No	0.32
619	40.62	117.05	56.99	2.42	0.41	0.71	78.00	69.55	147.55	0.273	No	No	0.29
620	40.68	113.13	57.80	2.43	0.41	0.70	74.94	68.99	143.94	0.253	No	No	0.27
621	40.75	109.21	58.59	2.44	0.42	0.70	71.83	68.40	140.23	0.236	No	No	0.25
622	40.84	106.70	59.22	2.45	0.42	0.69	69.87	68.06	137.93	0.226	No	No	0.24
623	40.90	105.54	59.69	2.46	0.43	0.69	68.97	67.95	136.92	0.222	No	No	0.24
624	40.96	103.88	60.57	2.47	0.43	0.69	67.70	67.87	135.57	0.217	No	No	0.23

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
625	41.04	104.39	60.41	2.47	0.43	0.69	68.01	67.91	135.92	0.218	No	No	0.23
626	41.09	104.18	60.75	2.47	0.43	0.69	67.82	67.96	135.78	0.217	No	No	0.23
627	41.15	104.29	60.94	2.47	0.43	0.69	67.86	68.03	135.89	0.218	No	No	0.23
628	41.22	105.79	60.24	2.47	0.43	0.69	68.90	68.11	137.00	0.222	No	No	0.24
629	41.30	107.60	59.14	2.45	0.42	0.69	70.15	68.11	138.26	0.227	No	No	0.24
630	41.35	109.11	58.17	2.44	0.42	0.69	71.21	68.08	139.29	0.232	No	No	0.25
631	41.41	110.32	57.33	2.43	0.42	0.69	72.03	68.03	140.06	0.235	No	No	0.25
632	41.48	111.93	56.41	2.42	0.42	0.69	73.14	68.00	141.15	0.240	No	No	0.25
633	41.55	112.93	55.96	2.41	0.42	0.69	73.82	68.03	141.84	0.243	No	No	0.26
634	41.62	113.44	55.74	2.41	0.42	0.69	74.22	68.06	142.27	0.245	No	No	0.26
635	41.68	113.13	55.85	2.41	0.42	0.69	73.93	68.02	141.95	0.244	No	No	0.26
636	41.74	112.63	56.09	2.41	0.42	0.69	73.42	67.96	141.39	0.241	No	No	0.26
637	41.80	112.23	56.43	2.42	0.42	0.69	73.08	67.99	141.07	0.239	No	No	0.25
638	41.88	112.23	56.46	2.42	0.42	0.69	73.01	67.99	141.00	0.239	No	No	0.25
639	41.95	112.73	56.24	2.42	0.42	0.69	73.32	67.99	141.31	0.241	No	No	0.26
640	42.00	113.03	56.10	2.41	0.42	0.69	73.49	67.99	141.48	0.241	No	No	0.26
641	42.08	112.13	56.71	2.42	0.42	0.69	72.77	68.01	140.78	0.238	No	No	0.25
642	42.15	110.72	57.57	2.43	0.42	0.69	71.68	68.01	139.70	0.233	No	No	0.25
643	42.22	107.30	59.42	2.46	0.43	0.68	69.14	67.92	137.06	0.222	No	No	0.24
644	42.28	103.48	61.58	2.48	0.43	0.68	66.33	67.79	134.12	0.211	No	No	0.22
645	42.34	98.45	64.51	2.52	0.44	0.67	62.67	67.56	130.23	0.198	No	No	0.21
646	42.39	95.44	66.41	2.54	0.44	0.67	60.50	67.41	127.91	0.191	No	No	0.20
647	42.48	94.23	67.32	2.55	0.44	0.67	59.58	67.37	126.95	0.189	No	No	0.20
648	42.53	94.63	67.08	2.55	0.44	0.67	59.82	67.38	127.21	0.189	No	No	0.20
649	42.59	96.44	66.16	2.54	0.44	0.67	61.07	67.52	128.58	0.193	No	No	0.21
650	42.68	98.76	65.39	2.53	0.44	0.67	62.67	67.78	130.45	0.199	No	No	0.21
651	42.72	100.46	64.47	2.52	0.44	0.67	63.85	67.88	131.73	0.203	No	No	0.22
652	42.79	106.20	61.23	2.48	0.43	0.68	67.91	68.13	136.04	0.218	No	No	0.23
653	42.87	113.64	56.79	2.42	0.42	0.68	73.31	68.18	141.49	0.241	No	No	0.26
654	42.92	116.35	54.76	2.40	0.41	0.68	75.21	67.95	143.17	0.250	No	No	0.27
655	43.00	117.66	52.96	2.37	0.41	0.68	76.04	67.45	143.49	0.251	No	No	0.27
656	43.05	118.16	52.70	2.37	0.41	0.68	76.36	67.43	143.79	0.253	No	No	0.27
657	43.13	121.38	51.07	2.35	0.41	0.69	78.64	67.33	145.97	0.264	No	No	0.28
658	43.22	123.89	47.60	2.31	0.41	0.69	80.23	66.05	146.29	0.266	No	No	0.28
659	43.27	122.18	47.02	2.30	0.41	0.68	78.83	65.38	144.21	0.255	No	No	0.27
660	43.33	116.34	48.62	2.32	0.42	0.68	74.38	65.04	139.42	0.232	No	No	0.25
661	43.37	110.71	51.05	2.35	0.43	0.67	70.29	65.09	135.39	0.216	No	No	0.23
662	43.47	94.71	58.72	2.45	0.45	0.66	58.93	64.85	123.78	0.180	No	No	0.19
663	43.52	86.26	64.07	2.51	0.46	0.65	53.09	64.71	117.80	0.167	No	No	0.18
664	43.57	73.38	74.99	2.65	0.48	0.64	44.41	0.00	44.41	4.000	No	Yes	2.00
665	43.66	55.18	93.05	2.88	0.51	0.62	32.52	0.00	32.52	4.000	No	Yes	2.00
666	43.72	49.35	99.04	2.95	0.52	0.62	28.78	0.00	28.78	4.000	No	Yes	2.00
667	43.77	43.01	100.00	3.04	0.53	0.61	24.78	0.00	24.78	4.000	No	Yes	2.00
668	43.83	38.59	100.00	3.10	0.54	0.60	22.03	0.00	22.03	4.000	No	Yes	2.00
669	43.90	33.96	100.00	3.17	0.55	0.60	19.20	0.00	19.20	4.000	No	Yes	2.00
670	43.97	40.30	100.00	3.02	0.54	0.60	23.04	0.00	23.04	4.000	No	Yes	2.00
671	44.03	40.00	100.00	3.01	0.54	0.60	22.84	0.00	22.84	4.000	No	Yes	2.00
672	44.13	36.98	100.00	3.02	0.54	0.60	20.96	0.00	20.96	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
673	44.17	34.67	100.00	3.04	0.55	0.60	19.56	0.00	19.56	4.000	No	Yes	2.00
674	44.23	31.55	100.00	3.07	0.55	0.59	17.68	0.00	17.68	4.000	No	Yes	2.00
675	44.33	27.83	100.00	3.12	0.56	0.59	15.46	0.00	15.46	4.000	No	Yes	2.00
676	44.37	26.12	100.00	3.16	0.57	0.58	14.45	0.00	14.45	4.000	No	Yes	2.00
677	44.43	23.31	100.00	3.24	0.57	0.58	12.81	0.00	12.81	4.000	No	Yes	2.00
678	44.52	20.59	100.00	3.36	0.58	0.58	11.24	0.00	11.24	4.000	No	Yes	2.00
679	44.57	19.39	100.00	3.42	0.58	0.58	10.55	0.00	10.55	4.000	No	Yes	2.00
680	44.62	19.59	100.00	3.44	0.58	0.58	10.66	0.00	10.66	4.000	No	Yes	2.00
681	44.72	29.64	100.00	3.20	0.56	0.59	16.44	0.00	16.44	4.000	No	Yes	2.00
682	44.76	47.94	95.71	2.91	0.52	0.61	27.50	0.00	27.50	4.000	No	Yes	2.00
683	44.83	80.92	70.90	2.60	0.47	0.64	48.77	65.01	113.78	0.159	No	No	0.17
684	44.92	103.64	60.88	2.47	0.44	0.66	64.41	67.04	131.45	0.202	No	No	0.21
685	44.97	115.31	56.66	2.42	0.42	0.67	72.84	68.01	140.85	0.238	No	No	0.25
686	45.02	116.81	57.44	2.43	0.42	0.67	73.96	68.59	142.55	0.246	No	No	0.26
687	45.09	117.31	58.69	2.45	0.41	0.67	74.34	69.13	143.47	0.251	No	No	0.27
688	45.16	119.30	57.93	2.44	0.41	0.67	75.75	69.26	145.02	0.259	No	No	0.28
689	45.22	121.80	56.61	2.42	0.41	0.67	77.53	69.29	146.81	0.269	No	No	0.29
690	45.29	126.81	53.94	2.39	0.40	0.68	81.13	69.24	150.37	0.291	No	No	0.31
691	45.37	127.39	53.72	2.38	0.40	0.68	81.51	69.25	150.76	0.294	No	No	0.31
692	45.41	121.05	57.17	2.43	0.41	0.67	76.86	69.31	146.17	0.265	No	No	0.28
693	45.47	104.45	67.75	2.56	0.43	0.66	64.88	69.00	133.88	0.210	No	No	0.22
694	45.56	77.30	82.53	2.74	0.47	0.63	46.15	0.00	46.15	4.000	No	Yes	2.00
695	45.62	62.02	92.19	2.86	0.50	0.62	36.12	0.00	36.12	4.000	No	Yes	2.00
696	45.70	49.06	100.00	2.99	0.52	0.60	27.94	0.00	27.94	4.000	No	Yes	2.00
697	45.75	44.53	100.00	3.04	0.53	0.60	25.13	0.00	25.13	4.000	No	Yes	2.00
698	45.81	35.29	100.00	3.19	0.55	0.58	19.55	0.00	19.55	4.000	No	Yes	2.00
699	45.90	36.39	100.00	3.16	0.55	0.59	20.18	0.00	20.18	4.000	No	Yes	2.00
700	45.95	41.62	100.00	3.07	0.53	0.59	23.30	0.00	23.30	4.000	No	Yes	2.00
701	46.01	51.57	96.50	2.92	0.52	0.60	29.36	0.00	29.36	4.000	No	Yes	2.00
702	46.10	61.73	86.39	2.79	0.50	0.61	35.67	0.00	35.67	4.000	No	Yes	2.00
703	46.15	63.94	84.55	2.77	0.50	0.61	37.03	0.00	37.03	4.000	No	Yes	2.00
704	46.21	66.55	82.52	2.74	0.49	0.61	38.66	0.00	38.66	4.000	No	Yes	2.00
705	46.29	70.98	80.09	2.71	0.49	0.62	41.51	0.00	41.51	4.000	No	Yes	2.00
706	46.33	73.09	79.17	2.70	0.48	0.62	42.87	0.00	42.87	4.000	No	Yes	2.00
707	46.41	79.42	75.71	2.66	0.47	0.63	46.99	0.00	46.99	4.000	No	Yes	2.00
708	46.47	83.85	73.50	2.63	0.47	0.63	49.90	0.00	49.90	4.000	No	Yes	2.00
709	46.53	85.04	69.49	2.58	0.47	0.63	50.59	65.25	115.84	0.163	No	No	0.17
710	46.59	86.46	65.80	2.53	0.46	0.63	51.42	64.66	116.08	0.163	No	No	0.17
711	46.66	89.17	65.20	2.53	0.46	0.63	53.22	65.03	118.25	0.168	No	No	0.18
712	46.75	93.69	63.84	2.51	0.45	0.63	56.25	65.55	121.80	0.176	No	No	0.19
713	46.79	95.10	63.61	2.51	0.45	0.64	57.19	65.76	122.95	0.178	No	No	0.19
714	46.85	93.89	65.34	2.53	0.45	0.63	56.36	65.96	122.33	0.177	No	No	0.19
715	46.92	94.09	65.63	2.53	0.45	0.63	56.47	66.06	122.53	0.177	No	No	0.19
716	47.00	99.52	62.60	2.49	0.45	0.64	60.10	66.31	126.42	0.187	No	No	0.20
717	47.05	99.32	62.79	2.50	0.45	0.64	59.94	66.32	126.25	0.187	No	No	0.20
718	47.12	97.51	63.81	2.51	0.45	0.64	58.66	66.23	124.89	0.183	No	No	0.19
719	47.20	94.19	65.69	2.53	0.45	0.63	56.36	66.05	122.41	0.177	No	No	0.19
720	47.26	90.87	67.38	2.55	0.46	0.63	54.08	65.79	119.87	0.171	No	No	0.18

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)													
Point ID	Depth (ft)	q _t (tsf)	FC (%)	I _c	m	C _N	q _{c1N}	Δq _{c1N}	q _{c1N,cs}	CRR _{7.5}	Belongs to trans. layer	Clay-like behaviour	FS
721	47.32	87.66	69.02	2.58	0.46	0.63	51.89	65.53	117.42	0.166	No	No	0.18
722	47.39	83.03	71.26	2.60	0.47	0.62	48.77	0.00	48.77	4.000	No	Yes	2.00
723	47.47	78.10	73.84	2.64	0.48	0.62	45.50	0.00	45.50	4.000	No	Yes	2.00
724	47.51	72.27	77.96	2.69	0.49	0.61	41.72	0.00	41.72	4.000	No	Yes	2.00
725	47.59	63.53	84.81	2.77	0.50	0.60	36.15	0.00	36.15	4.000	No	Yes	2.00
726	47.65	57.08	90.53	2.84	0.51	0.59	32.16	0.00	32.16	4.000	No	Yes	2.00
727	47.71	53.37	95.00	2.90	0.51	0.59	29.85	0.00	29.85	4.000	No	Yes	2.00
728	47.79	44.52	100.00	3.02	0.53	0.58	24.49	0.00	24.49	4.000	No	Yes	2.00
729	47.85	41.71	100.00	3.06	0.54	0.58	22.80	0.00	22.80	4.000	No	Yes	2.00
730	47.91	38.79	100.00	3.11	0.54	0.57	21.07	0.00	21.07	4.000	No	Yes	2.00
731	48.00	50.76	97.49	2.93	0.52	0.59	28.17	0.00	28.17	4.000	No	Yes	2.00
732	48.05	68.35	82.19	2.74	0.49	0.60	38.96	0.00	38.96	4.000	No	Yes	2.00
733	48.10	100.33	61.56	2.48	0.45	0.63	59.88	65.96	125.84	0.186	No	No	0.20
734	48.19	147.58	39.77	2.21	0.39	0.67	93.09	64.20	157.30	0.346	No	No	0.37
735	48.25	163.07	34.13	2.14	0.38	0.68	104.17	61.50	165.67	0.439	No	No	0.47
736	48.30	170.10	31.85	2.11	0.37	0.68	109.20	59.89	169.08	0.489	No	No	0.52
737	48.39	182.88	27.26	2.05	0.37	0.68	117.98	54.89	172.86	0.556	No	No	0.59
738	48.43	186.40	26.10	2.04	0.37	0.68	120.34	53.27	173.61	0.571	No	No	0.61
739	48.50	192.03	25.01	2.03	0.36	0.69	124.40	51.91	176.32	0.630	No	No	0.67
740	48.59	195.35	25.06	2.03	0.36	0.69	127.08	52.48	179.56	0.714	No	No	0.76
741	48.64	196.46	25.08	2.03	0.36	0.69	127.95	52.67	180.62	0.745	No	No	0.79
742	48.70	197.36	24.95	2.02	0.36	0.69	128.56	52.51	181.08	0.759	No	No	0.81
743	48.79	196.06	25.34	2.03	0.36	0.69	127.54	53.11	180.64	0.746	No	No	0.79
744	48.83	194.76	25.69	2.03	0.36	0.69	126.58	53.62	180.20	0.733	No	No	0.78
745	48.89	192.95	25.95	2.04	0.36	0.69	125.11	53.86	178.98	0.698	No	No	0.74
746	48.95	189.23	26.85	2.05	0.36	0.68	122.34	54.99	177.34	0.655	No	No	0.70
747	49.02	185.51	27.79	2.06	0.36	0.68	119.57	56.08	175.66	0.615	No	No	0.65
748	49.11	177.66	30.02	2.09	0.37	0.68	113.84	58.39	172.23	0.544	No	No	0.58
749	49.19	172.34	31.86	2.11	0.37	0.67	109.99	60.07	170.07	0.505	No	No	0.54
750	49.22	168.52	33.21	2.13	0.38	0.67	107.24	61.13	168.37	0.478	No	No	0.51
751	49.28	162.69	35.30	2.15	0.38	0.67	103.02	62.48	165.50	0.436	No	No	0.46
752	49.35	155.65	37.54	2.18	0.39	0.66	97.84	63.45	161.28	0.385	No	No	0.41
753	49.42	149.42	39.65	2.21	0.39	0.66	93.29	64.16	157.44	0.347	No	No	0.37
754	49.48	143.29	41.91	2.24	0.40	0.66	88.84	64.76	153.60	0.315	No	No	0.33
755	49.56	135.75	45.46	2.28	0.41	0.65	83.48	65.70	149.18	0.284	No	No	0.30
756	49.63	132.33	46.76	2.30	0.41	0.65	80.98	65.80	146.78	0.269	No	No	0.29
757	49.68	129.31	46.21	2.29	0.41	0.64	78.65	64.89	143.54	0.251	No	No	0.27
758	49.74	127.40	47.91	2.31	0.42	0.64	77.35	65.46	142.81	0.248	No	No	0.26
759	49.83	125.20	49.80	2.33	0.42	0.64	75.81	65.99	141.80	0.243	No	No	0.26
760	49.87	122.79	51.19	2.35	0.42	0.64	74.12	66.18	140.30	0.236	No	No	0.25
761	49.97	118.97	53.85	2.39	0.42	0.64	71.45	66.57	138.02	0.226	No	No	0.24
762	50.03	119.07	54.17	2.39	0.42	0.63	71.50	66.71	138.22	4.000	No	No	2.00
763	50.08	118.56	100.00	4.06	0.41	0.65	72.59	0.00	72.59	4.000	No	Yes	2.00
764	50.14	119.17	100.00	4.06	0.40	0.65	73.01	0.00	73.01	4.000	No	Yes	2.00
765	50.23	120.17	100.00	4.06	0.40	0.65	73.70	0.00	73.70	4.000	No	Yes	2.00
766	50.27	120.98	100.00	4.06	0.40	0.65	74.28	0.00	74.28	4.000	No	Yes	2.00
767	50.33	122.18	100.00	4.06	0.40	0.65	75.14	0.00	75.14	4.000	No	Yes	2.00
768	50.41	124.40	100.00	4.06	0.40	0.65	76.75	0.00	76.75	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	FC (%)	I_c	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
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Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_t :	Total cone resistance
FC:	Fines content (%)
I_c :	Soil behavior type index
m:	Stress exponent
C_N :	Overburden correction factor
q_{c1N} :	Normalized and adjusted cone resistance
Δq_{c1N} :	Cone resistance correction factor due to fines
$q_{c1N,cs}$:	Normalized and adjusted cone resistance
$CRR_{7.5}$:	Cyclic resistance ratio for $M_w=7.5$
FS:	Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
0.10	2.00	0.00	0.00	0.05	0.00	0.14	2.00	0.00	0.00	0.05	0.00
0.21	2.00	0.00	0.00	0.07	0.00	0.26	2.00	0.00	0.00	0.06	0.00
0.34	2.00	0.00	0.00	0.07	0.00	0.40	2.00	0.00	0.00	0.06	0.00
0.49	2.00	0.00	0.00	0.09	0.00	0.53	2.00	0.00	0.00	0.04	0.00
0.59	2.00	0.00	0.00	0.07	0.00	0.66	2.00	0.00	0.00	0.07	0.00
0.73	2.00	0.00	0.00	0.07	0.00	0.81	2.00	0.00	0.00	0.08	0.00
0.87	2.00	0.00	0.00	0.07	0.00	0.92	2.00	0.00	0.00	0.05	0.00
0.99	2.00	0.00	0.00	0.06	0.00	1.05	2.00	0.00	0.00	0.07	0.00
1.15	2.00	0.00	0.00	0.09	0.00	1.20	2.00	0.00	0.00	0.05	0.00
1.26	2.00	0.00	0.00	0.06	0.00	1.32	2.00	0.00	0.00	0.06	0.00
1.39	2.00	0.00	0.00	0.07	0.00	1.46	2.00	0.00	0.00	0.07	0.00
1.51	2.00	0.00	0.00	0.05	0.00	1.58	2.00	0.00	0.00	0.07	0.00
1.66	2.00	0.00	0.00	0.07	0.00	1.71	2.00	0.00	0.00	0.05	0.00
1.79	2.00	0.00	0.00	0.08	0.00	1.84	2.00	0.00	0.00	0.05	0.00
1.93	2.00	0.00	0.00	0.09	0.00	1.98	2.00	0.00	0.00	0.05	0.00
2.04	2.00	0.00	0.00	0.05	0.00	2.11	2.00	0.00	0.00	0.07	0.00
2.17	2.00	0.00	0.00	0.07	0.00	2.24	2.00	0.00	0.00	0.06	0.00
2.32	2.00	0.00	0.00	0.08	0.00	2.38	2.00	0.00	0.00	0.06	0.00
2.43	2.00	0.00	0.00	0.05	0.00	2.52	2.00	0.00	0.00	0.09	0.00
2.56	2.00	0.00	0.00	0.04	0.00	2.64	2.00	0.00	0.00	0.07	0.00
2.69	2.00	0.00	0.00	0.05	0.00	2.78	2.00	0.00	0.00	0.09	0.00
2.83	2.00	0.00	0.00	0.05	0.00	2.89	2.00	0.00	0.00	0.07	0.00
2.95	2.00	0.00	0.00	0.06	0.00	3.02	2.00	0.00	0.00	0.07	0.00
3.09	2.00	0.00	0.00	0.06	0.00	3.15	2.00	0.00	0.00	0.06	0.00
3.22	2.00	0.00	0.00	0.07	0.00	3.29	2.00	0.00	0.00	0.07	0.00
3.35	2.00	0.00	0.00	0.07	0.00	3.41	2.00	0.00	0.00	0.06	0.00
3.52	2.00	0.00	0.00	0.10	0.00	3.55	2.00	0.00	0.00	0.03	0.00
3.61	2.00	0.00	0.00	0.06	0.00	3.71	2.00	0.00	0.00	0.10	0.00
3.75	2.00	0.00	0.00	0.04	0.00	3.81	2.00	0.00	0.00	0.06	0.00
3.90	2.00	0.00	0.00	0.09	0.00	3.95	2.00	0.00	0.00	0.05	0.00
4.01	2.00	0.00	0.00	0.06	0.00	4.09	2.00	0.00	0.00	0.08	0.00
4.15	2.00	0.00	0.00	0.05	0.00	4.21	2.00	0.00	0.00	0.06	0.00
4.29	2.00	0.00	0.00	0.08	0.00	4.34	2.00	0.00	0.00	0.05	0.00
4.41	2.00	0.00	0.00	0.07	0.00	4.46	2.00	0.00	0.00	0.05	0.00
4.55	2.00	0.00	0.00	0.09	0.00	4.61	2.00	0.00	0.00	0.06	0.00
4.67	2.00	0.00	0.00	0.06	0.00	4.75	2.00	0.00	0.00	0.09	0.00
4.79	2.00	0.00	0.00	0.04	0.00	4.87	2.00	0.00	0.00	0.08	0.00
4.93	2.00	0.00	0.00	0.06	0.00	4.99	2.00	0.00	0.00	0.06	0.00
5.06	2.00	0.00	0.00	0.07	0.00	5.14	2.00	0.00	0.00	0.07	0.00
5.19	2.00	0.00	0.00	0.05	0.00	5.25	2.00	0.00	0.00	0.06	0.00
5.33	2.00	0.00	0.00	0.08	0.00	5.38	2.00	0.00	0.00	0.05	0.00
5.45	2.00	0.00	0.00	0.07	0.00	5.52	2.00	0.00	0.00	0.07	0.00
5.59	2.00	0.00	0.00	0.07	0.00	5.64	2.00	0.00	0.00	0.05	0.00
5.72	2.00	0.00	0.00	0.07	0.00	5.78	2.00	0.00	0.00	0.06	0.00
5.85	2.00	0.00	0.00	0.07	0.00	5.92	2.00	0.00	0.00	0.07	0.00
5.98	2.00	0.00	0.00	0.07	0.00	6.04	2.00	0.00	0.00	0.06	0.00
6.11	2.00	0.00	0.00	0.07	0.00	6.17	2.00	0.00	0.00	0.06	0.00
6.24	2.00	0.00	0.00	0.07	0.00	6.32	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
6.38	2.00	0.00	0.00	0.06	0.00	6.44	2.00	0.00	0.00	0.06	0.00
6.51	2.00	0.00	0.00	0.08	0.00	6.58	2.00	0.00	0.00	0.06	0.00
6.66	2.00	0.00	0.00	0.08	0.00	6.71	2.00	0.00	0.00	0.05	0.00
6.77	2.00	0.00	0.00	0.06	0.00	6.83	2.00	0.00	0.00	0.05	0.00
6.92	2.00	0.00	0.00	0.10	0.00	6.97	2.00	0.00	0.00	0.05	0.00
7.03	2.00	0.00	0.00	0.05	0.00	7.10	2.00	0.00	0.00	0.07	0.00
7.16	2.00	0.00	0.00	0.07	0.00	7.22	2.00	0.00	0.00	0.06	0.00
7.31	2.00	0.00	0.00	0.09	0.00	7.36	2.00	0.00	0.00	0.05	0.00
7.42	2.00	0.00	0.00	0.06	0.00	7.49	2.00	0.00	0.00	0.07	0.00
7.55	2.00	0.00	0.00	0.06	0.00	7.62	2.00	0.00	0.00	0.07	0.00
7.71	2.00	0.00	0.00	0.09	0.00	7.75	2.00	0.00	0.00	0.04	0.00
7.83	2.00	0.00	0.00	0.09	0.00	7.88	2.00	0.00	0.00	0.04	0.00
7.95	2.00	0.00	0.00	0.07	0.00	8.01	0.48	0.52	0.45	0.06	0.09
8.09	0.46	0.54	0.44	0.08	0.11	8.14	0.45	0.55	0.42	0.05	0.08
8.24	0.43	0.57	0.41	0.10	0.15	8.29	0.42	0.58	0.40	0.05	0.07
8.34	0.41	0.59	0.39	0.05	0.08	8.41	0.40	0.60	0.38	0.07	0.11
8.49	0.38	0.62	0.37	0.08	0.13	8.53	0.37	0.63	0.36	0.05	0.08
8.60	0.36	0.64	0.35	0.07	0.12	8.67	0.34	0.66	0.35	0.07	0.11
8.73	0.33	0.67	0.34	0.06	0.11	8.80	0.31	0.69	0.33	0.07	0.13
8.87	0.30	0.70	0.32	0.08	0.14	8.93	0.29	0.71	0.32	0.05	0.10
9.02	0.29	0.71	0.32	0.09	0.17	9.07	0.28	0.72	0.31	0.06	0.11
9.13	0.28	0.72	0.31	0.05	0.09	9.20	0.28	0.72	0.31	0.07	0.14
9.25	0.28	0.72	0.31	0.05	0.10	9.32	0.27	0.73	0.31	0.07	0.13
9.39	0.26	0.74	0.30	0.07	0.14	9.46	0.26	0.74	0.30	0.07	0.13
9.52	0.25	0.75	0.30	0.06	0.13	9.61	0.23	0.77	0.29	0.09	0.17
9.66	0.23	0.77	0.29	0.05	0.11	9.71	0.22	0.78	0.29	0.05	0.10
9.78	0.22	0.78	0.28	0.07	0.14	9.86	0.22	0.78	0.28	0.08	0.16
9.91	0.22	0.78	0.28	0.06	0.11	9.97	0.22	0.78	0.28	0.06	0.12
10.06	0.22	0.78	0.29	0.08	0.17	10.11	0.23	0.77	0.29	0.05	0.10
10.17	0.23	0.77	0.29	0.06	0.13	10.25	0.24	0.76	0.29	0.08	0.15
10.31	0.24	0.76	0.30	0.06	0.11	10.37	0.25	0.75	0.30	0.06	0.12
10.44	0.26	0.74	0.30	0.06	0.12	10.50	0.27	0.73	0.31	0.06	0.12
10.57	0.27	0.73	0.31	0.07	0.13	10.64	0.28	0.72	0.31	0.07	0.14
10.70	0.28	0.72	0.31	0.05	0.10	10.77	0.28	0.72	0.31	0.08	0.14
10.85	0.28	0.72	0.31	0.07	0.13	10.90	0.28	0.72	0.31	0.05	0.09
10.97	0.29	0.71	0.32	0.07	0.13	11.03	0.29	0.71	0.32	0.06	0.11
11.09	0.29	0.71	0.32	0.06	0.11	11.17	0.29	0.71	0.32	0.08	0.14
11.26	0.30	0.70	0.32	0.09	0.17	11.30	0.30	0.70	0.32	0.04	0.06
11.36	0.29	0.71	0.32	0.06	0.10	11.42	0.28	0.72	0.31	0.07	0.12
11.50	0.28	0.72	0.31	0.07	0.13	11.56	0.27	0.73	0.31	0.06	0.12
11.62	0.26	0.74	0.30	0.06	0.11	11.69	0.24	0.76	0.30	0.07	0.13
11.76	0.23	0.77	0.29	0.07	0.13	11.83	0.23	0.77	0.29	0.07	0.14
11.88	0.23	0.77	0.29	0.05	0.10	11.95	0.22	0.78	0.29	0.07	0.13
12.01	0.22	0.78	0.29	0.06	0.11	12.08	0.22	0.78	0.28	0.08	0.15
12.14	0.22	0.78	0.28	0.06	0.12	12.23	0.21	0.79	0.28	0.09	0.18
12.28	0.21	0.79	0.28	0.04	0.08	12.35	0.21	0.79	0.28	0.08	0.15
12.40	0.21	0.79	0.28	0.05	0.09	12.47	0.22	0.78	0.28	0.07	0.13
12.54	0.22	0.78	0.29	0.07	0.14	12.60	0.22	0.78	0.29	0.06	0.11

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
12.70	0.22	0.78	0.29	0.09	0.18	12.75	0.22	0.78	0.29	0.05	0.10
12.80	0.22	0.78	0.29	0.05	0.10	12.87	0.22	0.78	0.29	0.07	0.14
12.93	0.22	0.78	0.29	0.05	0.10	12.99	0.23	0.77	0.29	0.07	0.13
13.06	0.24	0.76	0.29	0.06	0.12	13.14	0.24	0.76	0.29	0.08	0.15
13.19	0.24	0.76	0.30	0.05	0.10	13.26	0.25	0.75	0.30	0.07	0.14
13.32	0.25	0.75	0.30	0.06	0.11	13.40	0.25	0.75	0.30	0.07	0.14
13.46	0.25	0.75	0.30	0.06	0.11	13.53	0.24	0.76	0.30	0.07	0.12
13.58	0.25	0.75	0.30	0.06	0.11	13.68	0.24	0.76	0.29	0.10	0.18
13.73	0.24	0.76	0.29	0.05	0.09	13.79	0.23	0.77	0.29	0.06	0.10
13.88	0.23	0.77	0.29	0.09	0.17	13.92	0.23	0.77	0.29	0.04	0.08
13.98	0.23	0.77	0.29	0.06	0.12	14.05	0.24	0.76	0.29	0.06	0.11
14.13	0.25	0.75	0.30	0.08	0.14	14.17	0.25	0.75	0.30	0.05	0.09
14.24	0.26	0.74	0.30	0.07	0.12	14.33	0.27	0.73	0.31	0.09	0.15
14.37	0.28	0.72	0.31	0.05	0.08	14.45	0.29	0.71	0.32	0.08	0.13
14.53	0.30	0.70	0.32	0.07	0.12	14.57	0.31	0.69	0.33	0.05	0.08
14.64	0.32	0.68	0.33	0.07	0.12	14.72	0.33	0.67	0.34	0.08	0.12
14.76	0.34	0.66	0.34	0.04	0.07	14.85	0.35	0.65	0.35	0.08	0.13
14.90	0.35	0.65	0.35	0.05	0.08	14.96	0.37	0.63	0.36	0.06	0.10
15.03	0.38	0.62	0.37	0.07	0.10	15.10	0.38	0.62	0.37	0.06	0.09
15.16	0.39	0.61	0.38	0.06	0.09	15.24	0.39	0.61	0.38	0.08	0.12
15.31	0.39	0.61	0.38	0.07	0.09	15.36	0.38	0.62	0.37	0.05	0.08
15.45	0.36	0.64	0.36	0.08	0.13	15.50	0.34	0.66	0.35	0.05	0.08
15.55	0.33	0.67	0.34	0.05	0.08	15.66	0.29	0.71	0.32	0.11	0.18
15.69	0.28	0.72	0.31	0.03	0.05	15.75	0.27	0.73	0.31	0.07	0.11
15.82	0.25	0.75	0.30	0.07	0.11	15.91	0.24	0.76	0.29	0.09	0.15
15.96	0.23	0.77	0.29	0.05	0.09	16.02	0.22	0.78	0.28	0.06	0.10
16.08	0.21	0.79	0.28	0.07	0.12	16.14	0.20	0.80	0.28	0.06	0.11
16.22	0.19	0.81	0.27	0.07	0.14	16.30	2.00	0.00	0.00	0.08	0.00
16.34	2.00	0.00	0.00	0.04	0.00	16.42	2.00	0.00	0.00	0.08	0.00
16.50	2.00	0.00	0.00	0.08	0.00	16.54	2.00	0.00	0.00	0.04	0.00
16.62	2.00	0.00	0.00	0.08	0.00	16.70	2.00	0.00	0.00	0.08	0.00
16.74	2.00	0.00	0.00	0.04	0.00	16.80	2.00	0.00	0.00	0.06	0.00
16.87	0.23	0.77	0.29	0.07	0.13	16.94	0.26	0.74	0.30	0.07	0.11
17.01	0.34	0.66	0.34	0.07	0.10	17.09	0.38	0.62	0.37	0.08	0.11
17.14	0.43	0.57	0.41	0.05	0.07	17.23	0.52	0.48	0.51	0.09	0.09
17.28	0.55	0.45	0.54	0.05	0.06	17.34	0.55	0.45	0.55	0.05	0.06
17.39	0.55	0.45	0.55	0.05	0.05	17.46	0.57	0.43	0.57	0.07	0.07
17.52	0.57	0.43	0.58	0.06	0.06	17.60	0.57	0.43	0.58	0.08	0.08
17.66	0.57	0.43	0.57	0.05	0.05	17.73	0.55	0.45	0.54	0.07	0.08
17.79	0.52	0.48	0.51	0.06	0.06	17.86	0.50	0.50	0.48	0.06	0.07
17.92	0.48	0.52	0.46	0.06	0.07	17.98	0.45	0.55	0.43	0.06	0.08
18.07	0.44	0.56	0.42	0.08	0.11	18.11	0.43	0.57	0.41	0.05	0.06
18.18	0.41	0.59	0.39	0.07	0.09	18.27	0.40	0.60	0.39	0.08	0.11
18.32	0.39	0.61	0.38	0.06	0.08	18.37	0.38	0.62	0.37	0.05	0.07
18.46	0.35	0.65	0.35	0.09	0.13	18.52	0.32	0.68	0.34	0.06	0.09
18.57	0.30	0.70	0.32	0.05	0.08	18.66	0.25	0.75	0.30	0.09	0.15
18.71	0.23	0.77	0.29	0.05	0.09	18.77	0.21	0.79	0.28	0.06	0.10
18.84	0.19	0.81	0.27	0.07	0.13	18.91	0.17	0.83	0.27	0.07	0.12

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
18.97	2.00	0.00	0.00	0.06	0.00	19.05	2.00	0.00	0.00	0.08	0.00
19.10	2.00	0.00	0.00	0.05	0.00	19.16	2.00	0.00	0.00	0.06	0.00
19.26	2.00	0.00	0.00	0.10	0.00	19.30	2.00	0.00	0.00	0.04	0.00
19.36	2.00	0.00	0.00	0.06	0.00	19.43	2.00	0.00	0.00	0.06	0.00
19.51	2.00	0.00	0.00	0.08	0.00	19.55	2.00	0.00	0.00	0.05	0.00
19.63	2.00	0.00	0.00	0.07	0.00	19.69	2.00	0.00	0.00	0.06	0.00
19.75	2.00	0.00	0.00	0.06	0.00	19.84	2.00	0.00	0.00	0.09	0.00
19.89	2.00	0.00	0.00	0.04	0.00	19.96	2.00	0.00	0.00	0.08	0.00
20.02	2.00	0.00	0.00	0.05	0.00	20.09	2.00	0.00	0.00	0.07	0.00
20.14	2.00	0.00	0.00	0.06	0.00	20.22	2.00	0.00	0.00	0.08	0.00
20.28	2.00	0.00	0.00	0.06	0.00	20.36	2.00	0.00	0.00	0.08	0.00
20.41	2.00	0.00	0.00	0.04	0.00	20.48	2.00	0.00	0.00	0.08	0.00
20.55	2.00	0.00	0.00	0.06	0.00	20.61	2.00	0.00	0.00	0.07	0.00
20.68	2.00	0.00	0.00	0.07	0.00	20.74	2.00	0.00	0.00	0.06	0.00
20.81	2.00	0.00	0.00	0.08	0.00	20.88	2.00	0.00	0.00	0.06	0.00
20.93	2.00	0.00	0.00	0.06	0.00	21.00	2.00	0.00	0.00	0.06	0.00
21.07	2.00	0.00	0.00	0.07	0.00	21.13	2.00	0.00	0.00	0.06	0.00
21.22	2.00	0.00	0.00	0.09	0.00	21.27	2.00	0.00	0.00	0.04	0.00
21.34	2.00	0.00	0.00	0.07	0.00	21.41	2.00	0.00	0.00	0.07	0.00
21.46	2.00	0.00	0.00	0.05	0.00	21.55	2.00	0.00	0.00	0.09	0.00
21.59	2.00	0.00	0.00	0.05	0.00	21.66	2.00	0.00	0.00	0.06	0.00
21.76	2.00	0.00	0.00	0.10	0.00	21.80	2.00	0.00	0.00	0.04	0.00
21.86	2.00	0.00	0.00	0.06	0.00	21.95	2.00	0.00	0.00	0.09	0.00
22.01	2.00	0.00	0.00	0.06	0.00	22.06	0.18	0.82	0.27	0.05	0.09
22.12	0.19	0.81	0.27	0.06	0.09	22.18	0.19	0.81	0.27	0.06	0.10
22.26	0.20	0.80	0.28	0.08	0.13	22.31	0.21	0.79	0.28	0.05	0.08
22.38	0.22	0.78	0.28	0.07	0.10	22.44	0.23	0.77	0.29	0.07	0.11
22.53	0.25	0.75	0.30	0.09	0.13	22.59	0.26	0.74	0.30	0.05	0.08
22.65	0.27	0.73	0.31	0.06	0.09	22.71	0.28	0.72	0.31	0.06	0.08
22.78	0.30	0.70	0.32	0.07	0.10	22.86	0.31	0.69	0.33	0.08	0.11
22.92	0.32	0.68	0.34	0.05	0.07	22.98	0.33	0.67	0.34	0.06	0.08
23.04	0.33	0.67	0.34	0.05	0.07	23.10	0.34	0.66	0.34	0.07	0.09
23.16	0.34	0.66	0.34	0.06	0.08	23.25	0.34	0.66	0.34	0.09	0.12
23.30	0.34	0.66	0.34	0.05	0.06	23.36	0.34	0.66	0.34	0.06	0.08
23.43	0.34	0.66	0.35	0.07	0.09	23.49	0.34	0.66	0.35	0.06	0.08
23.56	0.35	0.65	0.35	0.07	0.09	23.65	0.36	0.64	0.36	0.09	0.11
23.71	0.35	0.65	0.35	0.06	0.07	23.76	0.34	0.66	0.35	0.05	0.07
23.83	0.31	0.69	0.33	0.07	0.09	23.89	0.28	0.72	0.31	0.06	0.09
23.95	0.24	0.76	0.29	0.06	0.09	24.02	0.21	0.79	0.28	0.07	0.10
24.09	0.19	0.81	0.27	0.06	0.10	24.15	2.00	0.00	0.00	0.07	0.00
24.24	2.00	0.00	0.00	0.09	0.00	24.29	2.00	0.00	0.00	0.05	0.00
24.35	2.00	0.00	0.00	0.06	0.00	24.42	2.00	0.00	0.00	0.08	0.00
24.49	2.00	0.00	0.00	0.07	0.00	24.54	2.00	0.00	0.00	0.05	0.00
24.62	2.00	0.00	0.00	0.08	0.00	24.69	2.00	0.00	0.00	0.07	0.00
24.75	2.00	0.00	0.00	0.05	0.00	24.81	2.00	0.00	0.00	0.06	0.00
24.88	2.00	0.00	0.00	0.07	0.00	24.94	2.00	0.00	0.00	0.06	0.00
25.00	2.00	0.00	0.00	0.06	0.00	25.07	0.18	0.82	0.27	0.07	0.10
25.13	0.19	0.81	0.27	0.06	0.09	25.22	0.22	0.78	0.29	0.09	0.13

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
25.27	0.24	0.76	0.29	0.04	0.06	25.33	0.26	0.74	0.30	0.06	0.09
25.40	0.27	0.73	0.31	0.07	0.09	25.48	0.27	0.73	0.31	0.08	0.11
25.53	0.25	0.75	0.30	0.05	0.07	25.60	0.23	0.77	0.29	0.07	0.11
25.67	0.22	0.78	0.29	0.07	0.10	25.73	0.21	0.79	0.28	0.06	0.09
25.79	0.19	0.81	0.27	0.06	0.09	25.87	2.00	0.00	0.00	0.08	0.00
25.92	2.00	0.00	0.00	0.05	0.00	26.00	2.00	0.00	0.00	0.08	0.00
26.07	2.00	0.00	0.00	0.07	0.00	26.12	2.00	0.00	0.00	0.04	0.00
26.19	2.00	0.00	0.00	0.07	0.00	26.25	2.00	0.00	0.00	0.06	0.00
26.33	2.00	0.00	0.00	0.08	0.00	26.39	2.00	0.00	0.00	0.06	0.00
26.45	2.00	0.00	0.00	0.06	0.00	26.52	2.00	0.00	0.00	0.07	0.00
26.58	2.00	0.00	0.00	0.06	0.00	26.66	2.00	0.00	0.00	0.09	0.00
26.72	2.00	0.00	0.00	0.06	0.00	26.78	2.00	0.00	0.00	0.05	0.00
26.84	0.16	0.84	0.26	0.07	0.10	26.91	0.17	0.83	0.27	0.07	0.11
26.97	0.18	0.82	0.27	0.06	0.08	27.05	0.19	0.81	0.27	0.07	0.11
27.10	0.20	0.80	0.28	0.05	0.08	27.17	0.21	0.79	0.28	0.07	0.09
27.24	0.22	0.78	0.29	0.07	0.10	27.30	0.23	0.77	0.29	0.06	0.09
27.37	0.24	0.76	0.29	0.07	0.09	27.46	0.25	0.75	0.30	0.09	0.12
27.51	0.26	0.74	0.30	0.05	0.06	27.57	0.27	0.73	0.31	0.05	0.07
27.64	0.28	0.72	0.31	0.08	0.10	27.70	0.29	0.71	0.32	0.06	0.07
27.76	0.29	0.71	0.32	0.06	0.07	27.82	0.30	0.70	0.32	0.06	0.08
27.91	0.30	0.70	0.32	0.08	0.10	27.96	0.31	0.69	0.33	0.05	0.06
28.03	0.31	0.69	0.33	0.07	0.08	28.09	0.31	0.69	0.33	0.07	0.08
28.16	0.31	0.69	0.33	0.06	0.08	28.23	0.30	0.70	0.32	0.08	0.10
28.29	0.28	0.72	0.31	0.06	0.07	28.36	0.26	0.74	0.30	0.06	0.08
28.45	0.24	0.76	0.29	0.09	0.12	28.48	0.23	0.77	0.29	0.03	0.04
28.55	0.22	0.78	0.29	0.07	0.09	28.61	0.21	0.79	0.28	0.07	0.09
28.68	0.21	0.79	0.28	0.06	0.08	28.74	0.21	0.79	0.28	0.07	0.09
28.81	0.20	0.80	0.28	0.07	0.10	28.87	0.17	0.83	0.27	0.06	0.09
28.94	0.17	0.83	0.27	0.07	0.09	29.03	2.00	0.00	0.00	0.09	0.00
29.08	2.00	0.00	0.00	0.05	0.00	29.16	2.00	0.00	0.00	0.07	0.00
29.22	2.00	0.00	0.00	0.07	0.00	29.27	2.00	0.00	0.00	0.05	0.00
29.35	2.00	0.00	0.00	0.08	0.00	29.43	2.00	0.00	0.00	0.07	0.00
29.47	2.00	0.00	0.00	0.04	0.00	29.53	2.00	0.00	0.00	0.06	0.00
29.60	2.00	0.00	0.00	0.07	0.00	29.67	2.00	0.00	0.00	0.07	0.00
29.73	2.00	0.00	0.00	0.06	0.00	29.80	2.00	0.00	0.00	0.08	0.00
29.87	2.00	0.00	0.00	0.07	0.00	29.93	2.00	0.00	0.00	0.06	0.00
30.00	2.00	0.00	0.00	0.07	0.00	30.07	2.00	0.00	0.00	0.07	0.00
30.12	2.00	0.00	0.00	0.05	0.00	30.20	2.00	0.00	0.00	0.08	0.00
30.27	2.00	0.00	0.00	0.07	0.00	30.32	2.00	0.00	0.00	0.05	0.00
30.40	2.00	0.00	0.00	0.08	0.00	30.46	2.00	0.00	0.00	0.06	0.00
30.52	2.00	0.00	0.00	0.06	0.00	30.59	2.00	0.00	0.00	0.07	0.00
30.65	2.00	0.00	0.00	0.06	0.00	30.71	2.00	0.00	0.00	0.06	0.00
30.79	2.00	0.00	0.00	0.08	0.00	30.85	2.00	0.00	0.00	0.07	0.00
30.96	2.00	0.00	0.00	0.10	0.00	31.00	2.00	0.00	0.00	0.04	0.00
31.04	2.00	0.00	0.00	0.04	0.00	31.11	2.00	0.00	0.00	0.07	0.00
31.18	2.00	0.00	0.00	0.07	0.00	31.25	2.00	0.00	0.00	0.07	0.00
31.30	2.00	0.00	0.00	0.06	0.00	31.38	2.00	0.00	0.00	0.07	0.00
31.44	2.00	0.00	0.00	0.06	0.00	31.50	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
31.57	2.00	0.00	0.00	0.07	0.00	31.63	2.00	0.00	0.00	0.06	0.00
31.70	2.00	0.00	0.00	0.07	0.00	31.79	2.00	0.00	0.00	0.09	0.00
31.83	2.00	0.00	0.00	0.04	0.00	31.90	2.00	0.00	0.00	0.07	0.00
31.97	2.00	0.00	0.00	0.07	0.00	32.03	2.00	0.00	0.00	0.06	0.00
32.10	2.00	0.00	0.00	0.07	0.00	32.16	2.00	0.00	0.00	0.06	0.00
32.23	2.00	0.00	0.00	0.07	0.00	32.30	2.00	0.00	0.00	0.07	0.00
32.36	2.00	0.00	0.00	0.06	0.00	32.46	2.00	0.00	0.00	0.09	0.00
32.51	2.00	0.00	0.00	0.05	0.00	32.56	2.00	0.00	0.00	0.06	0.00
32.65	2.00	0.00	0.00	0.09	0.00	32.68	2.00	0.00	0.00	0.04	0.00
32.76	2.00	0.00	0.00	0.07	0.00	32.84	2.00	0.00	0.00	0.09	0.00
32.89	2.00	0.00	0.00	0.04	0.00	32.95	2.00	0.00	0.00	0.07	0.00
33.01	2.00	0.00	0.00	0.06	0.00	33.10	2.00	0.00	0.00	0.09	0.00
33.15	2.00	0.00	0.00	0.05	0.00	33.24	2.00	0.00	0.00	0.08	0.00
33.29	2.00	0.00	0.00	0.06	0.00	33.35	2.00	0.00	0.00	0.05	0.00
33.40	2.00	0.00	0.00	0.05	0.00	33.47	2.00	0.00	0.00	0.06	0.00
33.55	2.00	0.00	0.00	0.08	0.00	33.65	2.00	0.00	0.00	0.10	0.00
33.66	2.00	0.00	0.00	0.02	0.00	33.74	2.00	0.00	0.00	0.07	0.00
33.84	2.00	0.00	0.00	0.10	0.00	33.88	2.00	0.00	0.00	0.03	0.00
33.93	2.00	0.00	0.00	0.05	0.00	33.99	2.00	0.00	0.00	0.07	0.00
34.07	2.00	0.00	0.00	0.08	0.00	34.12	2.00	0.00	0.00	0.05	0.00
34.19	2.00	0.00	0.00	0.07	0.00	34.28	2.00	0.00	0.00	0.09	0.00
34.32	2.00	0.00	0.00	0.04	0.00	34.40	2.00	0.00	0.00	0.08	0.00
34.48	2.00	0.00	0.00	0.07	0.00	34.52	2.00	0.00	0.00	0.04	0.00
34.58	2.00	0.00	0.00	0.06	0.00	34.68	2.00	0.00	0.00	0.09	0.00
34.72	2.00	0.00	0.00	0.04	0.00	34.81	2.00	0.00	0.00	0.09	0.00
34.85	2.00	0.00	0.00	0.04	0.00	34.92	2.00	0.00	0.00	0.07	0.00
34.98	2.00	0.00	0.00	0.05	0.00	35.05	2.00	0.00	0.00	0.07	0.00
35.12	2.00	0.00	0.00	0.07	0.00	35.18	2.00	0.00	0.00	0.06	0.00
35.26	2.00	0.00	0.00	0.08	0.00	35.31	2.00	0.00	0.00	0.05	0.00
35.41	2.00	0.00	0.00	0.10	0.00	35.47	2.00	0.00	0.00	0.05	0.00
35.51	2.00	0.00	0.00	0.04	0.00	35.58	2.00	0.00	0.00	0.07	0.00
35.63	0.16	0.84	0.26	0.05	0.06	35.71	0.18	0.82	0.27	0.08	0.09
35.78	0.19	0.81	0.27	0.07	0.08	35.84	0.18	0.82	0.27	0.06	0.07
35.90	0.17	0.83	0.27	0.06	0.07	35.98	2.00	0.00	0.00	0.08	0.00
36.05	2.00	0.00	0.00	0.07	0.00	36.10	2.00	0.00	0.00	0.05	0.00
36.20	2.00	0.00	0.00	0.10	0.00	36.25	2.00	0.00	0.00	0.05	0.00
36.30	2.00	0.00	0.00	0.05	0.00	36.35	2.00	0.00	0.00	0.05	0.00
36.45	2.00	0.00	0.00	0.10	0.00	36.48	2.00	0.00	0.00	0.03	0.00
36.55	2.00	0.00	0.00	0.07	0.00	36.63	2.00	0.00	0.00	0.08	0.00
36.69	2.00	0.00	0.00	0.07	0.00	36.75	2.00	0.00	0.00	0.05	0.00
36.84	2.00	0.00	0.00	0.09	0.00	36.89	2.00	0.00	0.00	0.05	0.00
36.95	2.00	0.00	0.00	0.05	0.00	37.05	2.00	0.00	0.00	0.10	0.00
37.08	2.00	0.00	0.00	0.03	0.00	37.14	2.00	0.00	0.00	0.06	0.00
37.23	2.00	0.00	0.00	0.09	0.00	37.28	2.00	0.00	0.00	0.05	0.00
37.34	2.00	0.00	0.00	0.05	0.00	37.43	2.00	0.00	0.00	0.09	0.00
37.48	2.00	0.00	0.00	0.06	0.00	37.53	2.00	0.00	0.00	0.05	0.00
37.61	2.00	0.00	0.00	0.08	0.00	37.67	2.00	0.00	0.00	0.06	0.00
37.73	2.00	0.00	0.00	0.06	0.00	37.82	2.00	0.00	0.00	0.09	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
37.88	2.00	0.00	0.00	0.06	0.00	37.93	2.00	0.00	0.00	0.05	0.00
38.00	0.19	0.81	0.27	0.07	0.07	38.08	0.20	0.80	0.28	0.08	0.08
38.12	0.22	0.78	0.28	0.04	0.04	38.20	0.24	0.76	0.29	0.08	0.08
38.29	0.28	0.72	0.31	0.08	0.08	38.33	0.30	0.70	0.32	0.04	0.04
38.43	0.37	0.63	0.36	0.10	0.08	38.48	0.39	0.61	0.38	0.04	0.03
38.52	0.42	0.58	0.40	0.04	0.03	38.59	0.45	0.55	0.43	0.07	0.05
38.68	0.47	0.53	0.44	0.09	0.06	38.72	0.49	0.51	0.46	0.04	0.03
38.79	0.54	0.46	0.52	0.08	0.04	38.87	0.61	0.39	0.66	0.07	0.03
38.92	0.73	0.27	1.06	0.06	0.02	38.98	0.89	0.00	0.00	0.05	0.01
39.05	1.20	0.00	0.00	0.07	0.00	39.12	1.51	0.00	0.00	0.07	0.00
39.17	1.83	0.00	0.00	0.06	0.00	39.26	2.00	0.00	0.00	0.09	0.00
39.32	2.00	0.00	0.00	0.06	0.00	39.37	2.00	0.00	0.00	0.05	0.00
39.46	2.00	0.00	0.00	0.09	0.00	39.52	2.00	0.00	0.00	0.05	0.00
39.57	2.00	0.00	0.00	0.05	0.00	39.63	2.00	0.00	0.00	0.06	0.00
39.72	2.00	0.00	0.00	0.09	0.00	39.77	1.95	0.00	0.00	0.05	0.00
39.85	1.70	0.00	0.00	0.08	0.00	39.91	1.58	0.00	0.00	0.06	0.00
39.96	1.43	0.00	0.00	0.06	0.00	40.06	1.28	0.00	0.00	0.09	0.00
40.11	1.12	0.00	0.00	0.05	0.00	40.16	0.97	0.00	0.00	0.05	0.00
40.26	0.69	0.31	0.89	0.10	0.04	40.30	0.60	0.40	0.63	0.04	0.02
40.36	0.50	0.50	0.48	0.06	0.03	40.44	0.40	0.60	0.39	0.08	0.06
40.50	0.36	0.64	0.36	0.06	0.05	40.55	0.32	0.68	0.33	0.05	0.04
40.62	0.29	0.71	0.32	0.06	0.05	40.68	0.27	0.73	0.31	0.07	0.06
40.75	0.25	0.75	0.30	0.07	0.06	40.84	0.24	0.76	0.29	0.09	0.08
40.90	0.24	0.76	0.29	0.06	0.05	40.96	0.23	0.77	0.29	0.06	0.05
41.04	0.23	0.77	0.29	0.08	0.07	41.09	0.23	0.77	0.29	0.05	0.04
41.15	0.23	0.77	0.29	0.06	0.05	41.22	0.24	0.76	0.29	0.07	0.06
41.30	0.24	0.76	0.29	0.07	0.06	41.35	0.25	0.75	0.30	0.05	0.04
41.41	0.25	0.75	0.30	0.06	0.05	41.48	0.25	0.75	0.30	0.07	0.06
41.55	0.26	0.74	0.30	0.07	0.06	41.62	0.26	0.74	0.30	0.07	0.06
41.68	0.26	0.74	0.30	0.06	0.05	41.74	0.26	0.74	0.30	0.06	0.05
41.80	0.25	0.75	0.30	0.06	0.05	41.88	0.25	0.75	0.30	0.08	0.06
41.95	0.26	0.74	0.30	0.07	0.05	42.00	0.26	0.74	0.30	0.05	0.04
42.08	0.25	0.75	0.30	0.08	0.07	42.15	0.25	0.75	0.30	0.07	0.05
42.22	0.24	0.76	0.29	0.07	0.06	42.28	0.22	0.78	0.29	0.06	0.05
42.34	0.21	0.79	0.28	0.06	0.05	42.39	0.20	0.80	0.28	0.05	0.04
42.48	0.20	0.80	0.28	0.09	0.07	42.53	0.20	0.80	0.28	0.05	0.04
42.59	0.21	0.79	0.28	0.06	0.05	42.68	0.21	0.79	0.28	0.09	0.07
42.72	0.22	0.78	0.28	0.04	0.04	42.79	0.23	0.77	0.29	0.07	0.05
42.87	0.26	0.74	0.30	0.08	0.07	42.92	0.27	0.73	0.31	0.05	0.04
43.00	0.27	0.73	0.31	0.08	0.06	43.05	0.27	0.73	0.31	0.05	0.03
43.13	0.28	0.72	0.31	0.09	0.06	43.22	0.28	0.72	0.31	0.09	0.07
43.27	0.27	0.73	0.31	0.05	0.04	43.33	0.25	0.75	0.30	0.06	0.04
43.37	0.23	0.77	0.29	0.05	0.04	43.47	0.19	0.81	0.27	0.10	0.08
43.52	0.18	0.82	0.27	0.05	0.04	43.57	2.00	0.00	0.00	0.05	0.00
43.66	2.00	0.00	0.00	0.09	0.00	43.72	2.00	0.00	0.00	0.06	0.00
43.77	2.00	0.00	0.00	0.05	0.00	43.83	2.00	0.00	0.00	0.06	0.00
43.90	2.00	0.00	0.00	0.07	0.00	43.97	2.00	0.00	0.00	0.07	0.00
44.03	2.00	0.00	0.00	0.06	0.00	44.13	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}
44.17	2.00	0.00	0.00	0.04	0.00	44.23	2.00	0.00	0.00	0.06	0.00
44.33	2.00	0.00	0.00	0.10	0.00	44.37	2.00	0.00	0.00	0.04	0.00
44.43	2.00	0.00	0.00	0.06	0.00	44.52	2.00	0.00	0.00	0.10	0.00
44.57	2.00	0.00	0.00	0.05	0.00	44.62	2.00	0.00	0.00	0.05	0.00
44.72	2.00	0.00	0.00	0.10	0.00	44.76	2.00	0.00	0.00	0.04	0.00
44.83	0.17	0.83	0.27	0.07	0.05	44.92	0.21	0.79	0.28	0.09	0.07
44.97	0.25	0.75	0.30	0.05	0.04	45.02	0.26	0.74	0.30	0.05	0.03
45.09	0.27	0.73	0.31	0.07	0.05	45.16	0.28	0.72	0.31	0.07	0.05
45.22	0.29	0.71	0.32	0.06	0.04	45.29	0.31	0.69	0.33	0.07	0.05
45.37	0.31	0.69	0.33	0.07	0.05	45.41	0.28	0.72	0.31	0.04	0.03
45.47	0.22	0.78	0.29	0.06	0.05	45.56	2.00	0.00	0.00	0.09	0.00
45.62	2.00	0.00	0.00	0.05	0.00	45.70	2.00	0.00	0.00	0.09	0.00
45.75	2.00	0.00	0.00	0.05	0.00	45.81	2.00	0.00	0.00	0.06	0.00
45.90	2.00	0.00	0.00	0.09	0.00	45.95	2.00	0.00	0.00	0.05	0.00
46.01	2.00	0.00	0.00	0.06	0.00	46.10	2.00	0.00	0.00	0.09	0.00
46.15	2.00	0.00	0.00	0.05	0.00	46.21	2.00	0.00	0.00	0.05	0.00
46.29	2.00	0.00	0.00	0.08	0.00	46.33	2.00	0.00	0.00	0.04	0.00
46.41	2.00	0.00	0.00	0.07	0.00	46.47	2.00	0.00	0.00	0.07	0.00
46.53	0.17	0.83	0.27	0.06	0.05	46.59	0.17	0.83	0.27	0.06	0.04
46.66	0.18	0.82	0.27	0.06	0.04	46.75	0.19	0.81	0.27	0.09	0.06
46.79	0.19	0.81	0.27	0.04	0.03	46.85	0.19	0.81	0.27	0.06	0.05
46.92	0.19	0.81	0.27	0.07	0.05	47.00	0.20	0.80	0.28	0.08	0.06
47.05	0.20	0.80	0.28	0.05	0.04	47.12	0.19	0.81	0.27	0.06	0.04
47.20	0.19	0.81	0.27	0.08	0.05	47.26	0.18	0.82	0.27	0.07	0.05
47.32	0.18	0.82	0.27	0.05	0.04	47.39	2.00	0.00	0.00	0.07	0.00
47.47	2.00	0.00	0.00	0.08	0.00	47.51	2.00	0.00	0.00	0.05	0.00
47.59	2.00	0.00	0.00	0.08	0.00	47.65	2.00	0.00	0.00	0.06	0.00
47.71	2.00	0.00	0.00	0.06	0.00	47.79	2.00	0.00	0.00	0.08	0.00
47.85	2.00	0.00	0.00	0.06	0.00	47.91	2.00	0.00	0.00	0.06	0.00
48.00	2.00	0.00	0.00	0.09	0.00	48.05	2.00	0.00	0.00	0.05	0.00
48.10	0.20	0.80	0.28	0.05	0.03	48.19	0.37	0.63	0.36	0.09	0.04
48.25	0.47	0.53	0.44	0.06	0.03	48.30	0.52	0.48	0.50	0.05	0.02
48.39	0.59	0.41	0.61	0.09	0.03	48.43	0.61	0.39	0.64	0.04	0.01
48.50	0.67	0.33	0.81	0.07	0.02	48.59	0.76	0.00	0.00	0.08	0.02
48.64	0.79	0.00	0.00	0.05	0.01	48.70	0.81	0.00	0.00	0.06	0.01
48.79	0.79	0.00	0.00	0.10	0.02	48.83	0.78	0.00	0.00	0.03	0.01
48.89	0.74	0.26	1.13	0.06	0.01	48.95	0.70	0.30	0.90	0.06	0.02
49.02	0.65	0.35	0.76	0.07	0.02	49.11	0.58	0.42	0.59	0.09	0.03
49.19	0.54	0.46	0.53	0.08	0.03	49.22	0.51	0.49	0.49	0.03	0.01
49.28	0.46	0.54	0.44	0.06	0.03	49.35	0.41	0.59	0.39	0.07	0.03
49.42	0.37	0.63	0.36	0.06	0.03	49.48	0.33	0.67	0.34	0.07	0.03
49.56	0.30	0.70	0.32	0.07	0.04	49.63	0.29	0.71	0.32	0.08	0.04
49.68	0.27	0.73	0.31	0.05	0.03	49.74	0.26	0.74	0.30	0.06	0.03
49.83	0.26	0.74	0.30	0.09	0.05	49.87	0.25	0.75	0.30	0.04	0.02
49.97	0.24	0.76	0.29	0.10	0.06	50.03	2.00	0.00	0.00	0.05	0.00
50.08	2.00	0.00	0.00	0.06	0.00	50.14	2.00	0.00	0.00	0.05	0.00
50.23	2.00	0.00	0.00	0.10	0.00	50.27	2.00	0.00	0.00	0.03	0.00
50.33	2.00	0.00	0.00	0.06	0.00	50.41	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data ::											
Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}	Depth (ft)	FS	m(FS)	H ₁ *m(FS)	d _z	LPI _{ISH}

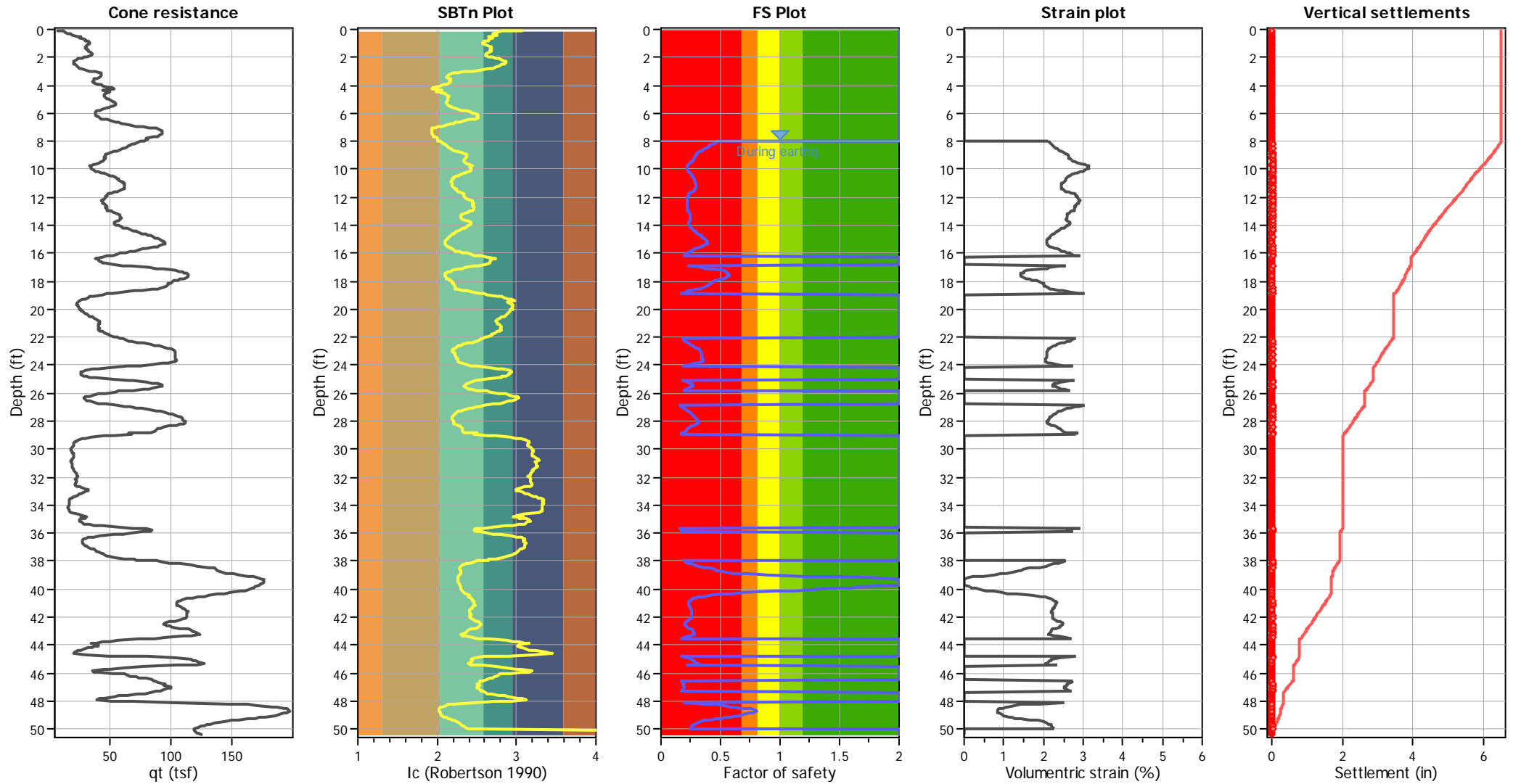
Overall liquefaction potential: 30.23

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

- FS: Calculated factor of safety for test point
- d_z: Layer thickness (ft)
- LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

- qt: Total cone resistance (cone resistance q_c corrected for pore water effects)
- I_c : Soil Behaviour Type Index
- FS: Calculated Factor of Safety against liquefaction
- Volumetric strain: Post-liquefaction volumetric strain

:: Post-earthquake settlement due to soil liquefaction ::											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
8.01	146.49	0.48	2.13	1.00	0.02	8.09	145.09	0.46	2.15	1.00	0.02
8.14	143.68	0.45	2.18	1.00	0.01	8.24	141.77	0.43	2.21	1.00	0.03
8.29	140.95	0.42	2.23	1.00	0.01	8.34	139.80	0.41	2.25	1.00	0.01
8.41	138.59	0.40	2.27	1.00	0.02	8.49	136.43	0.38	2.31	1.00	0.02
8.53	135.20	0.37	2.33	1.00	0.01	8.60	133.07	0.36	2.37	1.00	0.02
8.67	131.07	0.34	2.41	1.00	0.02	8.73	129.60	0.33	2.44	1.00	0.02
8.80	125.17	0.31	2.54	1.00	0.02	8.87	123.67	0.30	2.57	1.00	0.02
8.93	121.88	0.29	2.61	1.00	0.02	9.02	121.38	0.29	2.62	1.00	0.03
9.07	120.57	0.28	2.64	1.00	0.02	9.13	120.56	0.28	2.64	1.00	0.02
9.20	120.14	0.28	2.65	1.00	0.02	9.25	119.38	0.28	2.67	1.00	0.02
9.32	118.28	0.27	2.70	1.00	0.02	9.39	116.38	0.26	2.74	1.00	0.02
9.46	114.54	0.26	2.79	1.00	0.02	9.52	111.84	0.25	2.86	1.00	0.02
9.61	107.48	0.23	2.98	1.00	0.03	9.66	105.92	0.23	3.03	1.00	0.02
9.71	103.78	0.22	3.09	1.00	0.02	9.78	102.07	0.22	3.15	1.00	0.03
9.86	103.02	0.22	3.12	1.00	0.03	9.91	102.23	0.22	3.14	1.00	0.02
9.97	103.00	0.22	3.12	1.00	0.02	10.06	105.13	0.22	3.05	1.00	0.03
10.11	107.18	0.23	2.99	1.00	0.02	10.17	109.55	0.23	2.92	1.00	0.02
10.25	112.12	0.24	2.85	1.00	0.03	10.31	114.18	0.24	2.80	1.00	0.02
10.37	117.14	0.25	2.72	1.00	0.02	10.44	119.37	0.26	2.67	1.00	0.02
10.50	121.30	0.27	2.62	1.00	0.02	10.57	122.98	0.27	2.59	1.00	0.02
10.64	123.73	0.28	2.57	1.00	0.02	10.70	124.40	0.28	2.55	1.00	0.02
10.77	124.33	0.28	2.56	1.00	0.02	10.85	125.99	0.28	2.52	1.00	0.02
10.90	126.54	0.28	2.51	1.00	0.02	10.97	127.56	0.29	2.49	1.00	0.02
11.03	128.73	0.29	2.46	1.00	0.02	11.09	129.18	0.29	2.45	1.00	0.02
11.17	129.59	0.29	2.44	1.00	0.02	11.26	129.97	0.30	2.44	1.00	0.03
11.30	129.92	0.30	2.44	1.00	0.01	11.36	129.35	0.29	2.45	1.00	0.02
11.42	128.05	0.28	2.48	1.00	0.02	11.50	126.11	0.28	2.52	1.00	0.02
11.56	124.10	0.27	2.56	1.00	0.02	11.62	121.48	0.26	2.62	1.00	0.02
11.69	118.57	0.24	2.69	1.00	0.02	11.76	115.57	0.23	2.76	1.00	0.02
11.83	114.17	0.23	2.80	1.00	0.02	11.88	113.46	0.23	2.82	1.00	0.02
11.95	112.62	0.22	2.84	1.00	0.02	12.01	111.88	0.22	2.86	1.00	0.02
12.08	110.88	0.22	2.89	1.00	0.03	12.14	110.92	0.22	2.89	1.00	0.02
12.23	109.82	0.21	2.92	1.00	0.03	12.28	110.11	0.21	2.91	1.00	0.02
12.35	110.25	0.21	2.90	1.00	0.03	12.40	110.32	0.21	2.90	1.00	0.02
12.47	111.70	0.22	2.87	1.00	0.02	12.54	112.92	0.22	2.83	1.00	0.03
12.60	114.45	0.22	2.79	1.00	0.02	12.70	114.16	0.22	2.80	1.00	0.03
12.75	114.31	0.22	2.80	1.00	0.02	12.80	114.30	0.22	2.80	1.00	0.02
12.87	114.30	0.22	2.80	1.00	0.02	12.93	114.76	0.22	2.78	1.00	0.02
12.99	117.48	0.23	2.72	1.00	0.02	13.06	119.26	0.24	2.67	1.00	0.02
13.14	121.60	0.24	2.62	1.00	0.02	13.19	122.02	0.24	2.61	1.00	0.02
13.26	123.00	0.25	2.59	1.00	0.02	13.32	122.75	0.25	2.59	1.00	0.02
13.40	123.11	0.25	2.58	1.00	0.02	13.46	123.15	0.25	2.58	1.00	0.02
13.53	123.10	0.24	2.58	1.00	0.02	13.58	123.31	0.25	2.58	1.00	0.02
13.68	122.91	0.24	2.59	1.00	0.03	13.73	122.18	0.24	2.60	1.00	0.02
13.79	119.78	0.23	2.66	1.00	0.02	13.88	119.90	0.23	2.66	1.00	0.03
13.92	119.90	0.23	2.66	1.00	0.01	13.98	120.88	0.23	2.63	1.00	0.02
14.05	123.11	0.24	2.58	1.00	0.02	14.13	124.64	0.25	2.55	1.00	0.02
14.17	125.91	0.25	2.52	1.00	0.01	14.24	128.79	0.26	2.46	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
14.33	130.37	0.27	2.43	1.00	0.03	14.37	132.41	0.28	2.39	1.00	0.01
14.45	134.57	0.29	2.34	1.00	0.02	14.53	136.58	0.30	2.31	1.00	0.02
14.57	138.37	0.31	2.27	1.00	0.01	14.64	140.61	0.32	2.23	1.00	0.02
14.72	141.76	0.33	2.21	1.00	0.02	14.76	142.85	0.34	2.19	1.00	0.01
14.85	144.36	0.35	2.17	1.00	0.02	14.90	145.55	0.35	2.15	1.00	0.01
14.96	147.04	0.37	2.12	1.00	0.02	15.03	148.45	0.38	2.10	1.00	0.02
15.10	149.13	0.38	2.09	1.00	0.02	15.16	149.68	0.39	2.08	1.00	0.02
15.24	149.91	0.39	2.08	1.00	0.02	15.31	149.75	0.39	2.08	1.00	0.02
15.36	149.30	0.38	2.09	1.00	0.01	15.45	146.72	0.36	2.13	1.00	0.02
15.50	144.92	0.34	2.16	1.00	0.01	15.55	142.49	0.33	2.20	1.00	0.01
15.66	137.39	0.29	2.29	1.00	0.03	15.69	135.30	0.28	2.33	1.00	0.01
15.75	131.84	0.27	2.40	1.00	0.02	15.82	128.56	0.25	2.46	1.00	0.02
15.91	126.22	0.24	2.51	1.00	0.03	15.96	123.10	0.23	2.58	1.00	0.02
16.02	119.44	0.22	2.67	1.00	0.02	16.08	117.12	0.21	2.72	1.00	0.02
16.14	114.42	0.20	2.79	1.00	0.02	16.22	109.64	0.19	2.92	1.00	0.03
16.30	42.66	2.00	0.00	1.00	0.00	16.34	36.75	2.00	0.00	1.00	0.00
16.42	38.82	2.00	0.00	1.00	0.00	16.50	39.01	2.00	0.00	1.00	0.00
16.54	40.51	2.00	0.00	1.00	0.00	16.62	40.80	2.00	0.00	1.00	0.00
16.70	42.45	2.00	0.00	1.00	0.00	16.74	44.13	2.00	0.00	1.00	0.00
16.80	49.83	2.00	0.00	1.00	0.00	16.87	124.65	0.23	2.55	1.00	0.02
16.94	131.83	0.26	2.40	1.00	0.02	17.01	145.38	0.34	2.15	1.00	0.02
17.09	150.46	0.38	2.07	1.00	0.02	17.14	155.54	0.43	1.99	1.00	0.01
17.23	162.63	0.52	1.58	1.00	0.02	17.28	164.21	0.55	1.49	1.00	0.01
17.34	164.42	0.55	1.48	1.00	0.01	17.39	164.46	0.55	1.48	1.00	0.01
17.46	165.21	0.57	1.44	1.00	0.01	17.52	165.68	0.57	1.42	1.00	0.01
17.60	165.66	0.57	1.42	1.00	0.01	17.66	165.40	0.57	1.44	1.00	0.01
17.73	164.26	0.55	1.49	1.00	0.01	17.79	162.83	0.52	1.57	1.00	0.01
17.86	161.45	0.50	1.64	1.00	0.01	17.92	160.07	0.48	1.72	1.00	0.01
17.98	158.24	0.45	1.83	1.00	0.01	18.07	156.91	0.44	1.92	1.00	0.02
18.11	156.16	0.43	1.97	1.00	0.01	18.18	154.65	0.41	2.00	1.00	0.02
18.27	153.75	0.40	2.02	1.00	0.02	18.32	152.96	0.39	2.03	1.00	0.01
18.37	152.06	0.38	2.04	1.00	0.01	18.46	148.13	0.35	2.11	1.00	0.02
18.52	145.10	0.32	2.15	1.00	0.01	18.57	140.73	0.30	2.23	1.00	0.01
18.66	132.45	0.25	2.39	1.00	0.03	18.71	127.43	0.23	2.49	1.00	0.02
18.77	118.76	0.21	2.68	1.00	0.02	18.84	111.09	0.19	2.88	1.00	0.03
18.91	105.58	0.17	3.04	1.00	0.02	18.97	39.58	2.00	0.00	1.00	0.00
19.05	32.73	2.00	0.00	1.00	0.00	19.10	29.67	2.00	0.00	1.00	0.00
19.16	28.62	2.00	0.00	1.00	0.00	19.26	25.83	2.00	0.00	1.00	0.00
19.30	23.99	2.00	0.00	1.00	0.00	19.36	21.86	2.00	0.00	1.00	0.00
19.43	22.00	2.00	0.00	1.00	0.00	19.51	20.52	2.00	0.00	1.00	0.00
19.55	19.59	2.00	0.00	1.00	0.00	19.63	19.55	2.00	0.00	1.00	0.00
19.69	19.52	2.00	0.00	1.00	0.00	19.75	20.20	2.00	0.00	1.00	0.00
19.84	20.78	2.00	0.00	1.00	0.00	19.89	21.64	2.00	0.00	1.00	0.00
19.96	21.24	2.00	0.00	1.00	0.00	20.02	22.46	2.00	0.00	1.00	0.00
20.09	22.86	2.00	0.00	1.00	0.00	20.14	23.45	2.00	0.00	1.00	0.00
20.22	24.37	2.00	0.00	1.00	0.00	20.28	25.66	2.00	0.00	1.00	0.00
20.36	26.31	2.00	0.00	1.00	0.00	20.41	27.61	2.00	0.00	1.00	0.00
20.48	28.53	2.00	0.00	1.00	0.00	20.55	30.60	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
20.61	31.26	2.00	0.00	1.00	0.00	20.68	31.73	2.00	0.00	1.00	0.00
20.74	33.36	2.00	0.00	1.00	0.00	20.81	34.79	2.00	0.00	1.00	0.00
20.88	35.44	2.00	0.00	1.00	0.00	20.93	34.95	2.00	0.00	1.00	0.00
21.00	34.99	2.00	0.00	1.00	0.00	21.07	34.75	2.00	0.00	1.00	0.00
21.13	34.18	2.00	0.00	1.00	0.00	21.22	33.75	2.00	0.00	1.00	0.00
21.27	33.80	2.00	0.00	1.00	0.00	21.34	34.96	2.00	0.00	1.00	0.00
21.41	34.47	2.00	0.00	1.00	0.00	21.46	34.08	2.00	0.00	1.00	0.00
21.55	35.39	2.00	0.00	1.00	0.00	21.59	36.92	2.00	0.00	1.00	0.00
21.66	37.99	2.00	0.00	1.00	0.00	21.76	40.42	2.00	0.00	1.00	0.00
21.80	41.16	2.00	0.00	1.00	0.00	21.86	42.23	2.00	0.00	1.00	0.00
21.95	45.02	2.00	0.00	1.00	0.00	22.01	46.95	2.00	0.00	1.00	0.00
22.06	113.66	0.18	2.81	1.00	0.02	22.12	115.35	0.19	2.77	1.00	0.02
22.18	117.40	0.19	2.72	1.00	0.02	22.26	120.05	0.20	2.65	1.00	0.03
22.31	122.35	0.21	2.60	1.00	0.02	22.38	126.48	0.22	2.51	1.00	0.02
22.44	129.55	0.23	2.44	1.00	0.02	22.53	134.05	0.25	2.35	1.00	0.02
22.59	136.66	0.26	2.30	1.00	0.01	22.65	138.89	0.27	2.26	1.00	0.02
22.71	141.72	0.28	2.21	1.00	0.02	22.78	144.68	0.30	2.16	1.00	0.02
22.86	146.33	0.31	2.13	1.00	0.02	22.92	147.91	0.32	2.11	1.00	0.01
22.98	148.36	0.33	2.10	1.00	0.02	23.04	149.03	0.33	2.09	1.00	0.01
23.10	149.68	0.34	2.08	1.00	0.02	23.16	149.59	0.34	2.08	1.00	0.02
23.25	149.77	0.34	2.08	1.00	0.02	23.30	149.90	0.34	2.08	1.00	0.01
23.36	150.09	0.34	2.07	1.00	0.02	23.43	150.51	0.34	2.07	1.00	0.02
23.49	150.80	0.34	2.06	1.00	0.01	23.56	151.68	0.35	2.05	1.00	0.02
23.65	152.39	0.36	2.04	1.00	0.02	23.71	151.97	0.35	2.04	1.00	0.01
23.76	150.85	0.34	2.06	1.00	0.01	23.83	146.21	0.31	2.14	1.00	0.02
23.89	141.73	0.28	2.21	1.00	0.02	23.95	133.88	0.24	2.36	1.00	0.02
24.02	125.27	0.21	2.53	1.00	0.02	24.09	116.14	0.19	2.75	1.00	0.02
24.15	40.66	2.00	0.00	1.00	0.00	24.24	31.89	2.00	0.00	1.00	0.00
24.29	27.92	2.00	0.00	1.00	0.00	24.35	23.50	2.00	0.00	1.00	0.00
24.42	21.28	2.00	0.00	1.00	0.00	24.49	20.36	2.00	0.00	1.00	0.00
24.54	19.85	2.00	0.00	1.00	0.00	24.62	20.21	2.00	0.00	1.00	0.00
24.69	20.10	2.00	0.00	1.00	0.00	24.75	21.44	2.00	0.00	1.00	0.00
24.81	23.90	2.00	0.00	1.00	0.00	24.88	26.03	2.00	0.00	1.00	0.00
24.94	29.31	2.00	0.00	1.00	0.00	25.00	40.35	2.00	0.00	1.00	0.00
25.07	115.19	0.18	2.77	1.00	0.02	25.13	118.47	0.19	2.69	1.00	0.02
25.22	129.03	0.22	2.45	1.00	0.03	25.27	133.84	0.24	2.36	1.00	0.01
25.33	137.64	0.26	2.29	1.00	0.02	25.40	140.76	0.27	2.23	1.00	0.02
25.48	139.76	0.27	2.25	1.00	0.02	25.53	137.58	0.25	2.29	1.00	0.01
25.60	132.86	0.23	2.38	1.00	0.02	25.67	130.03	0.22	2.43	1.00	0.02
25.73	125.94	0.21	2.52	1.00	0.02	25.79	118.85	0.19	2.68	1.00	0.02
25.87	44.15	2.00	0.00	1.00	0.00	25.92	42.15	2.00	0.00	1.00	0.00
26.00	35.15	2.00	0.00	1.00	0.00	26.07	30.85	2.00	0.00	1.00	0.00
26.12	28.05	2.00	0.00	1.00	0.00	26.19	24.77	2.00	0.00	1.00	0.00
26.25	22.23	2.00	0.00	1.00	0.00	26.33	20.79	2.00	0.00	1.00	0.00
26.39	20.76	2.00	0.00	1.00	0.00	26.45	21.59	2.00	0.00	1.00	0.00
26.52	22.96	2.00	0.00	1.00	0.00	26.58	24.64	2.00	0.00	1.00	0.00
26.66	27.80	2.00	0.00	1.00	0.00	26.72	30.59	2.00	0.00	1.00	0.00
26.78	34.59	2.00	0.00	1.00	0.00	26.84	105.67	0.16	3.04	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
26.91	110.71	0.17	2.89	1.00	0.03	26.97	113.96	0.18	2.81	1.00	0.02
27.05	118.66	0.19	2.69	1.00	0.02	27.10	122.33	0.20	2.60	1.00	0.02
27.17	126.53	0.21	2.51	1.00	0.02	27.24	129.99	0.22	2.43	1.00	0.02
27.30	132.23	0.23	2.39	1.00	0.02	27.37	134.65	0.24	2.34	1.00	0.02
27.46	137.42	0.25	2.29	1.00	0.03	27.51	139.00	0.26	2.26	1.00	0.01
27.57	140.96	0.27	2.23	1.00	0.01	27.64	143.05	0.28	2.19	1.00	0.02
27.70	144.18	0.29	2.17	1.00	0.01	27.76	144.78	0.29	2.16	1.00	0.02
27.82	145.79	0.30	2.14	1.00	0.02	27.91	146.62	0.30	2.13	1.00	0.02
27.96	147.46	0.31	2.12	1.00	0.01	28.03	148.37	0.31	2.10	1.00	0.02
28.09	148.38	0.31	2.10	1.00	0.02	28.16	147.99	0.31	2.11	1.00	0.02
28.23	145.95	0.30	2.14	1.00	0.02	28.29	143.52	0.28	2.18	1.00	0.02
28.36	139.28	0.26	2.26	1.00	0.02	28.45	135.57	0.24	2.32	1.00	0.03
28.48	133.09	0.23	2.37	1.00	0.01	28.55	130.77	0.22	2.42	1.00	0.02
28.61	128.77	0.21	2.46	1.00	0.02	28.68	127.99	0.21	2.48	1.00	0.02
28.74	127.25	0.21	2.49	1.00	0.02	28.81	124.33	0.20	2.56	1.00	0.02
28.87	111.48	0.17	2.87	1.00	0.02	28.94	113.38	0.17	2.82	1.00	0.02
29.03	39.14	2.00	0.00	1.00	0.00	29.08	32.38	2.00	0.00	1.00	0.00
29.16	24.59	2.00	0.00	1.00	0.00	29.22	21.13	2.00	0.00	1.00	0.00
29.27	18.68	2.00	0.00	1.00	0.00	29.35	16.01	2.00	0.00	1.00	0.00
29.43	15.27	2.00	0.00	1.00	0.00	29.47	14.53	2.00	0.00	1.00	0.00
29.53	13.87	2.00	0.00	1.00	0.00	29.60	13.64	2.00	0.00	1.00	0.00
29.67	13.69	2.00	0.00	1.00	0.00	29.73	13.75	2.00	0.00	1.00	0.00
29.80	13.36	2.00	0.00	1.00	0.00	29.87	12.71	2.00	0.00	1.00	0.00
29.93	12.34	2.00	0.00	1.00	0.00	30.00	12.25	2.00	0.00	1.00	0.00
30.07	12.17	2.00	0.00	1.00	0.00	30.12	12.15	2.00	0.00	1.00	0.00
30.20	12.49	2.00	0.00	1.00	0.00	30.27	12.89	2.00	0.00	1.00	0.00
30.32	13.16	2.00	0.00	1.00	0.00	30.40	13.72	2.00	0.00	1.00	0.00
30.46	13.84	2.00	0.00	1.00	0.00	30.52	13.55	2.00	0.00	1.00	0.00
30.59	13.46	2.00	0.00	1.00	0.00	30.65	12.80	2.00	0.00	1.00	0.00
30.71	12.58	2.00	0.00	1.00	0.00	30.79	12.21	2.00	0.00	1.00	0.00
30.85	12.13	2.00	0.00	1.00	0.00	30.96	12.04	2.00	0.00	1.00	0.00
31.00	12.30	2.00	0.00	1.00	0.00	31.04	12.43	2.00	0.00	1.00	0.00
31.11	12.63	2.00	0.00	1.00	0.00	31.18	12.54	2.00	0.00	1.00	0.00
31.25	12.39	2.00	0.00	1.00	0.00	31.30	12.58	2.00	0.00	1.00	0.00
31.38	13.20	2.00	0.00	1.00	0.00	31.44	13.21	2.00	0.00	1.00	0.00
31.50	13.37	2.00	0.00	1.00	0.00	31.57	13.22	2.00	0.00	1.00	0.00
31.63	14.03	2.00	0.00	1.00	0.00	31.70	14.51	2.00	0.00	1.00	0.00
31.79	14.69	2.00	0.00	1.00	0.00	31.83	15.06	2.00	0.00	1.00	0.00
31.90	15.64	2.00	0.00	1.00	0.00	31.97	15.48	2.00	0.00	1.00	0.00
32.03	14.70	2.00	0.00	1.00	0.00	32.10	14.40	2.00	0.00	1.00	0.00
32.16	14.32	2.00	0.00	1.00	0.00	32.23	14.37	2.00	0.00	1.00	0.00
32.30	14.42	2.00	0.00	1.00	0.00	32.36	14.34	2.00	0.00	1.00	0.00
32.46	13.83	2.00	0.00	1.00	0.00	32.51	13.82	2.00	0.00	1.00	0.00
32.56	14.15	2.00	0.00	1.00	0.00	32.65	14.47	2.00	0.00	1.00	0.00
32.68	16.46	2.00	0.00	1.00	0.00	32.76	18.04	2.00	0.00	1.00	0.00
32.84	20.53	2.00	0.00	1.00	0.00	32.89	20.93	2.00	0.00	1.00	0.00
32.95	21.12	2.00	0.00	1.00	0.00	33.01	20.40	2.00	0.00	1.00	0.00
33.10	18.27	2.00	0.00	1.00	0.00	33.15	17.15	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
33.24	16.10	2.00	0.00	1.00	0.00	33.29	14.99	2.00	0.00	1.00	0.00
33.35	13.48	2.00	0.00	1.00	0.00	33.40	12.66	2.00	0.00	1.00	0.00
33.47	12.17	2.00	0.00	1.00	0.00	33.55	11.29	2.00	0.00	1.00	0.00
33.65	10.54	2.00	0.00	1.00	0.00	33.66	10.40	2.00	0.00	1.00	0.00
33.74	10.32	2.00	0.00	1.00	0.00	33.84	10.04	2.00	0.00	1.00	0.00
33.88	10.04	2.00	0.00	1.00	0.00	33.93	10.03	2.00	0.00	1.00	0.00
33.99	10.02	2.00	0.00	1.00	0.00	34.07	9.87	2.00	0.00	1.00	0.00
34.12	9.86	2.00	0.00	1.00	0.00	34.19	9.85	2.00	0.00	1.00	0.00
34.28	10.03	2.00	0.00	1.00	0.00	34.32	10.09	2.00	0.00	1.00	0.00
34.40	10.34	2.00	0.00	1.00	0.00	34.48	10.52	2.00	0.00	1.00	0.00
34.52	10.65	2.00	0.00	1.00	0.00	34.58	11.23	2.00	0.00	1.00	0.00
34.68	14.58	2.00	0.00	1.00	0.00	34.72	17.12	2.00	0.00	1.00	0.00
34.81	20.01	2.00	0.00	1.00	0.00	34.85	16.68	2.00	0.00	1.00	0.00
34.92	18.82	2.00	0.00	1.00	0.00	34.98	16.65	2.00	0.00	1.00	0.00
35.05	15.96	2.00	0.00	1.00	0.00	35.12	15.54	2.00	0.00	1.00	0.00
35.18	16.26	2.00	0.00	1.00	0.00	35.26	16.97	2.00	0.00	1.00	0.00
35.31	17.76	2.00	0.00	1.00	0.00	35.41	20.84	2.00	0.00	1.00	0.00
35.47	23.76	2.00	0.00	1.00	0.00	35.51	28.35	2.00	0.00	1.00	0.00
35.58	37.65	2.00	0.00	1.00	0.00	35.63	109.66	0.16	2.92	1.00	0.02
35.71	117.72	0.18	2.71	1.00	0.03	35.78	121.71	0.19	2.62	1.00	0.02
35.84	120.75	0.18	2.64	1.00	0.02	35.90	116.45	0.17	2.74	1.00	0.02
35.98	44.91	2.00	0.00	1.00	0.00	36.05	39.95	2.00	0.00	1.00	0.00
36.10	34.78	2.00	0.00	1.00	0.00	36.20	26.27	2.00	0.00	1.00	0.00
36.25	23.59	2.00	0.00	1.00	0.00	36.30	20.06	2.00	0.00	1.00	0.00
36.35	18.72	2.00	0.00	1.00	0.00	36.45	17.30	2.00	0.00	1.00	0.00
36.48	17.10	2.00	0.00	1.00	0.00	36.55	17.01	2.00	0.00	1.00	0.00
36.63	17.09	2.00	0.00	1.00	0.00	36.69	16.71	2.00	0.00	1.00	0.00
36.75	17.09	2.00	0.00	1.00	0.00	36.84	17.72	2.00	0.00	1.00	0.00
36.89	18.30	2.00	0.00	1.00	0.00	36.95	18.74	2.00	0.00	1.00	0.00
37.05	20.03	2.00	0.00	1.00	0.00	37.08	21.28	2.00	0.00	1.00	0.00
37.14	22.60	2.00	0.00	1.00	0.00	37.23	24.04	2.00	0.00	1.00	0.00
37.28	24.76	2.00	0.00	1.00	0.00	37.34	25.29	2.00	0.00	1.00	0.00
37.43	26.67	2.00	0.00	1.00	0.00	37.48	27.47	2.00	0.00	1.00	0.00
37.53	28.33	2.00	0.00	1.00	0.00	37.61	30.25	2.00	0.00	1.00	0.00
37.67	31.05	2.00	0.00	1.00	0.00	37.73	34.04	2.00	0.00	1.00	0.00
37.82	39.52	2.00	0.00	1.00	0.00	37.88	45.22	2.00	0.00	1.00	0.00
37.93	45.97	2.00	0.00	1.00	0.00	38.00	124.02	0.19	2.56	1.00	0.02
38.08	127.98	0.20	2.48	1.00	0.02	38.12	132.19	0.22	2.39	1.00	0.01
38.20	138.22	0.24	2.28	1.00	0.02	38.29	144.97	0.28	2.16	1.00	0.02
38.33	148.62	0.30	2.10	1.00	0.01	38.43	157.11	0.37	1.90	1.00	0.02
38.48	159.61	0.39	1.75	1.00	0.01	38.52	161.71	0.42	1.63	1.00	0.01
38.59	163.98	0.45	1.51	1.00	0.01	38.68	165.42	0.47	1.43	1.00	0.01
38.72	166.59	0.49	1.38	1.00	0.01	38.79	169.61	0.54	1.24	1.00	0.01
38.87	173.57	0.61	1.08	1.00	0.01	38.92	178.16	0.73	0.92	1.00	0.01
38.98	183.07	0.89	0.77	1.00	0.00	39.05	189.72	1.20	0.48	1.00	0.00
39.12	194.52	1.51	0.24	1.00	0.00	39.17	198.13	1.83	0.07	1.00	0.00
39.26	201.38	2.00	0.00	1.00	0.00	39.32	202.41	2.00	0.00	1.00	0.00
39.37	202.92	2.00	0.00	1.00	0.00	39.46	203.04	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
39.52	203.02	2.00	0.00	1.00	0.00	39.57	202.02	2.00	0.00	1.00	0.00
39.63	200.91	2.00	0.00	1.00	0.00	39.72	199.98	2.00	0.00	1.00	0.00
39.77	199.41	1.95	0.02	1.00	0.00	39.85	196.81	1.70	0.13	1.00	0.00
39.91	195.42	1.58	0.20	1.00	0.00	39.96	193.45	1.43	0.29	1.00	0.00
40.06	191.12	1.28	0.41	1.00	0.00	40.11	188.40	1.12	0.55	1.00	0.00
40.16	184.98	0.97	0.71	1.00	0.00	40.26	176.89	0.69	0.96	1.00	0.01
40.30	173.00	0.60	1.10	1.00	0.01	40.36	167.56	0.50	1.33	1.00	0.01
40.44	160.24	0.40	1.71	1.00	0.02	40.50	156.83	0.36	1.92	1.00	0.01
40.55	151.60	0.32	2.05	1.00	0.01	40.62	147.55	0.29	2.11	1.00	0.02
40.68	143.94	0.27	2.17	1.00	0.02	40.75	140.23	0.25	2.24	1.00	0.02
40.84	137.93	0.24	2.28	1.00	0.02	40.90	136.92	0.24	2.30	1.00	0.02
40.96	135.57	0.23	2.32	1.00	0.02	41.04	135.92	0.23	2.32	1.00	0.02
41.09	135.78	0.23	2.32	1.00	0.01	41.15	135.89	0.23	2.32	1.00	0.02
41.22	137.00	0.24	2.30	1.00	0.02	41.30	138.26	0.24	2.27	1.00	0.02
41.35	139.29	0.25	2.26	1.00	0.01	41.41	140.06	0.25	2.24	1.00	0.02
41.48	141.15	0.25	2.22	1.00	0.02	41.55	141.84	0.26	2.21	1.00	0.02
41.62	142.27	0.26	2.20	1.00	0.02	41.68	141.95	0.26	2.21	1.00	0.02
41.74	141.39	0.26	2.22	1.00	0.02	41.80	141.07	0.25	2.22	1.00	0.02
41.88	141.00	0.25	2.23	1.00	0.02	41.95	141.31	0.26	2.22	1.00	0.02
42.00	141.48	0.26	2.22	1.00	0.01	42.08	140.78	0.25	2.23	1.00	0.02
42.15	139.70	0.25	2.25	1.00	0.02	42.22	137.06	0.24	2.30	1.00	0.02
42.28	134.12	0.22	2.35	1.00	0.02	42.34	130.23	0.21	2.43	1.00	0.02
42.39	127.91	0.20	2.48	1.00	0.01	42.48	126.95	0.20	2.50	1.00	0.03
42.53	127.21	0.20	2.49	1.00	0.02	42.59	128.58	0.21	2.46	1.00	0.02
42.68	130.45	0.21	2.43	1.00	0.03	42.72	131.73	0.22	2.40	1.00	0.01
42.79	136.04	0.23	2.32	1.00	0.02	42.87	141.49	0.26	2.22	1.00	0.02
42.92	143.17	0.27	2.19	1.00	0.01	43.00	143.49	0.27	2.18	1.00	0.02
43.05	143.79	0.27	2.18	1.00	0.01	43.13	145.97	0.28	2.14	1.00	0.02
43.22	146.29	0.28	2.14	1.00	0.02	43.27	144.21	0.27	2.17	1.00	0.01
43.33	139.42	0.25	2.25	1.00	0.02	43.37	135.39	0.23	2.33	1.00	0.01
43.47	123.78	0.19	2.57	1.00	0.03	43.52	117.80	0.18	2.71	1.00	0.02
43.57	44.41	2.00	0.00	1.00	0.00	43.66	32.52	2.00	0.00	1.00	0.00
43.72	28.78	2.00	0.00	1.00	0.00	43.77	24.78	2.00	0.00	1.00	0.00
43.83	22.03	2.00	0.00	1.00	0.00	43.90	19.20	2.00	0.00	1.00	0.00
43.97	23.04	2.00	0.00	1.00	0.00	44.03	22.84	2.00	0.00	1.00	0.00
44.13	20.96	2.00	0.00	1.00	0.00	44.17	19.56	2.00	0.00	1.00	0.00
44.23	17.68	2.00	0.00	1.00	0.00	44.33	15.46	2.00	0.00	1.00	0.00
44.37	14.45	2.00	0.00	1.00	0.00	44.43	12.81	2.00	0.00	1.00	0.00
44.52	11.24	2.00	0.00	1.00	0.00	44.57	10.55	2.00	0.00	1.00	0.00
44.62	10.66	2.00	0.00	1.00	0.00	44.72	16.44	2.00	0.00	1.00	0.00
44.76	27.50	2.00	0.00	1.00	0.00	44.83	113.78	0.17	2.81	1.00	0.02
44.92	131.45	0.21	2.41	1.00	0.03	44.97	140.85	0.25	2.23	1.00	0.01
45.02	142.55	0.26	2.20	1.00	0.01	45.09	143.47	0.27	2.18	1.00	0.02
45.16	145.02	0.28	2.16	1.00	0.02	45.22	146.81	0.29	2.13	1.00	0.01
45.29	150.37	0.31	2.07	1.00	0.02	45.37	150.76	0.31	2.06	1.00	0.02
45.41	146.17	0.28	2.14	1.00	0.01	45.47	133.88	0.22	2.36	1.00	0.02
45.56	46.15	2.00	0.00	1.00	0.00	45.62	36.12	2.00	0.00	1.00	0.00
45.70	27.94	2.00	0.00	1.00	0.00	45.75	25.13	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)											
Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)	Depth (ft)	q _{c1N,cs}	FS	e _v (%)	DF	Settlement (in)
45.81	19.55	2.00	0.00	1.00	0.00	45.90	20.18	2.00	0.00	1.00	0.00
45.95	23.30	2.00	0.00	1.00	0.00	46.01	29.36	2.00	0.00	1.00	0.00
46.10	35.67	2.00	0.00	1.00	0.00	46.15	37.03	2.00	0.00	1.00	0.00
46.21	38.66	2.00	0.00	1.00	0.00	46.29	41.51	2.00	0.00	1.00	0.00
46.33	42.87	2.00	0.00	1.00	0.00	46.41	46.99	2.00	0.00	1.00	0.00
46.47	49.90	2.00	0.00	1.00	0.00	46.53	115.84	0.17	2.76	1.00	0.02
46.59	116.08	0.17	2.75	1.00	0.02	46.66	118.25	0.18	2.70	1.00	0.02
46.75	121.80	0.19	2.61	1.00	0.03	46.79	122.95	0.19	2.59	1.00	0.01
46.85	122.33	0.19	2.60	1.00	0.02	46.92	122.53	0.19	2.60	1.00	0.02
47.00	126.42	0.20	2.51	1.00	0.02	47.05	126.25	0.20	2.51	1.00	0.02
47.12	124.89	0.19	2.54	1.00	0.02	47.20	122.41	0.19	2.60	1.00	0.02
47.26	119.87	0.18	2.66	1.00	0.02	47.32	117.42	0.18	2.72	1.00	0.02
47.39	48.77	2.00	0.00	1.00	0.00	47.47	45.50	2.00	0.00	1.00	0.00
47.51	41.72	2.00	0.00	1.00	0.00	47.59	36.15	2.00	0.00	1.00	0.00
47.65	32.16	2.00	0.00	1.00	0.00	47.71	29.85	2.00	0.00	1.00	0.00
47.79	24.49	2.00	0.00	1.00	0.00	47.85	22.80	2.00	0.00	1.00	0.00
47.91	21.07	2.00	0.00	1.00	0.00	48.00	28.17	2.00	0.00	1.00	0.00
48.05	38.96	2.00	0.00	1.00	0.00	48.10	125.84	0.20	2.52	1.00	0.02
48.19	157.30	0.37	1.89	1.00	0.02	48.25	165.67	0.47	1.42	1.00	0.01
48.30	169.08	0.52	1.26	1.00	0.01	48.39	172.86	0.59	1.11	1.00	0.01
48.43	173.61	0.61	1.08	1.00	0.01	48.50	176.32	0.67	0.98	1.00	0.01
48.59	179.56	0.76	0.87	1.00	0.01	48.64	180.62	0.79	0.84	1.00	0.01
48.70	181.08	0.81	0.82	1.00	0.01	48.79	180.64	0.79	0.84	1.00	0.01
48.83	180.20	0.78	0.85	1.00	0.00	48.89	178.98	0.74	0.89	1.00	0.01
48.95	177.34	0.70	0.94	1.00	0.01	49.02	175.66	0.65	1.00	1.00	0.01
49.11	172.23	0.58	1.13	1.00	0.01	49.19	170.07	0.54	1.22	1.00	0.01
49.22	168.37	0.51	1.29	1.00	0.01	49.28	165.50	0.46	1.43	1.00	0.01
49.35	161.28	0.41	1.65	1.00	0.01	49.42	157.44	0.37	1.88	1.00	0.01
49.48	153.60	0.33	2.02	1.00	0.02	49.56	149.18	0.30	2.09	1.00	0.02
49.63	146.78	0.29	2.13	1.00	0.02	49.68	143.54	0.27	2.18	1.00	0.01
49.74	142.81	0.26	2.19	1.00	0.02	49.83	141.80	0.26	2.21	1.00	0.02
49.87	140.30	0.25	2.24	1.00	0.01	49.97	138.02	0.24	2.28	1.00	0.03
50.03	138.22	2.00	0.00	1.00	0.00	50.08	72.59	2.00	0.00	1.00	0.00
50.14	73.01	2.00	0.00	1.00	0.00	50.23	73.70	2.00	0.00	1.00	0.00
50.27	74.28	2.00	0.00	1.00	0.00	50.33	75.14	2.00	0.00	1.00	0.00
50.41	76.75	2.00	0.00	1.00	0.00						

Total estimated settlement: 6.51

Abbreviations

- Q_{tn,cs}: Equivalent clean sand normalized cone resistance
- FS: Factor of safety against liquefaction
- e_v (%): Post-liquefaction volumetric strain
- DF: e_v depth weighting factor
- Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
0.10	6.64	10.66	10.08	107.45	3.07	0.08	94.24
0.14	11.06	17.76	5.98	106.28	2.81	0.08	0.62
0.21	13.17	21.15	5.26	111.22	2.75	0.09	0.62
0.26	15.48	24.86	4.78	118.72	2.71	0.09	0.62
0.34	17.50	28.09	4.91	138.07	2.72	0.10	0.62
0.40	18.00	28.89	5.28	152.48	2.75	0.10	0.62
0.49	23.33	37.44	4.30	161.07	2.66	0.11	0.62
0.53	25.33	40.66	4.16	169.33	2.65	0.11	0.62
0.59	24.62	39.50	4.67	184.56	2.70	0.11	0.62
0.66	25.93	41.60	4.62	192.29	2.69	0.12	0.62
0.73	28.75	46.13	4.16	191.85	2.65	0.12	0.62
0.81	29.55	47.40	4.09	193.86	2.64	0.12	0.62
0.87	31.56	50.63	3.71	187.76	2.59	0.13	0.78
0.92	32.87	52.73	3.52	185.66	2.57	0.13	0.78
0.99	33.07	53.04	3.52	186.80	2.57	0.13	0.78
1.05	32.16	51.58	3.67	189.24	2.59	0.13	0.78
1.15	30.96	49.64	4.00	198.74	2.63	0.13	0.62
1.20	29.95	48.01	4.29	205.74	2.66	0.12	0.62
1.26	29.55	47.36	4.47	211.57	2.68	0.12	0.62
1.32	29.55	47.36	4.60	217.79	2.69	0.12	0.62
1.39	30.15	48.31	4.60	222.01	2.69	0.13	0.62
1.46	31.76	50.89	4.38	222.88	2.67	0.13	0.63
1.51	32.06	51.37	4.40	225.93	2.67	0.13	0.63
1.58	31.97	51.21	4.47	228.75	2.68	0.13	0.63
1.66	33.58	53.79	4.13	221.93	2.64	0.13	0.64
1.71	34.89	55.88	3.85	215.13	2.61	0.14	0.64
1.79	34.79	55.72	3.76	209.75	2.60	0.14	0.64
1.84	33.58	53.77	3.91	210.36	2.62	0.13	0.64
1.93	31.06	49.72	4.25	211.34	2.65	0.13	0.63
1.98	28.44	45.51	4.72	214.61	2.70	0.12	0.62
2.04	26.33	42.11	5.09	214.41	2.74	0.12	0.62
2.11	23.82	38.07	5.52	210.23	2.77	0.11	0.62
2.17	21.62	34.52	6.04	208.54	2.81	0.11	0.62
2.24	20.30	32.41	6.38	206.81	2.84	0.11	0.62
2.32	19.61	31.28	6.61	206.77	2.86	0.10	0.62
2.38	19.41	30.95	6.70	207.36	2.86	0.10	0.62
2.43	20.11	32.07	6.40	205.35	2.84	0.11	0.62
2.52	21.42	34.17	5.97	203.83	2.81	0.11	0.62
2.56	22.22	35.45	5.69	201.73	2.79	0.11	0.62
2.64	23.53	37.55	5.20	195.25	2.75	0.11	0.62
2.69	23.73	37.86	5.06	191.66	2.73	0.11	0.62
2.78	24.23	38.66	4.75	183.73	2.70	0.11	0.62
2.83	26.14	41.72	4.17	174.16	2.65	0.11	0.62
2.89	29.66	47.37	3.33	157.78	2.55	0.12	0.77
2.95	33.08	52.86	2.68	141.56	2.45	0.12	0.78
3.02	37.40	59.79	2.09	124.80	2.34	0.13	0.79
3.09	40.62	64.96	1.76	114.65	2.25	0.13	0.79
3.15	41.83	66.90	1.61	108.04	2.20	0.13	0.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
3.22	42.33	67.69	1.51	102.33	2.15	0.12	0.79
3.29	42.73	68.33	1.47	100.32	2.13	0.12	0.79
3.35	41.93	67.04	1.46	97.91	2.13	0.12	0.78
3.41	41.02	65.57	1.46	95.45	2.12	0.12	0.78
3.52	38.51	61.53	1.50	92.22	2.15	0.11	0.77
3.55	36.90	58.94	1.55	91.15	2.17	0.11	0.77
3.61	36.10	57.65	1.55	89.31	2.17	0.11	0.77
3.71	36.85	58.84	1.52	89.15	2.16	0.11	0.77
3.75	35.39	56.49	1.56	88.28	2.18	0.11	0.77
3.81	36.80	58.75	1.52	89.20	2.16	0.11	0.77
3.90	40.02	63.92	1.45	93.00	2.12	0.11	0.78
3.95	42.53	67.95	1.40	95.05	2.09	0.12	0.78
4.01	44.04	70.37	1.34	94.63	2.04	0.11	0.78
4.09	47.96	76.66	1.29	98.71	1.98	0.12	0.77
4.15	50.57	80.85	1.27	102.83	1.95	0.12	0.77
4.21	52.79	84.41	1.26	106.35	1.93	0.12	0.77
4.29	53.49	85.53	1.26	107.81	1.94	0.13	0.78
4.34	43.54	69.54	1.38	95.65	2.07	0.12	0.78
4.41	49.97	79.87	1.30	103.93	1.99	0.12	0.78
4.46	48.98	78.26	1.32	103.55	2.02	0.12	0.79
4.55	47.56	75.99	1.37	103.96	2.06	0.13	0.79
4.61	46.45	74.20	1.40	104.14	2.09	0.13	0.79
4.67	45.25	72.27	1.44	104.25	2.12	0.13	0.79
4.75	44.54	71.12	1.48	105.34	2.14	0.13	0.79
4.79	44.54	71.11	1.49	106.20	2.14	0.13	0.79
4.87	45.75	73.05	1.49	108.89	2.14	0.13	0.80
4.93	47.06	75.15	1.48	111.38	2.14	0.14	0.80
4.99	48.46	77.39	1.47	113.88	2.13	0.14	0.80
5.06	50.37	80.45	1.46	117.45	2.13	0.14	0.81
5.14	51.88	82.87	1.46	120.69	2.12	0.15	0.81
5.19	52.69	84.17	1.45	122.45	2.12	0.15	0.81
5.25	54.39	86.89	1.44	124.87	2.11	0.15	0.81
5.33	54.70	87.39	1.45	126.63	2.12	0.15	0.82
5.38	54.40	86.88	1.47	127.86	2.13	0.15	0.82
5.45	52.38	83.65	1.52	127.36	2.16	0.15	0.81
5.52	50.57	80.73	1.55	125.31	2.17	0.15	0.81
5.59	48.46	77.33	1.59	123.33	2.19	0.14	0.81
5.64	46.75	74.58	1.65	123.16	2.21	0.14	0.80
5.72	43.74	69.74	1.77	123.55	2.26	0.14	0.80
5.78	41.22	65.68	1.93	126.80	2.30	0.13	0.79
5.85	38.41	61.16	2.24	136.98	2.37	0.13	0.79
5.92	37.10	59.05	2.48	146.51	2.42	0.13	0.79
5.98	37.15	59.13	2.59	153.33	2.44	0.13	0.79
6.04	37.15	59.12	2.80	165.69	2.47	0.13	0.79
6.11	37.21	59.20	3.05	180.29	2.51	0.13	0.79
6.17	39.21	62.42	2.98	186.07	2.50	0.14	0.79
6.24	40.12	63.87	3.01	192.12	2.50	0.14	0.79
6.32	40.83	64.99	3.05	198.28	2.51	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
6.38	42.54	67.73	2.88	195.06	2.49	0.14	0.80
6.44	46.76	74.51	2.45	182.48	2.41	0.15	0.81
6.51	50.99	81.29	2.05	167.01	2.33	0.15	0.81
6.58	54.20	86.45	1.85	159.80	2.28	0.16	0.82
6.66	57.22	91.29	1.69	154.70	2.23	0.16	0.82
6.71	58.73	93.71	1.61	151.20	2.20	0.16	0.82
6.77	60.44	96.45	1.54	148.52	2.17	0.16	0.82
6.83	65.67	104.85	1.43	149.92	2.11	0.16	0.82
6.92	70.69	112.91	1.36	153.51	2.05	0.17	0.83
6.97	77.13	123.25	1.31	161.38	2.00	0.18	0.83
7.03	82.16	131.32	1.28	168.73	1.97	0.19	0.83
7.10	87.99	140.68	1.26	177.88	1.94	0.20	0.83
7.16	90.20	144.23	1.26	182.21	1.94	0.21	0.84
7.22	92.01	147.13	1.26	185.46	1.94	0.22	0.84
7.31	93.01	148.73	1.26	187.49	1.94	0.22	0.84
7.36	93.01	148.72	1.26	187.81	1.94	0.22	0.84
7.42	93.01	148.72	1.26	187.56	1.94	0.22	0.84
7.49	91.91	146.08	1.26	184.16	1.94	0.21	0.83
7.55	90.40	143.32	1.27	181.38	1.94	0.20	0.83
7.62	89.09	140.81	1.27	178.94	1.95	0.20	0.83
7.71	85.78	135.33	1.28	173.83	1.97	0.19	0.83
7.75	79.34	126.44	1.32	166.75	2.01	0.18	0.83
7.83	80.85	127.33	1.31	166.17	2.00	0.18	0.83
7.88	79.74	125.34	1.31	164.20	2.00	0.17	0.83
7.95	77.83	121.97	1.32	160.70	2.01	0.17	0.82
8.01	74.01	116.50	1.35	157.20	2.04	0.16	0.82
8.09	71.80	112.89	1.37	154.63	2.06	0.16	0.82
8.14	69.69	109.62	1.39	152.54	2.08	0.16	0.82
8.24	67.17	105.50	1.42	150.11	2.10	0.15	0.82
8.29	66.27	103.89	1.43	149.06	2.11	0.15	0.81
8.34	64.96	101.72	1.45	147.83	2.12	0.15	0.81
8.41	63.66	99.45	1.47	146.61	2.13	0.15	0.81
8.49	61.34	95.72	1.51	144.86	2.15	0.14	0.81
8.53	60.04	93.64	1.54	144.13	2.17	0.14	0.81
8.60	57.52	89.86	1.60	144.08	2.20	0.14	0.80
8.67	55.51	86.73	1.66	143.92	2.22	0.14	0.80
8.73	53.70	84.11	1.74	146.62	2.25	0.14	0.80
8.80	48.98	77.61	1.99	154.25	2.32	0.13	0.79
8.87	47.36	75.23	2.14	160.92	2.35	0.13	0.79
8.93	45.85	72.81	2.24	163.26	2.37	0.13	0.79
9.02	45.75	72.12	2.24	161.42	2.37	0.13	0.79
9.07	45.25	71.05	2.26	160.59	2.38	0.13	0.78
9.13	45.45	70.98	2.24	158.85	2.37	0.13	0.78
9.20	45.55	70.49	2.19	154.14	2.36	0.13	0.78
9.25	45.36	69.71	2.14	149.34	2.35	0.12	0.78
9.32	44.95	68.54	2.10	144.18	2.34	0.12	0.78
9.39	43.85	66.42	2.10	139.25	2.34	0.12	0.78
9.46	42.74	64.38	2.10	135.02	2.34	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
9.52	40.83	61.30	2.15	131.50	2.35	0.12	0.77
9.61	37.41	56.16	2.31	129.95	2.39	0.11	0.76
9.66	36.21	54.27	2.39	129.86	2.40	0.11	0.76
9.71	34.50	51.74	2.52	130.46	2.43	0.11	0.76
9.78	33.29	49.77	2.60	129.33	2.44	0.11	0.75
9.86	34.45	50.93	2.45	124.87	2.41	0.11	0.75
9.91	33.84	49.90	2.51	125.38	2.43	0.11	0.75
9.97	34.39	50.54	2.53	128.11	2.43	0.11	0.75
10.06	36.00	52.53	2.51	132.11	2.43	0.11	0.76
10.11	37.81	54.76	2.40	131.59	2.41	0.11	0.76
10.17	39.92	57.31	2.29	131.49	2.38	0.11	0.77
10.25	42.33	60.15	2.17	130.65	2.36	0.12	0.77
10.31	44.34	62.49	2.07	129.66	2.34	0.12	0.77
10.37	47.46	66.13	1.92	127.17	2.30	0.12	0.78
10.44	50.07	69.05	1.81	124.99	2.27	0.12	0.78
10.50	52.38	71.60	1.73	123.89	2.24	0.12	0.78
10.57	54.71	74.06	1.66	122.59	2.22	0.13	0.79
10.64	55.91	75.15	1.62	121.93	2.20	0.13	0.79
10.70	56.82	76.00	1.61	122.00	2.20	0.13	0.79
10.77	57.02	75.86	1.60	121.47	2.19	0.13	0.79
10.85	59.13	78.08	1.56	122.07	2.18	0.13	0.79
10.90	59.83	78.70	1.56	122.40	2.17	0.13	0.79
10.97	60.54	79.34	1.57	124.29	2.18	0.13	0.79
11.03	61.54	80.36	1.57	125.98	2.18	0.13	0.80
11.09	61.75	80.39	1.58	127.23	2.19	0.13	0.80
11.17	61.95	80.35	1.60	128.46	2.19	0.13	0.80
11.26	61.95	80.03	1.63	130.36	2.21	0.14	0.80
11.30	61.85	79.77	1.64	130.70	2.21	0.14	0.80
11.36	61.14	78.69	1.67	131.14	2.22	0.13	0.80
11.42	59.73	76.71	1.71	131.26	2.24	0.13	0.80
11.50	57.92	74.19	1.76	130.34	2.25	0.13	0.79
11.56	56.11	71.71	1.80	129.13	2.26	0.13	0.79
11.62	53.60	68.43	1.88	128.65	2.29	0.13	0.79
11.69	50.99	64.99	1.96	127.41	2.31	0.12	0.78
11.76	48.37	61.54	2.05	126.05	2.33	0.12	0.78
11.83	47.37	60.00	2.07	124.09	2.34	0.12	0.77
11.88	46.96	59.26	2.07	122.51	2.34	0.12	0.77
11.95	46.26	58.18	2.11	122.50	2.34	0.12	0.77
12.01	45.56	57.17	2.16	123.29	2.36	0.12	0.77
12.08	44.45	55.68	2.27	126.46	2.38	0.11	0.77
12.14	44.24	55.34	2.36	130.40	2.40	0.12	0.77
12.23	42.94	53.62	2.55	136.86	2.43	0.11	0.77
12.28	43.13	53.75	2.58	138.78	2.44	0.12	0.77
12.35	43.14	53.57	2.67	142.82	2.45	0.12	0.77
12.40	43.14	53.46	2.72	145.16	2.46	0.12	0.77
12.47	44.45	54.77	2.64	144.88	2.45	0.12	0.77
12.54	45.46	55.77	2.65	147.88	2.45	0.12	0.77
12.60	46.75	57.14	2.63	150.06	2.45	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
12.70	46.35	56.44	2.75	155.42	2.47	0.12	0.77
12.75	46.55	56.49	2.76	155.65	2.47	0.12	0.77
12.80	46.65	56.40	2.75	155.24	2.47	0.12	0.77
12.87	46.85	56.35	2.72	153.33	2.46	0.12	0.77
12.93	47.46	56.82	2.66	151.13	2.45	0.12	0.77
12.99	50.27	59.73	2.45	146.61	2.42	0.12	0.78
13.06	52.38	61.81	2.29	141.47	2.38	0.13	0.78
13.14	55.30	64.68	2.09	135.30	2.34	0.13	0.79
13.19	56.10	65.32	2.03	132.62	2.33	0.13	0.79
13.26	57.71	66.74	1.93	128.86	2.30	0.13	0.79
13.32	57.61	66.39	1.93	128.39	2.30	0.13	0.79
13.40	58.12	66.67	1.92	128.22	2.30	0.13	0.79
13.46	58.42	66.75	1.91	127.17	2.29	0.13	0.79
13.53	58.52	66.60	1.90	126.83	2.29	0.13	0.79
13.58	58.12	66.07	1.99	131.66	2.32	0.13	0.79
13.68	56.80	64.47	2.19	141.25	2.36	0.13	0.79
13.73	55.89	63.34	2.28	144.62	2.38	0.13	0.79
13.79	53.40	60.47	2.47	149.51	2.42	0.13	0.78
13.88	53.48	60.28	2.52	151.72	2.43	0.13	0.78
13.92	53.58	60.23	2.51	151.29	2.43	0.13	0.78
13.98	54.69	61.20	2.44	149.61	2.41	0.13	0.78
14.05	57.01	63.47	2.33	147.84	2.39	0.13	0.79
14.13	58.82	65.10	2.23	145.11	2.37	0.13	0.79
14.17	60.33	66.52	2.15	142.95	2.35	0.13	0.79
14.24	63.65	69.77	2.00	139.84	2.32	0.14	0.80
14.33	65.86	71.74	1.91	136.68	2.29	0.14	0.80
14.37	68.47	74.28	1.81	134.73	2.27	0.14	0.80
14.45	71.39	77.01	1.73	133.15	2.24	0.14	0.81
14.53	73.90	79.34	1.68	133.20	2.22	0.15	0.81
14.57	76.10	81.46	1.64	133.63	2.21	0.15	0.81
14.64	79.23	84.38	1.58	133.69	2.19	0.15	0.81
14.72	80.93	85.83	1.56	133.84	2.18	0.15	0.82
14.76	82.55	87.30	1.54	134.12	2.17	0.16	0.82
14.85	84.85	89.31	1.51	134.64	2.15	0.16	0.82
14.90	86.66	90.94	1.49	135.23	2.14	0.16	0.82
14.96	88.97	93.02	1.46	136.13	2.13	0.16	0.82
15.03	91.80	95.56	1.43	136.84	2.11	0.17	0.82
15.10	93.00	96.49	1.42	137.33	2.10	0.17	0.83
15.16	94.21	97.43	1.41	137.66	2.10	0.17	0.83
15.24	94.81	97.67	1.41	137.69	2.09	0.17	0.83
15.31	94.61	97.17	1.41	137.37	2.10	0.17	0.83
15.36	94.21	96.52	1.42	136.70	2.10	0.17	0.83
15.45	90.59	92.50	1.45	133.95	2.12	0.16	0.82
15.50	88.38	90.04	1.47	132.08	2.13	0.16	0.82
15.55	85.26	86.68	1.50	129.97	2.15	0.15	0.82
15.66	79.63	80.58	1.55	125.17	2.17	0.15	0.81
15.69	77.32	78.14	1.58	123.42	2.19	0.14	0.81
15.75	73.90	74.45	1.61	119.92	2.20	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
15.82	69.98	70.30	1.69	118.54	2.23	0.13	0.80
15.91	66.46	66.54	1.82	121.27	2.27	0.13	0.79
15.96	62.44	62.40	2.00	124.54	2.32	0.13	0.79
16.02	58.01	57.84	2.25	130.09	2.38	0.13	0.78
16.08	55.00	54.70	2.54	139.19	2.43	0.12	0.78
16.14	52.18	51.73	2.78	143.62	2.47	0.12	0.77
16.22	47.16	46.58	3.35	155.97	2.55	0.12	0.77
16.30	43.64	42.92	4.00	171.85	2.63	0.11	0.62
16.34	37.60	36.86	5.08	187.43	2.73	0.11	0.62
16.42	39.82	38.85	4.35	168.98	2.66	0.11	0.62
16.50	40.11	38.98	4.57	178.05	2.69	0.11	0.62
16.54	41.72	40.47	4.42	179.01	2.67	0.11	0.62
16.62	42.12	40.67	4.30	174.79	2.66	0.11	0.62
16.70	43.93	42.28	4.41	186.33	2.67	0.12	0.62
16.74	45.74	43.94	4.31	189.23	2.66	0.12	0.62
16.80	51.77	49.66	3.82	189.49	2.61	0.13	0.63
16.87	60.72	58.10	3.13	182.08	2.52	0.14	0.79
16.94	67.76	64.67	2.74	177.35	2.46	0.15	0.80
17.01	81.73	77.86	2.15	167.40	2.35	0.17	0.82
17.09	87.35	82.93	1.99	164.61	2.32	0.17	0.83
17.14	93.39	88.47	1.82	161.32	2.27	0.18	0.83
17.23	103.34	97.56	1.60	156.39	2.20	0.20	0.84
17.28	106.96	100.75	1.53	153.84	2.16	0.20	0.85
17.34	109.07	102.50	1.48	151.59	2.14	0.20	0.85
17.39	110.79	103.88	1.45	150.22	2.12	0.20	0.85
17.46	112.80	105.46	1.43	150.29	2.10	0.20	0.85
17.52	113.81	106.14	1.42	150.50	2.10	0.21	0.85
17.60	114.01	105.96	1.42	150.23	2.10	0.21	0.85
17.66	113.71	105.44	1.42	149.84	2.10	0.21	0.85
17.73	112.30	103.78	1.43	148.53	2.11	0.20	0.85
17.79	109.89	101.27	1.46	147.43	2.12	0.20	0.84
17.86	107.17	98.44	1.49	147.09	2.14	0.19	0.84
17.92	105.06	96.22	1.52	146.58	2.16	0.19	0.84
17.98	102.35	93.43	1.57	146.23	2.18	0.19	0.84
18.07	100.74	91.59	1.59	145.63	2.19	0.18	0.84
18.11	99.83	90.56	1.61	145.37	2.20	0.18	0.84
18.18	97.82	88.42	1.64	145.41	2.21	0.18	0.83
18.27	97.22	87.56	1.64	144.03	2.21	0.18	0.83
18.32	96.41	86.60	1.66	143.51	2.22	0.18	0.83
18.37	95.51	85.59	1.67	142.91	2.22	0.17	0.83
18.46	91.99	82.07	1.69	138.48	2.23	0.17	0.82
18.52	89.27	79.41	1.70	135.01	2.23	0.16	0.82
18.57	84.55	74.94	1.77	132.62	2.26	0.15	0.81
18.66	75.20	66.17	2.00	132.10	2.32	0.14	0.80
18.71	69.57	60.92	2.20	133.97	2.36	0.14	0.79
18.77	60.22	52.33	2.66	139.18	2.45	0.13	0.78
18.84	52.37	45.11	3.19	143.91	2.53	0.12	0.77
18.91	46.85	40.03	3.70	148.17	2.59	0.11	0.76

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
18.97	43.74	37.14	4.08	151.50	2.64	0.11	0.62
19.05	36.30	30.41	5.34	162.37	2.76	0.10	0.62
19.10	32.98	27.40	6.10	167.03	2.82	0.10	0.62
19.16	31.87	26.33	6.40	168.38	2.84	0.10	0.62
19.26	28.86	23.60	7.18	169.40	2.90	0.10	0.62
19.30	26.85	21.83	7.70	168.14	2.93	0.10	0.62
19.36	24.53	19.79	8.34	165.13	2.97	0.09	0.62
19.43	24.73	19.89	7.61	151.35	2.93	0.09	0.62
19.51	23.13	18.46	6.97	128.67	2.88	0.09	0.62
19.55	22.12	17.57	7.62	133.90	2.93	0.09	0.62
19.63	22.12	17.50	7.93	138.84	2.95	0.09	0.62
19.69	22.12	17.44	8.10	141.31	2.96	0.09	0.62
19.75	22.92	18.05	7.93	143.09	2.95	0.09	0.62
19.84	23.60	18.53	8.09	150.00	2.96	0.09	0.62
19.89	24.60	19.32	7.83	151.25	2.94	0.09	0.62
19.96	24.18	18.89	8.15	154.01	2.96	0.09	0.62
20.02	25.59	20.00	7.62	152.33	2.93	0.09	0.62
20.09	26.09	20.33	7.52	152.84	2.92	0.09	0.62
20.14	26.80	20.85	7.38	153.90	2.91	0.09	0.62
20.22	27.93	21.69	7.24	157.10	2.90	0.10	0.62
20.28	29.46	22.86	6.89	157.56	2.88	0.10	0.62
20.36	30.26	23.41	6.92	162.02	2.88	0.10	0.62
20.41	31.77	24.58	6.65	163.41	2.86	0.10	0.62
20.48	32.88	25.38	6.52	165.38	2.85	0.10	0.62
20.55	35.30	27.30	5.97	163.11	2.81	0.10	0.62
20.61	36.10	27.89	5.81	161.91	2.80	0.10	0.62
20.68	36.70	28.29	5.68	160.74	2.79	0.10	0.62
20.74	38.61	29.79	5.34	158.93	2.76	0.10	0.62
20.81	40.32	31.07	5.15	159.96	2.74	0.11	0.62
20.88	41.12	31.61	5.11	161.60	2.74	0.11	0.62
20.93	40.62	31.09	5.31	165.15	2.75	0.11	0.62
21.00	40.72	31.06	5.38	167.02	2.76	0.11	0.62
21.07	40.52	30.76	5.52	169.69	2.77	0.11	0.62
21.13	39.92	30.16	5.73	172.77	2.79	0.11	0.62
21.22	39.51	29.67	5.94	176.21	2.81	0.11	0.62
21.27	39.61	29.68	5.96	177.02	2.81	0.11	0.62
21.34	41.01	30.71	5.71	175.41	2.79	0.11	0.62
21.41	40.51	30.20	5.82	175.86	2.80	0.11	0.62
21.46	40.11	29.79	5.93	176.60	2.81	0.11	0.62
21.55	41.72	30.94	5.69	176.14	2.79	0.11	0.62
21.59	43.53	32.32	5.40	174.59	2.76	0.11	0.62
21.66	44.83	33.27	5.18	172.31	2.74	0.11	0.62
21.76	47.75	35.47	4.72	167.27	2.70	0.11	0.62
21.80	48.65	36.12	4.60	166.20	2.69	0.11	0.62
21.86	49.96	37.07	4.45	165.05	2.68	0.12	0.62
21.95	53.28	39.57	4.08	161.43	2.64	0.12	0.62
22.01	55.59	41.32	3.83	158.12	2.61	0.12	0.62
22.06	57.90	43.08	3.60	154.96	2.58	0.12	0.77

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
22.12	59.81	44.51	3.43	152.54	2.56	0.12	0.78
22.18	62.13	46.26	3.24	150.05	2.54	0.13	0.78
22.26	65.14	48.52	3.03	147.01	2.51	0.13	0.78
22.31	67.76	50.53	2.86	144.56	2.48	0.13	0.79
22.38	72.58	54.29	2.57	139.74	2.44	0.14	0.79
22.44	76.61	57.46	2.33	133.74	2.39	0.14	0.80
22.53	83.24	62.78	1.98	124.55	2.32	0.14	0.80
22.59	86.66	65.44	1.89	123.52	2.29	0.15	0.81
22.65	89.69	67.74	1.81	122.93	2.27	0.15	0.81
22.71	93.61	70.78	1.73	122.51	2.24	0.16	0.82
22.78	97.73	73.94	1.66	122.79	2.22	0.16	0.82
22.86	99.94	75.48	1.64	123.45	2.21	0.16	0.82
22.92	102.15	77.12	1.61	123.96	2.20	0.17	0.82
22.98	102.66	77.34	1.61	124.35	2.20	0.17	0.82
23.04	103.16	77.54	1.62	125.35	2.20	0.17	0.83
23.10	103.26	77.35	1.64	127.06	2.21	0.17	0.83
23.16	102.86	76.80	1.66	127.73	2.22	0.17	0.83
23.25	102.86	76.51	1.68	128.46	2.22	0.17	0.83
23.30	102.86	76.34	1.69	128.99	2.23	0.17	0.83
23.36	102.86	76.13	1.70	129.75	2.23	0.17	0.83
23.43	102.96	75.95	1.73	131.19	2.24	0.17	0.83
23.49	102.96	75.72	1.75	132.46	2.25	0.17	0.83
23.56	103.66	76.01	1.76	134.03	2.25	0.17	0.83
23.65	104.37	76.29	1.77	134.95	2.26	0.18	0.83
23.71	103.76	75.61	1.79	135.39	2.26	0.18	0.83
23.76	102.56	74.54	1.81	134.91	2.27	0.17	0.83
23.83	97.33	70.29	1.90	133.44	2.29	0.16	0.82
23.89	92.40	66.32	1.99	132.02	2.32	0.16	0.82
23.95	83.65	59.44	2.20	130.94	2.37	0.15	0.80
24.02	74.10	51.99	2.53	131.52	2.43	0.13	0.79
24.09	64.15	44.35	2.99	132.73	2.50	0.12	0.78
24.15	50.68	34.13	4.09	139.68	2.64	0.11	0.62
24.24	40.12	26.30	5.36	140.92	2.76	0.10	0.62
24.29	35.29	22.76	6.19	140.99	2.83	0.10	0.62
24.35	29.86	19.04	7.41	141.08	2.91	0.09	0.62
24.42	27.15	17.16	7.77	133.41	2.94	0.09	0.62
24.49	26.04	16.37	7.73	126.57	2.93	0.09	0.62
24.54	25.44	15.94	7.65	121.87	2.93	0.09	0.62
24.62	25.94	16.22	7.25	117.65	2.90	0.09	0.62
24.69	25.84	16.11	7.30	117.61	2.91	0.09	0.62
24.75	27.55	17.20	6.71	115.50	2.87	0.09	0.62
24.81	30.67	19.26	6.01	115.82	2.81	0.09	0.62
24.88	33.38	21.01	5.90	124.04	2.80	0.10	0.62
24.94	37.50	23.77	5.54	131.64	2.77	0.10	0.62
25.00	51.18	33.50	3.80	127.36	2.61	0.11	0.62
25.07	64.75	43.26	2.90	125.34	2.49	0.12	0.77
25.13	68.08	45.48	2.84	129.17	2.48	0.13	0.78
25.22	79.34	53.42	2.50	133.70	2.42	0.14	0.80

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
25.27	84.57	57.13	2.36	134.97	2.40	0.15	0.80
25.33	88.79	60.08	2.26	135.74	2.38	0.15	0.81
25.40	92.71	62.88	2.13	133.77	2.35	0.16	0.81
25.48	92.71	62.89	2.04	127.99	2.33	0.15	0.81
25.53	90.70	61.39	2.04	125.35	2.33	0.15	0.81
25.60	84.97	56.93	2.23	127.05	2.37	0.14	0.80
25.67	81.75	54.42	2.34	127.49	2.39	0.14	0.80
25.73	76.93	50.73	2.56	129.81	2.43	0.14	0.79
25.79	68.68	44.58	3.03	135.13	2.51	0.13	0.78
25.87	56.71	35.80	4.08	146.12	2.64	0.12	0.62
25.92	54.29	34.00	4.37	148.55	2.67	0.12	0.62
26.00	45.64	27.83	5.64	157.03	2.78	0.11	0.62
26.07	40.31	24.24	6.60	160.01	2.86	0.10	0.62
26.12	36.79	22.00	7.33	161.20	2.91	0.10	0.62
26.19	32.67	19.37	8.19	158.52	2.96	0.10	0.62
26.25	29.45	17.32	8.92	154.44	3.01	0.09	1.24
26.33	27.64	16.14	9.26	149.54	3.03	0.09	1.15
26.39	27.64	16.10	9.07	146.06	3.02	0.09	1.15
26.45	28.75	16.75	8.61	144.13	2.99	0.09	0.62
26.52	30.56	17.82	7.92	141.07	2.95	0.09	0.62
26.58	32.77	19.13	7.18	137.37	2.90	0.10	0.62
26.66	36.89	21.59	6.45	139.25	2.85	0.10	0.62
26.72	40.51	23.81	5.85	139.19	2.80	0.10	0.62
26.78	45.64	27.22	5.01	136.38	2.73	0.11	0.62
26.84	55.69	34.09	3.74	127.60	2.60	0.11	0.76
26.91	61.83	38.30	3.19	122.03	2.53	0.12	0.77
26.97	65.75	40.96	2.93	120.00	2.49	0.12	0.77
27.05	71.38	44.78	2.64	118.36	2.45	0.13	0.78
27.10	75.90	47.89	2.44	116.75	2.41	0.13	0.79
27.17	81.93	52.21	2.13	111.29	2.35	0.13	0.79
27.24	87.56	56.32	1.90	106.88	2.29	0.14	0.80
27.30	91.18	58.88	1.79	105.62	2.26	0.14	0.80
27.37	94.80	61.38	1.72	105.62	2.24	0.14	0.81
27.46	98.02	63.41	1.70	107.68	2.23	0.15	0.81
27.51	100.23	64.89	1.67	108.25	2.22	0.15	0.81
27.57	103.15	66.88	1.63	108.82	2.21	0.15	0.81
27.64	106.37	69.04	1.59	109.55	2.19	0.16	0.82
27.70	108.08	70.14	1.57	110.07	2.18	0.16	0.82
27.76	108.68	70.40	1.57	110.62	2.18	0.16	0.82
27.82	109.58	70.83	1.58	111.68	2.18	0.16	0.82
27.91	109.68	70.56	1.61	113.29	2.20	0.16	0.82
27.96	110.39	70.88	1.61	114.26	2.20	0.16	0.82
28.03	111.19	71.21	1.62	115.28	2.20	0.17	0.82
28.09	110.99	70.87	1.63	115.62	2.21	0.17	0.82
28.16	110.19	70.11	1.65	115.90	2.22	0.17	0.82
28.23	107.27	67.83	1.70	115.59	2.23	0.16	0.82
28.29	103.95	65.33	1.76	115.23	2.25	0.16	0.82
28.36	98.32	61.21	1.88	115.01	2.29	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
28.45	94.10	58.16	1.95	113.26	2.31	0.15	0.81
28.48	91.08	56.03	2.01	112.77	2.32	0.14	0.80
28.55	88.97	54.59	2.01	109.76	2.32	0.14	0.80
28.61	87.26	53.44	2.00	106.77	2.32	0.14	0.80
28.68	86.66	52.99	1.99	105.45	2.32	0.14	0.80
28.74	86.16	52.60	1.98	104.01	2.31	0.13	0.79
28.81	82.45	49.93	2.08	103.90	2.34	0.13	0.79
28.87	65.47	38.15	2.95	112.38	2.50	0.12	0.77
28.94	67.97	39.75	2.78	110.63	2.47	0.12	0.77
29.03	53.59	30.08	3.99	119.92	2.63	0.11	0.62
29.08	44.74	24.32	5.21	126.60	2.75	0.10	0.62
29.16	34.39	18.22	7.38	134.43	2.91	0.10	0.62
29.22	29.76	15.60	8.63	134.65	2.99	0.09	0.62
29.27	26.44	13.72	9.79	134.33	3.06	0.09	0.98
29.35	22.82	11.67	11.22	130.91	3.13	0.08	0.83
29.43	21.82	11.08	11.29	125.14	3.13	0.08	0.79
29.47	20.81	10.51	11.67	122.61	3.15	0.08	0.75
29.53	19.91	9.99	11.99	119.79	3.17	0.08	0.71
29.60	19.61	9.80	11.82	115.91	3.16	0.08	0.70
29.67	19.71	9.83	11.53	113.37	3.14	0.08	0.70
29.73	19.81	9.87	11.32	111.70	3.13	0.08	0.70
29.80	19.30	9.56	11.53	110.22	3.14	0.08	0.68
29.87	18.40	9.05	12.14	109.84	3.17	0.08	0.65
29.93	17.90	8.76	12.55	109.87	3.19	0.08	0.63
30.00	17.80	8.68	12.63	109.62	3.20	0.08	0.62
30.07	17.70	8.61	12.71	109.36	3.20	0.08	0.61
30.12	17.70	8.59	12.89	110.78	3.21	0.08	0.61
30.20	18.20	8.84	12.85	113.52	3.20	0.08	0.63
30.27	18.80	9.14	12.68	115.91	3.20	0.08	0.65
30.32	19.20	9.34	12.58	117.49	3.19	0.08	0.67
30.40	20.01	9.75	12.43	121.16	3.19	0.08	0.70
30.46	20.21	9.83	12.64	124.26	3.20	0.08	0.70
30.52	19.81	9.60	13.15	126.21	3.22	0.08	0.69
30.59	19.71	9.52	13.35	127.14	3.23	0.08	0.68
30.65	18.80	9.02	14.17	127.77	3.26	0.08	0.64
30.71	18.50	8.84	14.43	127.51	3.27	0.08	0.63
30.79	18.00	8.55	14.91	127.46	3.29	0.08	0.61
30.85	17.90	8.48	14.94	126.64	3.29	0.08	0.61
30.96	17.80	8.39	13.39	112.42	3.23	0.08	0.60
31.00	18.20	8.59	13.79	118.48	3.24	0.08	0.61
31.04	18.40	8.68	13.99	121.51	3.25	0.08	0.62
31.11	18.70	8.82	13.86	122.23	3.25	0.08	0.63
31.18	18.60	8.75	14.03	122.76	3.25	0.08	0.62
31.25	18.41	8.62	14.17	122.19	3.26	0.08	0.62
31.30	18.71	8.76	13.86	121.50	3.25	0.08	0.63
31.38	19.62	9.22	13.09	120.60	3.22	0.08	0.66
31.44	19.67	9.22	13.05	120.32	3.21	0.08	0.66
31.50	19.92	9.33	12.62	117.82	3.20	0.08	0.67

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
31.57	19.72	9.21	12.90	118.74	3.21	0.08	0.66
31.63	20.92	9.81	12.48	122.36	3.19	0.08	0.70
31.70	21.63	10.15	12.28	124.65	3.18	0.08	0.73
31.79	21.93	10.27	12.33	126.65	3.18	0.08	0.73
31.83	22.48	10.54	12.05	127.02	3.17	0.08	0.75
31.90	23.34	10.96	11.56	126.75	3.15	0.08	0.78
31.97	23.14	10.83	11.60	125.70	3.15	0.08	0.77
32.03	22.03	10.24	12.20	125.03	3.18	0.08	0.73
32.10	21.63	10.02	12.35	123.74	3.18	0.08	0.72
32.16	21.53	9.95	12.26	121.97	3.18	0.08	0.71
32.23	21.63	9.97	12.17	121.41	3.17	0.08	0.71
32.30	21.73	10.00	12.13	121.31	3.17	0.08	0.71
32.36	21.63	9.93	12.21	121.26	3.18	0.08	0.71
32.46	20.92	9.54	12.74	121.52	3.20	0.08	0.68
32.51	20.92	9.53	12.76	121.51	3.20	0.08	0.68
32.56	21.43	9.76	12.45	121.58	3.19	0.08	0.70
32.65	21.93	9.99	12.30	122.86	3.18	0.08	0.71
32.68	24.84	11.43	10.67	122.00	3.10	0.09	0.82
32.76	27.16	12.56	9.77	122.71	3.06	0.09	0.90
32.84	30.78	14.33	8.70	124.70	3.00	0.09	0.62
32.89	31.38	14.61	8.68	126.84	2.99	0.09	0.62
32.95	31.68	14.73	8.79	129.38	3.00	0.09	1.05
33.01	30.68	14.20	9.17	130.29	3.02	0.09	1.01
33.10	27.66	12.67	10.17	128.82	3.08	0.09	0.91
33.15	26.05	11.86	10.86	128.81	3.11	0.09	0.85
33.24	24.54	11.08	11.45	126.92	3.14	0.09	0.79
33.29	22.93	10.27	12.18	125.07	3.18	0.08	0.73
33.35	20.72	9.17	13.23	121.28	3.22	0.08	0.65
33.40	19.52	8.56	13.93	119.27	3.25	0.08	0.61
33.47	18.81	8.20	14.34	117.53	3.27	0.08	0.59
33.55	17.51	7.54	15.28	115.24	3.30	0.08	0.54
33.65	16.40	6.98	16.13	112.51	3.33	0.08	0.50
33.66	16.20	6.88	16.29	112.00	3.34	0.08	0.49
33.74	16.10	6.81	16.05	109.30	3.33	0.08	0.49
33.84	15.70	6.60	16.14	106.45	3.34	0.08	0.47
33.88	15.70	6.59	16.06	105.81	3.33	0.08	0.47
33.93	15.70	6.58	15.94	104.84	3.33	0.08	0.47
33.99	15.70	6.56	15.84	103.94	3.32	0.08	0.47
34.07	15.49	6.45	15.98	103.04	3.33	0.08	0.46
34.12	15.49	6.44	15.94	102.61	3.33	0.08	0.46
34.19	15.49	6.42	15.95	102.43	3.33	0.08	0.46
34.28	15.80	6.55	15.75	103.17	3.32	0.08	0.47
34.32	15.90	6.59	15.76	103.89	3.32	0.08	0.47
34.40	16.30	6.76	15.65	105.89	3.32	0.08	0.48
34.48	16.60	6.89	15.22	104.92	3.30	0.08	0.49
34.52	16.80	6.98	14.88	103.83	3.29	0.08	0.50
34.58	17.71	7.39	14.15	104.63	3.26	0.08	0.53
34.68	22.83	9.79	10.37	101.60	3.09	0.08	0.70

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ_v}	S _{u(peak)/σ_v}
34.72	26.65	11.58	8.88	102.83	3.01	0.09	0.83
34.81	30.98	13.59	8.07	109.64	2.96	0.09	0.62
34.85	26.05	11.26	10.37	116.71	3.09	0.09	0.80
34.92	29.26	12.74	9.41	119.85	3.04	0.09	0.91
34.98	26.04	11.21	11.15	124.97	3.13	0.09	0.80
35.05	25.04	10.72	11.71	125.50	3.15	0.08	0.77
35.12	24.43	10.41	12.09	125.82	3.17	0.08	0.74
35.18	25.54	10.91	11.51	125.47	3.14	0.09	0.78
35.26	26.64	11.39	11.23	127.91	3.13	0.09	0.81
35.31	27.86	11.93	10.82	129.12	3.11	0.09	0.85
35.41	32.49	14.04	9.37	131.65	3.03	0.09	1.00
35.47	36.81	16.02	8.19	131.13	2.96	0.10	0.62
35.51	43.55	19.11	6.68	127.61	2.86	0.10	0.62
35.58	56.92	25.57	4.70	120.23	2.70	0.11	0.62
35.63	68.38	31.89	3.59	114.37	2.58	0.12	0.77
35.71	78.94	37.84	2.89	109.46	2.49	0.13	0.78
35.78	83.97	40.58	2.69	109.34	2.46	0.13	0.79
35.84	82.46	39.53	2.83	111.90	2.48	0.13	0.78
35.90	76.73	36.09	3.22	116.14	2.53	0.13	0.78
35.98	67.37	30.65	4.03	123.40	2.63	0.12	0.62
36.05	60.53	26.84	4.74	127.22	2.70	0.11	0.62
36.10	53.19	23.15	5.67	131.38	2.79	0.11	0.62
36.20	40.92	17.53	7.77	136.17	2.94	0.10	0.62
36.25	37.01	15.73	8.58	134.93	2.99	0.10	0.62
36.30	31.77	13.34	10.02	133.73	3.07	0.09	0.95
36.35	29.76	12.42	10.47	130.07	3.09	0.09	0.89
36.45	27.65	11.43	10.64	121.69	3.10	0.09	0.82
36.48	27.35	11.29	10.54	118.93	3.10	0.09	0.81
36.55	27.25	11.22	10.42	116.91	3.09	0.09	0.80
36.63	27.40	11.26	10.51	118.33	3.09	0.09	0.80
36.69	26.86	11.00	10.95	120.38	3.12	0.09	0.79
36.75	27.46	11.25	10.92	122.83	3.12	0.09	0.80
36.84	28.46	11.66	10.86	126.61	3.11	0.09	0.83
36.89	29.37	12.05	10.71	129.06	3.10	0.09	0.86
36.95	30.07	12.34	10.79	133.12	3.11	0.09	0.88
37.05	32.08	13.19	10.53	138.97	3.10	0.09	0.94
37.08	33.99	14.02	10.01	140.40	3.07	0.09	1.00
37.14	36.01	14.89	9.54	141.98	3.04	0.09	1.06
37.23	38.22	15.82	9.19	145.38	3.02	0.10	1.13
37.28	39.32	16.28	9.05	147.42	3.02	0.10	1.16
37.34	40.13	16.61	8.99	149.28	3.01	0.10	1.19
37.43	42.24	17.49	8.69	151.97	2.99	0.10	0.62
37.48	43.45	17.99	8.51	153.04	2.98	0.10	0.62
37.53	44.75	18.53	8.14	150.87	2.96	0.10	0.62
37.61	47.67	19.76	6.92	136.71	2.88	0.10	0.62
37.67	48.88	20.26	6.91	139.97	2.88	0.10	0.62
37.73	53.30	22.14	6.19	137.11	2.83	0.11	0.62
37.82	61.34	25.57	5.14	131.40	2.74	0.11	0.62

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
37.88	69.49	29.73	4.24	125.96	2.65	0.12	0.62
37.93	70.59	30.26	4.14	125.17	2.64	0.12	0.62
38.00	87.79	39.53	2.93	115.68	2.49	0.13	0.79
38.08	93.01	42.32	2.69	113.79	2.46	0.14	0.80
38.12	98.64	45.45	2.46	111.77	2.42	0.14	0.80
38.20	106.79	49.97	2.20	109.75	2.36	0.15	0.81
38.29	115.74	54.91	1.99	109.18	2.32	0.16	0.82
38.33	120.56	57.57	1.90	109.56	2.29	0.17	0.83
38.43	130.02	62.31	1.85	115.02	2.28	0.19	0.84
38.48	132.73	63.63	1.83	116.71	2.27	0.19	0.84
38.52	134.94	64.66	1.83	118.30	2.27	0.20	0.84
38.59	136.65	65.16	1.87	121.67	2.28	0.20	0.85
38.68	137.25	64.96	1.93	125.42	2.30	0.21	0.85
38.72	138.26	65.31	1.94	126.95	2.31	0.21	0.85
38.79	141.28	66.62	1.94	129.57	2.31	0.22	0.85
38.87	145.40	68.55	1.93	132.27	2.30	0.23	0.86
38.92	150.43	71.07	1.89	134.45	2.29	0.25	0.86
38.98	155.85	73.85	1.85	136.51	2.28	0.27	0.87
39.05	162.89	77.35	1.81	140.05	2.27	0.30	0.88
39.12	167.92	79.82	1.79	142.65	2.26	0.32	0.88
39.17	171.44	81.43	1.78	145.16	2.26	0.34	0.88
39.26	174.46	82.65	1.79	147.82	2.26	0.36	0.89
39.32	175.36	82.90	1.80	148.84	2.26	0.37	0.89
39.37	175.76	82.92	1.80	149.52	2.27	0.37	0.89
39.46	175.76	82.62	1.82	150.08	2.27	0.37	0.89
39.52	175.76	82.47	1.82	150.11	2.27	0.37	0.89
39.57	174.66	81.73	1.83	149.95	2.27	0.37	0.89
39.63	173.45	80.90	1.85	149.77	2.28	0.36	0.89
39.72	172.55	80.22	1.86	149.35	2.28	0.35	0.89
39.77	172.04	79.85	1.87	148.95	2.28	0.35	0.89
39.85	169.23	78.13	1.90	148.37	2.29	0.34	0.88
39.91	167.82	77.26	1.91	147.79	2.30	0.33	0.88
39.96	165.81	76.09	1.93	146.93	2.30	0.32	0.88
40.06	163.80	74.97	1.93	144.72	2.30	0.30	0.88
40.11	160.88	73.32	1.96	143.90	2.31	0.29	0.87
40.16	157.16	71.24	2.01	143.03	2.32	0.28	0.87
40.26	148.52	66.60	2.10	140.18	2.34	0.25	0.86
40.30	144.19	64.24	2.17	139.54	2.36	0.23	0.86
40.36	138.16	61.01	2.27	138.48	2.38	0.22	0.85
40.44	130.13	56.79	2.40	136.54	2.41	0.20	0.84
40.50	126.91	55.29	2.40	132.47	2.40	0.19	0.84
40.55	122.28	53.40	2.32	124.13	2.39	0.18	0.83
40.62	117.05	50.41	2.51	126.49	2.42	0.17	0.82
40.68	113.13	48.41	2.57	124.25	2.43	0.17	0.82
40.75	109.21	46.45	2.63	121.95	2.44	0.16	0.81
40.84	106.70	45.14	2.67	120.62	2.45	0.16	0.81
40.90	105.54	44.48	2.71	120.46	2.46	0.15	0.81
40.96	103.88	43.54	2.78	120.92	2.47	0.15	0.81

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
41.04	104.39	43.69	2.76	120.80	2.47	0.15	0.81
41.09	104.18	43.49	2.79	121.41	2.47	0.15	0.81
41.15	104.29	43.43	2.81	121.92	2.47	0.15	0.81
41.22	105.79	44.11	2.75	121.36	2.47	0.15	0.81
41.30	107.60	45.00	2.67	120.00	2.45	0.16	0.81
41.35	109.11	45.77	2.59	118.73	2.44	0.16	0.81
41.41	110.32	46.42	2.53	117.60	2.43	0.16	0.81
41.48	111.93	47.20	2.47	116.53	2.42	0.16	0.81
41.55	112.93	47.64	2.44	116.14	2.41	0.16	0.82
41.62	113.44	47.81	2.42	115.85	2.41	0.16	0.82
41.68	113.13	47.58	2.43	115.65	2.41	0.16	0.82
41.74	112.63	47.25	2.45	115.60	2.41	0.16	0.82
41.80	112.23	46.94	2.47	115.92	2.42	0.16	0.81
41.88	112.23	46.83	2.47	115.78	2.42	0.16	0.81
41.95	112.73	47.01	2.46	115.49	2.42	0.16	0.81
42.00	113.03	47.11	2.45	115.28	2.41	0.16	0.82
42.08	112.13	46.50	2.49	115.78	2.42	0.16	0.81
42.15	110.72	45.62	2.55	116.36	2.43	0.16	0.81
42.22	107.30	43.75	2.69	117.61	2.46	0.15	0.81
42.28	103.48	41.70	2.86	119.26	2.48	0.15	0.80
42.34	98.45	39.07	3.11	121.56	2.52	0.14	0.80
42.39	95.44	37.49	3.29	123.25	2.54	0.14	0.80
42.48	94.23	36.78	3.37	124.10	2.55	0.14	0.79
42.53	94.63	36.92	3.35	123.75	2.55	0.14	0.79
42.59	96.44	37.74	3.26	123.14	2.54	0.14	0.80
42.68	98.76	38.71	3.19	123.52	2.53	0.15	0.80
42.72	100.46	39.50	3.11	122.76	2.52	0.15	0.80
42.79	106.20	42.33	2.83	119.82	2.48	0.15	0.81
42.87	113.64	46.19	2.49	115.23	2.42	0.16	0.82
42.92	116.35	47.68	2.36	112.42	2.40	0.16	0.82
43.00	117.66	48.51	2.24	108.89	2.37	0.16	0.82
43.05	118.16	48.72	2.23	108.63	2.37	0.16	0.82
43.13	121.38	50.33	2.13	107.43	2.35	0.17	0.82
43.22	123.89	52.07	1.95	101.71	2.31	0.17	0.82
43.27	122.18	51.41	1.93	98.98	2.30	0.16	0.82
43.33	116.34	48.49	2.00	97.16	2.32	0.15	0.81
43.37	110.71	45.55	2.13	97.16	2.35	0.15	0.81
43.47	94.71	37.38	2.63	98.49	2.45	0.13	0.79
43.52	86.26	33.13	3.07	101.76	2.51	0.13	0.78
43.57	73.38	26.68	4.20	112.18	2.65	0.12	0.62
43.66	55.18	19.52	6.86	133.83	2.88	0.11	0.62
43.72	49.35	17.33	7.97	138.17	2.95	0.10	0.62
43.77	43.01	14.95	9.46	141.47	3.04	0.10	1.07
43.83	38.59	13.29	10.63	141.31	3.10	0.09	0.95
43.90	33.96	11.56	11.96	138.22	3.17	0.09	0.83
43.97	40.30	13.88	9.18	127.40	3.02	0.09	0.99
44.03	40.00	13.75	8.92	122.67	3.01	0.09	0.98
44.13	36.98	12.61	9.09	114.59	3.02	0.09	0.90

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)/σ'_v}	S _{u(peak)/σ'_v}
44.17	34.67	11.75	9.48	111.38	3.04	0.09	0.84
44.23	31.55	10.58	9.98	105.60	3.07	0.09	0.76
44.33	27.83	9.20	10.96	100.76	3.12	0.08	0.66
44.37	26.12	8.56	11.87	101.64	3.16	0.08	0.61
44.43	23.31	7.52	13.67	102.82	3.24	0.08	0.54
44.52	20.59	6.51	16.72	108.83	3.36	0.08	0.47
44.57	19.39	6.07	18.78	113.90	3.42	0.08	0.43
44.62	19.59	6.13	19.42	119.03	3.44	0.08	0.44
44.72	29.64	9.76	12.84	125.42	3.20	0.09	0.70
44.76	47.94	16.40	7.34	120.28	2.91	0.10	0.62
44.83	80.92	29.12	3.74	108.94	2.60	0.12	0.77
44.92	103.64	39.23	2.80	109.92	2.47	0.15	0.80
44.97	115.31	44.60	2.49	110.88	2.42	0.16	0.81
45.02	116.81	44.94	2.54	114.17	2.43	0.16	0.82
45.09	117.31	44.79	2.63	117.93	2.45	0.17	0.82
45.16	119.30	45.65	2.58	117.63	2.44	0.17	0.82
45.22	121.80	46.89	2.48	116.41	2.42	0.17	0.82
45.29	126.81	49.39	2.31	113.85	2.39	0.18	0.83
45.37	127.39	49.58	2.29	113.62	2.38	0.18	0.83
45.41	121.05	46.22	2.52	116.55	2.43	0.17	0.82
45.47	104.45	37.79	3.42	129.14	2.56	0.15	0.80
45.56	77.30	26.53	5.19	137.64	2.74	0.12	0.62
45.62	62.02	21.06	6.71	141.24	2.86	0.11	0.62
45.70	49.06	16.42	8.59	141.00	2.99	0.10	0.62
45.75	44.53	14.79	9.54	141.06	3.04	0.10	1.06
45.81	35.29	11.50	12.52	143.95	3.19	0.09	0.82
45.90	36.39	11.86	11.82	140.28	3.16	0.09	0.85
45.95	41.62	13.69	9.97	136.54	3.07	0.09	0.98
46.01	51.57	17.19	7.48	128.61	2.92	0.10	0.62
46.10	61.73	20.73	5.76	119.34	2.79	0.11	0.62
46.15	63.94	21.48	5.48	117.70	2.77	0.11	0.62
46.21	66.55	22.37	5.19	116.01	2.74	0.11	0.62
46.29	70.98	23.88	4.85	115.82	2.71	0.12	0.62
46.33	73.09	24.59	4.73	116.27	2.70	0.12	0.62
46.41	79.42	26.80	4.29	115.03	2.66	0.12	0.62
46.47	83.85	28.60	4.03	115.28	2.63	0.13	0.63
46.53	85.04	29.53	3.59	106.09	2.58	0.13	0.78
46.59	86.46	30.52	3.23	98.55	2.53	0.13	0.78
46.66	89.17	31.55	3.17	100.12	2.53	0.13	0.78
46.75	93.69	33.34	3.05	101.73	2.51	0.13	0.79
46.79	95.10	33.86	3.03	102.65	2.51	0.13	0.79
46.85	93.89	33.09	3.19	105.46	2.53	0.13	0.79
46.92	94.09	33.06	3.21	106.24	2.53	0.13	0.79
47.00	99.52	35.46	2.94	104.42	2.49	0.14	0.79
47.05	99.32	35.31	2.96	104.54	2.50	0.14	0.79
47.12	97.51	34.43	3.05	104.99	2.51	0.14	0.79
47.20	94.19	32.86	3.22	105.81	2.53	0.13	0.79
47.26	90.87	31.36	3.38	106.04	2.55	0.13	0.78

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)							
Depth (ft)	q _t (tsf)	Q _{tn}	K _c	Q _{tn,cs}	I _c	S _{u(liq)} /σ' _v	S _{u(peak)} /σ' _v
47.32	87.66	29.95	3.54	106.15	2.58	0.13	0.78
47.39	83.03	27.96	3.78	105.70	2.60	0.12	0.62
47.47	78.10	25.85	4.07	105.19	2.64	0.12	0.62
47.51	72.27	23.66	4.57	108.14	2.69	0.12	0.62
47.59	63.53	20.64	5.52	113.88	2.77	0.11	0.62
47.65	57.08	18.42	6.42	118.29	2.84	0.11	0.62
47.71	53.37	17.13	7.21	123.44	2.90	0.10	0.62
47.79	44.52	14.10	9.11	128.38	3.02	0.10	1.01
47.85	41.71	13.13	9.90	130.01	3.06	0.09	0.94
47.91	38.79	12.12	10.87	131.81	3.11	0.09	0.87
48.00	50.76	16.14	7.67	123.81	2.93	0.10	0.62
48.05	68.35	22.05	5.14	113.34	2.74	0.11	0.62
48.10	100.33	35.01	2.86	100.03	2.48	0.14	0.79
48.19	147.58	57.81	1.64	94.71	2.21	0.18	0.84
48.25	163.07	65.70	1.48	97.46	2.14	0.20	0.85
48.30	170.10	69.30	1.43	99.44	2.11	0.22	0.85
48.39	182.88	76.16	1.36	103.47	2.05	0.23	0.86
48.43	186.40	78.04	1.34	104.80	2.04	0.24	0.86
48.50	192.03	80.75	1.33	107.35	2.03	0.25	0.86
48.59	195.35	82.01	1.33	109.08	2.03	0.26	0.86
48.64	196.46	82.39	1.33	109.60	2.03	0.27	0.87
48.70	197.36	82.72	1.33	109.92	2.02	0.27	0.87
48.79	196.06	81.85	1.33	109.15	2.03	0.27	0.87
48.83	194.76	81.11	1.34	108.51	2.03	0.26	0.86
48.89	192.95	80.14	1.34	107.47	2.04	0.26	0.86
48.95	189.23	78.12	1.35	105.68	2.05	0.25	0.86
49.02	185.51	76.09	1.37	103.95	2.06	0.24	0.86
49.11	177.66	71.88	1.40	100.73	2.09	0.23	0.86
49.19	172.34	68.94	1.44	98.94	2.11	0.22	0.85
49.22	168.52	66.88	1.46	97.84	2.13	0.21	0.85
49.28	162.69	63.77	1.51	96.36	2.15	0.20	0.85
49.35	155.65	60.19	1.57	94.53	2.18	0.19	0.84
49.42	149.42	57.05	1.63	93.25	2.21	0.19	0.84
49.48	143.29	53.96	1.71	92.40	2.24	0.18	0.83
49.56	135.75	50.08	1.85	92.88	2.28	0.17	0.83
49.63	132.33	48.39	1.91	92.58	2.30	0.17	0.82
49.68	129.31	47.34	1.89	89.38	2.29	0.16	0.82
49.74	127.40	46.16	1.97	90.87	2.31	0.16	0.82
49.83	125.20	44.82	2.06	92.55	2.33	0.16	0.82
49.87	122.79	43.59	2.14	93.34	2.35	0.16	0.81
49.97	118.97	41.54	2.30	95.52	2.39	0.15	0.81
50.03	119.07	41.46	2.32	96.18	2.39	0.15	0.81
50.08	118.56	37.32	54.25	2024.40	4.06	0.19	2.67
50.14	119.17	37.49	54.25	2033.57	4.06	0.19	2.68
50.23	120.17	37.76	54.25	2048.22	4.06	0.19	2.70
50.27	120.98	38.00	54.25	2061.37	4.06	0.19	2.71
50.33	122.18	38.35	54.25	2080.38	4.06	0.20	2.74
50.41	124.40	39.02	54.25	2116.86	4.06	0.20	2.79

:: Strength loss calculation (Idriss & Boulanger (2008)) :: (continued)

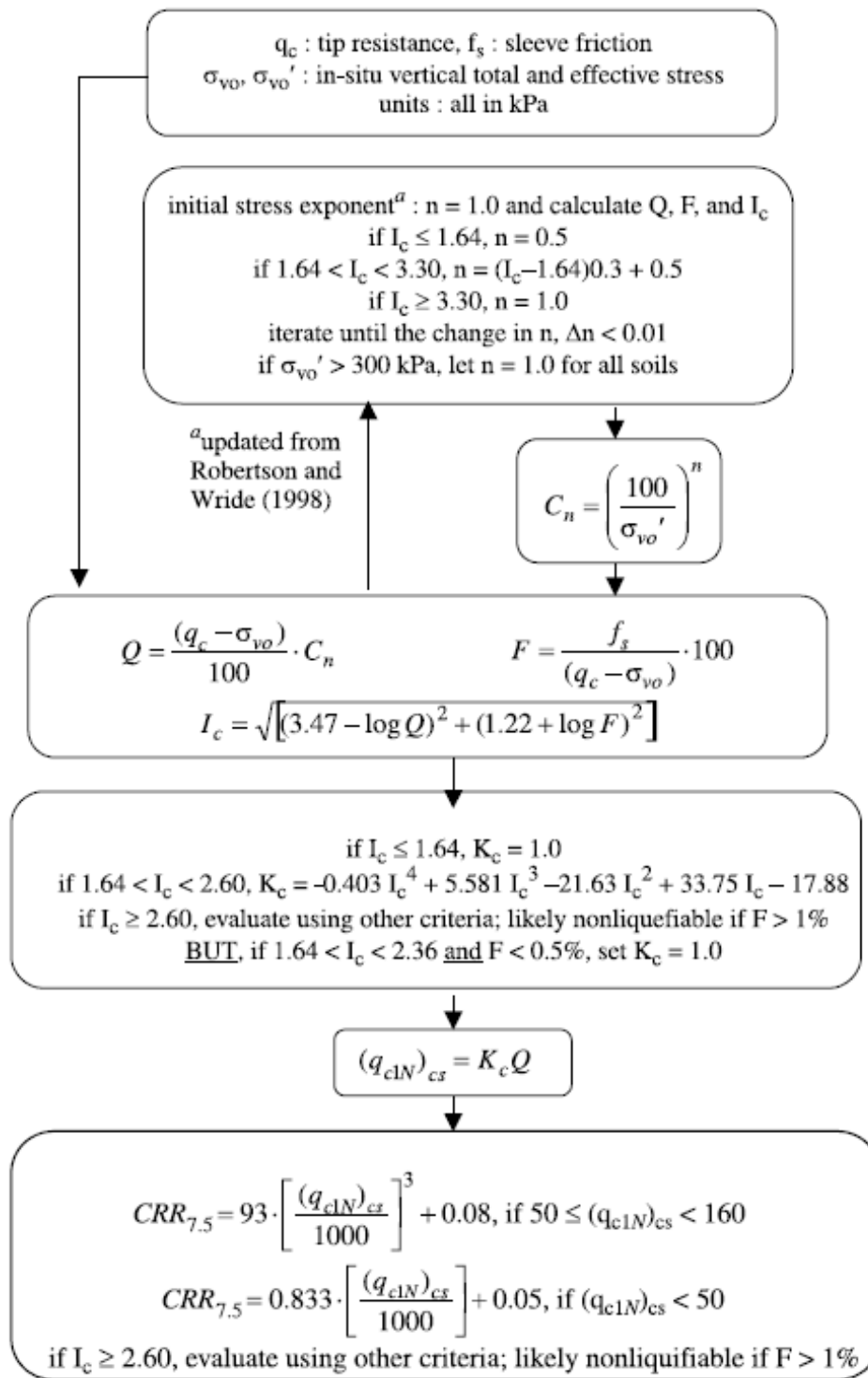
Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
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Abbreviations

q_t :	Total cone resistance
K_c :	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c :	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Procedure for the evaluation of soil liquefaction resistance, NCEER (1998)

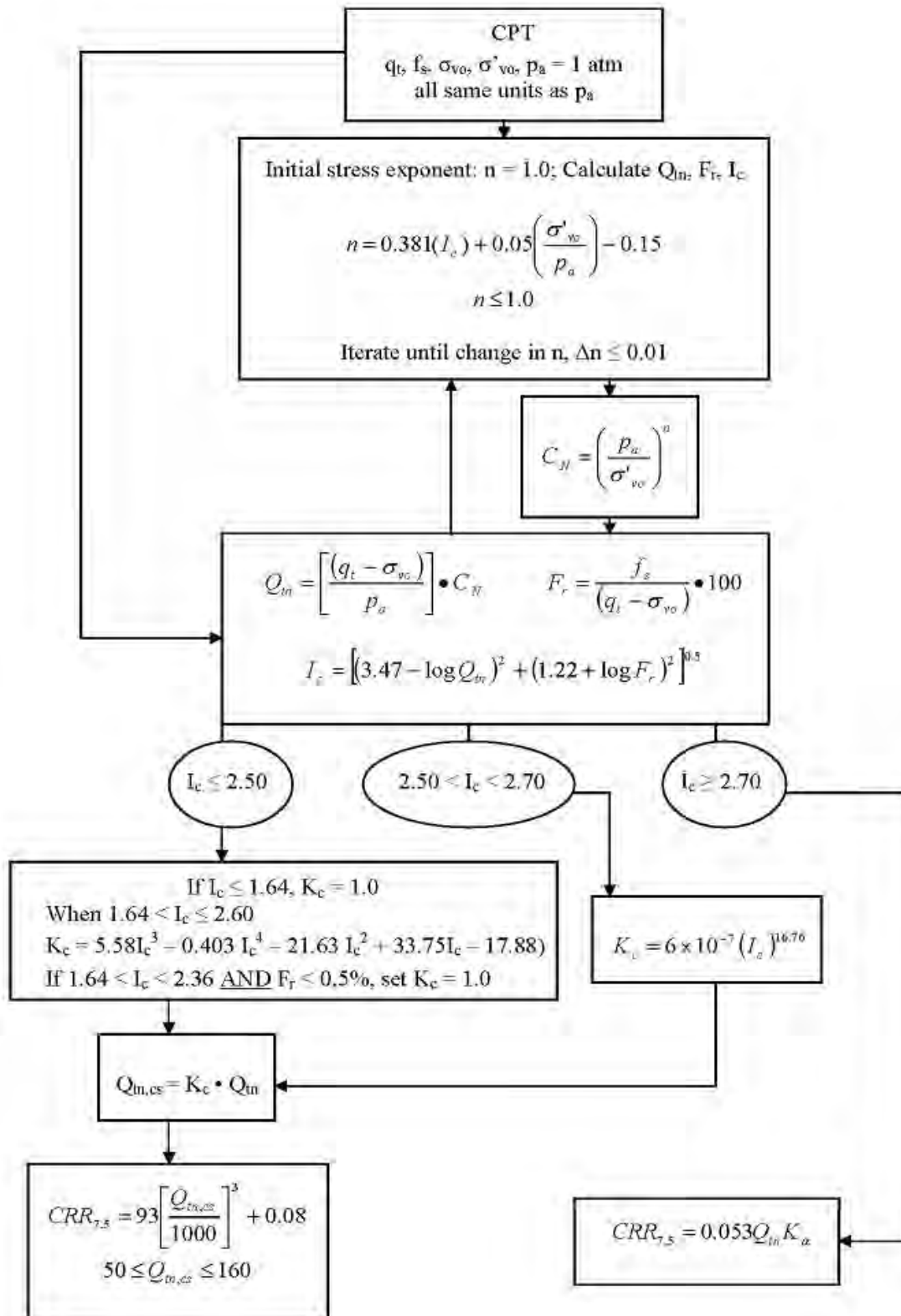
Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. The procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart¹:



¹ "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

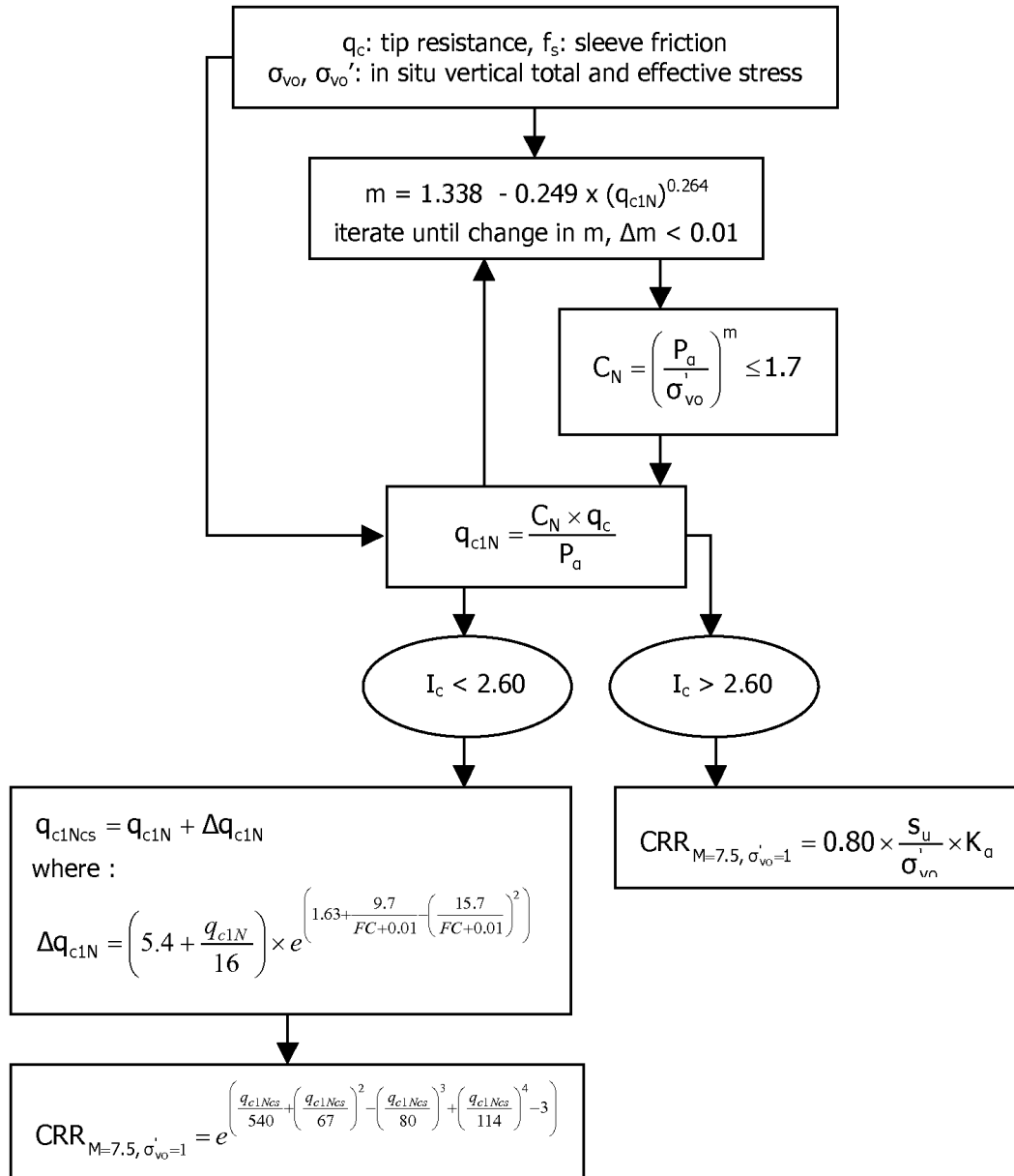
Procedure for the evaluation of soil liquefaction resistance (all soils), Robertson (2010)

Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. This procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart¹:

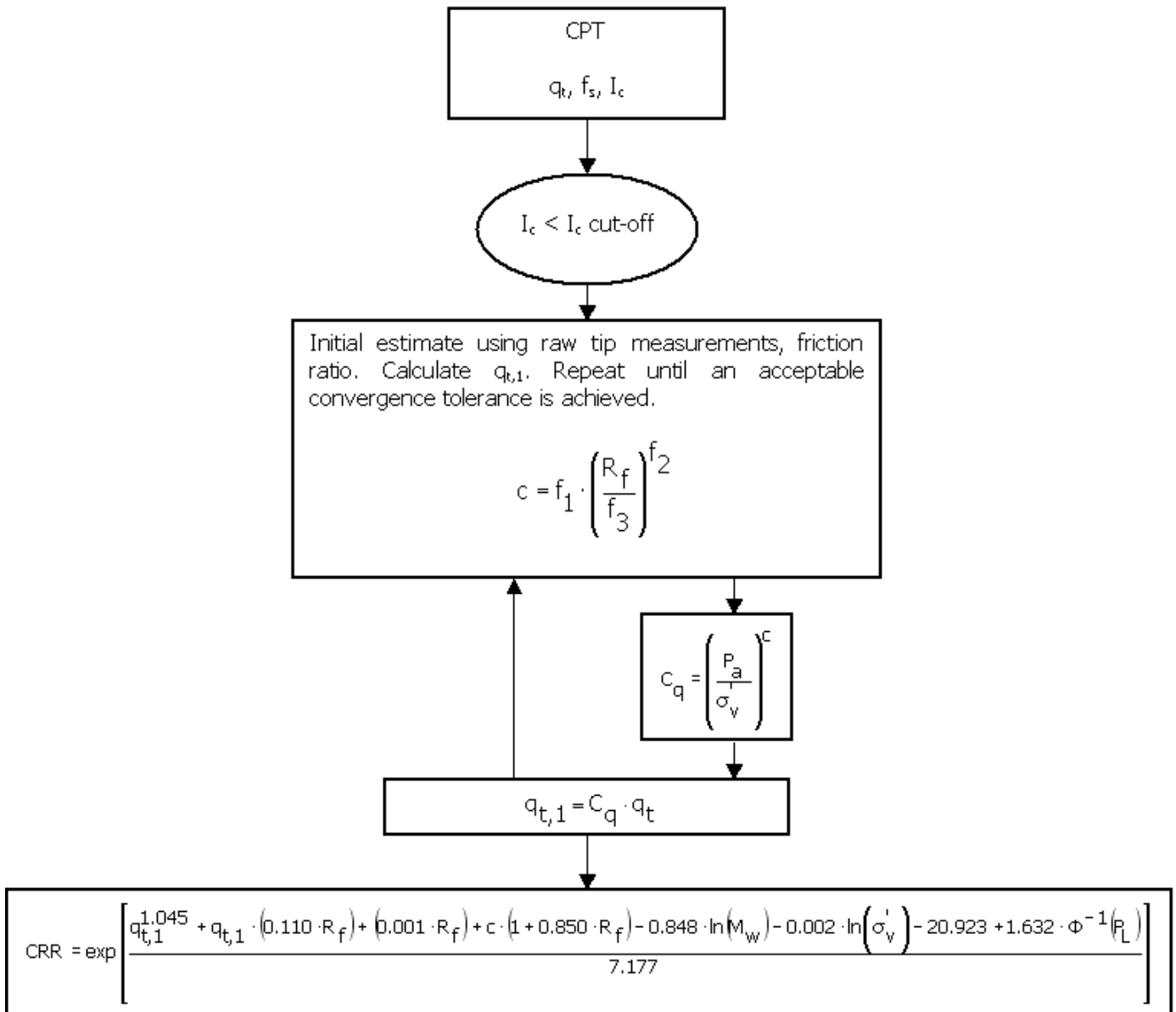


¹ P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering – from case history to practice, IS-Tokyo, June 2009

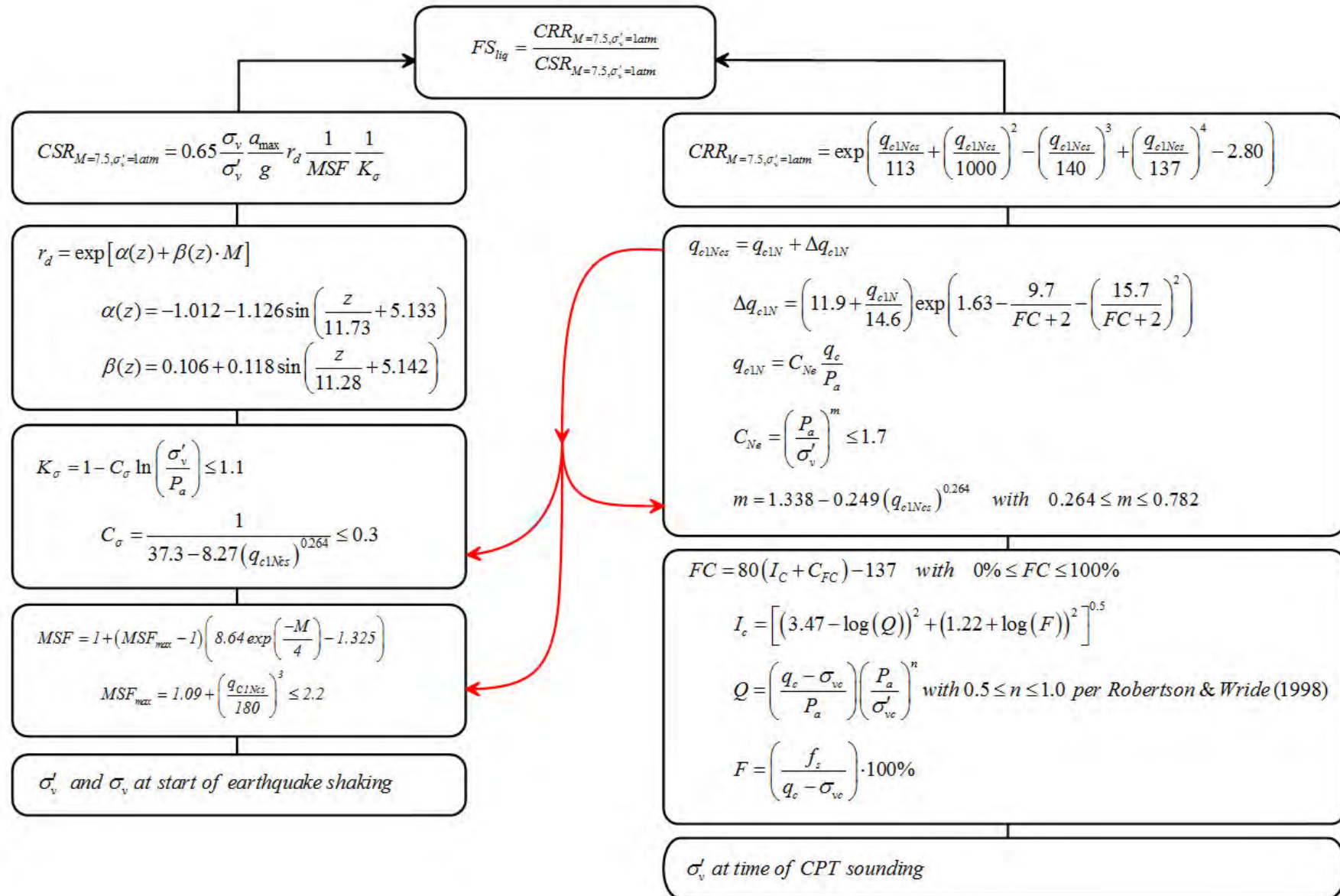
Procedure for the evaluation of soil liquefaction resistance, Idriss & Boulanger (2008)



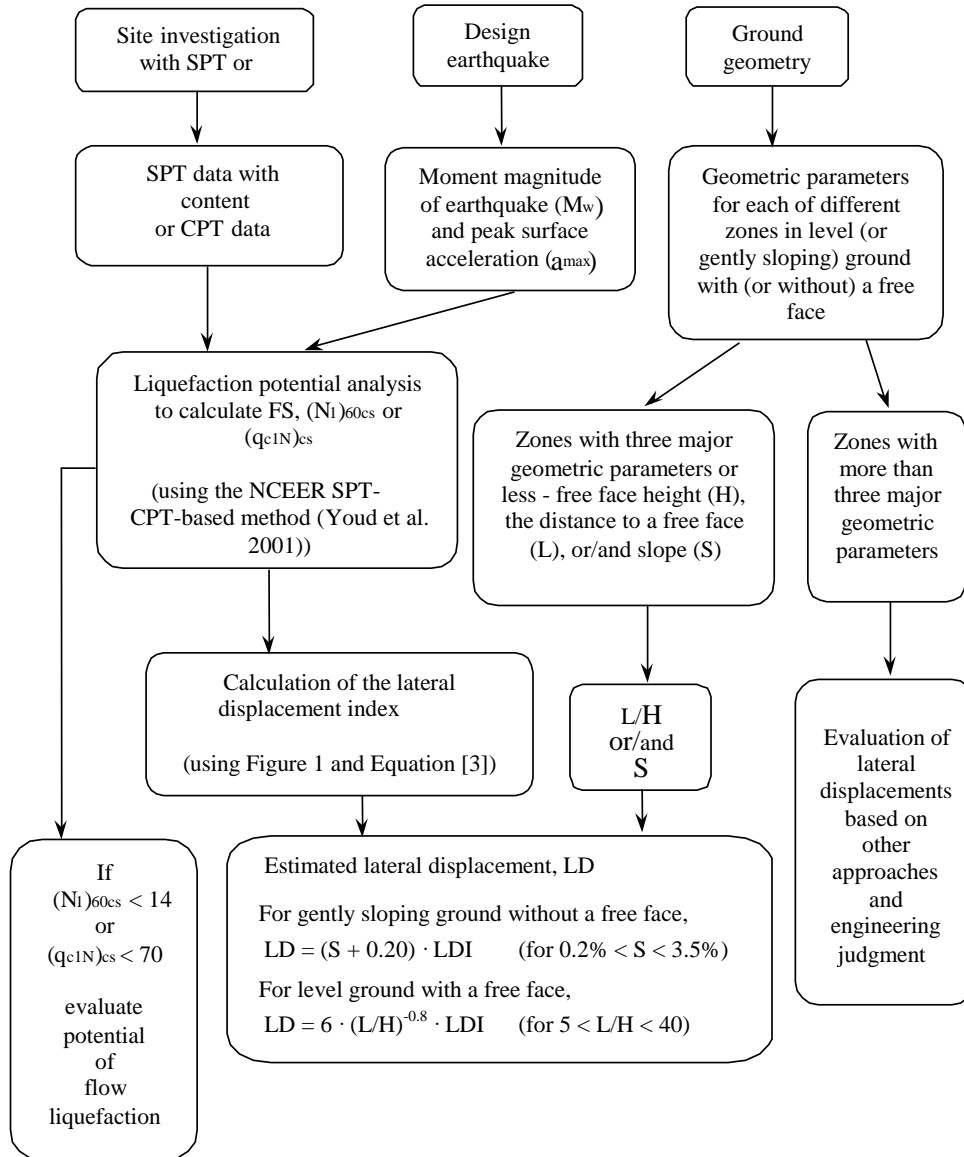
Procedure for the evaluation of soil liquefaction resistance (sandy soils), Moss et al. (2006)



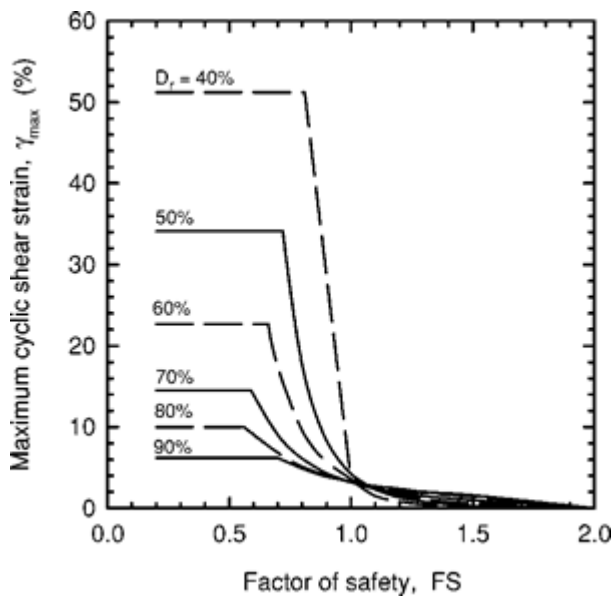
Procedure for the evaluation of soil liquefaction resistance, Boulanger & Idriss(2014)



Procedure for the evaluation of liquefaction-induced lateral spreading displacements



¹ Flow chart illustrating major steps in estimating liquefaction-induced lateral spreading displacements using the proposed approach



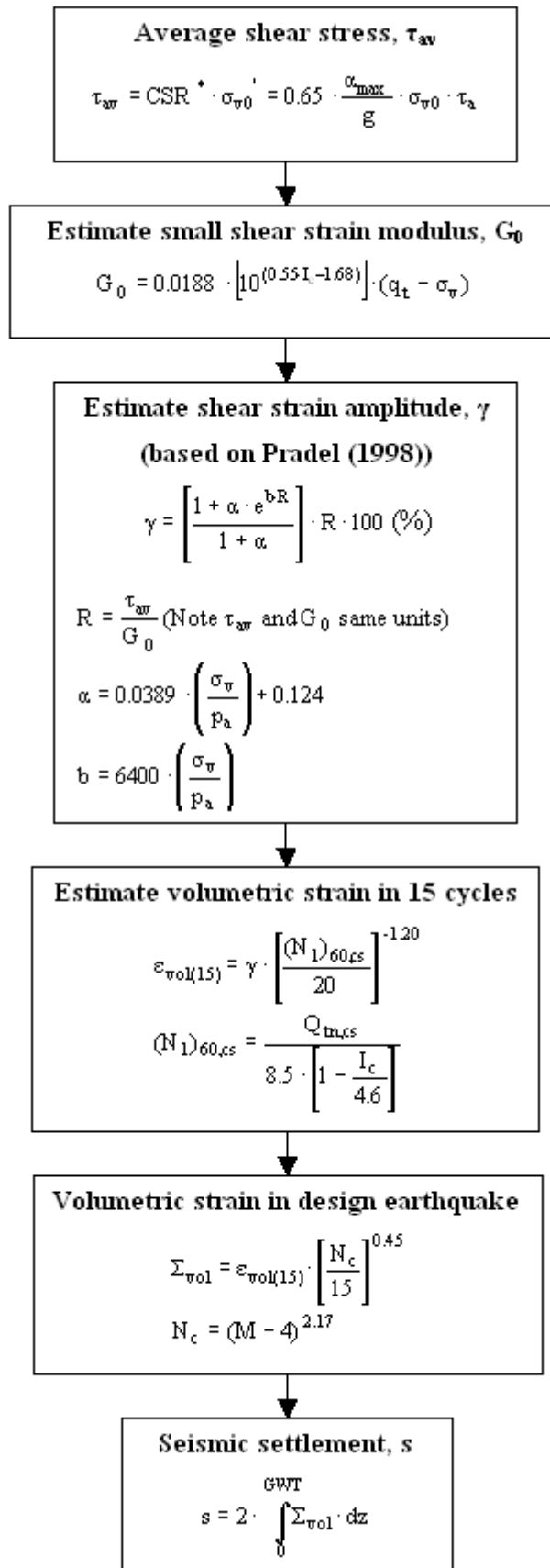
¹ Figure 1

$$LDI = \int_0^{Z_{max}} \gamma_{max} dz$$

¹ Equation [3]

¹ "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

Procedure for the estimation of seismic induced settlements in dry sands



Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, Symposium in honor of professor I. M. Idriss, San Diego, CA

Liquefaction Potential Index (LPI) calculation procedure

Calculation of the Liquefaction Potential Index (LPI) is used to interpret the liquefaction assessment calculations in terms of severity over depth. The calculation procedure is based on the methodology developed by Iwasaki (1982) and is adopted by AFPS.

To estimate the severity of liquefaction extent at a given site, LPI is calculated based on the following equation:

$$LPI = \int_0^{20} (10 - 0,5z) \times F_L \times d_z$$

where:

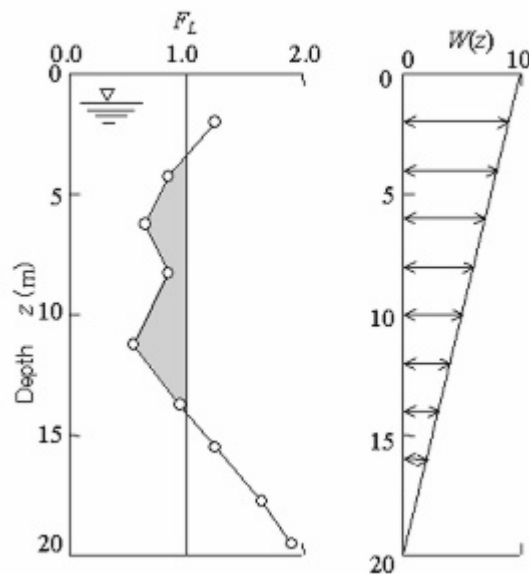
$F_L = 1$ - F.S. when F.S. less than 1

$F_L = 0$ when F.S. greater than 1

z depth of measurement in meters

Values of LPI range between zero (0) when no test point is characterized as liquefiable and 100 when all points are characterized as susceptible to liquefaction. Iwasaki proposed four (4) discrete categories based on the numeric value of LPI:

- LPI = 0 : Liquefaction risk is very low
- $0 < LPI \leq 5$: Liquefaction risk is low
- $5 < LPI \leq 15$: Liquefaction risk is high
- LPI > 15 : Liquefaction risk is very high



Graphical presentation of the LPI calculation procedure

Shear-Induced Building Settlement (Ds) calculation procedure

The shear-induced building settlement (Ds) due to liquefaction below the building can be estimated using the relationship developed by Bray and Macedo (2017):

$$\begin{aligned} \ln(D_s) = & c_1 + c_2 * LBS + 0.58 * \ln\left(\tanh\left(\frac{HL}{6}\right)\right) + \\ & 4.59 * \ln(Q) - 0.42 * \ln(Q)^2 - 0.02 * B + \\ & 0.84 * \ln(CAVdp) + 0.41 * \ln(Sa1) + \varepsilon \end{aligned}$$

where Ds is in the units of mm, c1= -8.35 and c2= 0.072 for LBS ≤ 16, and c1= -7.48 and c2= 0.014 otherwise. Q is the building contact pressure in units of kPa, HL is the cumulative thickness of the liquefiable layers in the units of m, B is the building width in the units of m, CAVdp is a standardized version of the cumulative absolute velocity in the units of g-s, Sa1 is 5%-damped pseudo-acceleration response spectral value at a period of 1 s in the units of g, and ε is a normal random variable with zero mean and 0.50 standard deviation in Ln units. The liquefaction-induced building settlement index (LBS) is:

$$LBS = \sum W * \frac{\varepsilon_{shear}}{z} dz$$

where z (m) is the depth measured from the ground surface > 0, W is a foundation-weighting factor wherein W = 0.0 for z less than Df, which is the embedment depth of the foundation, and W = 1.0 otherwise. The shear strain parameter (ε_{shear}) is the liquefaction-induced free-field shear strain (in %) estimated using Zhang et al. (2004). It is calculated based on the estimated Dr of the liquefied soil layer and the calculated safety factor against liquefaction triggering (FSL).

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APPENDIX D

Infiltration Testing

Falling Head Borehole Infiltration Test

Project Name:	Compton College Student Housing Project	Date:	1/4/2023
Project Number:	4230.2200025.0000	Tested By:	JK
Test Hole Number:	P-2	USCS Soil Classification:	SC-SM
Total Depth :	10.06	Water Temperature:	68 °F
Test Hole Diameter:	8.00 inches	radius=	4 inches
Note:			

Test No.	Start Time	End Time	ΔT	Total Time	Initial Depth of Water	Final Depth of Water	H_0	H_r	ΔH	H_{avg}	Unfactored Percolation Rate
			(min)	(min)	(ft)	(ft)	(in)	(in)	(in)	(in)	(in/hour)
1	8:57	9:12	15.0	15.0	8.05	10.06	24.12	0.00	24.12	12.06	13.72
2	9:14	9:29	15.0	30.0	6.76	8.22	39.60	22.08	17.52	30.84	4.27
3	9:31	9:46	15.0	45.0	6.70	8.20	40.32	22.32	18.00	31.32	4.32
4	9:50	10:05	15.0	60.0	6.65	8.00	40.92	24.72	16.20	32.82	3.72
5	10:20	10:35	15.0	75.0	6.68	8.02	40.56	24.48	16.08	32.52	3.73
6	10:40	10:55	15.0	90.0	6.68	8.00	40.56	24.72	15.84	32.64	3.66
7	10:56	11:11	15.0	105.0	6.71	8.02	40.20	24.48	15.72	32.34	3.66
8	11:14	11:29	15.0	120.0	6.70	8.00	40.32	24.72	15.60	32.52	3.62
9	11:32	11:47	15.0	135.0	6.66	7.97	40.80	25.08	15.72	32.94	3.60
10	11:49	12:04	15.0	150.0	6.70	7.99	40.32	24.84	15.48	32.58	3.58
11	12:07	12:22	15.0	165.0	6.72	7.99	40.08	24.84	15.24	32.46	3.54
12	12:24	12:39	15.0	180.0	6.74	8.00	39.84	24.72	15.12	32.28	3.53

WATER TEMPERATURE CORRECTION FACTOR:	0.92
SAFETY FACTOR*:	2.25
UNFACTORED INFILTRATION RATE (IN/HR):	3.37
FACTORED INFILTRATION RATE (IN/HR):	1.50

Falling Head Borehole Infiltration Test

Project Name:	Compton College Student Housing Project	Date:	1/4/2023
Project Number:	4230.2200025.0000	Tested By:	JK
Test Hole Number:	P-3	USCS Soil Classification:	SC-SM
Total Depth :	9.75	Water Temperature:	68 °F
Test Hole Diameter:	8.00 inches	radius=	4 inches

Test No.	Start Time	End Time	ΔT	Total Time	Initial Depth of Water	Final Depth of Water	H_0	H_r	ΔH	H_{avg}	Unfactored Percolation Rate
			(min)	(min)	(ft)	(ft)	(in)	(in)	(in)	(in)	(in/hour)
1	8:55	9:10	15.0	15.0	7.99	10.20	21.12	-5.40	26.52	7.86	21.52
2	9:11	9:26	15.0	30.0	6.39	7.72	40.32	24.36	15.96	32.34	3.72
3	9:28	9:43	15.0	45.0	6.23	7.42	42.24	27.96	14.28	35.10	3.08
4	9:46	10:01	15.0	60.0	6.33	7.29	41.04	29.52	11.52	35.28	2.47
5	10:18	10:33	15.0	75.0	6.30	7.26	41.40	29.88	11.52	35.64	2.45
6	10:38	10:53	15.0	90.0	6.22	7.12	42.36	31.56	10.80	36.96	2.22
7	10:54	11:09	15.0	105.0	6.30	7.19	41.40	30.72	10.68	36.06	2.24
8	11:10	11:25	15.0	120.0	6.27	7.16	41.76	31.08	10.68	36.42	2.22
9	11:28	11:43	15.0	135.0	6.29	7.15	41.52	31.20	10.32	36.36	2.15
10	11:45	12:00	15.0	150.0	6.29	7.17	41.52	30.96	10.56	36.24	2.21
11	12:03	12:18	15.0	165.0	6.24	7.20	42.12	30.60	11.52	36.36	2.40
12	12:20	12:35	15.0	180.0	6.27	7.16	41.76	31.08	10.68	36.42	2.22

WATER TEMPERATURE CORRECTION FACTOR:	0.92
SAFETY FACTOR*:	2.25
UNFACTORED INFILTRATION RATE (IN/HR):	2.04
FACTORED INFILTRATION RATE (IN/HR):	0.91



APPENDIX E

Standard Grading Specifications

RECOMMENDED EARTHWORK SPECIFICATIONS

The following specifications are recommended to provide a basis for quality control during the placement of compacted fill or backfill as applicable.

1. Areas that are to receive compacted fill shall be observed by Soil/Geotechnical Engineer (GE) or his/her representative prior to the placement of fill.
2. All drainage devices shall be properly installed and observed by GE and/or owner's representative(s) prior to placement of backfill.
3. Fill soils shall consist of imported soils or on-site soils free of organics, cobbles, and deleterious material provided each material is approved by GE. GE shall evaluate and/or test the import material for its conformance with the report recommendations prior to its delivery to the site. The contractor shall notify GE 72 hours prior to importing material to the site.
4. Fill shall be placed in controlled layers (lifts), the thickness of which is compatible with the type of compaction equipment used. The fill materials shall be brought to optimum moisture content or above, thoroughly mixed during spreading to obtain a near uniform moisture condition and uniform blend of materials, and then placed in layers with a thickness (loose) not exceeding 8 inches. Each layer shall be compacted to a minimum compaction of 90% relative to the maximum dry density determined per the latest ASTM D1557 test. Density testing shall be performed by GE to verify relative compaction. The contractor shall provide proper access and level areas for testing.
5. Rocks or rock fragments less than eight (8) inches in the largest dimension may be utilized in the fill, provided they are not placed in concentrated pockets, except rocks larger than four (4) inches shall not be placed within three (3) feet of finish grade.
6. Rocks greater than eight (8) inches in largest dimension shall be taken offsite or placed in accordance with the recommendation of the Soils Engineer in areas designated as suitable for rock disposal.
7. Where space limitations do not allow for conventional fill compaction operations, special backfill materials and procedures may be required. Pea gravel or other select fill can be used in areas of limited space. A sand and Portland cement slurry (2 sacks per cubic-yard mix) shall be used in limited space areas for shallow backfill near final pad grade, and pea gravel shall be placed in deeper backfill near drainage systems.
8. GE shall observe the placement of fill and conduct in-place field density tests on the compacted fill to check for adequate moisture content and the required relative compaction. Where less than specified relative compaction is indicated, additional compacting effort shall be applied and the soil moisture conditioned as necessary until adequate relative compaction is attained.
9. The Contractor shall comply with the minimum relative compaction out to the finish slope face of fill slopes, buttresses, and stabilization fills as set forth in the specifications for compacted

fill. This may be achieved by either overbuilding the slope and cutting back as necessary, or by direct compaction of the slope face with suitable equipment, or by any other procedure that produces the required result.

10. Any abandoned underground structures such as cesspools, cisterns, mining shafts, tunnels, septic tanks, wells, pipelines, or others not discovered prior to grading are to be removed or treated to the satisfaction of the Soils Engineer and/or the controlling agency for the project.
11. The Contractor shall have suitable and sufficient equipment during a particular operation to handle the volume of fill being placed. When necessary, fill placement equipment shall be shut down temporarily in order to permit proper compaction of fills, correction of deficient areas, or to facilitate required field-testing.
12. The Contractor shall be responsible for the satisfactory completion of all earthwork in accordance with the project plans and specifications.
13. Final reports shall be submitted after completion of earthwork and after the Soils Engineer and Engineering Geologist have finished their observations of the work. No additional excavation or filling shall be performed without prior notification to the Soils Engineer and/or Engineering Geologist.
14. Whenever the words “supervision”, “inspection” or “control” are used, they shall mean observation of the work and/or testing of the compacted fill by GE to assess whether substantial compliance with plans, specifications and design concepts has been achieved, and does not include direction of the actual work of the contractor or the contractor’s workmen.

RECOMMENDED SPECIFICATIONS
FOR PLACEMENT OF TRENCH BACKFILL

1. Trench excavations to receive backfill shall be free of trash, debris, or other unsatisfactory materials prior to backfill placement, and shall be observed by project soil/geotechnical engineer (GE) representative.
2. Except as stipulated herein, soils obtained from the excavation may be used as backfill if they are essentially free of organics and deleterious materials.
3. Rocks generated from the trench excavation not exceeding three (3) inches in largest dimension may be used as backfill material. However, such material may not be placed within 12 inches of the top of the pipeline. No more than 30 percent of the backfill volume shall contain particles larger than 1-½ inches in diameter, and rocks shall be well mixed with finer soil.
4. Soils (other than aggregates) with a Sand Equivalent (SE) greater than or equal to 30, as determined by ASTM D2419 Standard Test Method or at the discretion of the engineer or representative in the field, may be used for bedding and shading material in the pipe zone areas. These soils are considered satisfactory for compaction by jetting procedures.
5. No jetting will be permitted in utility trenches within the top 2 feet of the subgrade of concrete slabs-on-grade.
6. Trench backfill other than bedding and shading shall be compacted by mechanical methods as tamping sheepsfoot, vibrating or pneumatic rollers or other mechanical tampers to achieve the density specified herein. The backfill materials shall be brought to optimum moisture content or above, thoroughly mixed during spreading to obtain a near uniform moisture condition and uniform blend of materials, and then placed in horizontal layers with a thickness (loose) not exceeding 8 inches. Trench backfills shall be compacted to a minimum compaction of 90 percent relative to the maximum dry density determined per the latest ASTM D1557 test.
7. The contractor shall select the equipment and process to be used to achieve the specified density without damage to the pipeline, the adjacent ground, existing improvements or completed work.
8. Observations and field tests shall be carried on during construction by GE to confirm that the required degree of compaction has been obtained. Where compaction is less than that specified, additional compaction effort shall be made with adjustment of the moisture content as necessary until the specified compaction is obtained. Field density tests may be omitted at the discretion of the engineer or his representative in the field.
9. Whenever, in the opinion of GE or the Owner's Representative(s), an unstable condition is being created, either by cutting or filling, the work shall not proceed until an investigation has been made and the excavation plan revised, if deemed necessary.

10. Fill material shall not be placed, spread, or rolled during unfavorable weather conditions. When the work is interrupted by heavy rain, fill operations shall not be resumed until field tests by GE indicate the moisture content and density of the fill are as specified.
11. Whenever the words “supervision”, “inspection”, or “control” are used, they shall mean observation of the work and/or testing of the compacted fill by GE to assess whether substantial compliance with plans, specifications and design concepts has been achieved.

APPENDIX F
Site Specific Ground Motion Analysis

RISK TARGETED (MCE_R) GROUND MOTION HAZARD ANALYSIS
PROPOSED COMPTON COLLEGE STUDENT HOUSING
1111 EAST ARTESIA BOULEVARD
COMPTON, CALIFORNIA

UES has conducted a site-specific risk targeted ground motion hazard analysis for the proposed Compton College Student Housing in accordance with Chapter 21 of ASCE/SEI 7-16, the California Building Code (CBC), and USGS Ground Acceleration Maps.

Probabilistic ground motions were calculated using the USGS Unified Hazard Tool. This program enabled the calculation of Risk Targeted Ground Motion (RTGM) values in accordance with ASCE 21.2.1.2 Method 2. In order to represent the maximum response in the horizontal plane, the spectral response accelerations obtained with the RTGM calculator were scaled by appropriate factors to increase the motions to the maximum directional response, as specified in ASCE 21.2. The probabilistic MCE_R analysis data represent a two-percent probability of exceedance in fifty years.

Deterministic MCE_R ground motions were calculated using the NGAWest2 GMPE online worksheet provided by the Pacific Earthquake Engineering Research Center. Five NGA-West2 horizontal ground motion prediction equations were developed as part of the program.

Input variables were determined from UCERF3 fault parameters and magnitude-area relationships. Seismic sources were characterized by location, fault mechanism, geometry, probability of activity, magnitude recurrence distribution, and deterministic magnitude. As indicated on the GMPE worksheet NGA relationships used for the response analysis account for site-specific soil affects. Equally weighted NGA West 2 relationships by Abrahamson, et al. (2014), Boore, et al. (2014), Campbell and Bozorgnia (2014), and Chiou and Youngs (2014) were used for the analysis. As required, the 84th-percentile spectral acceleration values were averaged to conservatively calculate the deterministic spectral accelerations (in lieu of 150 percent of the median spectral accelerations).

Based on site location and information from USGS deaggregation and Earthquake Scenario Maps, a conservative controlling magnitude of 7.3, associated with the proximal segment of the Newport Inglewood Fault Zone, was assigned for the deterministic analysis. Shear wave velocity data based on site conditions within the upper 30 meters were input into the online calculators, as appropriate. The shear wave data were obtained based on direct measurement at four separate exploration locations during the site CPT advancements. Based on the field measurements, an average shear wave velocity of 849.4 feet/second (258.9 meters/second) was obtained. Based on noted subsurface conditions and site resistance data, Site Class D is considered appropriate and a shear wave velocity value of 259 meters per second was assigned for the risk targeted ground motion calculations, as permitted by the Unified Hazard Tool. Using regional geologic map relationships and geophysical evaluations of the Los Angeles Basin (Ma and Clayton), the depths to shear wave velocity of 1,000 m/s ($Z_{1.0}$) and 2,500 m/s ($Z_{2.5}$) appear to be on the order of 0.9 kilometers and 4.5 kilometers, respectively. Evaluation input data are attached.

In order to represent the maximum response in the horizontal plane, the spectral response accelerations obtained with the GMPE calculator were scaled by appropriate factors to increase the motions to the maximum direction response, as specified in ASCE 21.2.

In accordance with ASCE 7-16 Supplement No. 1 section 21.2.2, if the largest spectral response acceleration of the resulting deterministic ground motion response spectrum is less than $1.5 F_a$, then this response spectrum shall be scaled by a single factor such that the maximum response spectral acceleration equals $1.5 F_a$. Based on the deterministic output, the largest spectral value exceeded $1.5 F_a$ and the additional spectrum scaling was not required in this case.

Deterministic maximum considered earthquake (MCE) lower limit spectral response acceleration values were determined based on ASCE 7 Figure 21.2-1.

The site-specific MCE spectral response acceleration at any period is taken as the lesser of the scaled maximum-directional spectral response accelerations from the probabilistic MCE and the deterministic MCE. The design spectral response acceleration at any period is calculated as $2/3$ of the corresponding ordinate from the site-specific MCE, which should not be less than 80 percent of the spectral response acceleration from the design response spectrum determined in accordance with ASCE 7 Section 11.4.5.

The probabilistic MCE, max-direction scalar and adjusted probabilistic spectral acceleration ordinates are shown on Figure 1. The deterministic MCE, max direction scalar, F_a scalar, and the deterministic lower limit on MCE response spectra are shown on Figure 2. The site-specific MCE response spectrum, $2/3$ of site-specific MCE response spectrum, and 80 percent of NEHRP/ASCE design response spectrum are shown on Figure 3. The site-specific design response spectrum is presented on Figure 4 and a summary of spectral acceleration data is shown on the attached spreadsheet.

In Accordance with section 21.4 of ASCE/SEI 7-16, the resulting site-specific acceleration parameters are shown below. ASCE Section 21.4 states that the parameter S_{DS} shall be taken as 90 percent of the maximum spectral acceleration, S_a , obtained from the site-specific spectrum, at any period within the range from 0.2 to 5 seconds, inclusive. The value at 0.5 seconds (1.234g) exceeded the other 90 percent values within the specified range. In addition, Section 21.4 requires that S_{D1} be taken as the maximum value of the product, TS_a , for periods from 1 to 5s based on the site shear wave velocity, V_{S30} . The maximum value of the product TS_a (1.091g) was obtained at a period of 2 seconds.

Code and site-specific parameters are provided below.

<u>Code-Based Seismic Values (ASCE 7-16)</u>	<u>Site Specific Ground Motion Values</u>
$S_{DS} = 1.129g$	$S_{DS} = 1.234g$
$S_{D1} = \text{null}$	$S_{D1} = 1.091g$
$S_{MS} = 1.693g$	$S_{MS} = 1.851g$
$S_{M1} = \text{null}$	$S_{M1} = 1.636g$
$PGA_M = 0.801g$	$PGA_M = 0.773g$

Project No. 4230.2200060
Project Name : CCCD
Site Address : Compton, CA
For :
Latitude : 33.8797
Longitude : -118.2097
V₃₀ : 259 m/s
Depth to Vs=1000m/s : 900 m

CBC Mapped Acceleration Parameters

Site Class	D		
S _s	1.693	T ₀	0.179
S ₁	0.606	T _s	0.895
F _a	1.000	T _L	8
F _v	2.5		
S _{MS}	1.693		
S _{M1}	1.515		
S _{DS}	1.129		
S _{D1}	1.010		

Site-Specific Design Parameters

	Design Parameters
S _{MS}	1.851
S _{M1}	1.636
S _{ds}	1.234
S _{d1}	1.091
PGAM	0.773

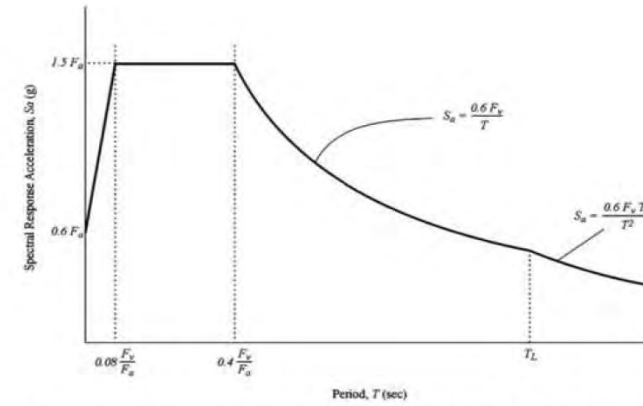


FIGURE 21.2-1 Deterministic Lower Limit on MCE_R Response Spectrum

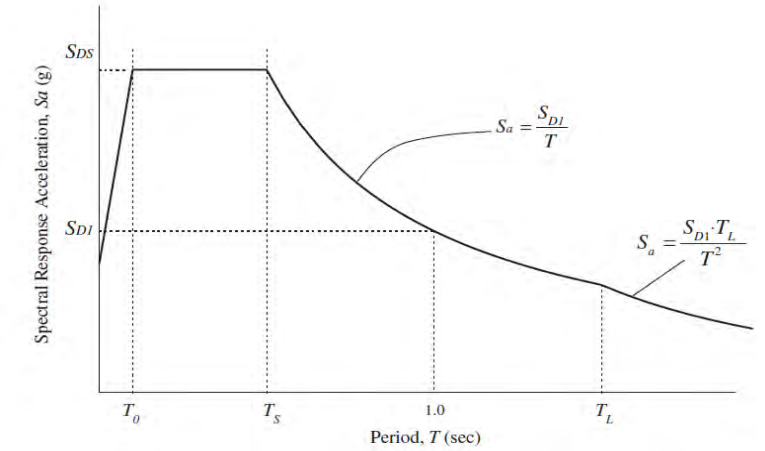


FIGURE 11.4-1 Design Response Spectrum

Period (sec)	Max. Direction Scale Factor	Probabilistic		Deterministic					Site Specific						
		RTGM (g)	Probabilistic MCE _R Spectral Acceleration (g)	84th-percentile Spectral Acceleration (g)	Max. Directional Deterministic SA	1.5*F _a Scaling (ASCE 7 Supplement 1)	Deterministic Lower Limit on MCE Response Spectrum ASCE 21.2-1	Deterministic MCE _R Spectral Acceleration (g)	Site Specific MCE _R Spectral Acceleration (g)	2/3 Site Specific MCE _R Spectral Acceleration (g)	ASCE 7-16 11.4-1 Design Response Spectrum	80% ASCE Design Response Spectrum	Site Specific Design Spectral Acceleration (g)	0.9 Design Response Spectrum (g)	Product of T _{sa} (T = 1.0 -5.0s)
0.001	1.1	0.737	0.811	0.717	0.789	0.789	0.600	0.789	0.789	0.526	0.455	0.364	0.526	--	--
0.100	1.1	1.264	1.390	1.068	1.175	1.175	1.050	1.175	1.175	0.783	0.830	0.664	0.783	--	--
0.200	1.1	1.685	1.854	1.476	1.624	1.624	1.500	1.624	1.624	1.082	1.129	0.903	1.082	0.974	--
0.300	1.125	1.859	2.091	1.739	1.956	1.956	1.500	1.956	1.956	1.304	1.129	0.903	1.304	1.174	--
0.500	1.175	1.75	2.056	1.801	2.116	2.116	1.500	2.116	2.056	1.371	1.129	0.903	1.371	1.234	--
0.750	1.2375	1.406	1.740	1.528	1.891	1.891	1.500	1.891	1.740	1.160	1.129	0.903	1.160	1.044	--
1.000	1.3	1.156	1.503	1.349	1.753	1.753	1.500	1.753	1.503	1.002	1.010	0.808	1.002	0.902	1.002
2.000	1.35	0.606	0.818	0.810	1.094	1.094	0.750	1.094	0.818	0.545	0.505	0.404	0.545	0.491	1.091
3.000	1.4	0.381	0.533	0.525	0.735	0.735	0.500	0.735	0.533	0.356	0.337	0.269	0.356	0.320	1.067
5.000	1.5	0.191	0.287	0.256	0.383	0.383	0.300	0.383	0.287	0.191	0.202	0.162	0.191	0.172	0.955

Figure 1: Probablistic Outputs

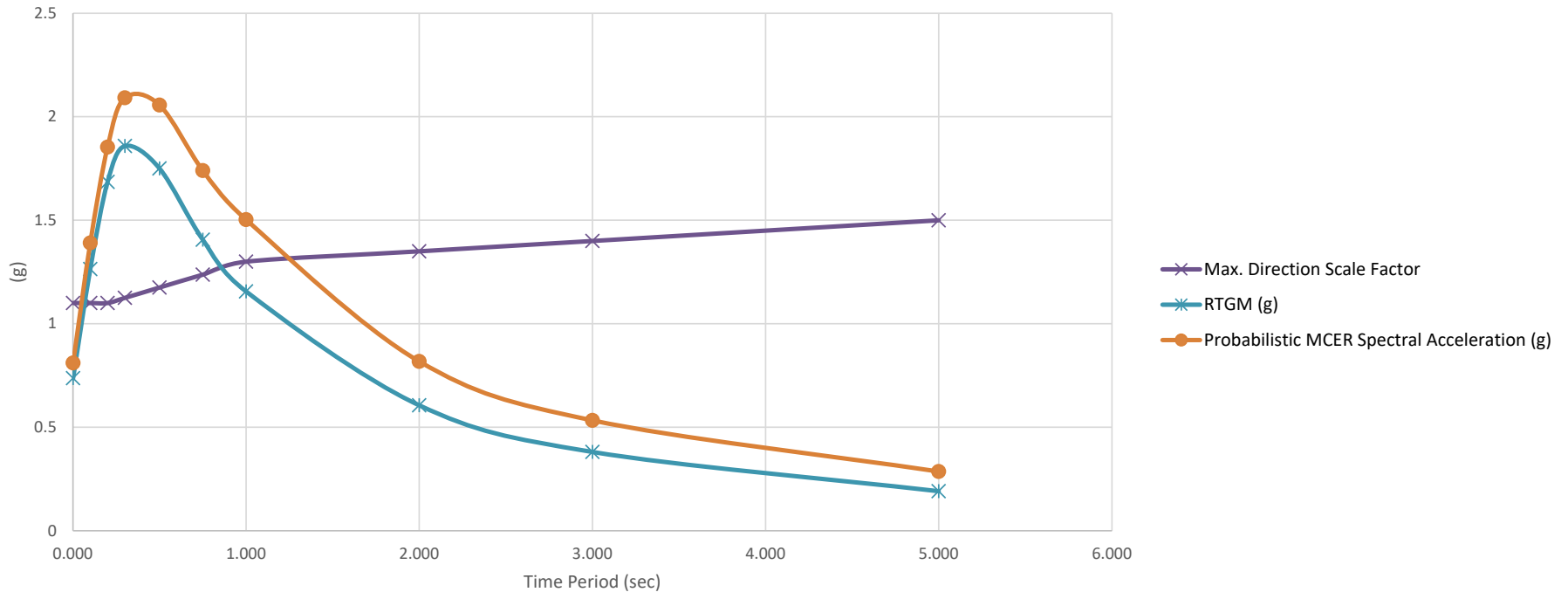


Figure 2: Deterministic Outputs

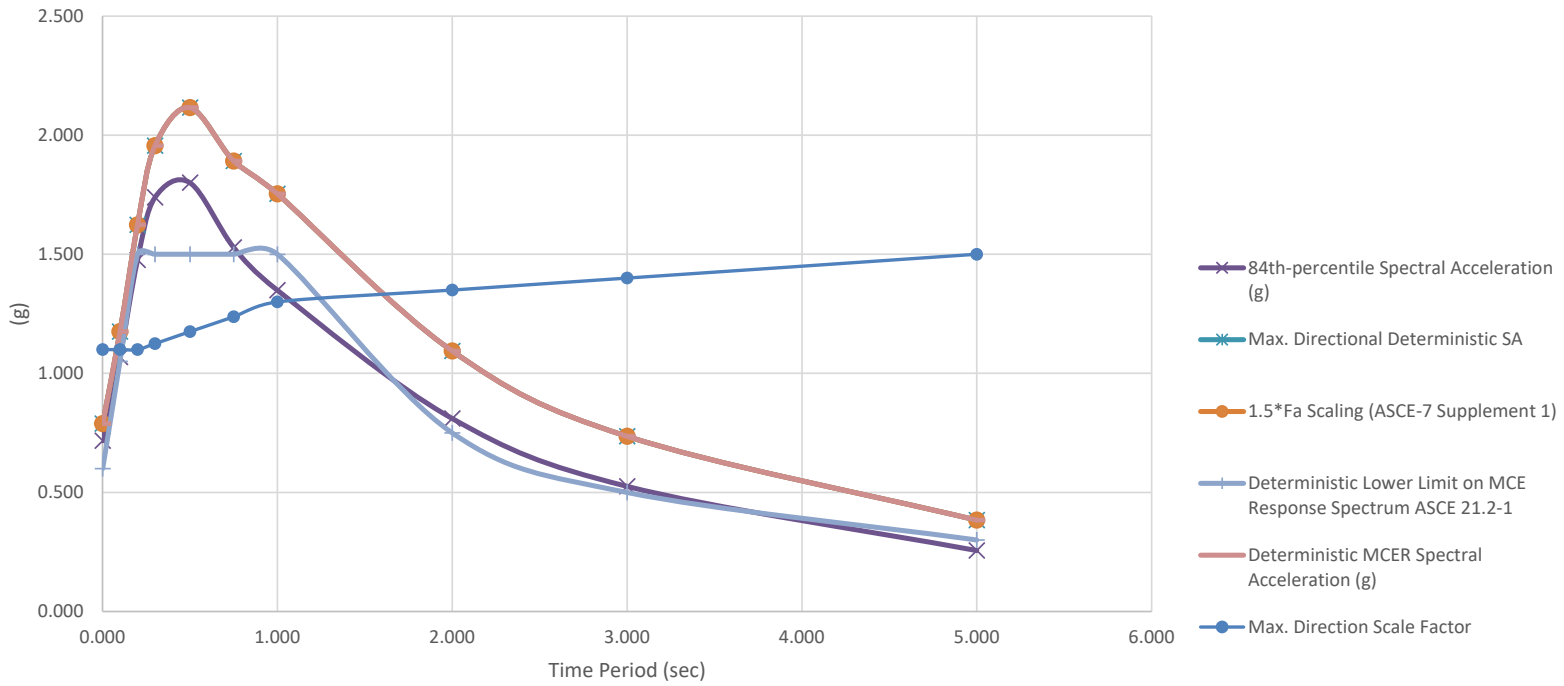


Figure 3: Site Specific Outputs

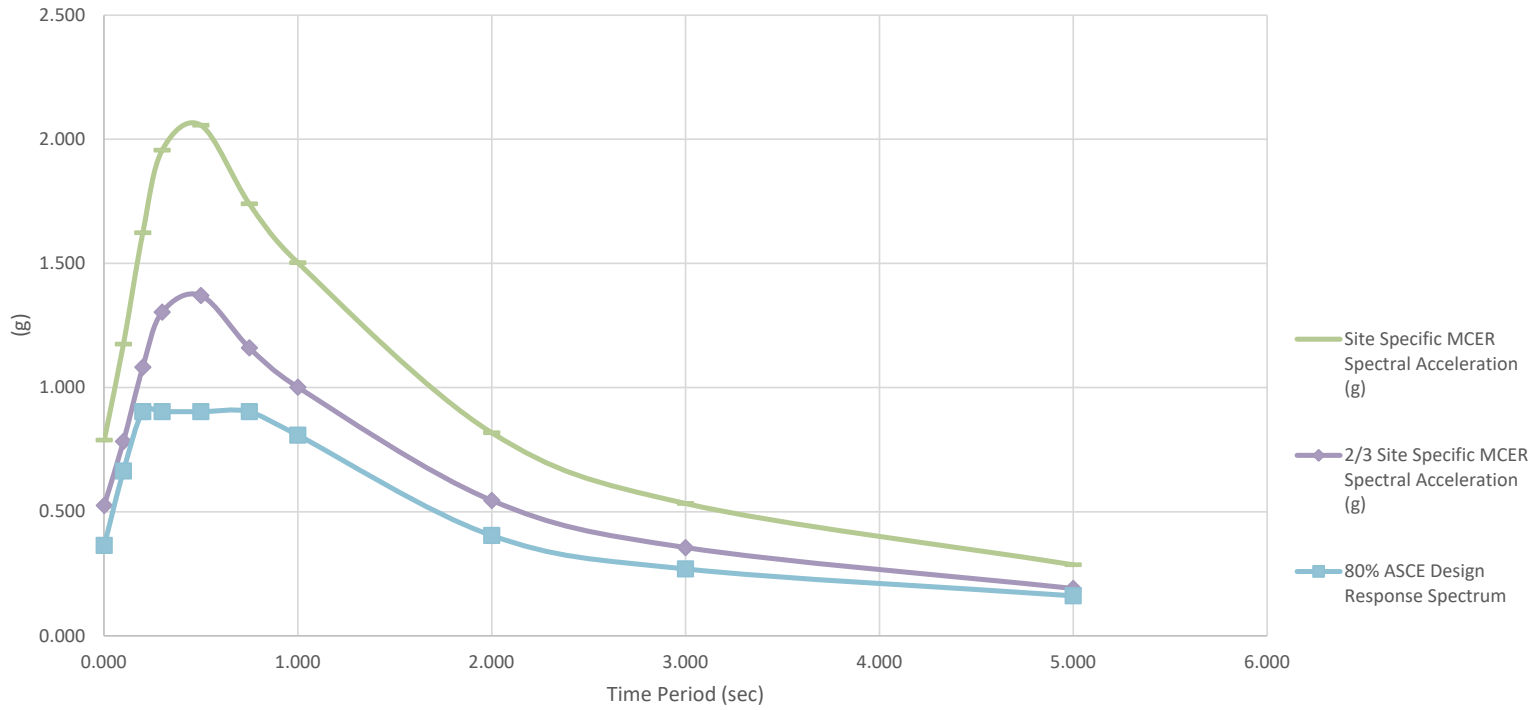
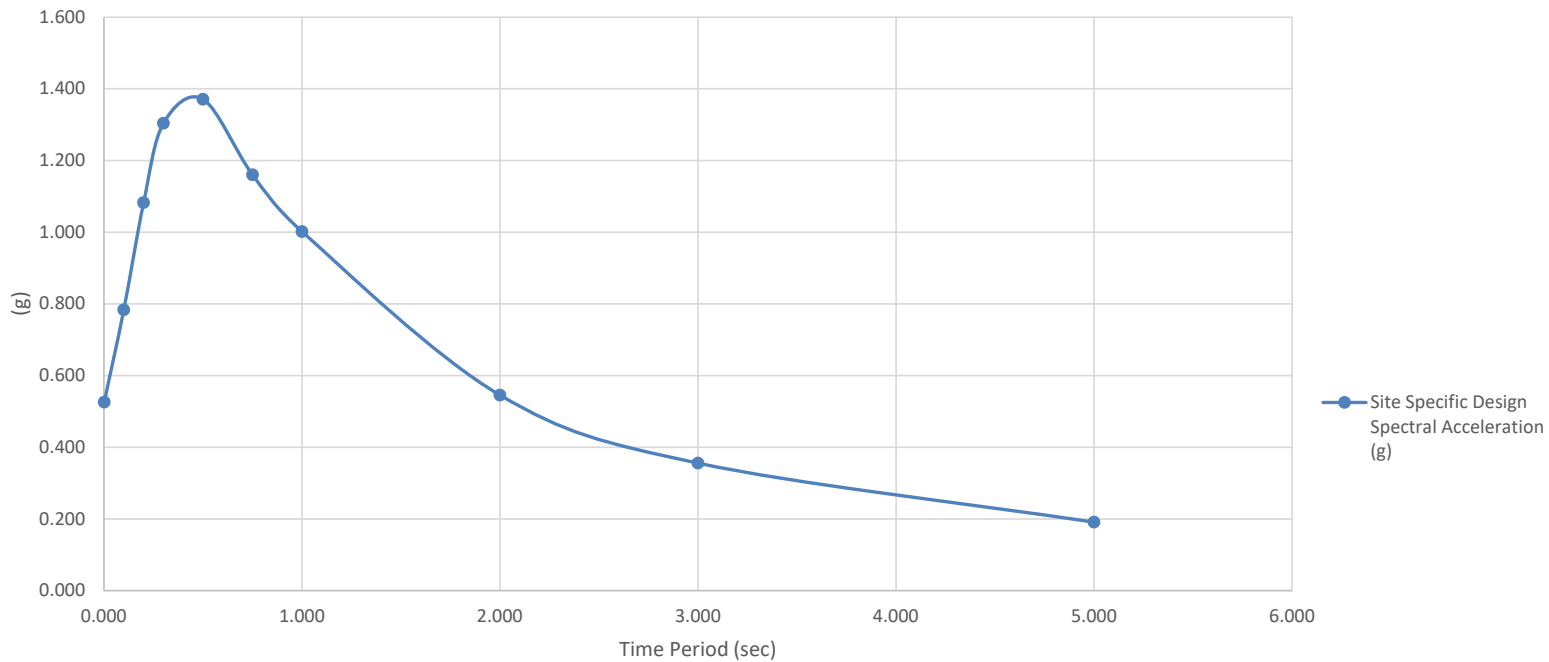


Figure 4: Site Specific Design Spectral Acceleration (g)



PROBABLISTIC INPUT DATA

Site Class: D		Ground Motion (g) vs. Annual Frequency of Exceedance (Total)									
	PGA	0.1 Sec	0.2 Sec	0.3 Sec	0.5 Sec	0.75 Sec	1.0 Sec	2.0 Sec	3.0 Sec	4.0 Sec	5.0 Sec
X	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
0.0025	0.93649507,	1.0631989,	1.2657008,	1.3500168,	1.3549628,	1.2343458,	1.0868799,	0.61815521,	0.37424315,	0.24842515,	0.17169908,
0.0045	0.6937083	0.8430971	1.0544462	1.1496668	1.1412731	0.9864909	0.8239579	0.4105002	0.2360877	0.1521996	0.10291422,
0.0075	0.5034032	0.6560909	0.8486749	0.9357093	0.9120188	0.7515061	0.6003610	0.2715232	0.1508939	0.0947441	0.06263791,
0.0113	0.3747635	0.5196372	0.6855059	0.7567568	0.7217695	0.5726675	0.4426690	0.1876646	0.1014895	0.0622445	0.040539586,
0.0169	0.2718445	0.4023602	0.5378397	0.5903076	0.5477278	0.4192938	0.3148439	0.1261128	0.0662135	0.0397772	0.025696908,
0.0253	0.1905548	0.3030538	0.4087363	0.4431293	0.3978406	0.2942518	0.2152573	0.0815039	0.0415435	0.0246013	0.015812213,
0.038	0.1276156	0.2207521	0.3004651	0.3201208	0.2769038	0.1979345	0.1411946	0.0504057	0.0250730	0.0146806	0.0093256938,
0.057	0.0809791	0.1547047	0.2138489	0.2234916	0.1857829	0.1281455	0.0890653	0.0300303	0.0146515	0.0084141	0.0052043844,
0.0854	0.0481896	0.1030334	0.146301,	0.1502460	0.1198962	0.0795577	0.0538447	0.0172622	0.0082180	0.0045469	0.0026898881,
0.128	0.0265815	0.0642341	0.0948924	0.0961793	0.0737526	0.0470135	0.0310503	0.0095058	0.0043454	0.0022652	0.0012565716,
0.192	0.0133562	0.0369077	0.0574872	0.0578459	0.0428385	0.0263105	0.0170285	0.0049498	0.0021312	0.0010197	0.00052034374,
0.288	0.0059693	0.0191734	0.0320866	0.0323361	0.0233583	0.0138943	0.0088380	0.0024113	0.0009555	0.0004084	0.00018756008,
0.432	0.0023017	0.0087515	0.0161809	0.0165937	0.0118562	0.0068569	0.0042930	0.0010841	0.0003857	0.0001423	0.000057217879,
0.649	0.0007319	0.0033773	0.0071120	0.0076373	0.0055032	0.0031105	0.0019237	0.0004401	0.0001364	0.0000417	0.000014193309,
0.973	0.0001840	0.0010750	0.0026213	0.0030807	0.0023068	0.0012852	0.0007855	0.0001589	0.0000416	0.0000099	0.0000027487141,
1.46	0.0000338	0.0002740	0.0007601	0.0010389	0.0008440	0.0004670	0.0002825	0.0000489	0.0000102	0.0000017	3.310378e-7,
2.19	0.0000040	0.0000566	0.0001624	0.0002769	0.0002594	0.0001445	0.0000865	0.0000121	0.0000018	1.6499415	1.5073871e-8,
3.28	2.3183936	0.0000095	0.0000242	0.0000543	0.0000638	0.0000362	0.0000214	0.0000021	1.7311683	3.4733584	6.095912e-11,
4.92	0.00000001,	0.0000012	0.0000023	0.0000069	0.0000116	0.0000067	0.0000038	2.0079733	2.5490535	1.363526e 1e-12,	
7.38	0	7.69E-08	1.10E-07	4.42E-07	1.34386E-06	7.41E-07	3.80E-07	1.95E-09	0	0	0

PGA	UHGM =	0.773	RTGM	0.737	RC =	0.95
0.1 Sec		1.301		1.264		0.97
0.2 Sec		1.724		1.685		0.98
0.3 Sec		1.95		1.859		0.95
0.5 Sec		1.881		1.75		0.93
0.75 Sec		1.535		1.406		0.92
1.0 Sec		1.267		1.156		0.91
2.0 Sec		0.671		0.606		0.9
3.0 Sec		0.423		0.381		0.90
4.0 Sec		0.289		0.259		0.90
5.0 Sec		0.212		0.191		0.90



WEIGHTED AVERAGE of 2014 NGA WEST-2 GMPEs

Last updated: 04 14 15

by Emel Seyhan, PhD, PEER & UCLA -- email: emel.seyhan@gmail.com, peer_center@berkeley.edu

This excel file will be updated as necessary on the PEER website to fix any typos or other errors. Please check the website frequently for new versions at: http://peer.berkeley.edu/ngawest2/databases/

Legend	Pre-defined option	Main input variable	Calculated variable	Input var. flag	Internal variable
--------	--------------------	---------------------	---------------------	-----------------	-------------------

GMPE averaging **Geometric** Weighted average of the natural logarithm of the spectral values

GMPEs	ASK14	BSSA14	CB14	CY14	I14
Weight	0.25	0.25	0.25	0.25	0
# of std. dev.	1				
Damping ratio (%)	5				

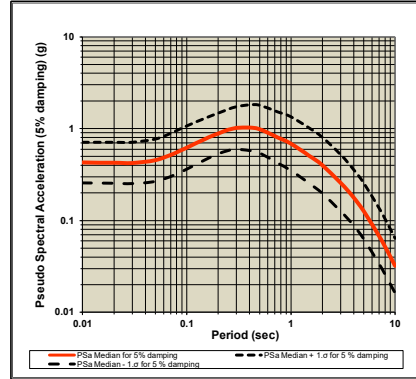
Modification factors are calculated in Sheet DSF

- ASK14 Abrahamson & Silva & Kamai 2014 NGA West-2 Model
- BSSA14 Boore & Stewart & Seyhan & Atkinson 2014 NGA West-2 Model
- CB14 Campbell & Bozorgnia 2014 NGA West-2 Model
- CY14 Chiou & Youngs 2014 NGA West-2 Model
- I14 Idriss 2014 NGA West-2 Model

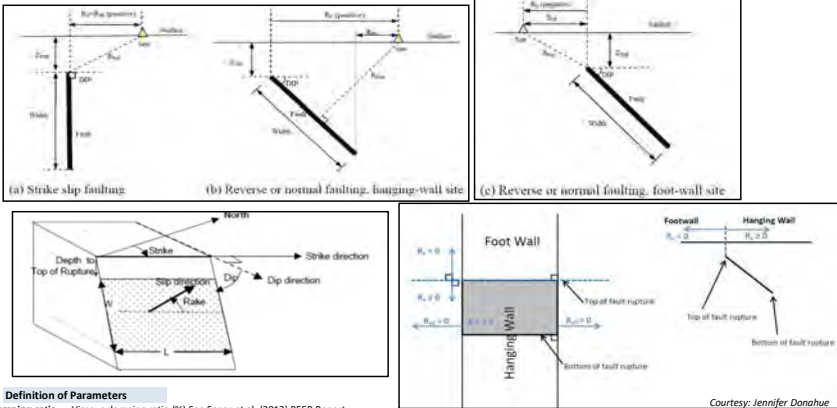
RotD50 Horizontal Component of PGA, PGV and IMs

Input variables	Errors and warnings
-----------------	---------------------

GMP	T (s)	Baseline: 5% Damping				User defined: 5% Damping				
		PSa Median for 5% damping	PSa Median + 1.0 for 5% damping	PSa Median - 1.0 for 5% damping	S _d Median for 5% damping	PSa Median for 5% damping	PSa Median + 1.0 for 5% damping	PSa Median - 1.0 for 5% damping	S _d Median for 5% damping	
M _w	0.01	0.4268129	0.710889	0.2562556	0.0010595	0.4268129	0.710889	0.2562556	0.0010595	
7.3	0.02	0.4248729	0.7104668	0.2538431	0.0042168	0.4248729	0.7104668	0.2538431	0.0042168	
R _{RUP} (km)	0.03	0.4236063	0.7116584	0.2521467	0.0094639	0.4231827	0.7109467	0.2518946	0.0094545	
10.48	0.05	0.4522987	0.7691247	0.2659831	0.0280993	0.4522987	0.7691247	0.2659831	0.0280993	
R _{JB} (km)	0.075	0.5329358	0.9174284	0.3605934	0.0744156	0.5340017	0.9192633	0.3102025	0.0745644	
4.2	0.10	0.6195034	1.0650587	0.3603412	0.1537836	0.6213619	1.0682539	0.3614222	0.154245	
R _x (km)	0.15	0.7707968	1.2997352	0.4571144	0.4305155	0.7723384	1.3023346	0.4580286	0.4313765	
4.2	0.2	0.8830628	1.4730864	0.5293647	0.8768351	0.8848289	1.4760326	0.5304234	0.8785888	
R _y (km)	0.25	0.9662769	1.6196691	0.5784702	1.4991598	0.9682094	1.6229085	0.5776231	1.5021582	
4.2	0.3	1.0154457	1.7368391	0.593682	2.2686399	1.0164612	1.738576	0.5942756	2.2709086	
R _{y0} (km)	0.4	1.0245076	1.8153381	0.578193	4.0691296	1.0255321	1.8171535	0.5787712	4.0731987	
999	0.5	0.9899353	1.7991164	0.5435963	6.1372559	0.9899242	1.8009155	0.5441399	6.1433932	
V ₃₃₀ (m/sec)	0.75	0.8921921	1.5284232	0.42103	11.201269	0.8921921	1.5284232	0.42103	11.201269	
259	1	0.6876058	1.3488324	0.3505287	17.068914	0.6876058	1.3488324	0.3505287	17.068914	
U (BSSA13)	1.5	0.5086626	1.0188528	0.25395	28.410485	0.5091712	1.0198716	0.2542039	28.438896	
0	2	0.401158	0.8118357	0.1982269	39.832884	0.4003556	0.8102121	0.1978305	39.753218	
F _{RV}	3	0.2583794	0.5257832	0.1269723	57.725376	0.258121	0.5252574	0.1268454	57.66765	
1: reverse fault	4	0.1786332	0.3600376	0.0886291	70.949349	0.1784545	0.3596776	0.0885405	70.8784	
0	5	0.1269893	0.2563224	0.062914	78.808576	0.1266083	0.2555535	0.0627253	78.57215	
F _{NW}	7.5	0.059879	0.1203561	0.029707	83.610932	0.0596993	0.119995	0.0297013	83.360099	
1: normal fault	10	0.0322326	0.0640441	0.0162222	80.013083	0.0321036	0.0637788	0.0161573	79.693031	
0	PGA (g)	0	0.4244691	0.7064799	0.2550306	0.0010537	0.4268129	0.710889	0.2562556	0.0010595
0	PGV (cm/s)	-1	62.849833	111.32164	35.48368	0.1560165	NA	NA	NA	NA



999	1: unknown use 999
0	1: Unspecified fault mech.
0	1: reverse fault
0	1: normal fault
0	1: hanging wall side
90	Dip (deg)
9.6	Z _{TOP} (km) If unknown use 999
999	Z _{HYP} (km) If unknown use 999
0.9	Z _{1.0} (km) If unknown use 999
4.5	Z _{2.5} (km) If unknown use 999
999	W (km) If unknown use 999
inferred	V ₃₃₀ Flag Choose options for V ₃₃₀ from the list
no	F _{AS} Aftershock effect is not applicable.
California	Region Choose region from the list



Definition of Parameters

Damping ratio = Viscous damping ratio (%) See Sanaz et al. (2012) PEER Report

PSA = Pseudo-absolute acceleration response spectrum (g)

PGA = Peak ground acceleration (g)

PGV = Peak ground velocity (cm/s)

S_d = Relative displacement response spectrum (cm)

M_w = Moment magnitude

R_{RUP} = Closest distance to coseismic rupture (km), used in ASK13, CB13 and CY13. See Figures a, b and c for illustration

R_{JB} = Closest distance to surface projection of coseismic rupture (km). See Figures a, b and c for illustration

R_x = Horizontal distance from top of rupture measured perpendicular to fault strike (km). See Figures a, b and c for illustration

R_{y0} = The horizontal distance off the end of the rupture measured parallel to strike (km)

V₃₃₀ = The average shear-wave velocity (m/s) over a subsurface depth of 30 m

U = Unspecified-mechanism factor: 1 for unspecified; 0 otherwise

F_{RV} = Reverse-faulting factor: 0 for strike slip, normal, normal-oblique; 1 for reverse, reverse-oblique and thrust

F_{NW} = Normal-faulting factor: 0 for strike slip, reverse, reverse-oblique, thrust and normal-oblique; 1 for normal

F_{HW} = Hanging-wall factor: 1 for site on down-dip side of top of rupture; 0 otherwise

Dip = Average dip of rupture plane (degrees)

Z_{TOP} = Depth to top of coseismic rupture (km)

Z_{HYP} = Hypocentral depth from the earthquake

Z_{1.0} = Depth to Vs=1 km/sec

Z_{2.5} = Depth to Vs=2.5 km/sec

W = Fault rupture width (km)

V_{330Flag} = 1 for measured, 0 for inferred V₃₃₀

F_{AS} = 0 for mainshock; 1 for aftershock

Region = Specific regions considered in the models, Click on Region to see codes

ΔDPP = Directivity term, direct point parameter; uses 0 for median predictions

PGA_r (g) = Peak ground acceleration on rock (g), this specific cell is updated in the cell for BSSA14 and CB14, for others it is taken account for in the macros

Z_{BOT} (km) = The depth to the bottom of the seismogenic crust

Z_{BOT} (km) = The depth to the bottom of the rupture plane

SS = 1 for strike slip, automatically updated in the cell

Calculated Variables/Flags

0	ΔDPP Always 0 for median calcs.
0.707	PGA _r (g)
15	Z _{BOT} (km) (CB14) Enter for default W calcs
1	SS auto calculated
0	V _{330Flag} inferred
0	F _{AS} Aftershock effect is not applicable.
0	Region California
1	Option for Sa value Weighted average of the natural logarithm of the spectral values

APPENDIX G

ReMi Analysis

Appendix G – Refraction Microtremor (ReMi) Survey

As requested, Universal Engineering Sciences, Inc. (UES) performed a Refraction Microtremor (ReMi) survey for the Proposed Student Housing project located at the Compton Community College in Compton, California. Please refer to the geotechnical engineering report for a project and site description.

Purpose and Scope of Services

The purpose of this ReMi survey is to approximate the physical properties of subsurface materials by estimating the depth and shear-wave velocities of various subsurface soil and rock layers (if encountered), and thereby characterize the site for seismic design (V_S100) according to ASCE 7-16. Our scope of services included:

- A review of published documents pertaining to the site
- A general reconnaissance of the site
- Acquisition of ReMi data along one line
- A geophysical analysis and evaluation of the acquired data
- A summary of our findings and recommendations in this report

This final report is intended for use in planning of the proposed development and as an aid in estimating physical properties of some of the subsurface materials that underlie the project site. Note that the ReMi data provided herein pertain specifically to the subject project site. While some correlation between soil and rock types to other neighboring sites is reasonable, site-specific surveys at those locations are recommended, if necessary.

ReMi Methodology

ReMi is a surface-wave seismic method developed by Optim™ of Reno, Nevada, for estimating in-situ Rayleigh-wave (shear-wave) velocities down to depths of approximately 100 meters with 5 percent to 15 percent accuracy, decreasing with depth. Testing is performed at the surface using simple seismic refraction equipment (as referenced in ASTM D5777) and the same vertical P-wave geophones used to acquire refraction data. The seismic source consists of ambient seismic “noise”, or microtremors, which are constantly generated by cultural and natural sources. In addition to the passive source noise, seismic “noise” can be induced with active sources by striking a sledgehammer off the end of the geophone array, and/or by jogging or driving a vehicle beside the line during acquisition. The data acquisition procedure consists of obtaining at least fifteen 30-second seismic noise records at a sample interval of 2 milliseconds. The result is a 1-D image of the subsurface shear-wave layering below the center of the geophone array. Unlike the seismic refraction method, ReMi can detect velocity inversions.

ReMi Line Location

The ReMi survey line was in the grass park area south of Parking Lot F, in the northern area of the campus. The line was oriented in an east northeast – west southwest direction, with Station 0 to the west and Station 115 to the east. The approximate line location is shown on the attached **Figure H-1**.

Line Survey

Line R-1 was oriented to minimize geophone placement on hardscape surfaces while maximizing line length. Down-line distances were measured with a survey tape to within ± 0.1 feet. Topographical relief along the line was less than 5 percent of the total line length; as such, relative station elevations were not measured. Geophone and shot locations were recorded with a hand-held GPS receiver, accurate to ± 10 feet.

Data Acquisition

Ambient noise records were recorded as well as noise induced by striking a sledgehammer off the end of the array and by walking up and down the line during data acquisition.

Instrumentation

ReMi data were acquired with a DaqLink4 24-channel seismograph, serial number 2432. The DaqLink4 is a portable 24-bit exploration seismograph system with a DC to 15 kHz bandwidth, and a noise floor of less than 0.2 microvolts RMS at 2 milliseconds (msec) sampling. The surface-wave signal was sensed at each station using a 14-Hz geophone. The DaqLink was controlled with a laptop computer utilizing the Windows 10 operating system. ReMi data were stored on the laptop's hard drive, and internally within the DaqLink.

Data Processing

Data were processed using Geogiga's Surface Plus application. A wavefield transformation was performed on the 30-second microtremor noise records, yielding the Rayleigh wave phase-velocity dispersion curve. The velocity spectrum from select individual records (gathers) was then stacked and summed to one spectrum, the dispersion curve picked, and the picks processed for one-dimensional velocity modeling.

Data Quality

Data quality for a ReMi survey is verified by observing the slowness-frequency plot of the Rayleigh-wave velocity spectrum. Good data quality is characterized by a well-defined energy envelope with a coherent dispersion curve that is continuous across all usable frequencies. Data quality for this ReMi survey was good. Several harmonic modes are apparent in the data. The fundamental mode is the 'lowest' along the velocity axis of the slowness-frequency plot.

Survey Depth

The maximum depth penetration for a ReMi survey is estimated by the usable lowest frequency data and is shown on the final model plot.

Data Presentation

ReMi analysis results are displayed as a 1-dimensional plot of shear-wave velocity versus depth below the existing ground surface at the center of the geophone spread (Figure H-2). A plot of the ReMi dispersion curve showing our data picks as well as a plot of model fits are also included (Figures H-3 and H-4).

Results

The weighted-average shear-wave velocity for the upper 100 feet (V_s100') is 796 feet/second (ft/s). ***This shear-wave velocity corresponds to a CBC seismic site classification of "D."***

Limitations

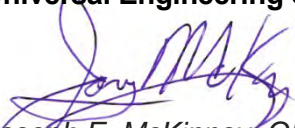
UES has striven to provide our services in accordance with generally accepted geotechnical engineering practices in this locality at this time; therefore, UES offers no guarantee or warranty, express or implied. This report was prepared for the exclusive use of the Client and the Client's authorized agents. It is understood that the owner or the owner's representative is responsible for submittal of this report to the appropriate governing agencies.

Our findings summarized in this report are based on a limited site reconnaissance using surface geophysical methods, experience, and our understanding of the proposed project. Furthermore, our findings assume that subsurface conditions do not vary significantly from those observed during the field reconnaissance.

Findings of this report are valid as of the issued date of the report; however, changes in conditions of a property can occur with passage of time, whether they are from natural processes or works of man, on this or adjoining properties. In addition, changes in applicable standards occur, whether they result from legislation or broadening of knowledge. Accordingly, findings of this report may be invalidated wholly or partially by changes outside our control. Therefore, this report is subject to review and should not be relied upon after a period of one year.

In the event that any changes in the nature, design, or location of structures or improvements are planned, the information contained in this report shall not be considered valid unless the changes are reviewed, and the conclusions of this report are modified or verified in writing.

Universal Engineering Sciences

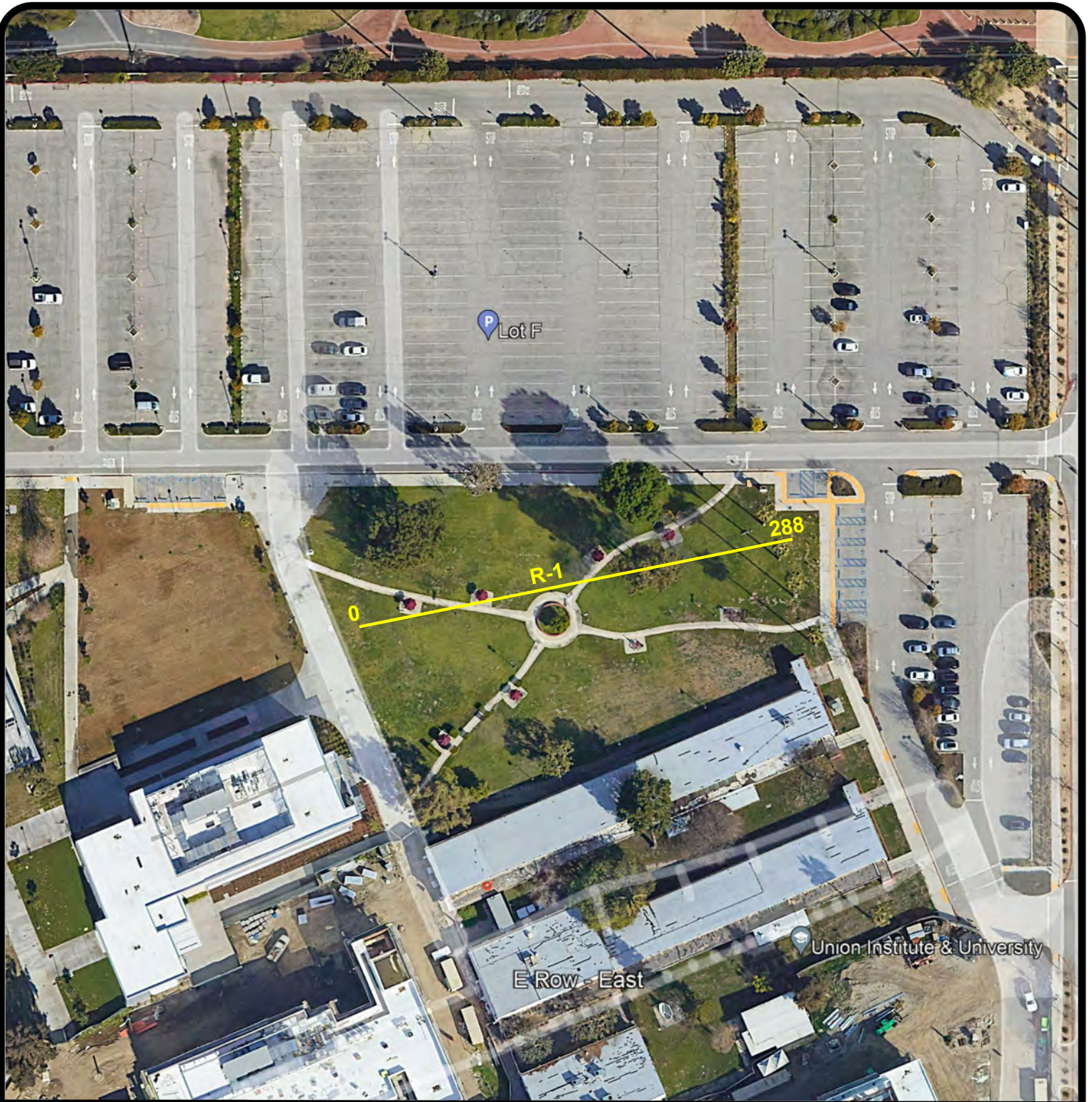

Joseph E. McKinney, GP, PG
Senior Geophysicist/Geologist



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- Building Seismic Safety Council of the National Institute of Building Sciences, 2009, NEHRP Recommended Seismic Provisions for New Buildings and Other Structures (FEMA P-750), Washington, D.C., 406 pages.
- Grant, F.S., and West, G.F., 1965, Interpretation Theory in Applied Geophysics, McGraw-Hill, Inc. 584 pages.
- Telford, W.M., Geldart, L.P., Sheriff, R.E., and Keys, D.A., 1976, Applied Geophysics, Cambridge University Press, New York, 860 pages.

Appendix



Base Map Source:
Google Earth Pro, 2022



Key

- Boring Location ●
- Infiltration Test Location ●
- ReMi Line Location — R-1

Job No.
4230.2200060.0000

ReMi Line Location

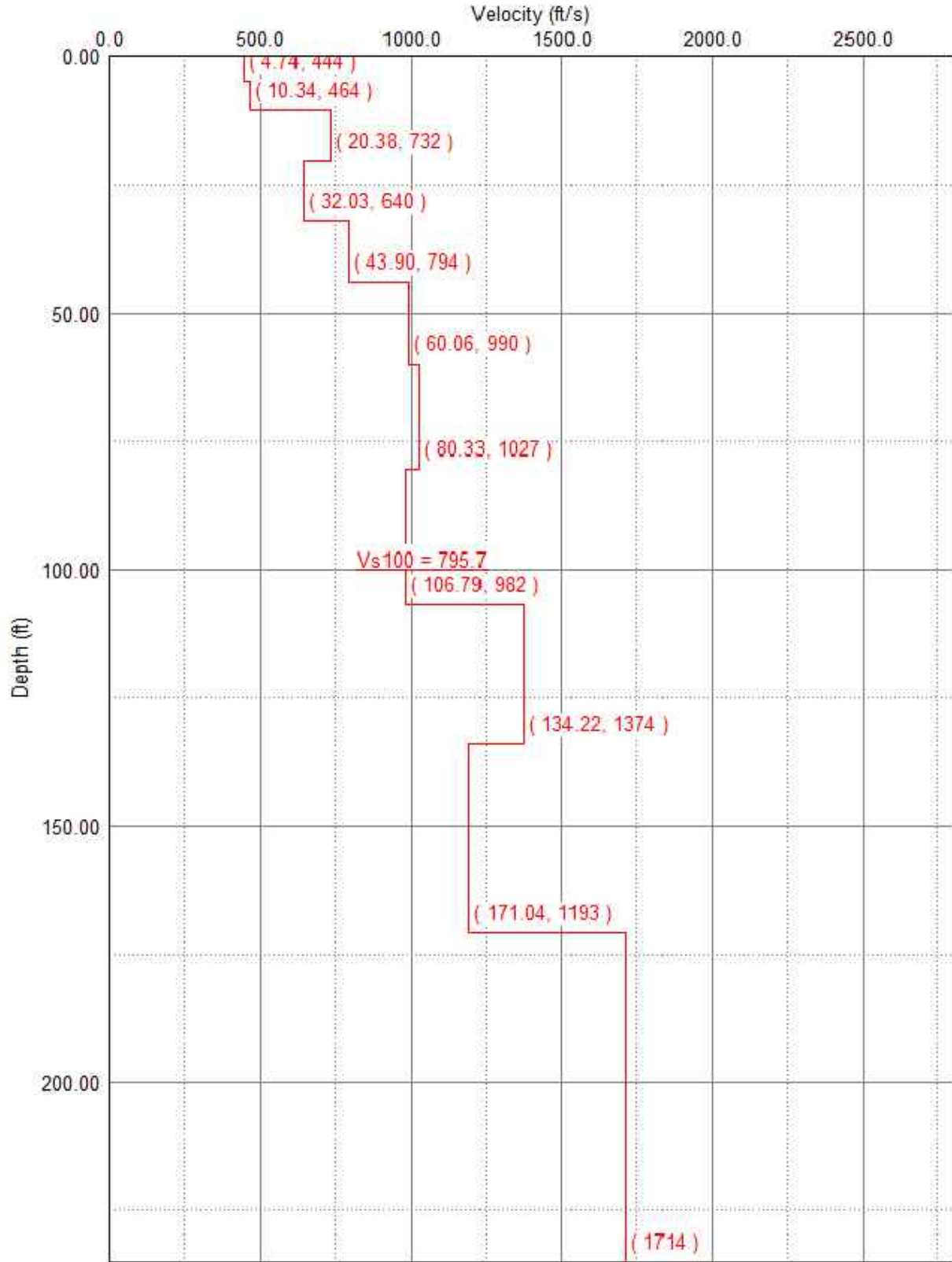
01-31-2023



Proposed Student Housing
Compton Community College District
1111 E. Artesia Blvd.
Compton, California

Figure H-1

Models



Job No.
4230.2200060.0000

ReMi Model

01-31-2023

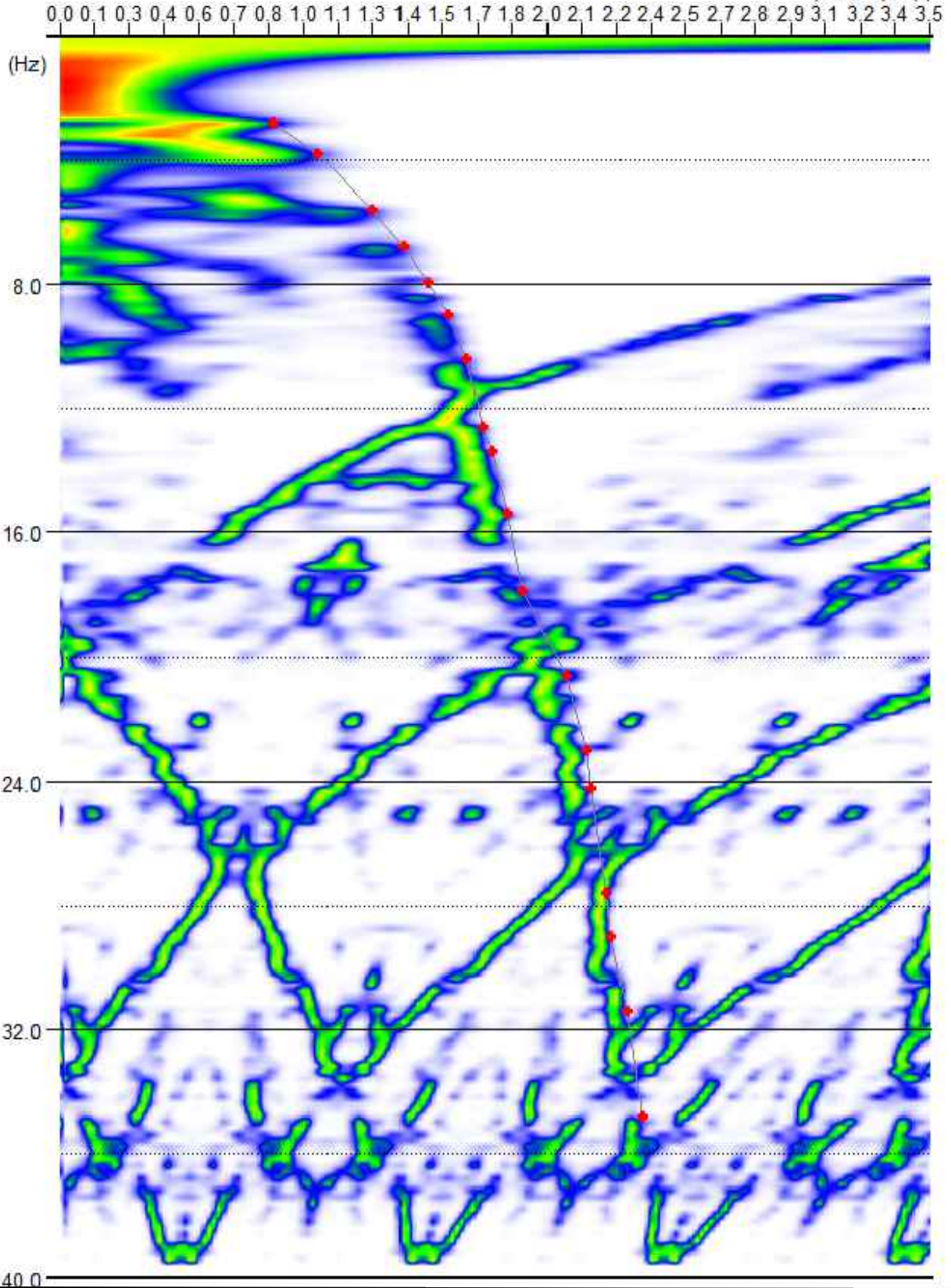



Proposed Student Housing
Compton Community College District
1111 E. Artesia Blvd.
Compton, California

Figure H-2

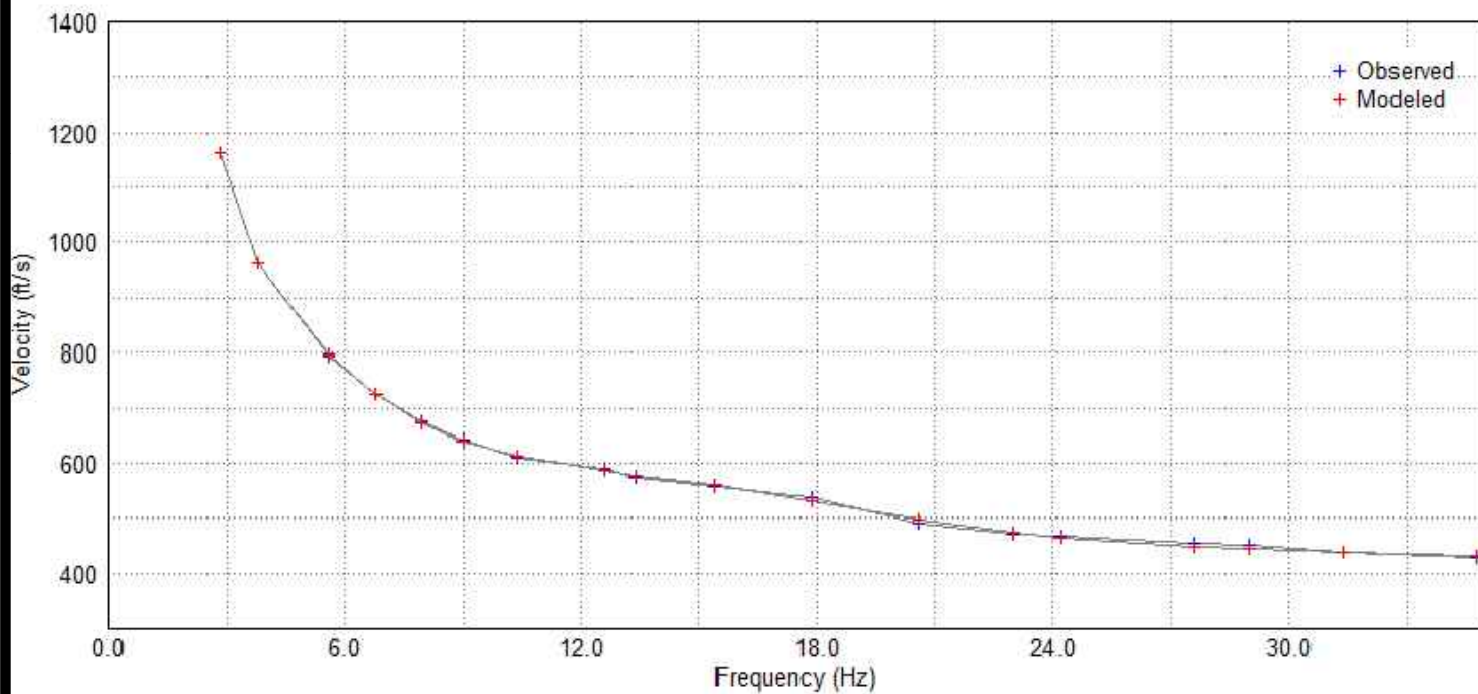
Slowness

($\times 10^{-3}$ (s/ft))



Job No. 4230.2200060.0000	ReMi Dispersion & Picks	01-31-2023
	Proposed Student Housing Compton Community College District 1111 E. Artesia Blvd. Compton, California	Figure H-3

Dispersion Curves



Job No.
4230.2200060.0000

ReMi Model Fit

01-31-2023



Proposed Student Housing
Compton Community College District
1111 E. Artesia Blvd.
Compton, California

Figure H-4



APPENDIX H
Ground Improvement Design - Deep Soil Mixing

Compton Community College

Proposed Student Housing

Ground Improvement Design – Deep Soil Mixing

1111 E Artesia Boulevard
Compton, California, 90221

Submitted to:
Compton Community College District
1111 E Artesia Boulevard
Compton, California, 90221

Submitted by:
Keller North America

April 7, 2023 (Rev 0)



Keller North America, Inc.
17461 Derian Avenue, Suite 106
Irvine, CA 92614
t: 909-393-9300
f: 909-393-0036



April 7, 2023

Keller Project No. 16121142

Compton Community College District
1111 E Artesia Boulevard
Compton, California, 90221

Attention: Ms. Linda Owens

Subject: Compton Community College Proposed Student Housing
Deep Soil Mixing Ground Improvement Design Submittal (Rev. 0)

Keller North America (Keller) is pleased to present the following design submittal for deep soil mixing ground improvements for the proposed 3-story low-income student housing facility at this project site. The purpose of the ground improvement program is to enhance the safety, stability, and serviceability of the proposed structures. This is accomplished by increasing the stiffness and strength of the ground to the point where the ground can safely support the anticipated structures under loading.

The design provided herein has been prepared for the exclusive use of Keller, with the special equipment and production procedures, for our client under the following strict limitations:

1. Only Keller may construct the work described by the design and
2. The design may not be used by others for any purpose.

Keller appreciates the opportunity to be of service. Please feel free to contact the undersigned at (805) 727-0039 with any questions, comments, or concerns.

Respectfully submitted,
Keller North America



Jim Gingery, PhD, PE, GE
Chief Engineer
Ground Improvement Design Engineer

Bailey Uy
Engineer

Matt Mudgett
Assistant Project Manager

1. Design summary

The site is located at 1111 E Artesia Boulevard, Compton, California 90221. The proposed development includes construction of a new 250-bed, 3-story low-income student housing building on campus. The proposed structures will consist of modular unit construction with steel and wood framing system.

Keller North America (Keller) proposes to install 3-foot diameter deep soil mixing (DSM) columns roughly arranged to achieve an equivalent ARR of 30%. The length of these columns shall be dictated by the depth to the sandy material and is expected to be encountered at approximately 20 feet below the existing ground surface. The proposed ground improvement system is designed to limit the calculated static and seismic settlements to allowable design levels and to stiffen the soils. Our shop drawing plans are presented in **Appendix A**.

2. Ground improvement design basis

This design is based on Keller's review of the following documents and performance requirements articulated by the project architect, structural, geotechnical, and civil engineers. Although many documents were reviewed, only those which provided information that directly affects our design are listed below:

- CCD Student Housing Geotechnical Report Draft by Universal Engineering Sciences dated, February 1, 2023
- Initial Liquefaction Analysis by Universal Engineering Sciences dated, February 1, 2023
- CPT data (# 1-6) provided by Universal Engineering Sciences dated, February 1, 2023
- 50% CD Progress Set provided by John A. Martin & Associates dated, February 13, 2023
- 75% CD Submittal Set provided by John A. Martin & Associates dated, March 13, 2023
- Loading Diagram provided by John A. Martin & Associates dated, March 15, 2023

If any of these documents are changed or altered in any way, Keller should be notified, and the design may require modifications.

2.1 Design criteria

The anticipated performance criteria have been established by the project team and are summarized in Table 1 below.

Table 1: Design inputs and performance criteria

Property	Criteria	Reference
Assumed Working Grade	EL +57 feet	VCA Engineers, Inc.
Max Foundation Bearing Pressure (Unfactored DL + LL)	2000 psf ^(a)	John A. Martin & Associates
Post-Construction Total Static Settlement	≤ 1 inch	
Post-Construction Total Liquefaction Settlement	≤ 1 inch	
Max Differential Settlement	0.006L ≤ 1 inch over 13.9 feet ^(b)	ASCE 7 Table 12.13-3

Notes

- (a) The allowable bearing pressure shown in the table is for dead + live loads; this value may be increased by 1/3 for transient loads such as wind and/or seismic loading.
- (b) This angular distortion value is from ASCE 7-16 Table 12.13-3 for a Risk Category III, "other" multi-story structure. The columns spacing (L) shown on the plans is 13.9± feet.

2.2 Subsurface conditions

According to the geotechnical report prepared by Universal Engineering Sciences, the site is underlain by Holocene Alluvium and artificial fill associated with the campus construction. The alluvium material was encountered at all exploratory excavation locations to the maximum depth of approximately 76.5 feet below the existing ground surface. Groundwater was encountered in the borings at approximately 52.8 and 54.2 feet below existing grade. The historic high ground water table which was used in this design is 8 feet below existing grade. A copy of the relevant boring logs and CPTs can be found in **Appendix B**.

3. DSM ground improvement system

The proposed ground improvement system consists of deep soil mixing columns arranged to form overlapping crisscrossing secant panels. The panels are aligned with the strip footings to provide static bearing capacity support and settlement reduction. The lattice grid shape of the DSM panels reinforces the soil and shields it from seismic loading to mitigate soil liquefaction. Details of the static and seismic design of the DSM ground improvement are provided in the following sections.

4. Static design

4.1 Geotechnical bearing and crushing capacity.

Based on Keller's analysis and the provided loads, the proposed DSM design provides a DSM crushing factor of safety between 4.4 and 14.5, and an end bearing factor of safety of 9.0. The calculated factors of safety meet or exceed the generally accepted minimum factor of safety of 3. A copy of the provided loads can be found in **Appendix C** and details of the individual calculations can be found in **Appendix D**.

4.2 Static settlement estimation

The static settlement of a supported structure using DSM consists of the two components:

compression of the DSM column under the applied load and the induced settlements below the bottom of the DSM matrix. As seen in **Appendix D**, settlements within the DSM column are computed assuming that the full footing load will be transferred to the DSM column and that the DSM column behaves in an elastic manner. Settlements below the bottom of DSM are computed per the method described in Bowles' Foundation Analysis and Design, 5th edition textbook.

This analysis shows the total expected settlement will be between 0.2 and 0.6 inches. Thus, the post-construction settlements meet the allowable settlement value of 1 inch.

5. Seismic design

5.1 Deep soil mixing technical background.

The installation of deep soil mixed columns at this site will mitigate liquefaction potential at the site through reinforcement of the native soils during seismic shaking. To account for the shear reinforcement effect of the proposed DSM grid, Nguyen, et al. (2013) suggests applying a shear stress reduction factor, R_{rd} , which is applied to the cyclic stress ratio used in soil liquefaction triggering calculations. This shear stress reduction value is computed as follows:

$$R_{rd} = \min \left\{ \frac{1}{G_r * [ARR * C_G * \gamma_r + 1/G_r * (1 - ARR)]}, 1 \right\}$$

where:

G_r = average stiffness ratio

ARR = area replacement ratio

C_G = equivalent shear factor computed as the shear stiffness of the DSM grid system:

$$C_G = 1 - 0.5\sqrt{1-ARR}$$

γ_r = shear strain ratio between DSM grid and soil:

$$\gamma_r = \left[1 - (1 - ARR)^{1.3} * \left(\frac{G_r - 1}{1.85} \right)^{0.4} \right] * \min \left(\frac{H}{S}, 1 \right)$$

The DSM is arranged to achieve an equivalent ARR of 30%. The length of these columns shall be dictated by the depth to the sandy material and is expected to be encountered at approximately 20 feet below the existing ground surface. Please refer to **Appendix C** for details of this computation.

5.2 Liquefaction mitigation

All 6 CPTs were evaluated for liquefaction potential. We did not analyze SPT data since it is inherently more uncertain, and the CPT penetration resistance data is considered more reliable. A summary of the design parameters and the respective sources used in our analysis can be found in Table 2 and details of the individual calculations can be found in **Appendix E**. This analysis shows the post-improvement liquefaction-induced settlements are estimated at 0.8 to 0.9 inches. Differential settlements are expected to be half of these values over a horizontal span of 40 feet, or about ½ inch or less. Thus, the post-improvement liquefaction differential settlements meet the allowable maximum value of 1 inch.

The DSM panels serve as an essentially impermeable horizontal barrier that prevent the migration of excess porewater pressure for soils that may still liquefy outside of the building footprint. Moreover, the DSM is designed to support the footings without any contribution from adjacent

soils, so liquefaction of soils outside the building footprint has no impact on the foundation bearing capacity. Because of these characteristics there is no need for a "sacrificial" zone of DSM outside of the building footprint. This differs from stone column ground improvement, which does not form a barrier against excess porewater pressure, and so is typically designed to extend outside the building footprint to provide a buffer zone that absorbs excess porewater pressure that could migrate into the ground improvement zone. But no such buffer zone is needed for DSM to perform successfully.

Table 2: Liquefaction analysis design parameters

Property	Criteria	Reference
Groundwater Level (Static and Seismic)	8 feet below existing grade	Universal Engineering Sciences, Inc.
Peak Ground Acceleration, PGA_M	0.77	
Moment Magnitude, M_w	7.30	
Triggering Method	Boulanger and Idriss (2014)	
Volumetric Settlement Method	Zhang et al. (2002)	
Transition Zones per Robertson (2009)	Applied	Keller North America
Depth Weighting Factor per Cetin et al. (2009)	Applied	

6. Construction

DSM construction involves using high torque equipment to mechanically mix grout with native soils to create a nearly homogeneous mixture of weak concrete called soilcrete. DSM is a top-down construction technique. As the mixing tool is advanced into the soil, grout slurry is pumped through the hollow stem of the shaft and injected into the soil at the tip and through the tool. The auger flights and mixing blades on the tool blend the soil with grout in a pug-mill fashion. When the design depth is reached, the tool is withdrawn to the surface. Left behind are stabilized soil mixed columns. Often predrilling can be used to simplify the disposal of construction spoils and waste soil. Depending on project requirements, DSM can be used to improve ~10% to ~100% of the soil within a given area.

The minimum average 28-day unconfined compressive strength is 150 psi. Keller plans to use pre-determined cement content at the beginning of the mixing operation and observe the wet soilcrete strength development to adjust cement dosage accordingly.

6.1 Layout

Keller will provide an AutoCAD shop drawing for each DSM column coordinate overlaid on the site

structural foundation drawing. Keller understands that the general contractor will be responsible and provide Keller with at least (5) control points and survey benchmarks before installation. Keller will then use a Topcon Hiper V system or similar global positioning system commonly used at construction projects for daily re-layouts of target locations. The layout will be done by Keller's field engineer. Once the project is complete, Keller will prepare as-built drawings and share as-built survey coordinates that show the delta of x (easting) and y (northing), the difference between target and staked location. Keller will layout and install DSM columns within 3 inches of the design locations as shown in the Keller shop drawing.

6.2 Sequence of work

Once a stable working platform has been established by others, DSM columns will be constructed sequentially based on a pattern dictated in the field. Keller requires access to all DSM locations at all times to maximize efficiency.

6.3 Pre-drill

To minimize the mixing tool damage and maintaining soil mixing quality, Keller may pre-drill holes or excavate for better mixing quality. The holes will be filled with soilcrete up to the working elevation during the mixing stage.

6.4 Soil mixing

In general, soil mixing operation parameters, such as mixing shaft speed, penetration rate, batching grout specific gravity, and pumping rate will be determined based on prior experience. These parameters may be fine-tuned during production. The design cement content in place (cement weight/ [soil volume + grout volume]) will start from the predetermined cement content and grout slurry specific gravity (SG). Keller engineers may adjust the cement content and grout SG based on the field sample strength development.

6.4.1 Vertical alignment

Vertical alignment of the mixing tool will be controlled by the drill rig operator. Two measurements of verticality will be monitored. These are the fore-aft and left-right vertical mast positions. Verticality will be measured by a level as measured on the mixing tool prior to penetration. Intermittent measurements will be made as necessary during mixing operations. Verticality will be checked to make sure it is within $\pm 1\%$ of being plumb.

6.4.2 Mixing shaft speed

The mixing shaft speed, which is anticipated to be ranging between 20-60 RPM, shall be adjusted to accommodate a constant rate of mixing shaft penetration based on the degree of drilling difficulty. The mixing shaft speed can be adjusted according to drilling difficulty. The mixing shaft speed can be adjusted to aid mixing of the soil mix column when needed or to assist penetration in hard drilling. Mixing shaft speed will be recorded by Keller's data acquisition system (DAQ).

6.4.3 Penetration rate

To ensure adequate mixing, the penetration rate of the mixing shaft shall be maintained at about 1.0 to 5.0 feet/minute during penetration. The penetration rate and maximum depth of each stroke shall be recorded by Keller's DAQ.

6.4.4 Practical refusal

It is possible that our equipment may experience practical refusal before reaching the design tip elevation. For the purposes of this design, Keller defines practical refusal as failure to penetrate

6 inches over 1 minute. Any practical refusal prior to reaching design tip elevation must be evaluated and approved by the Ground Improvement Design Engineer.

6.4.5 Grout take

The grout slurry flow per vertical foot of the column will be adjusted to the requirements of the design mix. Progressive cavity pumps will be used to transfer the grout from the mixing plant to the mixing rig. Flow monitoring devices will be installed in the grout line to detect any line blockage, monitor flow, total injected grout per column, and grout pressure. These parameters will be recorded by Keller's DAQ.

Inevitably, some variations of the grout take will occasionally occur due to field conditions. It is anticipated that a grout flow rate between 20 to 160 GPM will be used during penetration. Keller's DAQ can automatically adjust the grout flow rate based on the penetration rate and maintain the pre-set cement dosage prescribed by the design engineer.

6.4.6 Withdrawal and remixing/re-stroking rate

The mixing shaft will be withdrawn at a rate of 6 to 12 feet per minute during the re-stroke operation and complete removal of the mixing shaft from the mixed column.

6.4.7 Obstructions/mixing shaft refusal

Keller will use our proprietary DAQ system to monitor the mixing shaft penetration and the shaft rotation resistance in terms of the hydraulic pressure. The DAQ will calculate and plot the drilling index, a mixing parameter to detect penetration resistance and refusal depth, as a function of depth. Keller will set up the penetration criteria based on the site measurement. In case of underground obstruction, such as abandoned footings, piles, utilities, etc., the general contractor will be responsible to remove obstructions and backfilled with sandy soil prior to Keller mixing operation.

6.5 Material

6.5.1 Cement

Cement will be furnished by Keller and conform to ASTM C150 "Standard Specification for Portland Cement," Type II/V or equivalent. The cement will be adequately protected from moisture and contamination while in transit to and in storage at the job site. Reclaimed cement or cement containing lumps or deleterious material will not be used.

6.5.2 Water

Water for the slurry will be fresh, free of deleterious substances that adversely affect the strength and mixing properties of the slurry, will be provided by others.

6.6 Equipment

6.6.1 Batching equipment

The batch plant shall consist of in-line eductor (jet valve) mixers. Dry materials shall be stored in tankers and/or silos and fed to the mixers for shearing and circulation. The resulting grout slurry will be transferred to a surge tank for continuous agitation and to supply the in-situ soil mixing rig.

6.6.2 Mixing equipment

Single shaft mixing equipment that mechanically mixes the soil and cement slurry for the full

dimensions of the column will be used for the work. We anticipate using hydraulic drill rigs for the soil mixing operations. This rig is capable of up to > 150,000 ft-lbs of torque at > 20 rpm. The working shaft rate of rotation ranges between 20 and 60 rpm. The mixing shaft will have mixing augers and/or blades (paddles) configured in such a manner so that they are capable of thoroughly blending the in-situ soils and cement slurry. The power source for driving the mixing shafts will be sufficient to maintain the required mix tool (shaft) rotation speed in revolutions per minute and penetration/withdrawal rates from the ground surface to the maximum depth required. The design target blade rotation number (BRN), defined as the number of blades cut in each 1.0-meter of soil, will be at least 450 when averaged over a 3-foot length of column.

The DSM equipment will be equipped with devices to assure vertical alignment in two planes (90 degrees in plan from each other): fore-aft and left-right. The DSM equipment will be equipped with a real-time display of depth, rotation speed, grout flow rate, grout specific gravity, cumulative grout injected, and grout pressure for each soil mix column. The cement will be mixed with water within the jet valve to create a predetermined specific gravity mix ± 0.1 . No mixing operation will be allowed if the DAQ system is not functioning.

6.6.3 Pumping equipment

Grout slurry will be supplied to the drill using large size Moyno pumps. These pumps will be sized and powered so that design volumes and pressures can be maintained up to 1,000 feet away from the batching facility. It is anticipated that a continuous grout slurry flow of 150 gallons per minute at 100 psi to the drill rig will be necessary.

6.6.4 Equipment location

The batching and pumping facility will be set up at a central location to all soil mixing areas. This will eliminate the need to move the plant once it is established.

7. QA/QC

Following the installation of DSM columns, verification testing will include:

- unconfined compressive test on wet soil mixed samples
- unconfined compressive test on cored samples
- review of production DAQ logs

7.1 Wet soil mixed samples

Wet soil mix samples will be retrieved at various depths and cast into molds for one column per rig/shift. Samples will be retrieved using an in-situ wet sampler immediately after column construction and shall consist of no fewer than 8 specimens. Soil clods greater than 10% of the mold diameter will be screened off. Appropriate curing techniques shall be implemented until testing based on ASTM D1632.

Unconfined compression testing shall be performed by an approved laboratory in pairs of specimens at 7 days. If the 7-day specimens do not reach the desired strength according to the lab test curve, another pair of specimens will be tested at 14 days, 28 days, and if needed at 56 days. All 28-day-aged UCS tests will be used in the statistical calculation. The unconfined compressive strength (UCS) shall be determined by ASTM D1633 "Standard Test Methods for Compressive Strength of Molded Soil-Cement Cylinders". Sulfur or gypsum caps shall be required in the UCS tests to minimize the end effects on the test specimen. The advantage of the wet sampling is that Keller can get an early trend of the soilcrete strength development and can make early adjustments in the field.

7.2 Core samples

Additionally, Keller will core 2% of the production DSM columns. The purpose of the coring is to evaluate mixing quality and obtain samples for UCS testing.

Core locations will be selected by the Ground Improvement Design Engineer with concurrence from the QC Inspector. Coring will start after the soilcrete has gained adequate strength and has been verified by the strength development from the wet sample tests. At minimum, five (5) samples from each core will be extracted. Keller anticipates that 4 specimens trimmed from each core hole will be tested per ASTM D1633.

Uniformity of mixing shall be evaluated by the QC Inspector and the Ground Improvement Design Engineer based on the continuous core samples recovered. The continuous core holes shall extend the entire depth of the DSM column. The estimated recovery of a single core shall be no less than 85% for each 5-foot-long segment; that is, lumps of unimproved soils shall not exceed 15% of the total volume of any 5-foot-long core segment. Additionally, the estimated recovery shall be no less than 85% when averaged over all core runs. If the core recovery is below the anticipated value due to the gravel particles in the soilcrete matrix, Keller shall be allowed to utilize a downhole camera or other approved method to verify the core hole.

Keller will calculate the average 28-day UCS value from all core samples and wet grab samples. No more than 10% of all specimens tested shall exhibit an unconfined compressive strength of less than 75 psi at 28 days. Should the proposed design not meet the acceptance criteria in a given area, Keller may be given the opportunity to:

- conduct additional UCS testing on soilcrete specimens at 56 days of age
- conduct additional UCS testing on soilcrete specimens on additional cured specimen
- perform additional site explorations and cores
- utilize a downhole camera or other approved method to verify the core hole
- perform engineering to determine if the as-built conditions meet the project design requirements and intent

Any such work shall be performed at Keller's preference and expense. If a designated area is rejected, Keller shall submit a remixing or mitigation plan.

At the end of the project, to not unnecessary delay subsequent activities by waiting for a 28-day test result, correction of early strength gain will be used to approve the DSM work. However, this correlation will not relieve the contractor of the responsibility to achieve average 28-days strength of 150 psi. Based on FHWA (2013) guidelines, the following UCS aging factor correlations will be applied to this job:

- 3-day to 28-day projection factor of 1.72
- 7-day to 28-day projection factor of 1.35
- 14-day to 28-day projection factor of 1.15

A site-specific correlation between 3-days and 28-days strength may be used to supersede this correlation if in the opinion of the Engineer the site-specific correlation is more appropriate.

7.3 Production DAQ Logs

During the soil mixing production, Keller will review the wet soilcrete strength development as well as production column mixing logs and make any necessary adjustments. The adjustments can

include penetration rate, specific gravity and BRN. DAQ logs shall be submitted to Universal Engineering Services the following day after installation.

8. References

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Zhang, G. and Robertson, P.K. (2002). *Estimating liquefaction-induced ground settlements from CPT for level ground*, Can. Geotech. J., 39: 1168-1180.

Attachments:

Appendix A – Deep soil mixing design shop drawings

Appendix B – Exploration data as provided by Universal Engineering Sciences

Appendix C – Loads and bearing pressures as provided by John A. Martin & Associates

Appendix D – Bearing capacity and DSM design calculations

Appendix E – Liquefaction calculations

Appendix A

Deep soil mixing design shop drawings

Appendix B

Exploration data as provided by Universal Engineering Sciences, Inc.



Universal Engineering Sciences
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 Telephone: (949) 537-3222

CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/22/22 **COMPLETED** 12/22/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879695, -118.210009
GROUNDWATER LEVELS Encountered at 52' 9"
BACKFILL Native cuttings

NOTES

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist									
		(SC) Clayey SAND, dark olive brown, loose to med. dense, damp	AU SPT	7-5-5 (10)							
		(CL) Lean CLAY, olive brown, stiff, damp	MC	5-7-12 (19)		94.1	26.2				
10		(ML) Silt with SAND, olive brown, medium soft, damp	SPT	3-3-4 (7)				34	25	9	75.9
		(CL) Lean CLAY, very dark grayish brown, stiff, damp	MC	4-8-12 (20)		102.6	19.2				
		(CL-ML) Sandy silty CLAY, olive brown, stiff, damp	SPT	5-6-7 (13)							61.7
20		Very stiff, moist	MC	6-10-25 (35)		100.0	9.7				
		(CL) Lean CLAY, dark olive brown, stiff, moist	SPT	3-4-5 (9)				39	22	17	86.7
30		(ML) Silt with SAND, olive, fine, stiff, moist, no smell, *CH (bottom two rings)	MC	8-8-9 (17)		100.0	14.4				
		(CL) Lean CLAY, olive gray, stiff, moist,	SPT	4-4-7 (11)							97.7
40		(ML) Silt with SAND, olive gray, hard, moist	MC	10-23-35 (58)		103.9	16.6				
		Wet, fine grained, very stiff	SPT	7-8-8 (16)				29	24	5	74.7
50		(SP-SM) Poorly graded SAND with silt, fine to medium, very dark greenish gray, very dense, wet	MC	17-39-50 (89)		103.1	19.1				
		(SM) Silty SAND, very dark greenish gray, dense, saturated	SPT	10-19-24 (43)							14.0
60		(SP-SM) Poorly graded SAND with silt, fine to medium, very dark greenish gray, very dense, saturated	MC	19-50 (69)		107.0	20.5				
		(SM) Silty SAND, greenish black, medium dense, saturated	SPT	3-6-8 (14)				NP	NP	NP	23.5
70		(SP-SM) Poorly graded SAND with silt, fine, very dark greenish gray, medium dense, saturated	MC	8-11-24 (35)							
		No recovery									
Bottom of borehole at 76.5 feet.											

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CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/22/22 **COMPLETED** 12/22/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879977, -118.209528
GROUNDWATER LEVELS Not encountered
BACKFILL Native cuttings

NOTES

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist	AU								
		(CL) Lean CLAY, dark olive brown, stiff, moist	MC	4-5-6 (11)		101.5	18.0				
		(ML) Sandy SILT, olive brown, stiff, moist	SPT	4-6-6 (12)				29	23	6	60.8
10		Very stiff, fine	MC	5-15-19 (34)		97.5	6.6				
		(CL-ML) Sandy silty CLAY, olive brown, stiff to very stiff, damp	SPT	5-5-10 (15)							
		(ML) Sandy SILT, fine, light olive brown, very stiff, damp	MC	11-17-21 (38)		105.5	6.5				
20		(CL-ML) Sandy silty CLAY, olive, hard, damp	SPT	15-19-23 (42)							
		(CL) Lean CLAY, dark olive brown, very stiff, damp	MC	13-19-22 (41)		89.3	13.6				
30		(CL-ML) Sandy silty CLAY, olive, very stiff, damp	SPT	4-8-8 (16)							
		(CL) Lean CLAY, dark olive gray, very stiff, moist	MC	5-9-19 (28)		92.1	29.4				
40		Gray brown, hard	SPT	13-19-27 (46)							
		(ML) Sandy SILT, olive, hard, moist	MC	14-38-29 (67)		107.3	16.6				
50		(CL-ML) Sandy silty CLAY, light brown, very stiff, moist	SPT	6-9-10 (19)							
Bottom of borehole at 51.5 feet.											

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CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/29/22 **COMPLETED** 12/29/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA
NOTES _____

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879698, -118.210258
GROUNDWATER LEVELS Not encountered
BACKFILL Native cuttings

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, medium soft, moist	AU								
		(ML) Silt with SAND, light olive brown, stiff, damp	SPT	3-3-4 (7)							
		Sandy SILT, olive, stiff, moist	MC	7-11-11 (22)		98.0	6.0				
10		(CL-ML) Sandy silty CLAY, dark olive gray, stiff, moist	SPT	3-4-6 (10)				36	25	11	
		Olive	MC	4-8-12 (20)		113.5	15.7				
		(ML) Sandy SILT with GRAVEL, olive, stiff, moist, *siltstone	SPT	4-5-4 (9)				28	21	7	
20		(CL) Lean CLAY, olive, stiff, moist	MC	12-10-9 (19)		101.3	10.3				
		(CH) Fat CLAY, greenish black, greenish black, stiff to very stiff, moist	SPT	2-3-6 (9)							
30		(ML) Sandy SILT, olive, very stiff, moist	MC	6-12-13 (25)		88.1	31.4				
		Hard	SPT	4-7-10 (17)				38	27	11	
40		(CL) Lean CLAY, grayish brown, very stiff, moist, *trace silt	MC	6-19-34 (53)		104.4	12.1				
		(SC-SM) Silty, clayey SAND, very dark greenish gray, fine to medium, dense, wet	SPT	3-5-12 (17)							
50			MC	28-31-50 (81)		105.3	18.7				
Bottom of borehole at 51.5 feet.											



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PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/29/22 **COMPLETED** 12/29/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA
NOTES

PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879719, -118.209679
GROUNDWATER LEVELS Encountered at 54' 2"
BACKFILL Native cuttings

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DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, medium soft, moist (CL-ML) Silty CLAY, light olive brown, very stiff, dry	AU	7-9-10 (19)		97.1	7.2				
		Light olive, damp	MC	12-8-9 (17)							
10		(ML) Sandy SILT, fine, light olive brown, stiff, damp	SPT	7-8-13 (21)		94.3	3.4				
		(CL-ML) Silty CLAY, olive, very stiff, damp	MC	5-9-11 (20)							
		Olive brown, stiff, moist	SPT	10-11-13 (24)		105.7	7.8				
20		(CL) Lean CLAY, olive brown, stiff, moist	MC	5-5-6 (11)							89.3
		(ML) Sandy SILT, fine, olive brown, very stiff, moist	SPT	18-19-20 (39)		103.4	4.8				
30		(CL) Lean CLAY, dark olive gray, stiff, moist	MC	3-4-5 (9)							92.7
		Olive, very stiff, damp	SPT	8-12-17 (29)		93.5	26.6				
40		(SM) Silty SAND, dark olive gray, dense	MC	11-8-11 (19)							46.5
		(ML) Sandy SILT, olive, hard, moist	SPT	16-35-44 (79)		108.1	17.3				
50		(SM) Silty SAND, dark greenish gray, dense, moist	MC	9-17-19 (36)							33.0
		(ML) Sandy SILT, greenish black, hard, wet	SPT	9-19-39 (58)		94.5	30.0				
60		(SP-SM) Poorly graded SAND with silt, dark greenish gray, dense, saturated	MC	7-13-26 (39)				NP	NP	NP	8.5
		Fine to coarse, greenish gray	SPT	5-20-20 (40)		117.3	15.0				
70		Dark greenish gray, medium dense	MC	8-8-13 (21)							9.0
		Fine to medium, very dark greenish gray, very dense, less silt	SPT	6-22-50 (72)		111.4	18.8				
Bottom of borehole at 76.5 feet.											

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BORING NUMBER P-2

CLIENT <u>Compton Community College District</u> PROJECT NUMBER <u>4230.2200060.0000</u> DATE STARTED <u>12/23/22</u> COMPLETED <u>12/23/22</u> DRILLING CONTRACTOR <u>2R</u> DRILLING METHOD <u>HSA</u> LOGGED BY <u>AM</u> CHECKED BY <u>ER & DA</u> NOTES _____	PROJECT NAME <u>New 3-Story Student Housing Facility - Compton College</u> PROJECT LOCATION <u>1111 E Artesia Blvd, Compton, CA 90221</u> GROUND ELEVATION <u>57 ft MSL</u> HOLE SIZE <u>8 inches</u> COORDINATES <u>33.879726, -118.210124</u> GROUNDWATER LEVELS <u>Not encountered</u> BACKFILL <u>Native cuttings</u>
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DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		<u>Qya: young alluvial deposits.</u> Grassy topsoil, mostly clay, soft, moist	GB								
5	(CL)	Lean CLAY, very dark grayish brown, stiff, damp Light brown, *trace silt	MC	4-7		93.0	29.8				
			SPT	3-5-5 (10)							
10		(ML) SILT, olive brown, stiff, damp	MC	6-10-9 (19)		93.1	13.7				

Bottom of borehole at 10.0 feet.

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Universal Engineering Sciences
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 Irvine, CA 92618
 Telephone: (949) 537-3222

BORING NUMBER P-3

CLIENT Compton Community College District **PROJECT NAME** New 3-Story Student Housing Facility - Compton College
PROJECT NUMBER 4230.2200060.0000 **PROJECT LOCATION** 1111 E Artesia Blvd, Compton, CA 90221
DATE STARTED 12/29/22 **COMPLETED** 12/29/22 **GROUND ELEVATION** 57 ft MSL **HOLE SIZE** 8 inches
DRILLING CONTRACTOR 2R **COORDINATES** 33.879805, -118.209812
DRILLING METHOD HSA **GROUNDWATER LEVELS** Not encountered
LOGGED BY AM **CHECKED BY** ER & DA **BACKFILL** Native cuttings
NOTES _____

DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist	Hand icon GB								
5		(CL) Lean CLAY with sand, olive brown, medium soft, damp	SPT	3-3-3 (6)				32	22	10	69.8
		(CL-ML) Sandy silty CLAY, olive brown, very stiff, damp	MC	10-17-20 (37)		96.7	22.4				
10		Medium soft to stiff	SPT	4-4-4 (8)							

Bottom of borehole at 10.0 feet.

GEOTECH BH COLUMNS - GINT STD US LAB.GDT - 1/31/23 10:01 - \\UESNOVA.LJESORL.COM\ISOCAL\PROJECTS\GEOTECH\2022\4230.2200060.0000 COMPTON COLLEGE STUDENT HOUSING PROJECT\APPENDIX A - BORING LOGS\LOGS\4230.2200060.000



Universal Engineering Sciences
 16 Technology Dr., Ste 139
 Irvine, CA 92618
 Telephone: (949) 537-3222

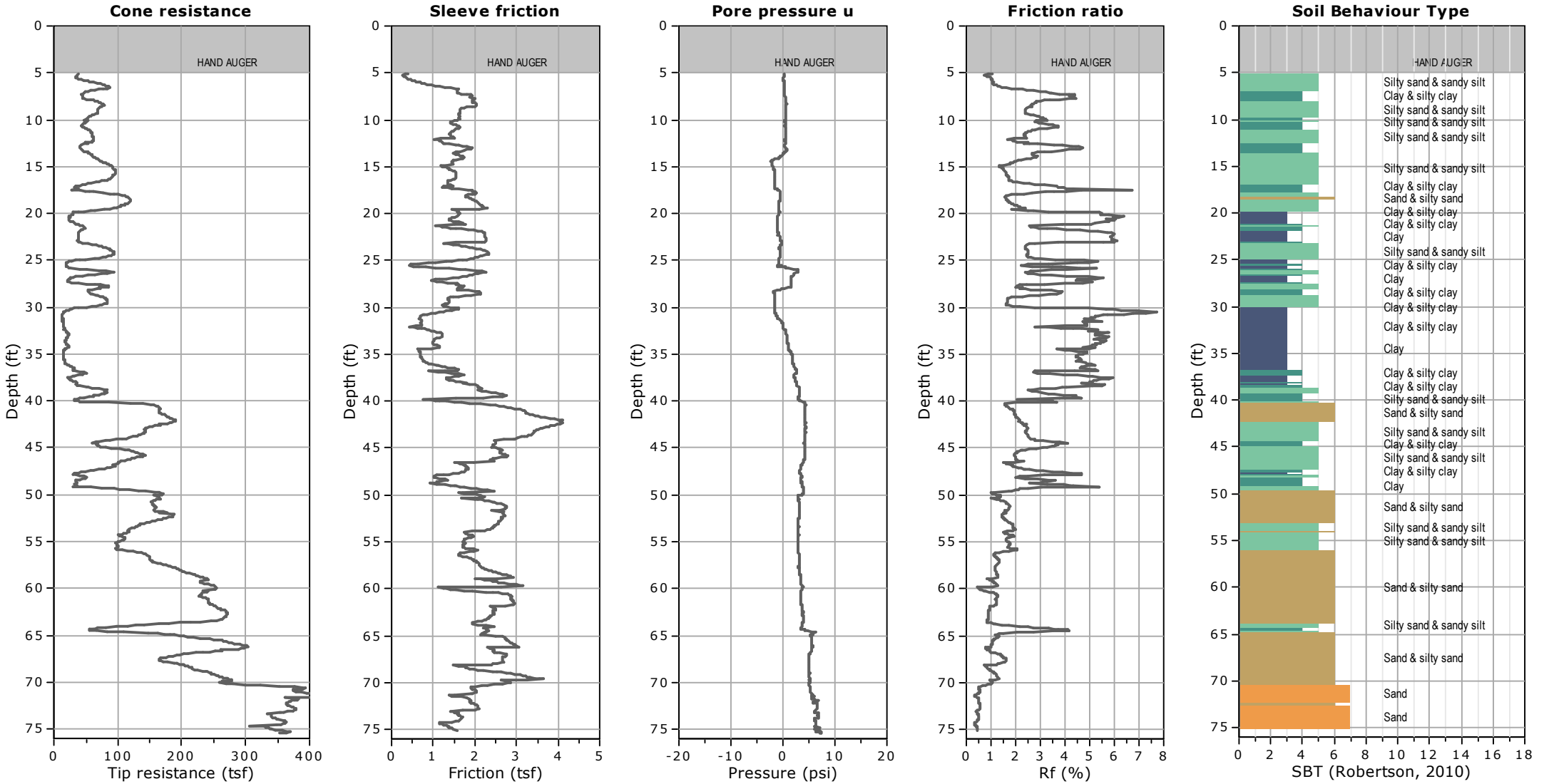
BORING NUMBER P-4

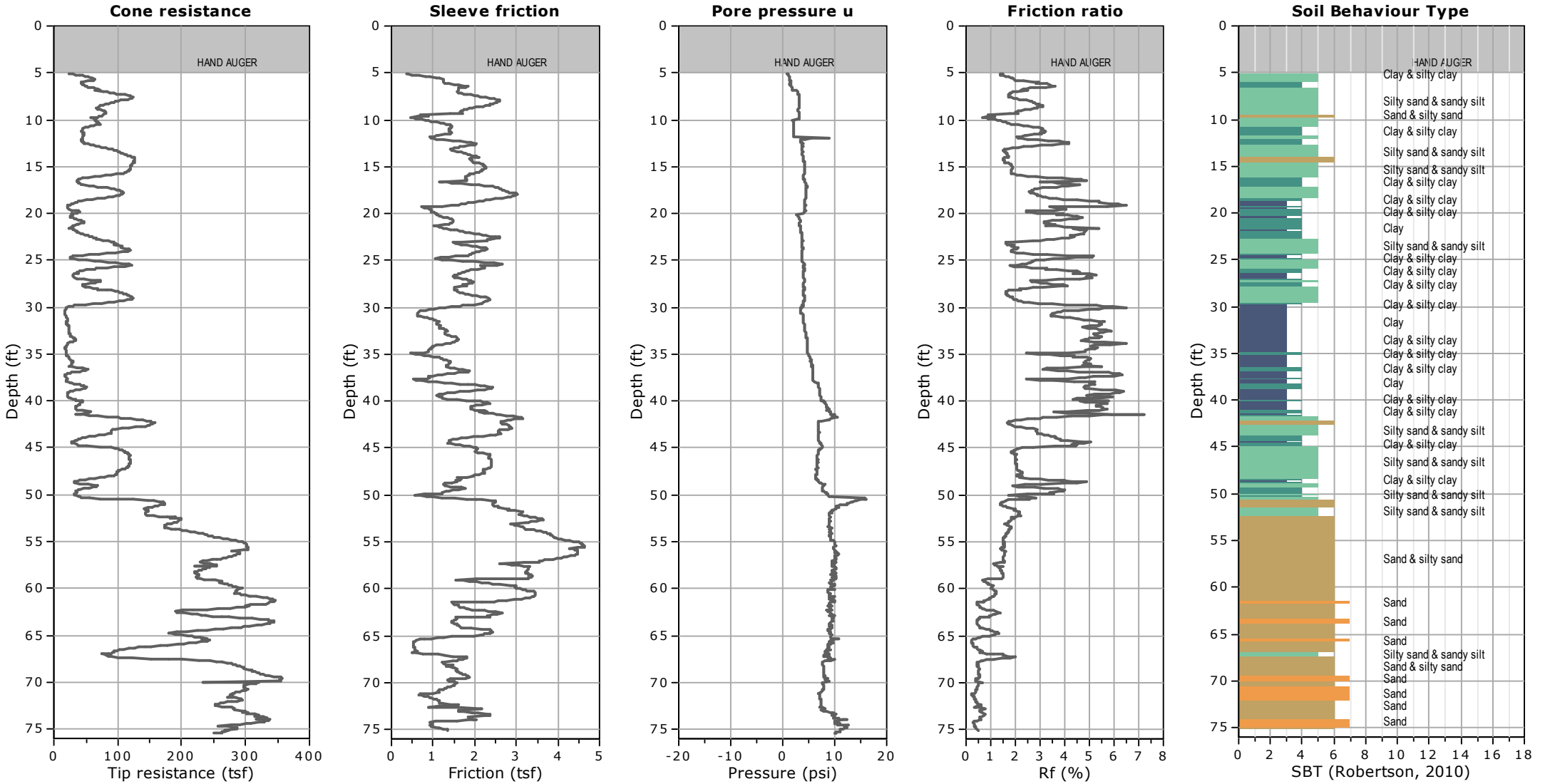
CLIENT Compton Community College District
PROJECT NUMBER 4230.2200060.0000
DATE STARTED 12/22/22 **COMPLETED** 12/22/22
DRILLING CONTRACTOR 2R
DRILLING METHOD HSA
LOGGED BY AM **CHECKED BY** ER & DA
NOTES _____

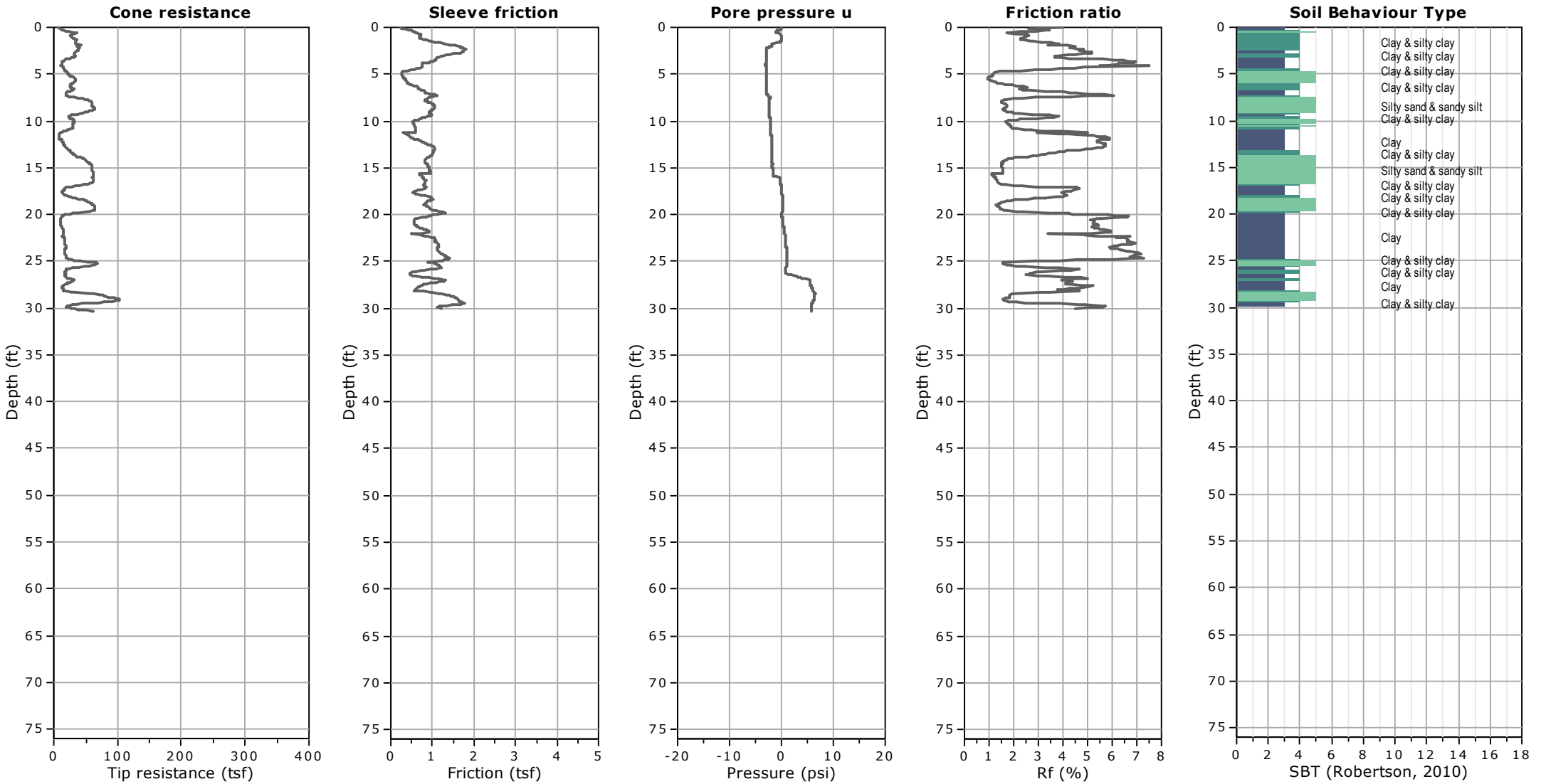
PROJECT NAME New 3-Story Student Housing Facility - Compton College
PROJECT LOCATION 1111 E Artesia Blvd, Compton, CA 90221
GROUND ELEVATION 57 ft MSL **HOLE SIZE** 8 inches
COORDINATES 33.879674, -118.209534
GROUNDWATER LEVELS Not encountered
BACKFILL Native cuttings

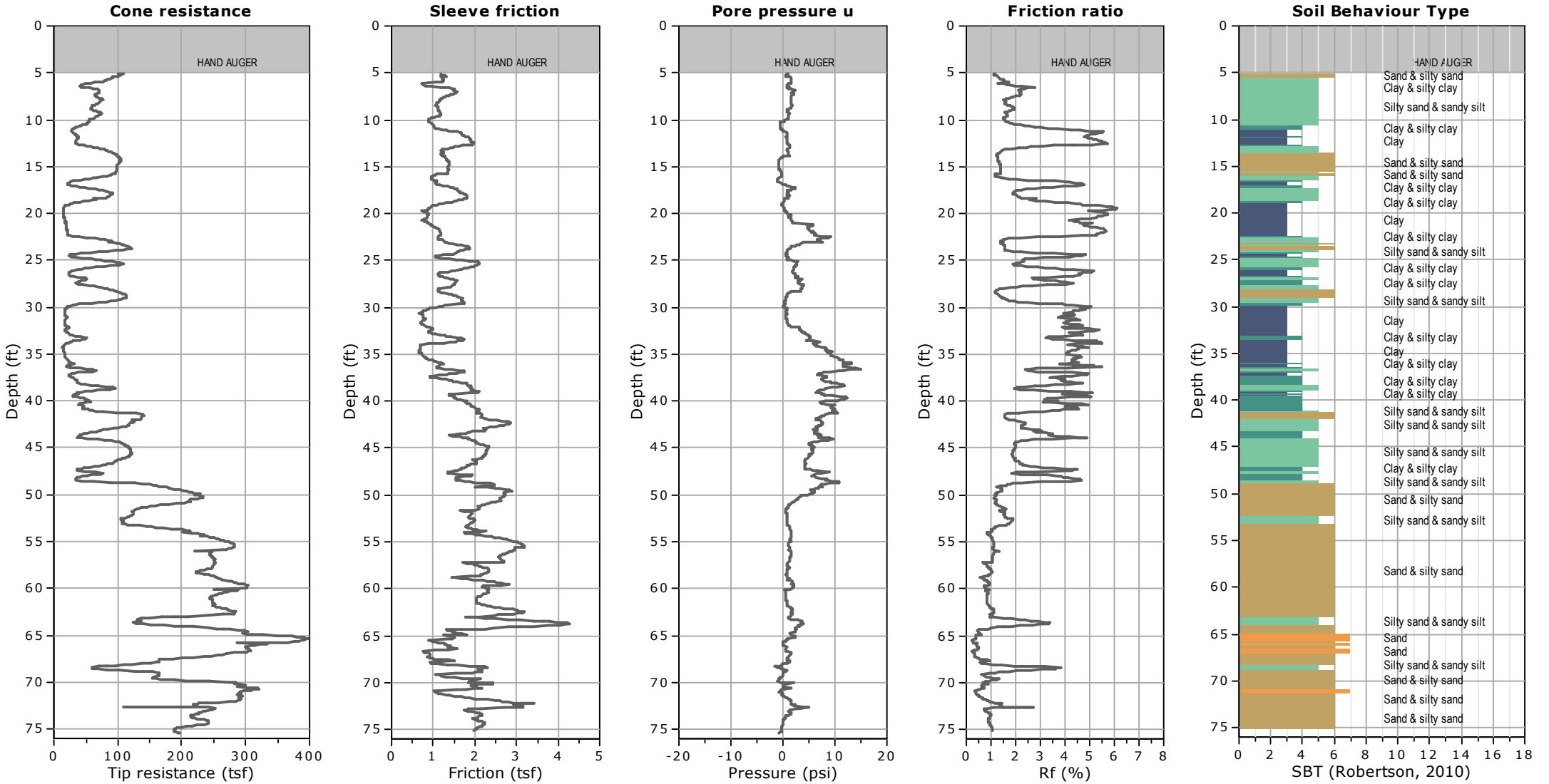
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS			FINES CONTENT (%)
								LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	
0		Qya: young alluvial deposits. Grassy topsoil, mostly clay, soft, moist	Hand icon GB								
5		(CL) Lean CLAY with sand, olive, medium soft, dry	SPT	3-4-5 (9)				32	22	10	72.3
		(CL-ML) Sandy silty CLAY, light olive brown, very stiff, damp	MC	9-18-30 (48)		99.6	6.6				
10		Olive	SPT	8-9-13 (22)							

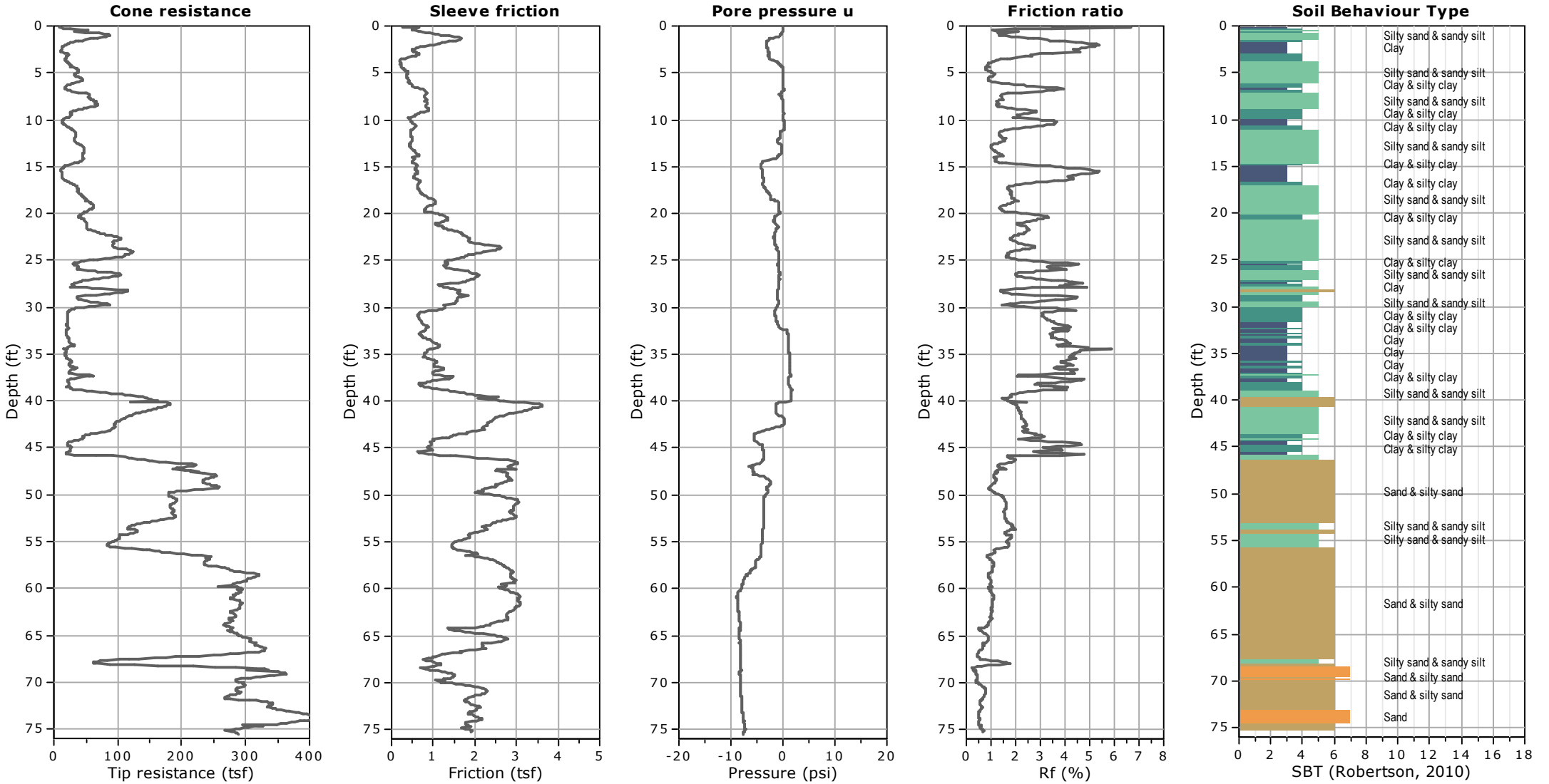
Bottom of borehole at 10.0 feet.

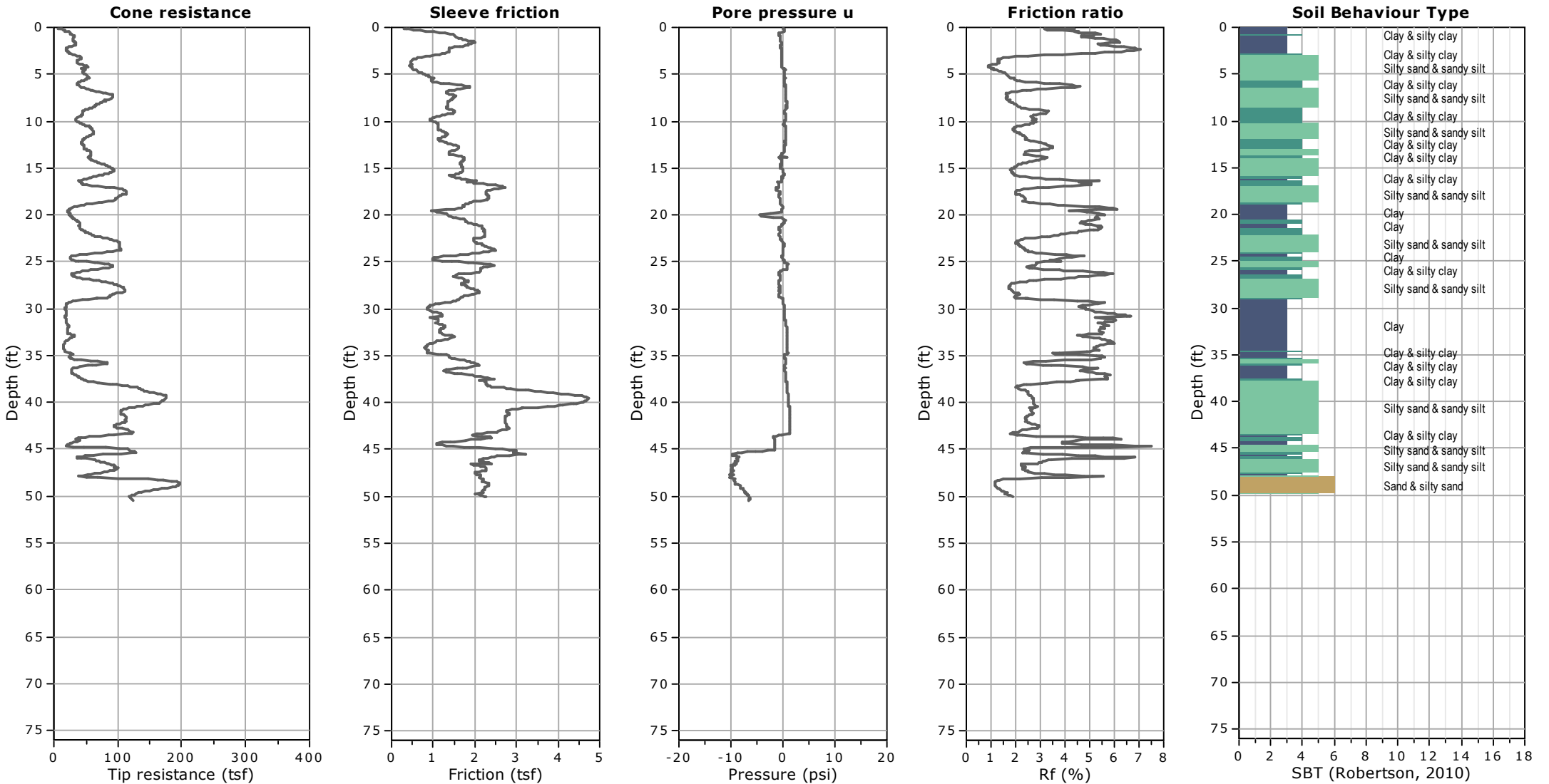












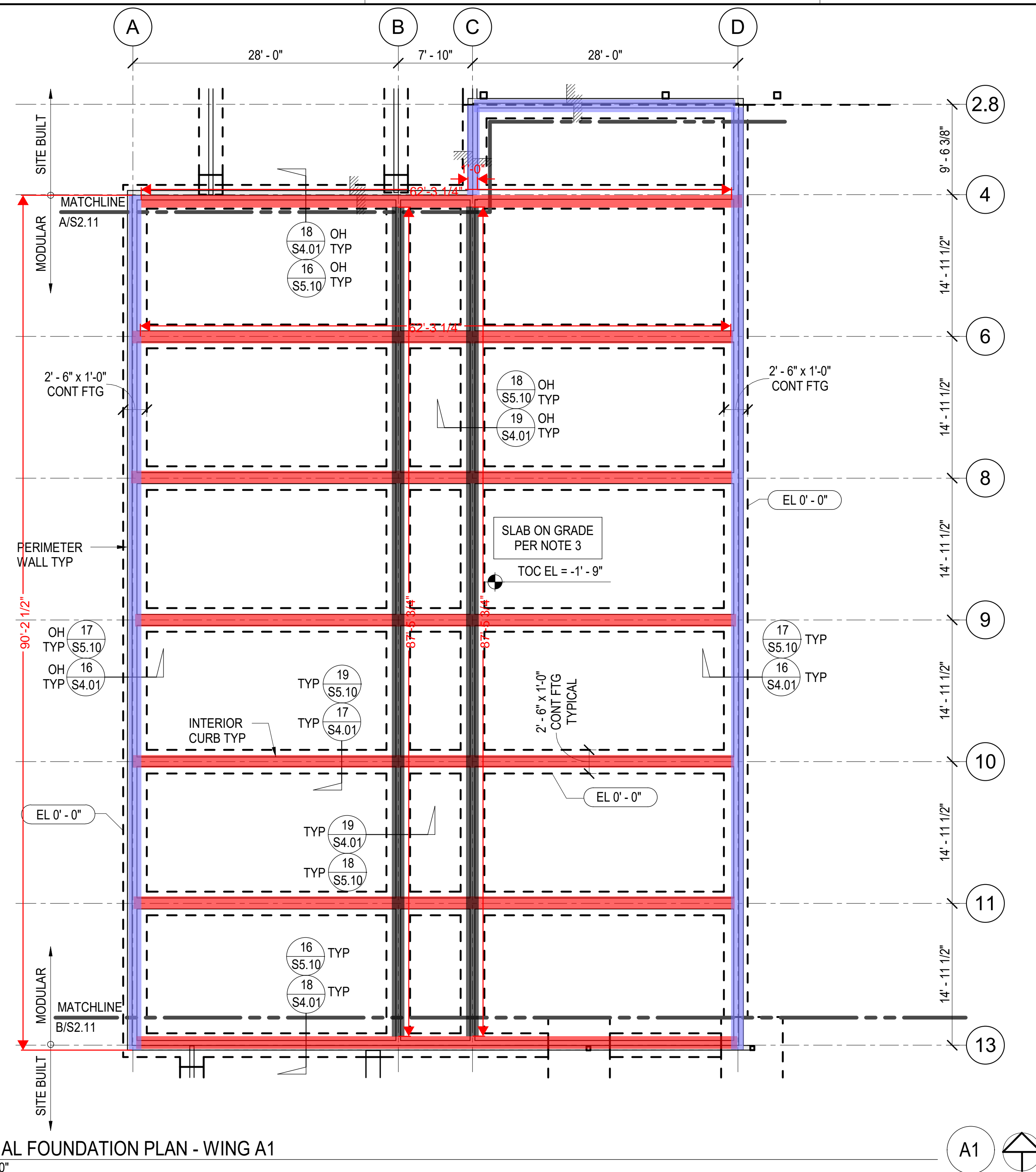
Appendix C

Structural loads as provided by John A. Martin and Associates, Inc.

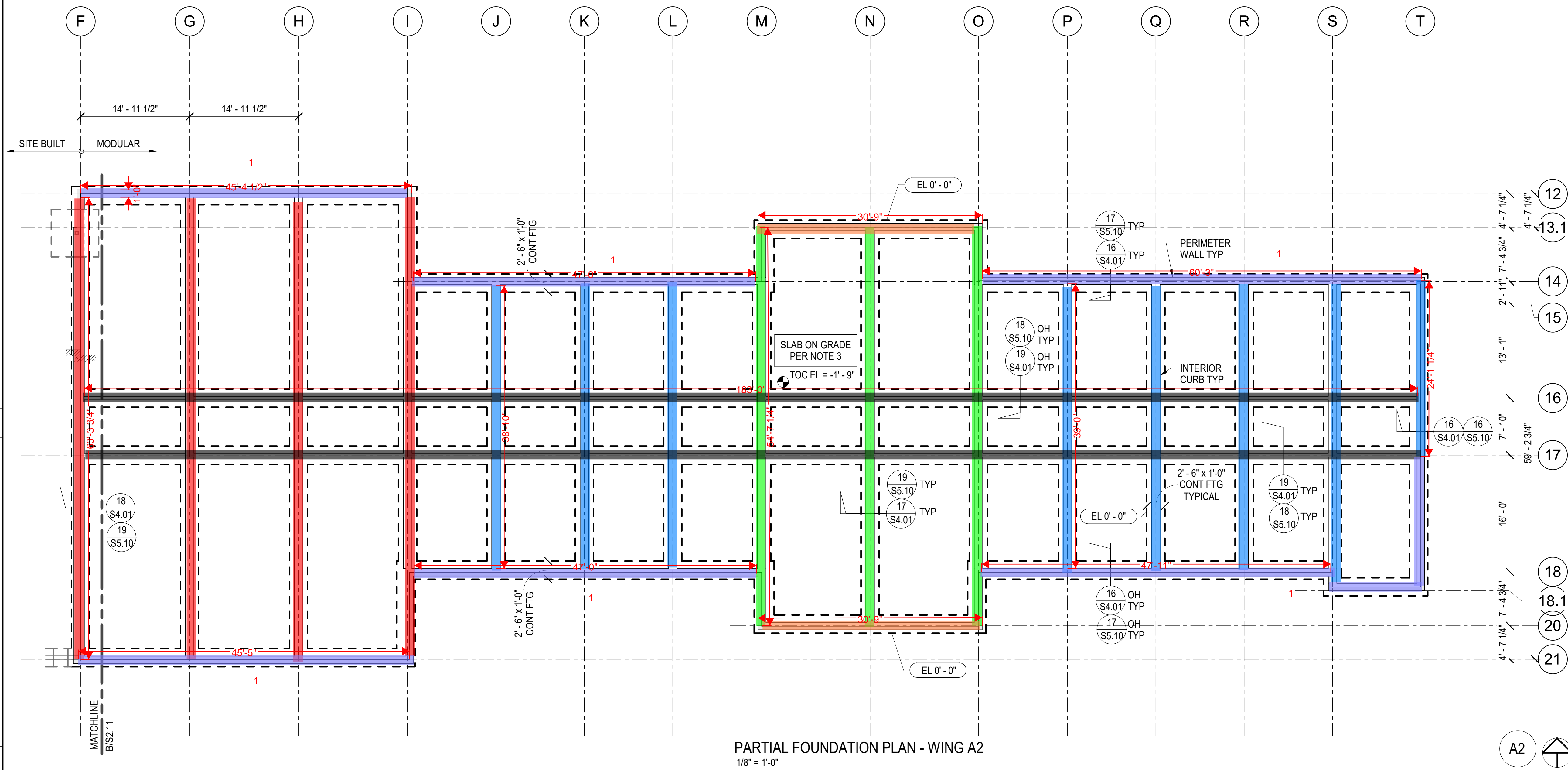
3/6/2023 5:27:09 PM Autodesk Docs://Compton College Student Housing/Compton College Student Housing_ST.rvt

LOADING DIAGRAM

- DL: 1850 plf, LL: 1148 plf, RL: 187 plf
- DL: 1622 plf, LL: 910 plf, RL: 228 plf
- DL: 2105 plf, LL: 2866 plf, RL: 287 plf
- DL: 738 plf, LL: 133 plf, RL: 15 plf
- DL: 890 plf, LL: 133 plf, RL: 15 plf
- DL: 687 plf, LL: 817 plf, RL: 82 plf



PARTIAL FOUNDATION PLAN - WING A1
1/8" = 1'-0"



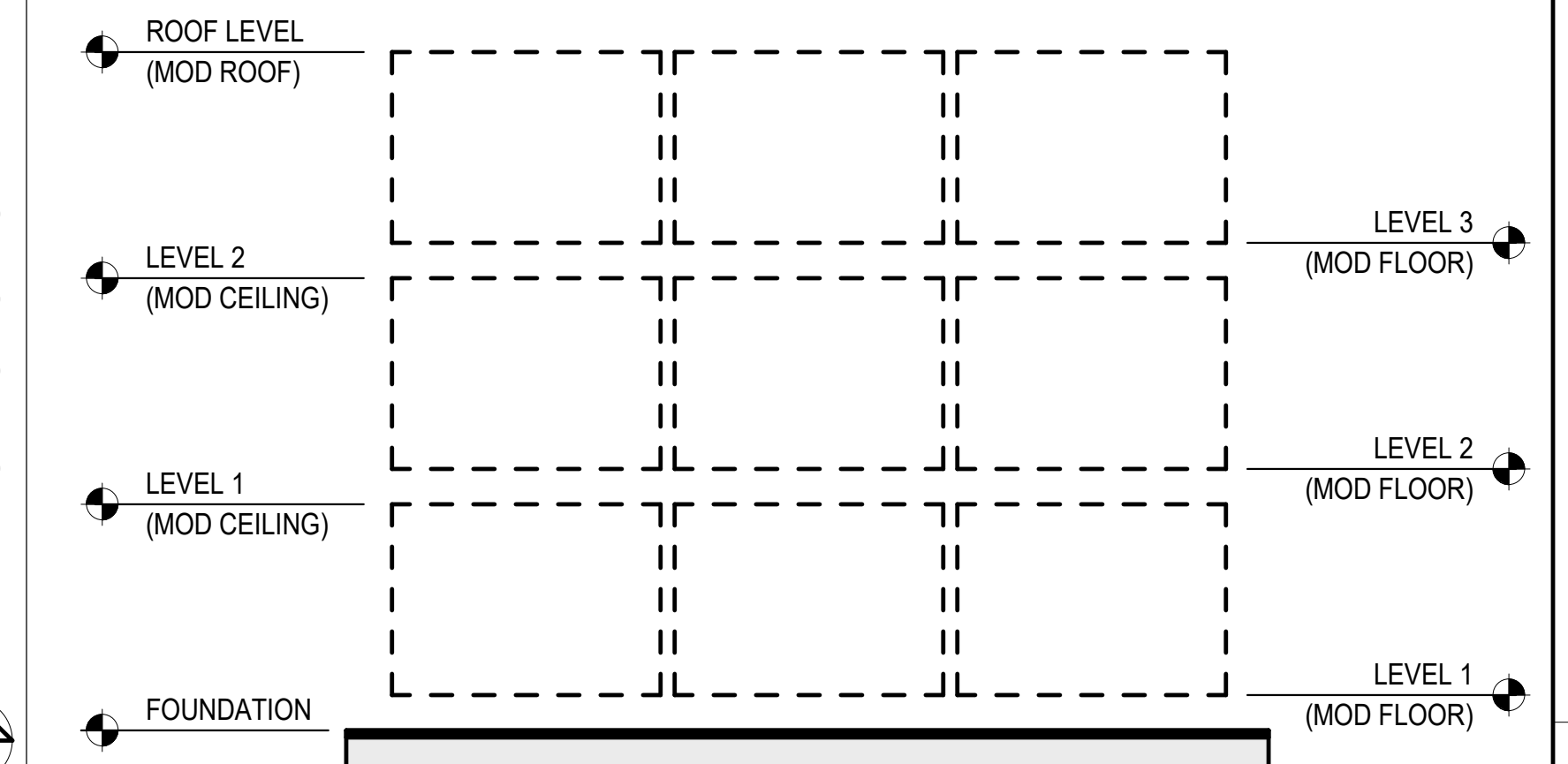
PARTIAL FOUNDATION PLAN - WING A2
1/8" = 1'-0"

PLAN NOTES:

1. VERIFY ALL DIMENSIONS WITH ARCHITECTURAL DRAWINGS.
2. FOR GENERAL NOTES AND TYPICAL DETAILS, SEE SHEETS S0.01 THRU S1.12.
3. SLAB ON GRADE: 5" THICK WITH #4@18" O.C. EACH WAY TOP OVER SUB-GRADE PER SOILS ENGINEER.

LEGEND:

- XX-X- TOP OF FOUNDATION ELEVATION (FROM TOP OF FINISHED FLOOR).
- CHANGE IN MAT FOOTING ELEVATION
- INDICATES UNDERGROUND UTILITIES SHOWN FOR CONVENIENCE ONLY. COORDINATE WITH MECHANICAL, ELECTRICAL AND PLUMBING SUBCONTRACTORS. STEP BOTTOM OF FOOTING AS REQUIRED PER XX.S.XX AND XX.S.XX.



DSA STAMP



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J22193

PROJECT TITLE

COMPTON COLLEGE
STUDENT HOUSING
INCREMENT 2 OF 2 - BUILDING & ASSOCIATED
SITE WORK
1111 E. ARTESIA BLVD COMPTON, CA 90221



ISSUED		
#	DATE	DESCRIPTION
1	11/08/2022	DSA PRE-APPLICATION
2	01/14/2023	DESIGN DEVELOPMENT
3	02/13/2023	50% CD PROGRESS SET
4	03/13/2023	75% CD SUBMITTAL

PROJECT IDENTIFICATION

THE DRAWINGS IN THE SHEET INDEX WERE ORIGINALLY CREATED IN AUTOCAD REV. 2018 UNLESS OTHERWISE NOTED.
THE ORIGINAL SIZE OF THIS SHEET IS 30" X 42".
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SHEET TITLE

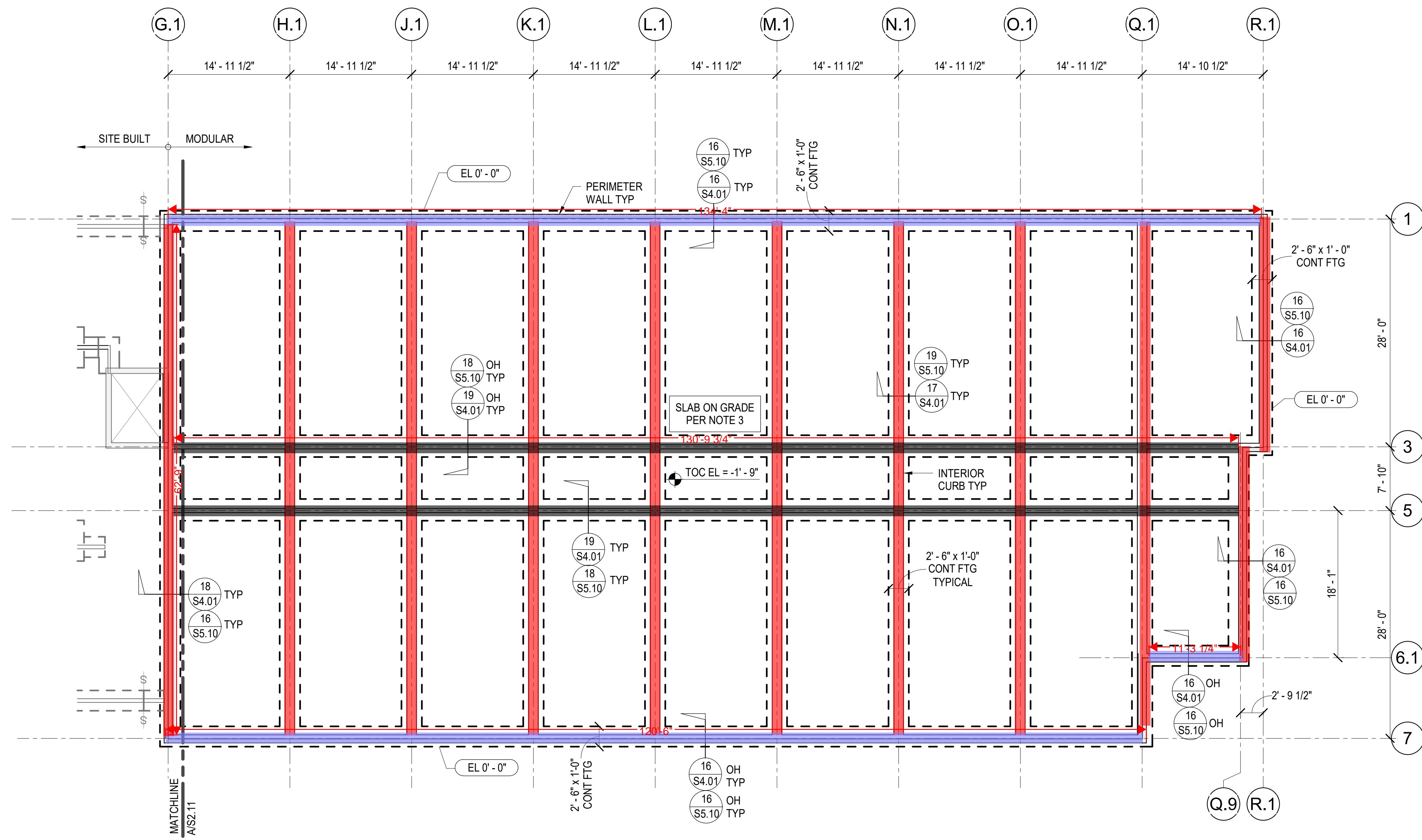
SITE BUILT FOUNDATION
PLAN - WING A

SHEET NUMBER

S2.21

75% CD SUBMITTAL
NOT FOR CONSTRUCTION

3/6/2023 5:27:43 PM Autodesk Docs://Compton College Student Housing/Compton College Student Housing_S1.rvt



PARTIAL FOUNDATION PLAN - WING B
1/8" = 1'-0"

PLAN NOTES:

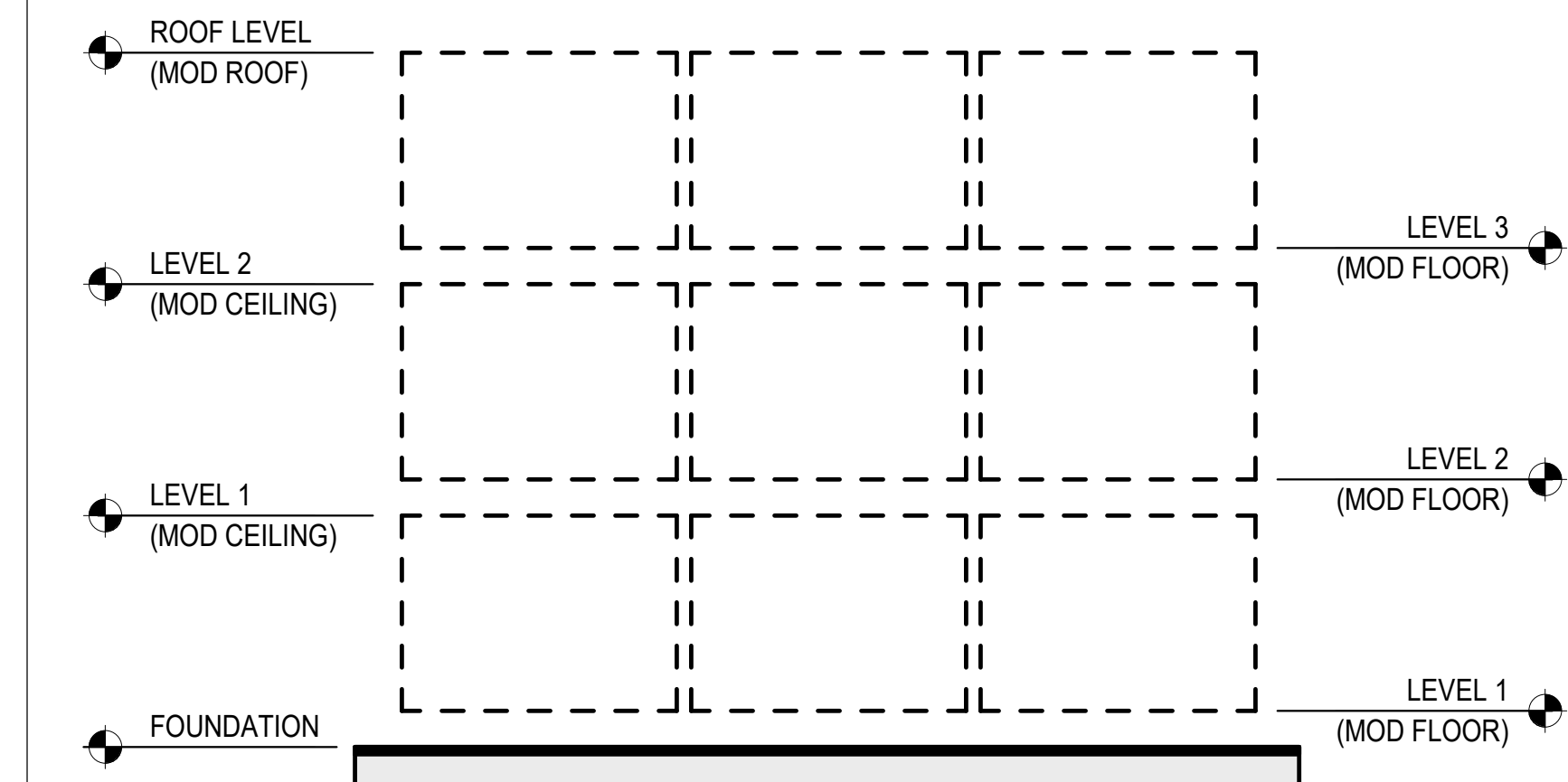
1. VERIFY ALL DIMENSIONS WITH ARCHITECTURAL DRAWINGS.
2. FOR GENERAL NOTES AND TYPICAL DETAILS, SEE SHEETS S0.01 THRU S1.12.
3. SLAB ON GRADE: 5" THICK WITH #4@18" O.C. EACH WAY TOP OVER SUB-GRADE PER SOILS ENGINEER.

LEGEND:

- XXX-X- TOP OF FOUNDATION ELEVATION (FROM TOP OF FINISHED FLOOR).
- Change in MAT FOOTING ELEVATION
- x-x-x- INDICATES UNDERGROUND UTILITIES SHOWN FOR CONVENIENCE ONLY, COORDINATE WITH MECHANICAL, ELECTRICAL, AND PLUMBING SUBCONTRACTORS. STEP BOTTOM OF FOOTING AS REQUIRED PER XX.S.XX AND XX.S.XX.

LOADING DIAGRAM

- DL: 1850 plf, LL: 1148 plf, RL: 187 plf
- DL: 738 plf, LL: 133 plf, RL: 15 plf
- DL: 687 plf, LL: 817 plf, RL: 82 plf



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SEAL

CONSULTANTS:

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Phone (213) 483-6490
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J22193

PROJECT TITLE
**COMPTON COLLEGE
STUDENT HOUSING**
INCREMENT 2 OF 2 - BUILDING & ASSOCIATED
SITE WORK
1111 E. ARTESIA BLVD COMPTON, CA 90221



ISSUED	
#	DESCRIPTION
1	11/08/2022 DSA PRE-APPLICATION
2	01/14/2023 DESIGN DEVELOPMENT
3	02/13/2023 50% CD PROGRESS SET
4	03/13/2023 75% CD SUBMITTAL

PROJECT IDENTIFICATION

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SHEET TITLE
SITE BUILT FOUNDATION
PLAN - WING B

SHEET NUMBER

S2.31

75% CD SUBMITTAL
NOT FOR CONSTRUCTION

Appendix D

Bearing capacity and DSM design calculations

Soil Mixing Design Properties

Design Strength of Soil Mixing

Column diameter	$D_{col} := 3 \text{ ft}$	
Column area	$A_{col} := \frac{\pi \cdot D_{col}^2}{4}$	
Design average 28-day unconfined compressive strength	$UCS_{28day} := 150 \text{ psi}$	average of test specimens to be equal to or greater than this value
Reduction for unmixed inclusions	$f_r := .9$	

Static design

Curing time	$t_{cure} := 180 \text{ day}$
Curing factor	$f_c := 0.187 \cdot \ln\left(\frac{t_{cure}}{\text{day}}\right) + 0.375 = 1.35$
UCS for design	$UCS_{Stat} := f_c \cdot UCS_{28day} = 201.9 \text{ psi}$
DSM shear strength	$S_{dm} := \frac{1}{2} \cdot f_r \cdot f_c \cdot UCS_{28day} = 13084 \text{ psf}$
Young's modulus of DSM	$E_{DSM} := 300 \cdot f_r \cdot f_c \cdot UCS_{28day} = 7850 \text{ ksf}$

Seismic design

Curing time	$t_{cureSeis} := 365 \text{ day}$
Curing factor	$f_{c_Seis} := 0.187 \cdot \ln\left(\frac{t_{cureSeis}}{\text{day}}\right) + 0.375 = 1.48$
UCS for design	$UCS_{Seis} := f_r \cdot f_{c_Seis} \cdot UCS_{28day} = 199.6 \text{ psi}$

Footing and load information

Footing width, B	Eccentricity in "B" direction, e_B	Area replacement ratio, ARR
Footing length, L	Eccentricity in "L" direction, e_L	Depth of ground improvement, Z_{GI}
Embedment depth, D	Bearing pressure, q_{applied}	
Slope of footing, α_b	Base shear, Q_{tr}	

CaseID	B (ft)	L (ft)	D (in)	α _b (°)	e _B (in)	e _L (in)	q _{applied} (psf)	Q _{tr} (kip)	ARR	Z _{GI} (ft)
"Strip"	2.5	100	20	0	0	0	2000	0	100%	20
"Braced Frame"	8	100	20	0	0	0	2000	0	30%	20
"F1"	5	5	24	0	0	0	2000	0	30%	20
"F2"	6.5	6.5	24	0	0	0	2000	0	30%	20
"F3"	4	4	24	0	0	0	2000	0	30%	20
"F4"	9	9	24	0	0	0	2000	0	30%	20

Index for calculations $i := 1 \dots \text{length}(\text{CaseID})$

Crushing Capacity Calculation

Design average 28-day unconfined compressive strength

$$UCS_{28day} = 150 \text{ psi}$$

UCS for design

$$UCS_{Stat} = 201.9 \text{ psi}$$

Applied loads per footing and associated area replacement ratio

$$CaseID = \begin{bmatrix} \text{"Strip"} \\ \text{"Braced Frame"} \\ \text{"F1"} \\ \text{"F2"} \\ \text{"F3"} \\ \text{"F4"} \end{bmatrix} \quad q_{applied} = \begin{bmatrix} 2000 \\ 2000 \\ 2000 \\ 2000 \\ 2000 \\ 2000 \end{bmatrix} \text{ psf} \quad ARR = \begin{bmatrix} 100\% \\ 30\% \\ 30\% \\ 30\% \\ 30\% \\ 30\% \end{bmatrix}$$

Factor of safety against crushing

$$FS_{crushing_i} := \frac{ARR_i \cdot UCS_{Stat}}{q_{applied_i}} = \begin{bmatrix} 14.5 \\ 4.4 \\ 4.4 \\ 4.4 \\ 4.4 \\ 4.4 \end{bmatrix}$$

Geotechnical Bearing Capacity

per AASHTO (2012)

Length of the DSM column

$$Z_{G_i} = \begin{bmatrix} 20 \\ 20 \\ 20 \\ 20 \\ 20 \\ 20 \end{bmatrix} \text{ ft}$$

Column diameter

$$D_{col} = 3 \text{ ft}$$

$$N_{c_i} := \min \left(6 \cdot \left(1 + 0.2 \left(\frac{Z_{G_i}}{D} \right) \right), 9 \right) = \begin{bmatrix} 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \end{bmatrix}$$

Representative undrained shear strength at bottom of column

$$S_u := 2 \text{ ksf}$$

$$q_{pClay_i} := N_{c_i} \cdot S_u = \begin{bmatrix} 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \end{bmatrix} \text{ ksf}$$

Nominal unit tip resistance if column is bearing into clay

Factor of safety against crushing

$$FS_{geotech_i} := \frac{q_{pClay_i}}{q_{applied_i}} = \begin{bmatrix} 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \end{bmatrix}$$

Static Settlement Calculation

Settlement of the DSM column

Working stress at the bottom of the DSM

$$\sigma_{DSM_i} := \frac{q_{applied_i}}{ARR_i} = \begin{bmatrix} 2000 \\ 6667 \\ 6667 \\ 6667 \\ 6667 \end{bmatrix} \text{ psf}$$

Secant Young's modulus of DSM

$$E_{DSM} = 7850 \text{ ksf}$$

Elastic compression of DSM

$$\delta_{DSM_i} := \frac{\sigma_{DSM_i} \cdot Z_{G_i}}{E_{DSM}} = \begin{bmatrix} 0.1 \\ 0.2 \\ 0.2 \\ 0.2 \\ 0.2 \end{bmatrix} \text{ in}$$

Settlement below the DSM column

Equivalent diameter of DSM

$$D_{equivDSM_i} := \sqrt{\frac{4 \cdot B_i \cdot L_i \cdot ARR_i}{\pi}} = \begin{bmatrix} 17.84 \\ 17.48 \\ 3.09 \\ 4.02 \\ 2.47 \\ 5.56 \end{bmatrix} \text{ ft}$$

Shape factor

$$m_{l_s} := 1$$

Fox embedment factor

$$I_{F_i} := \begin{cases} \frac{D_{equivDSM_i}}{Z_{G_i}} > 5 \\ 0.50 \\ \text{else} \\ 0.55 \end{cases} = \begin{bmatrix} 0.55 \\ 0.55 \\ 0.55 \\ 0.55 \\ 0.55 \\ 0.55 \end{bmatrix}$$

Reduction factor

- 0.25 if axial skin resistance reduces tip load to < 0
- 0.50 if tip load > 0
- 0.75 if end-bearing only

$$F_1 := 0.5$$

Young's modulus of bearing stratum

$$E_s := 1000 \text{ ksf}$$

Poisson's ratio of bearing stratum

$$\mu_s := 0.3$$

Settlements below DSM

$$\delta_{Bot_i} := \sigma_{DSM_i} \cdot m_{l_s} \cdot I_{F_i} \cdot F_1 \cdot D_{equivDSM_i} \cdot \left(\frac{1 - \mu_s^2}{E_s} \right) = \begin{bmatrix} 0.1 \\ 0.3 \\ 0.1 \\ 0.1 \\ 0.0 \\ 0.1 \end{bmatrix} \text{ in}$$

Total settlements

$$\delta_{Total_i} := \delta_{DSM} + \delta_{Bot} = \begin{bmatrix} 0.2 \\ 0.6 \\ 0.3 \\ 0.3 \\ 0.3 \\ 0.3 \end{bmatrix} \text{ in}$$

Appendix E

Liquefaction calculations

Liquefaction Analysis and Deep Soil Mixing Mitigation

Project: CCC Student Housing

CPT ID: CPT-1

Surface Elev.: 0.0 ft (use 0 ft to plot depth instead of elevation)



by: Mudgett

Date: 2/3/2023

LIQUEFACTION ANALYSIS PARAMETERS

Triggering Method = Boulanger & Idriss (2015)

Vol. Settlement Method = Zhang et al. (2002)

Depth of GW During CPT = 52.90 ft

Depth of GW During Earthquake = 8.00 ft

Depth of Fill = 0.00 ft

Unit Weight of fill = 120 pcf

PGApr = 0.77 g

Mw = 7.30

Ic Threshold = 2.6

Use $K\sigma$? = Yes

Depth Weighting Factor

Use Df? Yes

z (ft)	Df
0	1
60	0
60.01	0
200	0

Perform Ground Improvement Analysis?: **Deep Soil Mixing**

DSM GRID DESIGN PARAMETERS

Depth Below Existing Grade = 20 ft

ARR = 30 %

S = 28 ft

Gr = 30

Rrd = PGApr/PGApr = 0.301

PGApr in Impr. Zone = 0.232 g

ADVANCED LIQUEFACTION PARAMETERS

Use Ic Transition Zones? Yes - Method 2

Manual Trans Zones?: Yes

Use Manual Thin Layer Cor.? = Yes

No. Trans. Zone Points: 6

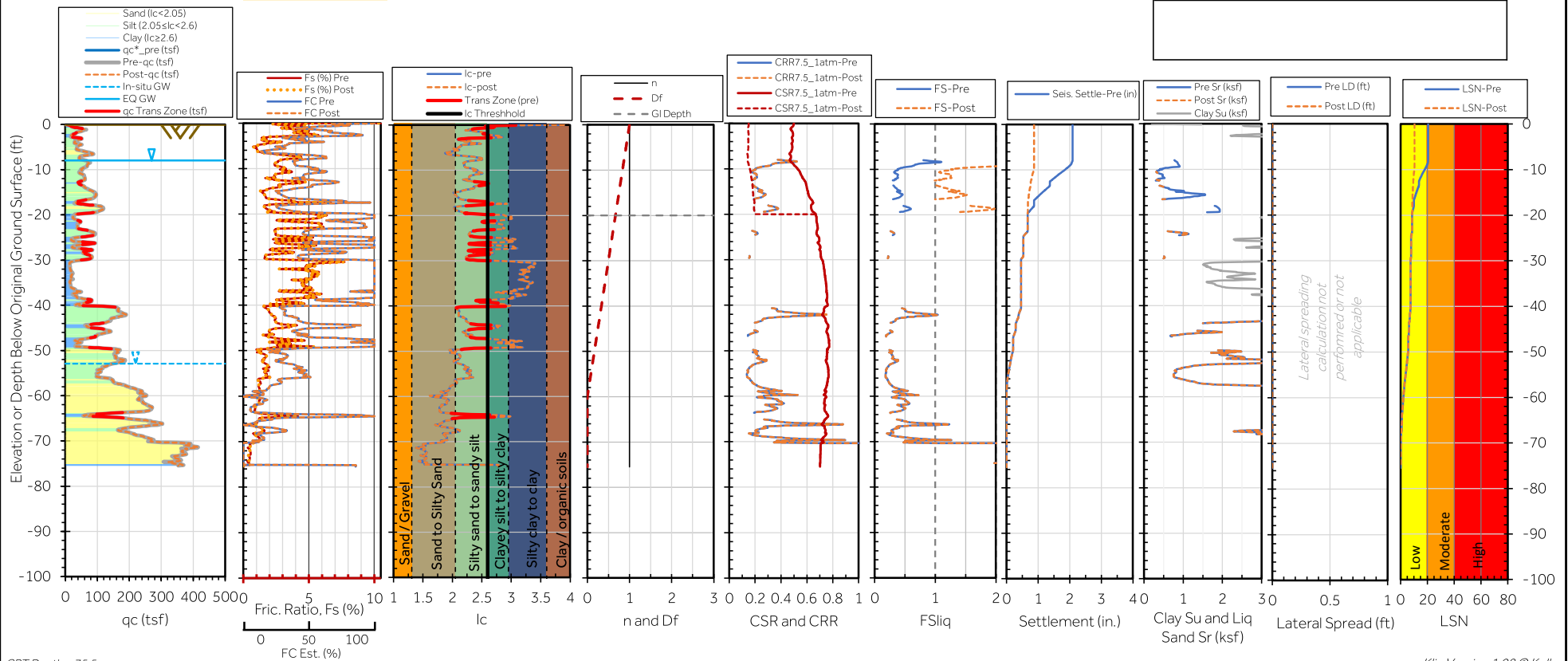
Zhang et al. (2004) Lat. Sprd? No

Ic_min and max = 1.6 4

Volumetric Settlement Results:

Existing (Pre-Treatment) Condition = 2.1 in.

Post-Improvement Condition = 0.9 in.



CPT Depth = 75.5

Kliq Version 1.08 © Keller

Liquefaction Analysis and Deep Soil Mixing Mitigation

Project: CCC Student Housing

CPT ID: CPT-2

Surface Elev.: 0.0 ft (use 0 ft to plot depth instead of elevation)



by: Mudgett
Date: 2/3/2023

LIQUEFACTION ANALYSIS PARAMETERS

Triggering Method = Boulanger & Idriss (2015)

Vol. Settlement Method = Zhang et al. (2002)

Depth of GW During CPT = 52.90 ft

Depth of GW During Earthquake = 8.00 ft

Depth of Fill = 0.00 ft

Unit Weight of fill = 120 pcf

PGApr = 0.77 g

Mw = 7.30

Ic Threshold = 2.6

Use K_σ? = Yes

Depth Weighting Factor

Use Df? Yes

z (ft)	Df
0	1
60	0
60.01	0
200	0

Perform Ground Improvement Analysis?: **Deep Soil Mixing**

DSM GRID DESIGN PARAMETERS

Depth Below Existing Grade = 20 ft

ARR = 30 %

S = 28 ft

Gr = 30

Rrd = PGApr/PGApost = 0.301

PGApost in Impr. Zone = 0.232 g

ADVANCED LIQUEFACTION PARAMETERS

Use Ic Transition Zones? Yes - Method 2

Manual Trans Zones? Yes

Use Manual Thin Layer Cor.? = Yes

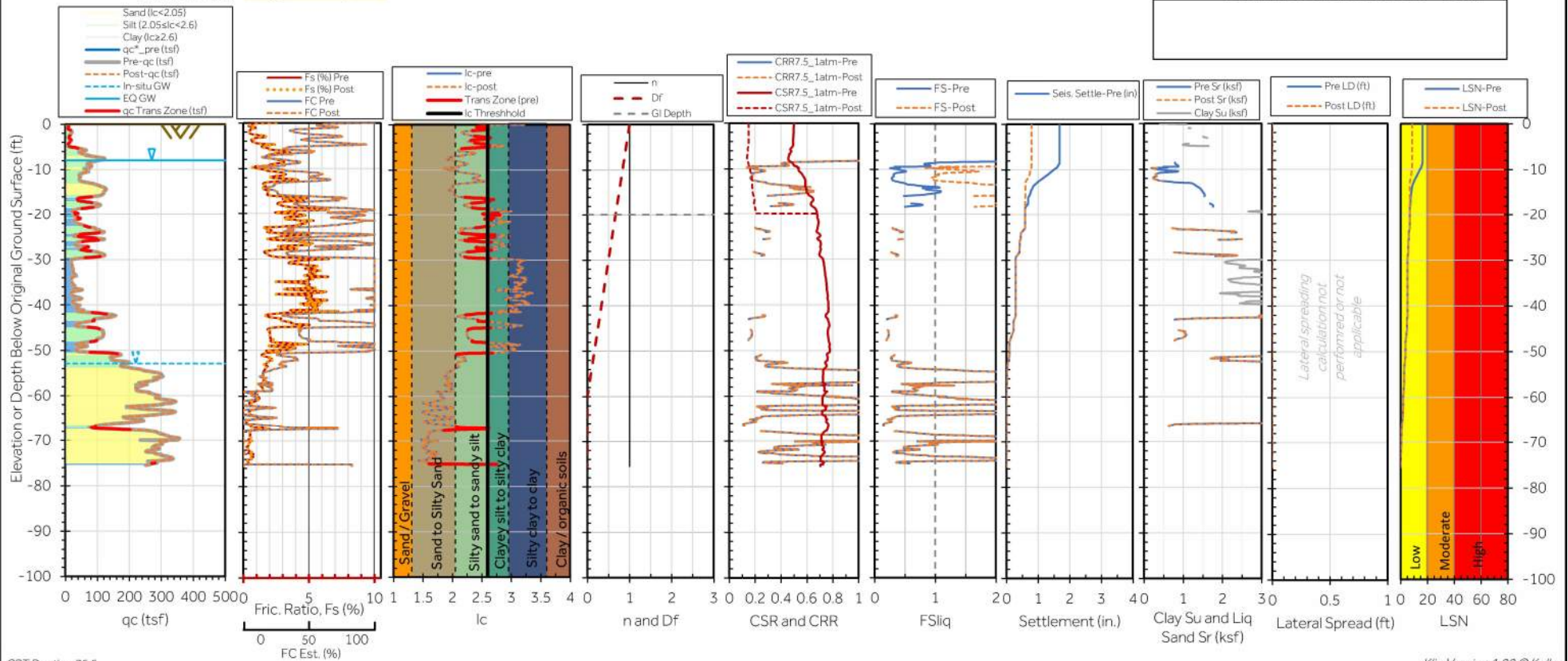
No. Trans. Zone Points: 6 Zhang et al. (2004) Lat. Sprd? No

Ic_min and max = 1.6 4

Volumetric Settlement Results:

Existing (Pre-Treatment) Condition = 1.7 in.

Post-Improvement Condition = 0.8 in.



CPT Depth = 75.5

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Liquefaction Analysis and Deep Soil Mixing Mitigation

Project: CCC Student Housing

CPT ID: CPT-4

Surface Elev.: 0.0 ft (use 0 ft to plot depth instead of elevation)



by: Mudgett
Date: 2/3/2023

LIQUEFACTION ANALYSIS PARAMETERS

Triggering Method = Boulanger & Idriss (2015)
 Vol. Settlement Method = Zhang et al. (2002)
 Depth of GW During CPT = 52.90 ft
 Depth of GW During Earthquake = 8.00 ft
 Depth of Fill = 0.00 ft
 Unit Weight of fill = 120 pcf
 PGApr = 0.77 g
 Mw = 7.30
 Ic Threshold = 2.6
 Use $K\sigma$? = Yes

Depth Weighting Factor
 Use Df? Yes

z (ft)	Df
0	1
60	0
60.01	0
200	0

Perform Ground Improvement Analysis?: **Deep Soil Mixing**

DSM GRID DESIGN PARAMETERS

Depth Below Existing Grade = 20 ft
 ARR = 30 %
 S = 28 ft
 Gr = 30

Rrd = PGApr/PGApr = 0.301
 PGApr in Impr. Zone = 0.232 g

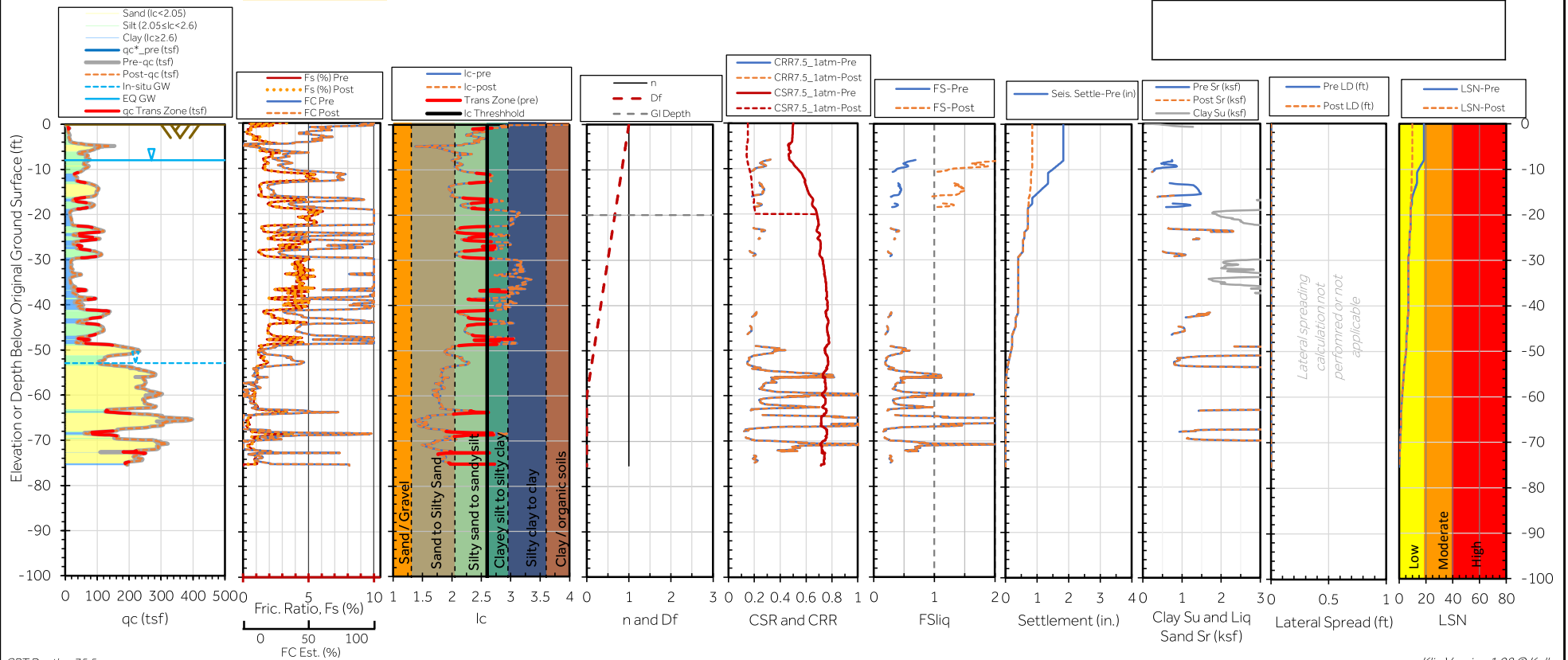
ADVANCED LIQUEFACTION PARAMETERS

Use Ic Transition Zones? Yes - Method 2
 Manual Trans Zones?: Yes
 Use Manual Thin Layer Cor.? = Yes

No. Trans. Zone Points: 6 Zhang et al. (2004) Lat. Sprd? No
 Ic_min and max = 1.6 4

Volumetric Settlement Results:

Existing (Pre-Treatment) Condition = 1.8 in.
 Post-Improvement Condition = 0.9 in.



CPT Depth = 75.5

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Liquefaction Mitigation from Shear Reinforcement

per Nguyen et al. (2013)

Design Strength of Soil Mixing

Column length	$H := 20 \text{ ft}$
Typical panel spacing	$S := 28 \text{ ft}$
Overall area replacement ratio	$ARR := 30\%$
Secant Young's modulus of DSM for seismic loads	$E_{50DSM_seis} := 300 \cdot UCS_{Seis} = (8.62 \cdot 10^3) \text{ ksf}$
Assumed secant Young's modulus of native soil	$E_{50soil} := 800 \text{ ksf}$
Seismic modulus reduction factor	$f_{soft} := .3$
"Softened" Young's modulus of native soil during seismic event	$E_{soil_seis} := f_{soft} \cdot E_{50soil}$
Modulus ratio between DSM and native soil	$Gr := \frac{E_{50DSM_seis}}{E_{soil_seis}} = 35.92$
	$Gr := 30$ used 30 for design
Unreinforced shear strain ratio	$\gamma_r := \left(1 - (1 - ARR)^{1.3} \cdot \left(\frac{Gr - 1}{185} \right)^{0.4} \right) \cdot \min \left(\frac{H}{S}, 1 \right) = 0.5$
Effective shear factor	$C_G := 1 - 0.5 \cdot \sqrt{1 - ARR} = 0.58$
Shear stress reduction ratio	$Rrd := \min \left(\left(\frac{1}{Gr \cdot \left(ARR \cdot C_G \cdot \gamma_r + \frac{(1 - ARR)}{Gr} \right)} \right), 1 \right) = 0.301$